

Simulation of Natural Convection under the Influence of Magnetic Field by Explicit Local Radial Basis Function Collocation Method

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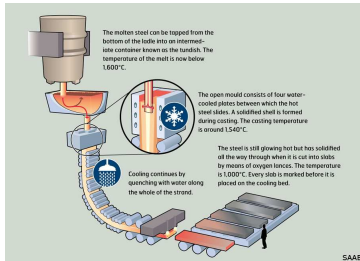
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Outline

- ▶ Introduction
- ▶ Numerical method
- ▶ Problem description
- ▶ Results
- ▶ Conclusions

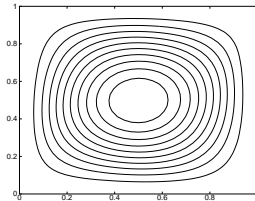
Introduction

Focus and motivation

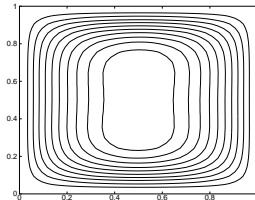


Focus and motivation

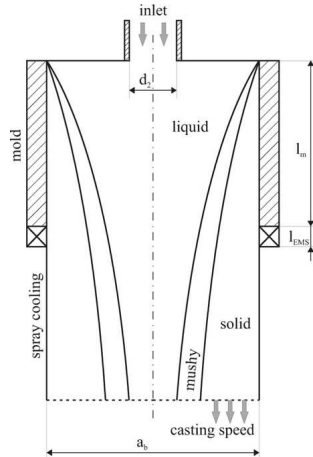
Natural convection.



Natural convection with applied magnetic field.



Continuous casting.



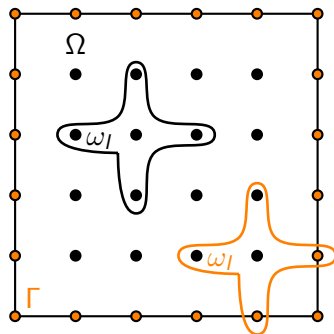
Numerical method

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Local Radial Basis Function Collocation Method

Used for solving PDF's.

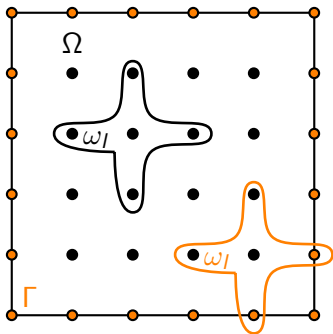
- ▶ **Local** influence domain
- ▶ **Radial Basis Function** are used as basis
- ▶ **Collocation** (interpolation) of scattered data



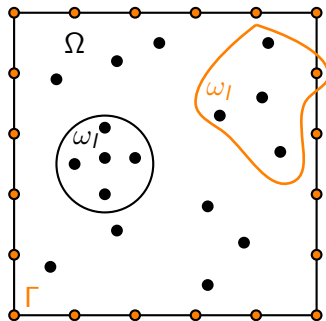
Local Radial Basis Function Collocation Method

Local influence domain

Uniform node arrangement



Non-uniform node arrangement



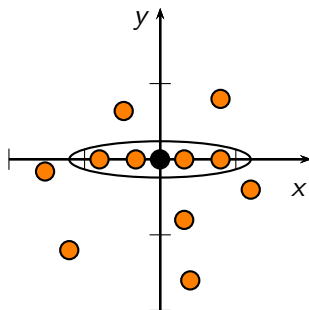
Local Radial Basis Function Collocation Method

Local influence domain

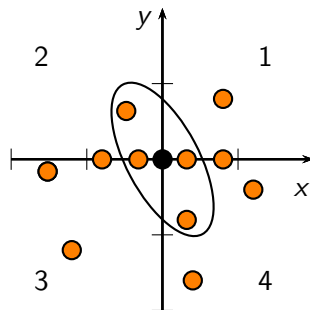
Influence domain for non-uniform node arrangement:

