

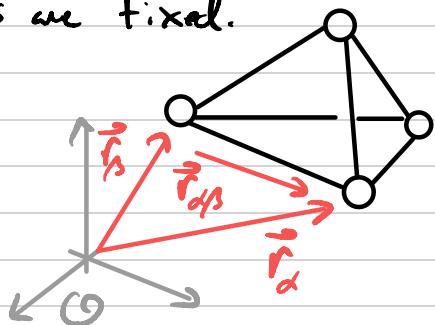
Physics 303
Classical Mechanics II

Rigid Body Motion

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Rigid Bodies

A rigid body is an abstract notion of a collection of particles / objects that move together in such a way to maintain their shape, i.e., their relative positions are fixed.



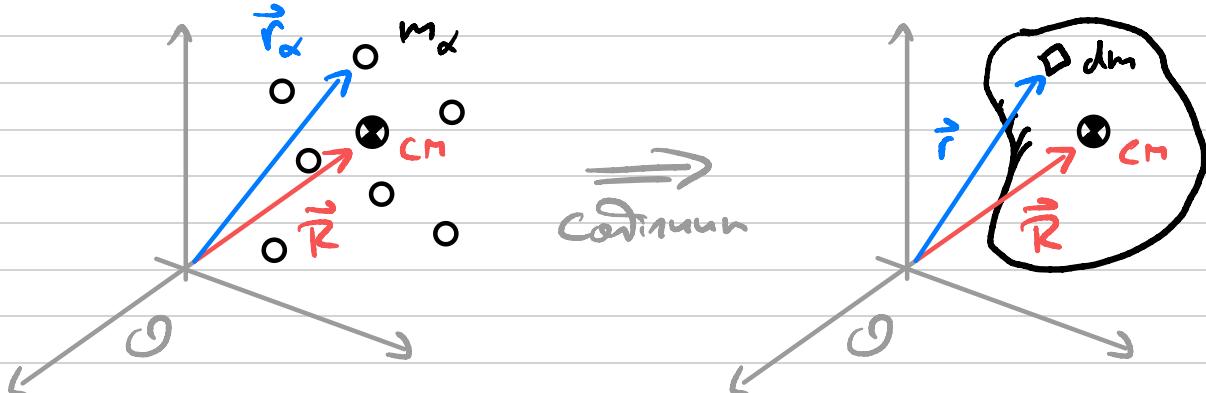
$$\vec{r}_{\alpha\beta} = \vec{r}_\alpha - \vec{r}_\beta \\ \Rightarrow |\vec{r}_{\alpha\beta}| = \text{constant}$$

This is an idealization, as atoms and molecules vibrate meaning no object is completely rigid. However, this is a good starting point to build on.

Since the distances between particles are fixed, the system is highly constrained. For N particles, there are $3N$ coordinates needed. But, since the distances between particles is fixed, the rigid body only needs 6 degrees of freedom.

- 3 to specify CM
- 3 to specify orientation

Consider system of N particles $\alpha = 1, \dots, N$ with masses m_α and positions \vec{r}_α measured w.r.t. O



The CM is

$$\vec{R} = \frac{1}{M} \sum_{\alpha=1}^N m_\alpha \vec{r}_\alpha , \quad M = \sum_\alpha m_\alpha$$

If the particles are small and numerous in a small volume, we can define a density $\rho(\vec{r})$ as

$$\Delta m = \rho(\vec{r}) \Delta x \Delta y \Delta z$$

then we can consider the rigid body of a continuous distribution of mass

$$M = \int dm = \int \rho(\vec{r}) dV$$

and CM

$$\vec{R} = \frac{1}{M} \int \vec{r} dm$$

We will switch between a discrete and continuous picture as needed.

Momentum & Angular Momentum

The total momentum of the system is

$$\vec{P} = \sum_{\alpha} \vec{p}_{\alpha} = \sum_{\alpha} m_{\alpha} \dot{\vec{r}}_{\alpha} = M \dot{\vec{R}}$$

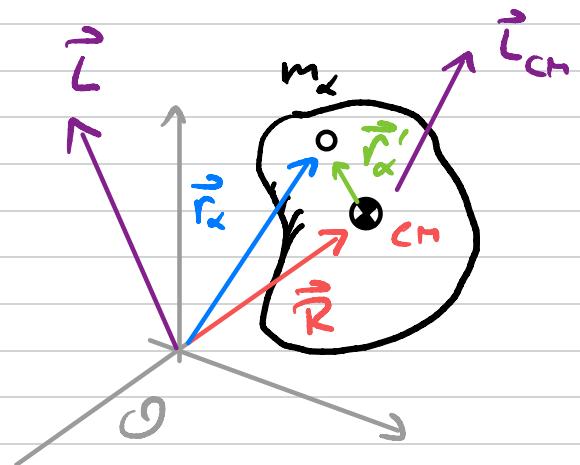
If the system is exposed to an external force \vec{F}^{ext} , then NII for the CM is

$$\ddot{\vec{P}} = \vec{F}^{\text{ext}} = M \ddot{\vec{R}}$$

Next we consider angular momentum.

Let \vec{l} be the angular momentum of the system w.r.t O.

We want to split \vec{l} into an \vec{l}_{CM} , the angular momentum of the body about the CM, and the \vec{l}_{ext} , the angular momentum of the CM.



The angular momentum of α about O is

$$\vec{l}_{\alpha} = \vec{r}_{\alpha} \times \vec{p}_{\alpha} = \vec{r}_{\alpha} \times m_{\alpha} \dot{\vec{r}}_{\alpha}$$

So the total angular momentum is $\vec{l} = \sum_{\alpha} \vec{l}_{\alpha}$

$$\text{So, } \vec{L} = \sum_{\alpha} \vec{l}_{\alpha} = \sum_{\alpha} \vec{r}_{\alpha} \times m_{\alpha} \dot{\vec{r}}_{\alpha}$$

Now, let \vec{r}'_{α} be location of α w.r.t. CM

$$\vec{r}_{\alpha} = \vec{R} + \vec{r}'_{\alpha}$$

So, find

$$\begin{aligned} \vec{L} &= \sum_{\alpha} (\vec{R} + \vec{r}'_{\alpha}) \times m_{\alpha} (\dot{\vec{R}} + \dot{\vec{r}}'_{\alpha}) \\ &= \sum_{\alpha} \vec{R} \times m_{\alpha} \dot{\vec{R}} + \sum_{\alpha} \vec{R} \times m_{\alpha} \dot{\vec{r}}'_{\alpha} \\ &\quad + \sum_{\alpha} \vec{r}'_{\alpha} \times m_{\alpha} \dot{\vec{R}} + \sum_{\alpha} \vec{r}'_{\alpha} \times m_{\alpha} \dot{\vec{r}}'_{\alpha} \end{aligned}$$

$$\text{Recall } M = \sum_{\alpha} m_{\alpha}$$

$$\begin{aligned} \Rightarrow \vec{L} &= \vec{R} \times M \dot{\vec{R}} + \vec{R} \times \sum_{\alpha} m_{\alpha} \dot{\vec{r}}'_{\alpha} \\ &\quad + \left(\sum_{\alpha} m_{\alpha} \vec{r}'_{\alpha} \right) \times \dot{\vec{R}} + \sum_{\alpha} \vec{r}'_{\alpha} \times m_{\alpha} \dot{\vec{r}}'_{\alpha} \end{aligned}$$

Now, $\sum_{\alpha} m_{\alpha} \vec{r}'_{\alpha} = \vec{0}$ since this is location of CM
relative to CM (of course)

like wise,
 $\sum_{\alpha} m_{\alpha} \dot{\vec{r}}'_{\alpha} = \vec{0}$

$$\text{So, } \vec{L} = \vec{R} \times \vec{P} + \sum_{\alpha} \vec{r}_{\alpha}' \times m_{\alpha} \dot{\vec{r}}_{\alpha}'$$

↑
angular momentum of CM
relative to O

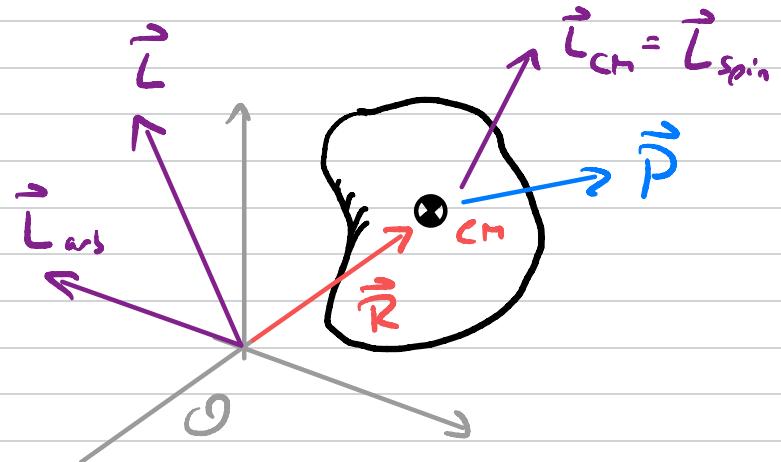
↑
angular momentum relative
to the CM

Define

$$\boxed{\vec{L}_{CM} = \vec{L}_{Spin} = \sum_{\alpha} \vec{r}_{\alpha}' \times m_{\alpha} \dot{\vec{r}}_{\alpha}'}$$

$$\boxed{\vec{L}_{orb} = \vec{R} \times \vec{P}}$$

$$\Rightarrow \boxed{\vec{L} = \vec{L}_{orb} + \vec{L}_{CM}}$$



This separation is often useful

as both are approximately conserved

$$\dot{\vec{L}}_{orb} = \dot{\vec{R}} \times \vec{P} + \vec{R} \times \dot{\vec{P}} = \vec{R} \times \vec{F}_{ext}^{\alpha} ; \quad \vec{F}_{ext}^{\alpha} = \sum_{\alpha} \vec{F}_{\alpha}^{\alpha}$$

We know $\dot{\vec{L}} = \vec{\tau}^{\alpha}$, the external torque relative to O

$$\begin{aligned} \text{So, } \dot{\vec{L}}_{CM} &= \dot{\vec{L}} - \dot{\vec{L}}_{orb} = \vec{\tau}^{\alpha} - \vec{R} \times \vec{F}_{ext}^{\alpha} \\ &= \sum_{\alpha} (\vec{r}_{\alpha} - \vec{R}) \times \vec{F}_{\alpha}^{\alpha} = \vec{\tau}_{CM}^{\alpha} \end{aligned}$$

↑
External torque relative to CM

Kinetic & Potential Energy

The total kinetic energy of N particles is

$$T = \sum_{\alpha=1}^N \frac{1}{2} m_{\alpha} \dot{\vec{r}}_{\alpha}^2$$

As before, write $\vec{r}_{\alpha} = \vec{R} + \vec{r}'_{\alpha}$, \vec{r}'_{α} position relative to CM

$$\Rightarrow \dot{\vec{r}}_{\alpha}^2 = \dot{\vec{R}}^2 + \dot{\vec{r}}'^2_{\alpha} + 2\vec{R} \cdot \vec{r}'_{\alpha}$$

$$\Rightarrow T = \frac{1}{2} \sum_{\alpha} m_{\alpha} \dot{\vec{R}}^2 + \frac{1}{2} \sum_{\alpha} m_{\alpha} \dot{\vec{r}}'^2_{\alpha} + \dot{\vec{R}} \cdot \underbrace{\sum_{\alpha} m_{\alpha} \vec{r}'_{\alpha}}_{=0 \text{ as before}}$$

