### Lecture 11 - MOSFET (III)

### MOSFET Equivalent Circuit Models

March 13, 2003

#### **Contents**:

- 1. Low-frequency small-signal equivalent circuit model
- 2. High-frequency small-signal equivalent circuit model

### Reading assignment:

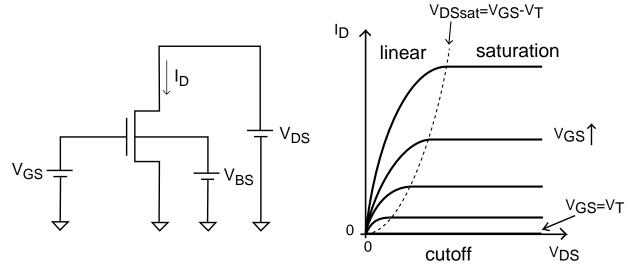
Howe and Sodini, Ch.  $4, \S 4.5-4.6$ 

### **Key questions**

- What is the topology of a small-signal equivalent circuit model of the MOSFET?
- What are the key dependencies of the leading model elements in saturation?

# 1. Low-frequency small-signal equivalent circuit model

Regimes of operation of MOSFET:



• Cut-off:

$$I_D = 0$$

• Linear:

$$I_D = \frac{W}{L} \mu_n C_{ox} (V_{GS} - \frac{V_{DS}}{2} - V_T) V_{DS}$$

• Saturation:

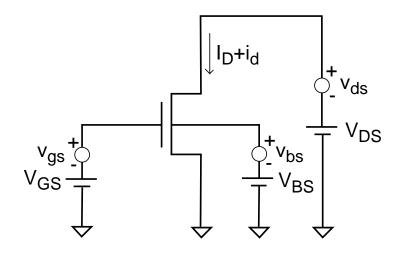
$$I_{D} = I_{Dsat} = \frac{W}{2L} \mu_{n} C_{ox} (V_{GS} - V_{T})^{2} [1 + \lambda (V_{DS} - V_{DSsat})]$$

Effect of back bias:

$$V_T(V_{BS}) = V_{To} + \gamma(\sqrt{-2\phi_p - V_{BS}} - \sqrt{-2\phi_p})$$

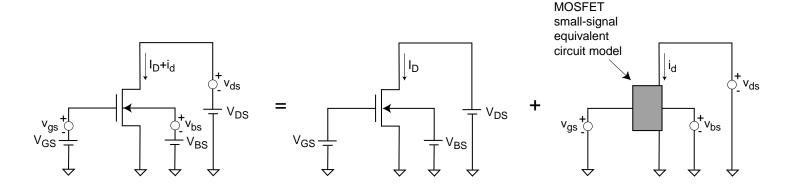
### Small-signal device modeling

In many applications, interested in response of device to a *small-signal* applied on top of bias:



### Key points:

- Small-signal is *small* 
  - $\Rightarrow$  response of non-linear components becomes linear
- Can separate response of MOSFET to bias and small signal.
- Since response is linear, superposition can be used
   ⇒ effects of different small signals are independent
  from each other



Mathematically:

$$i_D(V_{GS}+v_{gs},V_{DS}+v_{ds},V_{BS}+v_{bs}) \simeq$$

$$I_D(V_{GS}, V_{DS}, V_{BS}) + \frac{\partial I_D}{\partial V_{GS}}|_{Q} v_{gs} + \frac{\partial I_D}{\partial V_{DS}}|_{Q} v_{ds} + \frac{\partial I_D}{\partial V_{BS}}|_{Q} v_{bs}$$

where  $Q \equiv bias\ point\ (V_{GS}, V_{DS}, V_{BS})$ 

Small-signal  $i_d$ :

$$i_d \simeq g_m v_{gs} + g_o v_{ds} + g_{mb} v_{bs}$$

Define:

