

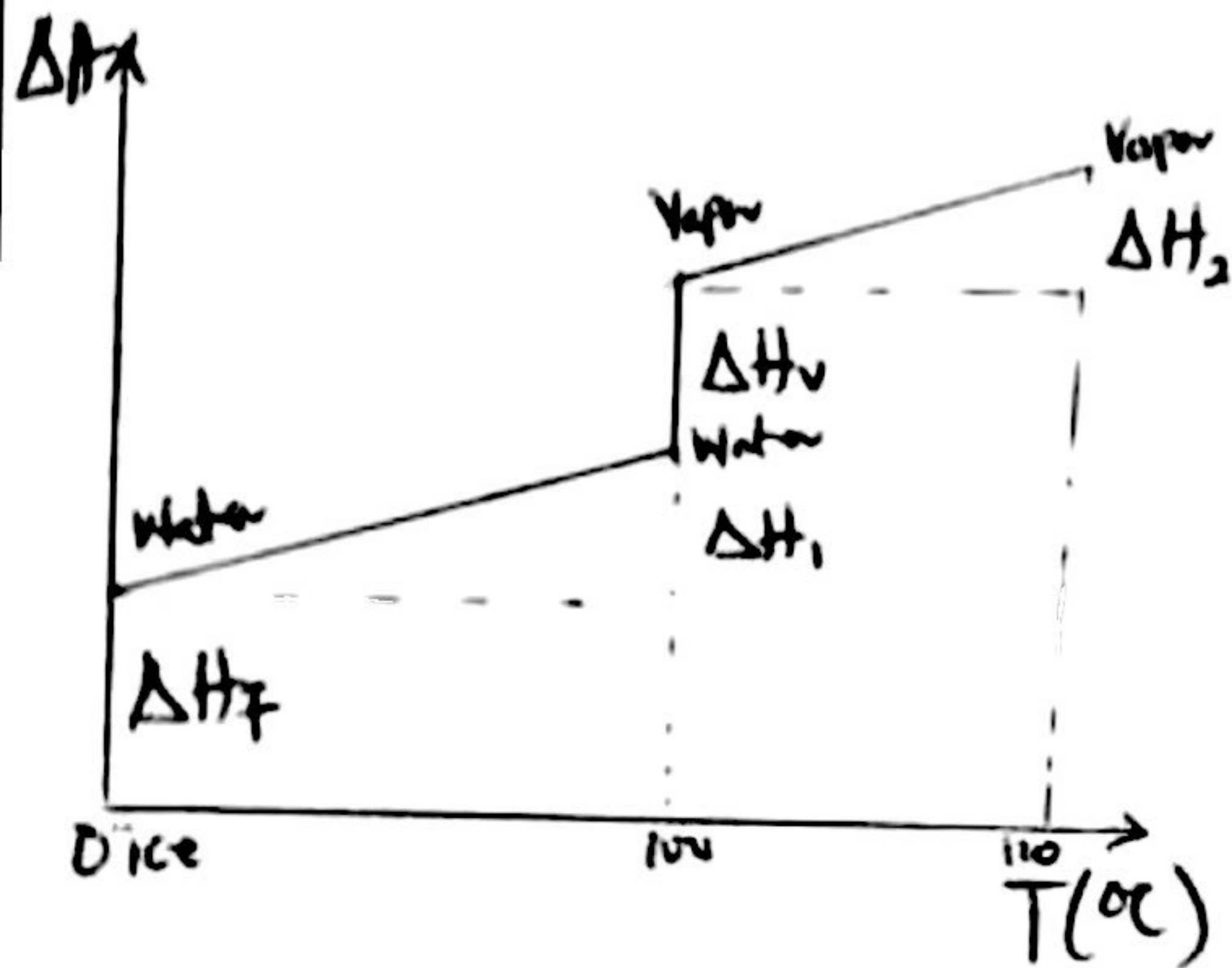
Calculate the enthalpy change of 1 kg of water from ice at  $0^\circ\text{C}$  to vapor at  $120^\circ\text{C}$  and pressure of 100 kPa. Express your answer in kJ/kg.

