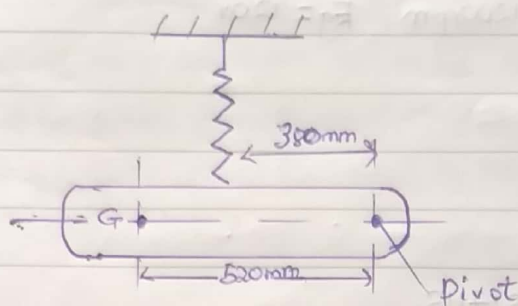


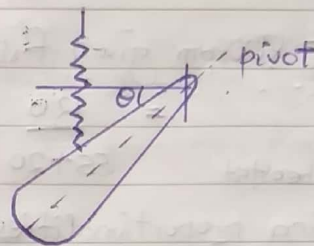
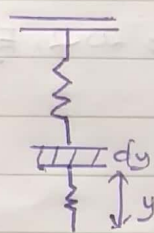
ME 362 VIBRATIONS ASSIGNMENT 1

1. Mass = 25kg, Radius of gyration = 0.235m, period of oscillation, $T = ?$



Let the system displaced by θ about the pivot and deflection of spring be x

$$\therefore x = 380\theta = 0.38\theta$$



Let spring of length l and mass per unit length, m

Let a strip dy at distance y from the base.

Then, dm (strip mass) = $m dy$

Let force and velocity ω

$$\text{velocity of strip} = \frac{v}{\omega} y$$

$$\therefore \text{Kinetic energy} = \int_0^l \frac{1}{2} m dy \left(\frac{v}{\omega} y \right)^2$$

$$K = \frac{1}{2} \frac{m' v^2}{\omega^2} \times \frac{1}{3} [y^3 - 0]$$

$$K = \frac{1}{2} \frac{m' l v^2}{\omega^2} \times \frac{1}{3}$$

$$\text{But } m' l \omega = m s$$

$$K = \frac{1}{2} \left(\frac{m s}{3} \times v^2 \right)$$

Applying the Energy Theorem,

Total energy

$$T = \frac{1}{2} \frac{m s}{3} v^2 + \frac{1}{2} I \dot{\theta}^2 + \frac{1}{2} k x^2$$

where $\frac{1}{2} k x^2$ is the strain energy of the spring.

$\frac{1}{2} I \dot{\theta}^2$ is the rotational kinetic energy of the bar about O.

$$I = mk^2 + m \times 0.52^2$$

$$v = \dot{x} = 0.38\dot{\theta}$$

$$T = \frac{1}{2} \frac{m_s}{3} \times (0.38\dot{\theta})^2 + \frac{1}{2} I \dot{\theta}^2 + \frac{1}{2} k (0.38\dot{\theta})^2$$

Differentiating about θ and putting $dT/d\theta = 0$ yields:

$$\frac{dT}{d\theta} = \frac{1}{2} \frac{m_s}{3} \times 0.38^2 \times 2\dot{\theta} \times \ddot{\theta} + \frac{1}{2} I \times 2\dot{\theta} \times \ddot{\theta} + \frac{1}{2} k \times 0.38^2 \times \dot{\theta} \times 2\dot{\theta} =$$

$$\dot{\theta} \left[\left(\frac{m_s}{3} \times 0.38^2 + I \right) \ddot{\theta} + k \times 0.38^2 \dot{\theta} \right] = 0$$

$$\therefore \dot{\theta} \neq 0$$

$$\Rightarrow \left(\frac{m_s}{3} \times 0.38^2 + I \right) \ddot{\theta} + k \times 0.38^2 \dot{\theta} = 0$$

$$I = 25 \times 0.235^2 + 25 \times 0.52^2$$

$$I = \frac{521}{64} \text{ kg-m}^2$$

$$\left(\frac{3}{3} \times 0.38^2 + \frac{521}{64} \right) \ddot{\theta} + 520 \times 0.38^2 \dot{\theta} = 0$$

$$\ddot{\theta} + 9.063098784 = 0$$

Compare the above with $\ddot{\theta} + \omega^2 \theta = 0$

$$\omega^2 = 9.063098784$$

$$\omega = 3.010498096 \text{ rad/s}$$

$$\therefore \frac{2\pi}{T} = 3.010498096$$

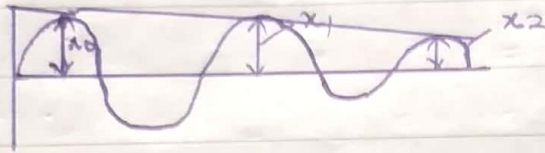
$$\text{Period, } T = 2.087091606 \text{ s}$$

