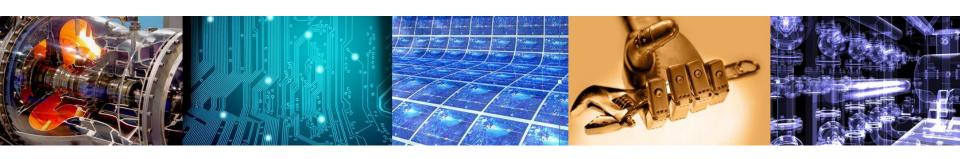


Faculty of Mechanical and Manufacturing Engineering MECH4880 Refrigeration and air conditioning



DA09 calculation method for cooling and heating loads

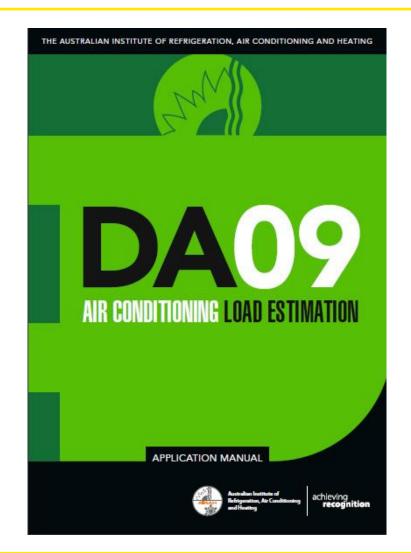
Semester 1 2017

Introduction

Brief overview of calculation method **comprehensively** outlined in DA09

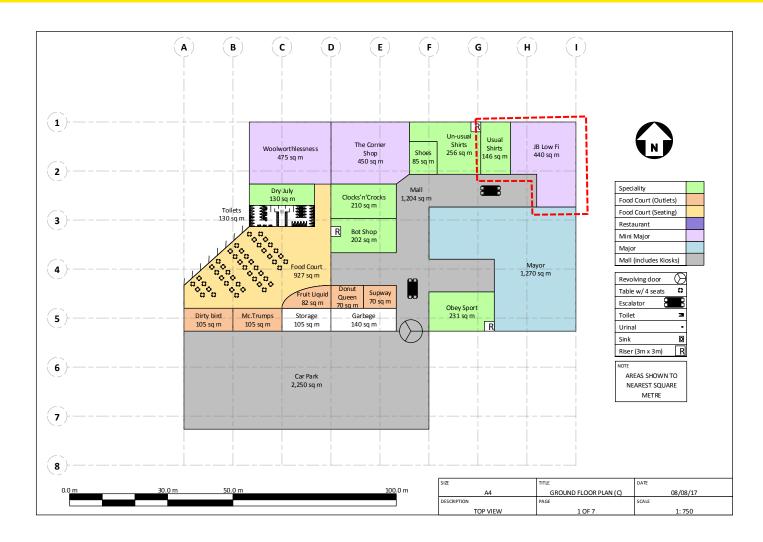
Overview:

- Components of thermal loads
- Thermal load calculations
 - U-value
 - Combined conduction and radiation
 - Glass radiation

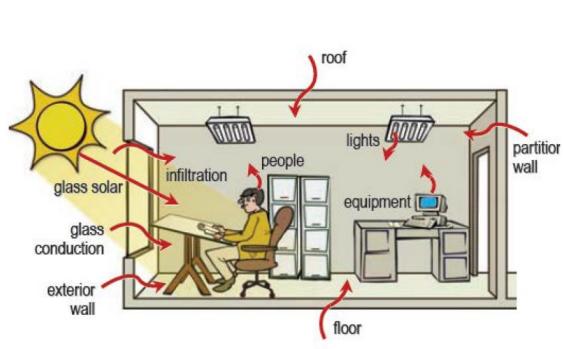




Orientation



Cooling load components



| External | Heat transfer mechanism |
|------------------|--------------------------------|
| Exposed walls | Combined conduction /radiation |
| Internal walls | Conduction |
| Glass conduction | Conduction |
| Glass radiation | Radiation |
| Infiltration | Convection |

| Internal | Sensible or latent |
|------------|--------------------|
| People | Sensible + latent |
| Lights | Sensible |
| Appliances | Sensible + latent |

