

Power Electronics :-

controlling and conversion of Electric power

→ Motor

→ AC ↔ DC

→ Batt. charger

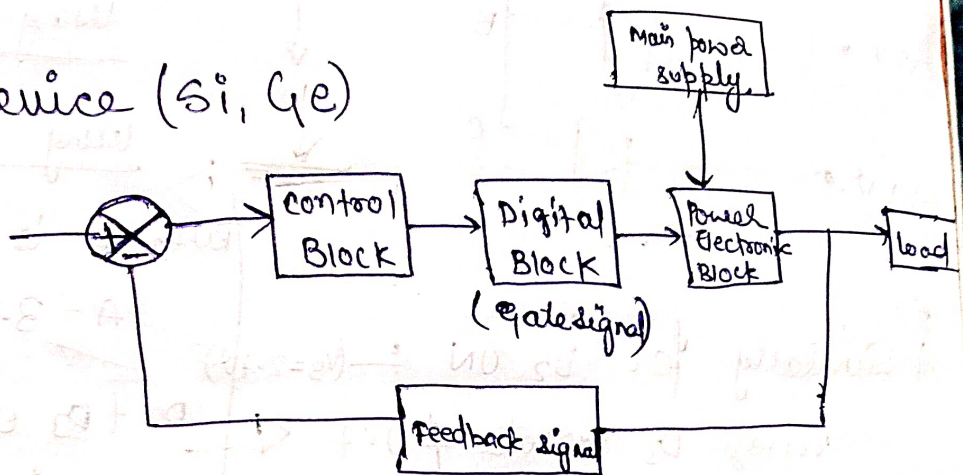
uses semiconductor device (Si, Ge)

→ Diode

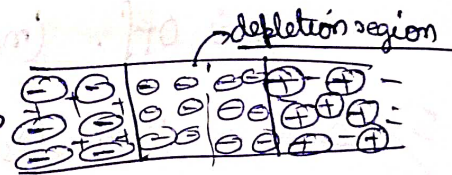
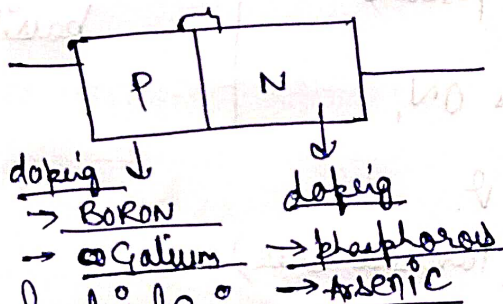
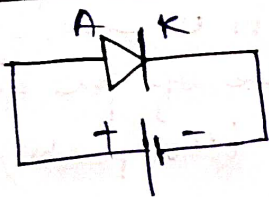
→ SCR / Thyristor

→ MOSFET

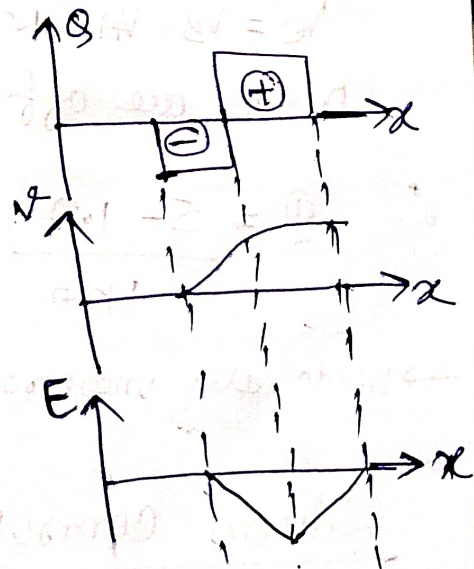
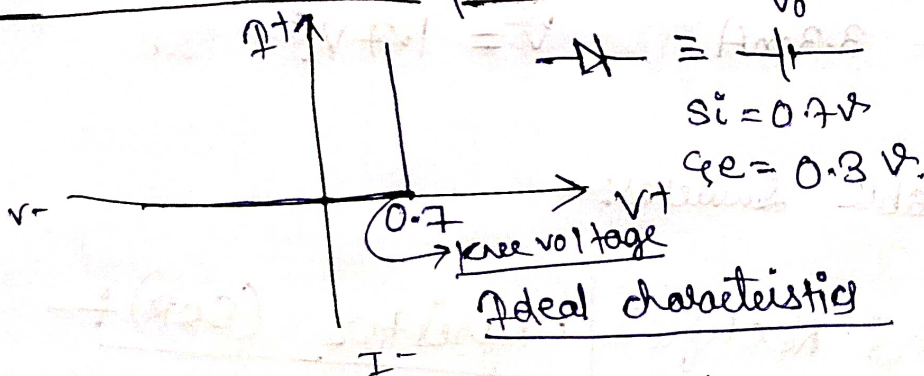
→ BJT