2. Mass = 25kg Spring stiffness = 15kN/m

Let x_0 be the initial amplitude

Let x_1 be final amplitude after two consecutive vibrations

Let x_2 be $1/5 (x_1)$



$$x_2 = \left(\frac{1}{5}\right) x_1$$

$$\therefore \frac{x_1}{x_2} = 5$$

Therefore, the logarithmic decrement

$$\delta = \ln\left(\frac{x_n}{x_{n+1}}\right) = \ln\left(\frac{x_1}{x_2}\right)$$

$$\delta = \ln(5) = 1.609$$

Now from the formula

$$\delta = \frac{2\pi\zeta}{\sqrt{1-\zeta^2}}$$

$$1.60 = \frac{2\pi\zeta}{\sqrt{1-\zeta^2}}$$

Continuation

$$(1.60)^2 = \frac{4\pi^2\zeta^2}{1-\zeta^2}$$

$$2.59(1-\zeta^2) = 4\pi^2\zeta^2$$

$$2.59 - 2.59\zeta^2 = 39.4\zeta^2$$

$$41.99\zeta^2 = 2.59$$

$$\zeta = 0.2483$$

\therefore the damping ratio, ζ is 0.2483

Calculating the damping co-efficient yields:

$$\zeta = \frac{c}{c_c} \quad \text{where } c = \text{actual damping coefficient}$$

$$c_c = \text{critical damping coefficient}$$

$$\text{But } c_c = 2\sqrt{km} = 2\sqrt{15 \times 10^3 \times 25}$$

$$c_c = 1224.7 \text{ Ns/m}$$

$$\zeta = \frac{c}{c_c}$$

$$0.2483 = \frac{c}{1224.7}$$

$$c = 0.2483 \times 1224.7$$

$$c = 304.1 \text{ Ns/m}$$

2. calculations of frequency of vibration

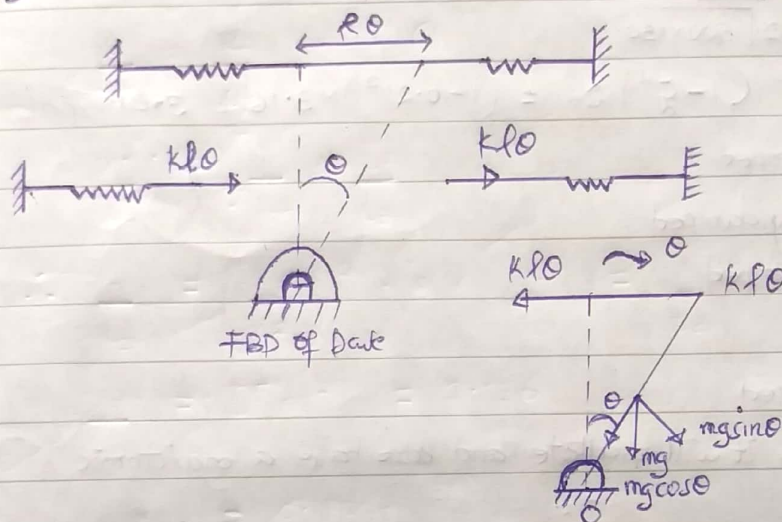
$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{15 \times 10^3}{25}}$$

$$\omega_n = 24.5 \text{ rad/s}$$

$$f_n = \frac{\omega_n}{2\pi} = \frac{24.5}{2 \times 3.14}$$

$$\therefore f_n = 3.9 \text{ Hz}$$

3.



Writing torque equation about O yields;

$$-mg \sin \theta \times \frac{l}{2} + 2kl^2 \theta = I \ddot{\theta} = \frac{ml^2}{3} \ddot{\theta}$$

$$\frac{ml^2}{3} \ddot{\theta} - mg \sin \theta \frac{l}{2} + 2kl^2 \theta = 0 \quad \text{since } \theta \text{ is small, } \sin \theta = \theta$$

$$\frac{ml^2}{3} \ddot{\theta} + \left(-mg \frac{l}{2} + 2kl^2 \right) \theta = 0$$

$$\frac{ml}{3} \ddot{\theta} + \left(\frac{mg}{2} + 2kl \right) \theta = 0$$

$$\omega_n = \sqrt{\frac{-mg/2 + 2kl}{ml/3}}$$

$$\omega_n = \sqrt{\frac{4kl - mg}{ml/3}}$$

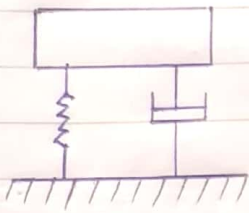
$$\omega_n = \sqrt{\frac{3(4kl - mg)}{2ml}}$$

$$f = \frac{1}{2\pi} \sqrt{\frac{3}{2} \frac{(4kl - mg)}{ml}}$$

The system is stable and will vibrate with the above frequency

9871517
Mechanical Engineering 3
ME 362 VIBRATIONS
ASSIGNMENT 2

1. Mass = 150 kg stiffness of spring, $k = 1500 \text{ N/m}$, damping coefficient, $c = 200 \text{ kg/s}$



i. Undamped natural frequency, $\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{1500}{150}} = 3.16 \text{ rad/s}$

ii. Damping ratio, $\xi = \frac{c}{2\sqrt{km}} = \frac{200}{2\sqrt{1500 \times 150}} = 0.21$