Data  $\Delta \hat{H}_f = 335 \text{ J/g}$  at  $0^\circ\text{C}$ , 101.3 kPa  
 $\Delta \hat{H}_v = 2256 \text{ J/g}$  at  $100^\circ\text{C}$ , 101.3 kPa

$$C_p(\text{Liq, H}_2\text{O}) = 18.296 + 47.212 \times 10^{-2}T - 133.88 \times 10^{-5}T^2 + 1314 \times 10^{-9}T^3$$

$$C_p(\text{Vap, H}_2\text{O}) = 23.46 + 0.688 \times 10^{-2}T + 0.7604 \times 10^{-5}T^2 - 3.593 \times 10^{-9}T^3$$

$$C_p = \left[ \frac{\text{J}}{\text{gmol} \cdot \text{K}} \right]$$



Soln

$$\Delta H_1 = \int_{273.15}^{373.15} (18.296 + 47.212 \times 10^{-2}T - 133.88 \times 10^{-5}T^2 + 1314 \times 10^{-9}T^3) dT$$

$$\therefore \Delta H_1 = 7534.33 \frac{\text{J}}{\text{gmol}}$$

$$\Delta H_2 = \int_{373.15}^{393.15} (23.46 + 0.688 \times 10^{-2}T + 0.7604 \times 10^{-5}T^2 - 3.593 \times 10^{-9}T^3) dT$$

$$\therefore \Delta H_2 = 740.21 \frac{\text{J}}{\text{gmol}}$$

$$\Delta H_{\text{total}} = \Delta H_f + n \Delta H_1 + \Delta H_v + n \Delta H_2$$

$$\therefore \Delta \hat{H}_f = 335 \frac{\text{J}}{\text{g}} = 335 \frac{\text{kJ}}{\text{kg}}$$

$$\Delta \hat{H}_v = 2256 \frac{\text{J}}{\text{g}} = 2256 \frac{\text{kJ}}{\text{kg}}$$