Equations summary

Conduction heat transfer $Q[W] = U.A.\Delta T$

 $Q[W] = 0.5.(U.A.\Delta T)$ (if the zone is adjacent to the unconditioned space)

Combined conduction/radiation

$$Q[W] = U.A.\Delta t_e$$

Glass radiation $Q[W] = Peaksolar \ heat \ gain \ \left[\frac{W}{m^2}\right] (table 5,14). A \ [m^2]. SF \ (tables 6)$

- 10). k1. k2. k3. k4. k5 (chapter 4)

Infiltration

$$Q_{infiltration} \ [W] = Q_{latent} + Q_{sensible}$$

$$Q_{sensible} = 1.2 \forall_{zone} AC_{hour} \Delta T$$

$$Q_{latent} = 2.9 \forall_{zone} AC_{hour} \Delta \omega$$

Internal loads

 $Q_{people\ or\ lights} = Heat\ gain\ [W](chapter\ 7).$ Storage factor (Table 11). Divrsity factor(Table 13)

Load calculation summary

| External | Heat transfer mechanism | Sensible or latent | DA09 Table | DA09 Chapter |
|------------------|--------------------------------|--------------------|----------------------------------|--------------|
| Exposed walls | Combined conduction /radiation | Sensible | Table 21 to 23 Table 24 to 37 | 5 |
| Internal walls | Conduction | Sensible | Table 24 to 37 | 5 |
| Glass conduction | Conduction | Sensible | Table 37 | 5 |
| Glass radiation | Radiation | Sensible | Table 5 to 19 | 3, 4 |
| Infiltration | Convection | Sensible + latent | Table 44 | 6 |

| External | Sensible or latent | Reference | | | |
|------------|--------------------|--------------------------------|--|--|--|
| People | Sensible + latent | | | | |
| Light | Sensible | DA09 Chapter 7 ASHRAE Handbook | | | |
| Appliances | Sensible + latent | - ACTIONE HARIABOOK | | | |

NOTE: References, chapters and tables are non-exhaustive. You may need to find additional sources.



U-value calculation: Layout

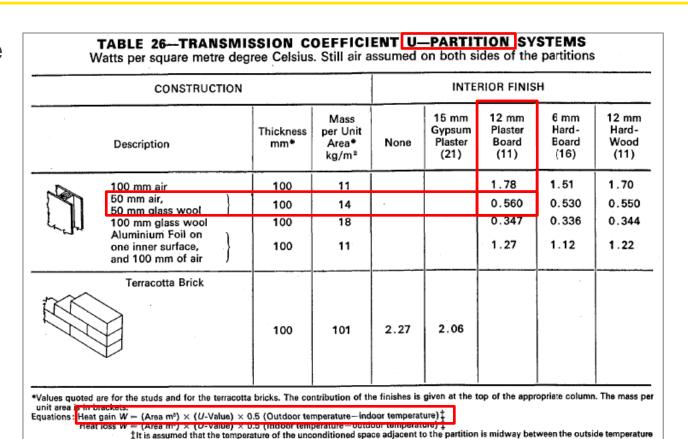
U-value: Measures a material thermal insulating properties. High values are insulating and low values are conducting.

It is the inverse of the R-value or thermal resistance where low values are conducting and high vales are insulating.

| Building section | Construction material | Area (m²) | Density (kg/m^3) | Thickness (m) | Surface density (kg/m^2) | U-value (W/m^2K) | Reference |
|------------------|--------------------------|--------------|--------------------|------------------|----------------------------|--------------------|-----------|
| Roof | | | | | | | |
| External wall | | | | | | | |
| Window | | | | | | | |
| Floor | | | | | | | |
| Ceiling | | | | | | | |
| Floor | | | | | | | |

