# **EEE 133 Key concepts and Equations**

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September 29, 2020

## **Differential Equations**

A linear ordinary differential equation of constant coefficients follows the form

$$a_n \frac{\mathrm{d}^n x}{\mathrm{d}t^n} + a_{n-1} \frac{\mathrm{d}^{n-1} x}{\mathrm{d}t^{n-1}} + \ldots + a_1 \frac{\mathrm{d}x}{\mathrm{d}t} + a_0 x = f(t)$$
 (1)

A homogenous differential equation is an equation where the independent variable appears to have the same power. Equation (1) is homogenous when f(t)=0.

The solution to the linear ODE in (1) has the form

$$x(t) = x_h(t) + x_n(t) \tag{2}$$

Where  $x_h(t)$  is a solution to the homogenous equation while  $x_p(t)$  is a solution to the nonhomogenous equation.

A homogenous equation has solutions of the form

$$x_h(t) = \exp(mt) \tag{3}$$

for m is a root of the equation

$$m^{n} + \frac{a_{n-1}}{a_n}m^{n-1} + \ldots + \frac{a_1}{a_n}m + \frac{a_0}{a_n} = 0$$
(4)

If a root  $m_i$  is repeated k times, the corresponding solutions are  $\exp(m_i t), \; t \exp(m_i t), \; \dots, \; t^{k-1} \exp(m_i t)$ 

### Some common forms (with constant coefficients) and solutions

Equation	Characteristic Equation	Determinant	Solution
$a_1 \frac{\mathrm{d}x}{\mathrm{d}t} + a_0 x = 0$	$a_1m + a_0 = 0$		$x = C \exp\left(-\frac{a_0}{a_1}t\right)$
$a_2 \frac{\mathrm{d}^2 x}{\mathrm{d}t^2} + a_1 \frac{\mathrm{d}x}{\mathrm{d}t} + a_0 x = 0$	$a_2m^2 + a_1m + a_0 = 0$	$a_1^2 - 4a_2a_0 > 0$	$x(t) = C_1 \exp(m_1 t) + C_2 \exp(m_2 t)$
		$a_1^2 - 4a_2a_0 = 0$	$x(t) = (C_1 x + C_2) \exp(m_1 t)$
		$a_1^2 - 4a_2a_0 < 0$	$x(t) = \exp(\alpha t) \left[ C_1 \cos(\beta t) + C_2 \sin(\beta t) \right]$

In the last line, the characteristic equation has solutions  $m_1=\alpha+j\beta,\ m_2=\alpha-j\beta$  where  $j^2=-1$ 

# **Laplace Transforms and Theorems**

A Laplace transform of a function f(t) defined for all  $t \geq 0$  is the transformation

$$\mathcal{L}[f(t)] = F(s) = \int_{0}^{\infty} f(t) \exp(-st) dt$$

An inverse Laplace transform of a function F(s) is defined as:

$$f(t) = \mathcal{L}^{-1}[F(s)] = \frac{1}{2\pi j} \lim_{T \to \infty} \int_{\gamma - jT}^{\gamma + jT} \exp(st) F(s) \, \mathrm{d}s$$