- ▶ spatial position
- ▶ range

Random neighbours



Optimal neighbours



Local Radial Basis Function Collocation Method

Local collocation

General approximation function:

$$\Phi(\vec{p}) \approx \sum_{i=1}^N \alpha_i \psi_i(\vec{p})$$

Collocation condition:

$$\Phi(\vec{p}_i) = \phi_i$$

System of N equations:

$$\underline{\Psi} \vec{\alpha} = \vec{\phi}$$

PDE's

$$\frac{\partial^i}{\partial p_j^i} \Phi(\vec{p}) = \sum_{n=1}^N \alpha_n \frac{\partial^i}{\partial p_j^i} \psi_n(\vec{p})$$

Local Radial Basis Function Collocation Method

Radial basis functions

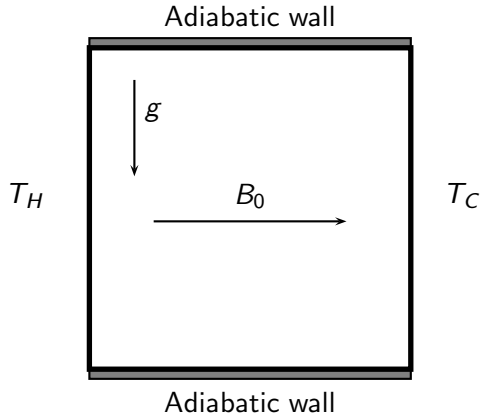
Multiquadric RBFs with normalized subdomain and shape parameter c :

$$\psi_n(\vec{p}) = \sqrt{r_n^2(\vec{p}) + c^2}$$
$$r_n = \sqrt{\left(\frac{p_x - p_{xn}}{p_{x_{max}}}\right)^2 + \left(\frac{p_y - p_{yn}}{p_{y_{max}}}\right)^2 + \left(\frac{p_z - p_{zn}}{p_{z_{max}}}\right)^2}$$

Problem description

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Problem description



Assumptions

- ▶ Laminar, steady fluid flow
- ▶ Incompressible fluid flow: $\nabla \vec{v} = 0$.
- ▶ Magnetic Raynold's number: $Re_m = VL\mu_0\sigma \ll 1$
 - ▶ induced magnetic field is negligible compared to applied magnetic field.
- ▶ Boussinesq approximation: $\rho = \rho_b(1 - \beta_T(T - T_C))$.

Governing equations

Momentum eq.:

$$\rho \left(\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \nabla) \vec{v} \right) = -\nabla p + \mu \nabla^2 \vec{v} + \vec{F}_m - \vec{g} \rho \beta_T (T - T_C)$$

Continuity eq.:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}) = 0 \quad \Rightarrow \quad \nabla \cdot \vec{v} = 0$$

Energy eq.:

$$\frac{\partial T}{\partial t} + (\vec{v} \cdot \nabla) T = \alpha_T \nabla^2 T$$

Lorentz force term

Equations for Electromagnetic field

Lorentz force:

$$\vec{F}_m = \vec{j} \times \vec{B}$$

Ohm's law:

$$\vec{j} = \sigma(-\nabla\phi + \vec{v} \times \vec{B}) = \vec{j}_i + \vec{j}_d$$

$$\nabla \cdot \vec{j} = 0$$

$$\nabla^2 \phi = \nabla(\vec{v} \times \vec{B})$$

Boundary conditions

Velocities on walls:

$$u = 0, \quad v = 0.$$

Temperatures:

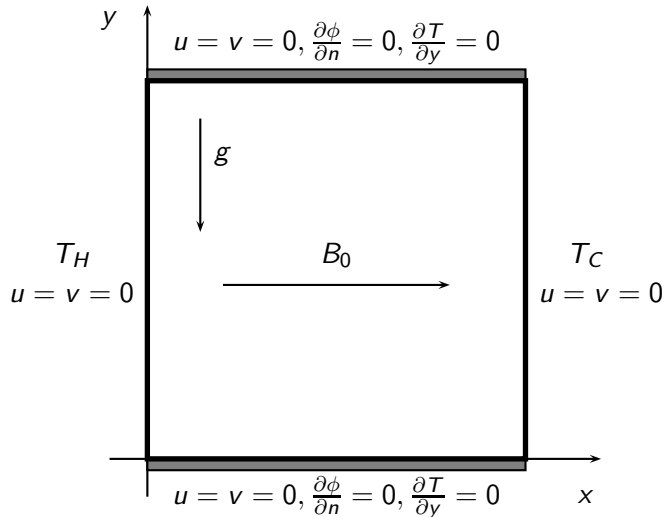
- ▶ at top and bottom wall (adiabatic): $\frac{\partial T}{\partial y} = 0$
- ▶ on the left and right walls have predetermined values: T_H, T_C

Electric potential (insulating boundary):

$$\frac{\partial \phi}{\partial n} = (\vec{v} \times \vec{B})_{boundary} \cdot \vec{n} \quad \Rightarrow \quad \frac{\partial \phi}{\partial n} = 0$$

Problem description

Domain scheme with boundary conditions



Governing equations

Dimensionless governing equations

Momentum eq.:

$$\left(\frac{\partial \vec{V}}{\partial \tau} + (\vec{V} \cdot \nabla) \vec{V} \right) = -\frac{1}{\rho} \nabla P + Pr \nabla^2 \vec{V} + Ha^2 Pr \vec{V} \hat{j} - Gr \Theta$$

Continuity eq.:

$$\nabla \cdot \vec{V} = 0$$

Energy eq.:

$$\frac{\partial \Theta}{\partial \tau} + (\vec{V} \cdot \nabla) \Theta = \nabla^2 \Theta$$

Governing equations

Dimensionless numbers and nondimensionalization

Dimensionless numbers:

$$Ra = \frac{g\beta_T(T_H - T_C)L^3}{\nu\alpha_T}$$

$$Pr = \frac{\nu}{\alpha_T}$$

$$Ha = BL\sqrt{\frac{\sigma}{\mu}}$$

$$Gr = \frac{g\beta_T(T_H - T_C)L^3}{\alpha_T^2}$$

Non-dimensional variables:

$$X = \frac{x}{L}, \quad Y = \frac{y}{L}$$

$$U = \frac{uL}{\alpha_T}, \quad V = \frac{vL}{\alpha_T}$$

$$P = \frac{\rho L^2}{\alpha_T^2}, \quad \Theta = \frac{T - T_C}{T_H - T_C}$$

$$\tau = \frac{t\alpha_T}{L^2}$$

Results

- ▶ Introduction
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Test cases

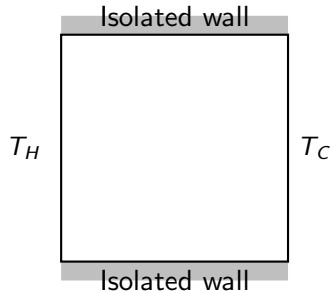
Three different test cases were devised in order to test the numerical method:

- ▶ De Vahl Davis benchmark test (TC1)
- ▶ Natural convection under the influence of magnetic field (TC2)
- ▶ Natural convection under the influence of magnetic field for low Pr numbers (TC3)

Natural convection

De Vahl Davis benchmark test (TC1)

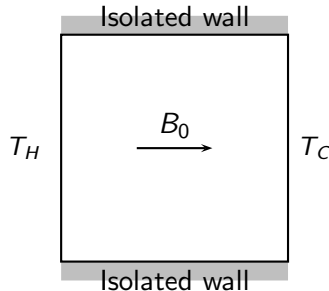
- ▶ closed, differentially heated square cavity
- ▶ $Pr = 0.71$
- ▶ $Ra = 10^4 - 10^6$
- ▶ $Ha = 0$



Natural convection

Natural convection under the influence of magnetic field (TC2)