U-value calculation: Direct method

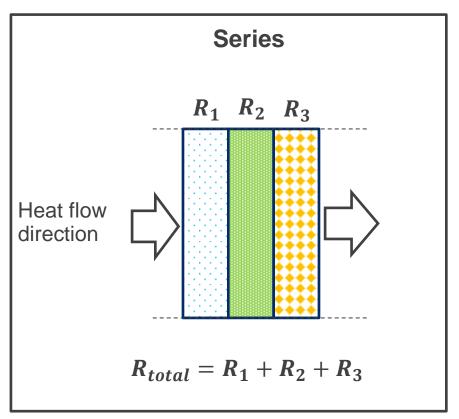
- Example of the direct method
- Table 24-36
- Read thickness, mass per unit area and Uvalue from table.
- Careful to consider assumptions

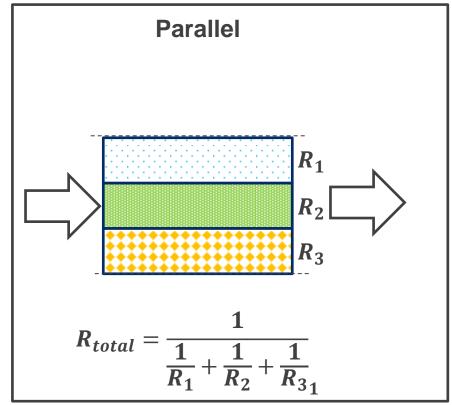


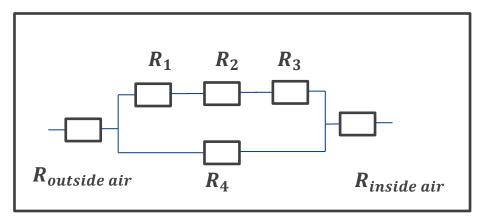
It is assumed that the temperature of the unconditioned space adjacent to the partition is midway between the outside temperature and the temperature inside the conditioned space

and the temperature inside the conditioned space.

When construction material NOT directly available







$$R_{total} = R_{outside \ air} + \left[\frac{1}{R_1 + R_2 + R_3} + \frac{1}{R_4} \right] + R_{inside \ air}$$

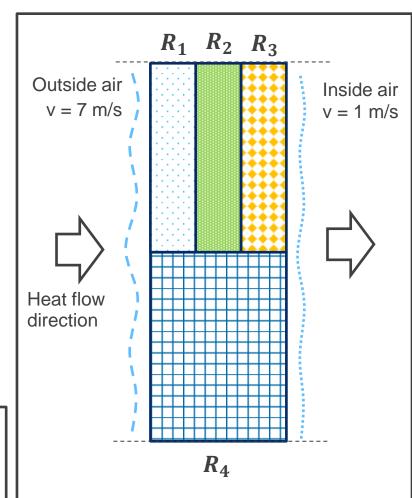


TABLE 37—THERMAL RESISTANCE R—BUILDING AND INSULATING MATERIALS (Cont.)

Note: An asterisk appearing in the density column signifies that the specimens have been conditioned in an atmopshere at 18°C and 65% relative humidity. Where two values are given in the temperature column, separated by a comma, the first refers to the hot face and the second to the cold face temperature.

| Moisture Content % | Density kg/m³ | Temp. °C | Thickness mm | Resistivity (1/k) m.°C/W | Resistance for listed thickness m ² .°C/W | Source of Info. |
|--------------------------|------------------------------|---|--|---|---|---|
| | | | _ | 1.28 | Water | 24 |
| 0 | 1762 | | 90 | 1.24 | 0.111 | 4 |
| 6 9 12 16 | 1874 1922 1970 2034 | | 90 90 90 90 | 0.83 0.70 0.68 0.60 | 0.074 0.063 0.061 0.054 | 4 4 4 |
| | 0 6 9 | Content kg/m³ 0 1762 6 1874 9 1922 12 1970 | Content kg/m³ °C % 0 1762 6 1874 9 1922 12 1970 16 2034 | Content kg/m³ °C mm 0 1762 90 6 1874 90 9 1922 90 12 1970 90 16 2034 90 | Content % kg/m³ °C mm (1/k) — 1.28 0 1762 90 1.24 6 1874 90 0.83 9 1922 90 0.70 12 1970 90 0.68 16 2034 90 0.60 | Content % kg/m³ °C mm (1/k) m.°C/W for listed thickness m².°C/W — 1.28 — 0 1762 90 1.24 0.111 6 1874 90 0.83 0.074 9 1922 90 0.70 0.063 12 1970 90 0.68 0.061 16 2034 90 0.60 0.054 |

