

A FORMULA BOOK
FOR
DESIGN OF MACHINE MEMBERS

**Principles of Designing Machine Elements
Under
Steady and Fatigue Loads**

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FAILURE UNDER STATIC LOADS

General Design Equation for Ductile Failure

$$n = S_{ys}/\tau_{max}$$

Maximum Shear Stress Theory

$$n = 0.5 Syt/\tau_{max}$$

Maximum Distortion Energy Theory

$$n = S_{yt}/\sigma_e$$

$$\sigma_e = \left[(\sigma_1)^2 - \sigma_1 \sigma_2 + (\sigma_2)^2 \right]^{\frac{1}{2}}$$

Von-Mises Theory

$$\therefore n = 0.577 S_{yt}/\tau_{max}$$

Ductile Coulomb Mohr Theory

$$n = S_{ys}/\tau_{max}$$

Maximum Normal Stress Theory (MNST)

$$n = S_{ut}/\sigma_1$$

$$n = S_{ut}/\sigma_1$$

$$n = S_{uc}/\sigma_2$$

$$n = S_{uc}/\sigma_2$$

Brittle Coulomb Mohr Theory (BCMT)

$$n = S_{ut}/\sigma_1 + S_{uc}/\sigma_2$$

Modified I-Mohr Theory (M1MT)

$$n = S_{ut}/\sigma_1$$

$$\frac{1}{n} = \left[\frac{(S_{uc} - S_{ut})\sigma_1}{S_{ut}S_{uc}} \right] + \frac{\sigma_2}{S_{uc}}$$

Modified II-Mohr Theory (M2MT)

$$n = S_{ut}/\sigma_1$$

$$\frac{n\sigma_1}{S_{ut}} + \left[\frac{(n\sigma_2 + S_{ut})}{(S_{ut} - S_{uc})} \right]^2 = 1$$

FAILURE UNDER FATIGUE LOADING

10³-Cycle Strength for Ductile Materials

$$\text{Bending: } S_{10^3} = 0.9S_{ut}$$

$$\text{Axial: } S_{10^3} = 0.75S_{ut}$$

$$\text{Torsion: } S_{10^3} = 0.9S_{us}$$

$$\text{Steel } S_{us} = 0.8S_{ut}$$

$$\text{Others } S_{us} = 0.7S_{ut}$$

Modifying Factors for Endurance Limits

$$S_e = k_a k_b k_c k_d k_e k_f$$

Surface factor, k_a

$$k_a = a S_{ut}^b$$

Table 1: Parameters for Marin Surface Modification Factor

Surface Finish	Factor a	Exponent b
Ground	1.58	- 0.085
Machined or Cold Drawn	4.51	- 0.265
Hot Rolled	57.70	- 0.718
As-Forged	272.00	- 0.995

Size factor, k_b for Bending and Torsion

$$k_b = 1.00 \quad \text{for } d \leq 2.8$$

$$k_b = 1.24 d^{-0.107} \quad \text{for } 2.8 < d \leq 50 \text{ mm}$$

$$k_b = 1.51 d^{-0.157} \quad \text{for } 50 < d \leq 250 \text{ mm}$$

Load factor, k_c

$$\text{Bending, } k_c = 1.0$$

Axial,

$$k_c = 0.85$$

Torsional,

$$k_c = 0.577$$

Reliability Factor, k_e

Table 2: Reliability Factors					
Reliability (%)	50	90	95	99	
Factor, k _e	1.000	0.897	0.868	0.814	0.753

Modified Goodman Criterion:

$$1/FS = \frac{\sigma_m}{S_{ut}} + \frac{\sigma_a}{S_e}$$

Langer Yield Criterion

$$1/FS = \frac{\sigma_m}{S_{yt}} + \frac{\sigma_a}{S_{yt}}$$

DESIGN OF SHAFT

Shaft Torque: T = 7124 P/n

Forces exerted on Shafts

Spur Gear:

$$W_t = 2T/D$$

$$W_r = W_t \tan \phi$$

Helical Gear:

$$W_r = W_t \frac{\tan \phi_n}{\cos \psi}$$

$$W_a = W_t \tan \psi$$

Chain Sprocket:

$$F_C = 2T/D$$

$$F_{Cx} = F_C \cos \theta \quad \text{and} \quad F_{Cy} = F_C \sin \theta$$

V-belt Sheaves::

$$F_N = 2T/D$$

$$F_B = 1.5F_N = 3T/D$$

Flat-belt Pulleys: The analysis of the bending

$$F_B = 2.0F_N = 4T/D$$

Shaft diameter

$$D = \left[\frac{32N}{\pi} \sqrt{\left(\frac{K_t M}{S'n} \right)^2 + \frac{3}{4} \left(\frac{T}{S_Y} \right)^2} \right]^{\frac{1}{3}}$$

$$\text{Shaft as Torsion Bar} \quad \theta = \frac{Tl}{GJ}$$

$$\text{The critical speed } n_c = (30/\pi) \sqrt{(g/\delta_{st})}$$

DESIGN OF KEYS AND KEYWAYS

$$\text{Shear Failure} \quad \tau_{xy} = F/A_{shear}$$

$$\text{Bearing Failure} \quad \sigma_x = F/A_{bearing}$$

$$\text{Length} \quad L = \frac{4TN}{DWS_y}$$

ROLLING CONTACT BEARINGS

Load/Life Relationship

$$L_2/L_1 = (P_1/P_2)^k$$

Design life

$$L_d = (C/P_d)^k (10^6)$$

$$L_d = (h)(rpm)(60 \text{ min}/h).$$

Basic dynamic load rating:

$$C = P_d (L_d/10^6)^{\frac{1}{k}}$$

$$C = P_d f_L / f_N$$

The equivalent load

$$P = VR$$

$V = 1.0$ if the inner race rotates

$V = 1.2$ if the outer race rotates

$$P = VXR + YT$$

$$P_A = 0.4F_{rA} + 0.5 \frac{Y_A}{Y_B} F_{rB} + Y_A T_A$$

$$P_B = F_{rB}$$

$$P_A = 0.4F_{rB} + 0.5 \frac{Y_B}{Y_A} F_{rA} - Y_B T_A$$

Life Prediction under Varying Loads

$$F_m = \left(\frac{\sum_i (F_i)^p N_i}{N} \right)^{\frac{1}{p}}$$

$$L = \left(C/F_m \right)^p$$

DESIGN OF SPRINGS

Helical Compression Springs

Diameters

$$OD = D_m + D_w$$

$$ID = D_m - D_w$$

$$\text{Spring Rate:} \quad k = \Delta F / \Delta L$$

$$\text{The pitch angle} \quad \lambda = \tan^{-1} \left[\frac{p}{\pi D_m} \right]$$

Installation Considerations:

$$OD_s = \sqrt{D_m^2 + \frac{p^2 - D_w^2}{\pi^2}} + D_w$$

Spring Index:

$$C = D_m / D_w$$

Number of Coils:

$$\text{Squared and ground ends} \quad N_a = N - 2$$

$$\text{Plain ends} \quad N_a = N$$

$$\text{Plain coils with ground ends} \quad N_a = N - 1$$

Pitch:

$$\text{Squared and ground ends: } L_f = pN_a + 2D_w$$

$$\text{Squared ends only: } L_f = pN_a + 3D_w$$

$$\text{Plain and ground ends: } L_f = p(N_a + 1)$$

$$\text{Plain ends: } L_f = pN_a + D_w$$

$$\text{Coil Clearance: } cc = \frac{L_o - L_s}{N_a}$$

$$\text{Stresses } \tau = \frac{8KFD_m}{\pi D_w^3} = \frac{8KFC}{\pi D_w^2}$$

$$\text{The Wahl factor, } K = \frac{4C-1}{4C-4} + \frac{0.615}{C}$$

$$\text{Deflection: } \theta = \frac{TL}{GJ}$$

The linear deflection,

$$f = \frac{8FD_m^3 N_a}{GD_w^4} = \frac{8FC^3 N_a}{GD_w}$$

$$\text{Buckling } \frac{L_f}{D_m} = 8.0$$

Extension springs

$$\text{Bending stress } \sigma_A = \frac{16D_m F_o K_1}{\pi D_w^3} + \frac{4F_o}{\pi D_w^2}$$

$$K_1 = \frac{4C_1^2 - C_1 - 1}{4C_1(C_1 - 1)}$$

$$C_1 = 2R_1/D_w$$

Torsion stress

$$\sigma_A = \frac{8D_m F_o K_2}{\pi D_w^3}$$

$$K_2 = \frac{4C_2 - 1}{4C_2 - 4}$$

$$C_2 = 2R_2/D_w$$

Helical Torsion Springs

$$D_m = \frac{D_{m1} N_a}{(N_a + \theta)}$$

$$L = D_w(N_a + 1 + \theta)$$

Stress

$$\sigma = \frac{McK_b}{I} = \frac{MK_b}{Z} = \frac{32MK_b}{\pi D_w^3}$$

$$K_b = \frac{4C^2 - C - 1}{4C(C - 1)}$$

Deflection

$$\theta = \frac{10.2MD_m N_a}{ED_w^4}$$

$$k_\theta = \frac{ED_w^4}{10.2D_m N_a}$$

Number of coils

$$N_e = \frac{(L_1 + L_2)}{3\pi D_m}$$

$$N_a = N_b + N_e$$

***** DESIGN OF JOINTS AND FASTENERS *****

Welded Joints

Stresses

$$\text{Direct tension or compression: } f = P/A_w$$

$$\text{Direct vertical shear: } f = V/A_w$$

$$\text{Bending: } f = M/Z_w$$

$$\text{Twisting: } f = Tc/J_w$$

Fastener

$$\text{Tightening Torque: } T = KDP$$

Externally Applied Force on a Bolted Joint

$$F_b = P + \frac{k_b}{k_b + k_c} F_e$$

$$F_c = P - \frac{k_c}{k_b + k_c} F_e$$

***** DESIGN OF POWER SCREWS *****

Power Screws

The tensile stress area, A_t :

$$A_t = \frac{\pi}{4} \left[\frac{D_r + D_p}{2} \right]^2$$

Torque and Efficiency

$$T_u = \frac{FD_p}{2} \left[\frac{L + \pi f D_p}{\pi D_p - f L} \right]$$

$$T_u = \frac{FD_p}{2} \left[\frac{\tan \lambda + f}{1 - f \tan \lambda} \right]$$

$$T_u = \frac{FD_p}{2} \left[\frac{\cos \phi \tan \lambda + f}{\cos \phi - f \tan \lambda} \right]$$

$$\tan \lambda = \frac{L}{\pi D_p}$$

$$T_d = \frac{FD_p}{2} \left[\frac{\pi f D_p - L}{\pi D_p + f L} \right]$$

$$T_d = \frac{FD_p}{2} \left[\frac{f - \tan \lambda}{1 + f \tan \lambda} \right]$$

$$T_d = \frac{FD_p}{2} \left[\frac{f - \cos \phi \tan \lambda}{\cos \phi + f \tan \lambda} \right]$$

$$e = \frac{T'}{T_u} = \frac{FL}{2\pi T_u}$$

Ball Screws

The load/life relationship

$$\frac{L_2}{L_1} = \left(\frac{P_1}{P_2} \right)^3$$

Torque and Efficiency

$$e = \frac{T'}{T_u} = \frac{FL}{2\pi T_u}$$

$$T_b = 0.43FL$$

DESIGN OF BRAKES AND CLUTCHES

Torque capacity

$$T = C PK/n$$

$$T = \frac{Wk^2(\Delta n)}{93.68t} N.m$$

The term WK^2

$$WK^2 = 122000 L \left(R_1^4 - R_2^4 \right)$$

$$Wk_e^2 = Wk^2 \left(n/n_c \right)^2$$

$$Wk_e^2 = W \left(\frac{V}{2\pi n} \right)^2$$

Energy Absorption

$$E = 5.6 \times 10^{-4} WK^2 n^2$$

Plate-Type Clutch

$$T_f = fNR_m$$

$$P_f = \frac{T_f n}{7124} hp$$

$$WR = \frac{P_f}{A}$$

$WR = 62 \text{hp/m}^2$ for frequent applications,
 $WR = 155 \text{hp/m}^2$ for average service
 $WR = 620 \text{hp/m}^2$ for infrequently applications

Cone Clutch Brake

$$T_f = fNR_m = \frac{fR_m F_a}{\sin \alpha + f \cos \alpha}$$

Drum Brake

$$F_f = WL/(a/f - b)$$

$$T_f = \frac{1}{2} F_f D_d$$

Long Shoe Drum Brakes

$$T_f = r^2 fwp_{\max} (\cos \theta_1 - \cos \theta_2)$$

$$W = (M_N + M_f)/L$$

$$M_N = 0.25 p_{\max} wrC \begin{bmatrix} 2(\theta_1 - \theta_2) \\ -\sin 2\theta_2 + \sin 2\theta_1 \end{bmatrix}$$

$$M_f = fp_{\max} wr \begin{bmatrix} r(\cos \theta_1 - \cos \theta_2) \\ + 0.25C(\cos 2\theta_2 - \cos 2\theta_1) \end{bmatrix}$$

$$P_f = \frac{T_f n}{7124} hp$$

$$A = L_s w = 2wr \sin \left[\frac{(\theta_2 - \theta_1)}{2} \right]$$

$$WR = \frac{P_f}{A}$$

Band Brakes

$$T_f = (P_1 - P_2)r$$

$$P_2 = P_1 / e^{f\theta}$$

$$P_1, P_1 = P_{\max} rw$$

$$W = P_2 a/L$$

DESIGN OF FLEXIBLE DRIVES

V-Belt Drive

The belt speed, V_b

$$V_b = R_1 \omega_1 = R_2 \omega_2$$

$$V_b = \frac{1}{2} D_1 \omega_1 = \frac{1}{2} D_2 \omega_2$$

$$\omega_1/\omega_2 = D_2/D_1$$

Pitch length, L , center distance, C relationship

$$L = \left[\begin{array}{l} 2C + 1.57(D_2 + D_1) \\ +(D_2 - D_1)^2 / 4C \end{array} \right]$$

$$C = \left[B + \sqrt{B^2 - 32(D_2 - D_1)^2} \right] / 16$$

$$B = 4L - 6.28(D_2 + D_1)$$

Angle of contact

$$\theta_1 = 180^\circ - 2 \sin^{-1} [(D_2 - D_1)/2C]$$

$$\theta_2 = 180^\circ + 2 \sin^{-1} [(D_2 - D_1)/2C]$$

Chain Drives

Strand factors:

Two strands: Factor = 1.7

Three strands: Factor = 2.5

Four strands: Factor = 3.3

The chain length

$$L = \left[\begin{array}{l} 2C + \frac{1}{2}(N_2 + N_1) \\ +(N_2 - N_1)^2 / 4\pi^2 C \end{array} \right]$$

The center distance

$$C = \frac{1}{4} \left[\begin{array}{l} L - \frac{1}{2}(N_2 + N_1) + \\ \sqrt{[L - \frac{1}{2}(N_2 + N_1)]^2} \\ - \frac{8}{4\pi^2} (N_2 - N_1)^2 \end{array} \right]$$

DESIGN OF GEARS

Spur Gear

Pitches

$$p = \pi D_p / N_p = \pi D_G / N_G$$

$$P_d = N/D = N_G/D_G = N_p/D_p$$

$$m = D_G / N_G = D_p / N_p$$

$$m = 25.4/P_d$$

Gear Features

$$c = b - a$$

$$D_o = (N + 2)/P_d \text{ or } D_o = m(N + 2)$$

$$D_R = D - 2b$$

$$h_t = a + b$$

$$h_k = a + a = 2a$$

$$h_t = h_k + c$$

$$t = p/2 = \pi/p_d$$

Center Distance (C)

$$C = \frac{1}{2}(D_G + D_P) \text{ or } C = \frac{1}{2P_d}(N_G + N_P)$$

$$\text{or } C = \frac{m}{2}(N_G + N_P)$$

Velocity Ratio

$$VR = \frac{\omega_p}{\omega_G} = \frac{n_p}{n_G} = \frac{R_G}{R_p} = \frac{D_G}{D_p} = \frac{N_G}{N_p}$$

$$v_t = \pi D_p n_p / 60 = \pi D_G n_G / 60$$

Loads on Gear

$$W_t = 746 P / v_t$$

$$W_n = W_t / \cos \phi$$

$$W_r = W_t \tan \phi$$

Stresses in Gear Teeth

$$\sigma_t = \left(\frac{W_t P_d}{FJ} \right) \left(\frac{K_a K_s K_m K_B}{K_v} \right)$$

$$\sigma_c = C_p \sqrt{(C_a C_s C_m / C_v)(W_t / FD_p I)}$$

Helical Gear

Pitches

$$p = \pi N / D$$

$$p_n = p \cos \psi$$

$$P_d = N / D$$

$$P_{nd} = P_d / \cos \psi$$

$$P_x = p / \tan \psi = \pi / (P_d \tan \psi)$$

Loads on Gear

$$W_x = W_t \tan \psi$$

$$\tan \phi_n = \tan \phi_t \cos \psi$$

$$W_r = W_t \tan \phi_t$$

$$W_n = W_t / \cos \phi_n \cos \psi$$

Bevel Gear

Pitches

$$\gamma = \tan^{-1}(N_p / N_G)$$

$$\Gamma = \tan^{-1}(N_G / N_p)$$

$$P_d = N_p / d = N_G / D$$

Geometrical Features

$$\text{Whole depth} \quad h_t = 2.188/P_d + 0.002$$

$$\text{Working depth} \quad h_k = 2.000/P_d$$

$$\text{Clearance} \quad c = 0.188/P_d + 0.002$$

$$\text{Addendum: Gear} \quad a_G = \frac{0.54}{P_d} + \frac{0.460}{P_d(N_G/N_p)^2}$$

$$\text{Addendum: Pinion} \quad a_P = h_k - a_G$$

$$\text{Outside diameter: Gear} \quad D_o = D + 2a_G \cos \Gamma$$

$$\text{Outside diameter: Pinion} \quad d_o = d + 2a_P \cos \gamma$$

$$\text{Outer cone distance} \quad A_o = D/(2 \sin \Gamma) = d/(2 \sin \gamma)$$

$$\text{Preferred face width} \quad F = A_o/3 \text{ or less (maximum } F = 10/P_d)$$

Load on Gear

$$W_{tP} = T / r_m$$

$$r_m = d/2 - (F/2) \sin \gamma$$

$$W_{rP} = W_{tP} \tan \phi \cos \gamma$$

$$W_{xP} = W_{tP} \tan \phi \sin \gamma$$

$$W_t = 14248 P / d n_p$$

Stresses

$$\sigma_t = \left(\frac{W_t P_d}{FJ} \right) \left(\frac{K_a K_s K_m}{K_v} \right)$$

Worm Gearing

Pitches

$$p = \pi D_G / N_G$$

$$P_d = N_G / D_G$$

$$P_d p = \pi$$

Lead

$$L = N_w P_x$$

$$\tan \lambda = L / \pi D_w$$

$$\tan \phi_n = \tan \phi_t \cos \lambda$$

Loads on Gear

$$T_o = 7124 P_o / n_G$$

$$T_o = W_{tG} r_G = W_{tG} (D_G / 2)$$

$$W_{tG} = 2T_o / D_G$$

$$W_{xG} = W_{tG} \left(\frac{\cos \phi_n \sin \lambda + \mu \cos \lambda}{\cos \phi_n \cos \lambda - \mu \sin \lambda} \right)$$

$$W_{rG} = \frac{W_{tG} \sin \phi_n}{\cos \phi_n \cos \lambda - \mu \sin \lambda}$$

$$W_f = \frac{\mu W_{tG}}{\cos \phi_n \cos \lambda}$$

Efficiency

$$P_i = P_o + P_L$$

$$P_L = v_s W_f$$

$$\eta = P_o / P_i$$

Stress in Worm Gear Teeth

$$\sigma = W_d / (y F p_n)$$

$$W_d = W_{tG} / K_v$$

$$K_v = 6.1 / (6.1 + v_{tG})$$

$$W_{tR} = C_s D_G^{0.8} F_e C_m C_v / 75$$

FAILURE THEORIES

Table 1: Recommended Factor of Safety

Stress Type	Material Condition	Environmental Condition	Recommended Design factor of safety
Very Certain	Ductile and Reliable Data	Well Controlled	1.25 to 1.5
Readily Determined	Ductile and Well Known	Reasonably Constant	1.5 to 2.0
Fairly Certain	Ductile and Common	Ordinary	2.0 to 2.5
Could Vary	Less Tried Ductile or Brittle	Average	2.5 to 3.0
Could Vary	Less Reliable Data	Average	3.0 to 4.0
Uncertain	Common	Uncertain	3.5 to 5.0