### **Common Functional Tranforms**

$f(t) = \mathcal{L}^{-1}[F(s)]$	$F(s) = \mathcal{L}[F(s)]$	$f(t) = \mathcal{L}^{-1}[F(s)]$	$F(s) = \mathcal{L}[F(s)]$
$\delta(t)$	1	$\frac{1}{\beta - \alpha} \left( \exp(-\alpha t) - \exp(-\beta t) \right) u(t)$	$\frac{1}{(s+\alpha)(s+\beta)}$
u(t)	$\frac{1}{s}$	$\sin(\omega t)u(t)$	$rac{\omega}{s^2 + \omega^2}$
tu(t)	$\frac{1}{s^2}$	$\cos(\omega t)u(t)$	$\frac{s}{s^2 + \omega^2}$
$\frac{t^{n-1}}{(n-1)!}u(t)$	$\frac{1}{s^n}$	$\sin(\omega t + \theta)u(t)$	$\frac{s\sin(\theta) + \omega\cos(\theta)}{s^2 + \omega^2}$
$\exp(-\alpha t)u(t)$	$\frac{1}{s+\alpha}$	$\cos(\omega t + \theta)u(t)$	$\frac{s\cos(\theta) - \omega\sin(\theta)}{s^2 + \omega^2}$
$t \exp(-\alpha t) u(t)$	$\frac{1}{(s+\alpha)^2}$	$\exp(-\alpha t)\sin(\omega t)u(t)$	$\frac{\omega}{(s+\alpha)^2 + \omega^2}$
$\frac{t^{n-1}}{(n-1)!}\exp(-\alpha t)u(t)$	$\frac{1}{(s+\alpha)^n}$	$\exp(-\alpha t)\cos(\omega t)u(t)$	$\frac{s+\alpha}{(s+\alpha)^2+\omega^2}$

### **Common Operational Transforms**

Operation	f(t)	F(s)
Multiplication by constant	cf(t)	cF(s)
Addition	$f_1(t) + f_2(t) - f_3(t) + \dots$	$F_1(s) + F_2(s) - F_3(s) + \dots$
First time derivative	$\frac{\mathrm{d}f(t)}{\mathrm{d}t}$	$sF(s) - f(0^-)$
Second time derivative	$\frac{\mathrm{d}^2 f(t)}{\mathrm{d}t^2}$	$s^2 F(s) - s f(0^-) - \frac{\mathrm{d}f(0^-)}{\mathrm{d}t}$
nth time derivative	$\frac{\mathrm{d}^n f(t)}{\mathrm{d}t^n}$	$s^n F(s) - \sum_{i=1}^n s^{n-1} \frac{\mathrm{d}^{i-1} f}{\mathrm{d}t^{i-1}}$
Time integral	$\int_{0}^{t} f(x)  \mathrm{d}x$	$\frac{F(s)}{s}$

Translation in time	$f(t-a)u(t-a), \ a>0$	$\exp(-as)F(s)$
Translation in frequency	$\exp(-at)f(t)$	F(s+a)
Scale change	f(at), a > 0	$\frac{1}{a}F\left(\frac{s}{a}\right)$
First frequency derivative	tf(t)	$\frac{\mathrm{d}F(s)}{\mathrm{d}s}$
nth frequency derivative	$t^n f(t)$	$(-1)^n \frac{\mathrm{d}^n F(s)}{\mathrm{d} s^n}$
Frequency integral	$rac{f(t)}{t}$	$\int_{0}^{\infty} F(u)  \mathrm{d}u$

# 1 Passive components

Current and Voltage for Passive Components:

Component	Current	Voltage	Energy
Resistor $R$	$i = \frac{v}{R}$	v = iR	$w_R = \int iv  \mathrm{d}t$
Capacitor $C$	$i(t) = C \frac{\mathrm{d}v}{\mathrm{d}t}$	$v(t) = v(t_0) + \frac{1}{C} \int_{t_0}^t i(t) dt$	$w_C(t) = \frac{1}{2}Cv^2(t)$
Inductor $L$	$i(t) = i(t_0) + \frac{1}{L} \int_{t_0}^t v(t) dt$	$v(t) = L \frac{\mathrm{d}i}{\mathrm{d}t}$	$w_L(t) = \frac{1}{2}Li^2(t)$

Combination of passive components:

Component	Series	Parallel
Resistor R	$R_{eq} = \sum_{i} R_{i}$	$\frac{1}{R_{eq}} = \sum_{i} \frac{1}{R_{i}}$
Capacitor C	$\frac{1}{C_{eq}} = \sum_{i} \frac{1}{C_{i}}$	$C_{eq} = \sum_{i} C_{i}$
Inductor $L$	$L_{eq} = \sum_{i} L_{i}$	$rac{1}{L_{eq}} = \sum_i rac{1}{L_i}$

