Model for Estimating Limit-State Displacements of Two-Column Steel Bridge Piers

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Yield Limit-State

$$\Delta_y = \gamma_{sc} \gamma_{cb} \Delta_y' \tag{1}$$

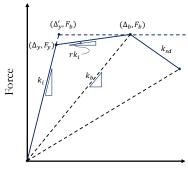
$$\gamma_{cb} = 1.05 \left(\frac{1}{K_{rcb}}\right)^{0.92} \tag{2}$$

$$\gamma_{sc} = 1.88 - 0.01 \left(\frac{D}{t}\right) \tag{3}$$

$$\Delta_y' = \frac{\phi_y L_c^2}{3} \tag{4}$$

$$\phi_y = \frac{2\epsilon_y}{D} \tag{5}$$

$$F_y = n_c \frac{f_y S}{L_c}$$



Displacement

(20)

(22)

Figur 1: Idealized force versus displacement response.

Buckling Limit-State

$$\Delta_b = \gamma_{sc}\gamma_{cb}\Delta_b' \qquad (7) \qquad r = 0.0136\left(\frac{D}{t}\right) + 0.004f_y - 0.35$$

$$\gamma_{cb} = 0.65 \left(\frac{1}{K_{rcb}}\right)^{0.58} \left(\frac{D}{t}\right)^{0.14}$$
 (8) Strength Degradation Rate

$$(K_{rcb})$$
 (t) Strength Degradation Rat

$$\gamma_{sc} = 1.73$$

$$\Delta'_{b} = \Delta_{e} + \Delta_{p}$$
(9)
$$k_{sd} = 540 \left(\frac{D}{t}\right)^{-1.3} - 0.18 \left(\frac{P}{P_{u}}\right) - 11.3$$
(21)

$$\Delta_e = \frac{\phi'_y L_c^2}{3}$$

$$\phi'_y = \phi_y \left(\frac{M_p}{M_y}\right)$$
(11) Displacement Corresponding to n%
(12) Strength Reduction

$$\Delta_p = L_p \left(\phi_b - \phi_y' \right) \left(L_c - \frac{L_p}{2} \right)$$

$$(13)$$

$$\Delta_{sd-n} = \Delta_b - \frac{F_b L_e \left(1 - 0.01n \right)}{100 k_{sd}}$$

$$\phi_b = \frac{b_c \epsilon_b}{D} \tag{14}$$

$$b_c = 2.81 - 0.019 \left(\frac{D}{t}\right)$$
 (15)

$$\epsilon_b = 15 \left(\frac{D}{t}\right)^{-2} \tag{16}$$

$$L_p = k_p L_c (17)$$

$$k_p \approx 0.035 \tag{18}$$

$$F_b = F_y \left[1 + r \left(\frac{\Delta_b'}{\Delta_y'} - 1 \right) \right] \le \frac{M_p}{L_c}$$
 (19)

Nomenclature

D = Column diameter

 F_{y} = System force at yield limit-state

 F_b = System force at local buckling limit-state

 K_{rcb} = Cap beam relative stiffness

 L_c = Column cantilever length

 L_p = Plastic hinge length

 M_p = Expected column maximum bending moment

 M_{ν} = Column yield moment

P = Column axial load

 P_u = Column axial load capacity

S = Column section modulus

 b_c = Dimensionless column curvature at local buckling

 f_y = Yield strength of steel

 k_p = Ratio of plastic hinge length to column cantilever length

 k_{sd} = Column strength degradation rate, % reduction per unit drift

n =Strength reduction in terms of percentage of F_b

 n_c = Number of columns

r = Column bi-linear factor

t = Column wall thickness

 Δ_b = System displacement at column local buckling

 Δ_b' = Single column displacement at column local buckling

 Δ_e = Elastic component of column displacement

 Δ_p = Plastic component of column displacement

 Δ_{sd-n} = Displacement at n% strength reduction

 Δ_y = System yield displacement

 Δ'_{y} = Single column yield displacement

 ϵ_v = Column yield strain

 ϵ_b = Column strain at local buckling

 γ_{sc} = Socket connection flexibility coefficient

 γ_{cb} = Cab beam flexibility coefficient

 ϕ_b = Column maximum curvature at local buckling

 $\phi_u = \text{Column yield curvature}$

 ϕ'_{y} = Equivalent column yield curvature