

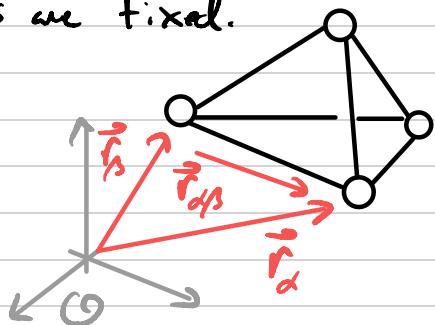
Physics 303  
Classical Mechanics II

Rigid Body Motion

A.W. Jackura — William & Mary

## Rigid Bodies

A rigid body is an abstract notion of a collection of particles / objects that move together in such a way to maintain their shape, i.e., their relative positions are fixed.



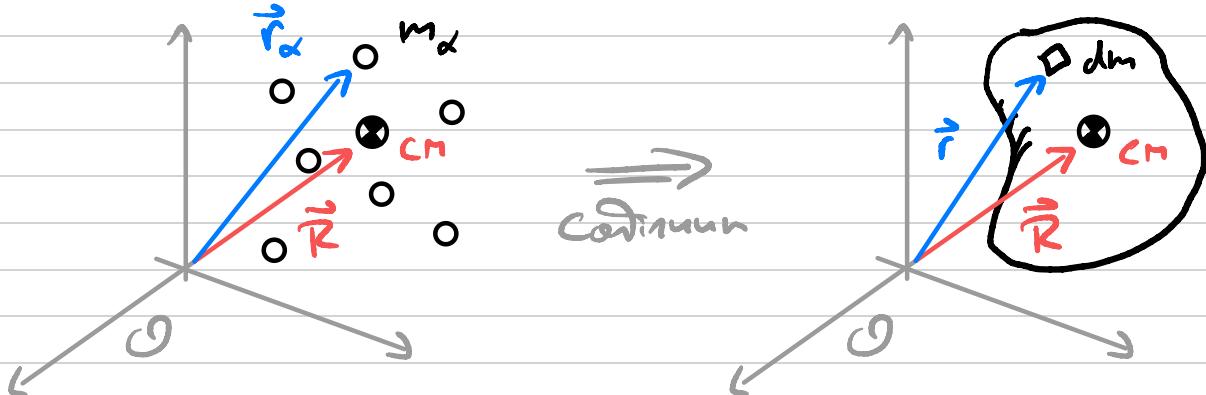
$$\vec{r}_{\alpha\beta} = \vec{r}_\alpha - \vec{r}_\beta \\ \Rightarrow |\vec{r}_{\alpha\beta}| = \text{constant}$$

This is an idealization, as atoms and molecules vibrate meaning no object is completely rigid. However, this is a good starting point to build on.

Since the distances between particles are fixed, the system is highly constrained. For  $N$  particles, there are  $3N$  coordinates needed. But, since the distances between particles is fixed, the rigid body only needs 6 degrees of freedom.

- 3 to specify CM
- 3 to specify orientation

Consider system of  $N$  particles  $\alpha = 1, \dots, N$  with masses  $m_\alpha$  and positions  $\vec{r}_\alpha$  measured w.r.t. O



The CM is

$$\vec{R} = \frac{1}{M} \sum_{\alpha=1}^N m_\alpha \vec{r}_\alpha , \quad M = \sum_{\alpha} m_\alpha$$

If the particles are small and numerous in a small volume, we can define a density  $\rho(\vec{r})$  as

$$\Delta m = \rho(\vec{r}) \Delta x \Delta y \Delta z$$

then we can consider the rigid body of a continuous distribution of mass

$$M = \int dm = \int \rho(\vec{r}) dV$$

and CM

$$\vec{R} = \frac{1}{M} \int \vec{r} dm$$

We will switch between a discrete and continuous picture as needed.

## Momentum & Angular Momentum

The total momentum of the system is

$$\vec{P} = \sum_{\alpha} \vec{p}_{\alpha} = \sum_{\alpha} m_{\alpha} \dot{\vec{r}}_{\alpha} = M \dot{\vec{R}}$$

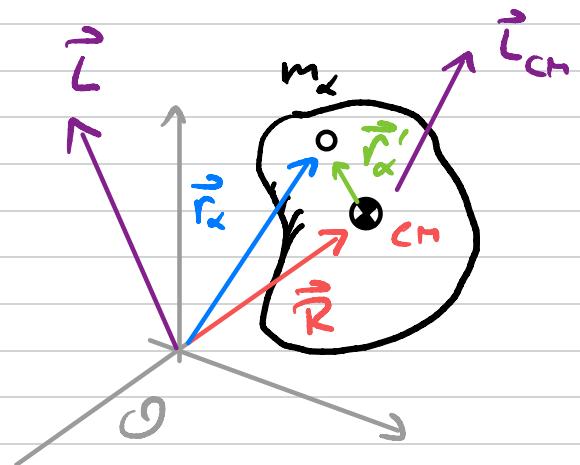
If the system is exposed to an external force  $\vec{F}^{\text{ext}}$ , then NII for the CM is

$$\ddot{\vec{P}} = \vec{F}^{\text{ext}} = M \ddot{\vec{R}}$$

Next we consider angular momentum.

Let  $\vec{l}$  be the angular momentum of the system w.r.t O.

We want to split  $\vec{l}$  into an  $\vec{l}_{\text{CM}}$ , the angular momentum of the body about the CM, and the  $\vec{l}_{\text{ext}}$ , the angular momentum of the CM.



The angular momentum of  $\alpha$  about O is

$$\vec{l}_{\alpha} = \vec{r}_{\alpha} \times \vec{p}_{\alpha} = \vec{r}_{\alpha} \times m_{\alpha} \dot{\vec{r}}_{\alpha}$$

So the total angular momentum is  $\vec{l} = \sum_{\alpha} \vec{l}_{\alpha}$

$$\text{So, } \vec{L} = \sum_{\alpha} \vec{l}_{\alpha} = \sum_{\alpha} \vec{r}_{\alpha} \times m_{\alpha} \dot{\vec{r}}_{\alpha}$$

Now, let  $\vec{r}'_{\alpha}$  be location of  $\alpha$  w.r.t. CM

$$\vec{r}_{\alpha} = \vec{R} + \vec{r}'_{\alpha}$$

So, find

$$\begin{aligned} \vec{L} &= \sum_{\alpha} (\vec{R} + \vec{r}'_{\alpha}) \times m_{\alpha} (\dot{\vec{R}} + \dot{\vec{r}}'_{\alpha}) \\ &= \sum_{\alpha} \vec{R} \times m_{\alpha} \dot{\vec{R}} + \sum_{\alpha} \vec{R} \times m_{\alpha} \dot{\vec{r}}'_{\alpha} \\ &\quad + \sum_{\alpha} \vec{r}'_{\alpha} \times m_{\alpha} \dot{\vec{R}} + \sum_{\alpha} \vec{r}'_{\alpha} \times m_{\alpha} \dot{\vec{r}}'_{\alpha} \end{aligned}$$

$$\text{Recall } M = \sum_{\alpha} m_{\alpha}$$

$$\begin{aligned} \Rightarrow \vec{L} &= \vec{R} \times M \dot{\vec{R}} + \vec{R} \times \sum_{\alpha} m_{\alpha} \dot{\vec{r}}'_{\alpha} \\ &\quad + \left( \sum_{\alpha} m_{\alpha} \vec{r}'_{\alpha} \right) \times \dot{\vec{R}} + \sum_{\alpha} \vec{r}'_{\alpha} \times m_{\alpha} \dot{\vec{r}}'_{\alpha} \end{aligned}$$