Define KE relative to CM

$$T_{CM} = \frac{1}{2} \sum_{\alpha} m_{\alpha} \dot{\vec{r}}'^2_{\alpha}$$

So,

$$T = \frac{1}{2} M \dot{\vec{R}}^2 + T_{CM}$$

KE of CM

For conservative forces, can write potential energy
and decompose as

$$U = U_{\text{ext}} + U_{\text{int}}$$

$$\begin{matrix} \uparrow & \uparrow \\ \text{(external) PE} & \text{(internal) PE} \end{matrix}$$

where $U_{\text{int}} = \sum_{\alpha < \beta} U_{\alpha\beta} (|\vec{r}_\alpha - \vec{r}_\beta|)$

assuming central forces

since $|\vec{r}_{\alpha\beta}| = \text{const.}$,

$$\Rightarrow U_{\text{int}} = \text{const.}$$

$\therefore U_{\text{int}}$ is irrelevant for rigid body dynamics

Rotation about a fixed Axis

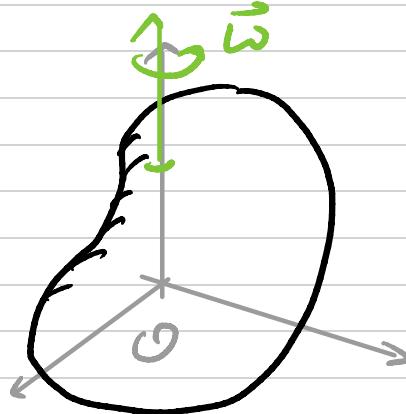
Here we consider the rotation of a rigid body about some fixed axis. Since the axis is fixed, let us define it as the z-axis.

$$\Rightarrow \vec{\omega} = (0, 0, \omega)$$

If the body consists of N particles, then

$$\vec{l} = \sum_{\alpha} \vec{l}_{\alpha}$$

$$= \sum_{\alpha} \vec{r}_{\alpha} \times m_{\alpha} \vec{v}_{\alpha}$$



Since the axis of rotation is fixed, $\vec{v}_{\alpha} = \vec{\omega} \times \vec{r}_{\alpha}$,
so, with $\vec{r}_{\alpha} = (x_{\alpha}, y_{\alpha}, z_{\alpha})$

$$\Rightarrow \vec{v}_{\alpha} = (-\omega y_{\alpha}, \omega x_{\alpha}, 0)$$

$$\therefore \vec{l}_{\alpha} = m_{\alpha} \vec{r}_{\alpha} \times \vec{v}_{\alpha}$$

$$= m_{\alpha} \omega (-z_{\alpha} x_{\alpha}, -z_{\alpha} y_{\alpha}, x_{\alpha}^2 + y_{\alpha}^2)$$

thus, $\vec{l} = \sum_{\alpha} \vec{l}_{\alpha}$ is total angular momentum.

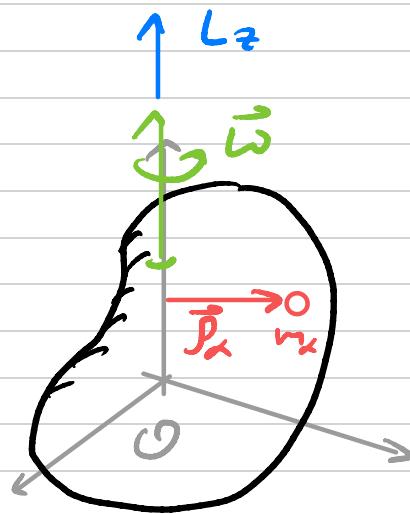
Let's examine components of \vec{L} .

The z -component is

$$L_z = \sum_{\alpha} m_{\alpha} (x_{\alpha}^2 + y_{\alpha}^2) \omega$$

Notice that

$$\rho_{\alpha}^2 = x_{\alpha}^2 + y_{\alpha}^2$$



with ρ_{α} being the distance
to any point from the z -axis.

Thus, $L_z = \sum_{\alpha} m_{\alpha} \rho_{\alpha}^2 \omega \equiv I_z \omega$

where $I_z = \sum_{\alpha} m_{\alpha} \rho_{\alpha}^2$

is the moment of inertia about the z -axis.

The kinetic energy is then

$$T = \frac{1}{2} \sum_{\alpha} m_{\alpha} v_{\alpha}^2 .$$

Since $v_{\alpha} = \rho_{\alpha} \omega$ for a rotation about fixed z -axis,

$$\Rightarrow T = \frac{1}{2} \sum_{\alpha} m_{\alpha} \rho_{\alpha}^2 \omega^2 = \frac{1}{2} I_z \omega^2 .$$

These should be familiar results from Phys 201.

Notice though that there is non-zero components for L_x & L_y ,

$$L_x = - \sum_{\alpha} m_{\alpha} x_{\alpha} z_{\alpha} \omega$$

$$L_y = - \sum_{\alpha} m_{\alpha} y_{\alpha} z_{\alpha} \omega$$

we define the products of inertia about the z -axis as

$$L_x = I_{xz} \omega, \quad L_y = I_{yz} \omega$$

with $I_{xz} = - \sum_{\alpha} m_{\alpha} x_{\alpha} z_{\alpha}$

$$I_{yz} = - \sum_{\alpha} m_{\alpha} y_{\alpha} z_{\alpha}$$

Obviously, \vec{L} is not parallel to $\vec{\omega}$!

$$\vec{L} = (I_{xz} \omega, I_{yz} \omega, I_{zz} \omega)$$

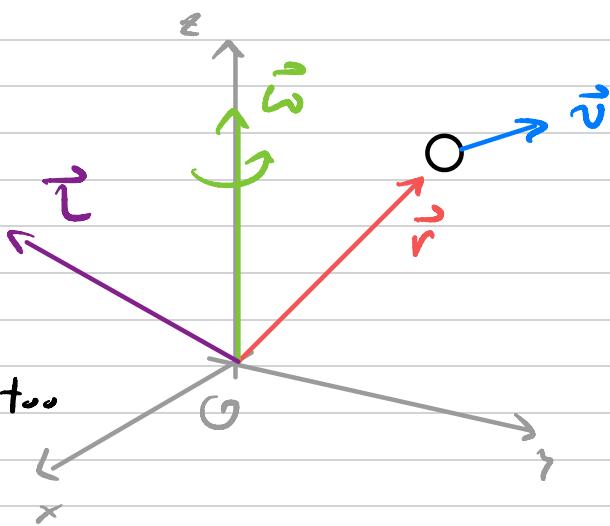
with $I_{zz} \equiv I_z$. Consider a single point particle,

$$\vec{L} = \vec{r} \times m \vec{v}$$

$$\text{if } \vec{v} \parallel -\hat{x}$$

\vec{r} lies in yz plane,

then \vec{L} lies in yz plane too.



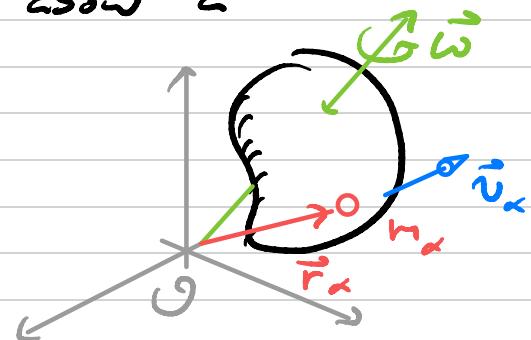
The Inertia Tensor

We saw that $\vec{L} \neq I \vec{\omega}$ with I being a number.

In general, I is a 3×3 symmetric tensor.

Let's see by consider a rotation about a general fixed axis $\vec{\omega}$.

$$\begin{aligned}\vec{L} &= \sum_{\alpha} \vec{r}_{\alpha} \times m_{\alpha} \vec{v}_{\alpha} \\ &= \sum_{\alpha} m_{\alpha} \vec{r}_{\alpha} \times (\vec{\omega} \times \vec{r}_{\alpha})\end{aligned}$$



Recall identity $\vec{A} \times (\vec{B} \times \vec{C}) = (\vec{A} \cdot \vec{C}) \vec{B} - (\vec{A} \cdot \vec{B}) \vec{C}$

$$\Rightarrow \vec{L} = \sum_{\alpha} m_{\alpha} \left[\vec{r}_{\alpha}^2 \vec{\omega} - (\vec{r}_{\alpha} \cdot \vec{\omega}) \vec{r}_{\alpha} \right]$$

(Or look at i^{th} -component,

$$\begin{aligned}L_i &= \sum_{\alpha} m_{\alpha} \left[\vec{r}_{\alpha}^2 \omega_i - \left(\sum_j r_{\alpha,j} \omega_j \right) r_{\alpha,i} \right] \\ &= \sum_j \left[\sum_{\alpha} m_{\alpha} \left(\vec{r}_{\alpha}^2 \delta_{ij} - r_{\alpha,i} r_{\alpha,j} \right) \right] \omega_j \\ &= \sum_j I_{ij} \omega_j\end{aligned}$$

we define the Inertia tensor as \mathbb{I} with matrix elements

$$I_{ij} = \sum_{\alpha} m_{\alpha} (\vec{r}_{\alpha}^2 \delta_{ij} - r_{\alpha,i} r_{\alpha,j})$$

In terms of a continuous distribution,

$$I_{ij} = \int dm (\vec{r}^2 \delta_{ij} - r_i r_j)$$

By inspection, \mathbb{I} is symmetric, $\mathbb{I}^T = \mathbb{I}$

$$\text{or } I_{ij} = I_{ji}.$$

It characterizes an object's resistance to change in rotational motion

$$\vec{\mathcal{L}} = \mathbb{I} \cdot \vec{\omega} \quad \text{or} \quad L_i = \sum_j I_{ij} \omega_j$$

The Cartesian components are

$$\mathbb{I} = \begin{pmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{pmatrix}$$

$$\text{with } I_{xx} \equiv I_x = \sum_\alpha m_\alpha (\vec{r}_\alpha^2 - x_\alpha^2) = \sum_\alpha m_\alpha (y_\alpha^2 + z_\alpha^2)$$

$$I_{xy} = - \sum_\alpha m_\alpha x_\alpha y_\alpha \quad \text{etc...}$$

Explicitly, $\vec{\tau} = \mathbb{I} \cdot \vec{\omega}$ is

$$\begin{pmatrix} \tau_x \\ \tau_y \\ \tau_z \end{pmatrix} = \begin{pmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{pmatrix} \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix}$$

The media tensor is a 3×3 symmetric matrix

which must transform as $\mathbb{I}' = R \mathbb{I} R^T$

$$\text{or } I'_{ij} = \sum_{m,n} R_{im} R_{jn} I_{mn}$$

↑ rotation matrix
 C this is what makes I a tensor

To see this, note that $\vec{\tau}$ & $\vec{\omega}$ are physical vectors which must transform as $\vec{\tau}' = R \cdot \vec{\tau}$, $\vec{\omega}' = R \cdot \vec{\omega}$ under a rotation R .

$$\therefore \vec{\tau}' = R \cdot \vec{\tau} = R \cdot \mathbb{I} \cdot \vec{\omega}$$

$$\begin{aligned} &= R \cdot \mathbb{I} \cdot R^T R \vec{\omega} && \text{C insert } 1 = R^{-1} \cdot R \\ &= (R \cdot \mathbb{I} \cdot R^T) \cdot \vec{\omega}' && = R^T \cdot R \text{ since} \\ &= \mathbb{I}' \cdot \vec{\omega}' && \text{R is orthogonal} \end{aligned}$$

\Rightarrow require $\mathbb{I}' = R \cdot \mathbb{I} \cdot R^T$ if $\vec{\tau}, \vec{\omega}$ are physical vectors.

