UNIVERSITY OF TORONTO FACULTY OF APPLIED SCIENCE AND ENGINEERING

ROBOTICS (AER 525F)

MID-TERM EXAMINATION October 18, 2013

Note: Rulers may be used in this test.

Time: 105 Minutes

Question 1:

Describe the following terms briefly (maximum 40 words for each, no formulation required):

a) Manipulator Redundancy	(5)
b) Degeneracy of a Manipulator's Spherical Wrist	(5)
c) Dexterous Workspace of a Manipulator	(5)
d) Coriolis Theorem	(5)

Question 2:

Consider the human body (up to the shoulders), when standing at a fixed location, as a manipulator, and calculate its number of d.o.f. Ignore the foot toes, but count the hand fingers and thumbs. Assume the base joints for thumbs and fingers as 2 d.o.f., the joints for wrists, shoulders, hips, ankles, and waist as 3 d.o.f., and consider the remaining joints, including the one connecting waist and torso, as 1 d.o.f. joints. How many d.o.f. do the hand fingers and thumbs add to the human manipulator? (20)

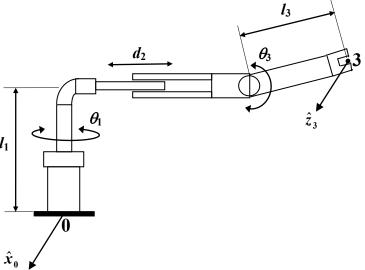
Question 3:

A small camera is positioned at $\begin{bmatrix} 3 & 4 & 2 \end{bmatrix}^T m$ with respect to a fixed coordinate frame. When the camera has a tilt (pitch) angle of 30° and a pan (yaw) angle of 60° (w.r.t. the fixed frame), it detects a light source at $\begin{bmatrix} 1 & 0 & 0.5 \end{bmatrix}^T m$ with respect to its own coordinates. What is the position of the light source with respect to the fixed coordinate frame?

Question 4:

For the spatial 3-d.o.f. manipulator shown in the figure ($0^\circ \le \theta_1, \theta_3 < 360^\circ$, $d_2 \ge 0$):

- a) By using Standard Denavit-Hartenberg convention, define link coordinate frames and link parameters, arrange the D-H table, and then determine ${}^{0}T_{3}$. For $\theta_{1} = 0$ and link 3 vertical down, check whether your computation is correct. (25)
- b) Having the location of the end-effector point (Point 3), expressed in the base frame, determine the corresponding joint variables. Show all possible solutions using simple sketches. (25)



 $I_{i-1}T_{i} = \begin{vmatrix} c\theta_{i} & -s\theta_{i}c\alpha_{i} & s\theta_{i}s\alpha_{i} & a_{i}c\theta_{i} \\ s\theta_{i} & c\theta_{i}c\alpha_{i} & -c\theta_{i}s\alpha_{i} & a_{i}s\theta_{i} \\ 0 & s\alpha_{i} & c\alpha_{i} & d_{i} \end{vmatrix}$

 $a_i \equiv \text{ the length of the common normal between } \hat{z}_{i-1} \text{ and } \hat{z}_i \text{ along } \hat{x}_i \text{ (link length)};$

 $\alpha_i \equiv$ the angle between \hat{z}_{i-1} and \hat{z}_i measured about \hat{x}_i (twist angle);

 $d_i \equiv \text{ the distance from } \hat{x}_{i-1} \text{ to } \hat{x}_i \text{ measured along } \hat{z}_{i-1} \text{ (link offset)};$

 $\theta_i \equiv \text{ the angle between } \hat{x}_{i-1} \text{ and } \hat{x}_i \text{ measured about } \hat{z}_{i-1} \text{ (joint angle);}$

$$\theta_{i} \equiv \text{ the angle between } x_{i-1} \text{ and } x_{i} \text{ measured about } z_{i-1} \text{ (joint angle)};$$

$$\cos q = A \implies q = \pm \operatorname{Atan2} \left(\frac{\sqrt{1 - A^{2}}}{A} \right)$$

$$-A \sin q + B \cos q = 0 \implies \begin{cases} q^{1} = A \tan 2 \left(\frac{B}{A} \right) \\ q^{2} = q^{1} + 180^{\circ} \end{cases}$$

$$-A \sin q + B \cos q = C \implies q = \operatorname{Atan2} \left(\frac{B}{A} \right) - \operatorname{Atan2} \left(\frac{C}{\pm \sqrt{A^{2} + B^{2} - C^{2}}} \right)$$

$$d.o. f. = \lambda \left(l - 1 \right) - \sum_{i=1}^{n} \left(\lambda - f_{i} \right)$$

$$\begin{cases} A\cos q_{1} + B\cos(q_{1} + q_{2}) + C\sin(q_{1} + q_{2}) = D \\ A\sin q_{1} + B\sin(q_{1} + q_{2}) - C\cos(q_{1} + q_{2}) = H \end{cases} \implies \begin{cases} q_{2} = 2A \tan 2 \left(\frac{C \pm \sqrt{C^{2} + B^{2} - F^{2}}}{B + F} \right) & \begin{cases} M = A + B\cos q_{2} + C\sin q_{2} \\ N = B\sin q_{2} - C\cos q_{2} \end{cases} \\ q_{1} = A \tan 2 \left(\frac{HM^{2} - DMN}{DM^{2} + HMN} \right) \end{cases} \qquad F = \frac{D^{2} + H^{2} - A^{2} - B^{2} - C^{2}}{2A}$$