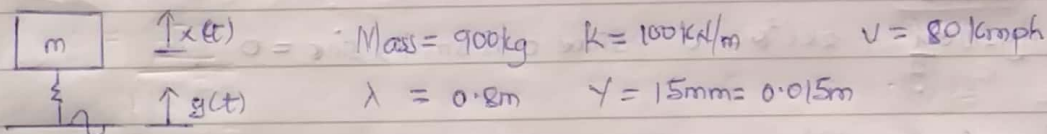
iii. Damped natural frequency, $\omega_d = (1 - \xi^2)^{1/2} \omega_n = (1 - 0.21^2)^{1/2} \times 3.16 = 3.019 \text{ rad/s}$

iv. W.K.T if $\xi > 1 \Rightarrow$ overdamped
 $\xi = 1 \Rightarrow$ critically damped
 $\xi < 1 \Rightarrow$ underdamped
 $\xi = 0.21 < 1$

\therefore the system is underdamped

v. YES, for an underdamped system, it will oscillate and also have a logarithmic decrement in every oscillation.

2.



Equation of motion:

$$m\ddot{x} + k(x - y) = 0$$

$$m\ddot{x} + kx = ky \quad \text{--- (1)}$$

But $y = \gamma \sin \omega t$

$$\omega = 2\pi f = 2\pi \left(\frac{v \times 1000}{3600} \right) \frac{1}{\lambda}$$

$$\omega = 2\pi \times 80 \times \frac{1000}{3600} \times \frac{1}{0.8} = 174.533 \text{ rad/s}$$

$$\therefore y = 0.015 \sin(174.533t) \quad \text{--- (2)}$$

Equation (1) then becomes

$$m\ddot{x} + kx = k\gamma \sin \omega t \quad \text{--- (3)}$$

The steady state response is given by particular solution of Equation (3)

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ME362 Assignment 2

2. Let $x_p(t) = A \cos \omega t + B \sin \omega t$ — (4)

$$\therefore \dot{x}(t) = -A \omega \sin \omega t + B \omega \cos \omega t$$

$$\ddot{x}(t) = -A \omega^2 \cos \omega t + B \omega^2 \sin \omega t$$

Substituting or putting in Eqn (3) yields:

$$-m \omega^2 (A \cos \omega t + B \sin \omega t) + k (A \cos \omega t + B \sin \omega t) = k Y \sin \omega t$$

$$\cos \omega t (-m \omega^2 A + k A) + \sin \omega t (-m \omega^2 B + k B) = k Y \sin \omega t$$

Now, comparing coefficients:

$$-m \omega^2 A + k A = 0 \Rightarrow A = 0$$

$$-m \omega^2 B + k B = k Y \Rightarrow B = \frac{k Y}{k - m \omega^2}$$

From Eqn (4),

$$x_p(t) = x(t) = \frac{k Y}{k - m \omega^2} \sin \omega t$$

Substituting values gives:

$$x(t) = \frac{100 \times 10^3 \times 0.015}{100 \times 10^3 - 9000 \times 174.533^2} \sin (174.533 t)$$

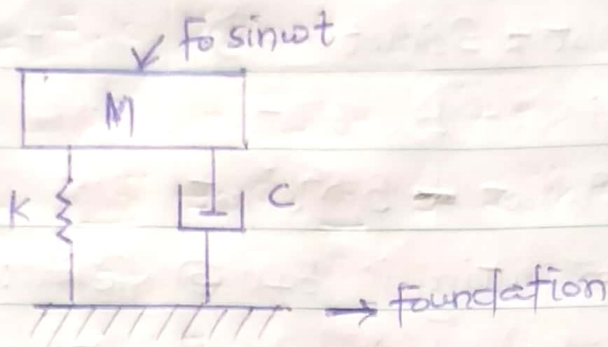
$$x(t) = -5.473 \times 10^{-6} \sin (174.533 t) \text{ — (5)}$$

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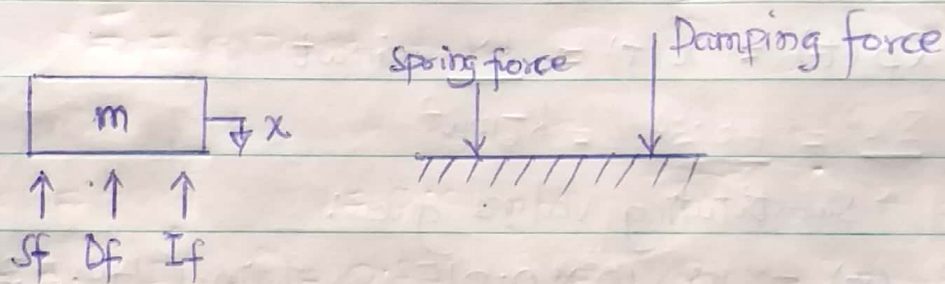
ME 362

ASSIGNMENT 2

3.



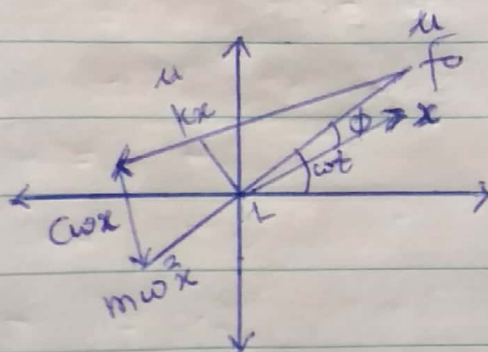
Total forces in the system are:

i F_0 ii Damping force $= C\dot{x}$ iii Inertia force $= m\omega^2 x$ iv Spring force $= Kx$ 

Let the force transmitted to the ground through spring and damper be F_T (Force Transmissibility).