Table 2: Typical Properties of Gray Cast Iron

ASTM Number	Ultimate Tensile Strength S_{ut} , MPa	Ultimate Compressive Strength S_{uc} , MPa	Torsional Shear Strength, S_{us} , MPa	Endurance Limit S_e , MPa	Brinell Hardness, H_B
20	152	572	179	69	156
25	179	669	220	79	174
30	214	752	276	97	210
35	252	855	334	110	212
40	293	965	393	128	235
50	362	1130	503	148	262

Table 3: Average Mechanical Properties of Selected Ductile (Nodular) Iron

Grade*	Ultimate Tensile Strength S_{ut} , MPa	Ultimate Compressive Strength S_{uc} , MPa	Tensile Yield Strength S_{yt} , MPa	Brinell Hardness, H_B	Elongation (%) 50 mm
60-40-18	461	359	329	167	15.0
65-45-12	464	362	332	167	15.0
80-55-06	559	386	362	192	11.2
120-90-02	974	920	864	331	1.5

Table 4: Mechanical Properties of Selected Steels

AISI No.	Processing	Ultimate Tensile Strength S_{ut} , MPa	Tensile Yield Strength S_{yt} , MPa	Brinell Hardness, H_B	Elongation (%)
1015	HR	340	190	101	28
	CD	390	320	111	18
	Annealed	386	284	111	37
1020	HR	380	210	111	25
	CD	470	390	131	15
	Annealed	395	296	111	36
1040	HR	520	290	149	10
	CD	590	490	170	12
	Normalized	590	374	170	28
	Annealed	519	353	149	30
1045	HR	570	310	163	16
	CD	630	530	179	12
1050	HR	620	340	179	15
	CD	690	580	197	10
	Normalized	748	427	217	20
	Annealed	636	365	187	24
	QT (425 C)	1090	793	444	13
1060	HR	680	370	201	12
	Normalized	776	421	229	18
	Annealed	626	372	179	22
	QT (425 C)	1080	765	311	14
1095	HR	830	460	248	10
	Normalized	1010	500	293	9
	Annealed	658	380	192	13
	QT (425 C)	1210	772	363	12
1118	HR	521	317	149	32
	Normalized	478	319	143	34
	Annealed	450	285	131	35
3140	Normalized	892	600	262	20
	Annealed	690	423	197	25
4130	Normalized	670	436	197	25
	Annealed	560	361	156	28
	QT (425 C)	1280	1190	380	13

Table 5: Guide to Selection of Plain Carbon Steels

Carbon (%)	Typical Uses
0.05 –	Stampings, rivets, wire, cold drawn parts
0.10	
0.10 –	Structural shapes, machine parts, carburized parts
0.20	
0.20 –	Gears, shafts, levers, cold-forged parts, welded tubing, carburized parts
0.30	
0.30 –	Shafts, gears, connecting rods, crane hooks
0.40	
0.40 –	Gears, shafts, screws, forgings
0.50	
0.50 –	Drawn-spring wire, lock washers, locomotive tires
0.70	
0.70 –	Plowshares, shovels, leaf springs, hand tools
0.90	
0.90 –	Springs, knives, drills, taps, milling cutters
1.20	
1.20 –	Files, knives, razors, saws, wire-drawing dies.
1.40	

Table 6: Mechanical Properties of Selected Non-Ferrous Materials

Material	Processing	Ultimate Tensile Strength S_{ut} , MPa	Tensile Yield Strength S_{yt} , MPa
Aluminum Alloys	1100-0	83	31
	2024-T4	448	296
	7075-0	234	99
	7075-T6	593	538
Magnesium Alloys	HK31XA-0	176	131
	HK31XA-H24	250	214
Copper Alloys	90-10 Brass A	251	58
	80-20 Brass A	247	50
	70-30 Brass A	303	72

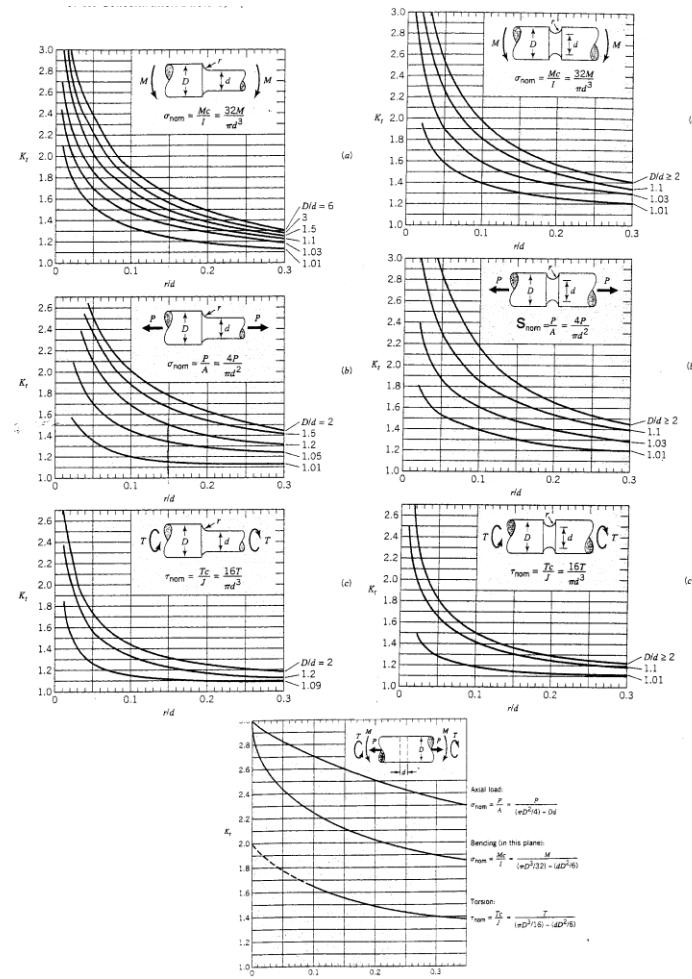
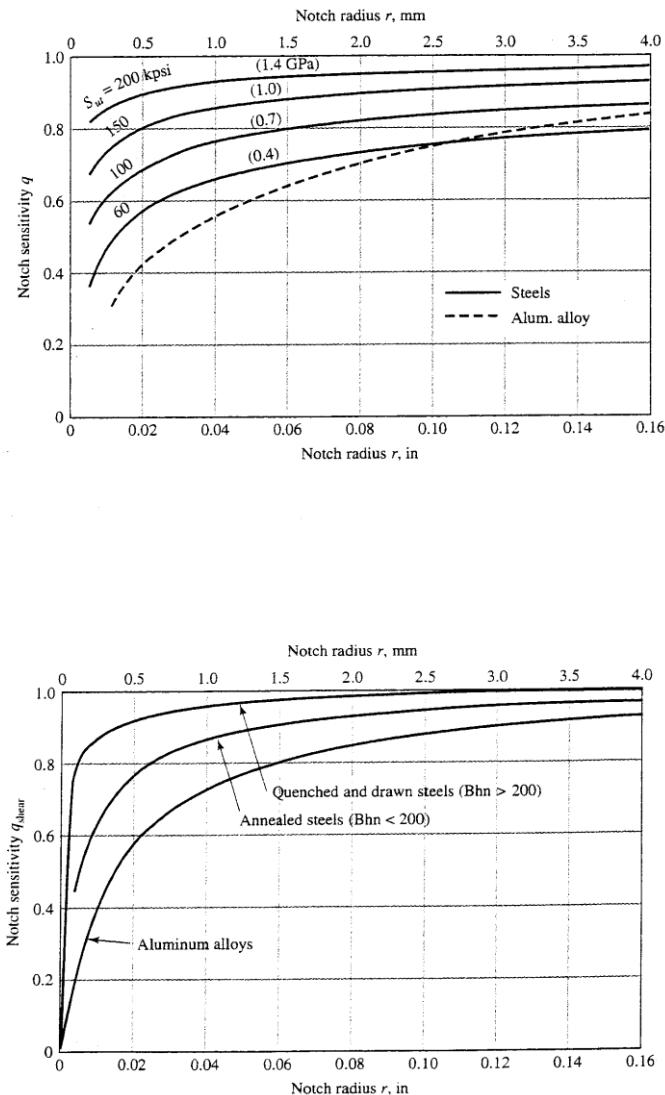


Figure 1: Stress Concentration Factors



KEYS AND KEYWAYS

Table 1: KEY SIZE VERSUS SHAFT DIAMETER

Nominal Shaft Diameter	Nominal Key Size			
	Over	To (Incl.)	Width, W	Height, H
			Square	Rectangular
$\frac{3}{16}$	$\frac{7}{16}$	$\frac{3}{32}$	$\frac{3}{32}$	
$\frac{7}{16}$	$\frac{9}{16}$	$\frac{1}{8}$	$\frac{1}{8}$	$\frac{3}{32}$
$\frac{9}{16}$	$\frac{7}{8}$	$\frac{3}{16}$	$\frac{3}{16}$	$\frac{1}{8}$
$\frac{7}{8}$	$1\frac{1}{4}$	$\frac{1}{4}$	$\frac{1}{4}$	$\frac{3}{16}$
$1\frac{1}{4}$	$1\frac{3}{8}$	$\frac{5}{16}$	$\frac{5}{16}$	$\frac{1}{4}$
$1\frac{3}{8}$	$1\frac{3}{4}$	$\frac{3}{8}$	$\frac{3}{8}$	$\frac{1}{4}$
$1\frac{3}{4}$	$2\frac{1}{4}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{3}{8}$
$2\frac{1}{4}$	$2\frac{3}{4}$	$\frac{5}{16}$	$\frac{5}{16}$	$\frac{3}{16}$
$2\frac{3}{4}$	$3\frac{1}{4}$	$\frac{3}{4}$	$\frac{3}{4}$	$\frac{1}{2}$
$3\frac{1}{4}$	$3\frac{3}{4}$	$\frac{7}{16}$	$\frac{7}{16}$	$\frac{3}{8}$
$3\frac{3}{4}$	$4\frac{1}{2}$	1	1	$\frac{3}{4}$
$4\frac{1}{2}$	$5\frac{1}{2}$	$1\frac{1}{4}$	$1\frac{1}{4}$	$\frac{3}{8}$
$5\frac{1}{2}$	$6\frac{1}{2}$	$1\frac{1}{2}$	$1\frac{1}{2}$	1
$6\frac{1}{2}$	$7\frac{1}{2}$	$1\frac{3}{4}$	$1\frac{3}{4}$	$1\frac{1}{2}$
$7\frac{1}{2}$	9	2	2	$1\frac{1}{2}$
9	11	$2\frac{1}{2}$	$2\frac{1}{2}$	$1\frac{3}{4}$
11	13	3	3	2
13	15	$3\frac{1}{2}$	$3\frac{1}{2}$	$2\frac{1}{2}$
15	18	4	4	3
18	22	5	5	$3\frac{1}{2}$
22	26	6	6	4
26	30	7	7	5

Note: Values in nonshaded areas preferred. Dimensions are in inches.

Source: ANSI Standard B17.1—1967, *Keys and Keyseats* (American Society of Mechanical Engineers, New York).

Table 2: WOODRUFF KEY DIMENSIONS

Key Number	Nominal Key Size, W × B	Actual Length, F	Height of Key, C	Shaft Keyseat Depth	Hub Keyseat Depth
202	1/16 × 1/4	0.248	0.104	0.072 8	0.037 2
204	1/16 × 1/2	0.491	0.200	0.166 8	0.037 2
406	1/8 × 3/4	0.740	0.310	0.245 5	0.068 5
608	3/16 × 1	0.992	0.435	0.339 3	0.099 7
810	1/4 × 1 1/4	1.240	0.544	0.417 0	0.131 0
1210	3/8 × 1 1/4	1.240	0.544	0.354 5	0.193 5
1628	1/2 × 3 1/2	2.880	0.935	0.683 0	0.256 0
2428	3/4 × 3 1/2	2.880	0.935	0.558 0	0.381 0

Note: All dimensions given in inches.

Source: ANSI Standard B17.2—1967, *Woodruff Keys and Keyseats* (American Society of Mechanical Engineers, New York).

BEARINGS

TABLE 1: PERFORMANCE PARAMETERS FOR BEARING MATERIALS IN BOUNDARY LUBRICATION

Material	pV psi·fpm	Wear Factor, K (10 ⁻¹⁰ in ³ ·min/ ft·lb·h)	Coefficient of Friction ^a
Copper-iron	75 000	2 625	—
Lead-bronze	60 000	2 100	—
Bronze	50 000	1 750	—
Aluminum	50 000	1 750	—
PPS filled with PTFE and glass	30 000	1 050	110
PTFE fabric	25 000	875	—
PTFE-bronze filled	21 000	735	5
PA filled with PTFE and glass	20 000	700	16
PTFE-glass filled	18 000	630	7
PTFE-PPS filled	15 000	525	1
Carbon-graphite	15 000	525	—
Nylon-filled with glass and PTFE	3 000	105	16

TABLE 2: BEARING MATERIALS PROPERTIES

	Material			
	Silicon Nitride	52100 Steel	440C Stainless Steel	M50 Steel
Room temperature hardness, HRC	78	62	60	64
Room temperature elastic modulus, 10 ⁶ psi	45	30	29	28
Maximum operating temperature	1 200°C 2 200°F	180°C 360°F	260°C 500°F	320°C 600°F
Density, g/cc	3.2	7.8	7.8	7.6

TABLE 3 COMPARISON OF BEARING TYPES

Bearing Type	Radial Load Capacity	Thrust Load Capacity	Misalignment Capability
Single-row, deep-groove ball	Good	Fair	Fair
Double-row, deep-groove ball	Excellent	Good	Fair
Angular contact	Good	Excellent	Poor
Cylindrical roller	Excellent	Poor	Fair
Needle	Excellent	Poor	Poor
Spherical roller	Excellent	Fair/good	Excellent
Tapered roller	Excellent	Excellent	Poor

TABLE AA9: RADIAL AND THRUST FACTOR FOR SINGLE-ROW DEEP-GROOVE BALL BEARING

e	T/C _o	Y	e	T/C _o	Y
0.19	0.014	2.30	0.34	0.170	1.31
0.22	0.028	1.99	0.38	0.280	1.15
0.26	0.056	1.71	0.42	0.420	1.04
0.28	0.084	1.55	0.44	0.560	1.00
0.30	0.110	1.45			

Note: X = 0.56 for all values of Y. *Also T = when same radial load*

TABLE 4: BEARING SELECTION DATA FOR SINGLE-ROW, DEEP-GROOVE CONRAD-TYPE BALL BEARING

Table 15-2 Bearing Selection Data for Single-row, Deep-groove, Conrad-type Ball Bearings

Bearing Number	Series 6200													
	Nominal Bearing Dimensions											Preferred Shoulder Diameter		
	d		D		B		r^*		Shaft	Housing	Bearing Weight	Basic Static Load Rating C_o	Basic Dynamic Load Rating C	
	mm	in	mm	in	mm	in	mm	in	in	in				lb
6200	10	0.3937	30	1.1811	9	0.3543	0.024	0.300	0.984	0.07	520	885		
6201	12	0.4724	32	1.2598	10	0.3937	0.024	0.378	1.063	0.08	675	1180		
6202	15	0.5905	35	1.3780	11	0.4331	0.024	0.703	1.181	0.10	790	1320		
6203	17	0.6693	40	1.5748	12	0.4724	0.024	0.787	1.380	0.14	1010	1660		
6204	20	0.7874	47	1.8504	14	0.5512	0.039	0.969	1.614	0.23	1400	2210		
6205	25	1.0000	52	2.0272	15	0.5905	0.039	1.172	1.811	0.29	1610	2430		
6206	30	1.1811	62	2.4409	16	0.6299	0.039	1.466	2.095	0.44	2070	3350		
6207	35	1.3780	72	2.8346	17	0.6693	0.039	1.614	2.559	0.64	3150	4450		
6208	40	1.5748	80	3.1496	18	0.7077	0.039	1.811	2.874	0.82	3650	5050		
6209	45	1.7717	85	3.3465	19	0.7480	0.039	2.008	3.071	0.89	4150	5650		
6210	50	1.9685	90	3.5433	20	0.7874	0.039	2.205	3.268	1.02	4650	6050		
6211	55	2.1654	100	3.9370	21	0.8258	0.039	2.441	3.602	1.36	5850	7500		
6212	60	2.3622	110	4.3307	22	0.8661	0.059	2.717	3.996	1.73	7250	9050		
6213	65	2.5591	120	4.7244	23	0.9055	0.059	2.913	4.390	2.18	8000	9900		
6214	70	2.7555	125	4.9213	24	0.9449	0.059	3.110	4.587	2.31	8800	10800		
6215	75	2.9528	130	5.1181	25	0.9843	0.059	3.307	4.783	2.64	9700	11400		
6216	80	3.1496	140	5.5118	26	1.0236	0.079	3.504	5.118	3.09	10500	12600		
6217	85	3.3465	150	5.9055	28	1.1024	0.079	3.740	5.512	3.97	12300	14600		
6218	90	3.5433	160	6.2992	30	1.1811	0.079	3.937	5.906	4.74	14200	16600		
6219	95	3.7402	170	6.6929	32	1.2598	0.079	4.213	6.220	5.73	16300	18800		
6220	100	3.9370	180	7.0866	34	1.3386	0.079	4.409	6.614	6.94	18600	21100		
6221	105	4.1339	190	7.4803	36	1.4173	0.079	4.606	7.008	8.15	20900	23000		
6222	110	4.3307	200	7.8740	38	1.4961	0.079	4.803	7.402	9.39	23400	24900		
6224	120	4.7244	215	8.4646	40	1.5748	0.079	5.197	7.992	11.4	26200	26900		

Bearing Number	Series 6200													
	Nominal Bearing Dimensions											Preferred Shoulder Diameter		
	d		D		B		r^*		Shaft	Housing	Bearing Weight	Basic Static Load Rating C_o	Basic Dynamic Load Rating C	
	mm	in	mm	in	mm	in	mm	in	in	in				lb
6226	130	5.1181	230	9.0551	40	1.5748	0.098	5.669	8.504	12.7	29100	28700		
6228	140	5.5118	250	9.8425	42	1.6535	0.098	6.063	9.291	19.6	29300	28700		
6230	150	5.9055	270	10.6299	45	1.7717	0.098	6.457	10.079	25.3	32500	30000		
6232	160	6.2992	290	11.4173	48	1.8898	0.098	6.850	10.886	32.0	35500	32000		
6234	170	6.6929	310	12.2047	52	2.0472	0.118	7.362	11.535	38.5	43000	36500		
6236	180	7.0866	320	12.5984	52	2.0472	0.118	7.558	11.929	41.0	46500	39000		
6238	190	7.4803	340	13.3858	55	2.1654	0.118	8.150	12.717	50.5	54500	44000		
6240	200	7.8740	360	14.1732	58	2.2835	0.118	8.543	13.504	61.5	60000	46500		

Bearing Number	Series 6300													
	Nominal Bearing Dimensions											Preferred Shoulder Diameter		
	d		D		B		r^*		Shaft	Housing	Bearing Weight	Basic Static Load Rating C_o	Basic Dynamic Load Rating C	
	mm	in	mm	in	mm	in	mm	in	in	in				lb
6300	10	0.3937	35	1.3780	11	0.4331	0.024	0.563	1.181	0.12	805	1400		
6301	12	0.4724	37	1.4567	12	0.4724	0.039	0.656	1.220	0.13	990	1680		
6302	15	0.5906	42	1.6535	13	0.5118	0.039	0.781	1.417	0.18	1200	1980		
6303	17	0.6693	47	1.8504	14	0.5512	0.039	0.875	1.614	0.25	1460	2360		
6304	20	0.7874	52	2.0472	15	0.5906	0.039	1.016	1.772	0.32	1730	2760		
6305	25	0.9843	62	2.4409	17	0.6693	0.039	1.220	2.165	0.52	2370	3550		
6306	30	1.1811	72	2.8346	19	0.7480	0.039	1.469	2.559	0.76	3150	4600		
6307	35	1.3780	80	3.1496	21	0.8268	0.039	1.688	2.795	1.01	4050	5800		
6308	40	1.5748	90	3.5433	23	0.9055	0.059	1.929	3.189	1.40	5050	7050		
6309	45	1.7717	100	3.9370	25	0.9843	0.059	2.126	3.583	1.84	6800	9150		
6310	50	1.9685	110	4.3307	27	1.0630	0.079	2.362	3.937	2.42	8100	10700		
6311	55	2.1654	120	4.7244	29	1.1417	0.079	2.559	4.331	2.98	9450	12300		
6312	60	2.3622	130	5.1181	31	1.2205	0.079	2.835	4.646	3.75	11000	14100		
6313	65	2.5591	140	5.5118	33	1.2992	0.079	3.031	5.039	4.63	12600	16000		
6314	70	2.7559	150	5.9055	35	1.3780	0.079	3.228	5.433	5.51	14400	18000		
6315	75	2.9528	160	6.2992	37	1.4567	0.079	3.425	5.827	6.61	16300	19600		



Bearing Number	Nominal Bearing Dimensions										Preferred Shoulder Diameter	Bearing Weight	Basic Static Load Rating C_o	Basic Dynamic Load Rating C
	d		D		B		r^*		Shaft	Housing				
	mm	in	mm	in	mm	in	mm	in	in	in	mm	in	lb	lb
6316	80	3.1496	170	6.6929	39	1.5354	0.079	3.622	6.220	7.93	18300	21300		
6317	85	3.3465	180	7.0866	41	1.6142	0.098	3.898	6.535	9.37	20400	22900		
6318	90	3.5433	190	7.4803	43	1.6929	0.098	4.094	6.929	10.8	22500	24700		
6319	95	3.7402	200	7.8740	45	1.7717	0.098	4.291	7.323	12.5	24900	26400		
6320	100	3.9370	215	8.4646	47	1.8504	0.098	4.488	7.913	15.3	29800	30000		
6321	105	4.1339	225	8.8583	49	1.9291	0.098	4.685	8.307	17.9	32500	31700		
6322	110	4.3307	240	9.4488	50	1.9685	0.098	4.882	8.898	21.0	38000	35500		
6324	120	4.7244	260	10.2362	55	2.1654	0.098	5.276	9.685	27.6				

TABLE 7: TAPERED ROLLER BEARING DATA

Bore	Outside Diameter	Width	a	Thrust Factor, Y	Basic Dynamic Load Rating, C
1.000 0	2.500 0	0.812 5	0.583	1.71	8 370
1.500 0	3.000 0	0.937 5	0.690	1.98	12 800
1.750 0	4.000 0	1.250 0	0.970	1.50	21 400
2.000 0	4.375 0	1.500 0	0.975	2.02	26 200
2.500 0	5.000 0	1.437 5	1.100	1.65	29 300
3.000 0	6.000 0	1.625 0	1.320	1.47	39 700
3.500 0	6.375 0	1.875 0	1.430	1.76	47 700

Note: Dimensions in inches. Load C in pounds for an L_{10} life of 1 million rev.