Now,  $\sum_{\alpha} m_{\alpha} \vec{r}'_{\alpha} = \vec{0}$  since this is location of CM  
relative to CM (of course)

like wise,  
 $\sum_{\alpha} m_{\alpha} \dot{\vec{r}}'_{\alpha} = \vec{0}$

$$\text{So, } \vec{L} = \vec{R} \times \vec{P} + \sum_{\alpha} \vec{r}_{\alpha}' \times m_{\alpha} \dot{\vec{r}}_{\alpha}'$$

↑  
angular momentum of CM  
relative to O

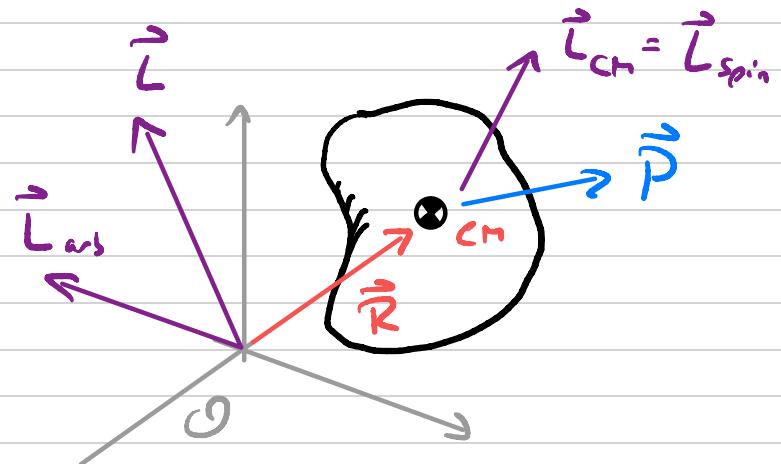
↑  
angular momentum relative  
to the CM

Define

$$\boxed{\vec{L}_{CM} = \vec{L}_{Spin} = \sum_{\alpha} \vec{r}_{\alpha}' \times m_{\alpha} \dot{\vec{r}}_{\alpha}'}$$

$$\boxed{\vec{L}_{orb} = \vec{R} \times \vec{P}}$$

$$\Rightarrow \boxed{\vec{L} = \vec{L}_{orb} + \vec{L}_{CM}}$$



This separation is often useful

as both are approximately conserved

$$\dot{\vec{L}}_{orb} = \dot{\vec{R}} \times \vec{P} + \vec{R} \times \dot{\vec{P}} = \vec{R} \times \vec{F}_{ext}^{\alpha} ; \quad \vec{F}_{ext}^{\alpha} = \sum_{\alpha} \vec{F}_{\alpha}^{\alpha}$$

We know  $\dot{\vec{L}} = \vec{\tau}^{\alpha}$ , the external torque relative to O

$$\begin{aligned} \text{So, } \dot{\vec{L}}_{CM} &= \dot{\vec{L}} - \dot{\vec{L}}_{orb} = \vec{\tau}^{\alpha} - \vec{R} \times \vec{F}_{ext}^{\alpha} \\ &= \sum_{\alpha} (\vec{r}_{\alpha} - \vec{R}) \times \vec{F}_{\alpha}^{\alpha} = \vec{\tau}_{CM}^{\alpha} \end{aligned}$$

↑  
External torque relative to CM

## Kinetic & Potential Energy

The total kinetic energy of  $N$  particles is

$$T = \sum_{\alpha=1}^N \frac{1}{2} m_\alpha \dot{\vec{r}}_\alpha^2$$

As before, write  $\vec{r}_\alpha = \vec{R} + \vec{r}'_\alpha$ ,  $\vec{r}'_\alpha$  position relative to CM

$$\Rightarrow \dot{\vec{r}}_\alpha^2 = \dot{\vec{R}}^2 + \dot{\vec{r}}'^2_\alpha + 2\vec{R} \cdot \vec{r}'_\alpha$$

$$\Rightarrow T = \frac{1}{2} \sum_{\alpha} m_\alpha \dot{\vec{R}}^2 + \frac{1}{2} \sum_{\alpha} m_\alpha \dot{\vec{r}}'^2_\alpha + \dot{\vec{R}} \cdot \underbrace{\sum_{\alpha} m_\alpha \vec{r}'_\alpha}_{=0 \text{ as before}}$$

Define KE relative to CM

$$T_{CM} = \frac{1}{2} \sum_{\alpha} m_\alpha \dot{\vec{r}}'^2_\alpha$$

So,

$$T = \frac{1}{2} M \dot{\vec{R}}^2 + T_{CM}$$

KE of CM

For conservative forces, can write potential energy  
and decompose as

$$U = U_{\text{ext}} + U_{\text{int}}$$

$$\begin{matrix} \uparrow & \uparrow \\ \text{(external) PE} & \text{(internal) PE} \end{matrix}$$

where  $U_{\text{int}} = \sum_{\alpha < \beta} U_{\alpha\beta} (|\vec{r}_\alpha - \vec{r}_\beta|)$

assuming central forces

since  $|\vec{r}_{\alpha\beta}| = \text{const.}$ ,

$$\Rightarrow U_{\text{int}} = \text{const.}$$

$\therefore U_{\text{int}}$  is irrelevant for rigid body dynamics

## Rotation about a fixed Axis

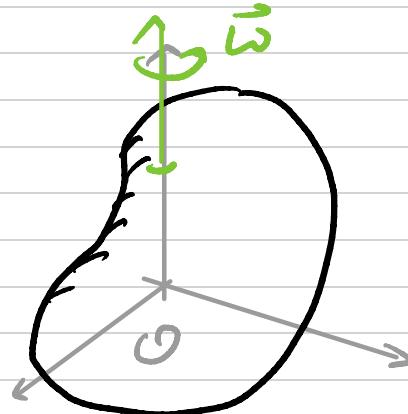
Here we consider the rotation of a rigid body about some fixed axis. Since the axis is fixed, let us define it as the z-axis.

$$\Rightarrow \vec{\omega} = (0, 0, \omega)$$

If the body consists of N particles, then

$$\vec{l} = \sum_{\alpha} \vec{l}_{\alpha}$$

$$= \sum_{\alpha} \vec{r}_{\alpha} \times m_{\alpha} \vec{v}_{\alpha}$$



Since the axis of rotation is fixed,  $\vec{v}_{\alpha} = \vec{\omega} \times \vec{r}_{\alpha}$ ,

$$\text{So, with } \vec{r}_{\alpha} = (x_{\alpha}, y_{\alpha}, z_{\alpha})$$

$$\Rightarrow \vec{v}_{\alpha} = (-\omega y_{\alpha}, \omega x_{\alpha}, 0)$$

$$\therefore \vec{l}_{\alpha} = m_{\alpha} \vec{r}_{\alpha} \times \vec{v}_{\alpha}$$

$$= m_{\alpha} \omega (-z_{\alpha} x_{\alpha}, -z_{\alpha} y_{\alpha}, x_{\alpha}^2 + y_{\alpha}^2)$$

thus,  $\vec{l} = \sum_{\alpha} \vec{l}_{\alpha}$  is total angular momentum.

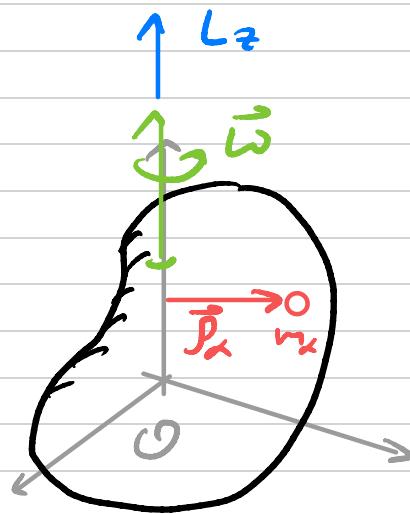
Let's examine components of  $\vec{L}$ .