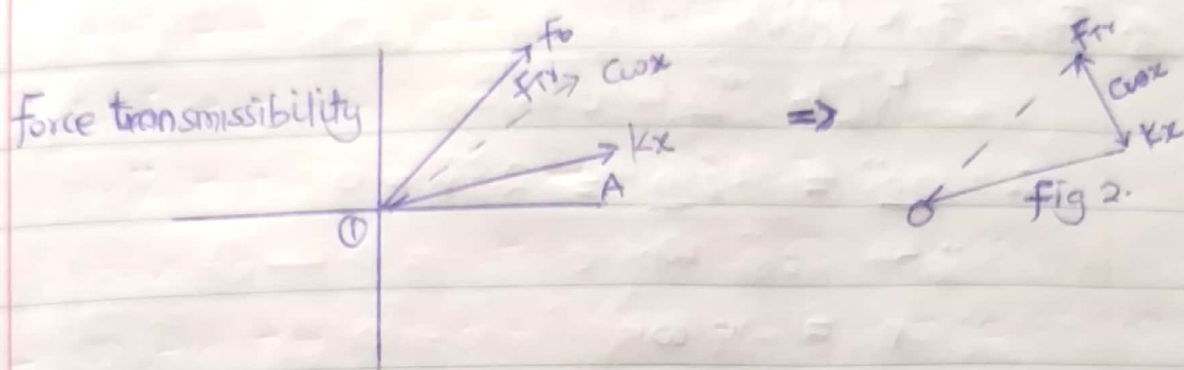
$F_T = \frac{\text{force transmitted to the foundation}}{\text{force impulsed upon the system}}$

Free Body Diagram



3

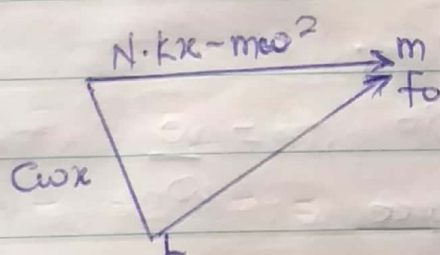
Phasor Diagram



From fig. 2

$$F_{Tr} = \sqrt{(cwx)^2 + (kx)^2}$$

$$F_{Tr} = x \sqrt{(c\omega)^2 + k^2} \quad \text{--- ①}$$



$$F_0 = \sqrt{(kx - m\omega^2 x)^2 + (cwx)^2}$$

$$F_0 = \sqrt{x^2 (k - m\omega^2)^2 + (c\omega)^2}$$

$$F_0 = x \sqrt{(k - m\omega^2)^2 + (c\omega)^2}$$

$$\Rightarrow x = \frac{F_0}{\sqrt{(k - m\omega^2)^2 + (c\omega)^2}} \quad \text{--- ②}$$

Putting the value of x in Eqn ① gives:

$$F_{Tr} = \frac{F_0 \sqrt{(c\omega)^2 + k^2}}{\sqrt{(k - m\omega^2)^2 + (c\omega)^2}} \quad \text{--- ③}$$

$$F_{Tr} = \frac{F_0 \cdot k \sqrt{\left(\frac{c\omega}{k}\right)^2 + 1}}{k^2 \left(1 - \frac{m\omega^2}{k}\right)^2 + (c\omega)^2}$$

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ME362 Assignment 2

$$3. F_{Tr} = \frac{F_0 \cdot k \sqrt{(c\omega/k)^2 + 1}}{k \sqrt{(1 - m\omega^2/k)^2 + (c\omega/k)^2}}$$

$$\therefore \frac{c\omega}{k} = 2\zeta \frac{\omega}{\omega_n} = 2\zeta r$$

$$r = \omega/\omega_n$$

$$\frac{F_{Tr}}{F_0} = \frac{\sqrt{1 + (2\zeta r)^2}}{\sqrt{(1 - r^2)^2 + (2\zeta r)^2}} \quad \text{--- (2)}$$

The expression about is for force transmitted to foundation where :

ζ = damping ratio , $r = \frac{\omega}{\omega_n}$
 F_0 = external force

Mass = 40kg, $m \cdot r = 0.01 \text{ kg} \cdot \text{m}$, Transmissibility = 10%

$$F_T = 0.1 \times F_0, \quad \zeta = 0.2, \quad N = 1480 \text{ rev/min} = \omega = \frac{2\pi \times 1480}{60}$$