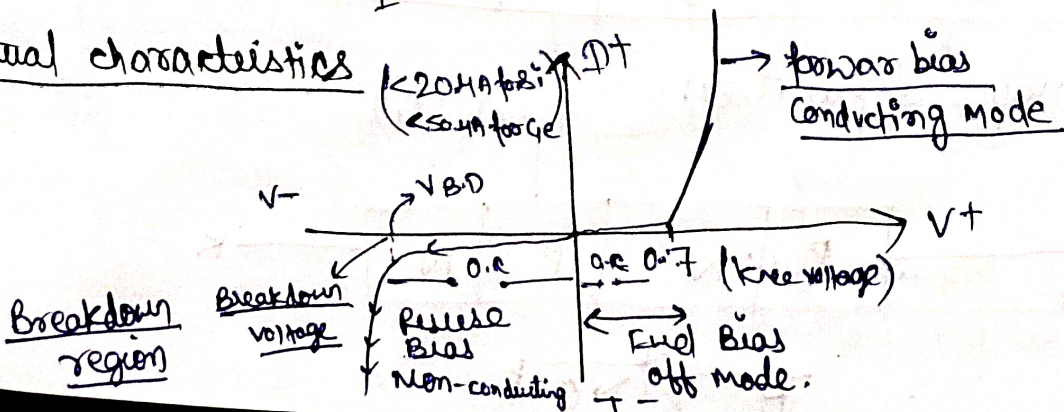
Diodes :-

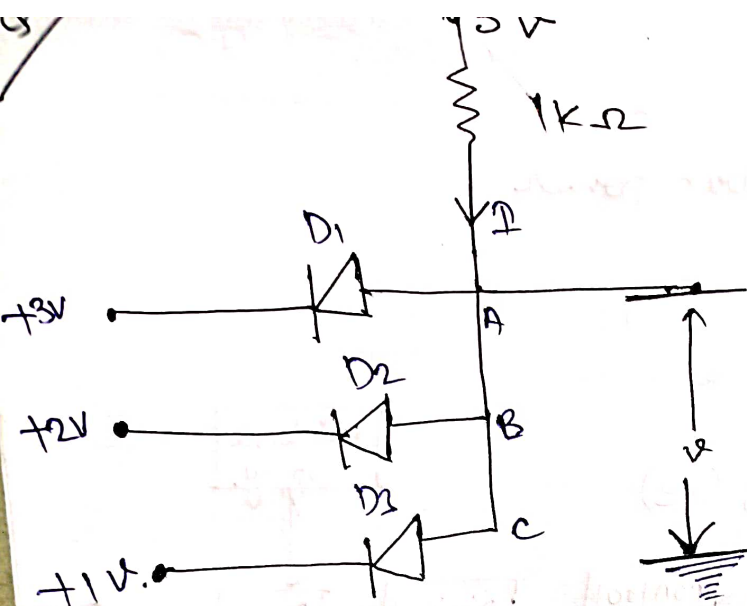


V-I characteristics of diode :-



Actual characteristics





Find V & I ?

