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Challenge Statement



To Design and develop a High pressure Trunnuion-Mounted Ball Valve within Target cost (€9000).

Concept / Scope of solution



The Concept and Scope of the project :

- To develop the Ball Valve within Target cost (€9000).
- To design as per API, PED, NACE & Fugitive Emission requirements.
- To Introduce unique design features like Automatic Cavity Pressure Relief,
 Anti-Blow out Stem, Fire Safe design, Sealant Injection Arrangement etc.
- To design major parts of the valve (Body /connector) through Forging process.
- •To develop the Supply chain & Prototypes of valve.

Pros and Cons of the solution



- Developing the design meeting to Target cost .
- Developing Unique Design Features like Automatic Cavity Pressure Relief, Sealant injection & Fire Safe design.
- Developing Forged design is a challenge compared to casting design.
- Developing Soft seat design for sealing at Normal & Fire condition.
- Achieving "Zero leakage" at less torque.(350 N)
- Challenges to fix the Tight tolerance band for critical assemblies.
- Developing Supply chain within India (High Capacity Forgings)

Detailed Description

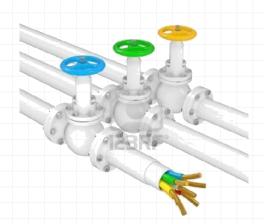


The project is to Design & Development of 8" Class 900 Trunnion Mounted High pressure Ball valve (TMBV) for the oil and gas industry application complying with API and NACE standards.

A valve is a Mechanical device that controls the flow of fluid & pressure

in the Pipe lines, Vessels etc by opening or closing.

- Stopping and starting flow On/Off applications.
- Regulating the fluid volume Throttling applications
- Preventing reverse flow Non-Return applications
- Relieving over pressure Safety relief.



Technology/Background



Super Critical & Ultra- Supercritical Technology

- Higher Pressure & Temperatures => Better Efficiency
- Better Efficiency = Less Emissions and Less Carbon Dioxide

Plant type with power rating	Steam Pressure PSI (Kg/cm ²⁾	Steam Temp. (°C)	Efficiency (%)
Sub Critical (500 MW)	2418 (170)	540	35 - 38%
Super Critical (800 MW)	3556 (250)	560 – 590	40 – 42 %
Advanced Ultra Super Critical (800 MW)	4267 (300)	> 700	45 – 47 %

In recent years, the valve manufacturers across the world focused their attention towards developing the High Pressure & Performance Ball valve.

Development Procedure/Methodology



Design of 8" class 900 Trunnion Mounted Soft Seated Ball Valve (Forged two-piece design) compliance to API standards, NACE & Customer specifications.

The detailed execution process:

- > Freezing the design specifications
- ➤ Concept Design & Development
- ➤ Design optimization using VAVE approach
- ➤ Design Calculations program
- ➤ 3D Modelling & Assembly
- ➤ Validation of the design using FEA & CFD analysis
- ➤ Tolerance Stack Up Analysis
- > Bill of materials with Material details
- ➤ 2D Manufacturing drawings
- ➤ Design Reports
- > Supplier Chain development for the Forging, Machining, Bought out parts, Assembly.
- > Prototype Development & Testing.



Implementation and prototype / POC



Trunnion Mounted Ball Valve

DESIGN FEATURES				
1	Double Block & Bleed Mechanism			
2	Automatic Cavity Pressure Relief system (Single Piston Effect)			
3	Anti-Blow out proof- Stem design			
4	Sealant Injection Arrangement			
5	Fire Safe design			

PARAMETERS	VALUE		
Valve	Trunnion Mounted Ball Valve (TMBV)		
Size	8 inches (DN 200)		
Class	900		
Construction	2 Piece – Forged Design		
Ball Bore Type	Full Bore		
Seat Sealing	Soft Seated		
Material	Carbon Steel (ASTM A105)		
Ball – Stem Drive	Spline Connection		
Service temperature range	- 40 deg. C to +200 deg. C		
Rated Pressure	15.52 Bar (2250 Psi)		