The  $z$ -component is

$$L_z = \sum_{\alpha} m_{\alpha} (x_{\alpha}^2 + y_{\alpha}^2) \omega$$

Notice that

$$\rho_{\alpha}^2 = x_{\alpha}^2 + y_{\alpha}^2$$



with  $\rho_{\alpha}$  being the distance  
to any point from the  $z$ -axis.

Thus,  $L_z = \sum_{\alpha} m_{\alpha} \rho_{\alpha}^2 \omega \equiv I_z \omega$

where  $I_z = \sum_{\alpha} m_{\alpha} \rho_{\alpha}^2$

is the moment of inertia about the  $z$ -axis.

The kinetic energy is then

$$T = \frac{1}{2} \sum_{\alpha} m_{\alpha} v_{\alpha}^2 .$$

Since  $v_{\alpha} = \rho_{\alpha} \omega$  for a rotation about fixed  $z$ -axis,

$$\Rightarrow T = \frac{1}{2} \sum_{\alpha} m_{\alpha} \rho_{\alpha}^2 \omega^2 = \frac{1}{2} I_z \omega^2 .$$

These should be familiar results from Phys 201.

Notice though that there is non-zero components for  $L_x$  &  $L_y$ ,

$$L_x = - \sum_{\alpha} m_{\alpha} x_{\alpha} z_{\alpha} \omega$$

$$L_y = - \sum_{\alpha} m_{\alpha} y_{\alpha} z_{\alpha} \omega$$

we define the products of inertia about the  $z$ -axis as

$$L_x = I_{xz} \omega, \quad L_y = I_{yz} \omega$$

with  $I_{xz} = - \sum_{\alpha} m_{\alpha} x_{\alpha} z_{\alpha}$

$$I_{yz} = - \sum_{\alpha} m_{\alpha} y_{\alpha} z_{\alpha}$$

Obviously,  $\vec{L}$  is not parallel to  $\vec{\omega}$ !

$$\vec{L} = (I_{xz} \omega, I_{yz} \omega, I_{zz} \omega)$$

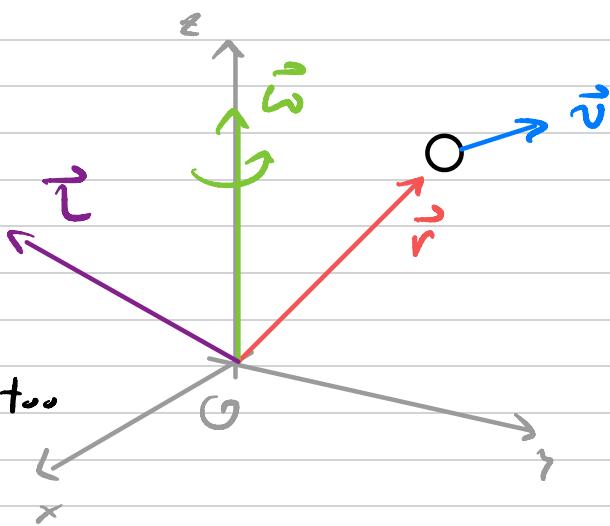
with  $I_{zz} \equiv I_z$ . Consider a single point particle,

$$\vec{L} = \vec{r} \times m \vec{v}$$

$$\text{if } \vec{v} \parallel -\hat{x}$$

$\vec{r}$  lies in  $yz$  plane,

then  $\vec{L}$  lies in  $yz$  plane too.



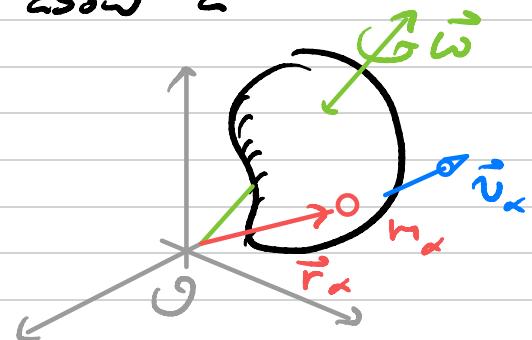
## The Inertia Tensor

We saw that  $\vec{L} \neq I \vec{\omega}$  with  $I$  being a number.

In general,  $I$  is a  $3 \times 3$  symmetric tensor.

Let's see by consider a rotation about a general fixed axis  $\vec{\omega}$ .

$$\begin{aligned}\vec{L} &= \sum_{\alpha} \vec{r}_{\alpha} \times m_{\alpha} \vec{v}_{\alpha} \\ &= \sum_{\alpha} m_{\alpha} \vec{r}_{\alpha} \times (\vec{\omega} \times \vec{r}_{\alpha})\end{aligned}$$



Recall identity  $\vec{A} \times (\vec{B} \times \vec{C}) = (\vec{A} \cdot \vec{C}) \vec{B} - (\vec{A} \cdot \vec{B}) \vec{C}$

$$\Rightarrow \vec{L} = \sum_{\alpha} m_{\alpha} \left[ \vec{r}_{\alpha}^2 \vec{\omega} - (\vec{r}_{\alpha} \cdot \vec{\omega}) \vec{r}_{\alpha} \right]$$

(Or look at  $i^{th}$ -component,

$$\begin{aligned}L_i &= \sum_{\alpha} m_{\alpha} \left[ \vec{r}_{\alpha}^2 \omega_i - \left( \sum_j r_{\alpha,j} \omega_j \right) r_{\alpha,i} \right] \\ &= \sum_j \left[ \sum_{\alpha} m_{\alpha} \left( \vec{r}_{\alpha}^2 \delta_{ij} - r_{\alpha,i} r_{\alpha,j} \right) \right] \omega_j \\ &= \sum_j I_{ij} \omega_j\end{aligned}$$

we define the Inertia tensor as  $\mathbb{I}$  with matrix elements

$$I_{ij} = \sum_{\alpha} m_{\alpha} (\vec{r}_{\alpha}^2 \delta_{ij} - r_{\alpha,i} r_{\alpha,j})$$

In terms of a continuous distribution,

$$I_{ij} = \int dm (\vec{r} \delta_{ij} - r_i r_j)$$

By inspection,  $\mathbb{I}$  is symmetric,  $\mathbb{I}^T = \mathbb{I}$

$$\text{or } I_{ij} = I_{ji}.$$

It characterizes an object's resistance to change in rotational motion

$$\vec{\mathcal{L}} = \mathbb{I} \cdot \vec{\omega} \quad \text{or} \quad L_i = \sum_j I_{ij} \omega_j$$

The Cartesian components are

$$\mathbb{I} = \begin{pmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{pmatrix}$$

$$\text{with } I_{xx} \equiv I_x = \sum_\alpha m_\alpha (\vec{r}_\alpha^2 - x_\alpha^2) = \sum_\alpha m_\alpha (y_\alpha^2 + z_\alpha^2)$$

$$I_{xy} = - \sum_\alpha m_\alpha x_\alpha y_\alpha \quad \text{etc...}$$

Explicitly,  $\vec{\tau} = \mathbb{I} \cdot \vec{\omega}$  is

$$\begin{pmatrix} \tau_x \\ \tau_y \\ \tau_z \end{pmatrix} = \begin{pmatrix} I_{xx} & I_{xy} & I_{xz} \\ I_{yx} & I_{yy} & I_{yz} \\ I_{zx} & I_{zy} & I_{zz} \end{pmatrix} \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix}$$