- Ceiling
 example of U value data
 presentation
- Make sure to include reference for each value
- Show calculations once to demonstrate method

| Component | Summer / Winter | R-Value (m^2C/W) | Reference |
|------------------------------|-----------------|-----------------------|-----------|
| Air film | Summer | 0.044 | |
| | Winter | 0.030 | |
| Carpet | | 0.1 | |
| Carpet underlay | | 0.4 | |
| Concrete slab 150mm | | 0.25 | |
| Air space 400mmm | Summer | 0.6 | |
| | Winter | 0.868 | |
| Air film | Summer | 0.044 | |
| | Winter | 0.03 | |
| Suspended grid ceiling tiles | | 2.84×10^{-5} | |
| Total R-value | Summer | 1.44 | |
| | Winter | 1.68 | |
| Total U-value | Summer | 0.7 | |
| | Winter | 0.6 | |

Conduction / radiation: External walls

$$Q = U \times A \times \Delta t_e$$

where:

 Δt_e = equivalent temperature difference for latitude, month and time of day desired.

Tables 21-22 for dark coloured walls based on 35°C outdoor design temperature in January and 40° South latitude.

Corrections to these values on page 62 of DA09. Shaded walls, different latitudes, lighter wall colours etc.

Conduction / radiation: External walls

TABLE 21-EQUIVALENT TEMPERATURE DIFFERENCE (°C)

FOR DARK COLOURED†, SUNLIT AND SHADED WALLS*
Based on Dark Coloured Walls, 35°C DB Outdoor Design Temp.; Constant 25°C DB Room Temp.; 10°C, Daily Range; 24-Hour Operation; January and 40° South Latitude†