### 1.1 Equilibrium Equations

### 1. Loop Current formulation:

- number of unknown currents equal number of loops
- KVL equation for each loop

### 2. Node Voltage formulation:

- number of unknown voltage equal number of nodes except reference
- KCL equation for each node

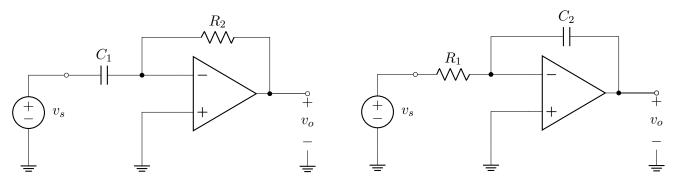


Figure 1: Op Amp Differentiator

Figure 2: Op Amp Integrator

$$v_o(t) = -R_2 C_1 \frac{\mathrm{d}v_s}{\mathrm{d}t}$$

$$v_o(t) = -\frac{1}{R_1 C_2} \int_0^t v_s(t') \,\mathrm{d}t'$$

#### 1.2 First Order Circuits

- 1. first order circuits are any circuit with a single energy storage element, an arbitrary number of sources and resistors
- 2. any current or voltage in such circuit is a solution to a first order differential equation

## 2 First order Unforced Response

Network	Current	Voltage	Time Constant	DC Steady State
Sourcefree RL	$i_L(t) = I_0 \exp\left(-\frac{R}{L}t\right)$	$v_L = -RI_0 \exp\left(-\frac{R}{L}t\right)$	$\tau = \frac{L}{R}$	$v_L = 0$
Sourcefree RC	$i_C(t) = -\frac{V_0}{R} \exp\left(-\frac{1}{RC}t\right)$	$v_c = V_0 \exp\left(-\frac{1}{RC}t\right)$	$\tau = RC$	$i_C = 0$

Typical time constant for RL is in ms, for RC in  $\mu$ s. For general RL and RC circuits, find the equivalent resistance as seen by the inductor/capacitor.

## 3 First order Forced Response

Consider a series RL circuit with voltage  $v(t) = V_0 u(t)$ . We have the following KVL equation of current

$$i(t) = 0 t < 0$$

$$Ri + L\frac{di}{dt} = V_0 t > 0$$

This differential equation gives a solution of

$$i(t) = \left[\underbrace{\frac{V_0}{R}}_{\text{forced response}} - \underbrace{\left(\frac{V_0}{R} - I_0\right) \exp\left(-\frac{R}{L}t\right)}_{\text{natural response}}\right] u(t) \tag{5}$$

1. Forced response

- dependent on forcing function
- steady state response  $t\gg au$
- 2. Natural response
  - similar to source-free circuit
  - · dependent on initial values and forcing function
  - · transient response

Generalization:

$$i_L(t) = \left[I_f - (I_f - I_i) \exp\left(-\frac{t}{\tau}\right)\right] u(t)$$
 (6)

$$v_c(t) = \left[ V_f - (V_f - V_i) \exp\left(-\frac{t}{\tau}\right) \right] u(t) \tag{7}$$

Note that equation (7) is for the voltage across the capacitor in an RC circuit.

### 3.1 Square Waves and Sequentially Switched Circuits

Now consider the series RL circuit with voltage  $v(t) = V_0 u(t) - V_0 u(t-t_0)$  and  $I_0 = 0$ . We can apply superposition to find the current:

$$i(t) = i_1(t) + i_2(t)$$
 
$$i(t) = \underbrace{\left[\frac{V_0}{R}\left(1 - \exp\left(-\frac{R}{L}t\right)\right)\right]u(t)}_{\text{caused by }V_0u(t) \text{ alone}} - \underbrace{\left[\frac{V_0}{R}\left(1 - \exp\left(-\frac{R}{L}(t - t_0)\right)\right)\right]u(t - t_0)}_{\text{caused by }V_0u(t - t_0) \text{ alone}}$$

For sequentially switched circuits, we consider the pulse width (PW) and period (T) of the pulsing.