The media tensor is a  $3 \times 3$  symmetric matrix

which must transform as  $\mathbb{I}' = R \mathbb{I} R^T$

$$\text{or } I'_{ij} = \sum_{m,n} R_{im} R_{jn} I_{mn}$$

↑ rotation matrix  
 C this is what makes  $I$  a tensor

To see this, note that  $\vec{\tau}$  &  $\vec{\omega}$  are physical vectors which must transform as  $\vec{\tau}' = R \cdot \vec{\tau}$ ,  $\vec{\omega}' = R \cdot \vec{\omega}$  under a rotation  $R$ .

$$\therefore \vec{\tau}' = R \cdot \vec{\tau} = R \cdot \mathbb{I} \cdot \vec{\omega}$$

$$\begin{aligned} &= R \cdot \mathbb{I} \cdot R^T R \vec{\omega} && \text{C insert } 1 = R^{-1} \cdot R \\ &= (R \cdot \mathbb{I} \cdot R^T) \cdot \vec{\omega}' && = R^T \cdot R \text{ since} \\ &= \mathbb{I}' \cdot \vec{\omega}' && \text{R is orthogonal} \end{aligned}$$

$\Rightarrow$  require  $\mathbb{I}' = R \cdot \mathbb{I} \cdot R^T$  if  $\vec{\tau}, \vec{\omega}$  are physical vectors.

The kinetic energy is

$$\begin{aligned}
 T &= \frac{1}{2} \sum_{\alpha} m_{\alpha} \dot{\vec{r}}_{\alpha}^2 = \frac{1}{2} \sum_{\alpha} m_{\alpha} (\vec{\omega} \times \vec{r}_{\alpha})^2 \\
 &= \frac{1}{2} \sum_{\alpha} m_{\alpha} \sum_i (\vec{\omega} \times \vec{r}_{\alpha})_i (\vec{\omega} \times \vec{r}_{\alpha})_i \\
 &= \frac{1}{2} \sum_{\alpha} m_{\alpha} \sum_i \sum_{j,k} \epsilon_{ijk} \omega_j r_{\alpha,k} \sum_{l,m} \epsilon_{ilm} \omega_l r_{\alpha,m}
 \end{aligned}$$

Note the relation  $\sum_i \epsilon_{ijk} \epsilon_{ilm} = \delta_{jl} \delta_{km} - \delta_{kl} \delta_{jm}$

$$\begin{aligned}
 \Rightarrow T &= \frac{1}{2} \sum_{\alpha} m_{\alpha} \sum_{j,k} \sum_{l,m} (\delta_{jl} \delta_{km} - \delta_{kl} \delta_{jm}) \omega_j \omega_l r_{\alpha,k} r_{\alpha,m} \\
 &= \frac{1}{2} \sum_{i,j} \omega_i \left[ \sum_{\alpha} m_{\alpha} (\vec{r}_{\alpha}^2 \delta_{ij} - r_{\alpha,i} r_{\alpha,j}) \right] \omega_j \\
 &= \frac{1}{2} \sum_{i,j} \omega_i I_{ij} \omega_j
 \end{aligned}$$

$$\Rightarrow T = \frac{1}{2} \vec{\omega}^T \mathbb{I} \cdot \vec{\omega} = \frac{1}{2} \vec{\omega} \cdot \vec{\mathbb{I}}$$

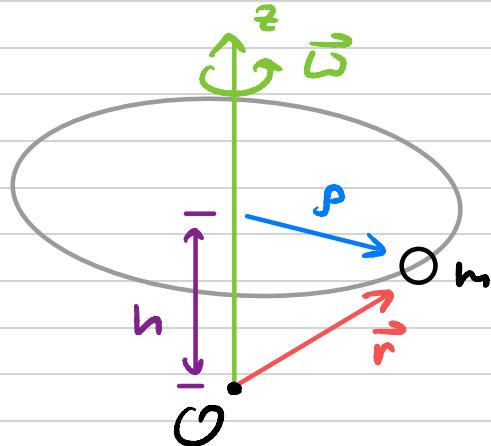
Example - Consider a point-particle with mass  $m$  rotating around  $z$ -axis at a constant radius  $\rho$ , height  $h$  above origin, & angular velocity  $\vec{\omega}$ .

Compute the elements of the inertia tensor.

$$\vec{\omega} = (0, 0, \omega)$$

& position

$$\vec{r}(t) = \rho \cos \omega t \hat{x} + \rho \sin \omega t \hat{y} + h \hat{z}$$



Since the rotation is about  $z$ , there are only 3 non-zero components,  $I_{zz}, I_{xz} = I_{zx}, I_{yz} = I_{zy}$

$$I_{zz} = m(x^2 + y^2) = m\rho^2$$

$$I_{xz} = -mxz = -mh\rho \cos \omega t$$

$$I_{yz} = -myz = -mh\rho \sin \omega t$$

$$\text{So, } \vec{L} = \vec{I} \cdot \vec{\omega} = I_{xz} \omega \hat{x} + I_{yz} \omega \hat{y} + I_{zz} \omega \hat{z}$$

$$= -mh\rho \omega (\cos \omega t \hat{x} + \sin \omega t \hat{y}) + m\rho^2 \omega \hat{z}$$

Exercise: compare  $\vec{L}$  to  $\vec{L} = \vec{r} \times m\vec{v}$ .

Notice that if  $\vec{\omega} = 0$ , i.e., the origin  
is in the plane of rotation

$$\Rightarrow \vec{I}_{\vec{\omega}=0} = I_z \vec{\omega}$$

which is the result from Phys 101. ■

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Example - Compute the inertia tensor

of a solid cube of mass  $M$  and side length  $a$   
about (a) the corner, (b) the center.

Compute  $\vec{I}$  for both cases given

$$\vec{\omega}_1 = \omega(1, 0, 0) \quad \text{&} \quad \vec{\omega}_2 = \frac{\omega}{\sqrt{3}}(1, 1, 1).$$

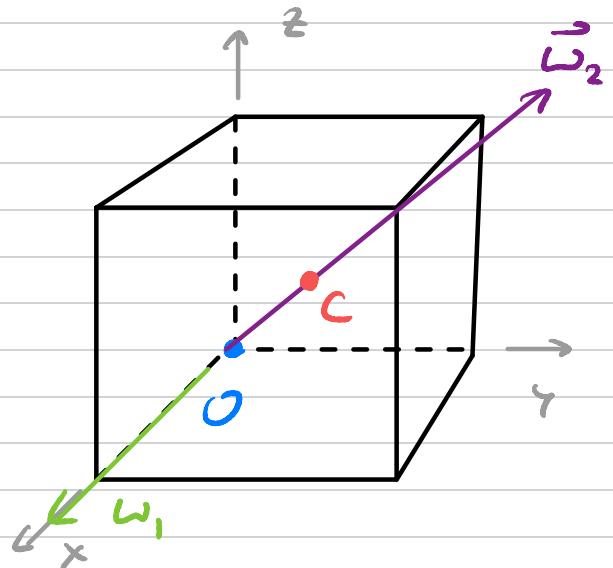
For a continuous distribution

$$I_{ij} = \int (\vec{r}^2 \delta_{ij} - r_i r_j) \rho dV$$

$$\text{where } \rho = \frac{M}{a^3}$$

- Corner (point O)  $\Rightarrow (0, 0, 0)$

- Center (point C)  $\Rightarrow \left(\frac{a}{2}, \frac{a}{2}, \frac{a}{2}\right)$