$$\therefore \Delta H = \int_{T_1}^{T_2} C_p dT$$

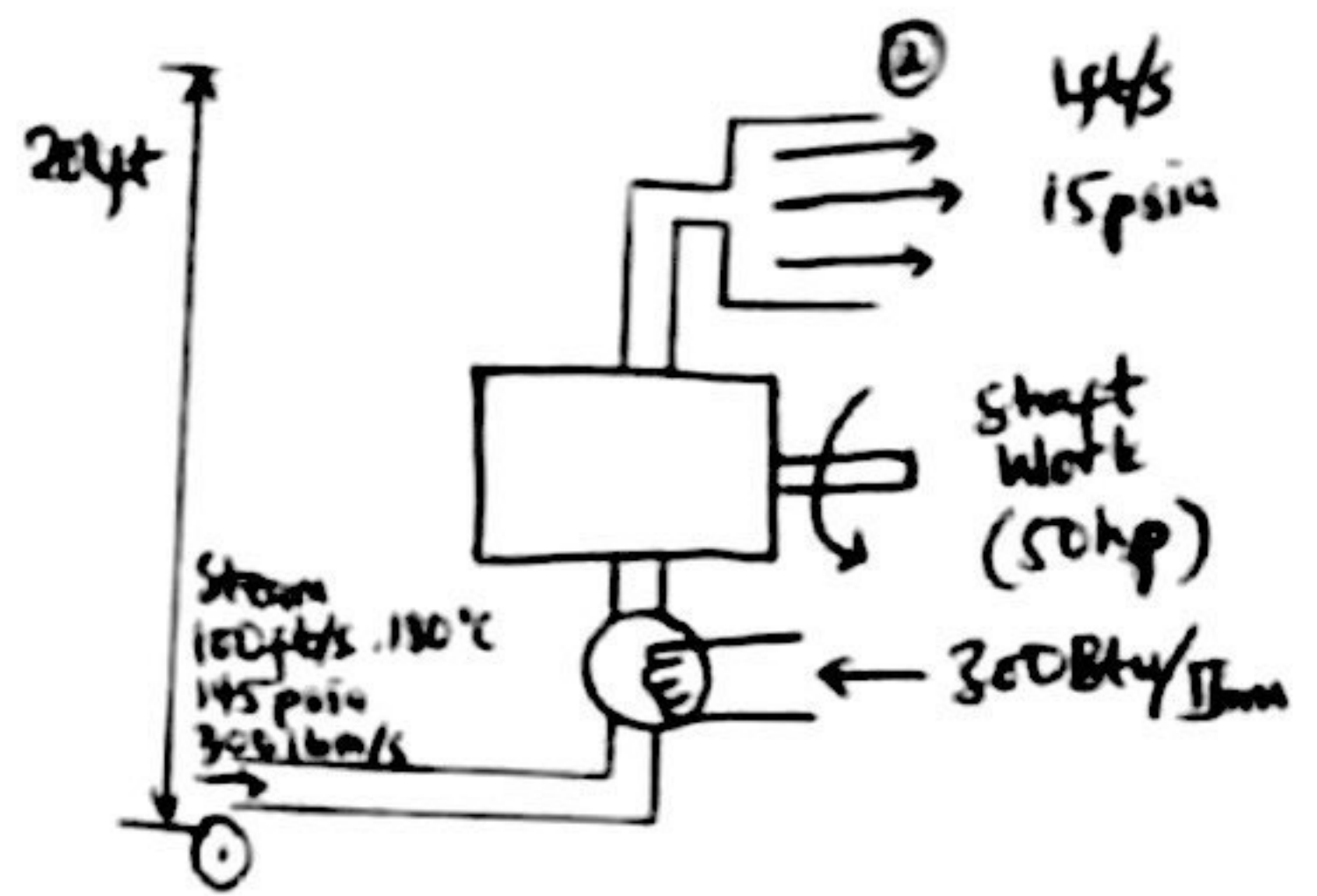
$$\therefore \Delta H_{\text{total}} = 335 \frac{\text{kJ}}{\text{kg}} + \left( 7534.33 \frac{\text{J}}{\text{gmol}} \times \frac{55.6 \text{ gmol}}{1 \text{ kg}} \right) + 2256 \frac{\text{kJ}}{\text{kg}} + \left( 740.21 \frac{\text{J}}{\text{gmol}} \times \frac{55.6 \text{ gmol}}{1 \text{ kg}} \right)$$

$$\therefore \Delta H_{\text{total}} = 335 \frac{\text{kJ}}{\text{kg}} + 418.91 \frac{\text{kJ}}{\text{kg}} + 2256 \frac{\text{kJ}}{\text{kg}} + 41.16 \frac{\text{kJ}}{\text{kg}}$$

$$\therefore \Delta H_{\text{total}} = 3051.07 \frac{\text{kJ}}{\text{kg}}$$



Question 3  
 Superheated steam is expanded through a turbine of 50 horse power and finally exits through a diffuser at 50 psia and a velocity  $1 \text{ ft/s}$ . The elevation change is 200 ft. Calculate the outlet temperature assuming negligible pressure drop due to friction and inlet steam flow of 300 lb/hr.



General Energy Balance:

$$\Delta U + \Delta E_k + \Delta E_p = Q - W$$

$$\Delta U + \Delta E_k + \Delta E_p = Q - (P\Delta V + W_k)$$

$$\Delta U + P\Delta U + \Delta E_k + \Delta E_p = Q - W_k$$

$$\Delta H + \Delta E_k + \Delta E_p = Q - W_k$$

$$\therefore Q = 300 \frac{\text{Btu}}{\text{lbm}} \left| \frac{1055.06 \text{ J}}{1 \text{ Btu}} \right| \left| \frac{1 \text{ lbm}}{0.454 \text{ kg}} \right|$$

$$Q = 697.176 \frac{\text{kJ}}{\text{kg}} \left| \frac{0.454 \text{ kg}}{1 \text{ lbm}} \right| \left| \frac{300 \text{ lbm}}{\text{s}} \right| = 92503.8 \text{ kW}$$