 $g_m \equiv transconductance [S]$   $g_o \equiv output \text{ or } drain \text{ } conductance [S]$  $g_{mb} \equiv backgate \text{ } transconductance [S]$ 

Then:

$$\left|g_{m} \simeq \frac{\partial I_{D}}{\partial V_{GS}}\right|_{Q} \quad \left|g_{o} \simeq \frac{\partial I_{D}}{\partial V_{DS}}\right|_{Q} \quad \left|g_{mb} \simeq \frac{\partial I_{D}}{\partial V_{BS}}\right|_{Q}$$

### $\square$ Transconductance

In saturation regime:

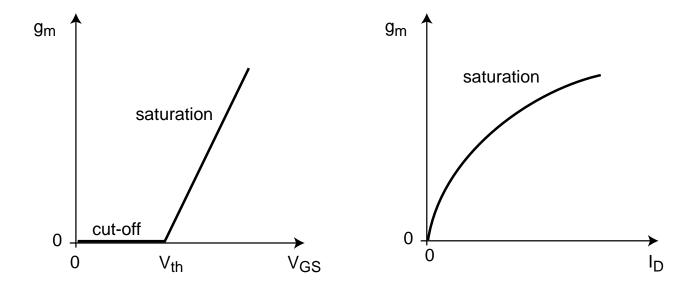
$$I_D = \frac{W}{2L} \mu_n C_{ox} (V_{GS} - V_T)^2 [1 + \lambda (V_{DS} - V_{DSsat})]$$

Then (neglecting channel length modulation):

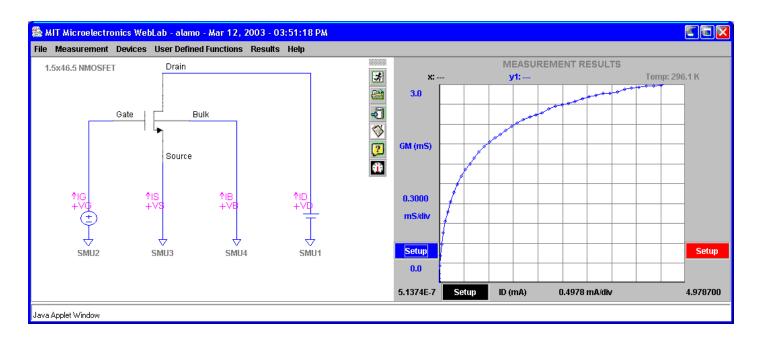
$$g_m = \frac{\partial I_D}{\partial V_{GS}}|_Q \simeq \frac{W}{L} \mu_n C_{ox} (V_{GS} - V_T)$$

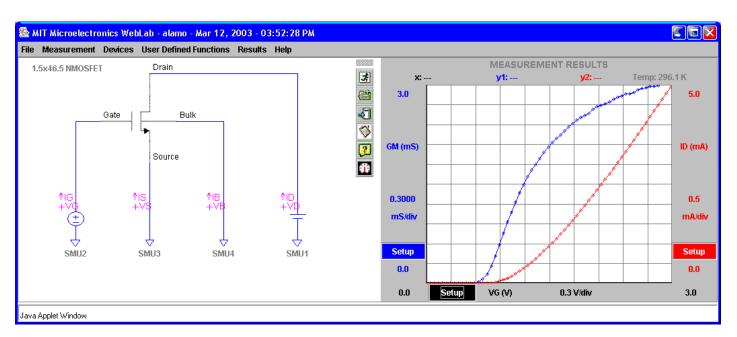
Rewrite in terms of  $I_D$ :

$$g_m = \sqrt{2\frac{W}{L}\mu_n C_{ox} I_D}$$

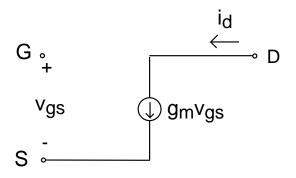


# Transconductance of $1.5 \times 46.5 \mu m$ nMOSFET ( $V_{DS} = 3 V$ ):





### Equivalent circuit model representation of $g_m$ :



В.