(a) for point O,

$$\begin{aligned}
 I_x(O) &= \int_0^a dx \int_0^a dy \int_0^a dz \rho (y^2 + z^2) \\
 &= \rho \left( \int_0^a dx \right) \left( \int_0^a dy y^2 \right) \left( \int_0^a dz z^2 \right) \\
 &\quad + \rho \left( \int_0^a dx \right) \left( \int_0^a dy \right) \left( \int_0^a dz z^2 \right) \\
 &= \rho \cdot a \cdot \frac{a^3}{3} \cdot a + \rho \cdot a \cdot a \cdot \frac{a^3}{3} \\
 &= \frac{2}{3} \rho a^5 = \frac{2}{3} \left( \frac{M}{a^3} \right) a^5
 \end{aligned}$$

$$\Rightarrow I_x(O) = \frac{2}{3} Ma^2$$

By inspection, find  $I_x(O) = I_y(O) = I_z(O) = \frac{2}{3} Ma^2$

The product of inertia is

$$\begin{aligned}
 I_{xy}(O) &= -\rho \int_0^a dx \int_0^a dy \int_0^a dz \cdot xy \\
 &= -\left( \frac{M}{a^3} \right) \frac{a^2}{2} \cdot \frac{a^2}{2} \cdot a = -\frac{1}{4} Ma^2
 \end{aligned}$$

By inspection, find all products of inertia are equal

$\zeta_0$ ,

$$\mathbb{II}(0) = Ma^2 \begin{pmatrix} 2/3 & -1/4 & -1/4 \\ -1/4 & 2/3 & -1/4 \\ -1/4 & -1/4 & 2/3 \end{pmatrix}$$

(b) for point C,

$$\begin{aligned} I_x(C) &= \rho \int_{-a/2}^{a/2} dx \int_{-a/2}^{a/2} dy \int_{-a/2}^{a/2} dz (y^2 + z^2) \\ &= \frac{M}{a^3} \cdot a \cdot a \cdot \frac{1}{3} \cdot 2 \left[ \left(\frac{a}{2}\right)^3 + \left(\frac{a}{2}\right)^3 \right] \\ &= \frac{1}{6} Ma^2 \end{aligned}$$

Likewise,  $I_y(C) = I_z(C) = \frac{1}{6} Ma^2$

$$I_{xy}(C) = \rho \int_{-a/2}^{a/2} dx \int_{-a/2}^{a/2} dy \int_{-a/2}^{a/2} dz xy = 0$$

↳ odd integrand  
over even interval

$$\Rightarrow \text{All } I_{ij} = 0 \text{ for } i \neq j$$

$$\Rightarrow \mathbb{II}(C) = \frac{1}{6} Ma^2 \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$= \frac{1}{6} Ma^2 \mathbb{II} .$$

The angular momenta are

$$\vec{L}_1(\omega) = \underline{\underline{I}}(\omega) \cdot \vec{\omega}_1,$$

$$= Ma^2 \omega \begin{pmatrix} 2/3 & -1/4 & -1/4 \\ -1/4 & 2/3 & -1/4 \\ -1/4 & -1/4 & 2/3 \end{pmatrix} \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}$$

$$= \frac{1}{12} Ma^2 \omega (8, -3, -3)$$

$$\vec{L}_2(\omega) = \underline{\underline{I}}(\omega) \cdot \vec{\omega}_2$$

$$= \frac{1}{\sqrt{3}} Ma^2 \omega \begin{pmatrix} 2/3 & -1/4 & -1/4 \\ -1/4 & 2/3 & -1/4 \\ -1/4 & -1/4 & 2/3 \end{pmatrix} \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

$$= \frac{1}{6\sqrt{3}} Ma^2 \omega (1, 1, 1) = \frac{1}{6} Ma^2 \vec{\omega}_2$$

For point C,

$$\vec{L}_1(C) = \underline{\underline{I}}(C) \cdot \vec{\omega}_1 = \frac{1}{6} Ma^2 \underline{\underline{I}} \cdot \vec{\omega}_1 = \frac{1}{6} Ma^2 \vec{\omega}_1$$

$$\vec{L}_2(C) = \underline{\underline{I}}(C) \cdot \vec{\omega}_2 = \frac{1}{6} Ma^2 \underline{\underline{I}} \cdot \vec{\omega}_2 = \frac{1}{6} Ma^2 \vec{\omega}_2$$

The previous example shows something interesting, for a particular choice of origin and/or axis of rotation, the relation  $\vec{L} = \mathbb{I} \cdot \vec{\omega}$  simplifies such that  $\vec{L} \parallel \vec{\omega}$ .

This particular set of axes are called principal axes. The moment of inertia about the principal axes is called the principal moments, and generally, the moment of inertia is

$$\mathbb{I} = \begin{pmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{pmatrix}$$

so that  $\vec{L} = \lambda \vec{\omega}$ .

Principal axes are associated with some symmetry axis.

### Theorem: Existence of Principal Axes

For any rigid body and point O,  
 $\exists$  three perpendicular axes through O s.t.  $\mathbb{I}$  is diagonal.

$$\Rightarrow \mathbb{I} \vec{\omega} = \lambda \vec{\omega} \text{ and } \vec{L} \parallel \vec{\omega}$$

To prove this, we need to recall some Linear Algebra ...

## Diagonalizing a Real-Symmetric Matrix

Let us remind ourself of some aspects of linear algebra, namely eigensystems & solutions.

Consider a real, symmetric  $n \times n$  matrix  $A$ .

We'd like to solve the eigenvalue equation

$$\rightarrow A\vec{v} = \lambda \vec{v}, \quad \lambda = \text{eigenvalue}$$

$\uparrow$   
number

$$(A - \lambda I)\vec{v} = 0 \quad \vec{v} = \text{eigenvector}$$

This is equivalent to  $(A - \lambda I)\vec{v} = 0$

From linear algebra, we know that this has a nontrivial solution ( $\vec{v} \neq 0$ ) iff  $\det(A - \lambda I) = 0$ .

← characteristic eqn.

This is a polynomial of degree  $n$ . In general, it has  $n$  complex solutions.

For each solution  $\lambda_\alpha$ ,  $\det(A - \lambda_\alpha I) = 0$ ,

so  $\exists$  a null vector  $\vec{v}_\alpha$   $\in A - \lambda_\alpha I$ , i.e.,

$$A\vec{v}_\alpha = \lambda_\alpha \vec{v}_\alpha \quad (1)$$

and  $\vec{v}_\alpha$  an eigenvector.

In general,  $\vec{v}_\alpha \in \mathbb{C}^n$ . Let's act (1) on the left by  $\vec{v}_\alpha^+ = (\vec{v}_\alpha^\top)^*$  ( $+$  = conjugate transpose)

$$\vec{v}_\alpha^+ / A \vec{v}_\alpha = \lambda_\alpha \vec{v}_\alpha^+ \vec{v}_\alpha$$

$$\text{Note that } \vec{v}_\alpha^+ \vec{v}_\alpha = |\vec{v}_\alpha|^2 \in \mathbb{R}$$

$$\Rightarrow \lambda_\alpha = \frac{\vec{v}_\alpha^+ / A \vec{v}_\alpha}{|\vec{v}_\alpha|^2}$$

Recall that, in general,  $\lambda_\alpha \in \mathbb{C}$ , so it is a  $1 \times 1$  matrix and is symmetric,  $\lambda_\alpha^\top = \lambda_\alpha$   
Similarly,  $|\vec{v}_\alpha|^2 \in \mathbb{R} \Rightarrow (|\vec{v}_\alpha|^2)^\top = |\vec{v}_\alpha|^2$