Condition	Output	Condition	Output
$PW \gg \tau$	time enough to fully charge	T - PW $\gg  au$	time enough to fully discharge
$PW \ll \tau$	time NOT enough to fully charge	T - PW $\ll  au$	time NOT enough to fully discharge

#### 3.2 RC Oscillator

- 1. For a low pass RC circuit, the output (voltage at capacitor) is simply the input for low frequencies
  - (a) at  $\omega = 0$ ,  $v_o = v_i$
  - (b) at  $\omega \to \infty$ ,  $v_o \to 0$

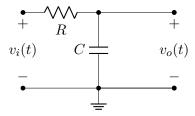
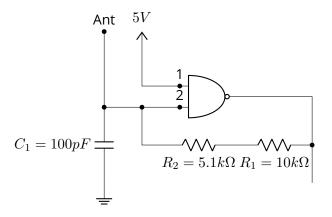


Figure 3: Low Pass Circuit



### 2. Schmitt Trigger RC

- (a)  $V_p = 2.9V \approx 3.0V, V_n = 1.9V \approx 2.0V$
- (b) As the voltage on  $C_1$  reaches  $V_p$ , the output will become voltage low. Then the voltage across the capacitor decays
- (c) When the voltage across  $C_1$  decays to  $V_n$ , output will become voltage high. Then the voltage across the capacitor increases
- (d) The behavior oscillates.
- (e) the voltage across the charging capacitor is

$$v = V_{cc} \left[ 1 - \exp\left(-\frac{t}{\tau}\right) \right]$$

(f) the time to charge to  $V_p$  is

$$t_1 = -\tau \ln \left( 1 - \frac{V_p}{V_{cc}} \right)$$

(g) the voltage across the discharging capacitor is

$$v = V_p \exp\left(-\frac{t}{\tau}\right)$$

(h) the time to discharge to  $V_n$  is

$$t_2 = -\tau \ln \left(\frac{V_n}{V_p}\right)$$

(i) the voltage across the charging capacitor from  ${\it V}_n$  to  ${\it V}_p$  is

$$v = V_{cc} - (V_{cc} - V_n) \exp\left(-\frac{t}{\tau}\right)$$

(j) the time to charge to from  $V_n$  to  $V_p$  is

$$t_3 = -\tau \ln \left( \frac{V_{cc} - V_p}{V_{cc} - V_n} \right)$$

- 3. For a high pass RC circuit, the output (voltage at capacitor) is simply the input for high frequencies
  - (a) at  $\omega = 0$ ,  $v_o = 0$
  - (b) at  $\omega \to \infty$ ,  $v_o \to v_i$

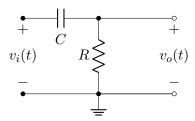


Figure 4: High Pass Circuit

## **Diode and Transistor Switching: Half Wave Rectifier**

1. The half wave rectifier has the following circuit

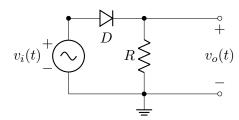


Figure 5: Half Wave Rectifier

(a) the diode is open only when  $v_i(t)>v_{
m on}$ , hence only the positive voltage are seen by  $v_o(t)$ 

i. Average Value 
$$\frac{V_{\rm m}}{\pi}$$

ii. 
$$V_{\rm rms}=rac{V_{\rm m}}{2}$$

iii. 
$$I_{\rm m}=\frac{V_{\rm m}}{R_{\rm L}}$$

iv. Ripple Factor 
$$\frac{I_{\rm rms}}{I_{\rm DC}}$$

iv. Ripple Factor 
$$\frac{I_{\rm rms}}{I_{\rm DC}}$$
 v. Efficiency  $e=\frac{{
m DC~Output~Power}}{{
m AC~Output~Power}}$ 