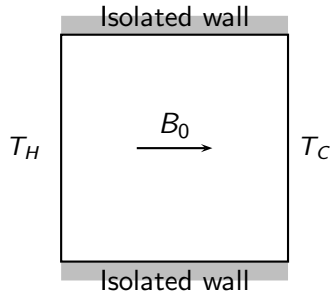
- ▶ closed, differentially heated square cavity
- ▶ $Pr = 0.71$
- ▶ $Gr = 10^4 - 10^6$
- ▶ $Ha = 0 - 100$



Natural convection

Natural convection under the influence of magnetic field for low Pr numbers (TC3)

- ▶ closed, differentially heated square cavity
- ▶ $Pr = 0.14$
- ▶ $Gr = 10^4 - 10^6$
- ▶ $Ha = 0 - 100$



Natural convection

Natural convection under the influence of magnetic field for low Pr numbers (TC3)

Material properties of molten steel:

- ▶ $\rho = 7200 \text{ kg/m}^3$
- ▶ $c_p = 700 \text{ J/(kg K)}$
- ▶ $\alpha_T = 30 \text{ W/(mK)}$
- ▶ $\beta_T = 1.0 \cdot 10^{-4} / \text{K}$
- ▶ $\mu = 0.006 \text{ kg/(ms)}$

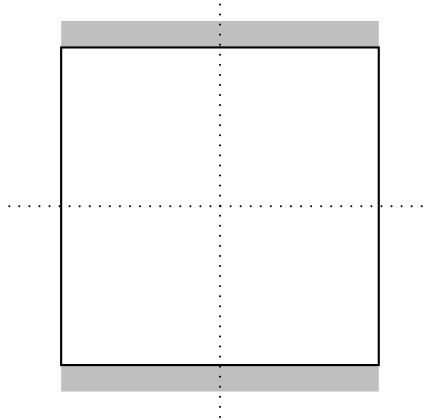
$$Pr = 0.14$$

Results

- Nusselt number:

$$Nu = \int_0^L \left. \frac{\partial T}{\partial x} \right|_{x=0} dy$$

- u along $y = 0.5$
- v along $x = 0.5$

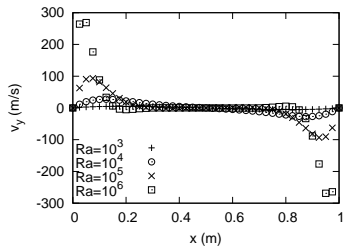
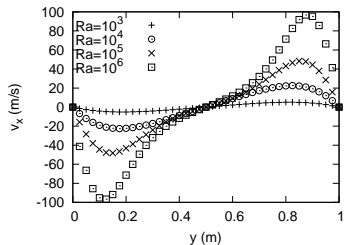


Results

De Vahl Davis benchmark test (TC1)

Ra	$Nu_{(a)}$	$Nu_{(b)}$	$Nu_{(c)}$
10^3	1.108	1.116	1.101
10^4	2.223	2.234	2.075
10^5	4.497	4.510	4.624
10^6	8.685	8.798	8.97*

(a) present; (b) De Vahl Davis, 1983; (c) Kosec et al., 2007

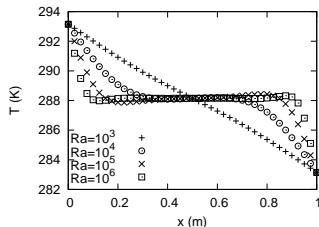


Results

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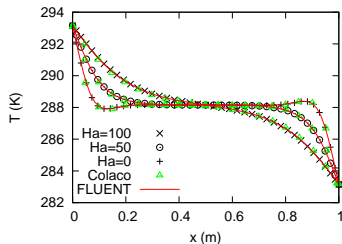
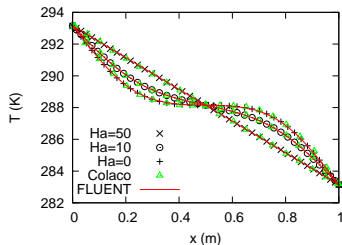


Results

Natural convection under the influence of magnetic field (TC2)