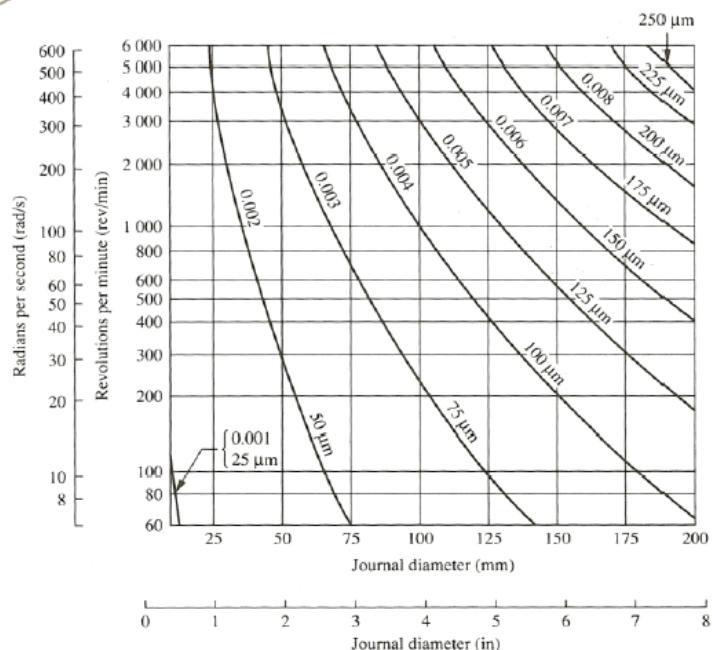


FIGURE 1: MINIMUM RECOMMENDED DIAMETRAL CLEARANCE FOR BEARINGS CONSIDERING JOURNAL DIAMETER AND ROTATIONAL SPEED

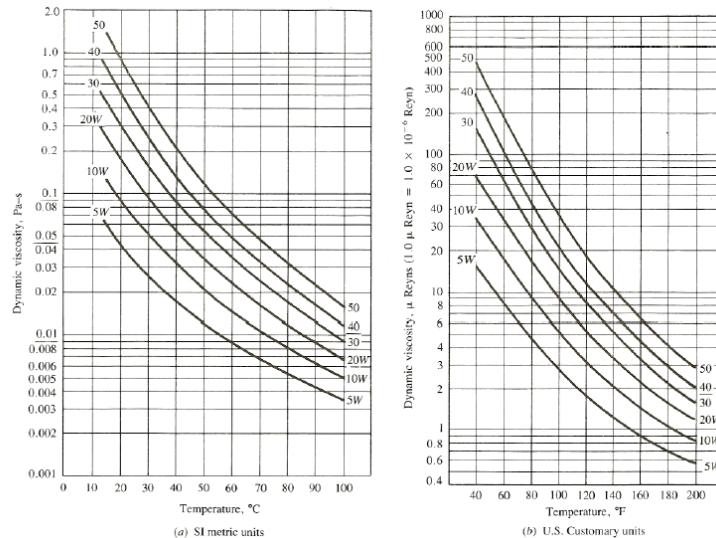


FIGURE 2: VISCOSITY VERSUS TEMPERATURE FOR SAE OILS

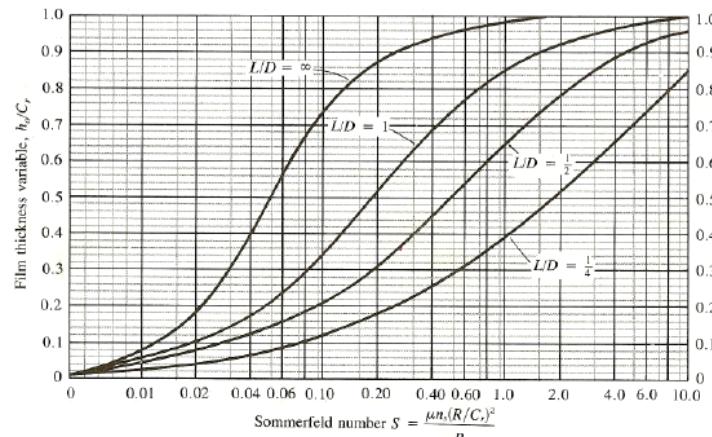


FIGURE 3: FILM THICKNESS VARIABLE, h_o/C_r , VERSUS SOMMERFELD NUMBER, S

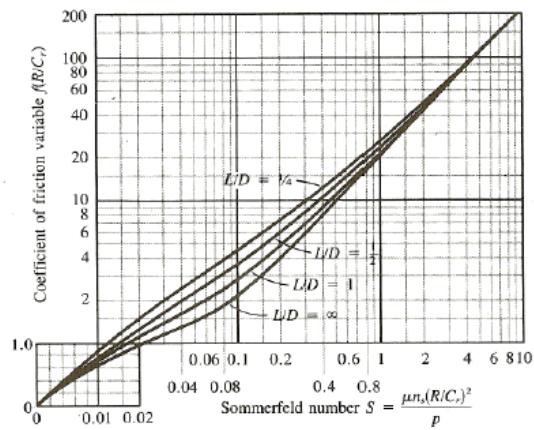


FIGURE 4: COEFFICIENT OF FRICTION VARIABLE, $F(R/C)$, VERSUS SOMMERFELD NUMBER, S

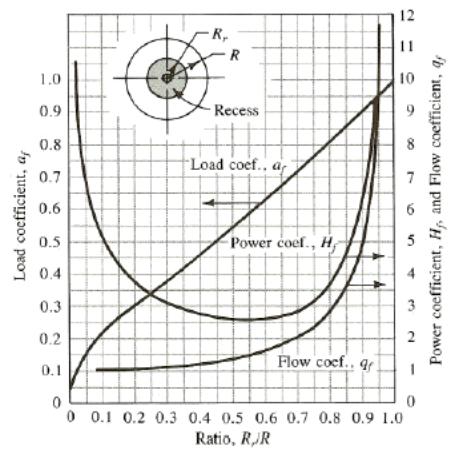


FIGURE 5: DIMENSIONLESS PERFORMANCE COEFFICIENTS FOR CIRCULAR PAD HYDROSTATIC BEARING

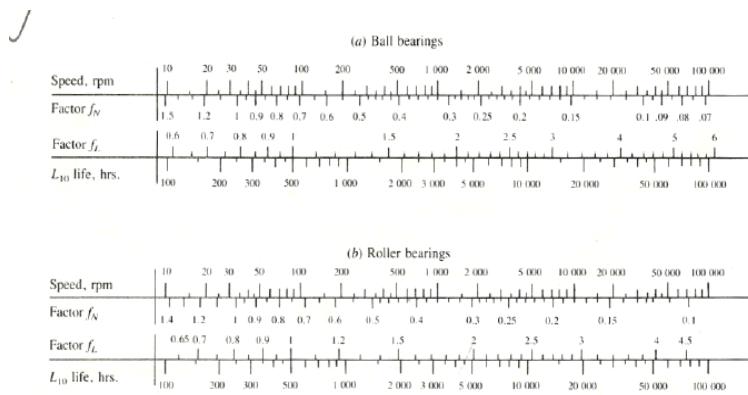


FIGURE 6: LIFE AND SPEED FACTORS FOR BALL AND ROLLER BEARINGS

APPENDIX B: DESIGN OF SPRINGS

APPENDIX-TAB AB1: TYPES OF BEARING

<i>Uses</i>	<i>Types of Springs</i>
Push	Helical compression spring
	Belleville spring
	Torsion spring: force acting at the end of the torque arm
	Flat spring, such as a cantilever or leaf spring
Pull	Helical extension spring
	Torsion spring: force acting at the end of the torque arm
	Flat spring, such as a cantilever or leaf spring
	Drawbar spring (special case of the compression spring)
	Constant-force spring
	Garter spring, elastomeric band, spring clamp
	Torsion spring, power spring

<i>Gage No.</i>	<i>U.S. Steel Wire Gage (in)^a</i>	<i>Music Wire Gage (in)^b</i>	<i>Brown & Sharpe Gage (in)^c</i>	<i>Preferred Metric Diameter (mm)^d</i>
7/0	0.490 0	—	—	13.0
6/0	0.461 5	0.004	0.580 0	12.0
5/0	0.430 5	0.005	0.516 5	11.0
4/0	0.393 8	0.006	0.460 0	10.0
3/0	0.362 5	0.007	0.409 6	9.0
2/0	0.331 0	0.008	0.364 8	8.5
0	0.306 5	0.009	0.324 9	8.0
1	0.283 0	0.010	0.289 3	7.0
2	0.262 5	0.011	0.257 6	6.5
3	0.243 7	0.012	0.229 4	6.0
4	0.225 3	0.013	0.204 3	5.5
5	0.207 0	0.014	0.181 9	5.0
6	0.192 0	0.016	0.162 0	4.8
7	0.177 0	0.018	0.144 3	4.5
8	0.162 0	0.020	0.128 5	4.0
9	0.148 3	0.022	0.114 4	3.8
10	0.135 0	0.024	0.101 9	3.5
11	0.120 5	0.026	0.090 7	3.0
12	0.105 5	0.029	0.080 8	2.8
13	0.091 5	0.031	0.072 0	2.5
14	0.080 0	0.033	0.064 1	2.0
15	0.072 0	0.035	0.057 1	1.8
16	0.062 5	0.037	0.050 8	1.6
17	0.054 0	0.039	0.045 3	1.4
18	0.047 5	0.041	0.040 3	1.2
19	0.041 0	0.043	0.035 9	1.0
20	0.034 8	0.045	0.032 0	0.90
21	0.031 7	0.047	0.028 5	0.80
22	0.028 6	0.049	0.025 3	0.70

APPENDIX-TAB AB2: WIRE GAGES AND DIAMETERS FOR SPRINGS

23	0.025 8	0.051	0.022 6	0.65
24	0.023 0	0.055	0.020 1	0.60 or 0.55
25	0.020 4	0.059	0.017 9	0.50 or 0.55
26	0.018 1	0.063	0.015 9	0.45
27	0.017 3	0.067	0.014 2	0.45
28	0.016 2	0.071	0.012 6	0.40
29	0.015 0	0.075	0.011 3	0.40
30	0.014 0	0.080	0.010 0	0.35
31	0.013 2	0.085	0.008 93	0.35
32	0.012 8	0.090	0.007 95	0.30 or 0.35
33	0.011 8	0.095	0.007 08	0.30
34	0.010 4	0.100	0.006 30	0.28
35	0.009 5	0.106	0.005 01	0.25
36	0.009 0	0.112	0.005 00	0.22
37	0.008 5	0.118	0.004 45	0.22
38	0.008 0	0.124	0.003 96	0.20
39	0.007 5	0.130	0.003 53	0.20
40	0.007 0	0.138	0.003 14	0.18

^aUse the U.S. Steel Wire Gage for steel wire, except music wire. This gage has also been called the *Washburn and Moen Gage* (W&M), the *American Steel Wire Co. Gage*, and the *Roebling Wire Gage*.

APPENDIX-TAB AB3 SPRING MATERIALS

<i>Material Type</i>	<i>ASTM No.</i>	<i>Relative Cost</i>	<i>Temperature Limits, °F</i>
<i>High-carbon steels:</i>			
Hard drawn	A227	1.0	
General-purpose steel with 0.60%–0.70% carbon; low cost			
Music wire	A228	2.6	
High-quality steel with 0.80%–0.95% carbon; very high strength; excellent finish; hard drawn; good fatigue performance; used mostly in smaller sizes up to 0.125 in			
Oil-tempered	A229	1.3	
General-purpose steel with 0.60%–0.70% carbon; used mostly in larger sizes up to 0.125 in; not good for shock or impact			
<i>Alloy steels:</i>			
Chromium-vanadium	A231	3.1	
Good strength, fatigue resistance, impact strength, high-temperature valve spring quality			
Chromium-silicon	A401	4.0	
Very high strength and good fatigue and shock resistance			
<i>Stainless steels:</i>			
Type 302	A313(302)	7.6	
Very good corrosion resistance and high-temperature performance; nearly nonmagnetic; cold drawn; types 304 and 316 also fall under this ASTM class and have improved workability but lower strength			
Type 17-7 PH	A313(631)	11.0	
Good high-temperature performance			
<i>Copper alloys:</i> All have good corrosion resistance and electrical conductivity			
Spring brass	B134	High	
Phosphor bronze	B159	8.0	
Beryllium copper	B197	27.0	
<i>Nickel-base alloys:</i> All are corrosion resistant, have good high- and low-temperature properties, are nonmagnetic or nearly nonmagnetic (trade names of the International Nickel Company)			
Monel	—	—	-100–425
K-Monel	—	—	-100–450
Inconel	—	—	Up to 700
Inconel-X	—	44.0	Up to 850

APPENDIX-TAB AB4 SPRING WIRE MODULUS OF ELASTICITY IN SHEAR (G) AND TENSION (E)

<i>Material And ASTM No.</i>	<i>Shear Modulus, G (psi)</i>	<i>Tension Modulus, E (GPa)</i>	<i>(psi)</i>	<i>(GPa)</i>
Hard drawn steel: A227	11.5×10^6	79.3	28.6×10^6	197
Music wire: A228	11.85×10^6	81.7	29.0×10^6	200
Oil-tempered: A229	11.2×10^6	77.2	28.5×10^6	196
Chromium-vanadium: A231	11.2×10^6	77.2	28.5×10^6	196
Chromium-silicon: A401	11.2×10^6	77.2	29.5×10^6	203
<i>Stainless steels: A313</i>				
Types 302, 304, 316	10.0×10^6	69.0	28.0×10^6	193
Type 17-7 PH	10.5×10^6	72.4	29.5×10^6	203
<i>Spring brass: B134</i>				
	5.0×10^6	34.5	15.0×10^6	103
<i>Phosphor bronze: B159</i>				
	6.0×10^6	41.4	15.0×10^6	103
<i>Beryllium copper: B197</i>				
	7.0×10^6	48.3	17.0×10^6	117
<i>Monel and K-Monel</i>				
	9.5×10^6	65.5	26.0×10^6	179
<i>Inconel and Inconel-X</i>				
	10.5×10^6	72.4	31.0×10^6	214

Note: Data are average values. Slight variation with wire size and treatment may occur.

APPENDIX-TAB AB5 ALLOWABLE STRESSES FOR BOLTS

<i>ASTM Grade</i>	<i>Allowable Shear Stress</i>	<i>Allowable Tensile Stress</i>
A307	10 ksi (69 MPa)	20 ksi (138 MPa)
A325 and A449	17.5 ksi (121 MPa)	44 ksi (302 MPa)
A490	22 ksi (152 MPa)	54 ksi (375 MPa)

<i>Base Metal ASTM Grade</i>	<i>Electrode</i>	<i>Allowable Shear Stress</i>
<i>Building Type Structures</i>		
A36, A441	E60	13 600 psi
A36, A441	E70	15 800 psi
<i>Bridge Type Structures</i>		
A36	E60	12 400 psi
A441, A242	E70	14 700 psi

<i>Steel</i>														
<i>Electrode Type</i>	<i>Typical Metals Joined (ASTM Grade)</i>			<i>Allowab Shear Str</i>										
E60	A36, A500				18 ksi (124 MPa)									
E70	A242, A441				21 ksi (145 MPa)									
E80	A572 Grade 65				24 ksi (165 MPa)									
E90	—				27 ksi (186 MPa)									
E100	—				30 ksi (207 MPa)									
E110	—				33 ksi (228 MPa)									
<i>Aluminum</i>														
<i>Filler Alloy</i>														
<i>1100</i>		<i>4043</i>		<i>5356</i>		<i>5556</i>								
<i>Allowable Shear Stress</i>														
<i>Metal Joined</i>	<i>Ksi</i>	<i>MPa</i>	<i>Ksi</i>	<i>MPa</i>	<i>Ksi</i>	<i>MPa</i>	<i>Ksi</i>							
1100	3.2	22	4.8	33	—	—	—							
3003	3.2	22	5.0	34	—	—	—							
6061	—	—	5.0	34	7.0	48	8.5							
6063	—	—	5.0	34	6.5	45	6.5							

APPENDIX-TAB AB5 CONTINUES

APPENDIX-TAB AB6 MINIMUM WELD SIZES FOR THICK PLATES

<i>Plate Thickness (in)</i>	<i>Minimum Leg Size for (in)</i>
$\leq \frac{1}{2}$	$\frac{3}{16}$
$> \frac{1}{2}-\frac{3}{4}$	$\frac{1}{4}$
$> \frac{3}{4}-1\frac{1}{2}$	$\frac{5}{16}$
$> 1\frac{1}{2}-2\frac{1}{4}$	$\frac{3}{8}$
$> 2\frac{1}{4}-6$	$\frac{1}{2}$
> 6	$\frac{5}{8}$

<i>Nominal Major Diameter (in)</i>	<i>Threads per in n</i>	<i>Pitch, p = 1/n (in)</i>	<i>Minimum Minor Diameter (in)</i>	<i>Minimum Pitch Diameter (in)</i>	<i>Tensile Stress Area (in²)</i>
$\frac{1}{4}$	16	0.0625	0.1618	0.2043	0.02632
$\frac{5}{16}$	14	0.0714	0.2140	0.2614	0.04438
$\frac{3}{8}$	12	0.0833	0.2632	0.3161	0.06589
$\frac{7}{16}$	12	0.0833	0.3253	0.3783	0.09720
$\frac{1}{2}$	10	0.1000	0.3594	0.4306	0.1225
$\frac{5}{8}$	8	0.1250	0.4570	0.5408	0.1955
$\frac{3}{4}$	6	0.1667	0.5371	0.6424	0.2732
$\frac{7}{8}$	6	0.1667	0.6615	0.7663	0.4003
1	5	0.2000	0.7509	0.8726	0.5175
$1\frac{1}{8}$	5	0.2000	0.8753	0.9967	0.6881
$1\frac{1}{4}$	5	0.2000	0.9998	1.1210	0.8831
$1\frac{3}{8}$	4	0.2500	1.0719	1.2188	1.030
$1\frac{1}{2}$	4	0.2500	1.1965	1.3429	1.266
$1\frac{3}{4}$	4	0.2500	1.4456	1.5916	1.811
2	4	0.2500	1.6948	1.8402	2.454
$2\frac{1}{4}$	3	0.3333	1.8572	2.0450	2.982
$2\frac{1}{2}$	3	0.3333	2.1065	2.2939	3.802
$2\frac{3}{4}$	3	0.3333	2.3558	2.5427	4.711
3	2	0.5000	2.4326	2.7044	5.181
$3\frac{1}{2}$	2	0.5000	2.9314	3.2026	7.388
4	2	0.5000	3.4302	3.7008	9.985
$4\frac{1}{2}$	2	0.5000	3.9291	4.1991	12.972
5	2	0.5000	4.4281	4.6973	16.351

*Per inch of length of engagement.