(b) a smoothing capacitor is added (capacitor filter) so that the output waveform does not have a 0value:

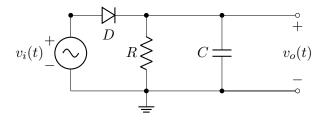


Figure 6: Half Wave Rectifier with Capacitor Filter

i. C is chosen such that  $RC\gg T$  so the exponential seems linear

### 5 LC Oscillations

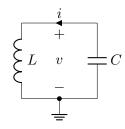


Figure 7: LC Oscillator

- 1. most of the time, either v(0) or i(0) are given.
- 2. by conservation of energy:  $\frac{1}{2}Li^2 = \frac{1}{2}Cv^2$
- 3. the differential equations are  $v=Lrac{\mathrm{d}i}{\mathrm{d}t}$  and  $i=-Crac{\mathrm{d}v}{\mathrm{d}t}\implies i=rac{1}{LC}rac{\mathrm{d}^2i}{\mathrm{d}t^2}$
- 4. we have  $\omega = \frac{1}{\sqrt{LC}}$
- 5. the solutions have the form

$$i = I_0 \cos \left(\frac{t}{\sqrt{LC}} + \phi\right)$$
$$v = -I_0 \sqrt{\frac{L}{C}} \sin \left(\frac{t}{\sqrt{LC}} + \phi\right)$$

or

$$v = V_0 \cos \left(\frac{t}{\sqrt{LC}} + \phi\right)$$
$$i = -V_0 \sqrt{\frac{C}{L}} \sin \left(\frac{t}{\sqrt{LC}} + \phi\right)$$

## **6 Source-free RLC Circuits**

	Characteristic Equation	$(\alpha)$	$(\omega_0)$	Damping Factor $(\zeta)$
Series $i(t)$	$s^2 + \left(\frac{R}{L}\right)s + \frac{1}{LC} = 0$	$\alpha = \frac{R}{2L}$	$\omega_0 = \frac{1}{\sqrt{LC}}$	$\zeta = \frac{R}{2} \sqrt{\frac{C}{L}}$
Parallel $v(t)$	$s^2 + \left(\frac{1}{RC}\right)s + \frac{1}{LC} = 0$	$\alpha = \frac{1}{2RC}$	$\omega_0 = \frac{1}{\sqrt{LC}}$	$\zeta = \frac{1}{2R} \sqrt{\frac{L}{C}}$

$$s_{1,2} = -\alpha \pm \sqrt{\alpha^2 - \omega_0^2} \tag{8}$$

Case	Condition	Characteristic	Roots
Overdamped	$\zeta > 1$	Does not oscillate about the steady state value	Real, Distinct
Underdamped	$\zeta < 1$	Oscillation with decay envelope	Complex
Critacally damped	$\zeta = 1$	Decays fastest to steady state without oscillation	Real, equal

### 7 Resonance

- 1. resonance the fixed amplitude forcing function produces a response of maximum amplitude
- 2. Series Resonant Conditions:

(a) 
$$\omega_0 = \frac{1}{\sqrt{LC}}$$

- (b)  $Z_{in} = R$
- (c) voltage and current of source in phase
- (d) current magnitude is maximum
- (e) electric filter
- (f) the half-power-point frequency is where the power is half:

$$\omega_{1, 2} = \mp \frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}}$$
 (9)

(g) bandwidth: 
$$BW = \omega_2 - \omega_1 = \frac{R}{L}$$

(h) Quality factor: 
$$Q = \frac{\omega_0}{BW} = \frac{1}{R} \sqrt{\frac{L}{C}}$$

(i) 
$$\omega_0^2 = \omega_1 \omega_2$$

3. Parallel Resonant Conditions:

(a) 
$$\omega_0=rac{1}{\sqrt{LC}}$$

(b) 
$$Y_{in} = \frac{1}{R}$$

- (c) voltage and current of source in phase
- (d) voltage magnitude is maximum
- (e) electri c filter
- (f) the half-power-point frequency is where the power is half:

$$\omega_{1, 2} = \mp \frac{1}{2RC} + \sqrt{\left(\frac{1}{2RC}\right)^2 + \frac{1}{LC}} \tag{10}$$