$$\omega = 155 \text{ rad/s}$$

Total rotating unbalance

$$F_0 = m \cdot r \cdot \omega^2$$

$$F_0 = (0.01) \times (155)^2 = 240 \text{ N}$$

$$\text{force transmitted} = \frac{10}{100} F_0$$

$$F_T = 24 \text{ N}$$

From Eqn (2), the force transmitted to foundation is

$$F_T = \sqrt{1 + (2\zeta r)^2}$$

$$24 = \sqrt{1 + (2(\zeta r))^2}$$

$$\text{But } \zeta = 0.2$$

3. $r = 59.94 = \frac{\omega}{\omega_n}$, $\omega = 155 \text{ rad/s}$

$$\omega_n = \sqrt{\frac{k}{m}} = \frac{\omega}{r} = \frac{155}{59.94} = 2.58$$

$$2.58^2 = \frac{k}{40}$$

$$k = 267.4 \text{ N/m}$$

\therefore the stiffness of the spring is 267.4 N/m

Removing the damping element from the system makes the damping ratio $= 0$. So we have to take $(r^2 - 1)$ instead of $(1 - r^2)$

$$\frac{F_I}{F_0} = \xi = 0.1 = \frac{1}{(1 - r^2)} \quad \text{from eqn ①}$$

$$(1 - r^2) = 10$$

$$r^2 = -9$$

Taking $(r^2 - 1)$,

$$0.1 = \frac{1}{r^2 - 1}$$

$$r^2 - 1 = 10$$

$$r = \sqrt{11} = 3.32$$

$$\therefore \omega/\omega_n = 3.32$$

In conclusion, removing the damping element will make the frequency of the system greater than the natural frequency.

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Mechanical Engineering 3
ME 362 VIBRATIONS
ASSIGNMENT 3

1. $M = 100\text{kg}$, $m = 10\text{kg}$, $k = 2\text{kN/m}$, $l = 2\text{m}$

$$(M+m)\ddot{x} + 2kx + ml\ddot{\phi} = 0$$

$$(100+10)\ddot{x} + 2(2)x + (10 \times 2)\ddot{\phi} = 0$$

$$110\ddot{x} + 20\ddot{\phi} + 4x = 0 \quad \text{--- (1)}$$

$$\ddot{x} + 2\ddot{\phi} + 5\phi = 0$$

$$\ddot{x} + 2\ddot{\phi} + 9.8\phi = 0 \quad \text{--- (2)}$$

Assuming the above solution in second order is:

$$x = x \cos(\omega_n t + \theta), \quad \ddot{x} = -\omega_n^2 x \cos(\omega_n t + \theta)$$

$$\phi = \theta \cos(\omega_n t + \theta), \quad \ddot{\phi} = -\omega_n^2 \theta \cos(\omega_n t + \theta)$$

where θ is the phase angle.

Now, substituting or putting the values in the equation:

$$-110\omega_n^2 x \cos(\omega_n t + \theta) - 20\omega_n^2 \theta \cos(\omega_n t + \theta) + 4x \cos(\omega_n t + \theta) = 0$$

$$[(-110\omega_n^2 + 4)x - 20\omega_n^2 \theta] \cos(\omega_n t + \theta) = 0 \quad \text{--- (3)}$$

$$-\omega_n^2 x \cos(\omega_n t + \theta) - 2\omega_n^2 \theta \cos(\omega_n t + \theta) + 9.8\theta \cos(\omega_n t + \theta) = 0$$

$$[-\omega_n^2 x + (-2\omega_n^2 + 9.8\theta)\theta] \cos(\omega_n t + \theta) = 0$$

Multiplying the above by 20 gives:

$$[-20\omega_n^2 x + (-40\omega_n^2 + 196)\theta] \cos(\omega_n t + \theta) = 0 \quad \text{--- (4)}$$

Using eqns (3) & (4), the natural frequency is calculated by

$$\det \begin{vmatrix} -110\omega_n^2 + 4 & -20\omega_n^2 \\ -20\omega_n^2 & -40\omega_n^2 + 196 \end{vmatrix} = 0$$

$$(-110\omega_n^2 + 4)(-40\omega_n^2 + 196) - (20\omega_n^2)^2 = 0$$

$$4000\omega_n^4 - 21640\omega_n^2 + 784 = 0 \quad \text{--- (5)}$$

From eqn (5),

$$\omega_n^2 = 0.036475, \quad 5.373525$$

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ME 362

ASSIGNMENT 3

1. $\omega_1 = 0.19 \text{ rad/s}$, $\omega_2 = 2.318 \text{ rad/s}$

For the mode shapes,

$$x_1 = \frac{\phi^{(1)}}{x^{(1)}} = \frac{-110\omega_1^2 + 4}{20\omega_1^2} = \frac{20\omega_1^2}{40\omega_1^2 + 196}$$

$$x_1 = \frac{-110(0.19)^2 + 4}{20 \times (0.19)^2} = -0.0168$$

$$x_2 = \frac{\phi^{(2)}}{x^{(2)}} = \frac{-110\omega_2^2 + 4}{20\omega_2^2} = \frac{-110(2.318)^2 + 4}{20(2.318)^2} = -5.46278$$

$$x^{(1)} = \begin{Bmatrix} x_1^{(1)} \\ \phi^{(1)} \end{Bmatrix} = \begin{Bmatrix} x_1^{(1)} \\ 0.0168 x^{(1)} \end{Bmatrix} = \begin{Bmatrix} x^{(1)} \\ -0.0168 x^{(1)} \end{Bmatrix}$$