The kinetic energy is

$$\begin{aligned}
 T &= \frac{1}{2} \sum_{\alpha} m_{\alpha} \dot{\vec{r}}_{\alpha}^2 = \frac{1}{2} \sum_{\alpha} m_{\alpha} (\vec{\omega} \times \vec{r}_{\alpha})^2 \\
 &= \frac{1}{2} \sum_{\alpha} m_{\alpha} \sum_i (\vec{\omega} \times \vec{r}_{\alpha})_i (\vec{\omega} \times \vec{r}_{\alpha})_i \\
 &= \frac{1}{2} \sum_{\alpha} m_{\alpha} \sum_i \sum_{j,k} \epsilon_{ijk} \omega_j r_{\alpha,k} \sum_{l,m} \epsilon_{ilm} \omega_l r_{\alpha,m}
 \end{aligned}$$

Note the relation $\sum_i \epsilon_{ijk} \epsilon_{ilm} = \delta_{jl} \delta_{km} - \delta_{kl} \delta_{jm}$

$$\begin{aligned}
 \Rightarrow T &= \frac{1}{2} \sum_{\alpha} m_{\alpha} \sum_{j,k} \sum_{l,m} (\delta_{jl} \delta_{km} - \delta_{kl} \delta_{jm}) \omega_j \omega_l r_{\alpha,k} r_{\alpha,m} \\
 &= \frac{1}{2} \sum_{i,j} \omega_i \left[\sum_{\alpha} m_{\alpha} (\vec{r}_{\alpha}^2 \delta_{ij} - r_{\alpha,i} r_{\alpha,j}) \right] \omega_j \\
 &= \frac{1}{2} \sum_{i,j} \omega_i I_{ij} \omega_j
 \end{aligned}$$

$$\Rightarrow T = \frac{1}{2} \vec{\omega}^T \mathbb{I} \cdot \vec{\omega} = \frac{1}{2} \vec{\omega} \cdot \vec{\mathbb{I}}$$

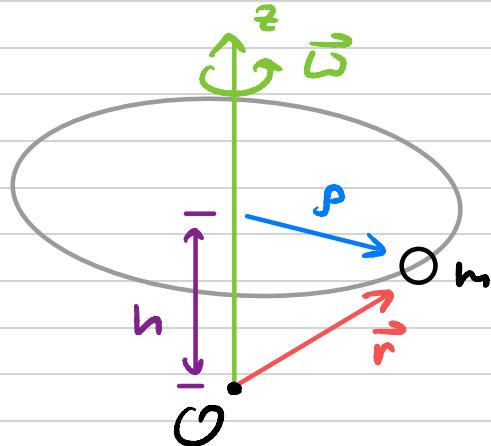
Example - Consider a point-particle with mass m rotating around z -axis at a constant radius ρ , height h above origin, & angular velocity $\vec{\omega}$.

Compute the elements of the inertia tensor.

$$\vec{\omega} = (0, 0, \omega)$$

& position

$$\vec{r}(t) = \rho \cos \omega t \hat{x} + \rho \sin \omega t \hat{y} + h \hat{z}$$



Since the rotation is about z , there are only 3 non-zero components, $I_{zz}, I_{xz} = I_{zx}, I_{yz} = I_{zy}$

$$I_{zz} = m(x^2 + y^2) = m\rho^2$$

$$I_{xz} = -mxz = -mh\rho \cos \omega t$$

$$I_{yz} = -myz = -mh\rho \sin \omega t$$

$$\text{So, } \vec{L} = \vec{I} \cdot \vec{\omega} = I_{xz} \omega \hat{x} + I_{yz} \omega \hat{y} + I_{zz} \omega \hat{z} \\ = -mh\rho \omega (\cos \omega t \hat{x} + \sin \omega t \hat{y}) + m\rho^2 \omega \hat{z}$$

Exercise: compare \vec{L} to $\vec{L} = \vec{r} \times m\vec{v}$.

Notice that if $\vec{\omega} = 0$, i.e., the origin
is in the plane of rotation

$$\Rightarrow \vec{I}_{\vec{\omega}=0} = I_z \vec{\omega}$$

which is the result from Phys 101. ■

Example - Compute the inertia tensor

of a solid cube of mass M and side length a
about (a) the corner, (b) the center.

Compute \vec{I} for both cases given

$$\vec{\omega}_1 = \omega(1, 0, 0) \quad \text{&} \quad \vec{\omega}_2 = \frac{\omega}{\sqrt{3}}(1, 1, 1).$$

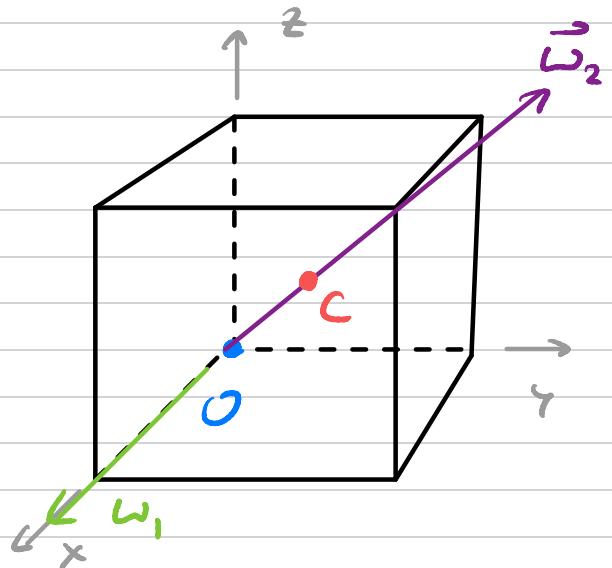
For a continuous distribution

$$I_{ij} = \int (\vec{r}^2 \delta_{ij} - r_i r_j) \rho dV$$

$$\text{where } \rho = \frac{M}{a^3}$$

- Corner (point O) $\Rightarrow (0, 0, 0)$

- Center (point C) $\Rightarrow \left(\frac{a}{2}, \frac{a}{2}, \frac{a}{2}\right)$



(a) for point O,

$$\begin{aligned}
 I_x(O) &= \int_0^a dx \int_0^a dy \int_0^a dz \rho (y^2 + z^2) \\
 &= \rho \left(\int_0^a dx \right) \left(\int_0^a dy y^2 \right) \left(\int_0^a dz z^2 \right) \\
 &\quad + \rho \left(\int_0^a dx \right) \left(\int_0^a dy \right) \left(\int_0^a dz z^2 \right) \\
 &= \rho \cdot a \cdot \frac{a^3}{3} \cdot a + \rho \cdot a \cdot a \cdot \frac{a^3}{3} \\
 &= \frac{2}{3} \rho a^5 = \frac{2}{3} \left(\frac{M}{a^3} \right) a^5
 \end{aligned}$$

$$\Rightarrow I_x(O) = \frac{2}{3} Ma^2$$

By inspection, find $I_x(O) = I_y(O) = I_z(O) = \frac{2}{3} Ma^2$

The product of inertia is

$$\begin{aligned}
 I_{xy}(O) &= -\rho \int_0^a dx \int_0^a dy \int_0^a dz \cdot xy \\
 &= -\left(\frac{M}{a^3} \right) \frac{a^2}{2} \cdot \frac{a^2}{2} \cdot a = -\frac{1}{4} Ma^2
 \end{aligned}$$

By inspection, find all products of inertia are equal

ζ_0 ,

$$\mathbb{II}(0) = Ma^2 \begin{pmatrix} 2/3 & -1/4 & -1/4 \\ -1/4 & 2/3 & -1/4 \\ -1/4 & -1/4 & 2/3 \end{pmatrix}$$

(b) for point C,

$$\begin{aligned} I_x(C) &= \rho \int_{-a/2}^{a/2} dx \int_{-a/2}^{a/2} dy \int_{-a/2}^{a/2} dz (y^2 + z^2) \\ &= \frac{M}{a^3} \cdot a \cdot a \cdot \frac{1}{3} \cdot 2 \left[\left(\frac{a}{2}\right)^3 + \left(\frac{a}{2}\right)^3 \right] \\ &= \frac{1}{6} Ma^2 \end{aligned}$$

Likewise, $I_y(C) = I_z(C) = \frac{1}{6} Ma^2$

$$I_{xy}(C) = \rho \int_{-a/2}^{a/2} dx \int_{-a/2}^{a/2} dy \int_{-a/2}^{a/2} dz xy = 0$$

↳ odd integrand
over even interval

$$\Rightarrow \text{All } I_{ij} = 0 \text{ for } i \neq j$$

$$\Rightarrow \mathbb{II}(C) = \frac{1}{6} Ma^2 \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$= \frac{1}{6} Ma^2 \mathbb{II} .$$

The angular momenta are

$$\vec{L}_1(\omega) = \underline{\underline{I}}(\omega) \cdot \vec{\omega}_1,$$

$$= Ma^2 \omega \begin{pmatrix} 2/3 & -1/4 & -1/4 \\ -1/4 & 2/3 & -1/4 \\ -1/4 & -1/4 & 2/3 \end{pmatrix} \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}$$

$$= \frac{1}{12} Ma^2 \omega (8, -3, -3)$$

$$\vec{L}_2(\omega) = \underline{\underline{I}}(\omega) \cdot \vec{\omega}_2$$

$$= \frac{1}{\sqrt{3}} Ma^2 \omega \begin{pmatrix} 2/3 & -1/4 & -1/4 \\ -1/4 & 2/3 & -1/4 \\ -1/4 & -1/4 & 2/3 \end{pmatrix} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

$$= \frac{1}{6\sqrt{3}} Ma^2 \omega (1, 1, 1) = \frac{1}{6} Ma^2 \vec{\omega}_2$$

For point C,

$$\vec{L}_1(C) = \underline{\underline{I}}(C) \cdot \vec{\omega}_1 = \frac{1}{6} Ma^2 \underline{\underline{I}} \cdot \vec{\omega}_1 = \frac{1}{6} Ma^2 \vec{\omega}_1$$

$$\vec{L}_2(C) = \underline{\underline{I}}(C) \cdot \vec{\omega}_2 = \frac{1}{6} Ma^2 \underline{\underline{I}} \cdot \vec{\omega}_2 = \frac{1}{6} Ma^2 \vec{\omega}_2$$

The previous example shows something interesting,
 for a particular choice of origin and/or axis
 of rotation, the relation $\vec{L} = \mathbb{I} \cdot \vec{\omega}$ simplifies
 such that $\vec{L} \parallel \vec{\omega}$.

This particular set of axes are called
principal axes. The moment of inertia about
 the principal axes is called the principal moments,
 and generally, the moment of inertia is

$$\mathbb{I} = \begin{pmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{pmatrix}$$

so that $\vec{L} = \lambda \vec{\omega}$.

Principal axes are associated with some symmetry axis.

Theorem: Existence of Principal Axes

For any rigid body and point O,
 \exists three perpendicular axes through
 O s.t. \mathbb{I} is diagonal.

$$\Rightarrow \mathbb{I} \vec{\omega} = \lambda \vec{\omega} \quad \text{and} \quad \vec{L} \parallel \vec{\omega}$$

To prove this, we need to recall some Linear Algebra ...