- Exposure: North, South etc
- Mass of wall per unit area
- Sun Time

| | Mass of wall | | | | | | | | | | | | | SU | N T | IME | | | | | | | | | | | | | | |
|---------------|-----------------|-----|-----|-----|------|------|------|--------|--------|------|-----|------|------|-------|------|--------|-----|------|-----|----------|------|-------|-------|-----|------|------|------|------------|------------|-----|
| Exposure | per unit area ‡ | | | | | M | | | | | | | | | | | | M | | | | | | | | | | AM | | |
| | kg/m² | 6 | 1 7 | '! | 8 | 9 | 10 | 11 | 12 | | 1 j | 2 | 3 | | 1 | 5 | 6 | 7 | | 8 | 9 | 10 | | 11 | 12 | 1 | 2 | 3 | 4 | |
| | 100 | 1. | | | | | 4.4 | 10.0 | 14. | 4 1 | 7.2 | 18.9 | 17.8 | 3 16 | - 7 | 13.3 | 11. | 1 8 | . 9 | 7.8 | 6. | 5. | | 3.9 | | | | 2.2 | | |
| | 300 | 1. | | | | 0.6 | 1.1 | 6. | 1 8. | 9 13 | 3.3 | 15.6 | 16.1 | 116 | . 7[| 15.0 | 13. | 3 10 | . 6 | 8.9 | 7.8 | 6. | / | 5.6 | 4.4 | 3.3 | | | 2.2 5.6 | |
| North | 500 | 4.4 | | . 4 | 3.3 | | 3.3 | 3. | 9 4. | 4 (| 6.7 | 8.9 | 10.6 | 3 1 1 | .1 | 12.2 | 12. | 2 10 | .6 | 10.0 | 8. | 7. | 8 | 7.2 | 6.7 | 6.7 | 6.1 | | 6.7 | |
| | 700 | 6. | 1 5 | . 6 | 5.6 | 5.0 | 4.4 | 4. | 4. | 4 4 | 4.4 | 4.4 | 6. | 1 / | .8 | 9.4 | 10. | 0110 | . 6 | <u> </u> | 11. | 110. | .0 | 8.9 | 7.8 | 7.8 | 7.2 | 7.2 | 0.7 | 0 |
| | 100 | 7. | 8 5 | . 6 | 9.4 | 12.8 | 16. | 17. | 2 17. | 8 1 | 6.7 | 15.6 | 12.8 | 3 11 | .1 | 10.6 | 10. | 8 0 | . 9 | 7.8 | 6.7 | 7 5. | | 4.4 | | | | | | |
| | 300 | 2. | 8 2 | 8.1 | 2.2 | 9.4 | 13.3 | 15. | 617. | 8 1 | 6.7 | 16.1 | 13.9 | 9 12 | . 2 | 10.6 | 10. | 0 9 | . 4 | 8.9 | 8.3 | | | | 5.6 | | | | | |
| Northeast | 500 | 6. | | 5.1 | 5.6 | 5.6 | 5.6 | 8. | 3 11 . | 1 1 | 1.7 | 12.2 | 12. | 3 12 | . 2 | 11.1 | 10. | 0 9 | . 4 | 8.9 | 8.3 | 3 7. | 8 | 7.8 | 7.8 | 7.2 | 7.2 | 6.7 | 6.7 | |
| | 700 | 7. | 2 6 | .7 | 6.7 | 6.7 | 6. | 6. | 1 5. | 6 | 8.3 | 10.0 | 10. | 6 11 | .1 | 12.2 | 11. | 1 10 | .6 | 10.0 | 9.4 | 4 8. | .9 | 8.9 | 8.9 | 8.3 | 8.3 | 7.8 | 7.8 | |
| | 100 | 2. | 811 | .7 | 18.9 | 20.6 | 22. | 2 21 . | 7 20. | 0 1 | 3.3 | 8.9 | 9.4 | 4 10 | .0 | 10.0 | 10. | 0 8 | . 9 | 7.8 | 6. | 7 5. | | 4.4 | | | 1.7 | | | |
| | 300 | 1. | 7 1 | .7 | 2.2 | 13.9 | 18. | 19. | 4 19. | 4 1: | 2.8 | 10.0 | 9.4 | 4 8 | . 9 | 9.4 | 10. | 이 9 | . 4 | 8.9 | 8.3 | 3 7. | 8 | 6.7 | 5.0 | 4.4 | 3.9 | | | |
| East | 500 | 5. | 0 5 | 5.0 | 5.6 | 6.7 | 10.6 | 13. | 3 15. | 6 1 | 6.1 | 15.6 | 13.3 | 3 12 | . 2 | 11.1 | 10. | 0 10 | .0 | 10.0 | 9.4 | 4 8. | 9 | 8.3 | 7.8 | 7.2 | 6.7 | | | |
| | 700 | 8. | 3 7 | .8 | 7.8 | 7.2 | 6. | 7 7. | 2 7. | 8 1 | 0.6 | 12.2 | 12. | 3 12 | . 2 | 11.7 | 11. | 1 10 | .0 | 8.9 | 9.4 | 110. | 0 1 | 0.0 | 10.0 | 9.4 | 9.4 | 8.9 | 8.9 | 8 |
| | 100 | 5. | 010 | 0.6 | 14.4 | 15.0 | 15. | 12. | 810. | 0 | 9.4 | 8.9 | 9.4 | 4 10 | .0 | 10.0 | 10. | 0 8 | . 9 | 7.8 | 6.7 | 7 5. | | 4.4 | | | | | | |
| | 300 | 1. | 7 1 | .1 | 1.1 | 5.0 | 15. | 14. | 4 13. | 3 1 | 0.6 | 7.8 | 8.3 | 3 8 | . 9 | 9.4 | 10. | 0 9 | | | 8.3 | | | | 5.6 | | | | | |