APPENDIX-TAB AB7 PREFERRED ACME SCREW THREADS

APPENDIX-TAB AB8 SAE GRADES OF STEELS FOR FASTENER

Grade Number	Bolt Size (in)	Tensile Strength (Ksi)	Yield Strength (Ksi)	Proof Strength (Ksi)	Head Marking
1	1/4-1½	60	36	33	None
2	1/4-3/4	74	57	55	None
	>3/4-1½	60	36	33	
4	1/4-1½	115	100	65	None
5	1/4-1	120	92	85	Ⓐ
	>1-1½	105	81	74	
7	1/4-1½	133	115	105	Ⓑ
8	1/4-1½	150	130	120	Ⓒ

APPENDIX-TAB AB9 ASTM STANDARD BOLT STEELS

ASTM Grade	Bolt Size (in)	Tensile Strength (Ksi)	Yield Strength (Ksi)	Proof Strength (Ksi)	Head Mark
A307	1/4-4	60	(Not reported)		N
A325	1/2-1	120	92	85	Ⓐ
	>1-1½	105	81	74	
A354-BC	1/4-2½	125	109	105	+
A354-BD	1/4-2½	150	130	120	+
A449	1/4-1	120	92	85	+
	>1-1½	105	81	74	
	>1½-3	90	58	55	
A574	0.060-1½	180	—	140	(Soc)
	5/8-4	170	—	135	Caps

APPENDIX-TAB AB10 METRIC GRADES OF STEELS FOR BOLTS

Grade	Bolt Size	Tensile Strength (MPa)	Yield Strength (MPa)	Proof Strength (MPa)
4.6	M5-M36	400	240	225
4.8	M1.6-M16	420	340 ^a	310
5.8	M5-M24	520	415 ^a	380
8.8	M17-M36	830	660	600
9.8	M1.6-M16	900	720 ^a	650
10.9	M6-M36	1 040	940	830
12.9	M1.6-M36	1 220	1 100	970

^aYield strengths approximate and not included in standard.

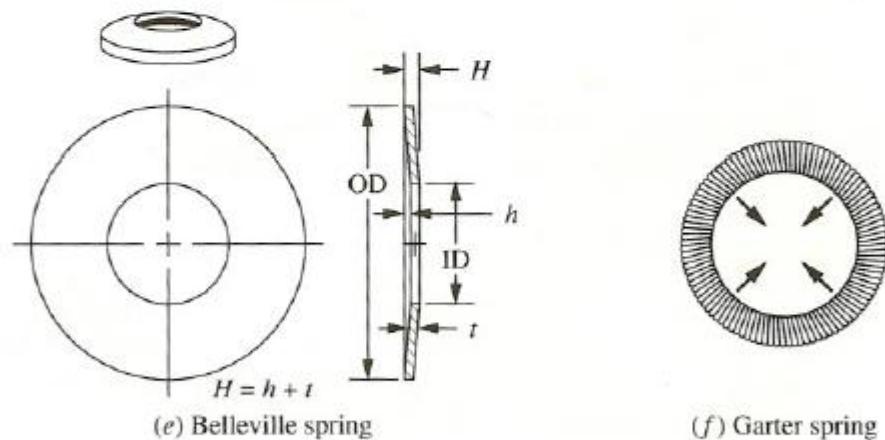
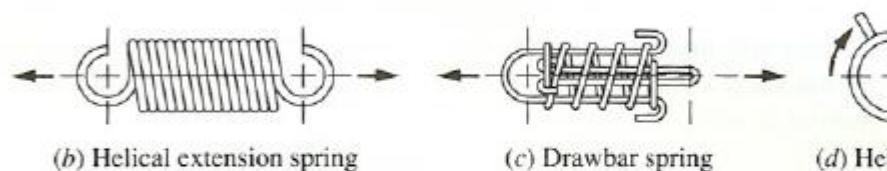
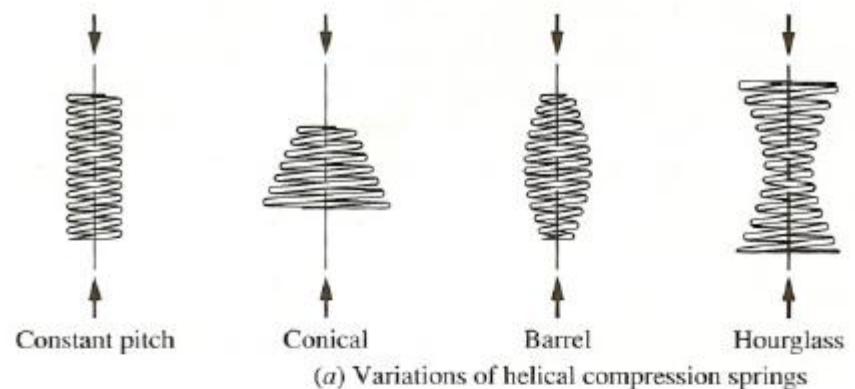
APPENDIX-TAB AB11 AMERICAN STANDARD THREAD DIMENSION, NUMBERED SIZES

Size	Basic Major Diameter (in)	Coarse Threads: UNC		Fine Threads: UNF	
		Threads per in	Tensile Stress Area (in ²)	Threads per in	Tensile Stress Area (in ²)
0	0.060 0	—	—	80	0.001 8
1	0.073 0	64	0.002 63	72	0.002 1
2	0.086 0	56	0.003 70	64	0.003 5
3	0.099 0	48	0.004 87	56	0.005 2
4	0.112 0	40	0.006 04	48	0.006 0
5	0.125 0	40	0.007 96	44	0.008 1
6	0.138 0	32	0.009 09	40	0.010 0
8	0.164 0	32	0.014 0	36	0.014 7
10	0.190 0	24	0.017 5	32	0.020 0
12	0.216 0	24	0.024 2	28	0.025 8

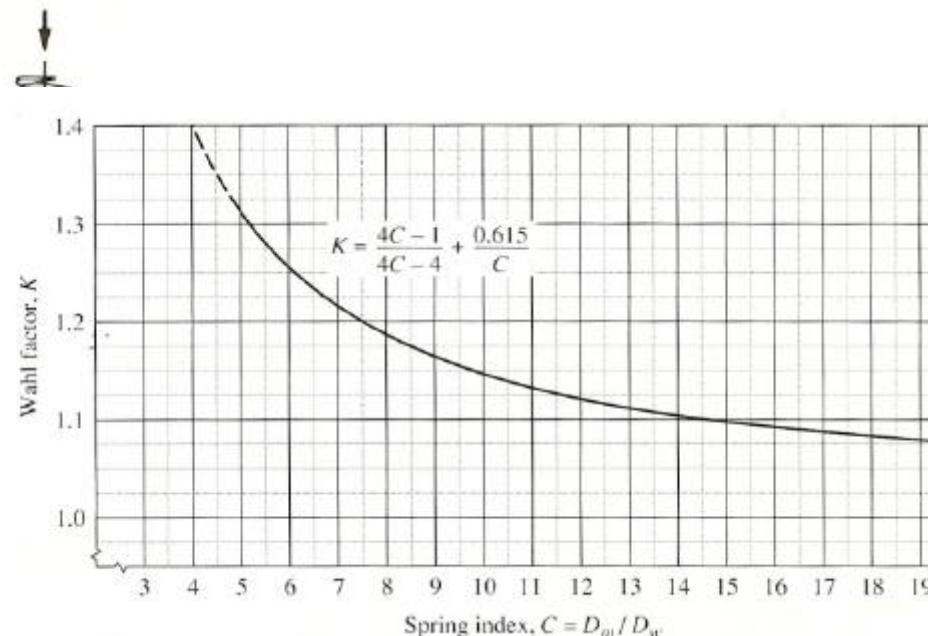
APPENDIX-TAB AB12 AMERICAN STANDARD THREAD DIMENSION, FRACTIONAL SIZES

Size	Coarse Threads: UNC			Fine Thread		Basic Major Diameter (mm)	Coarse Threads		Fine Threads	
	Basic Major Diameter (in)	Threads per in	Tensile Stress Area (in ²)	Threads per in	Basic Major Diameter (mm)	Pitch (mm)	Tensile Stress Area (mm ²)	Pitch (mm)	Tensile Stress Area (mm ²)	
1/4	0.250 0	20	0.031 8	28	1	0.25	0.460	—	—	
5/16	0.312 5	18	0.052 4	24	1.6	0.35	1.27	0.20	1.57	
3/8	0.375 0	16	0.077 5	24	2	0.4	2.07	0.25	2.45	
7/16	0.437 5	14	0.106 3	20	2.5	0.45	3.39	0.35	3.70	
1/2	0.500 0	13	0.141 9	20	3	0.5	5.03	0.35	5.61	
9/16	0.562 5	12	0.182	18	4	0.7	8.78	0.5	9.79	
5/8	0.625 0	11	0.226	18	5	0.8	14.2	0.5	16.1	
3/4	0.750 0	10	0.334	16	6	1	20.1	0.75	22.0	
7/8	0.875 0	9	0.462	14	8	1.25	36.6	1	39.2	
1	1.000	8	0.606	12	10	1.5	58.0	1.25	61.2	
1 1/8	1.125	7	0.763	12	12	1.75	84.3	1.25	92.1	
1 1/4	1.250	7	0.969	12	16	2	157	1.5	167	
1 3/8	1.375	6	1.155	12	20	2.5	245	1.5	272	
1 1/2	1.500	6	1.405	12	24	3	353	2	384	
1 3/4	1.750	5	1.90	—	30	3.5	561	2	621	
2	2.000	4 1/2	2.50	—	36	4	817	3	865	
					42	4.5	1 121	—	—	
					48	5	1 473	—	—	

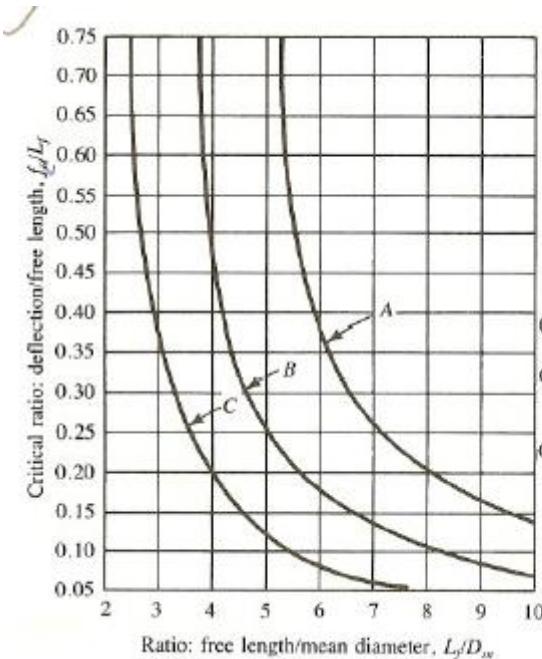
APPENDIX-TAB AB13 METRIC THREAD DIMENSIONS



APPENDIX-FIG AB1: SEVERAL TYPES OF SPRINGS



APPENDIX-FIG AB2: WAHL FACTOR VS. SPRING INDEX FOR ROUNDWIRE

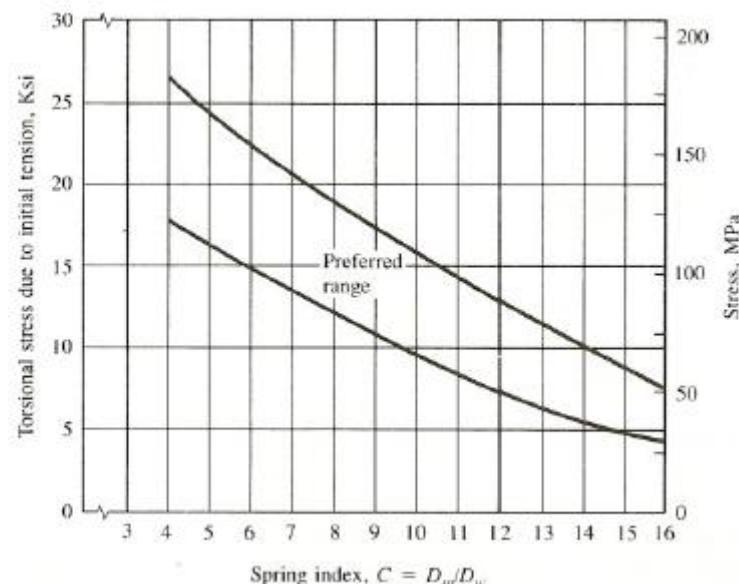


APPENDIX-FIG AB3: SPRING BUCKLING CRITERIA.

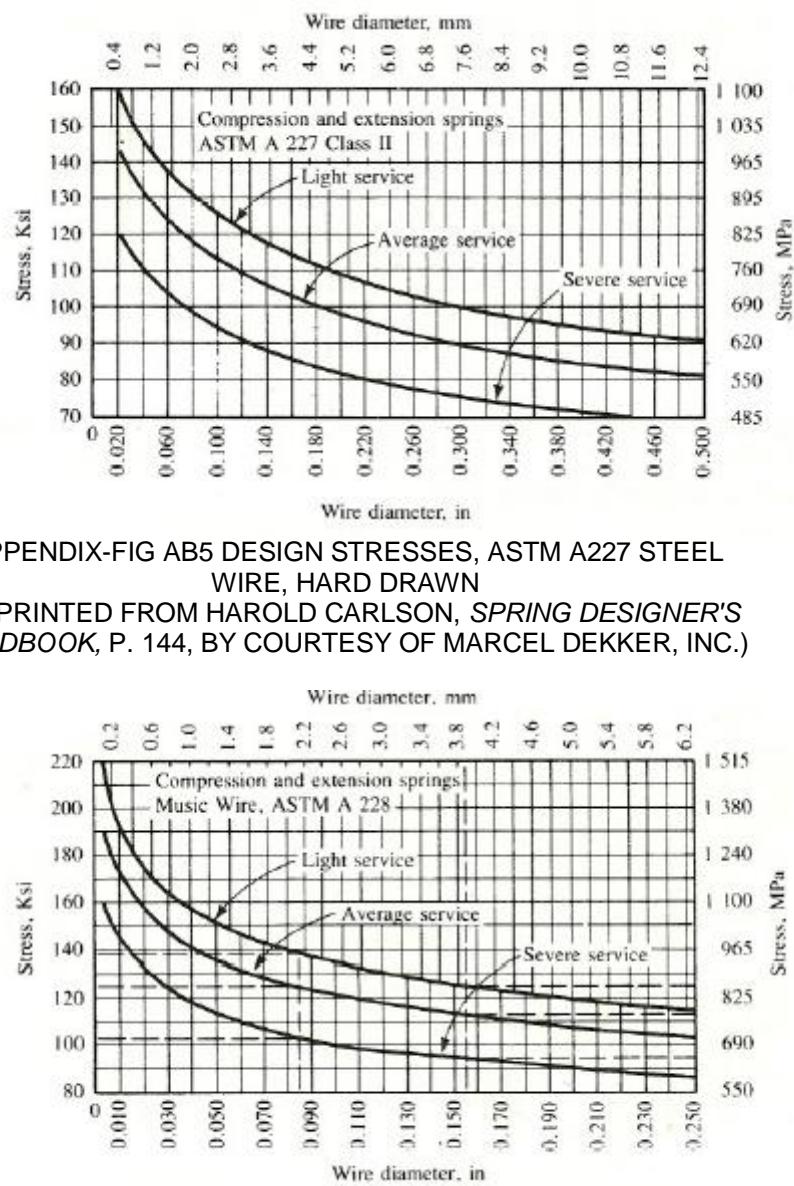
Curve A: Fixed ends (e.g., squared and ground ends; ends on guided, flat, parallel surfaces)

 Curve B: One fixed end; one pinned end (end on flat surface, one in contact with a spherical ball)

 Curve C: Both ends pinned (e.g., ends in contact with surfaces which are pinned to the spring and permitted to rotate)

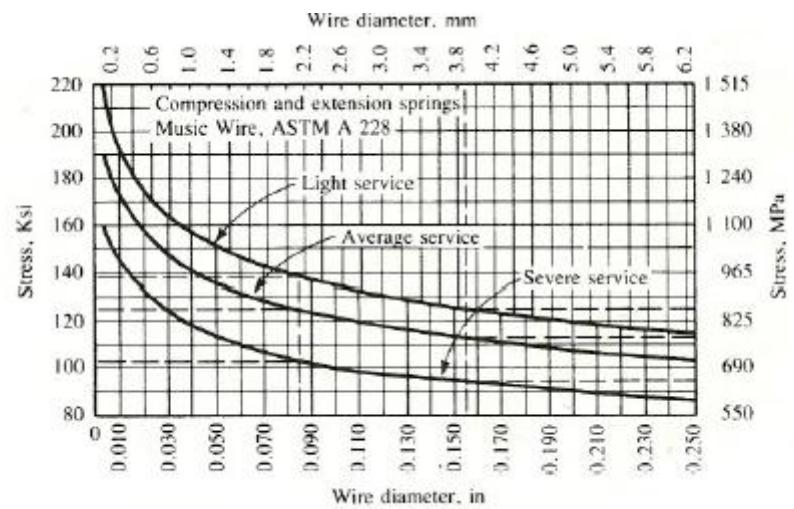


APPENDIX-FIG AB4 RECOMMENDED TORSIONAL SHEAR STRESS IN AN EXTENSION SPRING DUE TO INITIAL TENSION (DATA FROM ASSOCIATED SPRING, BARNES GROUP, INC.)



APPENDIX-FIG AB5 DESIGN STRESSES, ASTM A227 STEEL WIRE, HARD DRAWN

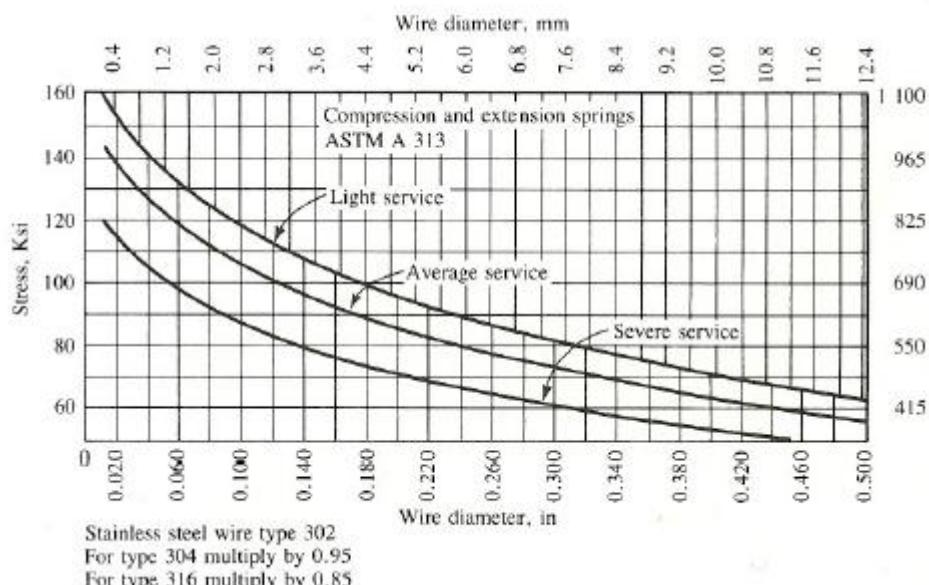
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Similar design stresses for ASTM A313, type 631 stainless steel wire, 17-7 PH

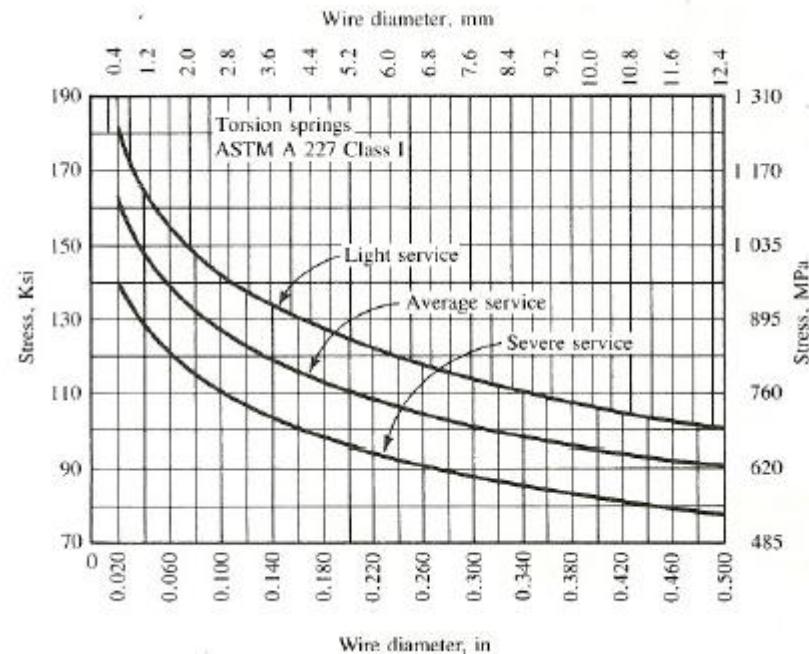
APPENDIX-FIG AB6 DESIGN STRESSES, ASTM A228 STEEL WIRE (MUSIC WIRE)