Diagonalizing a Real-Symmetric Matrix

Let us remind ourself of some aspects of linear algebra, namely eigensystems & solutions.

Consider a real, symmetric $n \times n$ matrix A .

We'd like to solve the eigenvalue equation

$$\rightarrow A\vec{v} = \lambda \vec{v}, \quad \lambda = \text{eigenvalue}$$

\uparrow
number

$$(A - \lambda I)\vec{v} = 0 \quad \vec{v} = \text{eigenvector}$$

This is equivalent to $(A - \lambda I)\vec{v} = 0$

From linear algebra, we know that this has a nontrivial solution ($\vec{v} \neq 0$) iff $\det(A - \lambda I) = 0$.

← characteristic eqn.

This is a polynomial of degree n . In general, it has n complex solutions.

For each solution λ_α , $\det(A - \lambda_\alpha I) = 0$,

so \exists a null vector $\vec{v}_\alpha \in A - \lambda_\alpha I$, i.e.,

$$A\vec{v}_\alpha = \lambda_\alpha \vec{v}_\alpha \quad (1)$$

and \vec{v}_α an eigenvector.

In general, $\vec{v}_\alpha \in \mathbb{C}^n$. Let's act (1) on the left by $\vec{v}_\alpha^+ = (\vec{v}_\alpha^\top)^*$ ($+$ = conjugate transpose)

$$\vec{v}_\alpha^+ / A \vec{v}_\alpha = \lambda_\alpha \vec{v}_\alpha^+ \vec{v}_\alpha$$

$$\text{Note that } \vec{v}_\alpha^+ \vec{v}_\alpha = |\vec{v}_\alpha|^2 \in \mathbb{R}$$

$$\Rightarrow \lambda_\alpha = \frac{\vec{v}_\alpha^+ / A \vec{v}_\alpha}{|\vec{v}_\alpha|^2}$$

Recall that, in general, $\lambda_\alpha \in \mathbb{C}$, so it is a 1×1 matrix and is symmetric, $\lambda_\alpha^\top = \lambda_\alpha$
Similarly, $|\vec{v}_\alpha|^2 \in \mathbb{R} \Rightarrow (|\vec{v}_\alpha|^2)^\top = |\vec{v}_\alpha|^2$

So, take transpose,

$$\lambda_\alpha = \lambda_\alpha^\top = \frac{(\vec{v}_\alpha^+ / A \vec{v}_\alpha)^\top}{|\vec{v}_\alpha|^2}$$

$$\text{Recall } (ABC)^\top = C^\top B^\top A^\top$$

$$\Rightarrow (\vec{v}_\alpha^+ / A \vec{v}_\alpha)^\top = \vec{v}_\alpha^\top / A^\top \vec{v}_\alpha^* \\ = \vec{v}_\alpha^{+\top} / A^\top \vec{v}_\alpha^*$$

Now, $/A$ is real and symmetric $\Rightarrow /A^\top = /A = /A^*$

$$\text{So, } \lambda_\alpha = \frac{\vec{V}_\alpha^+ A^* \vec{V}_\alpha^*}{|\vec{V}_\alpha|^2}$$

$$= \left(\frac{\vec{V}_\alpha^+ A \vec{V}_\alpha}{|\vec{V}_\alpha|^2} \right)^* = \lambda_\alpha^*$$

$$\therefore \lambda_\alpha = \lambda_\alpha^* \Rightarrow \boxed{\lambda_\alpha \in \mathbb{R}}$$

for real, symmetric matrix A

Notice also

$$A^* \vec{V}_\alpha^* = \lambda_\alpha^* \vec{V}_\alpha^* \Rightarrow A \vec{V}_\alpha^* = \lambda_\alpha \vec{V}_\alpha^*$$

So, \vec{V}_α^* is also an eigenvector w/ same eigenvalue

$\Rightarrow \vec{V}_\alpha$. \Rightarrow Can take $\vec{V}_\alpha + \vec{V}_\alpha^*$, this must

also be an eigenvector with eigenvalue λ_α .

$$\text{But, } \vec{V}_\alpha + \vec{V}_\alpha^* = 2\operatorname{Re}(\vec{V}_\alpha) \in \mathbb{R}^n.$$

\Rightarrow Through suitable manipulations, all eigenvectors can be chosen to be real.

We may also normalize the eigenvectors

$$\vec{V}_\alpha \rightarrow \frac{\vec{V}_\alpha}{\sqrt{\vec{V}_\alpha^T \vec{V}_\alpha}}, \text{ so that } \vec{V}_\alpha^T \vec{V}_\alpha = 1.$$

From now on, assume \vec{V}_α is normalized.

Finally, consider two eigenvalues $\lambda_\alpha \neq \lambda_\beta$.

Then,

$$A \vec{V}_\alpha = \lambda_\alpha \vec{V}_\alpha$$

$$\& A \vec{V}_\beta = \lambda_\beta \vec{V}_\beta \Rightarrow \vec{V}_\beta^T A = \lambda_\beta \vec{V}_\beta^T$$

↑ take transpose

At second eqn. on \vec{V}_α

$$\Rightarrow \vec{V}_\beta^T A \vec{V}_\alpha = \lambda_\beta \vec{V}_\beta^T \vec{V}_\alpha$$

||

$$\vec{V}_\beta^T (\lambda_\alpha \vec{V}_\alpha) = \lambda_\alpha \vec{V}_\beta^T \vec{V}_\alpha$$

$$\therefore (\lambda_\alpha - \lambda_\beta) \vec{V}_\beta^T \cdot \vec{V}_\alpha = 0 \Rightarrow \vec{V}_\beta^T \cdot \vec{V}_\alpha = 0$$

We conclude

$$\vec{V}_\alpha^T \cdot \vec{V}_\beta = \delta_{\alpha\beta}$$

(orthonormality)

With all this, we can now show that A

can be diagonalized as $A = V D V^T$

where D is diagonal matrix with the eigenvalues on the diagonal and V is an orthogonal matrix formed by placing \vec{V}_α at column α in the same order as λ_α in D .

Proof. Since \vec{v}_α are orthonormal, they form a complete basis & we just need to show

$$A \vec{v}_\alpha = (V D V^T) \vec{v}_\alpha$$

In the usual basis of A , $\vec{e}_1 = (1, 0, 0, \dots, 0)$

$$\vec{e}_2 = (0, 1, 0, \dots, 0)$$

:

$$\vec{e}_d = (0, 0, \dots, 1, \dots, 0)$$

We can write the β -element
of the α -basis vector $(\vec{e}_\alpha)_\beta = \delta_{\alpha\beta}$.

With this basis, we can expand the eigenvector as

$$\vec{v}_\alpha = \sum_\beta v_{\alpha,\beta} \vec{e}_\beta$$

Then, $V_{\alpha\beta} = v_{\alpha,\beta}$ is an orthogonal matrix $V^{-1} = V^T$.

To see this, $V \vec{e}_\alpha = \vec{v}_\alpha$, also

$$(V^T \vec{v}_\alpha)_\beta = \sum_r (V^T)_{\beta r} (\vec{v}_\alpha)_r$$

$$= \sum_r (V)_{\gamma\beta} (\vec{v}_\alpha)_r = \sum_r v_{\gamma,\beta} v_{\alpha,r}$$

$$= \vec{v}_\beta^T \cdot \vec{v}_\alpha = \delta_{\alpha\beta}$$

$$\Rightarrow V^T \vec{v}_\alpha = \vec{e}_\alpha \Rightarrow V^T V \vec{e}_\alpha = \vec{e}_\alpha$$

$$\Rightarrow V^T V = I \quad \forall \alpha$$

Finally,

$$(V D V^T) \vec{v}_\alpha = V D \vec{e}_\alpha = \lambda_\alpha V \vec{e}_\alpha = \lambda_\alpha \vec{v}_\alpha \equiv A \vec{v}_\alpha$$

$$\therefore \boxed{A = V D V^T}$$

Principle Axes & Principal Moments

For the inertia tensor, a real symmetric matrix, we can diagonalize it, i.e., choose a set of axes, such that $\mathbb{I} \parallel \vec{\omega}$.

The diagonal elements are given by the eigenvalues of \mathbb{I} , i.e., the solutions to

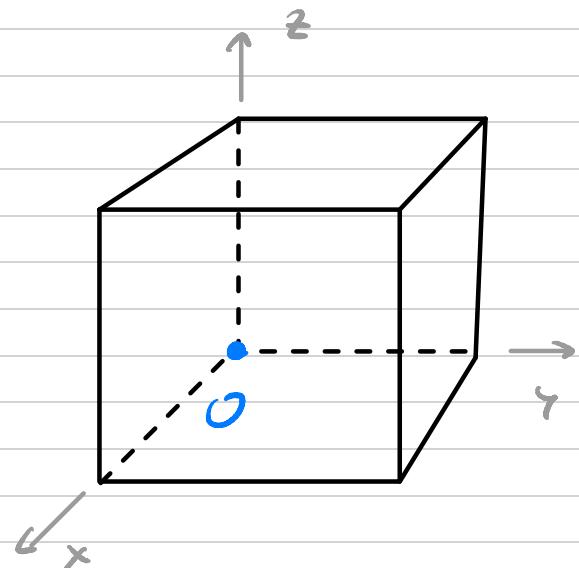
$$\det(\mathbb{I} - \lambda \mathbb{1}) = 0$$

Example - Principle axes of cube about corner?

Recall from previous example

$$\mathbb{I}_0 = M_a^2 \begin{pmatrix} 2/3 & -1/4 & -1/4 \\ -1/4 & 2/3 & -1/4 \\ -1/4 & -1/4 & 2/3 \end{pmatrix}$$

$$= \mu \begin{pmatrix} 8 & -3 & -3 \\ -3 & 8 & -3 \\ -3 & -3 & 8 \end{pmatrix}$$



with $\mu = \frac{1}{12} M_a^2$

So, we want to solve $\det(\mathbb{I}_3 - \lambda \mathbb{1}) = 0$

$$\Rightarrow \det \begin{bmatrix} 8\mu - \lambda & -3\mu & -3\mu \\ -3\mu & 8\mu - \lambda & -3\mu \\ -3\mu & -3\mu & 8\mu - \lambda \end{bmatrix} = 0$$

To solve, note the following:

- Replacing a column (row) of a matrix with the sum of that column (row) & a multiple of another column (row) does NOT change \det .
- Multiplying a column (row) by number, multiplies \det by same number
- $\det \begin{bmatrix} a_1 & \cdot & \cdot \\ 0 & a_2 & \cdot \\ 0 & 0 & a_3 \end{bmatrix} = \det \begin{bmatrix} a_1 & 0 & 0 \\ \cdot & a_2 & 0 \\ \cdot & \cdot & a_3 \end{bmatrix} = a_1 a_2 a_3$

So, take

$$0 = \det \begin{bmatrix} 8\mu - \lambda & -3\mu & -3\mu \\ -3\mu & 8\mu - \lambda & -3\mu \\ -3\mu & -3\mu & 8\mu - \lambda \end{bmatrix}$$

take col 1 \rightarrow col 1 - col 2

$$\Rightarrow O = \det \begin{bmatrix} 11\mu - \lambda & -3\mu & -3\mu \\ -11\mu + \lambda & 8\mu - \lambda & -3\mu \\ 0 & -3\mu & 8\mu - \lambda \end{bmatrix}$$

row 2 \rightarrow row 2 + row 1

$$= \det \begin{bmatrix} 11\mu - \lambda & -3\mu & -3\mu \\ 0 & 5\mu - \lambda & -6\mu \\ 0 & -3\mu & 8\mu - \lambda \end{bmatrix}$$

col 2 \rightarrow col 2 - col 3

$$= \det \begin{bmatrix} 11\mu - \lambda & 0 & -3\mu \\ 0 & 11\mu - \lambda & -6\mu \\ 0 & -11\mu + \lambda & 8\mu - \lambda \end{bmatrix}$$

row 3 \rightarrow row 3 + row 2

$$= \det \begin{bmatrix} 11\mu - \lambda & 0 & -3\mu \\ 0 & 11\mu - \lambda & -6\mu \\ 0 & 0 & 3\mu - \lambda \end{bmatrix}$$

so, find

$$\det[\dots] = (11\mu - \lambda)^2 (2\mu - \lambda) = 0$$

$$\Rightarrow \begin{cases} \lambda_1 = 2\mu \\ \lambda_2 = \lambda_3 = 11\mu \end{cases}$$

So, the principal moments are

$$\mathbb{I}'_0 = \mathbb{D} = \mu \begin{pmatrix} 2 & 0 & 0 \\ 0 & 11 & 0 \\ 0 & 0 & 11 \end{pmatrix}$$

What about the axes?