~~using O.C test~~

using S.C test

When D_1 is ON :-

$$V_A = 3.7 = V_B = V_C = 3.7V$$

2) Similarly for D_2 ON :- ($V_B = 2.7V$)
 voltage D_3 violate $\neq 0.7V$
 $\uparrow D_1$ is off. (not possible)

D_2 & D_3 ON & voltage across them
 is $1.7 + 2.7V$ which is not
 possible (as it is equal to $0.7V$ is
 case of fwd bias)
 (not possible)

3) case III \rightarrow when D_3 is ON,

$$V_C = V_B = V_A = 1.7V$$

D_1 & D_2 are off (Possible case)

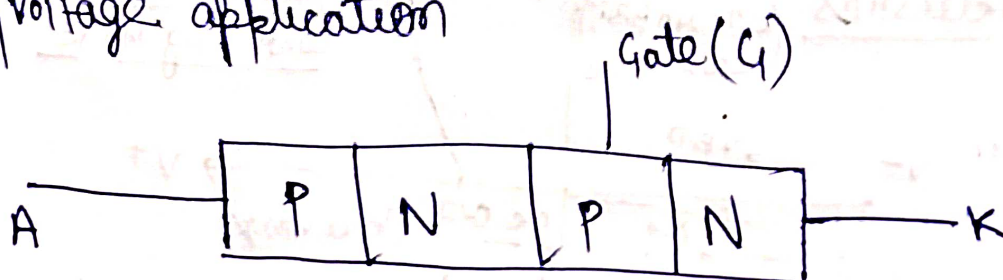
$$\therefore I = \frac{5 - 1.7}{1k\Omega} = 3.3mA$$

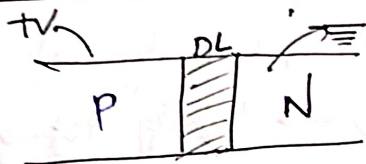
$$V = 1.7V$$

\rightarrow Diode are uncontrollable switches:-

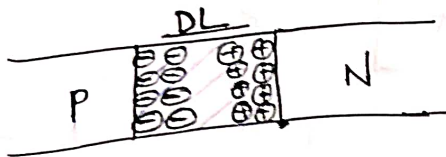
Silicon Controlled Rectifier / Thyristor (SCR) :-

\rightarrow High current / voltage application

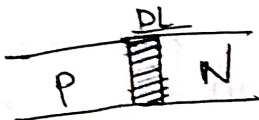




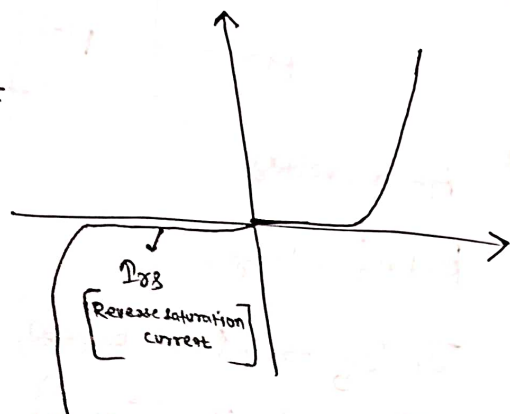
equilibrium
 $V=0$



$V < 0$



$V > 0$



I_{rs} depends on - Applied voltage
(very little for $V > V_{BD}$)

→ temperature (strongly dependent)

→ due to increase in free charge carriers (e^- -holes pair formation)

$$I_f = I_{rs} (e^{\frac{qV}{kT}} - 1)$$

$\eta = 1$ (assume)