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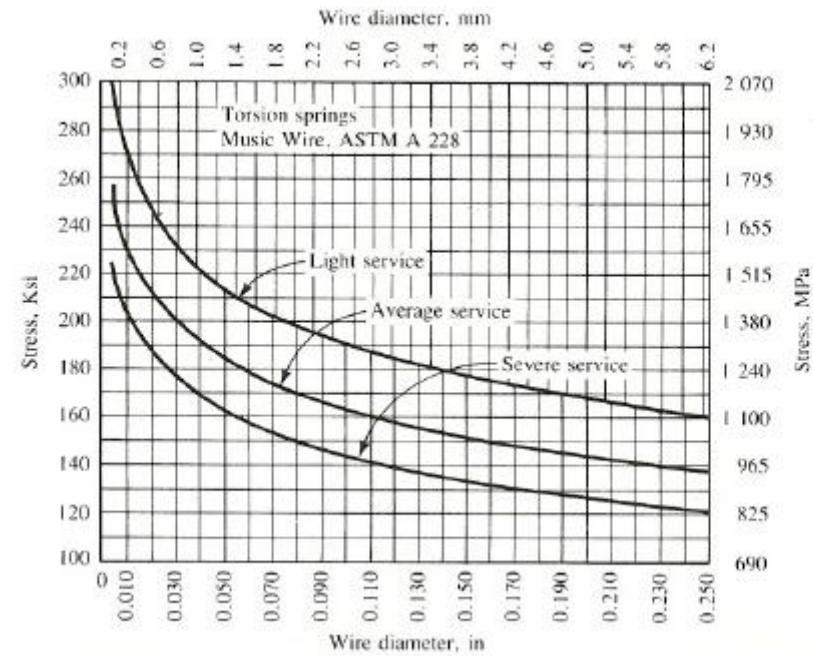


APPENDIX-FIG AB7 DESIGN STRESSES, ASTM A313 CORROSION-RESISTANT STAINLESS STEEL WIRE

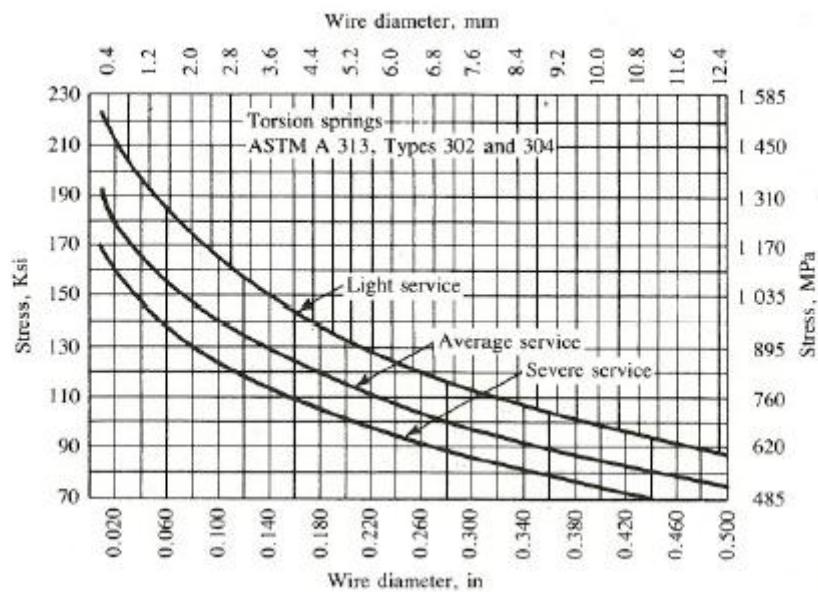
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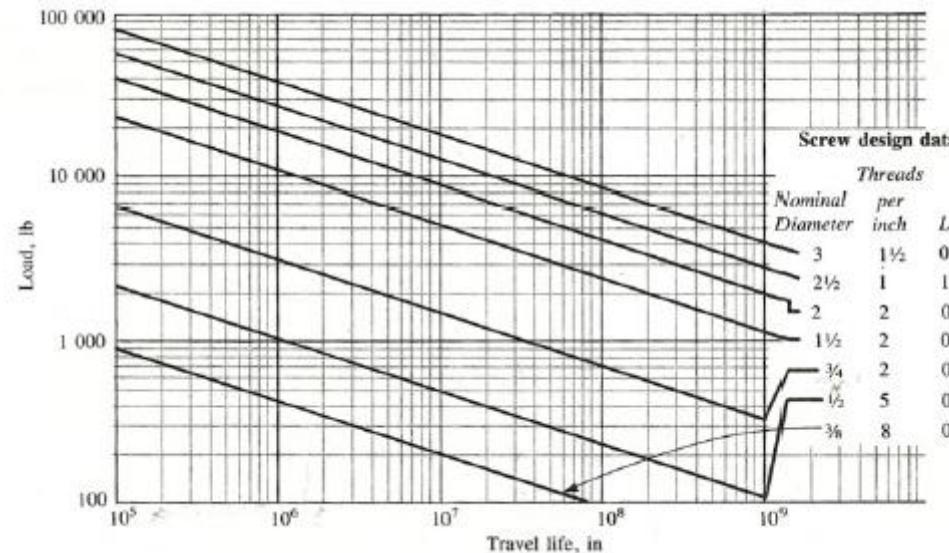
APPENDIX-FIG AB8 APPENDIX A-21-1 DESIGN STRESSES FOR TORSION SPRINGS ASTM A227 STEEL WIRE, HARD DRAWN
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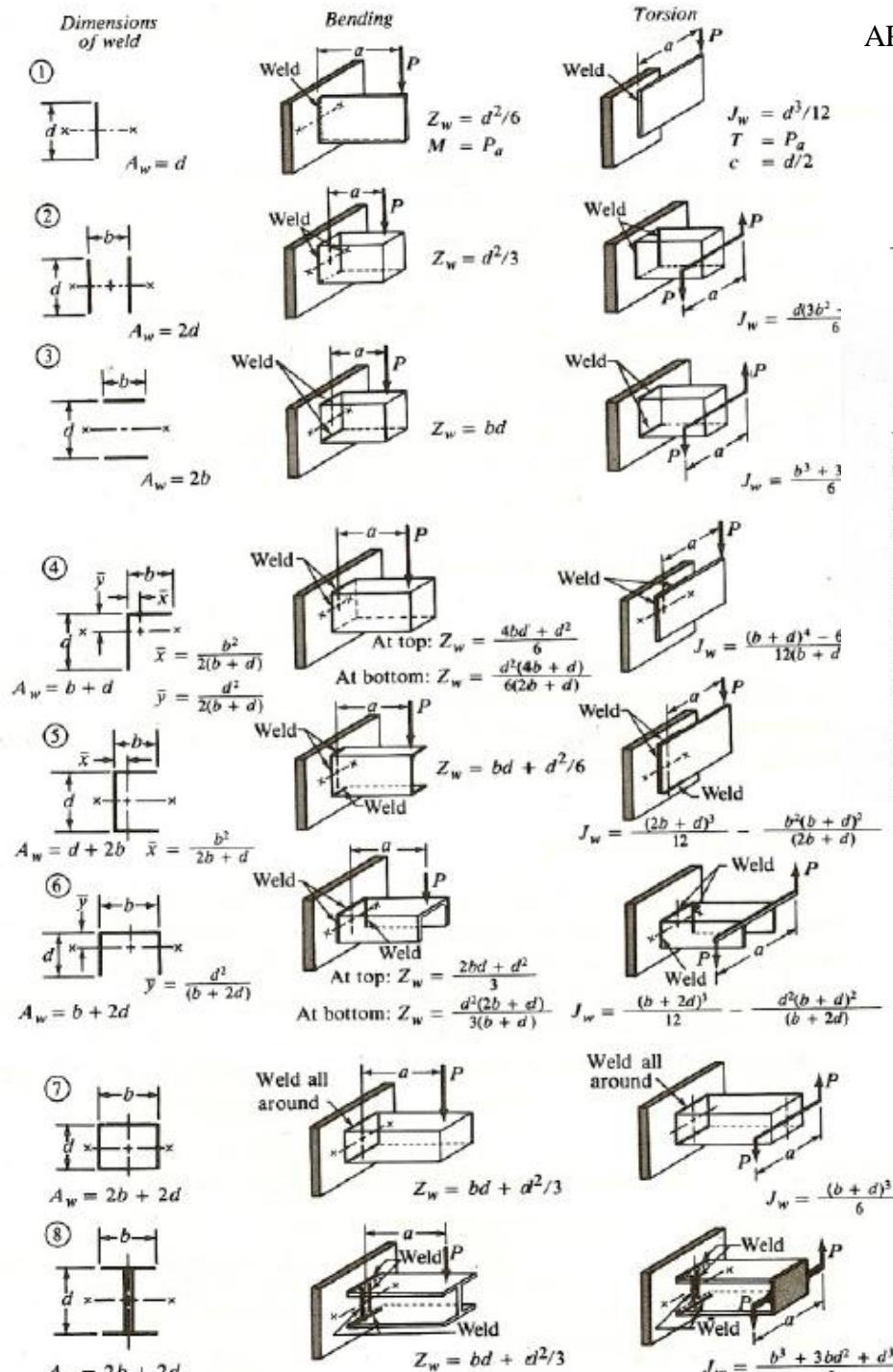
APPENDIX-FIG AB9 DESIGN SFRESSESFOR TORSION SPRINGSASTM A228 MUSIC WIN'
(REPRINTED FROM HAROLD CARLSON, SPRING DESIGNER'S HANDBOOK, P. 143, BY COURTESY OF MARCEL DEKKER, INC.)



APPENDIX-FIG AB10 DESIGN STRESSES FOR TORSION SPRINGS ASTM A313 STAINLESS STEEL WIRE, TYPES 302 AND 304, CORROSION RESISTANT (REPRINTED FROM HAROLD CARLSON, *SPRING DESIGNER'S HANDBOOK*, P. 150, BY COURTESY OF MARCEL DEKKER, INC.)



APPENDIX-FIG AB12: BALL SCREW PERFORMANCE



APPENDIX-FIG AB11: GEOMETRY FACTORS FOR WELD ANALYSIS

Design of Flexible Drives

Table 1: V-Belt Service Factor

Driven Machine Type	Driver Type		
	AC Motors: Normal Torque ^a		
	DC Motors: Shunt-wound, Compound-wound	Engines: Multiple Cylinder	AC Motors: High Torque ^b
Agitators, blowers, fans, centrifugal pumps, conveyors, light	1.0	1.1	1.2
Generators, machine tools, mixers, conveyors, gravel	1.1	1.2	1.3
Bucket elevators, textile machines, hammer mills, conveyors, heavy	1.2	1.3	1.4
Crushers, ball mills, hoists, rubber extruders	1.3	1.4	1.5
Any machine that can choke	2.0	2.0	2.0

Table 2: Standard Belt Lengths for 3V, 5V, and BV Belts (in)

<i>3V Only</i>	<i>3V and 5V</i>	<i>3V, 5V, and 8V</i>	<i>5V and 8V</i>	<i>8V Only</i>
25	50	100	150	375
26.5	53	106	160	400
28	56	112	170	425
30	60	118	180	450
31.5	63	125	190	475
33.5	67	132	200	500
35.5	71	140	212	
37.5	75		224	
40	80		236	
42.5	85		250	
45	90		265	
47.5	95		280	
			300	
165			315	
			330	

Table 3 Roller Chain Sizes

<i>Chain Number</i>	<i>Pitch (in)</i>	<i>Average Tensile Strength (lb)</i>
25	1/4	925
35	5/8	2 100
41	1/2	2 000
40	5/8	3 700
50	5/8	6 100
60	3/4	8 500
80	1	14 500
100	1 1/4	24 000
120	1 1/2	34 000
140	1 3/4	46 000
160	2	58 000
180	2 1/4	80 000
200	2 1/2	95 000
240	3	130 000

Table 4 Service Factors for Chain Drives

<i>Load Type</i>	<i>Type of Driver</i>							
	<i>Hydraulic Drive</i>	<i>Electric Motor or Turbine</i>	<i>Internal Combustion Engine with Mechanical Drive</i>					
Smooth (agitators, fans, light uniformly loaded conveyors)	1.0	1.0						1.2
Moderate shock (machine tools, cranes, heavy conveyors, food mixers and grinders)	1.2	1.3						1.4
Heavy shock (punch presses, hammer mills, reciprocating conveyors, rolling mill drive)	1.4	1.5						1.7

Table 5: Horsepower Ratings, Standard Single-strand Roller Chain, No. 40, 12.7-mm Pitch

<i>No. Of Teeth Small Sprocket</i>	<i>Revolutions Per Minute—Small Sprocket</i>																								
	10	25	50	100	200	300	400	500	700	800	1000	1200	1400	1600	1800	2100	2400	2700	3000	3500	4000	5000	6000	7000	8000
9	0.04	0.10	0.19	0.35	0.65	0.93	1.21	1.48	2.00	2.51	2.75	3.25	3.73	4.12	3.45	2.74	2.24	1.88	1.66	1.27	1.04	0.75	0.57	0.45	0.37
10	0.05	0.11	0.21	0.39	0.73	1.04	1.35	1.65	2.24	2.81	3.09	3.64	4.18	4.71	4.04	3.21	2.63	2.20	1.88	1.49	1.22	0.87	0.66	0.53	0.43
11	0.05	0.12	0.23	0.43	0.80	1.16	1.50	1.83	2.40	3.11	3.42	4.03	4.63	5.22	4.66	3.70	3.03	2.54	2.17	1.72	1.41	1.01	0.77	0.61	0.50
12	0.06	0.14	0.25	0.47	0.88	1.17	1.65	2.00	2.71	3.42	3.76	4.43	5.09	5.74	5.31	4.22	3.45	2.89	2.47	1.96	1.60	1.15	0.87	0.69	0.57
13	0.06	0.15	0.26	0.52	0.96	1.39	1.80	2.20	2.97	3.73	4.10	4.83	5.55	6.26	5.99	4.76	3.89	3.26	2.79	2.21	1.81	1.29	0.98	0.78	0.64
14	0.07	0.16	0.36	0.56	1.04	1.50	1.95	2.38	3.12	4.04	4.44	5.23	6.01	6.78	6.70	5.31	4.35	3.65	3.11	2.47	2.02	1.45	1.01	0.87	0.71
15	0.07	0.17	0.37	0.60	1.12	1.62	2.10	2.36	3.17	4.05	4.78	5.64	6.47	7.30	7.43	5.89	4.82	4.04	3.45	2.76	2.24	1.66	1.22	0.97	0.79
16	0.08	0.19	0.35	0.65	1.20	1.74	2.25	2.75	3.77	4.66	5.13	6.04	6.94	7.83	8.18	6.49	5.31	4.45	3.80	3.02	2.47	1.77	1.34	1.07	0.86
17	0.08	0.20	0.37	0.69	1.29	1.85	2.40	2.93	3.97	4.98	5.48	6.45	7.41	8.36	9.11	8.12	6.82	4.88	4.17	3.33	2.71	1.94	1.47	1.17	0.96
18	0.09	0.21	0.39	0.73	1.37	1.97	2.55	3.12	4.21	5.30	5.82	6.86	7.88	8.89	9.76	7.75	6.34	5.31	4.54	3.60	2.95	2.11	1.60	1.27	0
19	0.09	0.22	0.42	0.76	1.45	2.09	2.71	3.31	4.48	5.62	6.17	7.27	8.36	9.42	10.5	8.40	6.88	5.76	4.92	3.91	3.20	2.29	1.74	1.38	0
20	0.10	0.24	0.44	0.82	1.53	2.11	2.86	3.50	4.71	5.94	6.53	7.69	8.83	9.96	11.1	9.07	7.43	6.22	5.31	4.22	3.45	2.47	1.88	1.49	0
21	0.11	0.25	0.46	0.87	1.62	2.33	3.02	3.69	4.99	6.26	6.88	8.11	9.31	10.5	11.7	9.76	7.99	6.70	5.72	4.54	3.71	2.66	2.02	1.60	0
22	0.11	0.26	0.48	0.91	1.70	2.45	3.17	3.88	5.27	6.58	7.23	8.52	9.79	11.0	12.3	10.5	8.57	7.18	6.13	5.55	5.20	4.26	3.03	2.32	1.84
23	0.12	0.27	0.51	0.96	1.78	2.57	3.33	4.07	5.51	6.90	7.59	8.94	10.3	11.6	12.9	11.2	9.16	7.68	6.55	5.20	4.26	3.03	2.32	1.84	0
24	0.13	0.29	0.56	1.06	1.87	2.69	3.48	4.26	5.76	7.23	7.95	9.36	10.8	12.1	13.5	11.9	9.76	8.18	6.99	5.54	4.54	3.25	2.47	1.96	0
25	0.13	0.30	0.58	1.05	1.95	2.81	3.64	4.44	6.02	7.55	8.30	9.78	11.2	12.7	14.1	12.7	10.4	8.70	7.43	5.89	4.82	3.45	2.63	0	
26	0.14	0.31	0.58	1.09	2.04	2.93	3.80	4.68	6.28	7.88	8.66	10.2	11.7	13.2	14.7	13.5	11.0	9.23	7.88	6.25	5.12	3.66	2.79	0	
28	0.15	0.34	0.63	1.18	2.20	3.18	4.11	5.03	6.81	8.54	9.39	11.1	12.7	14.3	15.9	15.0	12.3	10.3	8.80	6.99	5.72	4.09	3.11	0	
30	0.16	0.37	0.68	1.27	2.38	3.42	4.43	5.42	7.31	9.20	10.1	11.9	13.7	15.4	17.2	16.7	13.6	11.4	9.76	7.75	6.34	4.54	3.45	0	
32	0.17	0.39	0.73	1.36	2.55	3.67	4.75	5.81	7.86	9.86	10.8	12.8	14.7	16.5	18.4	15.0	12.6	10.8	8.64	6.99	5.00	0			
35	0.19	0.43	0.81	1.50	2.81	4.04	5.24	6.40	8.66	10.9	11.9	14.1	16.2	18.2	20.2	20.3	21.0	17.2	14.4	12.3	9.76	7.99	5.72	0	
40	0.22	0.50	0.93	1.74	3.24	4.67	6.05	7.39	10.0	12.5	13.8	16.3	18.7	21.1	23.4	25.7	21.0	17.6	15.0	11.9	9.76	6.99	0		
45	0.25	0.57	1.06	1.97	3.68	5.30	6.87	8.40	11.4	14.2	15.7	18.5	21.2	23.9	26.6	30.5	25.1	21.0	17.9	14.2	11.7	0			

Table 6: Horsepower Ratings, Standard Single-strand Roller Chain, No. 60, 19-mm Pitch