| Southeast | 500 | 4. | | 3.9 | | 4.4 | 4.4 | 1 7. | 8 11. | 1 1 | 0.6 | 10.0 | 8. | 9 7 | . 8 | 8.3 | 8. | 9 8 | | | 8.3 | | | | 6.7 | | | | | |
| | 700 | 5. | 0 5 | 5.0 | 5.6 | 5.6 | 5.0 | 5. | 6 5. | 6 | 7.8 | 10.0 | 11. | 1 10 | .0 | 8.9 | 7. | B 7 | . 8 | 7.8 | 7.8 | 3 7. | 8 | 7.8 | 7.8 | 7.2 | 7.2 | 6.7 | 6.1 | -6 |
| | 100 | 0. | 6 0 | 0.0 | 0.0 | 1.1 | 2.: | 2 3. | 9 5. | | 7.8 | | 12. | 8 15 | . 6 | 20.6 | 24. | 4 22 | .82 | 21.1 | 12.2 | | | 4.4 | | | | | | |
| | 300 | 1. | | 0.6 | | | | | | | | 6.7 | 7.8 | 8 8 | . 9 | 13.9 | 18. | 9 19 | . 4 | 20.0 | 13.9 | 8. | 9 | 6.7 | 5.6 | 4.4 | 3.9 | | | |
| Southwest | 500 | 5. | | 1.4 | | | | | | | 4.4 | 4.4 | 5.0 | 0 5 | . 6 | 7.2 | 8. | 9 11 | .7/ | 13.3 | 13.5 | 914. | 4 1 | 0.0 | 6.7 | 6.1 | 6.1 | 5.6 8.3 | | |
| | 700 | 6. | 7 6 | 3.1 | 5.6 | 5.6 | 5. | 6 5. | 6 5. | 6 | 5.6 | 5.6 | 5. | 6 5 | . 6 | 6.1 | 6. | 7 7 | . 2 | 7.8 | 10.0 | 12. | . 2 1 | 2.8 | 13.3 | 11.1 | 9.4 | 8.3 | 7.8 | |
| | 100 | 1. | 1 (| 0.6 | 0.0 | 1.1 | 2. | 2 3. | 9 5. | 6 1 | 0.0 | 13.3 | 20. | 0 24 | .4 | 27.2 | 28. | 9 21 | .1 | 14.4 | 10.0 | 6. | .7 | 5.0 | 3.3 | 2.8 | | | 1.7 | |
| | 300 | 3. | 3 2 | 2.8 | | | | | | 4 | 6.1 | 7.8 | 12. | 8 16 | . 7 | 21 . 1 | 24. | 4 25 | .0 | 22.2 | 17.1 | 3 11. | .1 | 7.8 | 5.6 | 5.0 | 4.4 | 3.9 | | |
| West | 500 | 6. | | 5.1 | 5.6 | | 5. | | 6 5. | 6 | 6.1 | 6.7 | 7.8 | 8 8 | . 9 | 11.7 | 13. | 3 16 | -1 | 17.8 | 17. | 2 16. | 7 1 | 2.8 | 10.0 | 8.9 | 8.3 | 7.8 | 7.2 | 6 |
| | 700 | 8. | 9 8 | 3.3 | 7.8 | 7.2 | 6. | 7 6. | 7 6. | .7 | 7.2 | 7.8 | 7. | B 7 | . 8 | 8.3 | 8. | 9 10 | .0 | 11.1 | 13. | 914. | . 4 1 | 5.0 | 14.4 | 13.3 | 12.2 | 11.1 | 10.6 | 9 |
| | 100 | 1. | 1 0 | 0.0 | 0.0 | 1.1 | 2. | | | 61 | 2.8 | 16.7 | 21. | 1 24 | . 4 | 25.0 | 25. | 6 18 | .9 | 15.6 | 8. | 5. | 6 | 4.4 | 3.3 | 2.8 | | | 1.7 | |
| | 300 | 3. | 3 2 | 2.8 | | | 2. | | 8 3. | 3 | 6.7 | 8.8 | 15. | 6 20 | 0.0 | 21.7 | 22. | 2 21 | . 7 | 21.1 | 13.: | 3 7. | 8 | 6.1 | 5.6 | 5.0 | 4.4 | 4.4 | 3.9 | 3 |
| Northwest | 500 | 6. | | 5.0 | 5.6 | 5.0 | 4. | 4 5. | 0 5. | 6 | 6.1 | 6.7 | 8. | 9 10 | 0.0 | 12.8 | 14. | 4 15 | .0 | 15.6 | 15.0 | 14. | 4 1 | 0.6 | 7.8 | 7.8 | 7.2 | 7.2 | 6.7 | 6 |
| | 700 | 6. | 7 6 | 3.7 | 6.7 | 6.7 | 6. | 7 6. | 1 5. | 6 | 5.6 | 5.6 | 6. | 1 6 | . 7 | 7.2 | 7. | 8 10 | . 6 | 12.2 | 12.1 | 313. | . 3 | 9.4 | 6.7 | 6.7 | 6.7 | 0./ | 6.7 | ь |
| | 100 | 0. | 6 0 | 0.6 | 0.0 | 0.6 | 1. | | 8 4. | | 6.7 | | | | | 9.4 | 8. | 9 7 | . 8 | 6.7 | | | | 3.3 | | | 1.7 | | 1.1 | |
| | 300 | | | | 0.0 | | 1. | | 7 2. | | | | 6. | | | | | | | | | | | | 4.4 | 3.3 | 2.8 | | 1.7 | |
| South (Shade) | 500 | | | | | 2.2 | | 2 2. | 2 2. | 2 | 2.8 | 3.3 | 3. | 9 4 | .4 | 5.0 | | | | | 6. | | | | 4.4 | | 3.9 | | | |
| | 700 | 2. | 8 2 | 2.8 | 2.2 | 2.2 | 2. | 2 2. | 2 2. | .2 | 2.2 | 2.2 | 2. | 8∣3 | .3 | 3.9 | 4. | 4 5 | .0 | 5.6 | 1 6. | ijij. | . / | 0.1 | 5.6 | 4.4 | 3.9 | 3.3 | 3.3 | : 2 |