### □ Output conductance

In saturation regime:

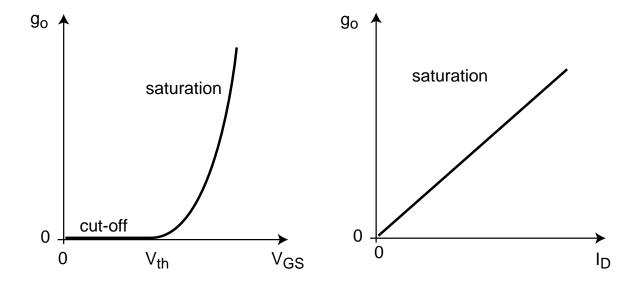
$$I_D = \frac{W}{2L} \mu_n C_{ox} (V_{GS} - V_T)^2 [1 + \lambda (V_{DS} - V_{DSsat})]$$

Then:

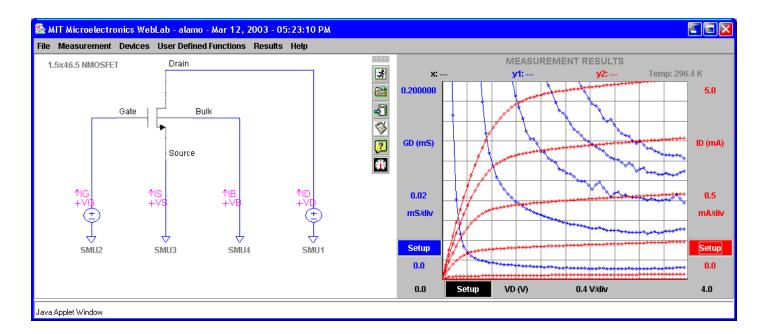
$$g_o = \frac{\partial I_D}{\partial V_{DS}}|_Q = \frac{W}{2L} \mu_n C_{ox} (V_{GS} - V_T)^2 \lambda \simeq \lambda I_D \propto \frac{I_D}{L}$$

Output resistance is inverse of output conductance:

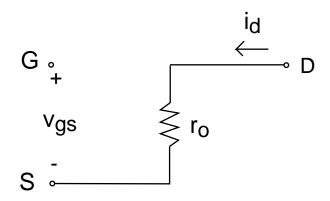
$$r_o = \frac{1}{g_o} \propto \frac{L}{I_D}$$



### Output conductance of $1.5 \times 46.5 \mu m$ nMOSFET:



Equivalent circuit model representation of  $g_o$ :



В.

### □ Backgate transconductance

In saturation regime (neglect channel-length modulation):

$$I_D \simeq \frac{W}{2L} \mu_n C_{ox} (V_{GS} - V_T)^2$$

Then:

$$g_{mb} = \frac{\partial I_D}{\partial V_{BS}}|_Q = \frac{W}{L} \mu_n C_{ox} (V_{GS} - V_T) (-\frac{\partial V_T}{\partial V_{BS}}|_Q)$$

Since:

$$V_T(V_{BS}) = V_{To} + \gamma(\sqrt{-2\phi_p - V_{BS}} - \sqrt{-2\phi_p})$$

Then:

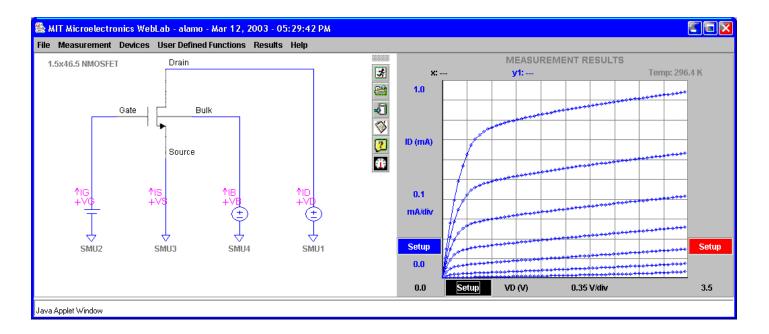
$$\frac{\partial V_T}{\partial V_{BS}}|_Q = \frac{-\gamma}{2\sqrt{-2\phi_p - V_{BS}}}$$