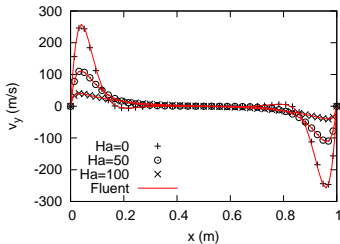
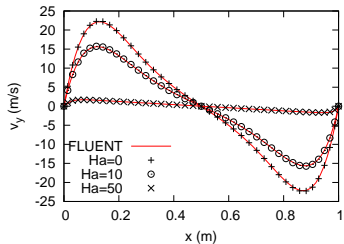
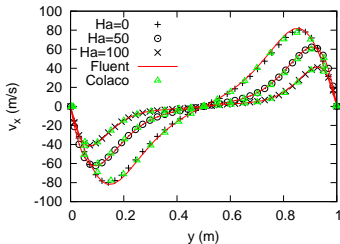
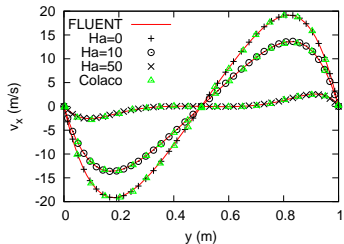
Ha	$Nu_{(a)}$	$Nu_{(b)}$	$Nu_{(c)}$
$Gr = 10^4$			
0	2.03	2.02	2.06
10	1.71	1.70	1.84
50	1.01	0.97	1.06
$Gr = 10^6$			
0	8.15	9.21	7.98
10	7.99	9.04	7.88
100	3.33	3.54	4.27

(a) present; (b) Colaço et al, 2009; (c) FVM



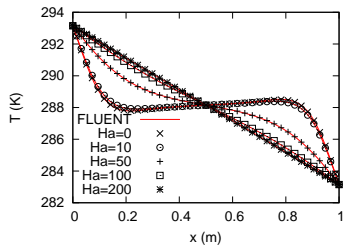
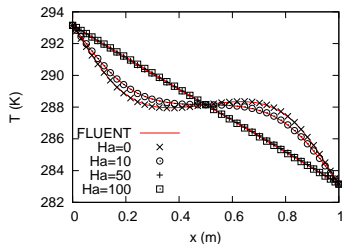
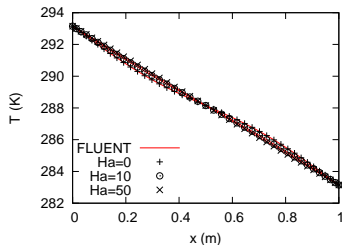
Results

Natural convection under the influence of magnetic field (TC2)



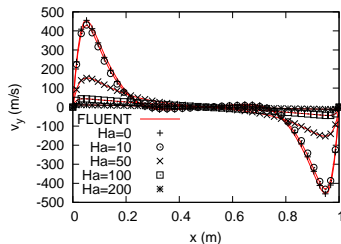
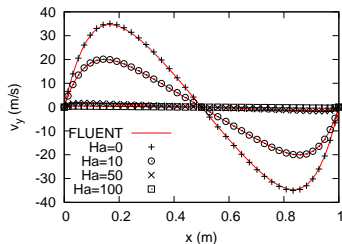
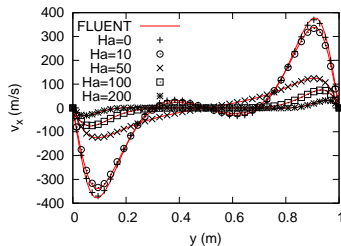
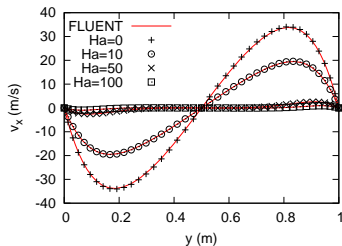
Natural convection under the influence of magnetic field for low Pr numbers (TC3)