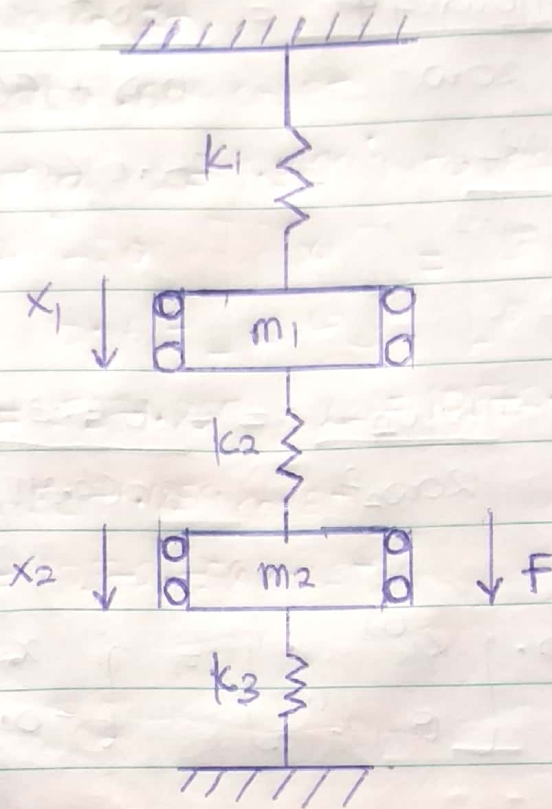
$$x^{(2)} = \begin{Bmatrix} x^{(2)} \\ \phi^{(2)} \end{Bmatrix} = \begin{Bmatrix} x^{(2)} \\ -5.46278 x^{(2)} \end{Bmatrix}$$

$$x_t^{(1)} = \begin{Bmatrix} x^{(1)} \\ \phi^{(1)} \end{Bmatrix} = \begin{Bmatrix} x^{(1)} \cos(\omega_1 t + \phi_1) \\ -0.0168 x^{(1)} \cos(\omega_1 t + \phi_1) \end{Bmatrix} = \text{first mode}$$

$$x_t^{(2)} = \begin{Bmatrix} x^{(2)} \\ \phi^{(2)} \end{Bmatrix} = \begin{Bmatrix} x^{(2)} \cos(\omega_2 t + \phi_2) \\ -5.46278 x^{(2)} \cos(\omega_2 t + \phi_2) \end{Bmatrix} = \text{second mode}$$

937151T
ME 362 VIBRATIONS
ASSIGNMENT 3

2. $f(t) = 15 \cos 3t$ kN, $m_1 = 7$ kg, $m_2 = 17$ kg, $k_1 = 30$ kN/m, $k_2 = 20$ kN/m, $k_3 = 16$ kN/m



Applying Newton's law of motion,

$$m_1 \ddot{x}_1 + k_1 x_1 + k_2 (x_1 - x_2) = F(t) \quad \text{--- ①}$$

$$m_2 \ddot{x}_2 + k_2 (x_2 - x_1) + k_3 x_2 = 0 \quad \text{--- ②}$$

Writing Eqns ① and ② in matrix form gives

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + \begin{bmatrix} (k_1 + k_2) & -k_2 \\ -k_2 & (k_2 + k_3) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} F(t) \\ 0 \end{bmatrix}$$

Calculating the undamped system solution of the system:

$$x_1(t) = x_1 \cos \omega t$$

$$= x_1 \cos 3t$$

$$\ddot{x}_1(t) = -\omega^2 x_1 \cos 3t$$

$$= -\omega^2 x_1 \cos 3t$$

$$2. \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} -\omega^2 x_1 \\ -\omega^2 x_2 \end{bmatrix} \cos 3t + \begin{bmatrix} k_1+k_2 & -k_2 \\ -k_2 & k_2+k_3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \cos 3t = \begin{bmatrix} 15 \\ 0 \end{bmatrix} \cos 3t$$

$$\begin{bmatrix} (k_1+k_2)-\omega^2 m_1 & -k_2 \\ -k_2 & (k_2+k_3)-\omega^2 m_2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 15 \\ 0 \end{bmatrix}$$

Putting the values in the matrix, let $\omega^2 = \lambda$

$$\begin{bmatrix} 50-7\lambda & -20 \\ -20 & 36-17\lambda \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 15 \\ 0 \end{bmatrix} \rightarrow \textcircled{3}$$

Solving for the determinant of eqn $\textcircled{3}$ gives:

$$\begin{bmatrix} 50-7\lambda & -20 \\ -20 & 36-17\lambda \end{bmatrix} = 0$$

$$(50-7\lambda)(36-17\lambda) - 400 = 0$$

$$119\lambda^2 - 1102\lambda + 1400 = 0$$

$$\lambda_1 = 7.7406, \lambda_2 = 1.5199$$

For the Natural frequency (ω),

$$\omega_1 = \sqrt{\lambda_1}$$

$$\omega_1 = \sqrt{7.7406}$$

$$\omega_1 = 2.78 \text{ rad/s}$$

$$\omega_2 = \sqrt{\lambda_2}$$

$$= \sqrt{1.5199}$$

$$\omega_2 = 1.23 \text{ rad/s}$$

Substituting $\lambda_1 = 7.7406$ into eqn $\textcircled{3}$

$$\begin{bmatrix} -4.1842 & -20 \\ -20 & -95.5902 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 15 \\ 0 \end{bmatrix}$$

$$\therefore x_1 = -44361.426, x_2 = 9281.604$$

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M/E 362 VIBRATIONS
ASSIGNMENT 3