No. Of Teeth Small Sprok.	Revolutions Per Minute—Small Sprocket																								
	10	25	50	100	150	200	300	400	500	600	700	800	900	1000	1100	1200	1400	1600	1800	2000	2500	3000	3500	4000	4500
9	0.15	0.33	0.62	1.16	1.67	2.16	3.12	4.04	4.94	5.82	6.68	7.54	8.38	9.21	9.99	8.77	6.96	5.70	4.77	4.08	2.92	2.22	1.76	1.44	1.21
10	0.16	0.37	0.70	1.23	1.74	2.23	3.49	4.53	5.53	6.32	7.49	8.44	9.39	10.3	11.2	10.3	8.15	6.67	5.59	4.77	3.42	2.60	2.06	1.69	1.41
11	0.18	0.41	0.77	1.44	2.07	2.69	3.87	5.02	6.13	7.23	8.30	9.36	10.4	11.4	12.5	11.9	9.41	7.70	6.45	5.51	3.94	3.00	2.38	1.95	1.63
12	0.20	0.45	0.85	1.50	2.28	2.95	4.25	5.51	6.74	7.94	9.12	10.3	11.4	12.6	13.7	13.5	10.7	8.77	7.35	6.28	4.49	3.42	2.71	2.22	1.86
13	0.22	0.50	0.92	1.73	2.49	3.22	4.64	6.01	7.38	8.65	9.94	11.2	12.5	13.7	14.9	15.2	12.1	9.81	8.29	7.08	5.06	3.85	3.05	2.50	0
14	0.24	0.54	1.00	1.87	2.69	3.49	5.02	6.51	7.96	9.37	10.8	12.1	13.5	14.8	16.2	17.0	13.5	11.1	9.26	7.91	5.66	4.31	3.45	2.80	0
15	0.25	0.58	1.08	2.00	2.90	3.76	5.41	7.01	8.57	10.1	11.6	13.1	14.5	16.0	17.4	18.8	15.0	12.3	10.3	8.77	6.28	4.77	3.79	3.10	0
16	0.27	0.62	1.16	2.16	3.11	4.03	5.80	7.52	9.19	10.1	12.4	14.0	15.6	17.1	18.7	20.2	16.5	13.5	11.3	9.66	6.91	5.27	4.17	3.42	0
17	0.29	0.66	1.24	2.31	3.32	4.30	6.20	8.03	9.81	11.6	13.3	15.0	16.7	18.3	19.9	21.6	18.1	14.8	12.4	10.6	7.57	5.76	4.57	3.74	0
18	0.31	0.70	1.31	2.45	3.53	4.58	6.59	8.54	10.4	12.3	14.1	15.9	17.7	19.5	21.2	19.7	16.1	13.5	11.5	8.25	6.28	4.98	4.08	0	
19	0.33	0.75	1.39	2.60	3.74	4.85	6.99	9.05	11.1	13.0	15.0	16.9	18.8	20.6	22.5	24.3	21.4	17.5	14.6	12.5	8.95	6.81	5.40	4.42	0
20	0.35	0.79	1.47	2.75	3.96	5.13	7.38	9.57	11.7	13.8	15.8	17.9	19.8	21.8	23.8	25.7	23.1	18.9	15.6	13.5	9.66	7.35	5.83	0	
21	0.36	0.83	1.55	2.90	4.17	5.40	7.78	10.1	12.3	14.5	16.7	18.8	20.9	23.0	25.1	27.1	24.8	20.3	17.0	14.5	10.4	7.91	6.28	0	
22	0.38	0.87	1.63	3.05	4.30	5.68	8.19	10.6	13.0	15.3	17.5	19.8	22.0	24.2	26.4	28.5	26.6	21.8	18.2	15.6	11.1	8.48	6.73	0	
23	0.40	0.92	1.71	3.19	4.60	5.96	8.59	11.1	13.6	16.0	18.4	20.8	23.1	25.4	27.7	29.9	28.4	23.3	19.5	16.7	11.9	9.07	7.19	0	
24	0.42	0.96	1.79	3.35	4.82	6.24	8.99	11.6	14.2	16.8	19.3	21.7	24.2	26	29.0	31.0	30.3	24.8	20.8	17.8	12.7	9.66	7.67	0	
25	0.44	1.00	1.87	3.50	5.04	6.52	9.40	12.2	14.9	17.5	20.1	22.7	25.3	27.8	30.3	32.7	32.2	26.4	22.1	18.9	13.5	10.3	8.15	0	
26	0.46	1.05	1.95	3.65	5.25	6.81	9.80	12.7	15.5	18.3	21.0	23.7	26.4	29.0	31.6	34.1	34.2	28.0	23.4	20.0	14.3	10.9	8.65	0	
28	0.48	1.13	2.12	3.96	5.69	7.37	10.6	13.8	16.8	19.8	22.8	25.7	28.5	31.4	34.2	37.0	38.2	31.3	26.2	22.4	16.0	12.2	0		
30	0.54	1.22	2.28	4.26	6.13	7.94	11.4	14.8	18.1	21.4	24.5	27.7	30.8	33.6	36	39.4	42.4	34.7	29.1	24.8	17.8	13.5	0		
32	0.57	1.31	2.45	4.56	6.57	8.52	12.3	15.9	19.4	22.9	26.3	29.7	33.0	36.3	39.5	42.7	46.7	38.2	32.0	27.3	19.6	14.9	0		
35	0.63	1.44	2.69	5.03	7.24	9.38	13.5	17.5	21.4	25.2	29.0	32.7	36.3	39.9	43.5	47.1	51.4	53.4	43.7	36.6	31.3	22.4	17.0	0	
40	0.73	1.67	3.11	5.81	8.77	10.8	15.6	20.2	24.7	29.1	33.5	37.7	42.0	46.1	50.3	54.4	62.5	53.4	44.7	38.2	27.3	0			
45	0.83	1.89	3.53	6.60	9.50	12.3	17.7	23.0	28.1	33.1	38.0	42.0	47.7	52.4	57.1	61.7	70.5	63.7	53.4	45.6	32.6	0			

TYPE I

TYPE II

TYPE III

Source: Adapted from *Chain for Belts Transmission and Material Handling*, p. 160, by courtesy of Metal Publishing Inc.

Table 7: Horsepower Ratings, Standard Single-strand Roller Chain, No. 80,
25.4-mm Pitch

No. Of Teeth Small Sprok.	Revolutions Per Minute—Small Sprocket																								
	10	25	50	100	150	200	300	400	500	600	700	800	900	1000	1100	1200	1400	1600	1800	2000	2200	2400	2700	3000	3400
9	0.34	0.78	1.45	2.71	3.90	5.05	7.28	9.43	11.5	13.6	15.6	17.6	17.0	14.5	12.6	11.0	8.76	7.17	6.01	5.13	4.45	3.90	3.27	2.79	2.32
10	0.38	0.87	1.63	3.03	4.37	5.66	8.16	10.6	12.9	15.2	17.5	19.7	19.9	17.0	14.7	12.9	10.3	8.40	7.04	6.01	5.21	4.57	3.83	3.27	2.71
12	0.47	1.06	1.98	3.69	5.32	6.89	9.93	12.9	15.7	18.5	21.3	24.0	26.2	22.3	19.4	17.0	14.5	12.6	11.0	9.25	7.90	6.85	5.61	4.30	0
13	0.51	1.16	2.16	4.03	5.80	7.52	10.8	14.0	17.1	20.2	23.2	26.2	29.1	25.2	21.8	18.2	15.2	12.5	10.4	8.91	7.72	6.78	5.68	4.85	0
14	0.55	1.25	2.34	4.36	6.29	8.14	11.7	15.2	18.6	21.9	25.1	28.4	31.5	28.2	24.4	21.4	17.0	13.9	11.7	9.96	8.63	7.57	6.35	5.42	0
15	0.59	1.35	2.52	4.77	6.77	8.77	12.6	16.4	20.0	23.7	27.1	30.6	34.0	31.2	27.1	23.8	18.9	15.4	12.9	11.0	9.57	8.40	7.04	6.01	0
16	0.63	1.45	2.70	5.04	7.26	9.41	13.5	17.6	21.5	25.5	29.0	32.5	36.4	34.4	29.8	26.2	20.8	17.0	14.2	12.2	10.5	9.25	7.76	6.62	0
17	0.68	1.58	2.87	5.35	7.55	9.75	13.7	17.8	21.9	25.9	31.0	35.0	38.9	37.7	32.7	28.7	22.7	18.6	15.6	13.3	11.5	10.1	8.49	7.25	0
18	0.72	1.64	3.07	5.72	8.25	10.7	15.4	19.9	24.4	28.7	33.0	37.2	41.4	41.1	35.6	31.2	24.8	20.3	17.0	14.5	12.6	11.0	9.25	7.90	0
19	0.76	1.74	3.25	6.07	8.74	11.3	16.3	21.1	25.8	30.4	35.0	39.4	43.8	44.5	38.6	33.9	26.9	22.0	18.4	15.7	13.6	12.0	10.8	8.57	0
20	0.81	1.84	3.45	6.41	9.24	12.0	17.2	22.3	27.3	32.2	37.0	41.7	46.3	48.1	41.7	36.6	29.0	23.8	19.9	17.0	14.7	12.9	10.8	0	
21	0.85	1.94	3.62	6.76	9.74	12.6	18.2	23.5	28.8	33.9	39.0	43.9	48.9	51.7	44.8	39.4	31.2	25.6	21.4	18.3	15.9	13.9	11.7	0	
22	0.90	2.04	3.81	7.11	10.2	14.9	19.1	24.8	30.3	35.7	41.0	46.7	51.4	55.5	48.1	42.7	33.5	27.4	23.0	19.6	17.0	14.9	12.5	0	
23	0.94	2.14	4.00	7.46	10.7	13.9	20.1	26.0	31.8	37.4	43.0	48.5	53.9	59.3	51.4	45.1	35.8	29.3	24.6	21.0	18.2	15.9	13.4	0	
24	0.98	2.24	4.19	7.81	11.3	14.6	21.0	27.2	33.2	39.2	45.4	50.4	56.4	62.0	54.8	48.1	38.2	31.2	26.2	22.3	19.4	17.0	14.2	0	
25	1.03	2.34	4.37	8.16	11.8	15.6	21.2	29.4	34.7	40.9	47.0	53.0	59.0	64.8	58.2	51.1	40.6	33.2	27.8	23.8	20.6	18.1	15.1	0	
26	1.07	2.45	4.56	8.52	12.3	15.9	22.9	29.7	36.2	42.7	47.7	54.1	55.3	61.5											

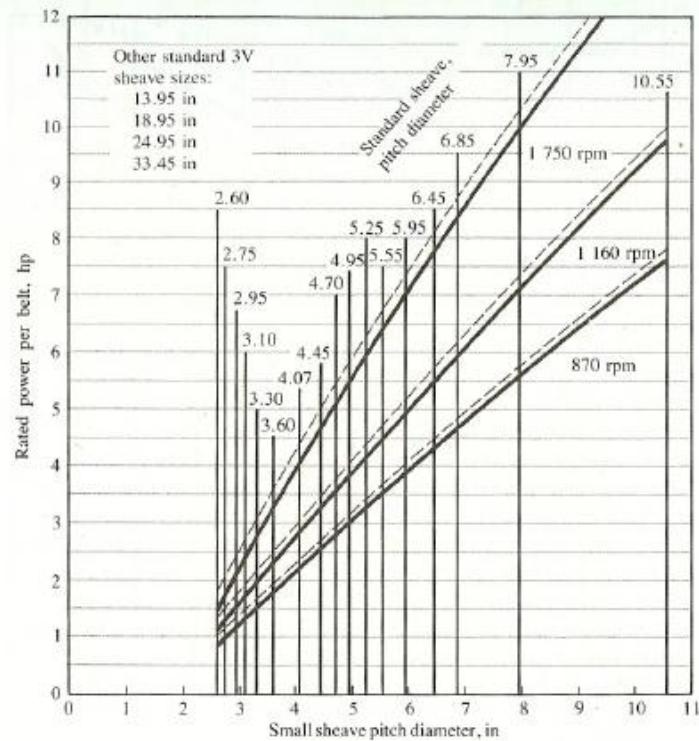


Figure 2: Power Rating: 3V Belts

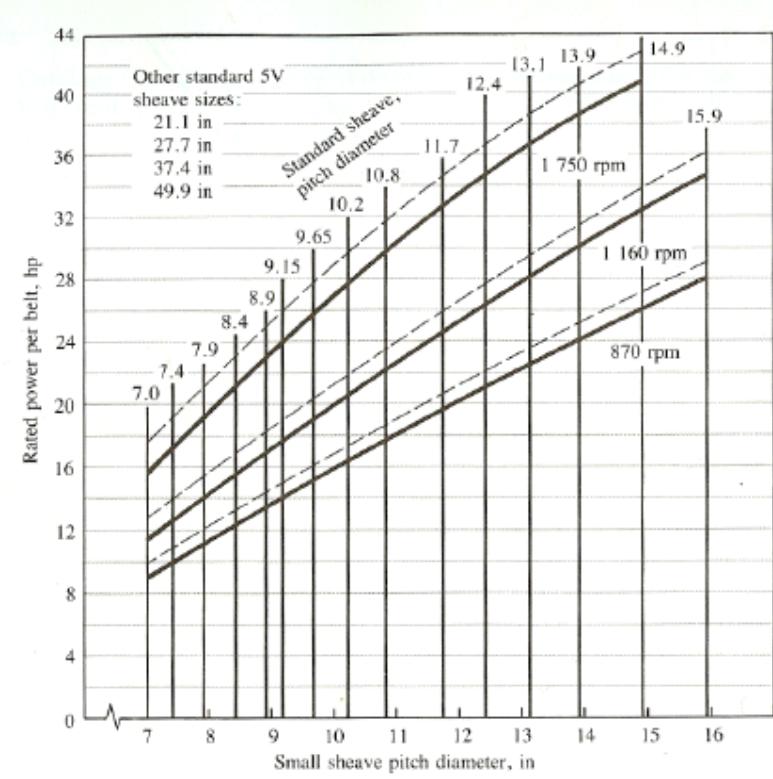


Figure 3: Power Rating: 5V Belts

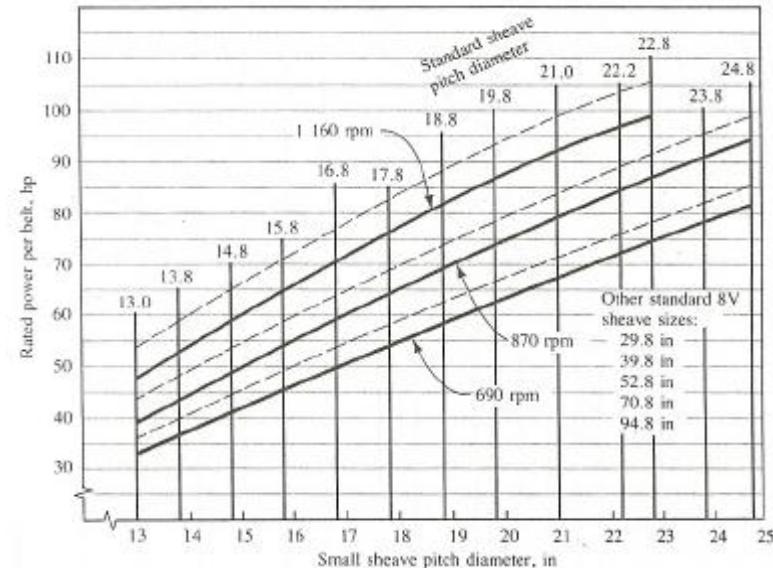


Figure 4: Power Rating: 8V Belts

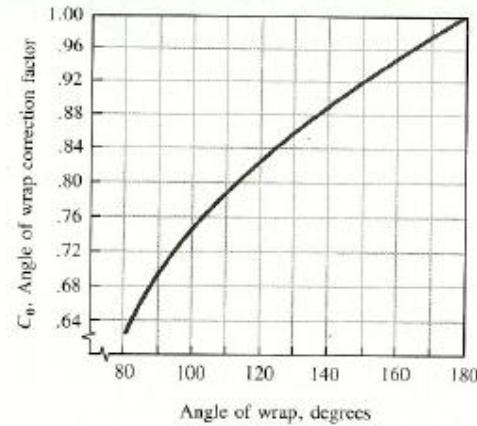


Figure 5: Angle of Wrap Correction Factor, C_o

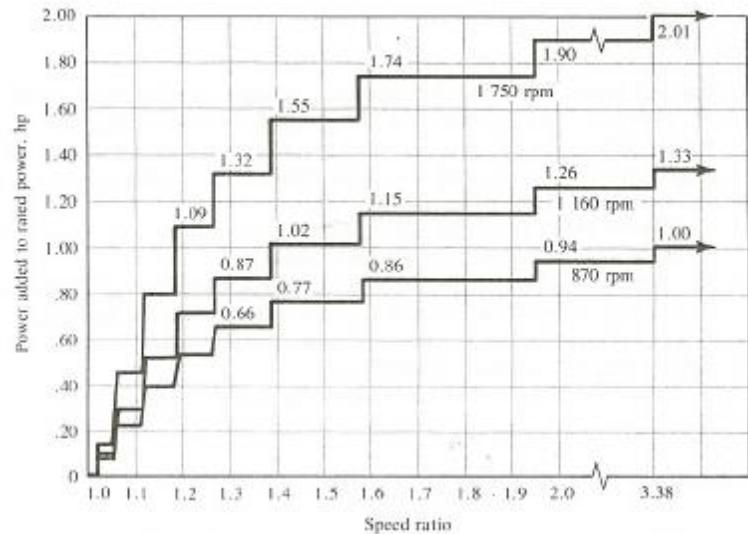


Figure 6: Power Added versus Speed Ratio: 5V Belts

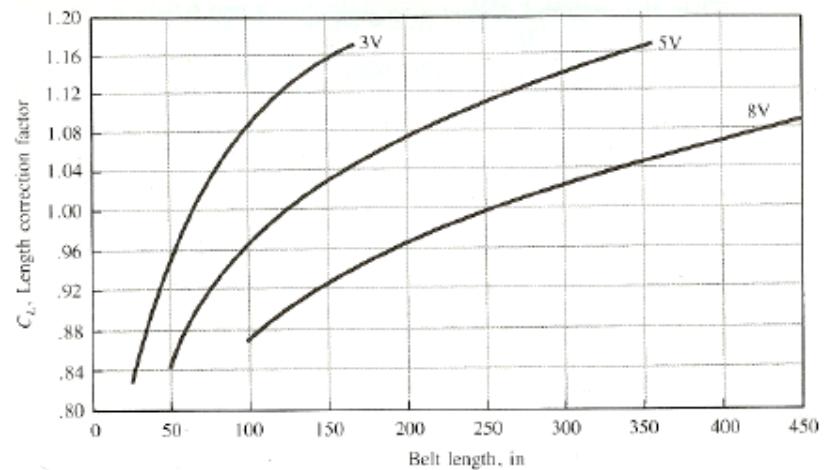


Figure 7: Belt Length Correction Factor, C_L

Design of Gears

Table 1: Standard Circular Pitches (inches)

10.0	7.5	5.0
9.5	7.0	4.5
9.0	6.5	4.0
8.5	6.0	3.5
8.0	5.5	

Table 2: Standard Diametral Pitches (teeth/inch)

Coarse Pitch ($P_d < 20$)			Fine Pitch ($P_d \geq 20$)		
1	2	5	12	20	72
1.25	2.5	6	14	24	80
1.5	3	8	16	32	96
1.75	4	10	18	48	120
					64

Table 3: Standard Modules

Module (mm)	Equivalent P_d	Closest Standard P_d (Teeth/inch)
0.3	84.667	80
0.4	63.500	64
0.5	50.800	48
0.8	31.750	32
1	25.400	24
1.25	20.320	20
1.5	16.933	16
2	12.700	12
2.5	10.160	10
3	8.466	8
4	6.350	6
5	5.080	5
6	4.233	4
8	3.175	3
10	2.540	2.5
12	2.117	2
16	1.587	1.5
20	1.270	1.25
25	1.016	1

Table 4: Formulas for Gear-tooth Features for 20° Pressure Angle

Feature	Symbol	Full-depth Involute System		Metric Module System
		Coarse Pitch ($P_d < 20$)	Fine Pitch ($P_d \geq 20$)	
Addendum	a	$1/P_d$	$1/P_d$	1.00m
Dedendum	b	$1.25/P_d$	$1.200/P_d + 0.002$	1.25m
Clearance	c	$0.25/P_d$	$0.200/P_d + 0.002$	0.25m

Table 5: Recommended Minimum Backlash for Coarse Pitch Gears

P_d	A. Diametral Pitch System (Backlash in Inches) Center Distance, C (in)				
	2	4	8	16	32
18	0.005	0.006	—	—	—
12	0.006	0.007	0.009	—	—
8	0.007	0.008	0.010	0.014	—
5	—	0.010	0.012	0.016	—
3	—	0.014	0.016	0.020	0.028
2	—	—	0.021	0.025	0.033
1.25	—	—	—	0.034	0.042

Module m	B. Metric Module System (Backlash in Millimeters) Center Distance, C (mm)				
	50	100	200	400	800
1.5	0.13	0.16	—	—	—
2	0.14	0.17	0.22	—	—
3	0.18	0.20	0.25	0.35	—
5	—	0.26	0.31	0.41	—
8	—	0.35	0.40	0.50	0.70
12	—	—	0.52	0.62	0.82
18	—	—	—	0.80	1.00

Source: Extracted from AGMA 2002-B88 Standard, *Tooth Thickness Specification and Measurement*, with permission of the publisher, American Gear Manufacturers Association, 1500 King Street, Suite 201, Alexandria, Va. 22314.

Table 6: Number of Pinion Teeth to Ensure No Interference

For a Pinion Meshing with a Rack		For a 20° Full-depth Pinion Meshing with a Gear	
Tooth Form	Minimum Number of Teeth	Number of Pinion Teeth	Maximum Number of Gear Teeth
14½° Involute, Full-Depth	32	17	1309
20° Involute, Full-Depth	18	16	101
25° Involute, Full-Depth	12	15	45
		14	26
		13	16

Table 7: Allowable Stress Numbers for Through-hardened Steel Gear Materials

Hardness at Surface (HB)	Allowable Bending Stress Number		Allowable Contact Stress Number	
	Grade 1 (Ksi)	Grade 2 (Ksi)	Grade 1 (MPa)	Grade 2 (MPa)
Up to 180	25	170	33	230
240	31	210	41	280
300	36	250	47	325
360	40	280	52	360
400	42	290	56	390
85	85	590	95	660
105	105	720	115	790
120	120	830	135	930
145	145	1000	160	1100
155	155	1100	170	1200

Source: Extracted from AGMA Standard 2001-B88, *Fundamental Rating Factors and Calculation Methods for Involute Spur and Helical Gear Teeth*, with the permission of the publisher, American Gear Manufacturers Association, 1500 King Street, Suite 201, Alexandria, Va. 22314.