Temperatures along the line through the center of the cavity



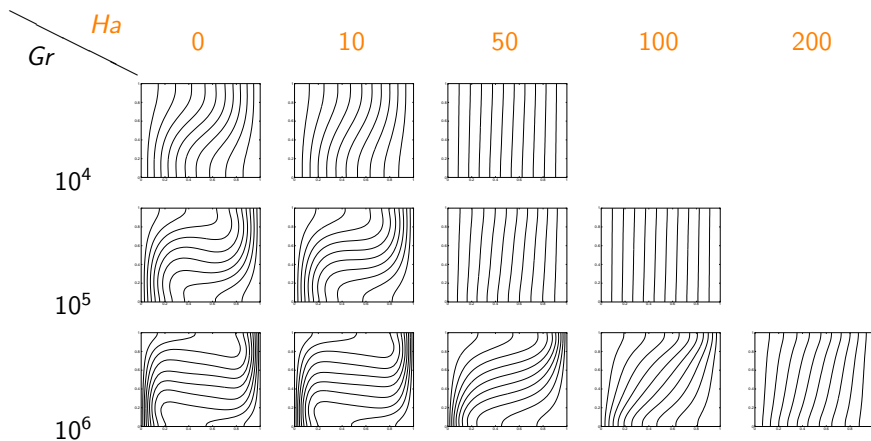
Natural convection under the influence of magnetic field for low Pr numbers (TC3)

Velocities along line through the center of the cavity



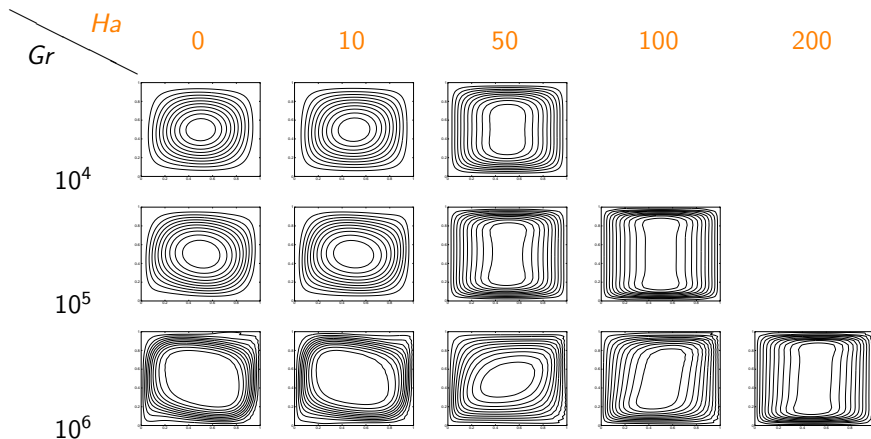
Natural convection under the influence of magnetic field for low Pr numbers (TC3)

Isotherms



Natural convection under the influence of magnetic field for low Pr numbers (TC3)

Stream Functions



Conclusions

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Summary and Conclusions

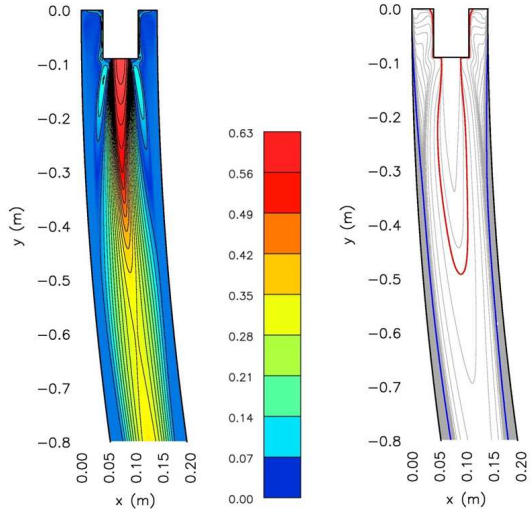
Summary

- ▶ Method is tested first for a natural convection benchmark test and then for natural convection under the influence of external magnetic field.
- ▶ A comparison between in-house meshless method, FLUENT commercial code and results from published papers (De Vahl Davis, 1983; Colaço et al., 2009) is made.

Conclusions

Future plans:

- ▶ complex geometries
- ▶ simplified industrial application
- ▶ continuous casting real curved geometry



Affiliation

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Nusselt numbers