2. $x_1(t) = x_1 \cos 3t$
 $= -44361.426 \cos 3t$

$x_2(t) = x_2 \cos 3t$
 $= 9281.604 \cos 3t$

Putting $\lambda_2 = 1.5199$ into eqn ②

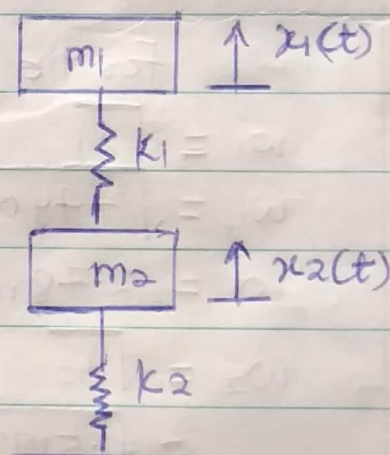
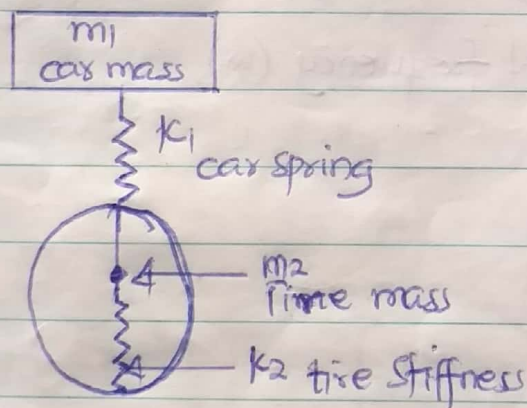
$$\begin{bmatrix} 39.3607 & -20 \\ -20 & 10.1617 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 15 \\ 0 \end{bmatrix}$$

$x_1 = 5371.859, x_2 = 10572.758$

$x_1(t) = 5371.859 \cos 3t$

$x_2(t) = 10572.758 \cos 3t$

3.



$m_1 = 200 \text{ kg}, m_2 = 50 \text{ kg}, k_1 = 1000 \text{ N/m}, k_2 = 10000 \text{ N/m}$

Equations of motion for the system:

$$m_1 \ddot{x}_1 + k_1 x_1 - k_1 x_2 = 0$$

$$m_2 \ddot{x}_2 - k_1 x_1 + (k_1 + k_2) x_2 = 0$$

Putting the values into the equations of motion yields:

$$200 \ddot{x}_1 + 1000 x_1 - 1000 x_2 = 0$$

$$50 \ddot{x}_2 - 1000 x_1 + (1000 + 10000) x_2 = 0$$

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ME 362 VIBRATIONS
ASSIGNMENT 3

3. Rewriting the above equations in matrix form:

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \ddot{x} + \begin{bmatrix} k_1 & -k_1 \\ -k_1 & k_1 + k_2 \end{bmatrix} x = 0$$

$$\begin{bmatrix} 2000 & 0 \\ 0 & 50 \end{bmatrix} \ddot{x} + \begin{bmatrix} 1000 & -1000 \\ -1000 & 11000 \end{bmatrix} x = 0$$

For the natural frequency,
 $\det(-\omega^2 m + k) = 0$

$$\begin{vmatrix} -m_1 \omega^2 + k_1 & -k_1 \\ -k_1 & -m_2 \omega^2 + (k_1 + k_2) \end{vmatrix} = 0$$

Substituting the values into the natural frequency,

$$\begin{vmatrix} -2000\omega^2 + 1000 & -1000 \\ -1000 & -50\omega^2 + 11000 \end{vmatrix} = 0$$