Want $\hat{\mathbf{e}}_1, \hat{\mathbf{e}}_2, \hat{\mathbf{e}}_3$

First, find $\vec{\omega}_1 = \omega \hat{\mathbf{e}}_1$ associated w/ λ_1

Solve $(\mathbb{I}_0 - \lambda_1 \mathbb{I}) \vec{\omega}_1 = 0$

$$\Rightarrow \mu \begin{pmatrix} 6 & -3 & -3 \\ -3 & 6 & -3 \\ -3 & -3 & 6 \end{pmatrix} \begin{pmatrix} \omega_{1,x} \\ \omega_{1,y} \\ \omega_{1,z} \end{pmatrix} = 0$$

$$\Rightarrow 2\omega_{1,x} - \omega_{1,y} - \omega_{1,z} = 0 \quad (a)$$

$$-\omega_{1,x} + 2\omega_{1,y} - \omega_{1,z} = 0 \quad (b)$$

$$-\omega_{1,x} - \omega_{1,y} + 2\omega_{1,z} = 0 \quad (c)$$

$$\text{Take (a)-(b)} \Rightarrow \omega_{1,x} = \omega_{1,y}$$

$$\text{From (c)} \Rightarrow \omega_{1,x} = \omega_{1,y} = \omega_{1,z}$$

So, $\vec{\omega} \parallel (1,1,1) \Rightarrow$ Normalize to find

$$\hat{\mathbf{e}}_1 = \frac{1}{\sqrt{3}} (1,1,1)$$

This means that if $\vec{\omega}_1 = \omega \hat{e}_1$,

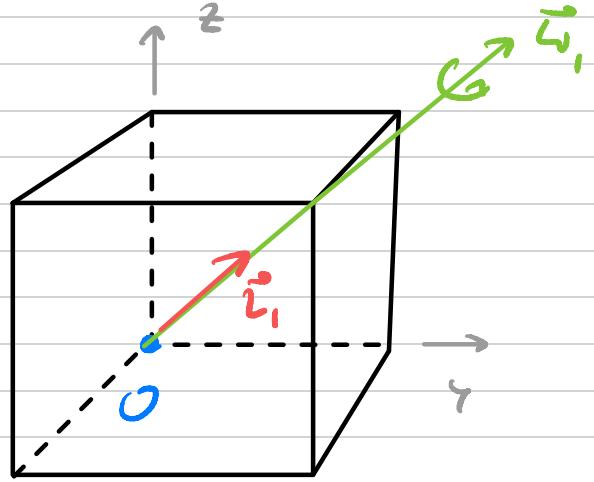
$$\text{then } \vec{\lambda}_1 = \vec{\mathbb{I}} \vec{\omega}_1 = \omega \vec{\mathbb{I}} \hat{e}_1 = \omega \lambda_1 \hat{e}_1 = \lambda_1 \vec{\omega}_1,$$

$$\Rightarrow \vec{\lambda}_1 = \lambda_1 \vec{\omega}_1$$

For $\vec{\omega}_2$ & $\vec{\omega}_3$, $\lambda_2 = \lambda_3$

Solve

$$(\vec{\mathbb{I}}_0 - \lambda_2 \vec{\mathbb{I}}) \vec{\omega} = 0$$



$$\Rightarrow \mu \begin{bmatrix} -3 & -3 & -3 \\ -3 & -3 & -3 \\ -3 & -3 & -3 \end{bmatrix} \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix} = 0$$

$$\Rightarrow \omega_x + \omega_y + \omega_z = 0$$

Notice that this is equal to $\vec{\omega} \cdot \hat{e}_1 = 0$

$\Rightarrow \vec{\omega}$ needs to be orthogonal to \hat{e}_1 ,

$\Rightarrow \hat{e}_2$ & \hat{e}_3 need to be orthogonal to \hat{e}_1 ,

Two such solutions are

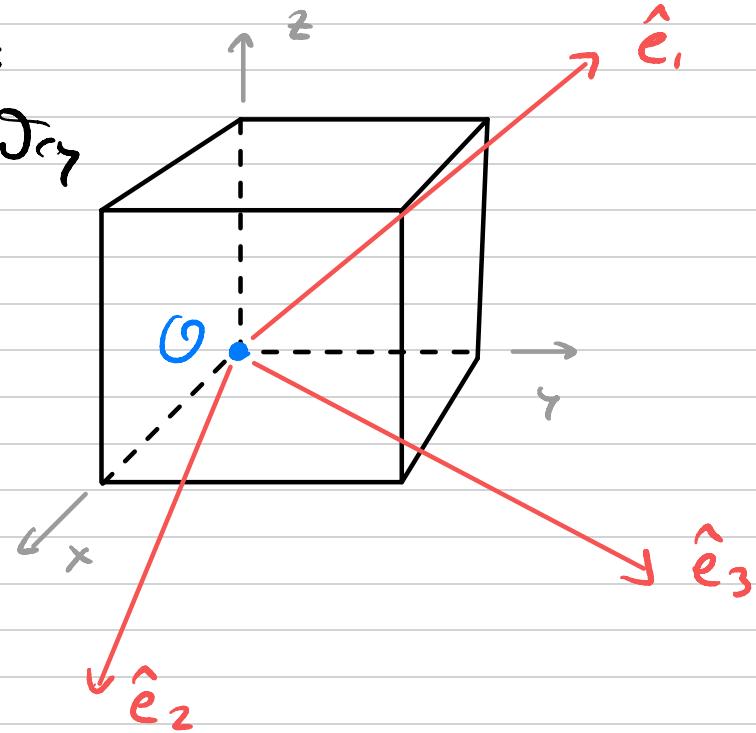
$$\hat{e}_2 = \frac{1}{\sqrt{2}} (1, 0, -1), \quad \hat{e}_3 = \frac{1}{\sqrt{6}} (-1, 2, -1)$$

(using)

So, principal axes (eigenvectors) are

$$\hat{e}_1 = \frac{1}{\sqrt{3}}(1,1,1), \hat{e}_2 = \frac{1}{\sqrt{2}}(1,0,-1), \hat{e}_3 = \frac{1}{\sqrt{6}}(-1,2,-1)$$

The principal axes correspond to symmetry of the cube and the body diagonal with center at O.



Can decompose $\mathbb{I}_0 = V D_0 V^T$

with $D_0 = \frac{1}{12} M a^2 \begin{pmatrix} 2 & 0 & 0 \\ 0 & 11 & 0 \\ 0 & 0 & 11 \end{pmatrix}$

$$V = \frac{1}{\sqrt{6}} \begin{pmatrix} \sqrt{2} & \sqrt{3} & -1 \\ \sqrt{2} & 0 & 2 \\ \sqrt{2} & -\sqrt{3} & -1 \end{pmatrix}$$

$$\hat{e}_1 \quad \hat{e}_2 \quad \hat{e}_3$$

■

Precession of Symmetric Top due to Weak Torque

Having all the tools in our arsenal, let's apply them for a "simple" physics problem.

Consider a symmetric top with mass M and inertia tensor $\mathbb{I} = \text{diag}(\lambda_1, \lambda_2, \lambda_3)$ in the basis of its principal axes, $(\hat{\mathbf{e}}_1, \hat{\mathbf{e}}_2, \hat{\mathbf{e}}_3)$.

It rotates freely with its tip pivoted at a fixed point O in a lab frame (inertial)

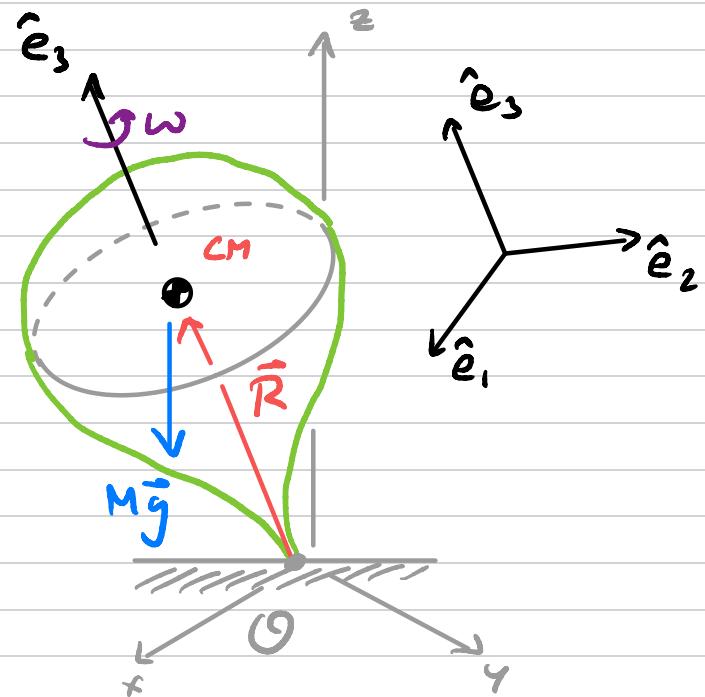
Its CM is at \bar{R} .

We assume its angular velocity is initially along its symmetry axis,

$$\vec{\omega} = \omega \hat{\mathbf{e}}_3$$

The angular momentum is initially

$$\vec{L} = \mathbb{I} \vec{\omega} = \lambda_3 \omega \hat{\mathbf{e}}_3$$



(initial config)

If we release the top, gravity will exert a torque, and cause a change of angular momentum.

The torque due to gravity is $\vec{\tau} = \vec{R} \times M\vec{g}$, at the CM w.r.t fixed point O.