Design Standards

Design : ISO 17292 / API 6D

· Face-to-Face : ASME B16.10

Testing : ISO 17292 / API 6D

Pressure-Temperature rating

ASME B16.34

End Connection

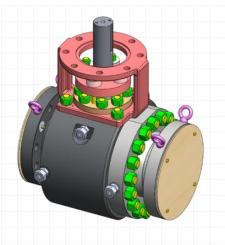
Flanged End : ASME B16.5

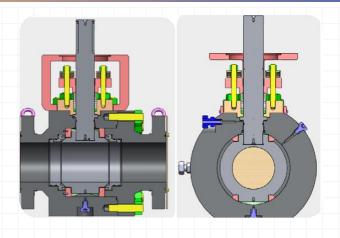
· Socket Weld End: ASME B16.11

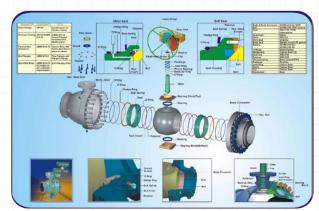
Butt Weld End : ASME B16.25

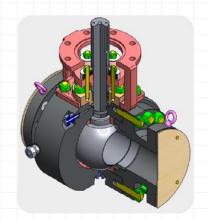
Implementation and prototype / POC







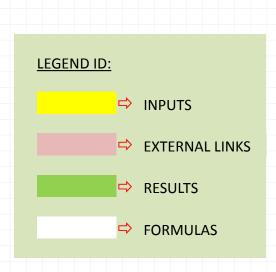




Implementation and prototype / POC

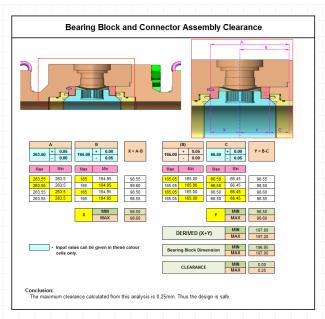


			BODY WALL THICKNESS				
SI.No	Parameters		Formulae		Value	Unit	SOURCE
		Min	imum Shell Thickness - ASME B	16.34			
Case 1	Body material				ASTM A105		
	Pressure rating		Pc		900		
	Stress based constant		Sf		7000		Non-Mandatory App-8
	Inside diameter		d			mm	
	OL HUI: I		4 5		7.9		
	Shell thickness		1.5* [(Pc * d) / (2*Sf-1.2*Pc)]		0.83 21.0		
Case 2	Shell thickness from table					mm	Table-3A
outo E	SHELL ELLICKHESS HOLL LUDIC	Minin	num Shell Thickness - ASME VIII	UG - 27	23.4		Tubic SA
	Pressure rating		Р		2250	Psi	
						N/Sq.mm	
Case 3	Allowable stress		S			N/Sq.mm	
Cuse 5	Inside radius		R		100.50		
	Joint efficiency		E		1.00		
	Shell thickness (Under Circumferential s				12.1	mm	
	0-1-1-1-1	Mini	num Shell Thickness - EN12516 -	Part 1	45.47	N/O	T-11- 4
	Calculation pressure Allowable stress		Pc S			N/Sq.mm N/Sq.mm	
Caso 4	Inside diameter		Di			mm	Table-1
Cusc 4	Constant (Erosion & Linear corrosion)		E		1		Table-1
	Shell thickness		(1.5*Pc*Di)/((2*S) - (1.2*Pc)) + Coi	nstant(F)		mm	Tubic
Case 5	Shell thickness from table		(112 1 2) (112 1 3))	iota.ii(L)		mm	Table-10
	Maximum wall thickness				23.70	mm	
	Thickness	provide	ed in the design		24.0	mm	
No. of	spring			Nos.	1	18	18
Force	on each spring			N	24	8.2	248.2
Defle	ction			mm		4	4
Stiffness of spring k		k=F/	deflection	N/mm	62	.05	62.05
		F*nc	of spring	N	44	167	4467
Total Force at upsteam			, ,	N	82	201	8201
'		pi()/	4(Dso^2-Dsi^2)	mm²	174	1.70	1741.70
			3D model	mm ²		542	2542
			Force/Seat area	N/mm		.71	4.71
		_	d on 3d Model	N/mm	+	.23	3,23
	esign		ating stress > 2 N/mm2			ES	YES
Sale Design		III 26	uting 5ti C33 / 2 iv/ iiilil2				11.5