$$100000\omega^4 - 2.205 \times 10^7 \omega^2 + 10^7 = 0$$

$$\therefore \omega_1^2 = 0.454, \quad \omega_2^2 = 220.046$$

Therefore the natural frequency turns to be,

$$\omega_1^2 = 0.454$$

$$\omega_1 = \sqrt{0.454}$$

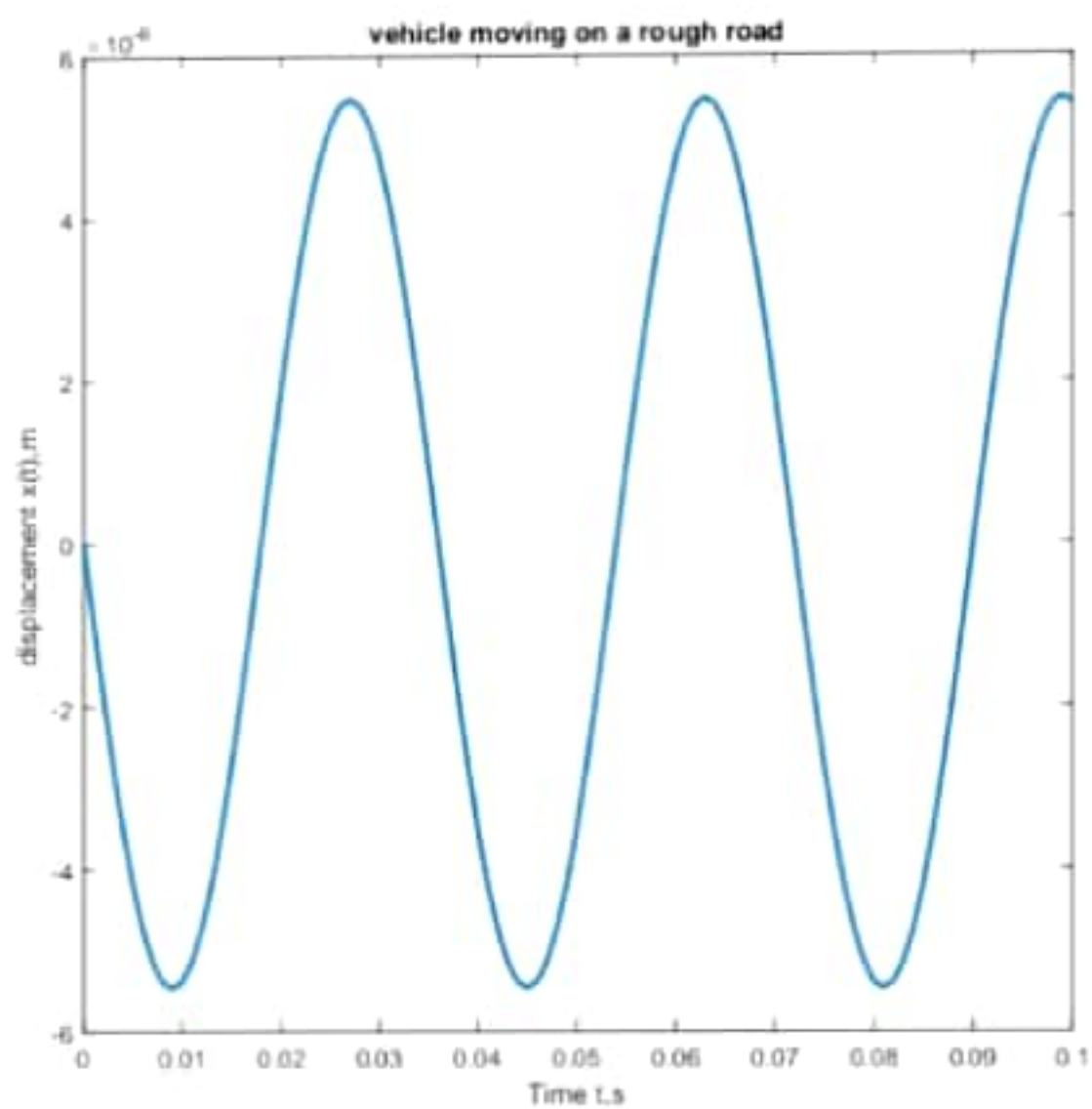
$$\omega_1 = 0.674 \text{ rad/s}$$

$$\omega_2^2 = 220.046$$

$$\omega_2 = \sqrt{220.046}$$

$$\omega_2 = 14.834 \text{ rad/s}$$

\therefore the values of the natural frequencies are $\omega_1 = 0.674 \text{ rad/s}$
and $\omega_2 = 14.834 \text{ rad/s}$



	A	B	C	D	E	F	G
1	t/s	x(t)/m					
2	0	-0.005000027					
3	0.1	-0.003555737					
4	0.2	-0.001961684					
5	0.3	-0.000384571					
6	0.4	0.001031289					
7	0.5	0.002174579					
8	0.6	0.002973191					
9	0.7	0.003396022					
10	0.8	0.003450743					
11	0.9	0.003178246					
12	1	0.002644695					
13	1.1	0.00193223					
14	1.2	0.001129343					
15	1.3	0.000418432					
16	1.4	-0.000414645					
17	1.5	-0.001020683					
18	1.6	-0.00145627					
19	1.7	-0.001702252					
20	1.8	-0.001759468					
21	1.9	-0.001646181					
22	2	-0.001394202					
23	2.1	-0.001044247					
24	2.2	-0.000641042					
25	2.3	-0.000228674					
26	2.4	0.000153426					
27	2.5	0.000473563					
28	2.6	0.000709752					
29	2.7	0.000850547					
30	2.8	0.00089479					
31	2.9	0.000850431					
32	3	-0.001394202					
33	3.1	0.000561561					
34	3.2	0.000359697					
35	3.3	0.000149647					
36	3.4	-4.80647E-05					
37	3.5	-0.000216623					
38	3.6	-0.000344018					
39	3.7	-0.000423563					
40	3.8	-0.000453849					
41	3.9	-0.000438214					
42	4	-0.000383846					
43							
44							