So, take transpose,

$$\lambda_\alpha = \lambda_\alpha^\top = \frac{(\vec{v}_\alpha^+ / A \vec{v}_\alpha)^\top}{|\vec{v}_\alpha|^2}$$

$$\text{Recall } (ABC)^\top = C^\top B^\top A^\top$$

$$\Rightarrow (\vec{v}_\alpha^+ / A \vec{v}_\alpha)^\top = \vec{v}_\alpha^\top / A^\top \vec{v}_\alpha^* \\ = \vec{v}_\alpha^{+\top} / A^\top \vec{v}_\alpha^*$$

Now,  $/A$  is real and symmetric  $\Rightarrow /A^\top = /A = /A^*$

$$\text{So, } \lambda_\alpha = \frac{\vec{V}_\alpha^+ A^* \vec{V}_\alpha^*}{|\vec{V}_\alpha|^2}$$

$$= \left( \frac{\vec{V}_\alpha^+ A \vec{V}_\alpha}{|\vec{V}_\alpha|^2} \right)^* = \lambda_\alpha^*$$

$$\therefore \lambda_\alpha = \lambda_\alpha^* \Rightarrow \boxed{\lambda_\alpha \in \mathbb{R}}$$

for real, symmetric matrix  $A$

Notice also

$$A^* \vec{V}_\alpha^* = \lambda_\alpha^* \vec{V}_\alpha^* \Rightarrow A \vec{V}_\alpha^* = \lambda_\alpha \vec{V}_\alpha^*$$

So,  $\vec{V}_\alpha^*$  is also an eigenvector w/ same eigenvalue

$\Rightarrow \vec{V}_\alpha$ .  $\Rightarrow$  Can take  $\vec{V}_\alpha + \vec{V}_\alpha^*$ , this must

also be an eigenvector with eigenvalue  $\lambda_\alpha$ .

$$\text{But, } \vec{V}_\alpha + \vec{V}_\alpha^* = 2\operatorname{Re}(\vec{V}_\alpha) \in \mathbb{R}^n.$$

$\Rightarrow$  Through suitable manipulations, all eigenvectors can be chosen to be real.

We may also normalize the eigenvectors

$$\vec{V}_\alpha \rightarrow \frac{\vec{V}_\alpha}{\sqrt{\vec{V}_\alpha^T \vec{V}_\alpha}}, \text{ so that } \vec{V}_\alpha^T \vec{V}_\alpha = 1.$$

From now on, assume  $\vec{V}_\alpha$  is normalized.

Finally, consider two eigenvalues  $\lambda_\alpha \neq \lambda_\beta$ .

Then,

$$A \vec{V}_\alpha = \lambda_\alpha \vec{V}_\alpha$$

$$\& A \vec{V}_\beta = \lambda_\beta \vec{V}_\beta \Rightarrow \vec{V}_\beta^T A = \lambda_\beta \vec{V}_\beta^T$$

↑ take transpose

At second eqn. on  $\vec{V}_\alpha$

$$\Rightarrow \vec{V}_\beta^T A \vec{V}_\alpha = \lambda_\beta \vec{V}_\beta^T \vec{V}_\alpha$$

||

$$\vec{V}_\beta^T (\lambda_\alpha \vec{V}_\alpha) = \lambda_\alpha \vec{V}_\beta^T \vec{V}_\alpha$$

$$\therefore (\lambda_\alpha - \lambda_\beta) \vec{V}_\beta^T \cdot \vec{V}_\alpha = 0 \Rightarrow \vec{V}_\beta^T \cdot \vec{V}_\alpha = 0$$

We conclude

$$\vec{V}_\alpha^T \cdot \vec{V}_\beta = \delta_{\alpha\beta}$$

(orthonormality)

With all this, we can now show that  $A$  can be diagonalized as  $A = V D V^T$  where  $D$  is diagonal matrix with the eigenvalues on the diagonal and  $V$  is an orthogonal matrix formed by placing  $\vec{V}_\alpha$  at column  $\alpha$  in the same order as  $\lambda_\alpha$  in  $D$ .

Proof. Since  $\vec{v}_\alpha$  are orthonormal, they form a complete basis & we just need to show

$$A \vec{v}_\alpha = (V D V^T) \vec{v}_\alpha$$

In the usual basis of  $A$ ,  $\vec{e}_1 = (1, 0, 0, \dots, 0)$

$$\vec{e}_2 = (0, 1, 0, \dots, 0)$$

:

$$\vec{e}_d = (0, 0, \dots, 1, \dots, 0)$$

We can write the  $\beta$ -element  
of the  $\alpha$ -basis vector  $(\vec{e}_\alpha)_\beta = \delta_{\alpha\beta}$ .

With this basis, we can expand the eigenvector as

$$\vec{v}_\alpha = \sum_\beta v_{\alpha,\beta} \vec{e}_\beta$$

Then,  $V_{\alpha\beta} = v_{\alpha,\beta}$  is an orthogonal matrix  $V^{-1} = V^T$ .

To see this,  $V \vec{e}_\alpha = \vec{v}_\alpha$ , also

$$(V^T \vec{v}_\alpha)_\beta = \sum_r (V^T)_{\beta r} (\vec{v}_\alpha)_r$$

$$= \sum_r (V)_{\gamma\beta} (\vec{v}_\alpha)_r = \sum_r v_{\gamma,r} v_{\alpha,r}$$

$$= \vec{v}_\beta^T \cdot \vec{v}_\alpha = \delta_{\alpha\beta}$$

$$\Rightarrow V^T \vec{v}_\alpha = \vec{e}_\alpha \Rightarrow V^T V \vec{e}_\alpha = \vec{e}_\alpha$$

$$\Rightarrow V^T V = I \quad \forall \alpha$$

Finally,

$$(V D V^T) \vec{v}_\alpha = V D \vec{e}_\alpha = \lambda_\alpha V \vec{e}_\alpha = \lambda_\alpha \vec{v}_\alpha \equiv A \vec{v}_\alpha$$

$$\therefore \boxed{A = V D V^T}$$

## Principle Axes & Principal Moments

For the inertia tensor, a real symmetric matrix, we can diagonalize it, i.e., choose a set of axes, such that  $\mathbb{I} \parallel \vec{\omega}$ .

The diagonal elements are given by the eigenvalues of  $\mathbb{I}$ , i.e., the solutions to

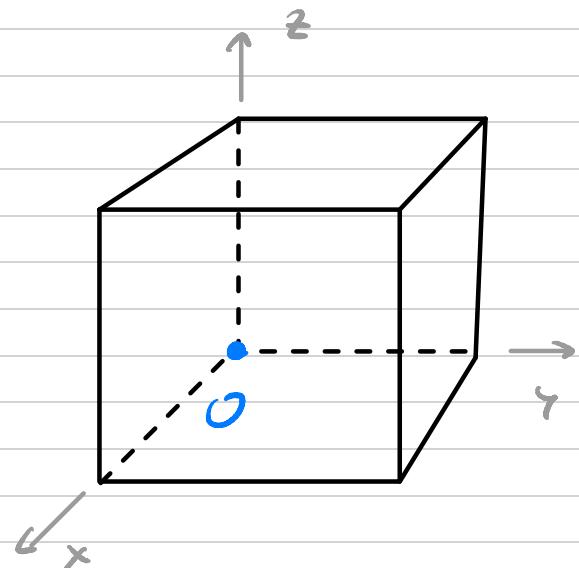
$$\det(\mathbb{I} - \lambda \mathbb{1}) = 0$$

Example - Principle axes of cube about corner?