Equation: Heat Gain through Walls, $W = (\text{Area, m}^2) \times (\text{Equivalent temperature difference}) \times (\text{Transmission coefficient } U, Tables 24 and 25).$ *All values are for both insulated and uninsulated walls.



The values are to upon insidered and distributed with a state of the result of the conditions refer to confections listed after 73ble 23.
This sper unit area" values for common types of construction are listed in Tables 24 and 25.
For wall constructions less than 100 kg/m², use listed values of 100 kg/m², for wall constructions more than 700 kg/m², use listed values of 700 kg/m².

Glass radiation

$$Q[W] = Peaksolar \ heat \ gain \ \left[\frac{W}{m^2}\right] (table 5,14). A \ [m^2]. SF \ (tables 6 - 10). k1. k2. k3. k4. k5 \ (chapter 4)$$

```
SF = storage \ load \ factor \ (tables6 - 10)
k1 = sash \ correction \ factor, table \ 5,14
k2 = haze \ correction \ factor, table \ 5,14
k3 = Altitude \ correction \ factor, table \ 5,14
k4 = dewpoint \ correction \ factor, table \ 5,14
k5 = glass \ factor, table \ 15
k6 = SOLAR \ factor, table \ 16-18
k5, k6 = OVERALL \ FACOTRS = T15 - T18
```

Glass radiation: Peak solar heat gain

TABLE 14-SOLAR HEAT GAIN THROUGH REFERENCE GLASS

Watts per square metre sash area (W/m²)