$$\therefore W_s = 50 \text{ hp} \left| \frac{735.50 \text{ W}}{1 \text{ hp}} \right| = 36.78 \frac{\text{kJ}}{\text{s}}$$

$$V_1 = 100 \frac{\text{ft}}{\text{s}} = 30.48 \frac{\text{m}}{\text{s}}$$

$$V_2 = 1 \frac{\text{ft}}{\text{s}} = 0.3048 \frac{\text{m}}{\text{s}}$$

$$\Delta E_k = \frac{1}{2} m (V_2^2 - V_1^2)$$

$$m = 300 \frac{\text{lbm}}{\text{s}} = 136.2 \frac{\text{kg}}{\text{s}}$$

$$\Delta E_k = \frac{1}{2} \times 136.2 \times (0.3048^2 - 30.48^2) = -63.26 \text{ kW}$$

$$H = 200 \text{ ft} = 60.96 \text{ m}$$

$$\Delta E_p = m g H$$

$$\therefore m = 136.2 \frac{\text{kg}}{\text{s}}, g = 9.81 \text{ m/s}^2$$

Soln

$$\Delta E_p = 136.2 \frac{\text{kg}}{\text{s}} \times 9.81 \frac{\text{m}}{\text{s}^2} \times 60.96 \text{ m}$$

$$\Delta E_p = 81.45 \text{ kW}$$

$$\therefore \Delta H = Q - W_k - \Delta E_k - \Delta E_p$$

$$\Delta H = 92503.8 - 36.78 - (-63.26) - 81.45$$

$$\therefore \Delta H = 92448.8 \text{ kW}$$

$$\therefore \Delta H = m (H_2 - H_1)$$

From steam tables:

$$H_1 (\text{superheated steam @ } 180^\circ\text{C}, 145 \text{ psia}) =$$

$$H_1 = 2776.2 \frac{\text{kJ}}{\text{kg}}$$

$$\therefore H_2 = \frac{\Delta H}{m} + H_1$$

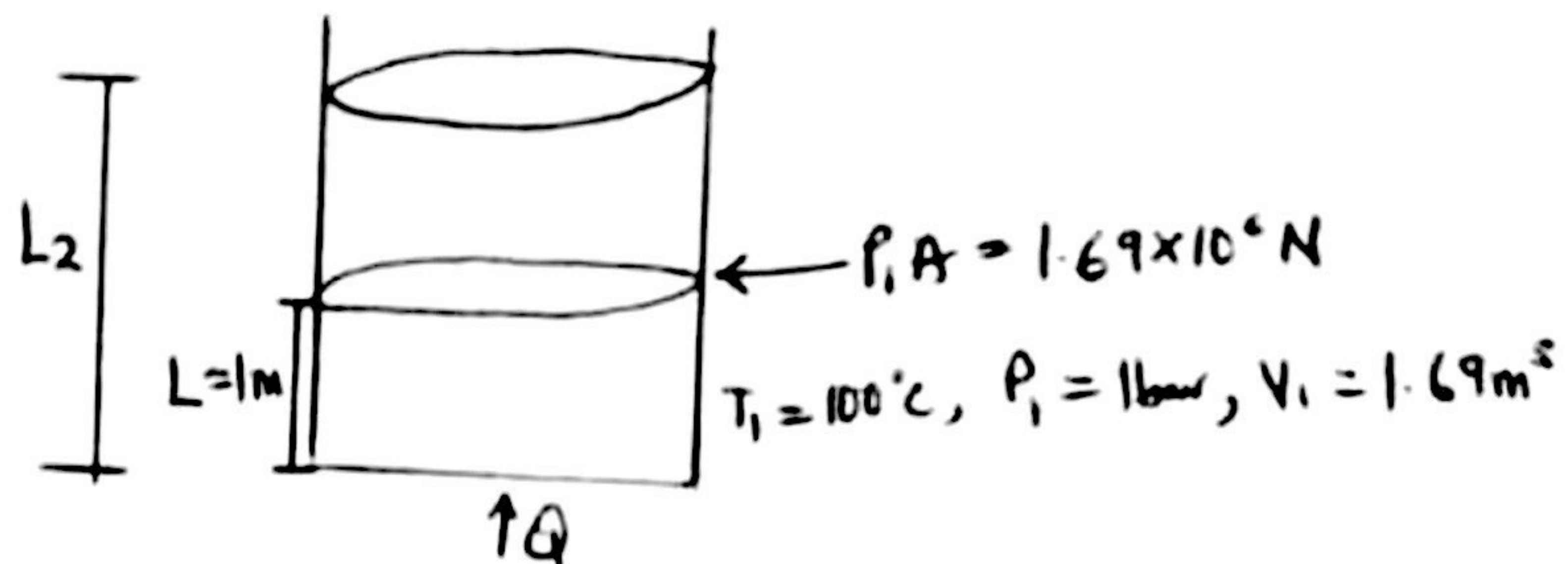
$$H_2 = \frac{92448.8 \text{ kW}}{136.2 \text{ kg/s}} + 2776.2 \frac{\text{kJ}}{\text{kg}}$$

