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Faculty of Engineering

The University of New South Wales

Vibration Diagnosis of Planetary Gearbox under Variable Speed Condition

by

Hengcheng Zhang

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Student ID: z5130844

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Abstract



Acknowledgements



Abbreviations


BE Bachelor of Engineering 

L^AT_EX A document preparation computer program


PhD Doctor of Philosophy

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Chapter 1

Introduction

The aim  of this article is to investigate a method to identify planetary gearbox fault by vibration analysis. The planetary gearbox is

Chapter 2

Literature Review

In this chapter, some basic concepts and important knowledge are provided. These concepts are

2.1 Planetary gearbox

Planetary gearing or epicyclic gearing is a gear system typically consisting of four parts: sun gear, planet gear, ring gear and the planet carrier.

There are several ways of input-output method such as stationary ring gear, fixed carrier or no stationary part. The gear ratio of the planetary gearbox could be calculated as:

$$N_s\omega_s + N_p\omega_p - (N_s + N_p)\omega_c = 0 \quad (2.1)$$

$$N_r\omega_r - N_p\omega_p - (N_r - N_p)\omega_c = 0 \quad (2.2)$$

The following figure shows a typical planetary gearing system, which contains 3 planet gears.

The characters of planetary gearbox make it suitable for large transmission ratio, high load and split input or output circumstances. So it is widely used in wind turbines,

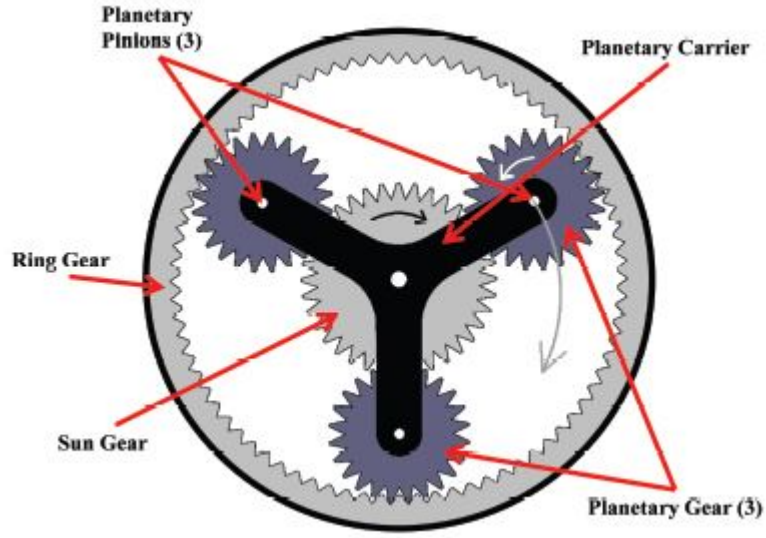



Figure 2.1: Planetary Gearbox Layout[2]

lathes, automobiles and helicopters. The widely appliance and tough working environment of planetary gearbox require it to be highly dependable. Failures of planetary gearbox may lead to huge economic losses as well as safety incidents. But the compact and complex structure on the other hand make it difficult to monitor its condition. Especially when the load and operating speed are varying. This project focuses on the varying speed conditions.

2.2 Planetary Gearbox fault diagnosis

Vibration of gear is caused by the geometric deviation of gears and teeth deformation under load. These two effects introduce a 'meshing error' or 'transmission error' (TE).

 The transmission error could be divided into three types: unloaded static TE, loaded static TE and dynamic TE. The unloaded static TE could be measured under a very light load, and it is realised to be caused by the geometric deviation. The load static TE is introduced by the tooth deflection under a constant load torque. Dynamic TE is caused by the fluctuation of torque and transmission speed.

