Model for Estimating Limit-State Displacements of Two-Column Steel Bridge Piers

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Yield Limit-State

$$\Delta_y = \gamma_{sc} \gamma_{cb} \Delta_y' \tag{1}$$

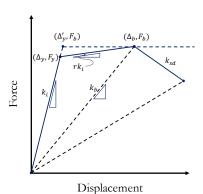
$$\gamma_{cb} = 1.05 \left(\frac{1}{K_{rcb}}\right)^{0.92} \tag{2}$$

$$\gamma_{sc} = 1.88 - 0.01 \left(\frac{D}{t}\right) \tag{3}$$

$$\Delta_y' = \frac{\phi_y L_c^2}{3} \tag{4}$$

$$\phi_y = \frac{2\epsilon_y}{D} \tag{5}$$

$$F_y = n_c \frac{f_y S}{L_c}$$



Figur 1: Idealized force versus displacement response.

Buckling Limit-State

$$\Delta_b = \gamma_{sc} \gamma_{cb} \Delta_b' \tag{7}$$

$$\gamma_{cb} = 0.58 \left(\frac{1}{K_{rcb}}\right)^{0.58} \left(\frac{D}{t}\right)^{0.14} \left(1 + \frac{P}{P_u}\right)^{1.44} (8)$$

$$\gamma_{sc} = 1.73 \tag{9}$$

$$\Delta_b' = \Delta_e + \Delta_p \tag{10}$$

$$\Delta_e = \frac{\phi_y' L_c^2}{3} \tag{11}$$

$$\phi_y' = \phi_y \left(\frac{M_p}{M_y}\right) \tag{12}$$

$$\Delta_p = L_p \left(\phi_b - \phi_y' \right) \left(L_c - \frac{L_p}{2} \right) \tag{13}$$

$$\phi_b = \frac{b_c \epsilon_b}{D} \tag{14}$$

$$b_c = 2.81 - 0.019 \left(\frac{D}{t}\right) \tag{15}$$

$$\epsilon_b = 15 \left(\frac{D}{t}\right)^{-2} \tag{16}$$

$$L_p = k_p L_c (17)$$

$$k_p \approx 0.035$$
 (18)

$$F_b = F_y \left[1 + r \left(\frac{\Delta_b'}{\Delta_y'} - 1 \right) \right] \le \frac{M_p}{L_c}$$
 (19)

$$r = 0.0136 \left(\frac{D}{t}\right) + 0.004 f_y - 0.35 \qquad (20)$$

Strength Degradation Rate

$$k_{sd} = 540 \left(\frac{D}{t}\right)^{-1.3} - 0.18 \left(\frac{P}{P_u}\right) - 11.3$$
 (21)

Displacement Corresponding to n% Strength Reduction

$$\Delta_{sd-n} = \Delta_b - 0.01 \frac{n}{k_{sd}} L_e \tag{22}$$

Nomenclature

D = Column diameter

 F_{y} = System force at yield limit-state

 F_b = System force at local buckling limit-state

 K_{rcb} = Cap beam relative stiffness

 L_c = Column cantilever length

 L_p = Plastic hinge length

 M_p = Expected column maximum bending moment

 M_{ν} = Column yield moment

P = Column axial load

 P_u = Column axial load capacity

S = Column section modulus

 b_c = Dimensionless column curvature at local buckling

 f_y = Yield strength of steel

 k_p = Ratio of plastic hinge length to column cantilever length

 k_{sd} = Column strength degradation rate, % reduction per unit drift

n =Strength reduction in terms of percentage of F_b

 n_c = Number of columns

r = Column bi-linear factor

t = Column wall thickness

 Δ_b = System displacement at column local buckling

 Δ_b' = Single column displacement at column local buckling

 Δ_e = Elastic component of column displacement

 Δ_p = Plastic component of column displacement

 Δ_{sd-n} = Displacement at n% strength reduction

 Δ_y = System yield displacement

 Δ'_{y} = Single column yield displacement

 ϵ_v = Column yield strain

 ϵ_b = Column strain at local buckling

 γ_{sc} = Socket connection flexibility coefficient

 γ_{cb} = Cab beam flexibility coefficient

 ϕ_b = Column maximum curvature at local buckling

 $\phi_u = \text{Column yield curvature}$

 ϕ'_{y} = Equivalent column yield curvature