- If $\vec{\tau} = \vec{0}$ (c.g., $\vec{R} \times \vec{g} = \vec{0}$)
 $\Rightarrow \vec{L} = \text{const.}$

To see, take

$$\begin{aligned} \left(\frac{d\vec{L}}{dt} \right)_{\text{lab}} &= \lambda_3 \frac{d}{dt} \left(\omega \hat{e}_3 \right)_{\text{lab}} \\ &= \lambda_3 \left(\dot{\omega} \hat{e}_3 + \omega \left(\frac{d\hat{e}_3}{dt} \right)_{\text{lab}} \right) = 0 \end{aligned}$$

Since $\vec{\omega} \parallel \hat{e}_3 \Rightarrow \left(\frac{d\hat{e}_3}{dt} \right)_{\text{lab}} = \vec{\omega} \times \hat{e}_3 = \vec{0}$

That is, \hat{e}_3 is fixed in the lab frame too!

$$\Rightarrow \dot{\omega} = 0$$

• If $\vec{\Gamma} \neq \vec{0}$, but ω_1, ω_2 are small, so $\vec{\omega} \approx \omega_3 \hat{e}_3$

$\Rightarrow \vec{\Gamma} \perp \vec{\omega}$ and $\dot{\omega}$ remains small

so, EOM gives $\left(\frac{d\vec{L}}{dt} \right)_{\text{lab}} = \vec{\Gamma}$

$$\Rightarrow \lambda \left(i\dot{\omega} \hat{e}_3 + \omega \left(\frac{d\hat{e}_3}{dt} \right)_{\text{lab}} \right) = \vec{R} \times M\vec{g}$$

Since $i\dot{\omega} \approx 0$, $\left(\frac{d\hat{e}_3}{dt} \right)_{\text{lab}} = \pm \frac{1}{\lambda\omega} \vec{R} \times M\vec{g}$

Now, $\vec{R} = R\hat{e}_3$, $\vec{g} = -g\hat{z}$ $\Rightarrow \vec{R} \times \vec{g} = Rg\hat{z} \times \hat{e}_3$

$$\Rightarrow \left(\frac{d\hat{e}_3}{dt} \right)_{\text{lab}} = \left(\frac{MRg}{\lambda\omega} \right) \hat{z} \times \hat{e}_3$$

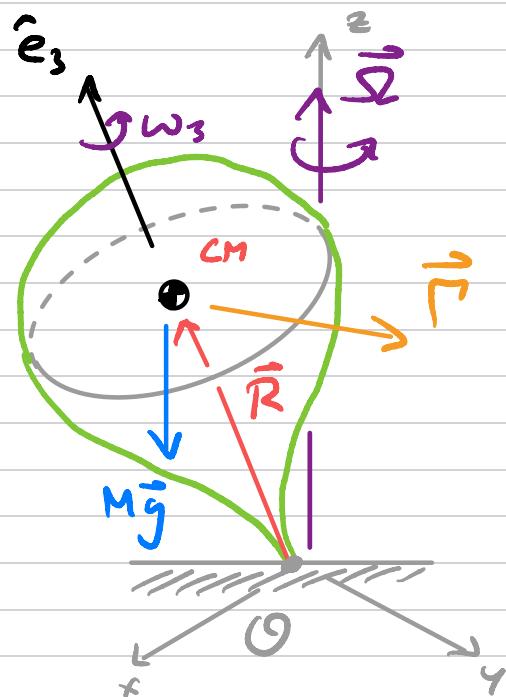
Define $\vec{\Omega} = \frac{MRg}{\lambda\omega} \hat{z}$

\Rightarrow the symmetry axis of the

to rotates w/ $\Omega = \frac{MRg}{\lambda\omega}$

about \hat{z} axis

\Rightarrow precession



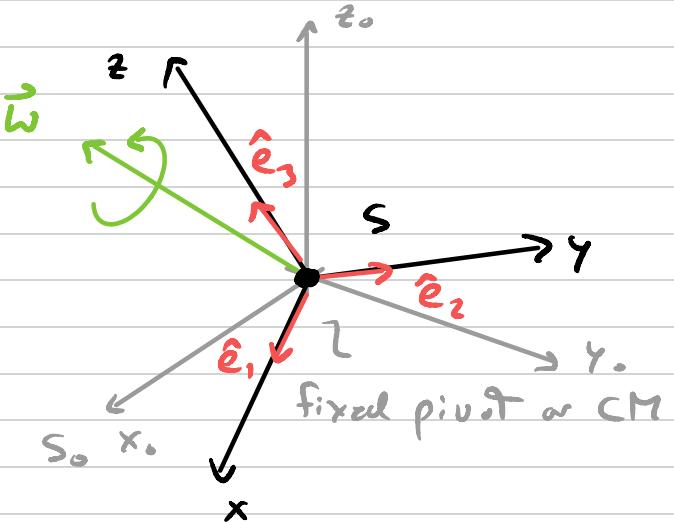
Euler's Equations

Newton's Law's of motion for a body rotating in some inertial (space-fixed) frame S_0 .

$$\left(\frac{d\vec{L}}{dt} \right)_{S_0} = \vec{\Gamma}$$

Recall that

$$\left(\frac{d\vec{L}}{dt} \right)_{S_0} = \left(\frac{d\vec{L}}{dt} \right)_S + \vec{\omega} \times \vec{L}$$



Where S is a frame fixed to the body.

Therefore, we find

$$\dot{\vec{L}} + \vec{\omega} \times \vec{L} = \vec{\Gamma}$$

in body-fixed frame S

Notice: If $\vec{\Gamma} = \vec{0} \Rightarrow \vec{L}$ is conserved in S_0

BUT NOT in S !

The use of the body-fixed frame makes it possible to choose the principle axes of the moment of inertia, $(\hat{e}_1, \hat{e}_2, \hat{e}_3)$, as the coordinate axes.

Therefore,

$$\vec{L} = \mathbb{I} \vec{\omega} = \lambda_1 \omega_1 \hat{e}_1 + \lambda_2 \omega_2 \hat{e}_2 + \lambda_3 \omega_3 \hat{e}_3$$

$$\text{so, } \dot{\vec{L}} + \vec{\omega} \times \vec{L} = \vec{\Gamma}$$

$$\lambda_1 \dot{\omega}_1 - (\lambda_2 - \lambda_3) \omega_2 \omega_3 = \Gamma_1$$

$$\lambda_2 \dot{\omega}_2 - (\lambda_3 - \lambda_1) \omega_3 \omega_1 = \Gamma_2$$

$$\lambda_3 \dot{\omega}_3 - (\lambda_1 - \lambda_2) \omega_1 \omega_2 = \Gamma_3$$

These are called the Euler Equations of rotational motion

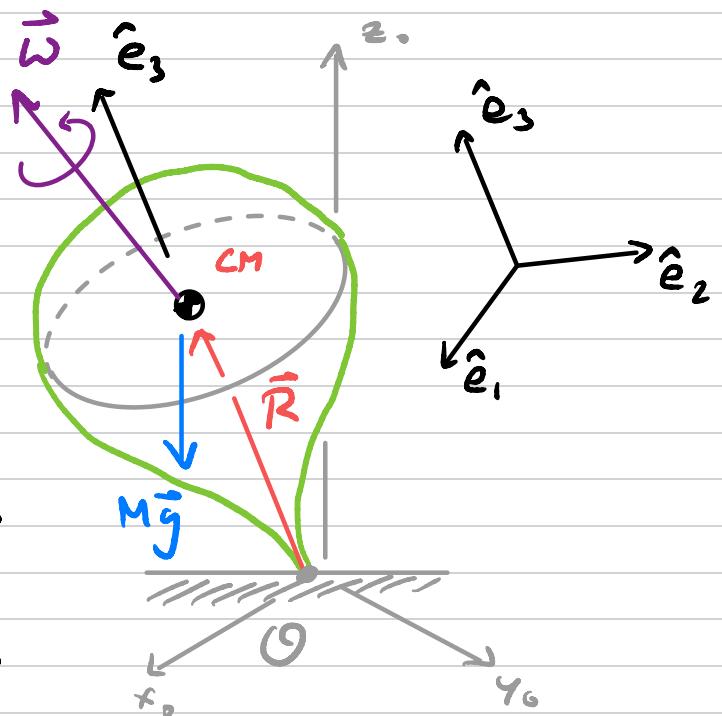
An example is the symmetric spinning top we considered before

$$\lambda_1 = \lambda_2$$

$$\& \Gamma_3 = 0 \Rightarrow \underline{\lambda_3 \dot{\omega}_3 = 0}$$

The other two Euler eqns. are

$$\left\{ \begin{array}{l} \dot{\omega}_1 = \frac{1}{\lambda_1} \Gamma_1 - \left(\frac{\lambda_3}{\lambda_1} - 1 \right) \omega_2 \omega_3 \\ \dot{\omega}_2 = \frac{1}{\lambda_2} \Gamma_2 + \left(\frac{\lambda_3}{\lambda_1} - 1 \right) \omega_1 \omega_3 \end{array} \right.$$



Take the axis (\hat{e}_3) to be & spherical angles (θ, φ)
in the space frame, we find $\vec{\Gamma} \parallel \hat{\varphi}$.

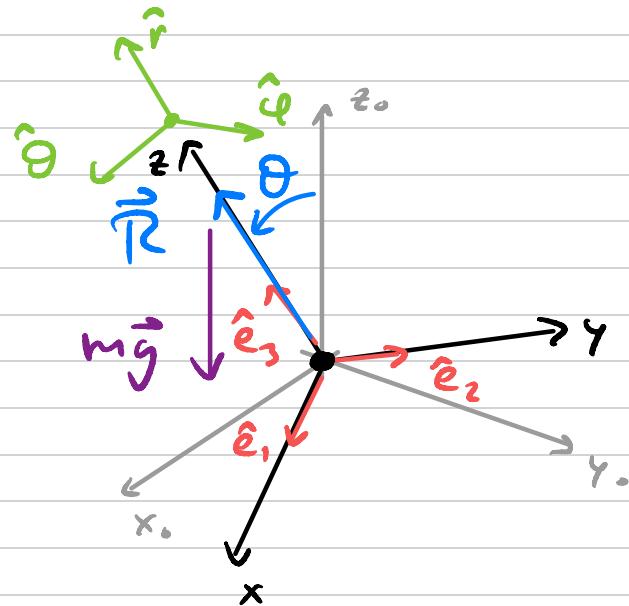
Let's choose the axes at time $t=0$ such that

$\hat{e}_1 \parallel \vec{\Gamma} \parallel \hat{y}_0$ and \hat{e}_3
is in the xz plane.