Recall from previous example

$$\mathbb{I}_0 = M_a^2 \begin{pmatrix} 2/3 & -1/4 & -1/4 \\ -1/4 & 2/3 & -1/4 \\ -1/4 & -1/4 & 2/3 \end{pmatrix}$$

$$= \mu \begin{pmatrix} 8 & -3 & -3 \\ -3 & 8 & -3 \\ -3 & -3 & 8 \end{pmatrix}$$



with  $\mu = \frac{1}{12} M_a^2$

So, we want to solve  $\det(\mathbb{I}_3 - \lambda \mathbb{1}) = 0$

$$\Rightarrow \det \begin{bmatrix} 8\mu - \lambda & -3\mu & -3\mu \\ -3\mu & 8\mu - \lambda & -3\mu \\ -3\mu & -3\mu & 8\mu - \lambda \end{bmatrix} = 0$$

To solve, note the following:

- Replacing a column (row) of a matrix with the sum of that column (row) & a multiple of another column (row) does NOT change  $\det$ .
- Multiplying a column (row) by number, multiplies  $\det$  by same number
- $\det \begin{bmatrix} a_1 & \cdot & \cdot \\ 0 & a_2 & \cdot \\ 0 & 0 & a_3 \end{bmatrix} = \det \begin{bmatrix} a_1 & 0 & 0 \\ \cdot & a_2 & 0 \\ \cdot & \cdot & a_3 \end{bmatrix} = a_1 a_2 a_3$

So, take

$$0 = \det \begin{bmatrix} 8\mu - \lambda & -3\mu & -3\mu \\ -3\mu & 8\mu - \lambda & -3\mu \\ -3\mu & -3\mu & 8\mu - \lambda \end{bmatrix}$$

take col 1  $\rightarrow$  col 1 - col 2

$$\Rightarrow O = \det \begin{bmatrix} 11\mu - \lambda & -3\mu & -3\mu \\ -11\mu + \lambda & 8\mu - \lambda & -3\mu \\ 0 & -3\mu & 8\mu - \lambda \end{bmatrix}$$

row 2  $\rightarrow$  row 2 + row 1

$$= \det \begin{bmatrix} 11\mu - \lambda & -3\mu & -3\mu \\ 0 & 5\mu - \lambda & -6\mu \\ 0 & -3\mu & 8\mu - \lambda \end{bmatrix}$$

col 2  $\rightarrow$  col 2 - col 3

$$= \det \begin{bmatrix} 11\mu - \lambda & 0 & -3\mu \\ 0 & 11\mu - \lambda & -6\mu \\ 0 & -11\mu + \lambda & 8\mu - \lambda \end{bmatrix}$$

row 3  $\rightarrow$  row 3 + row 2

$$= \det \begin{bmatrix} 11\mu - \lambda & 0 & -3\mu \\ 0 & 11\mu - \lambda & -6\mu \\ 0 & 0 & 3\mu - \lambda \end{bmatrix}$$

so, find

$$\det[\dots] = (11\mu - \lambda)^2(2\mu - \lambda) = 0$$

$$\Rightarrow \begin{cases} \lambda_1 = 2\mu \\ \lambda_2 = \lambda_3 = 11\mu \end{cases}$$

So, the principal moments are

$$\mathbb{I}'_0 = \mathbb{D} = \mu \begin{pmatrix} 2 & 0 & 0 \\ 0 & 11 & 0 \\ 0 & 0 & 11 \end{pmatrix}$$

What about the axes?

Want  $\hat{\mathbf{e}}_1, \hat{\mathbf{e}}_2, \hat{\mathbf{e}}_3$

First, find  $\vec{\omega}_1 = \omega \hat{\mathbf{e}}_1$  associated w/  $\lambda_1$

Solve  $(\mathbb{I}_0 - \lambda_1 \mathbb{I}) \vec{\omega}_1 = 0$

$$\Rightarrow \mu \begin{pmatrix} 6 & -3 & -3 \\ -3 & 6 & -3 \\ -3 & -3 & 6 \end{pmatrix} \begin{pmatrix} \omega_{1,x} \\ \omega_{1,y} \\ \omega_{1,z} \end{pmatrix} = 0$$

$$\Rightarrow 2\omega_{1,x} - \omega_{1,y} - \omega_{1,z} = 0 \quad (a)$$

$$-\omega_{1,x} + 2\omega_{1,y} - \omega_{1,z} = 0 \quad (b)$$

$$-\omega_{1,x} - \omega_{1,y} + 2\omega_{1,z} = 0 \quad (c)$$

$$\text{Take (a)-(b)} \Rightarrow \omega_{1,x} = \omega_{1,y}$$

$$\text{From (c)} \Rightarrow \omega_{1,x} = \omega_{1,y} = \omega_{1,z}$$

So,  $\vec{\omega} \parallel (1,1,1) \Rightarrow$  Normalize to find

$$\hat{\mathbf{e}}_1 = \frac{1}{\sqrt{3}} (1,1,1)$$

This means that if  $\vec{\omega}_1 = \omega \hat{e}_1$ ,

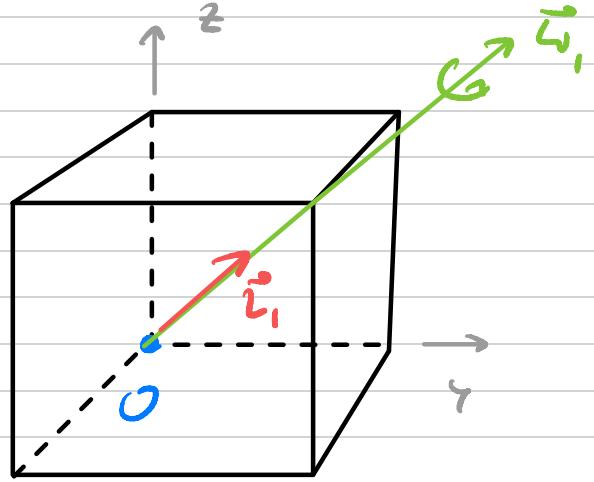
$$\text{then } \vec{\lambda}_1 = \vec{\mathbb{I}} \vec{\omega}_1 = \omega \vec{\mathbb{I}} \hat{e}_1 = \omega \lambda_1 \hat{e}_1 = \lambda_1 \vec{\omega}_1,$$

$$\Rightarrow \vec{\lambda}_1 = \lambda_1 \vec{\omega}_1$$

For  $\vec{\omega}_2$  &  $\vec{\omega}_3$ ,  $\lambda_2 = \lambda_3$

Solve

$$(\vec{\mathbb{I}}_0 - \lambda_2 \vec{\mathbb{I}}) \vec{\omega} = 0$$



$$\Rightarrow \mu \begin{bmatrix} -3 & -3 & -3 \\ -3 & -3 & -3 \\ -3 & -3 & -3 \end{bmatrix} \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix} = 0$$