$$\frac{kT}{q} = V_T = \text{constant at given temp.} = 26 \text{ mV}$$

$$I_f = I_{rs} \left(e^{\frac{V_f}{V_T}} - 1 \right)$$

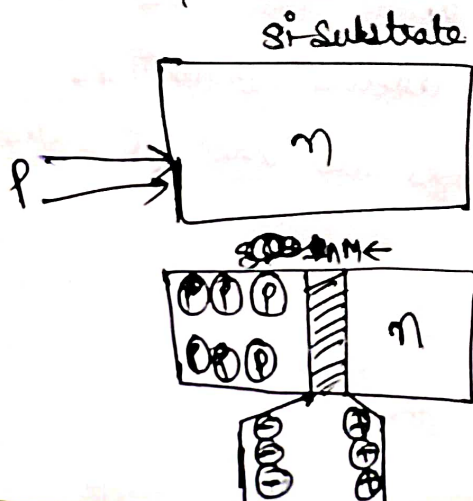
$$\frac{dI_f}{dV_f} = \frac{I_{rs}}{V_T} \times e^{\frac{V_f}{V_T}}$$

$$\frac{dV_f}{dI_f} = \frac{V_T}{I_{rs}} e^{-\frac{V_f}{V_T}} = r_{ac} \rightarrow \text{dynamic resistance}$$

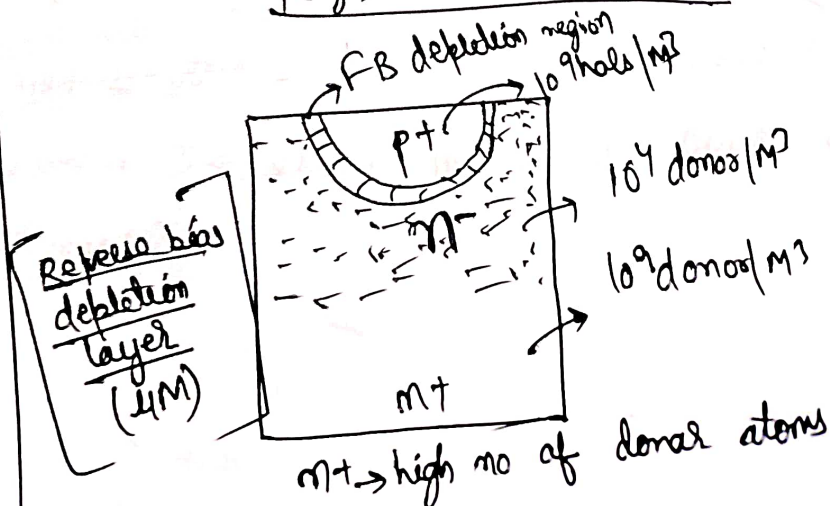
Q. A P-N junction diode has a reverse saturation current 50 nA at 32° . What I_f ? If $V_f = 0.5 \text{ V}$ & assume $V_T = 26 \text{ mV}$.

Ans 11.24 A

low power diode



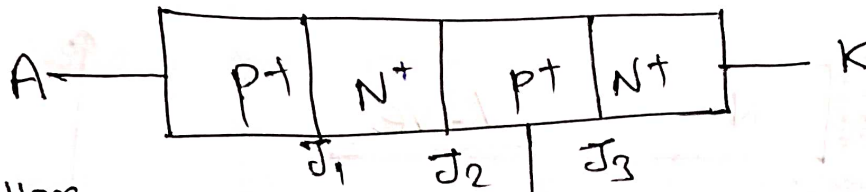
High Power diode



SCR Thyristor

⊕ → heavily doped.

⊖ → lightly doped.



A (-ve) voltage

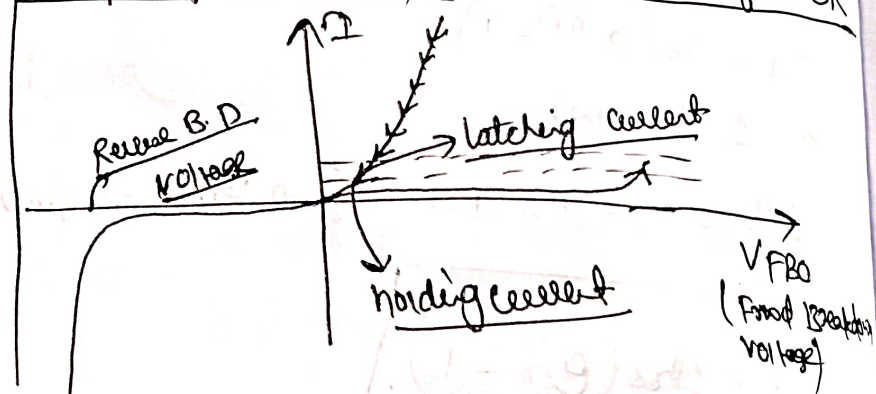
K (+ve) voltage.