All together:

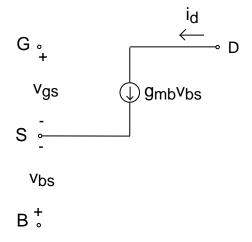
$$g_{mb} = \frac{\gamma g_m}{2\sqrt{-2\phi_p - V_{BS}}}$$

 $g_{mb}$  inherits all dependencies of  $g_m$ 

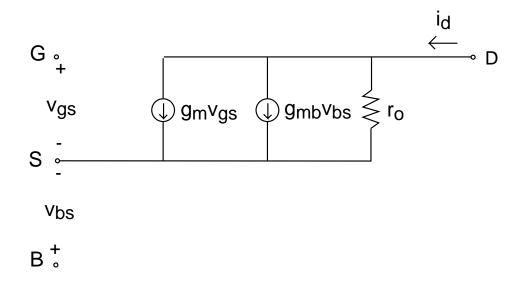
Body of MOSFET is a true gate: output characteristics for different values of  $V_{BS}$  ( $V_{BS} = 0 - (-3) V$ ,  $\Delta V_{BS} = -0.5 V$ ,  $V_{GS} = 1.5 V$ ):



Equivalent circuit model representation of  $g_{mb}$ :

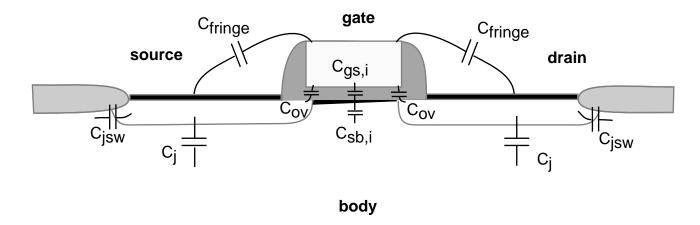


Complete MOSFET small-signal equivalent circuit model for low frequency:



# 2. High-frequency small-signal equivalent circuit model

Need to add capacitances. In saturation:



$$C_{gs} \equiv \text{intrinsic gate capacitance} + \text{overlap capacitance}, C_{ov} (+\text{fringe})$$

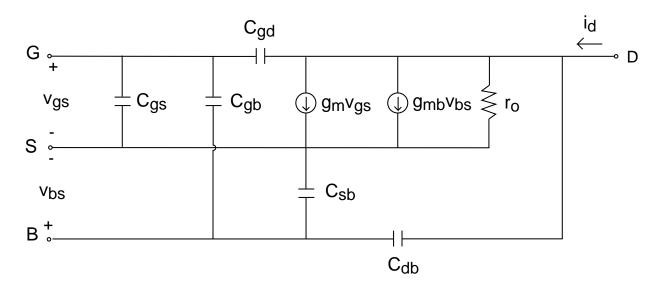
$$C_{gd} \equiv \text{overlap capacitance}, C_{ov}$$
 (+fringe)

$$C_{gb} \equiv \text{(only parasitic capacitance)}$$

$$C_{sb} \equiv \text{source junction depletion capacitance} + \text{sidewall}(+\text{channel-substrate capacitance})$$

$$C_{db} \equiv \text{drain junction depletion capacitance} + \text{sidewall}$$

Complete MOSFET high-frequency small-signal equivalent circuit model:



Plan for development of capacitance model:

- Start with  $C_{gs,i}$ 
  - compute gate charge  $Q_G = -(Q_N + Q_B)$
  - compute how  $Q_G$  changes with  $V_{GS}$
- Add pn junction capacitances