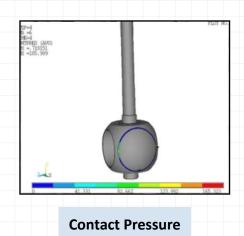


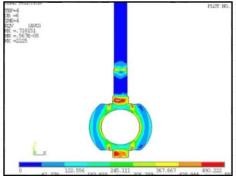
Validation / Testing / Analysis Method





Tolerance Stack - Up analysis

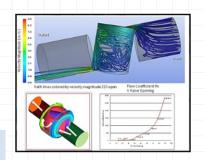


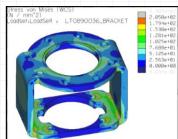






FE model Ball-valve assembly





Cost /benefits



Weight Forging **Casting Machining Details** Cost Cost Cost Project:METSO-Phase1C-Standard Valve **Production Quote** V Two piece HPBV -8" CL 900 TM Carbon Steel- S.S Trim -Cost Estimation Report Weight -Machining **Drop Forging** Casting Forged Qty Components S.no Material After Weight Open Die Forging Sand Casting Machining Indian Supplier Pouring Each weight Production-40 No's Production-40 No's Production-40 No's Tooling Tooling Tooling Unit Price-In Unit Price Unit Price-Unit Price Unit Price-In **Unit Price** nvestment in Kg in no's in Kg Investment Investment nvestment In INR INR In Euro In Euro In Euro Cost in Cost in INR Cost in Euro Cost in INR Body -(Forging+machining) ASTM A105 575.60 1.00 982.40 103543.00 1532 74900.00 1109 23120.00 342 2 Connector - (Forging+Machining) ASTM A105 200.20 1.00 421.40 54443.00 806 21000.00 311 10350.00 153 3 Seat Ring -(Casting+Machining) ASTM A 351 Gr CF8M 10.10 13.40 27000.00 400 14793.60 219 17338.00 257 4320.00 64 2.00 Ball -(Forging+Machining) ASTM A182 F316 55.80 1.00 144.50 64125.00 949 0.00 0 11300.00 167 Gland Flange -(casting+Machining) ASTM A216 Gr WCB 17900.00 265 1713.48 25 13400.00 9.20 1.00 13.10 198 950.00 14 Bearing Block -(Casting+Machining) ASTM A216 Gr WCB 4.20 5.70 25000.00 370 3556.80 53 17500.00 259 1390.00 21 2.00 Bonnet -(Forging+Machining) ASTM A105 24.20 1.00 38.60 4100.00 61 11245.00 166 2670.00 40 Bracket-(Casting + Machining) ASTM A216 Gr WCB 585 6409.20 95 10940.00 1542.00 41.00 1.00 49.00 39500 162 23 Stem-(Bar+Machining) ASTM A479 TY 316 34.10 1.00 86.40 0.00 0 30800.00 456 Rs. 2.26,211 € 3.348 Rs. 1.09.400 € 1.619 Rs. 26.473 € 392 Rs. 1.66.323 € 2.462 Rs. 86.442 € 1.279 Total

Results and potential Business Impact for L&T TS



Key Achievements:

- Achieved the target cost of ball valve (€9000)
- Implemented unique product features to boost up the product sales.
- Optimized the Torque by 10% through introduction of bearings & material selection.
- The sealing integrity is enhanced by the fire safe & emergency sealant design.

Conclusion



Achieved the within target cost €8100 as set by client, helps to be competitive on the market.



- Top down assembly helps to reduce the design lead time for size extension.
- Automated the Design calculations and tolerance stack up analysis & parametric relations programs which helped to reduce the lead time.
- Design is successfully validated through FEA (both linear & non-linear) & CFD flow analysis (with different openings).

References



- http://ec.europa.eu/enterprise/sectors/pressure-and-gas/documents/ped/
- Beychok, Milton R. (2005). <u>Fundamentals Of Stack Gas Dispersion</u> (4th ed.). author-published. <u>ISBN 0-9644588-0-2</u>. See Chapter 11, Flare Stack Plume Rise.
- ONE TUEV BV Technische Inspektions GmbH. "List of countries accepting the ASME Boiler & Pressure Vessel Code". Onetb.com. Retrieved 2012-01-19.
- <u>"API 5210-1, Sizing and Selection of Pressure-Relieving Devices"</u>. Techstreet.com. Retrieved 2012-01-19.
- "DIERS". Iomosaic.com. Retrieved 2012-01-19.
- H.G. Fisher, H.S. Forrest, Stanley S. Grossel, J. E. Huff, A. R. Muller, J. A. Noronha, D. A. Shaw, B. J. Tilley (1992). Emergency Relief System Design Using DIERS Technology: The Design Institute for Emergency Relief Systems (DIERS) Project Manual. <u>ISBN</u> 978-0-8169-0568-3.
- "EDUG: European DIERS Users' Group". Edug.eu. Retrieved 2012-01-19.
- "CRR 1998/136 Workbook for chemical reactor relief system sizing". Hse.gov.uk. Retrieved 2012-01-19.