Table 8: Approximate Allowable Tooth Bending Stress in Plastic Gears

Material	Approximate Allowable Bending Stress, ksi (MPa)	
	Unfilled	Glass-filled
ABS	3 (21)	6 (41)
Acetal	5 (34)	7 (48)
Nylon	6 (41)	12 (83)
Polycarbonate	6 (41)	9 (62)
Polyester	3.5 (24)	8 (55)
Polyurethane	2.5 (17)	—

Source: *Plastics Gear*, Manchester, Conn.: ABA/PGT Publishing, 1976.

Table 9: Allowable Stress Numbers for Case Hardened Steel Gear Materials

Hardness at Surface	Allowable Bending Stress Number		Allowable Contact Stress Number	
	Grade 1 (Ksi) (MPa)	Grade 2 (Ksi) (MPa)	Grade 1 (Ksi) (MPa)	Grade 2 (Ksi) (MPa)
Flame or Induction Hardened:				
50 HRC	45 (310)		170	1200
54 HRC		55 (380)	175	1200
Carburized and Case Hardened:				
55–64 HRC	55 (380)		180	1250
58–64 HRC		65 (450)		225 (1560)
Nitrided AISI 4140:				
84.5 15N	34 (230)	45 (310)	155	1100
Nitrided AISI 4340:				
83.5 15N	36 (250)	47 (325)	150	1050
Nitrided Nitralloy 135M: ^a				
90.0 15N	38 (260)	48 (330)	170	1170
Nitrided Nitralloy N: ^a				
90.0 15N	40 (280)	50 (345)	195	1340
			205	1410

Table 10: Suggested Application Factor K_a

Power Source	Driven Machine		
	Uniform	Light Shock	Moderate Shock
Uniform	1.00	1.25	1.50
Light shock	1.20	1.40	1.75
Moderate shock	1.30	1.70	2.00
			2.75

Table 11: Suggested Size Factor K_s

Diametral Pitch, P _d	Metric Module, m	Size Factor K _s
≥5	≤5	1.00
4	6	1.05
3	8	1.15
2	12	1.25
1.25	20	1.40

Table 12 Allowable Stress Numbers for Iron and Bronze Gear Materials

Material Designation	Hardness at Surface (HB)	Allowable Bending Stress Number		Allowable Contact Stress Number	
		(Ksi)	(MPa)	(Ksi)	(MPa)
Gray Cast Iron—ASTM A48					
Class 20	—	5	35	50	340
Class 30	175	8.5	59	65	450
Class 40	200	13	90	75	520
Nodular (Ductile) Iron—ASTM A536					
60-14-18	140	22	150	77	530
80-55-06	180	22	150	77	530
100-70-03	230	27	180	92	630
120-90-02	270	31	210	103	710
Malleable Iron—ASTM A220					
45007	165	10	70	72	500
50005	180	13	90	78	540
53007	195	16	110	83	570
80002	240	21	145	94	650
Tin Bronze—UNS No. 90700—$s_{u\min} = 40$ ksi (275 MPa)					
Bronze 2 (Former)	—	5.7	40	30	200
Aluminum Bronze—UNS No. 95400—$s_{u\min} = 90$ ksi (620 MPa)					
ALBR 3 (Former)	—	23.6	160	65	450

Table 13: Basic Coefficient C_p

Pinion Material	Modulus of Elasticity E_p (lb/in ²) (MPa)	Gear Material and Modulus of Elasticity E_G , lb/in ² (MPa)					
		Malleable Iron		Cast Iron		Aluminum Bronze	
		Steel	Iron	Iron	Iron	Bronze	Bronze
Steel	30×10^6 (2×10^5)	2 300 (191)	2 180 (181)	2 160 (179)	2 100 (174)	1 950 (162)	1 900 (158)
Mall. iron	25×10^6 (1.7×10^5)	2 180 (181)	2 090 (174)	2 070 (172)	2 020 (168)	1 900 (158)	1 850 (154)
Nod. iron	24×10^6 (1.7×10^5)	2 160 (179)	2 070 (172)	2 050 (170)	2 000 (166)	1 880 (156)	1 830 (152)
Cast iron	22×10^6 (1.5×10^5)	2 100 (174)	2 020 (168)	2 000 (166)	1 960 (163)	1 850 (154)	1 800 (149)
Al. bronze	17.5×10^6 (1.2×10^5)	1 950 (162)	1 900 (158)	1 880 (156)	1 850 (154)	1 750 (145)	1 700 (141)
Tin bronze	16×10^6 (1.1×10^5)	1 900 (158)	1 850 (154)	1 830 (152)	1 800 (149)	1 700 (141)	1 650 (137)

Note: Poisson's ratio = 0.30; Units for C_p are (lb/in²)^{1/2} or (MPa)^{1/2}.Source: Extracted from AGMA Standard 2001-B88, *Fundamental Rating Factors and Calculation Methods for Involute Spur and Helical Gear Teeth*, with the permission of the publisher, American Gear Manufacturers Association, 1509 King Street, Suite 201, Alexandria, Va. 22314.

Table 14: Selected Values for Total Composite Tolerance

AGMA Quality Number	Diametral Pitch P_d	Number of Gear Teeth				
		20	40	60	100	200
Q5	2	0.026 0	0.029 0	0.032 0	0.035 0	0.041 0
	8	0.012 0	0.013 0	0.014 0	0.015 0	0.017 0
	20	0.007 4	0.008 0	0.008 5	0.009 2	0.010 0
	32	0.006 0	0.006 4	0.006 8	0.007 3	0.008 0
Q8	2	0.009 4	0.011 0	0.012 0	0.013 0	0.015 0
	8	0.004 3	0.004 7	0.005 0	0.005 5	0.006 2
	20	0.002 7	0.002 9	0.003 1	0.003 4	0.003 7
	32	0.002 2	0.002 3	0.002 5	0.002 7	0.002 9
Q10	2	0.004 8	0.005 4	0.005 9	0.006 6	0.007 6
	8	0.002 2	0.002 4	0.002 6	0.002 8	0.003 2
	20	0.001 4	0.001 5	0.001 6	0.001 7	0.001 9
	32	0.001 1	0.001 2	0.001 3	0.001 4	0.001 5
Q12	2	0.002 5	0.002 8	0.003 0	0.003 4	0.003 9
	8	0.001 1	0.001 2	0.001 3	0.001 4	0.001 6
	20	0.000 71	0.000 77	0.000 81	0.000 87	0.000 97
	32	0.000 57	0.000 60	0.000 64	0.000 69	0.000 76
Q14	2	0.001 3	0.001 4	0.001 5	0.001 7	0.002 0
	8	0.000 57	0.000 62	0.000 67	0.000 73	0.000 82
	20	0.000 36	0.000 39	0.000 41	0.000 45	0.000 50
	32	0.000 29	0.000 31	0.000 33	0.000 35	0.000 39

Table 15: Recommended AGMA Quality Numbers

Application	Quality Number	Application	Quality Number
Cement mixer drum drive	3-5	Small power drill	7-9
Cement kiln	5-6	Clothes washing machine	8-10
Steel mill drives	5-6	Printing press	9-11
Grain harvester	5-7	Computing mechanism	10-11
Cranes	5-7	Automotive transmission	10-11
Punch press	5-7	Radar antenna drive	10-12
Mining conveyor	5-7	Marine propulsion drive	10-12
Paper-box-making machine	6-8	Aircraft engine drive	10-13
Gas meter mechanism	7-9	Gyroscope	12-14
<i>Machine Tool Drives and Drives for Other High-Quality Mechanical Systems</i>			
Pitch Line Speed (fpm)	Quality Number	Pitch Line Speed (m/s)	Quality Number
0-800	6-8	0-4	
800-2 000	8-10	4-11	
2 000-4 000	10-12	11-22	
Over 4 000	12-14	Over 22	

Table 16 Geometry Factors for Pitting Resistance, I , for Helical Gears with 20° Normal Pressure Angle and Standard Addendum

Gear Teeth	Pinion Teeth (helix angle $\psi = 15.0^\circ$)				
	17	21	26	35	55
17	0.124				
21	0.139	0.128			
26	0.154	0.143	0.132		
35	0.175	0.165	0.154	0.137	
55	0.204	0.196	0.187	0.171	0.143
135	0.244	0.241	0.237	0.229	0.209

Gear Teeth	Pinion Teeth (helix angle $\psi = 25.0^\circ$)				
	14	17	21	26	35
14	0.123				
17	0.137	0.126			
21	0.152	0.142	0.130		
26	0.167	0.157	0.146	0.134	
35	0.187	0.178	0.168	0.156	0.138
55	0.213	0.207	0.199	0.189	0.173
135	0.248	0.247	0.244	0.239	0.230
					0.210

Table 17 Load Distribution Factors for Bevel Gears, K_m

Type of Gearing	Both Gears Straddle-mounted	One Gear Straddle-mounted	Neither Gear Straddle-mounted
General commercial quality	1.44	1.58	1.80
High-quality commercial gearing	1.20	1.32	1.50

Table 18 Approximate Lewis Form Factor for Worm Gear Teeth

ϕ_a	y
14½°	0.100
20°	0.125
25°	0.150
30°	0.175

Table 19: Geometry Factor for Pitting-Resistance, I , for Helical 25° Normal Pressure Angle and Standard Addendum

Gear Teeth	Pinion Teeth (helix angle $\psi = 15.0^\circ$)				
	14	17	21	26	35
14	0.130				
17	0.144	0.133			
21	0.160	0.149	0.137		
26	0.175	0.165	0.153	0.140	
35	0.195	0.186	0.175	0.163	0.143
55	0.222	0.215	0.206	0.195	0.178
135	0.257	0.255	0.251	0.246	0.236

Gear Teeth	Pinion Teeth (helix angle $\psi = 25.0^\circ$)				
	12	14	17	21	26
12	0.129				
14	0.141	0.132			
17	0.155	0.146	0.135		
21	0.170	0.162	0.151	0.138	
26	0.185	0.177	0.166	0.154	0.141
35	0.203	0.197	0.188	0.176	0.163
55	0.227	0.223	0.216	0.207	0.196
135	0.259	0.258	0.255	0.251	0.246

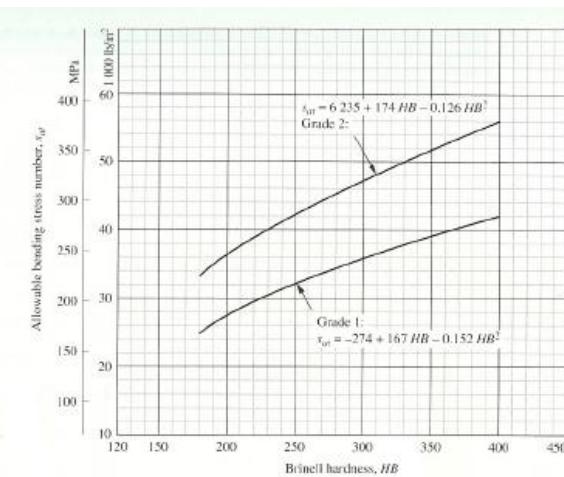


Figure 1: Allowable Bending Stress Number for Steel Gears

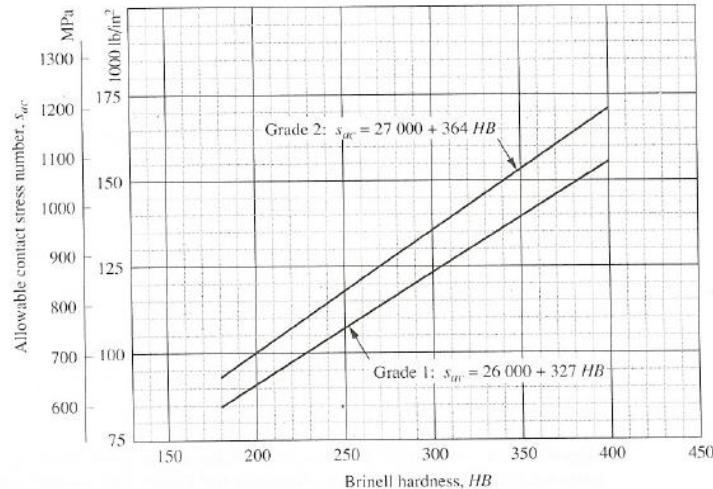


Figure 2: Allowable Contact Stress Number for Steel Gears,

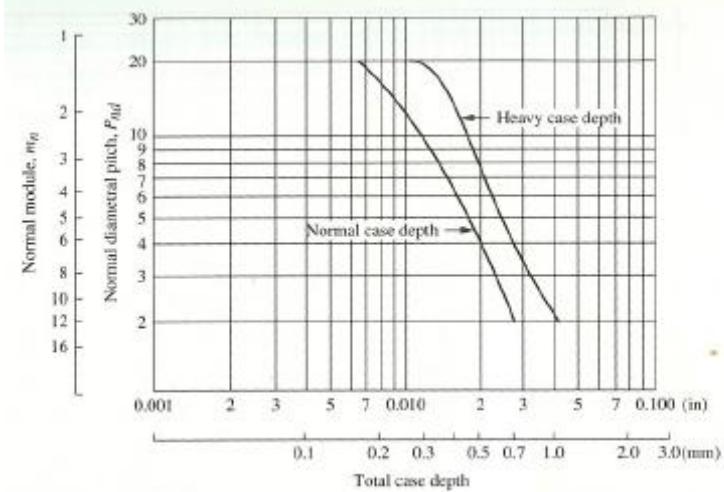


Figure 4: Recommended Case Depth for Nitrided Gears,

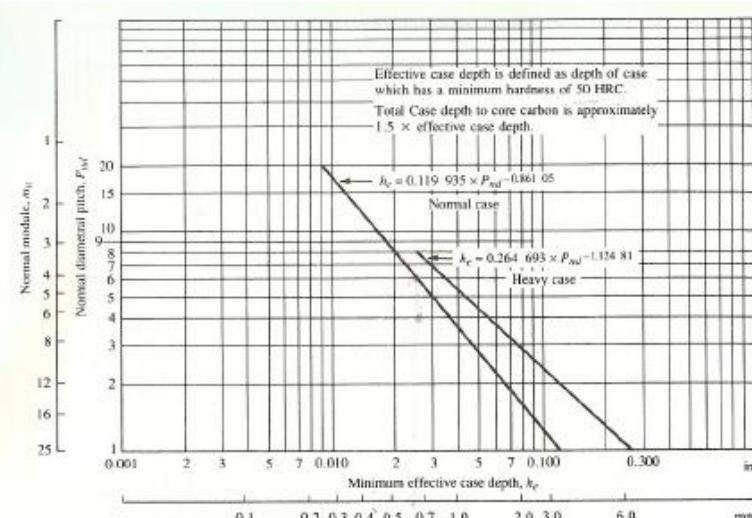


Figure 3: Effective Case Depth for Carburized Gears,

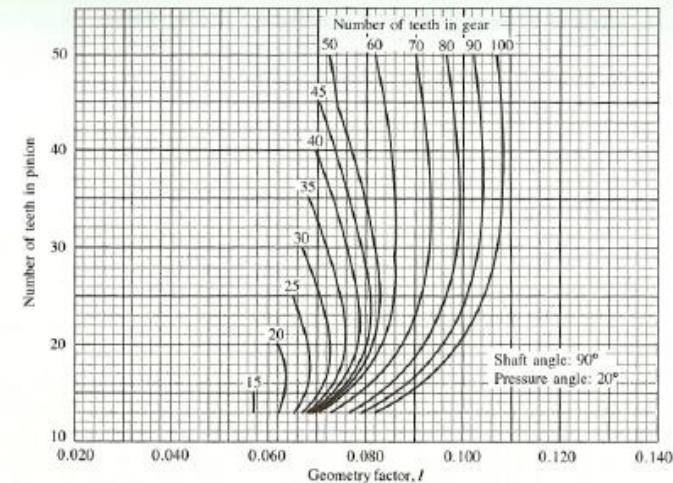


Figure 5 Geometry Factors for Straight and Bevel Gears

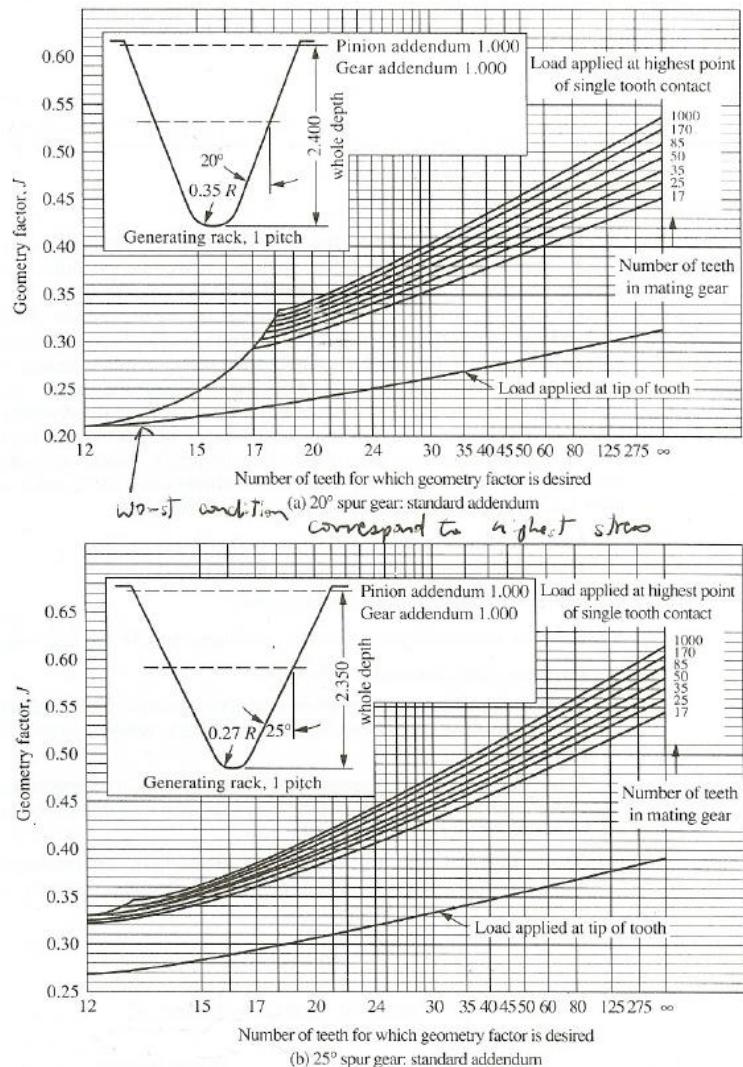


Figure 6: Geometry Factor, (Extracted from AGMA Standard for Rating the Pitting Resistance and Bending Strength of Spur and Helical Involute Gear Teeth, AGMA 218.01