### Inversion layer charge in saturation

$$Q_N(V_{GS}) = W \int_0^L Q_n(y) dy = W \int_0^{V_{GS}-V_T} Q_n(V_c) \frac{dy}{dV_c} dV_c$$

But:

$$\frac{dV_c}{dy} = -\frac{I_D}{W\mu_n Q_n(V_c)}$$

Then:

$$Q_N(V_{GS}) = -\frac{W^2 L \mu_n}{I_D} \int_0^{V_{GS} - V_T} Q_n^2(V_c) dV_c$$

Remember:

$$Q_n(V_c) = -C_{ox}(V_{GS} - V_c - V_T)$$

Then:

$$Q_N(V_{GS}) = -\frac{W^2 L \mu_n C_{ox}^2}{I_D} \int_0^{V_{GS} - V_T} (V_{GS} - V_c - V_T)^2 dV_c$$

Do integral, substitute  $I_D$  in saturation and get:

$$Q_N(V_{GS}) = -\frac{2}{3}WLC_{ox}(V_{GS} - V_T)$$

Gate charge:

$$Q_G(V_{GS}) = -Q_N(V_{GS}) - Q_{B,max}$$

Intrinsic gate-to-source capacitance:

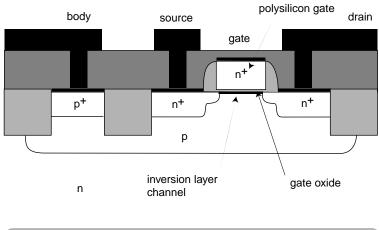
$$C_{gs,i} = \frac{dQ_G}{dV_{GS}} = \frac{2}{3}WLC_{ox}$$

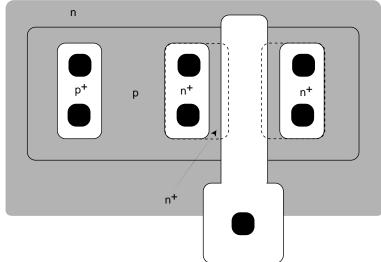
Must add overlap capacitance:

$$C_{gs} = \frac{2}{3}WLC_{ox} + WC_{ov}$$

Gate-to-drain capacitance - only overlap capacitance:

$$C_{qd} = WC_{ov}$$





Body-to-source capacitance = source junction capacitance:

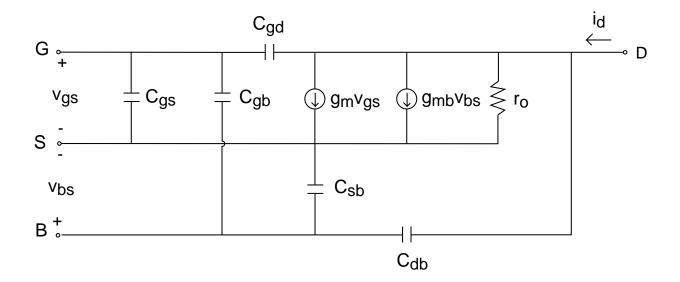
$$C_{sb} = C_j + C_{jsw} = WL_{diff} \sqrt{\frac{q\epsilon_s N_a}{2(\phi_B - V_{BS})}} + (2L_{diff} + W)C_{JSW}$$

Body-to-drain capacitance = drain junction capacitance:

$$C_{db} = C_j + C_{jsw} = WL_{diff} \sqrt{\frac{q\epsilon_s N_a}{2(\phi_B - V_{BD})}} + (2L_{diff} + W)C_{JSW}$$

### **Key conclusions**

High-frequency small-signal equivalent circuit model of MOSFET:



In saturation:

$$g_m \propto \sqrt{\frac{W}{L}I_D}$$

$$g_o \propto \frac{I_D}{L}$$

$$C_{gs} \propto WLC_{ox}$$