The CM is $\vec{R} = R\hat{r}$

where $m\vec{g}$ is given by

$$m\vec{g} = mg(-\cos\theta \hat{r} + \sin\theta \hat{\theta})$$



At time t , \hat{e}_1 will have rotated

by an angle $\omega_3 t$ around \hat{e}_3 (since $\dot{\omega}_3 = 0 \Rightarrow \omega_3 = \text{const.}$)

Therefore, $\vec{\Gamma}_1 = \Gamma \sin \omega_3 t$, $\vec{\Gamma}_2 = \Gamma \cos \omega_3 t$

where

$$\Gamma = |\vec{\Gamma}| = MgR \sin\theta$$

To solve the remaining Euler eqns., we introduce a
Complex variable

$$\gamma = \omega_1 + i\omega_2$$

Therefore,

$$\dot{\eta} = \bar{\omega}_1 + i\bar{\omega}_2$$

$$= \frac{1}{\lambda_1} (\Gamma_1 + i\Gamma_2) + \left(\frac{\lambda_3 - 1}{\lambda_1} \right) \omega_3 (-\omega_2 + i\omega_1)$$

$$\Rightarrow \dot{\eta} = i \frac{\Gamma}{\lambda_1} e^{-i\omega_3 t} + i \left(\frac{\lambda_3 - 1}{\lambda_1} \right) \omega_3 \eta .$$

We can write the solution as $\eta = \eta_h + \eta_p$

The homogeneous eqn is

$$\ddot{\eta} = i \left(\frac{\lambda_3 - 1}{\lambda_1} \right) \omega_3 \eta ,$$

↑
homogeneous
general solution

which by direct integration gives homogeneous solution

$$\eta_h = A \exp \left[i \left(\frac{\lambda_3 - 1}{\lambda_1} \right) \omega_3 t \right]$$

↑
TBD from ICs

$$\text{The particular solution is } \eta_p = \eta_0 e^{-i\omega_3 t}$$

Fix η_0 by substituting into EOM,

$$-i\omega_3 \eta_0 = i \frac{\Gamma}{\lambda_1} + i \left(\frac{\lambda_3 - 1}{\lambda_1} \right) \omega_3 \eta_0$$

$$\Rightarrow \eta_0 = -\frac{\Gamma}{\lambda_3 \omega_3}$$

To fix A , the ICs are $\omega_1 = \omega_2 = 0$ at $t = 0$

$$\Rightarrow \gamma(0) = 0 = A + M_0 \Rightarrow A = -M_0$$

So, altogether

$$\gamma(t) = \sum_{\lambda_3 \omega_3} \left[e^{i(\frac{\lambda_3}{\lambda_1} - 1)\omega_3 t} - e^{-i\omega_3 t} \right]$$

Writing $\vec{\omega} = \vec{\omega}_1 + \omega_3 \hat{e}_3$, the small torque condition

is

$$|\gamma| = |\vec{\omega}_1| \ll \omega_3 \quad \& \quad \theta \ll 1$$

$$\Rightarrow \frac{\Gamma}{\lambda_3 \omega_3} \ll \omega_3 \Rightarrow \underbrace{\frac{MgR}{\lambda_3 \omega_3}}_{\equiv \Omega} \ll \omega_3$$

$\equiv \Omega$ = the precession frequency

Zero Torque

The zero-torque Euler eqns. are

$$\lambda_1 \dot{\omega}_1 = (\lambda_2 - \lambda_3) \omega_2 \omega_3$$

$$\lambda_2 \dot{\omega}_2 = (\lambda_3 - \lambda_1) \omega_3 \omega_1$$

$$\lambda_3 \dot{\omega}_3 = (\lambda_1 - \lambda_2) \omega_1 \omega_2$$

Let's consider again the "free" motion of a symmetric top, $\lambda_1 = \lambda_2$ w/ \hat{e}_3 being the symmetry axis.

$$\text{Then } \lambda_3 \dot{\omega}_3 = 0$$

$$\text{& } \dot{\omega}_1 = -\left(\frac{\lambda_3}{\lambda_1} - 1\right) \omega_2 \omega_3, \quad \dot{\omega}_2 = +\left(\frac{\lambda_3}{\lambda_1} - 1\right) \omega_1 \omega_3$$

$$\text{As before, introduce } \eta = \omega_1 + i\omega_2$$

$$\Rightarrow \dot{\eta} = i\Omega_b \eta \quad \text{where } \Omega_b = \left(\frac{\lambda_3}{\lambda_1} - 1\right) \omega_3$$

The general solution is $\eta = A e^{i\Omega_b t}$

So,

\downarrow free precession

$$\vec{\omega} = A \cos \Omega_b t \hat{e}_1 + A \sin \Omega_b t \hat{e}_2 + \omega_3 \hat{e}_3$$

$$\text{Notice that since } \vec{\omega} = \lambda_1 \omega_1 \hat{e}_1 + \lambda_2 \omega_2 \hat{e}_2 + \lambda_3 \omega_3 \hat{e}_3$$

$$= \lambda_1 A \cos \Omega_b t \hat{e}_1 + \lambda_2 A \sin \Omega_b t \hat{e}_2 + \lambda_3 \omega_3 \hat{e}_3$$

$$\text{BUT, } \lambda_1 = \lambda_2 \Rightarrow \vec{\omega} = \lambda_1 A (\cos \Omega_b t \hat{e}_1 + \sin \Omega_b t \hat{e}_2) + \lambda_3 \omega_3 \hat{e}_3$$

$$\text{Define } \vec{\omega}_\perp \text{ via } \vec{\omega} = \vec{\omega}_\perp + \omega_3 \hat{e}_3$$

$$\text{where } \vec{\omega}_\perp \cdot \hat{e}_3 = 0$$

$$\text{Then, } \vec{\omega} = \vec{\omega}_\perp + \lambda_3 \omega_3 \hat{e}_3$$

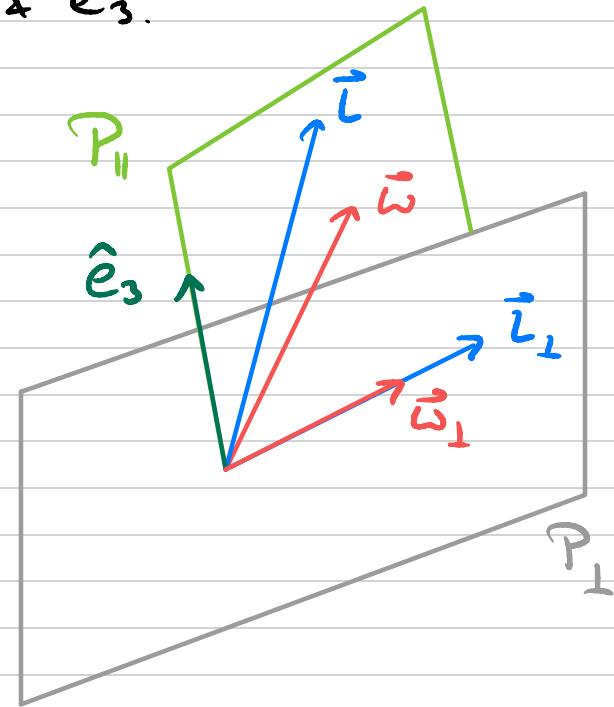
Geometrically, since the perpendicular component of $\vec{\omega}$, $\vec{\omega}_\perp = \lambda_1 \vec{\omega}_\perp$, is parallel to $\vec{\omega}_\perp$, $\vec{\omega}$ should be in the same plane as $\vec{\omega}$ & \hat{e}_3 .

Analytically, we can show three vectors, $\vec{A}, \vec{B}, \vec{C}$ are in the same plane iff $\vec{A} \cdot (\vec{B} \times \vec{C}) = 0$

$$\vec{\omega} \cdot (\hat{e}_3 \times \vec{\omega})$$

$$= \lambda_1 \vec{\omega}_\perp \cdot (\hat{e}_3 \times \vec{\omega}_\perp) + \lambda_3 \omega_3 \hat{e}_3 \cdot (\hat{e}_3 \times \vec{\omega}_\perp)$$

$$= 0$$



Thus, we see that $\vec{\omega}, \vec{\omega}_\perp$, & \hat{e}_3 all lie in the same plane.

What if $\lambda_1 \neq \lambda_2$?

For a body whose principal moments of inertia are all different, we may assume $\lambda_1 < \lambda_3 < \lambda_2$

to find

$$\left\{ \begin{array}{l} \dot{\omega}_1 = \left(\frac{\lambda_2 - \lambda_3}{\lambda_1} \omega_3 \right) \omega_2 \\ \dot{\omega}_2 = \left(\frac{\lambda_3 - \lambda_1}{\lambda_2} \omega_3 \right) \omega_1 \end{array} \right.$$

As long as ω_1 & ω_2 are small, ω_3 remains small & we can take ω_3 to be constant. Then, the two coupled equations for ω_1 & ω_2 can be solved easily.

$$\ddot{\omega}_1 = \left(\frac{\lambda_2 - \lambda_3}{\lambda_1} \omega_3 \right) \dot{\omega}_2 = \left[\frac{(\lambda_2 - \lambda_3)(\lambda_3 - \lambda_1)}{\lambda_1 \lambda_2} \omega_3^2 \right] \omega_1$$

Since $(\lambda_2 - \lambda_3)(\lambda_3 - \lambda_1) > 0$, this solution will have a real exponential solution — which is unstable & grows rapidly.

In fact, a very strong argument about this instability can be shown to be true :

There is no purely decaying solution $\sim e^{-\alpha t}$, $\alpha > 0$ for any initial conditions.

To see this, note that $\text{sgn}(\dot{\omega}_1) = \text{sgn}(\omega_3) \cdot \text{sgn}(\omega_2)$

For an initial value $\omega_1(t=0) = \omega_{1,0}$, we have

$$\text{sgn}(\dot{\omega}_1(t=0)) = \text{sgn}(\omega_3) \cdot \text{sgn}(\omega_{1,0}) .$$

Shortly after $t=0$, $\text{sgn}(\omega_2) = \text{sgn}(\dot{\omega}_2(t=0)) = \text{sgn}(\omega_3) \cdot \text{sgn}(\omega_{1,0})$

So, $\text{sgn}(\dot{\omega}_1(t=0)) = \text{sgn}(\omega_3) \cdot \text{sgn}(\omega_2) = \text{sgn}(\omega_{1,0})$.

This is a constraint that must be satisfied by all initial conditions & solutions.

⇒ It is NOT satisfied by a purely decaying solution:

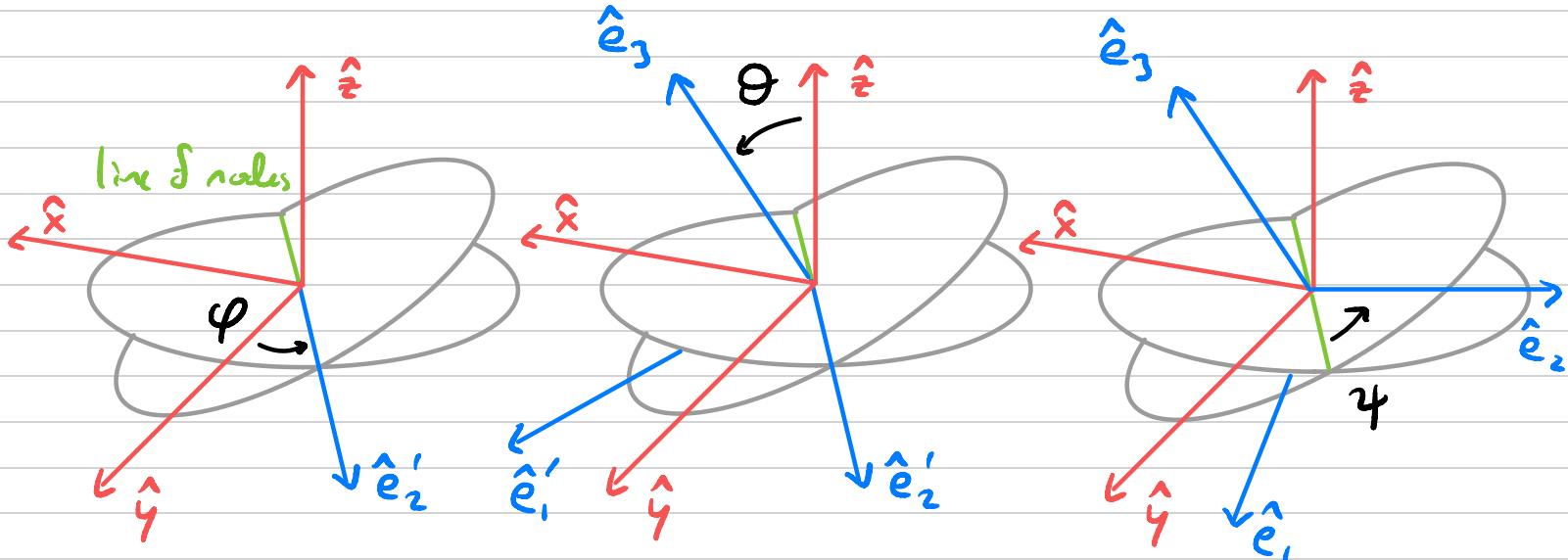
$$\omega_1 \sim e^{-\alpha t} \Rightarrow \dot{\omega}_{1,0} = -\alpha \omega_{1,0}$$

$$\Rightarrow \text{sgn}(\dot{\omega}_{1,0}) = -\text{sgn}(\omega_{1,0})$$

which is a contradiction.