2.2.1 Vibration generated by gear

Based on the understanding of transmission error, vibration generated by gears is classified as follows: [3]

1. Mean effects for all tooth pairs

The mean effects here are the same for all tooth pairs. Torque varies when each pair of teeth mesh and cause vibration. Therefore it is dominated by harmonics of tooth-mesh frequencies. It could be sub divided into tree parts:

- Tooth deflection due to mean torque.
- The mean part of initial profile errors resulting from manufacturing.
- Uniform wear over all teeth.

Uniform wear of teeth could increase friction force, which would results in higher harmonics of the gearmesh frequency.

2. Variation from the mean.

Variation from the mean could give rise to side bands of harmonics and maybe caused by:

- Slow variations, such as distortion and runout.
- Local faults, such as tooth spalls and root cracks.
- Random errors.
- Systematic erros.

Sidebands around the harmonics of gearmesh frequencies contain the gear fault information. The spaces between sidebands and harmonics shows which gear has fault, while the form of sidebands identify the type of fault. For example, local faults may give rise to a flat sideband spectrum, while distributed fault may inspire higher level but narrowly grouped sidebands. Due to limitation of time and resource, the main fault investigated in this project is Local fault, including tooth spalls and root cracks.

Separation of spalls and cracks is another important topic due to the reason that cracks could cause a much more rapid failure. Endo[6] developed a finite element analysis method to investigate their difference. It was found that cracks at tooth root give a two-stage deviation of transmission error due to the reason that at first stage, faulty tooth together with a healthy tooth share the load and at the second stage, faulty tooth stands the load alone. Spalls on the other hand inspire one deviation of TE when mating tooth pass the spall.

2.2.2 Characteristic of Planetary Gearbox

Comparing to fixed-axis gearbox, in which each gear rotates around a fixed centre, planetary gearbox has planet gears which rotate around not only their own centres but also the centre of sun gear. The transmission structure of planetary gearbox bring unique behaviours. [4]

1. The planet gears are meshing simultaneously with sun gear and the ring gear. Part of the vibrations exited by different component and their different meshing phases could be neutralized or cancelled by each other.
2. The multiple vibration transmission paths are time-varying and load effected in planetary gearbox. It could attenuate the vibration signal of defective part and weaken the fault characteristics.
3. Differ from fixed-axis gear box, side bands appear in spectrum for both healthy and faulty planetary gearboxes and asymmetric about the tooth-mesh frequency. It may caused by multiple planet gears meshing with different phases.
4. Vibrations of low speed faulty components are easily masked and difficult to discover.

2.2.3 Diagnosis techniques

As discussed in the former section, when gears are operating in good condition, the vibration signal tend to be stationary, containing gearmesh frequency and shafts rotating frequencies. When fault happens, the amplitude or frequency components change according to the fault types. Plenty of diagnosis techniques are developed to separate the faulty information from the original signal. [7]

Statistic Indicators

Time domain statistical indicators are carried out directly from the vibration signal. Some of them are scaled including peak value, peak to peak value, mean value, root mean squared value and variance. Among which RMS (root mean squared) value, as its name suggests, is the root of the mean of the squared signal values. It represents the overall vibration level. It is calculated as:

$$RMS = \sqrt{\frac{1}{N} \sum_{i=1}^n x_i^2} \quad (2.3)$$

Variance indicates the power of the vibration, and its formula is:

$$\sigma^2 = \frac{1}{N} \sum_{i=1}^n (x_i - \bar{x})^2 \quad (2.4)$$

There are also some useful unscaled indicators, including kurtosis, crest factor and pulse factor. Kurtosis is the fourth moment normalised by the square of the mean square of the vibration signal waveform and represents the amplitude of impulse energy. [8]

$$K = \frac{\frac{1}{N} \sum_{i=1}^n (x_i - \bar{x})^4}{RMS^4} \quad (2.5)$$

Crest factor shows impulse energy in another form:

$$C = \frac{x_{peak}}{RMS} \quad (2.6)$$

Scaled indicators not only depend on the condition of the machine but also its running speed and load. Unscaled indicators have the benefit that they are independent of the running status.