$J_1, J_3 \rightarrow$ (Fwd biased)

$J_2 \rightarrow$ (Rev biased)

G (gate terminal)

V_T - char of SCR

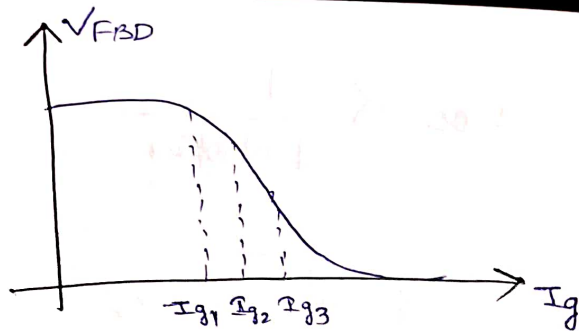


→ The latching current is minimum value of anode current which must be reached during turn on process to maintain conduction.

→ Holding current is the minimum value of holding anode current below which if it falls the device will turn off.

Modes of SCR :-

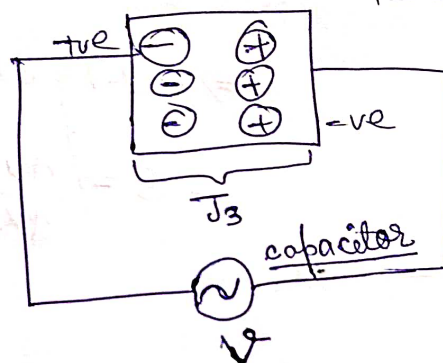
- 1> Reverse blocking mode - J_1, J_3 Rev biased, J_2 is Fwd biased
- 2> Fwd blocking mode - J_2 is Rev biased, J_1, J_3 are fwd biased.
- 3> Fwd conduction mode - J_2 becomes very thin and allows conduction. (I_g injects +ve charges into inner P-section)



Different methods of turning on the SCR?

- 1) Voltage triggering (increase in input voltage).
- 2) Gate triggering (Applying ve I_g during FWD Bias case
 +ve voltage pulse,

3) $\frac{dv}{dt}$ triggering



Not voluntarily
Choice of SCR must be protected against this type of switching action.

$Q = CV$
 $IA = C \frac{dv}{dt}$
 $IA \propto \frac{dv}{dt}$

4) Temperature

Triggering.

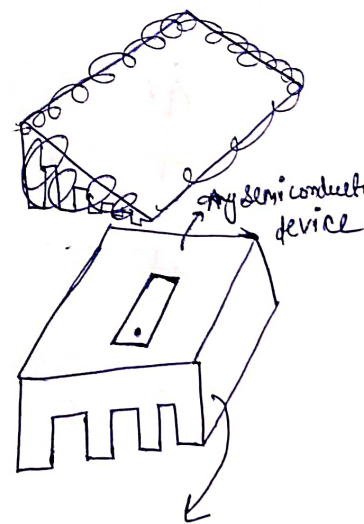
T_2 is heated up.

$e^-/hole$ pair formation.

Flow of e^- current \uparrow .

Heating of T_2

Threshold of Thermal Runaway.