$$H_2 = 3454.97 \frac{\text{kJ}}{\text{kg}}$$

From steam tables,  $H_2$  (enthalpy of outlet) corresponds to approximately  $484^\circ\text{C}$  for superheated steam @ 15 psia.



1 kg steam at a pressure 1 bar contained in a cylinder of cross-sectional area  $1.69 \text{ m}^2$ . The cylinder is heated externally to raise the temperature to  $300^\circ\text{C}$ . Assume no heat loss to the environment. Calculate the amount of heat required for the process. Apply steam tables.



Soln

General Energy Balance:

$$\Delta \hat{U} + \Delta \hat{E}_k + \Delta \hat{E}_p = \hat{Q} - \hat{W}$$

Kinetic energy is negligible  $\therefore \Delta \hat{E}_k = 0$

$$\therefore \Delta \hat{U} + \Delta \hat{E}_p = \hat{Q} - \hat{W}$$

For compressive or expansive systems,  
 $\hat{W} = P \Delta V + W_s$

$$\therefore \Delta \hat{U} + \Delta \hat{E}_p = \hat{Q} - P \Delta V - W_s$$

$$\Delta \hat{U} + P \Delta V + \Delta \hat{E}_p = \hat{Q} - W_s$$

$$\Delta \hat{H} + \Delta \hat{E}_p = \hat{Q} - W_s$$

No shaft work  $\therefore W_s = 0$

$$\therefore \Delta \hat{H} + \Delta \hat{E}_p = \hat{Q}$$

$$\Delta \hat{E}_p = g h = \Delta \hat{E}_p$$

$$= 9.81 \text{ m/s}^2 \times 1 \text{ m} = 9.81 \text{ m}^2/\text{s}^2$$

$$= 9.81 \text{ J}$$

$$\therefore \Delta \hat{H} = H_2 - H_1$$

From steam tables:

$$H_2 \text{ (saturated steam @ } 300^\circ\text{C, 1 bar)} \\ = 3074 \frac{\text{kJ}}{\text{kg}}$$

$$H_1 \text{ (saturated steam @ } 100^\circ\text{C, 1 bar)} \\ = 2676 \frac{\text{kJ}}{\text{kg}}$$

$$\therefore \Delta \hat{H} + \Delta \hat{E}_p = \hat{Q}$$

$$(3074 - 2676) \frac{\text{kJ}}{\text{kg}} + 9.81 \times 10^{-3} \frac{\text{kJ}}{\text{kg}} = \hat{Q}$$

$$398 \frac{\text{kJ}}{\text{kg}} + 9.81 \times 10^{-3} \frac{\text{kJ}}{\text{kg}} = \hat{Q}$$

$$\therefore \hat{Q} = 398.01 \frac{\text{kJ}}{\text{kg}}$$

398.01 kJ/kg