$$\Rightarrow \omega_x + \omega_y + \omega_z = 0$$

Notice that this is equal to  $\vec{\omega} \cdot \hat{e}_1 = 0$

$\Rightarrow \vec{\omega}$  needs to be orthogonal to  $\hat{e}_1$ ,

$\Rightarrow \hat{e}_2$  &  $\hat{e}_3$  need to be orthogonal to  $\hat{e}_1$ ,

Two such solutions are

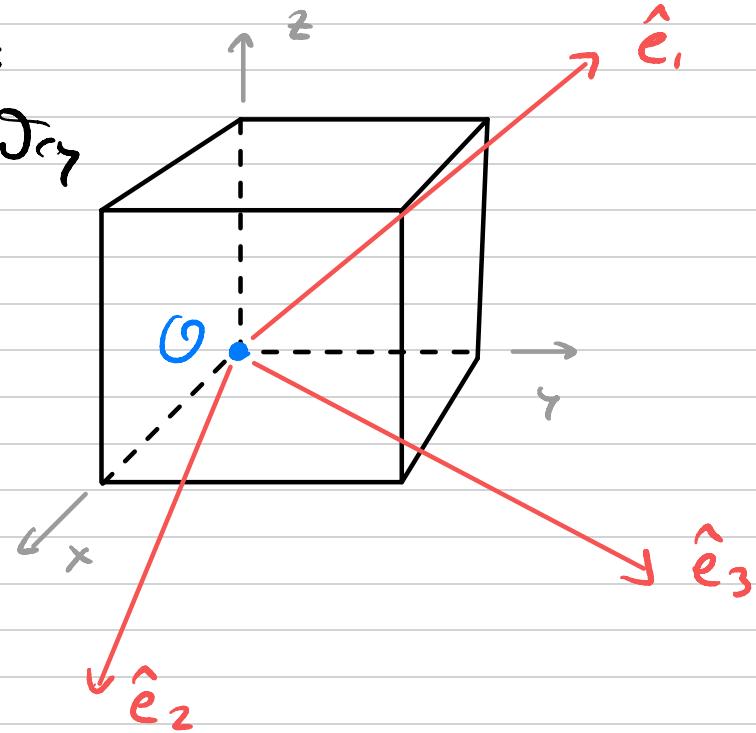
$$\hat{e}_2 = \frac{1}{\sqrt{2}} (1, 0, -1), \quad \hat{e}_3 = \frac{1}{\sqrt{6}} (-1, 2, -1)$$

(using)

So, principal axes (eigenvectors) are

$$\hat{e}_1 = \frac{1}{\sqrt{3}}(1,1,1), \hat{e}_2 = \frac{1}{\sqrt{2}}(1,0,-1), \hat{e}_3 = \frac{1}{\sqrt{6}}(-1,2,-1)$$

The principal axes correspond to symmetry of the cube and the body diagonal with center at O.



Can decompose  $\mathbb{I}_0 = V D_0 V^T$

with  $D_0 = \frac{1}{12} M a^2 \begin{pmatrix} 2 & 0 & 0 \\ 0 & 11 & 0 \\ 0 & 0 & 11 \end{pmatrix}$

$$V = \frac{1}{\sqrt{6}} \begin{pmatrix} \sqrt{2} & \sqrt{3} & -1 \\ \sqrt{2} & 0 & 2 \\ \sqrt{2} & -\sqrt{3} & -1 \end{pmatrix}$$

$$\hat{e}_1 \quad \hat{e}_2 \quad \hat{e}_3$$

■

## Precession of Symmetric Top due to Weak Torque

Having all the tools in our arsenal, let's apply them for a "simple" physics problem.

Consider a symmetric top with mass  $M$  and inertia tensor  $\mathbb{I} = \text{diag}(\lambda_1, \lambda_2, \lambda_3)$  in the basis of its principal axes,  $(\hat{\mathbf{e}}_1, \hat{\mathbf{e}}_2, \hat{\mathbf{e}}_3)$ .

It rotates freely with its tip pivoted at a fixed point  $O$  in a lab frame (inertial)

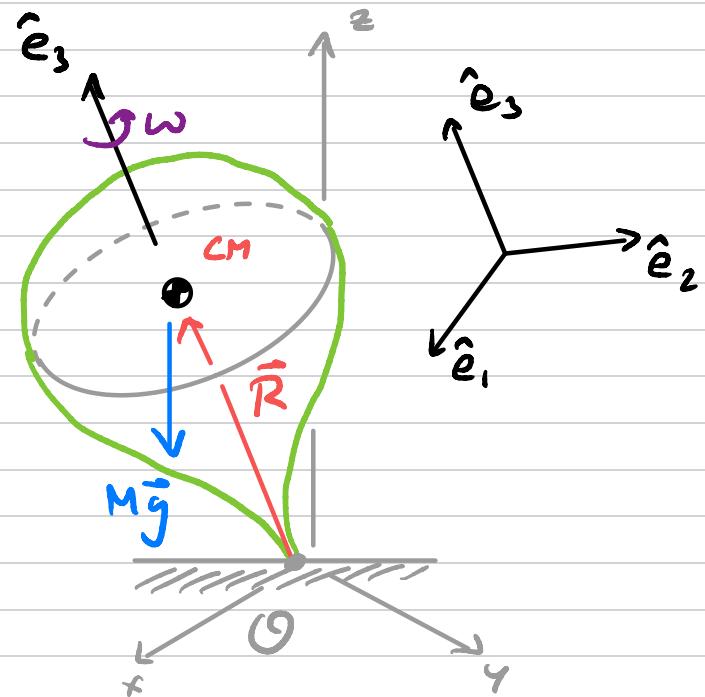
Its CM is at  $\bar{R}$ .

We assume its angular velocity is initially along its symmetry axis,

$$\vec{\omega} = \omega \hat{\mathbf{e}}_3$$

The angular momentum is initially

$$\vec{L} = \mathbb{I} \vec{\omega} = \lambda_3 \omega \hat{\mathbf{e}}_3$$



(initial config)

If we release the top, gravity will exert a torque, and cause a change of angular momentum.

The torque due to gravity is  $\vec{\tau} = \vec{R} \times M\vec{g}$ , at the CM w/r fixed point O.

- If  $\vec{\tau} = \vec{0}$  (c.g.,  $\vec{R} \times \vec{g} = \vec{0}$ )  
 $\Rightarrow \vec{L} = \text{const.}$

To see, take

$$\begin{aligned} \left( \frac{d\vec{L}}{dt} \right)_{\text{lab}} &= \lambda \frac{d}{dt} \left( \omega \hat{e}_3 \right)_{\text{lab}} \\ &= \lambda \left( \dot{\omega} \hat{e}_3 + \omega \left( \frac{d\hat{e}_3}{dt} \right)_{\text{lab}} \right) = 0 \end{aligned}$$

Since  $\vec{\omega} \parallel \hat{e}_3 \Rightarrow \left( \frac{d\hat{e}_3}{dt} \right)_{\text{lab}} = \vec{\omega} \times \hat{e}_3 = \vec{0}$

That is,  $\hat{e}_3$  is fixed in the lab frame too!

$$\Rightarrow \dot{\omega} = 0$$

• If  $\vec{\Gamma} \neq \vec{0}$ , but  $\omega_1, \omega_2$  are small, so  $\vec{\omega} \approx \omega_3 \hat{e}_3$

$\Rightarrow \vec{\Gamma} \perp \vec{\omega}$  and  $\dot{\omega}$  remains small

so, EOM gives  $\left( \frac{d\vec{L}}{dt} \right)_{\text{lab}} = \vec{\Gamma}$

$$\Rightarrow \lambda \left( i\dot{\omega} \hat{e}_3 + \omega \left( \frac{d\hat{e}_3}{dt} \right)_{\text{lab}} \right) = \vec{R} \times M\vec{g}$$

Since  $i\dot{\omega} \approx 0$ ,  $\left( \frac{d\hat{e}_3}{dt} \right)_{\text{lab}} = \frac{1}{\lambda\omega} \vec{R} \times M\vec{g}$

Now,  $\vec{R} = R\hat{e}_3$ ,  $\vec{g} = -g\hat{z}$   $\Rightarrow \vec{R} \times \vec{g} = Rg\hat{z} \times \hat{e}_3$

$$\Rightarrow \left( \frac{d\hat{e}_3}{dt} \right)_{\text{lab}} = \left( \frac{MRg}{\lambda\omega} \right) \hat{z} \times \hat{e}_3$$

Define  $\vec{\Omega} = \frac{MRg}{\lambda\omega} \hat{z}$

$\Rightarrow$  the symmetry axis of the

to rotates w/  $\vec{\Omega} = \frac{MRg}{\lambda\omega}$

about  $\hat{z}$  axis

$\Rightarrow$  precession

