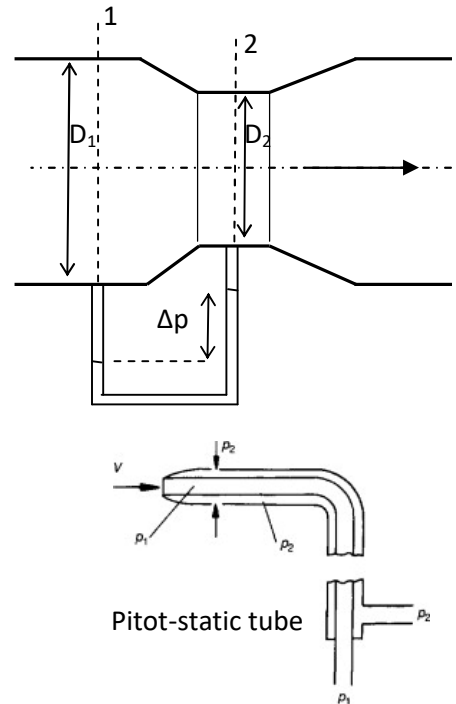


1. (a) In the Venturi meter shown, air flows at a steady rate. The flow may be assumed to be incompressible. Derive an expression for the mass flow rate as a function of pressure difference  $\Delta p$  (Pascals),  $D_1$ ,  $\beta = D_2/D_1$ , and density of air  $\rho_{\text{air}}$ ,  $\text{kg/m}^3$ . Discharge coefficient is unity. However there is a frictional loss  $\hat{W}_{fr}$ , (J/kg) between section 1 and 2. (3 marks)

- (b) If a **pitot-static** tube placed in the center of the narrow section 2 (throat), shows a pressure difference of 200 Pa, what is the flow rate? (2 marks)

density  $\rho_{\text{air}} = 1.18 \text{ kg/m}^3$ ,  $D_1 = 0.2\text{m}$ ,  $\beta = D_2/D_1 = 0.5$ ; and  $\hat{W}_{fr} = 50 \text{ J/kg}$ . Pitot static is ideal: no correction required.

[Assume flow to be uniform across any cross-section].



**BONUS question IIA:** Is the assumption of uniform flow reasonable?

Show with numbers;  $\mu_{\text{air}} = 20 \times 10^{-6} \text{ Pa.s}$

(1mark)

Overall energy balance :  $\frac{V_2^2 - V_1^2}{2} + g(z_2 - z_1) + \frac{p_2 - p_1}{\rho} + \hat{W}_s + \hat{W}_{fr} = 0$ ; for constant  $\rho$

Newtons Law:  $\tau_{xz} = -\mu \frac{\partial V_z}{\partial x}$

2(a) Mass balance between sections 1 & 2

$$A_1 \rho_1 \bar{V}_1 = A_2 \rho_2 \bar{V}_2 \Rightarrow A_1 \bar{V}_1 = A_2 \bar{V}_2 \quad (\because \rho \text{ constant})$$

$$D_1^2 \bar{V}_1 = D_2^2 \bar{V}_2$$

$$\bar{V}_2 = \bar{V}_1 \left( \frac{D_1}{D_2} \right)^2 = \frac{\bar{V}_1}{\beta^2}$$

$$\frac{D_2}{D_1} = \beta; D_1 \left( \frac{D_2}{\beta} \right)$$

Energy balance:

$$\frac{\bar{V}_2^2 - \bar{V}_1^2}{2} + g(z_2 - z_1) + \frac{p_2 - p_1}{\rho} + \hat{W}_s + \hat{W}_{fr} = 0$$

$$\frac{\Delta p}{\rho} = \frac{p_1 - p_2}{\rho} = \frac{\bar{V}_2^2 - \bar{V}_1^2}{2} + \hat{W}_{fr} = \frac{\bar{V}_1^2}{2} \left[ \frac{1}{\beta^4} - 1 \right] + \hat{W}_{fr}$$

$$\bar{V}_1 = \sqrt{\frac{2(\Delta p/\rho - \hat{W}_{fr})}{\left(\frac{1}{\beta^4} - 1\right)}}$$

Volumetric flow rate =

$$\dot{Q} = \frac{\pi D_1^2}{4} \cdot \bar{V}_1 = \frac{\pi D_1^2}{4} \sqrt{\frac{2(\Delta p/\rho - \hat{W}_{fr})}{\left(\frac{1}{\beta^4} - 1\right)}} = \frac{\pi D_2^2}{4} \sqrt{\frac{2(\Delta p/\rho - \hat{W}_{fr})}{(1 - \beta^4)}}$$

Mass flow rate:

$$\dot{m} = \dot{Q} \rho = \frac{\pi D_2^2}{4} \rho \sqrt{\frac{2(\Delta p/\rho - \hat{W}_{fr})}{(1 - \beta^4)}} = \frac{\pi D_2^2}{4} \sqrt{\frac{2(\Delta p - \hat{W}_{fr} \rho)}{(1 - \beta^4)}}$$

(b) Pitot-static tube directly gives the velocity:  $\frac{\bar{V}_2^2}{2} = \frac{p_{\text{total}} - p_{\text{static}}}{\rho}$

$$\rho \frac{\bar{V}_2^2}{2} = 200 \text{ Pa} \Rightarrow \bar{V}_2 = \sqrt{\frac{400}{1.18}} = 18.41 \text{ m/s}$$

$$\bar{V}_1 = 18.41 \times \beta^2 = 4.60 \text{ m/s}$$

$$\dot{Q} = \frac{\pi D_2^2}{4} \cdot 18.41 = \frac{\pi \times 0.2^2}{4} \times 18.41 = 0.578 \text{ m}^3/\text{s}$$

$$\dot{m} = 0.682 \text{ kg/s}$$

Comment: If instead  $\Delta p$  (shown in fig) was given, one had use the formula in (a)

BONUS: Is the flow laminar or turbulent?

$$Re_{D_2} = \frac{1.18 \times 18.41 \times 0.1}{20 \times 10^{-6}} = 108619: \text{turbulent}$$

$$Re_{D_1} = 54280.$$

Both sections, flow is turbulent. Hence uniform assumption valid.