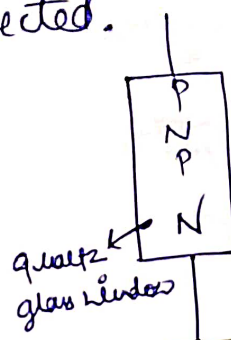


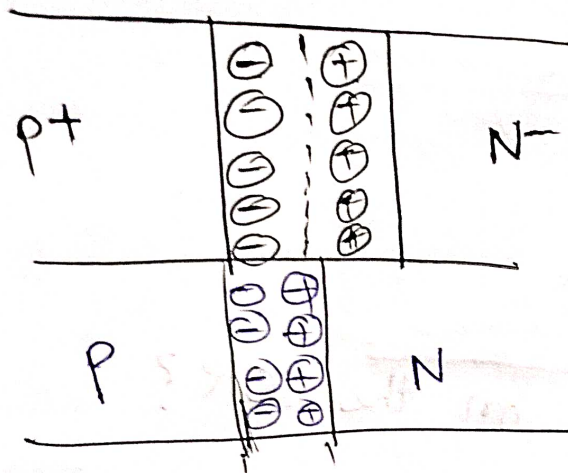
Temp triggering

→ Non voluntary.

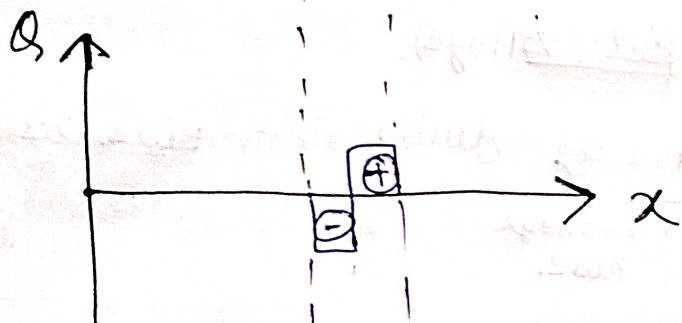
→ Device (SCR) must be protected.

5) Light triggering -
light actuated
SCR (LASCR).



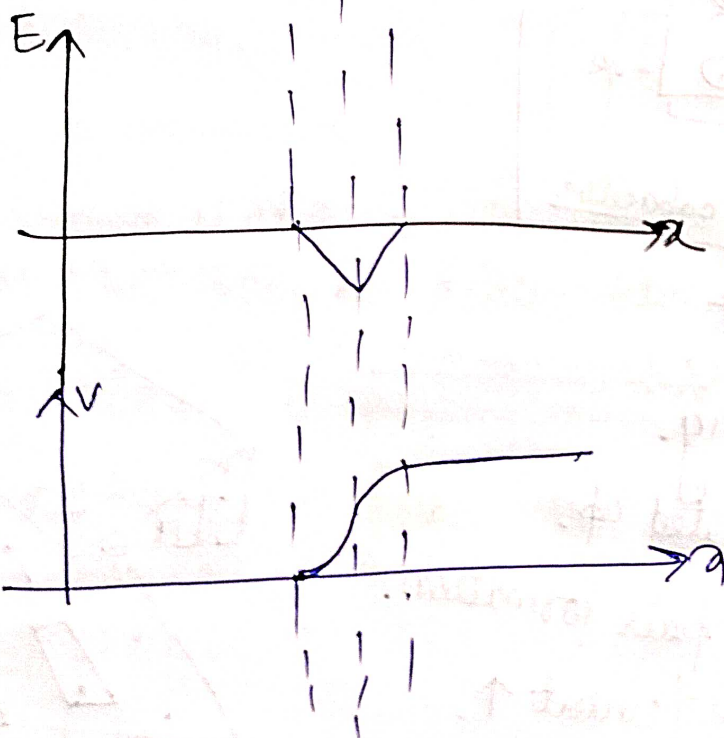


$$WDL \propto \frac{1}{\sqrt{N_{doping}}}$$



$$\nabla \cdot E = \rho_v$$

$$\frac{E}{dv} = \rho_v$$



$$\Rightarrow E(x) = \rho_v(x) + C$$

$$-E = \frac{dv}{dx} \Rightarrow \boxed{\frac{dE}{dx} = \frac{d^2v}{dx^2}}$$