| O° South | | AM | | | | | Sun Time | | | | PM ' | | | |
|-----------------------|---------------------------------|-----|------------------|------------------|------------------|------------------|------------------|-------------------|------------------|-------------------|-------------------|-------------------|-------------------|-------------|
| Time of Year | Exposure | 6 | . 7 | 8 | 9 | 10 | П | Noon | | 2 | 3 | 4 | 5 | 6 |
| | North Northeast East | 000 | 20 155 410 | 37 175 510 | 44 120 470 | 47 60 320 | 47 47 145 | 47 47 47 | 47 47 47 | 47 47 47 | 44 44 44 | 37 37 37 | 20 20 20 | 0 |
| Jan 21 | Southeast South Southwest | 0 | 400 125 20 | 520 180 37 | 510 210 44 | 420 220 47 | 290 220 55 | 145 230 145 | 55 220 290 | 47 220 420 | 210 510 | 37 180 520 | 20 125 400 | 0 0 0 |
| | West Northwest Horizontal | 0 | 20 20 100 | 37 37 310 | 44 44 510 | 47 47 660 | 47 47 750 | 47 47 790 | 145 47 750 | 320 60 660 | 470 120 510 | 510 175 310 | 410 155 100 | 0 |
| | North Northeast East | 0 | 19 210 410 | 38 250 510 | 40 210 470 | 45 110 320 | 45 47 145 | 45 45 45 | 45 45 45 | 45 45 45 | 40 40 40 | 38 38 38 | 19 19 19 | 0 |
| Feb 20 & Oct 23 | Southeast South Southwest | 0 | 350 54 19 | 440 90 38 | 420 100 40 | 320 105 45 | 190 105 45 | 75 105 75 | 45 105 190 | 45 105 320 | 40 100 420 | 38 90 440 | 19 54 350 | 0 |
| | West Northwest Horizontal | 0 0 | 19 19 100 | 38 38 310 | 40 40 470 | 45 45 650 | 45 45 740 | 45 45 770 | 145 47 740 | 320 110 650 | 470 210 470 | 510 250 310 | 410 210 100 | 0 |

Glass radiation: Storage load factor

TABLE 6-STORAGE LOAD FACTORS, SOLAR HEAT GAIN THROUGH GLASS

WITH INTERNAL SHADE*

24 Hour Operation, Constant Space Temperature†

| | Mass per | SUN TIME | | | | | | | | | | | |
|-----------|--------------------------|------------------------------------|---|--|--|--|--|--|--|--|--|--|--|
| Exposure | unit area of floor | AM | PM | AM | | | | | | | | | |
| | kg/m² ‡ | 6 7 8 9 10 11 12 | 1 2 3 4 5 6 7 8 9 10 11 12 | 1 2 3 4 5 | | | | | | | | | |
| North | 700 & Over 500 150 | 0.040.040.220.380.520.630.7 | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 0.08 0.07 0.06 0.06 0.0 | | | | | | | | | |
| Northeast | 700 & Over 500 150 | lo 03l0 28l0 47l0 61l0 67l0 65l0 5 | 3 0 . 41 0 . 27 0 . 24 0 . 21 0 . 19 0 . 16 0 . 14 0 . 12 0 . 11 0 . 10 0 . 09 0 . 08 0 0 . 0 0 . 0 0 | 0.07 0.05 0.05 0.05 0.05 0.05 0.04 0.04 0.04 | | | | | | | | | |

Equation: Cooling Load, W = [Peak solar heat gain, W/m², (Table 5)]

× [Window area, m²]

× [Overall solar factor, Haze factor, etc. (Chapter 4)] × [Storage factor, (above Table at desired time)]

*Internal shading device is any type of shade located on the inside of the glass.

†These factors apply when maintaining a CONSTANT TEMPERATURE in the space during the operating period. Where the temperature is allowed to swing, additional storage will result during peak load periods. Refer to Table 12 for applicable storage factors.

** Mass per unit area of floor-

(Mass of outside walls, kg) +0.5 (Mass of partitions, floor and ceiling, kg) Room on Building Exterior (one or more outside walls) =

Floor area in room, m2

Room in Building Interior (no outside walls) = 0.5 (Mass of Partitions, Floor and ceiling, kg)

(Mass of outside walls, kg) + (Mass of floor, kg) + 0.5 (Mass of partitions and ceilings, kg)

Basement Room (floor on ground) = Floor area in room, m2

(Mass of outside wall, partitions, floors, ceilings, structural members and supports, kg)

Air conditioned floor area m2

With rug on floor-Mass of floor should be multiplied by 0.50 to compensate for insulating effect of rug.

Mass per unit area of common types of construction are contained in Tables 24 to 36.

Summary of loads

| Description | Total sensible load (W) | Total Latent load (W) | |
|--------------|----------------------------|--------------------------|--|
| Infiltration | | | |
| Internals | | | |
| Conductions | | | |
| Radiations | | | |
| | Total: | Total: | |

$$SHF = rac{Q_{S,total}}{Q_{S,total} + Q_{L,total}}$$