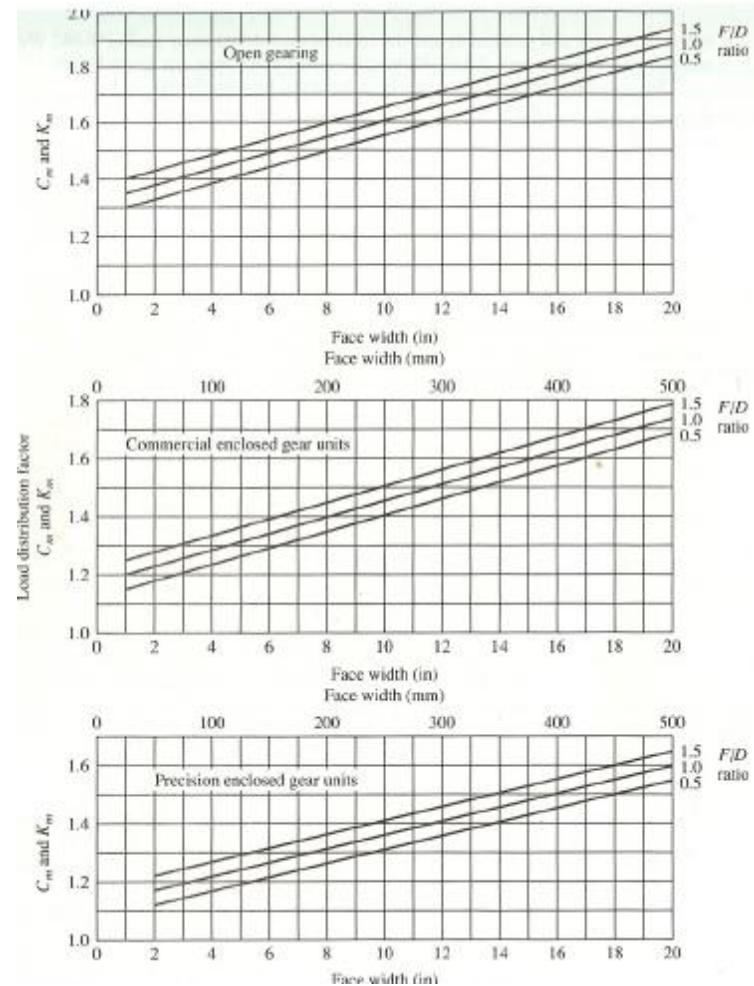
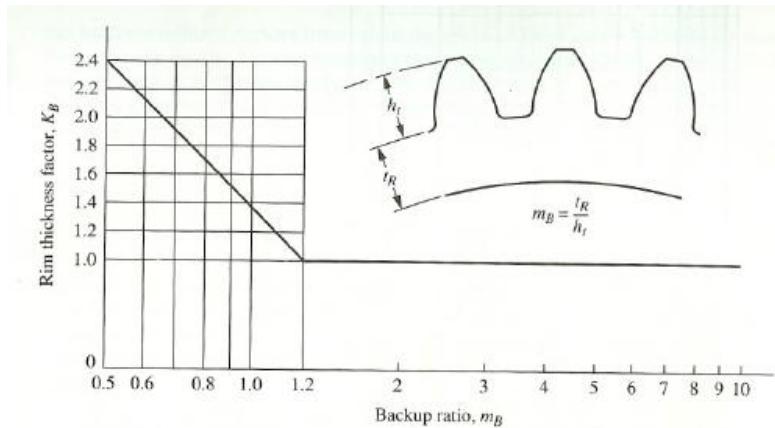
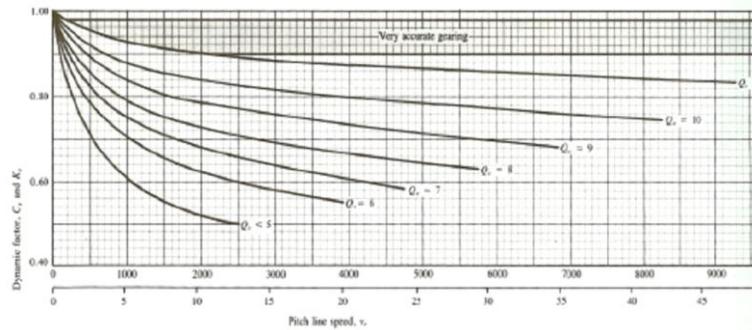
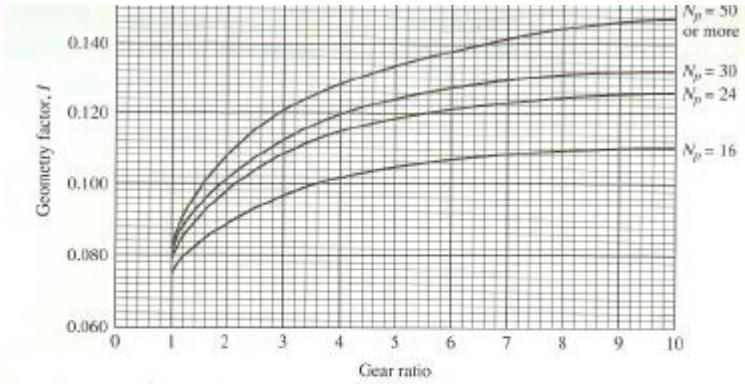
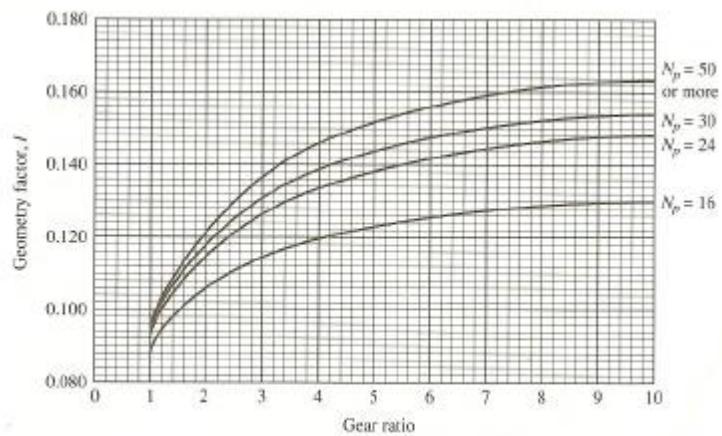


Figure 7: Load Distribution Factor, K_m and C_m

Figure 8 Rim Thickness Factor, K_B Figure 9: Dynamic Factor C_v and K_v (a) 20° pressure angle, full depth teeth (standard addendum = $1/P_d$)(b) 25° pressure angle full depth teeth (standard addendum = $1/P_d$)Figure 10: External Spur Pinion Geometry Factor, I , for Standard Center Distances. All curves are for the lowest point of single tooth contact on the pinion.

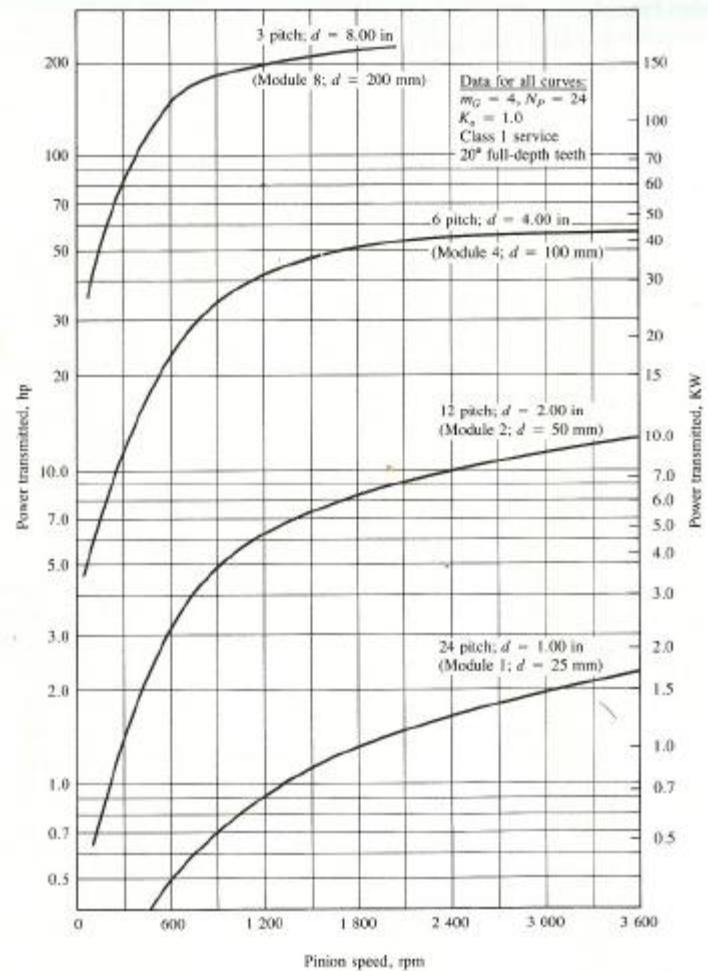
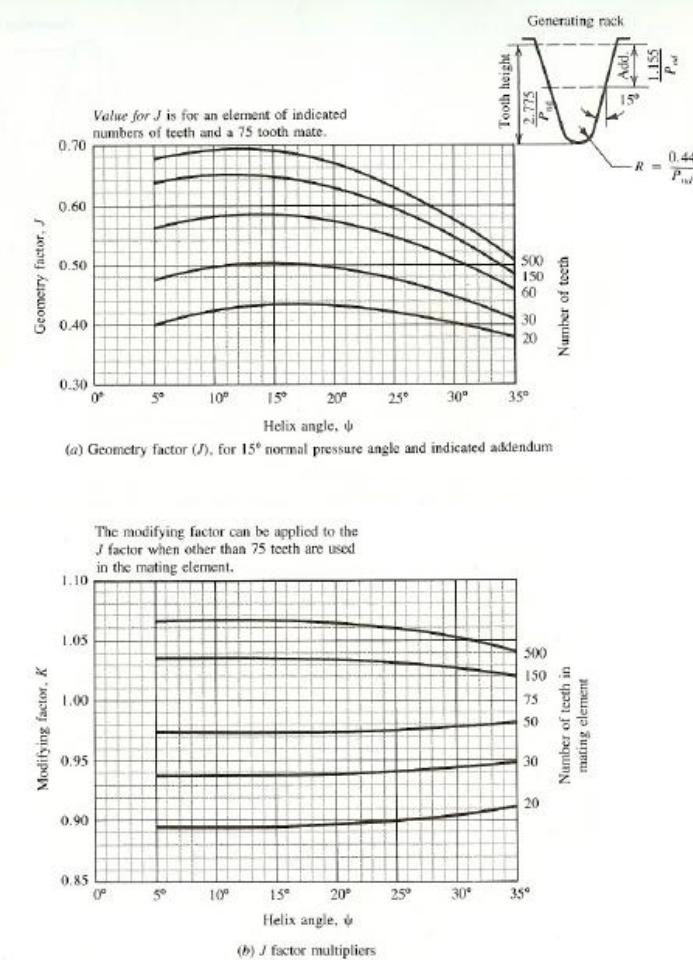
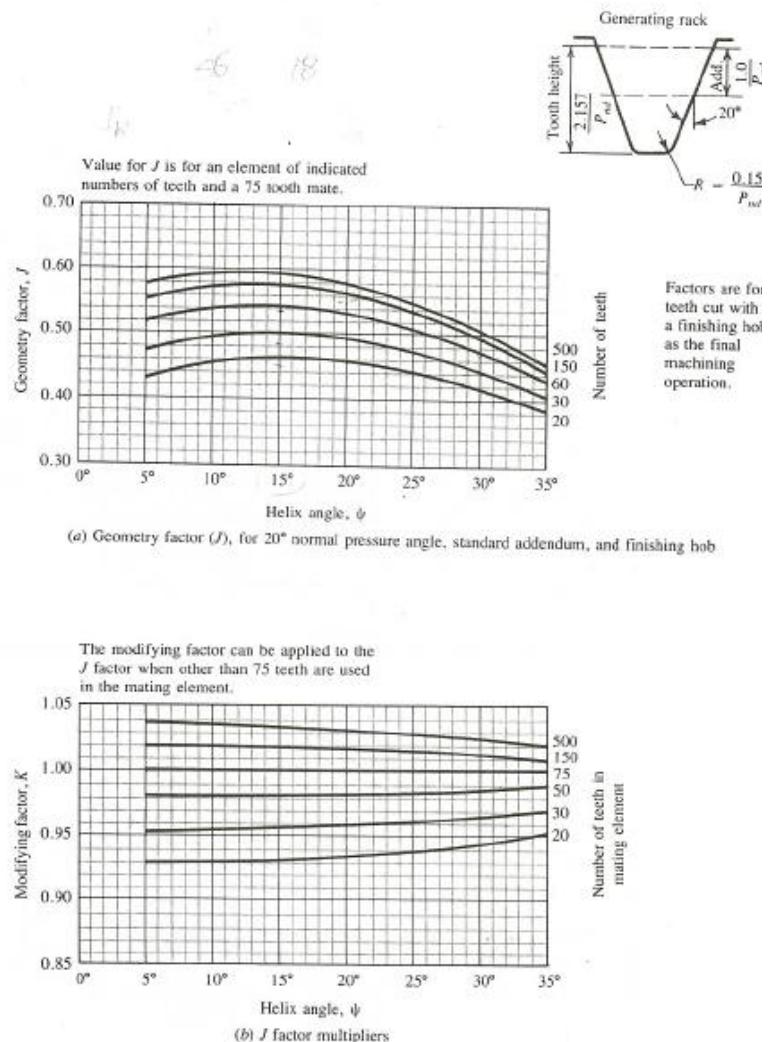
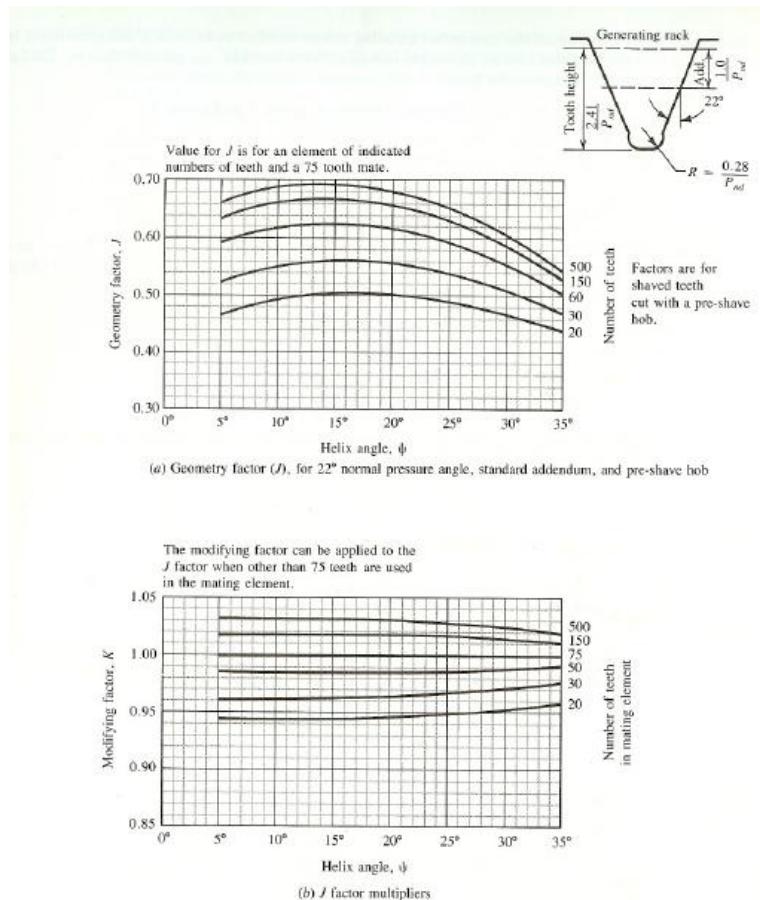


Figure 11: Power vs. Pinion Speed

Figure 12: Geometry Factor J for 15° Normal Pressure Angle

Figure 13: Geometry Factor J for 20° Normal Pressure AngleFigure 14: Geometry Factor J for 22° Normal Pressure Angle

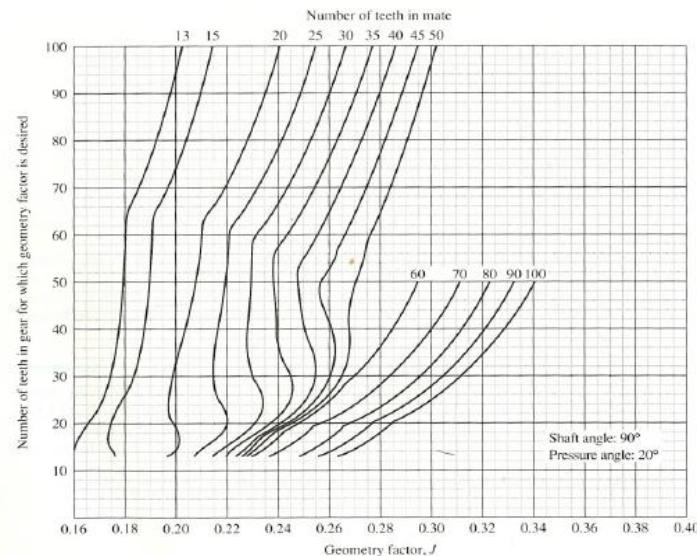


Figure 15 Geometry Factor, I , for Straight Bevel Gears with 20° Pressure Angle and $0.120/P_d$ Tool Edge Radius

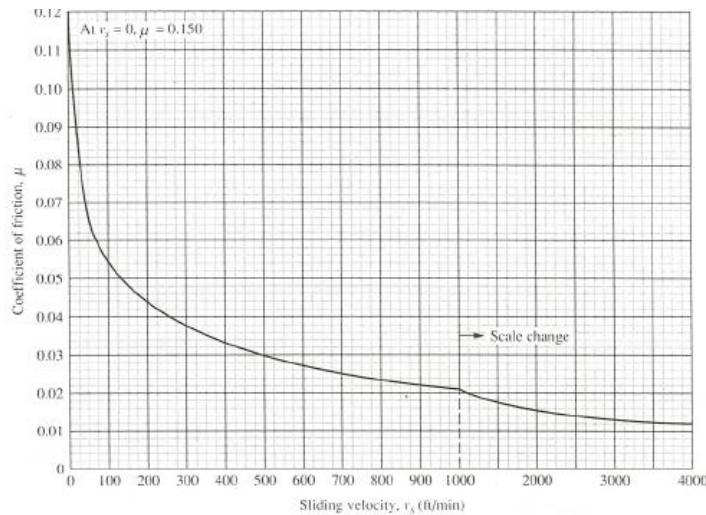


Figure 16 Coefficient of Friction vs. Sliding Velocity for Steel Worm and Bronze Worm Gear

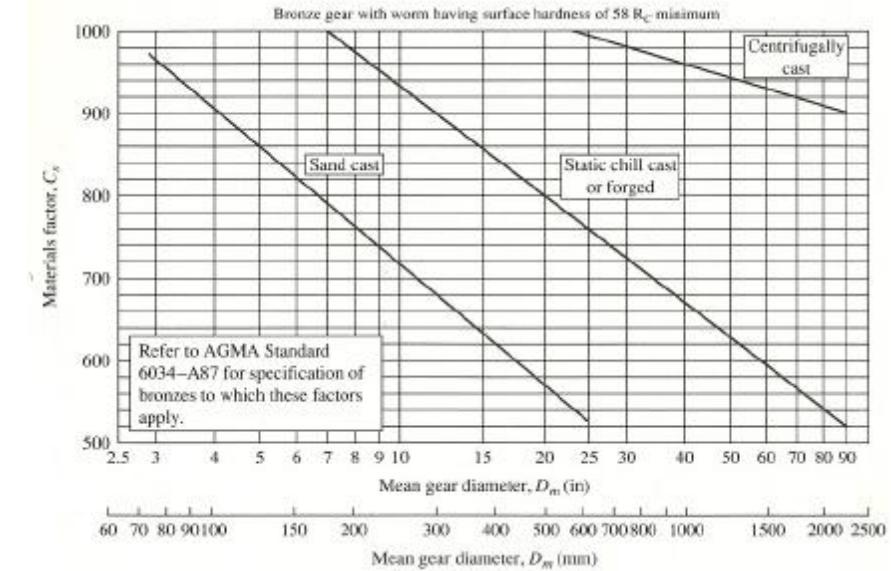


Figure 17 Materials Factor, C_s , for Center Distance > 3.0 in (76 mm) (,

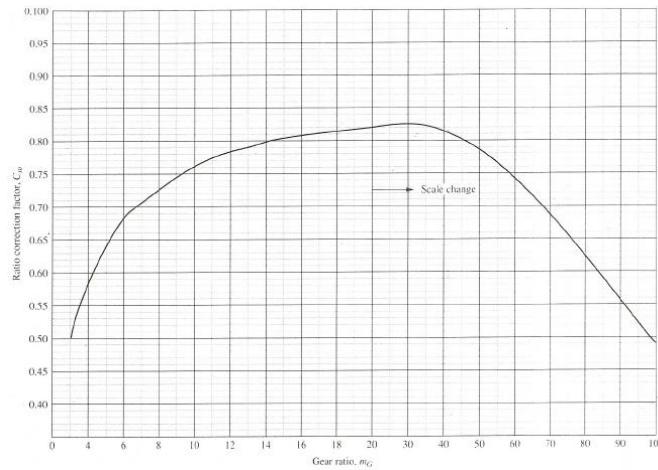


Figure B18 Ratio Correction Factor, C_m , vs. Gear Ratio, m_G

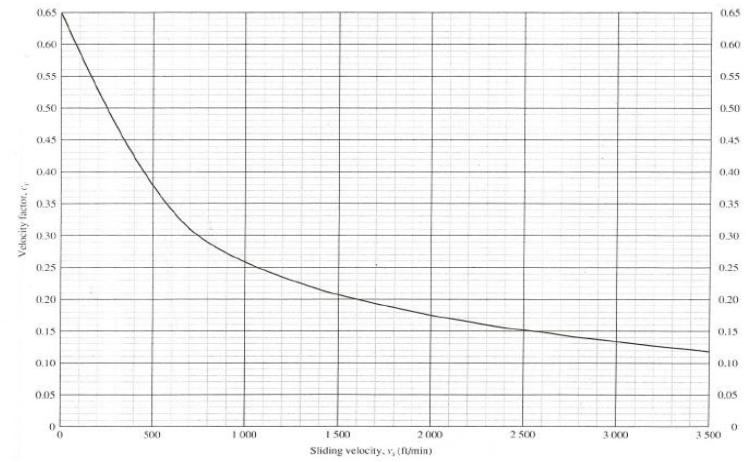


Figure B19 Velocity Factor, C_v , vs. Sliding Velocity