(g) bandwidth: 
$$BW = \omega_2 - \omega_1 = \frac{1}{RC}$$

(h) Quality factor: 
$$Q = \frac{\omega_0}{BW} = R\sqrt{\frac{C}{L}}$$

(i) 
$$\omega_0^2 = \omega_1 \omega_2$$

4. Physical model:  $R_1$  series to L, C parallel to that series and to  $R_2$ 

(a) 
$$\omega_0 = \sqrt{rac{1}{LC} - \left(rac{R_1}{L}
ight)^2}$$

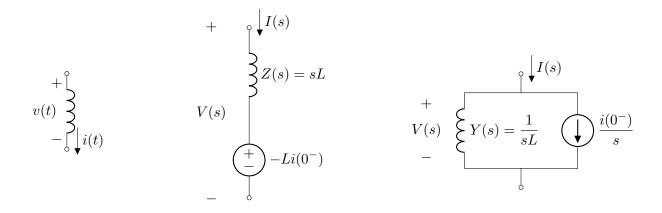
## 8 Laplace Transform Applications

Transform of circuit elements:

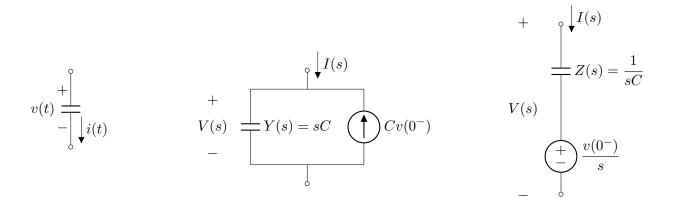
1. Resistor:



2. Inductor:



3. Capacitor:



#### 8.1 Method 1

- 1. Write the differential equations for the unknown function  $\boldsymbol{x}(t)$
- 2. Apply Laplace transform on the equation

- 3. Use algebraic manipulation for X(s)
- 4. Apply inverse Laplace transform to get x(t)

#### 8.2 Method 2

- 1. Apply Laplace transform on each element
- 2. Use DC circuit analysis techniques to write the s-domain equations involving X(s)
- 3. Apply inverse Laplace transform to get x(t)

#### **Examples**

- 1. Resistors:  $v = iR \iff V = IR$ , where  $V = \mathcal{L}\{v\}, I = \mathcal{L}\{i\}$
- 2. Inductors:  $v = L \frac{\mathrm{d}i}{\mathrm{d}t} \Longleftrightarrow V = L \left[ sI i(0^{-}) \right] = sLI LI_0$
- 3. Capacitors:  $i = C \frac{\mathrm{d}v}{\mathrm{d}t} \Longleftrightarrow I = C \left[ sV v(0^-) \right] = sCV CV_0$
- **8.3**  $v(t) = V_0 u(t)$ 
  - 1. Find the equivalent circuit using the Laplace equivalent of the circuit
  - 2. Solve for V(s). May involve partial fraction decomposition. This is a nice guide
  - 3. Use Inverse Laplace transform to get v(t)

**Transfer function.** The *s*-domain ratio of the output to input signal.

$$H(s) = \frac{Y(s)}{X(s)} \tag{11}$$

		H(s) of series RL
Input is $V(t)$	Output is $i(t)$	$H(s) = \frac{1}{R + sL}$
	Output is $v(t)$	$H(s) = \frac{sL}{R + sL}$

**8.3.1** 
$$v(t) = V_0 \cos(\omega t)$$

The response has the form  $i(t) = I_1 \cos(\omega t) + I_2 \sin(\omega t)$ . Exploit the transfer function of the circuit.

## 9 Ramp and Sine Response

- 10 Second Order System
- 11 Transients in Power Systems
- 12 Switching Power Supply
- 13 Filter Design