Euler Angles

The Euler angles are a special set of angles which are frequently used to describe rotational motion.



From some fixed coordinate system \$(x, y, z)\$ [zyz convention]

1. Rotate about \$\hat{z}\$ by \$\varphi\$
2. Rotate about \$\hat{e}_2'\$ by \$\theta\$
3. Rotate about \$\hat{e}_3\$ by \$\psi\$

By definition, $\vec{\omega} = \dot{\varphi} \hat{z} + \dot{\theta} \hat{e}_1' + \dot{\psi} \hat{e}_3$

Can decompose \hat{z} , \hat{e}_1' , & \hat{e}_2' into \hat{e}_1 , \hat{e}_2 , \hat{e}_3

$$\left\{ \begin{array}{l} \hat{z} = \cos \theta \hat{e}_3 - \sin \theta \hat{e}_1' \\ \hat{e}_1' = \cos \psi \hat{e}_1 - \sin \psi \hat{e}_2 \\ \hat{e}_2' = \sin \psi \hat{e}_1 + \cos \psi \hat{e}_2 \end{array} \right.$$

Therefore

$$\vec{\omega} = (-\dot{\varphi} \sin \theta \cos \psi + \dot{\theta} \sin \psi) \hat{e}_1 + (\dot{\varphi} \sin \theta \sin \psi + \dot{\theta} \cos \psi) \hat{e}_2 + (\dot{\varphi} \cos \theta + \dot{\psi}) \hat{e}_3$$

We can also express $\vec{\omega}$ in terms of $\hat{x}, \hat{y}, \hat{z}$

$$\left\{ \begin{array}{l} \hat{e}'_1 = -\sin \varphi \hat{x} + \cos \varphi \hat{y} \\ \hat{e}'_3 = \sin \theta \cos \varphi \hat{x} + \sin \theta \sin \varphi \hat{y} + \cos \theta \hat{z} \end{array} \right.$$

Therefore,

$$\vec{\omega} = (-\dot{\theta} \sin \varphi + \dot{\psi} \sin \theta \cos \varphi) \hat{x} + (\dot{\theta} \cos \varphi + \dot{\psi} \sin \theta \sin \varphi) \hat{y} + (\dot{\varphi} + \dot{\psi} \cos \theta) \hat{z}$$

Note that for a body w/ 2 axis of symmetry parallel to \hat{e}_3 ,
then $\lambda_1 = \lambda_2$ for any chosen axes \perp to \hat{e}_3 .

For example, \hat{e}'_1 & \hat{e}'_2 work just as well as \hat{e}_1 & \hat{e}_2

$$\Rightarrow \vec{\omega} = -\dot{\varphi} \sin \theta \hat{e}'_1 + \dot{\theta} \hat{e}'_2 + (\dot{\varphi} \cos \theta + \dot{\psi}) \hat{e}_3$$

We find then ($\lambda_1 = \lambda_2$)

$$\vec{L} = I\vec{\omega}$$

$$= (-\lambda_1 \dot{\varphi} \sin \theta) \hat{e}_1' + \lambda_1 \dot{\theta} \hat{e}_2' + \lambda_3 (\dot{\varphi} \cos \theta + \dot{\psi}) \hat{e}_3$$

Note that

$$\hat{e}_1' \cdot \hat{z} = -\sin \theta, \quad \hat{e}_2' \cdot \hat{z} = 0, \quad \hat{e}_3 \cdot \hat{z} = \cos \theta$$

$$\Rightarrow \begin{cases} L_z = \vec{L} \cdot \hat{z} = \lambda_1 \dot{\varphi} \sin^2 \theta + L_3 \cos \theta \\ L_3 = \lambda_3 (\dot{\varphi} \cos \theta + \dot{\psi}) \end{cases}$$

Finally, the kinetic energy can be written

$$T = \frac{1}{2} \vec{\omega} \cdot \vec{L} = \frac{1}{2} \lambda_1 (\dot{\varphi}^2 \sin^2 \theta + \dot{\theta}^2) + \frac{1}{2} \lambda_3 (\dot{\varphi} \cos \theta + \dot{\psi})^2$$

Spinning Top

We are now in position to solve for the full motion of a symmetric spinning top.

The Lagrangian is

$$L = T - U$$

$$= \frac{1}{2} \lambda_1 (\dot{\varphi}^2 \sin^2 \theta + \dot{\theta}^2) + \frac{1}{2} \lambda_3 (\dot{\varphi} \cos \theta + \dot{\psi})^2 - M g R \cos \theta$$

Notice that φ is cyclic

$$\rho_{\varphi} = \frac{\partial L}{\partial \dot{\varphi}} = \lambda_1 \dot{\varphi} \sin^2 \theta + \lambda_3 \cos \theta (\dot{\varphi} \cos \theta + \dot{\psi}) \\ = \text{const.} \equiv L_2$$

Notice that also φ is cyclic

$$\rho_{\varphi} = \frac{\partial L}{\partial \dot{\varphi}} = \lambda_3 (\dot{\varphi} \cos \theta + \dot{\psi}) = \text{const.} \equiv L_3$$

Finally, for θ

$$\frac{\partial L}{\partial \theta} = \frac{d}{dt} \frac{\partial L}{\partial \dot{\theta}} \Rightarrow \lambda_1 \ddot{\theta} = \lambda_1 \dot{\varphi}^2 \sin \theta \cos \theta - \lambda_3 \dot{\varphi} \sin \theta (\dot{\varphi} \cos \theta + \dot{\psi})$$

$$+ MgR \sin \theta$$

The total energy is conserved

$$E = T + U$$

$$= \frac{1}{2} \lambda_1 (\dot{\varphi}^2 \sin^2 \theta + \dot{\theta}^2) + \frac{1}{2} \lambda_3 (\dot{\varphi} \cos \theta + \dot{\psi})^2 + MgR \cos \theta$$

Writing in terms of L_2 & L_3

$$E = \frac{1}{2} \lambda_1 \dot{\theta}^2 + \frac{1}{2} \lambda_1 \left(\frac{L_2 - L_3 \cos \theta}{\lambda_1 \sin^2 \theta} \right)^2 \sin^2 \theta$$

$$+ \frac{1}{2} \lambda_3 \left(\frac{L_3}{\lambda_3} \right)^2 + MgR \cos \theta$$

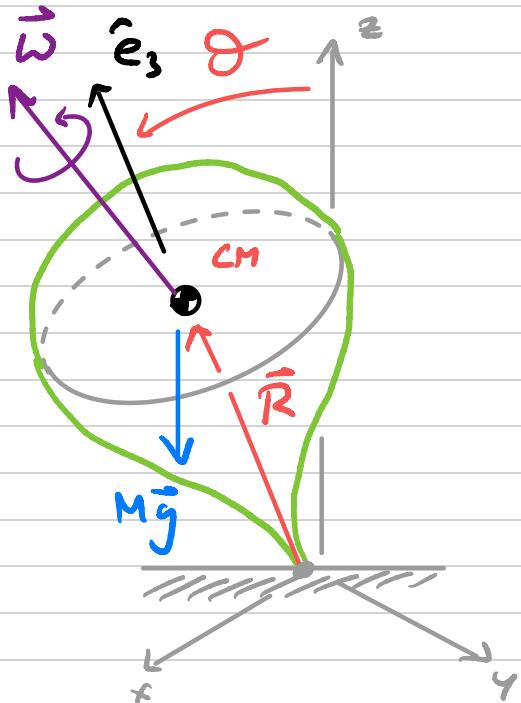
We can write this as

$$E = \frac{1}{2} \lambda_1 \dot{\theta}^2 + U_{\text{eff}}(\theta)$$

where the effective potential is

$$U_{\text{eff}}(\theta) = \frac{(L_z - L_3 \cos \theta)^2}{2 \lambda_1 \sin^2 \theta} + \frac{L_3^2}{2 \lambda_3} + MgR \cos \theta$$

Depending on the energy of the top, the angle θ = angle between the symmetry axis & the z-direction will vary between two limiting values



If the energy is exactly matched to be at the minimum of U_{eff} , θ will be fixed. An especially simple example arises, since

$$\dot{\varphi} = \frac{L_z - L_3 \cos \theta}{\lambda_1 \sin^2 \theta} = \text{const.}$$

Since $\dot{\phi} \equiv \Omega$ is constant, the top will precess at a fixed angle θ & constant angular velocity.

From the expression for ω_{xy} ,

$$\frac{d\Omega_{xy}}{d\theta} = 0 \Rightarrow \frac{d\Omega_{xy}}{d\cos\theta} = 0$$

$$\Rightarrow \frac{(L_2 - L_3 \cos\theta)^2}{\lambda_1 \sin^4\theta} \cos\theta - L_3 \cdot \frac{L_2 - L_3 \cos\theta}{\lambda_1 \sin^2\theta} + MgR = 0$$

Since $\Omega = \frac{L_2 - L_3 \cos\theta}{\lambda_1 \sin^2\theta}$, we find

$$\underbrace{\lambda_1 \cos\theta \Omega^2}_a - \underbrace{L_3 \Omega}_b + \underbrace{MgR}_c = 0$$

$$\Rightarrow a\Omega^2 + b\Omega + c = 0$$

$$\text{There are two solutions : } \Omega \pm = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

When $b^2 \gg ac$, we expand $\sqrt{b^2 - 4ac} \approx b \left(1 - \frac{2ac}{b^2}\right)$

$$\text{So, } \begin{cases} \Omega_+ \approx -\frac{c}{b} = \frac{MgR}{L_3} = \frac{MgR}{\lambda_3 \omega_3} \leftarrow \text{precession} \\ \Omega_- \approx -\frac{b}{a} = \frac{L_3}{\lambda_1 \cos\theta} \leftarrow \text{free precession} \end{cases}$$

For the angular momentum, we have

$$\vec{L} = -\lambda_1 \dot{\varphi} \sin \theta \hat{e}_1 + L_3 \hat{e}_3$$

Since \hat{z} , \hat{e}_1 , & \hat{e}_3 are all in the same plane,
the horizontal component of \vec{L} is

$$L_h = -\lambda_1 \dot{\varphi} \sin \theta \cos \theta + L_3 \sin \theta$$

For the large solution $S2_- \approx -\frac{b}{a} = +\frac{L_3}{\lambda_1 \cos \theta}$,
we find

$$L_h \approx -\lambda_1 \cdot \frac{L_3}{\lambda_1 \cos \theta} \sin \theta \cos \theta + L_3 \sin \theta = 0$$

That is, \vec{L} is nearly vertical.