Time Synchronous Averaging

TSA (Time synchronous averaging) is also a time domain signal processing method other than statistical indicators. It is implemented by averaging several segments of synchronising signals together to extract the periodic signal from the background noises. It is calculated by:

$$y_a(t) = \frac{1}{N} \sum_{n=0}^{N-1} y(t + nT) \quad (2.7)$$

The implementation of TSA depend on the corresponding of sample signals. Which means to be averaged numbers at each point should have the same rotating phase. This is guaranteed by 'Order traking' method. When analysing vibration signals of the rotating machines, a slight fluctuation of the rotating speed could cause smearing of the frequecy components. Order tracking is taking use of a shaft encoder signal or a tacho signal to resample the original signals with constant time interval into constant phase intervalled signal. This method make sure that the samples have same number and starting phase during each revolution. It is recomment to always perform order tracking before implementing TSA even at a constant speed.

The TSA method is firstly introduced into gear fault diagnosis by Stewart [9], whose propose to obtain the residual signal by removing the periodic gearmeshing pattern, and use the kurtosis of the residual signal as the fault indicator. Peter McFadden [10] enhanced this method by improvements of the TSA as well as order tracking operations. He proposed to select short section of signals which correspond to the vibration of one tooth and assembly together to the whole gear. Taking twice length of toothmesh period signal sections with Hanning window was recommended to improve the frequency spectra in his later papers. [12] Time synchronous averaged signals for a fixed period, normally one or two rotation of the shaft, would illustrate the fault type

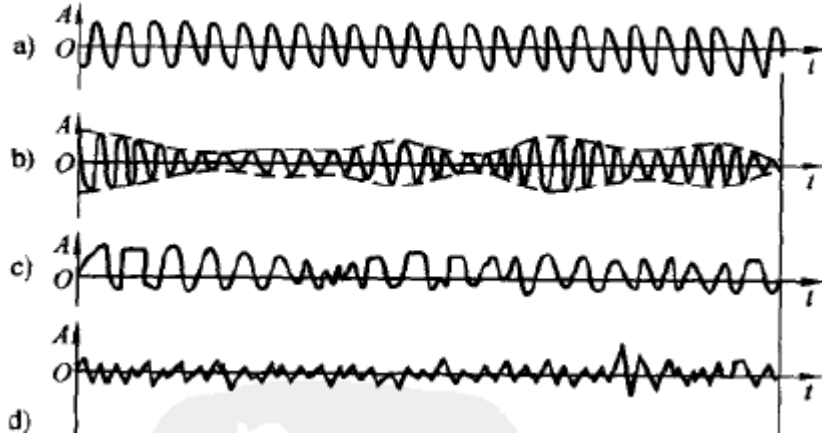


Figure 2.2: Time Synchronous Averaged signals [11]

of the gear. As shown in Figure 2.2, plot a) is a steady gearmesh vibration. In plot b), the signal is amplitude modulated, which maybe a consequence of misalignment. Plot c) is possibly because of significant wear of teeth surface, and plot d) may caused by cracked tooth.

Frequency-domain Methods

Time-domain methods such as statistical indicators is able to find whether the gear is in malfunction, but not sufficient to the fault type. Frequency-domain methods are more capable of this requirement. They are developed based on Fourier transform. Under normal operating condition, the spectrum is dominated by shaft rotating and gearmesh frequency. Sidebands around them and their harmonics would identify the type of fault in some content as discussed in chapter 2.2.1. Further than Fourier transform or its implementation for digital signal, DFT and FFT, demodulation techniques and cepstrum analysis are utilized to run the diagnosis.

As already known that the faulty information of gears ususally hide in the sidebands around gearmesh frequency and its harmonics, and these sidebands are mostly caused by amplitude and frequency modulation. Demodulation techniques such as Hilbert transform are effective to carry out the modulation signal. Thus it is able to investigate

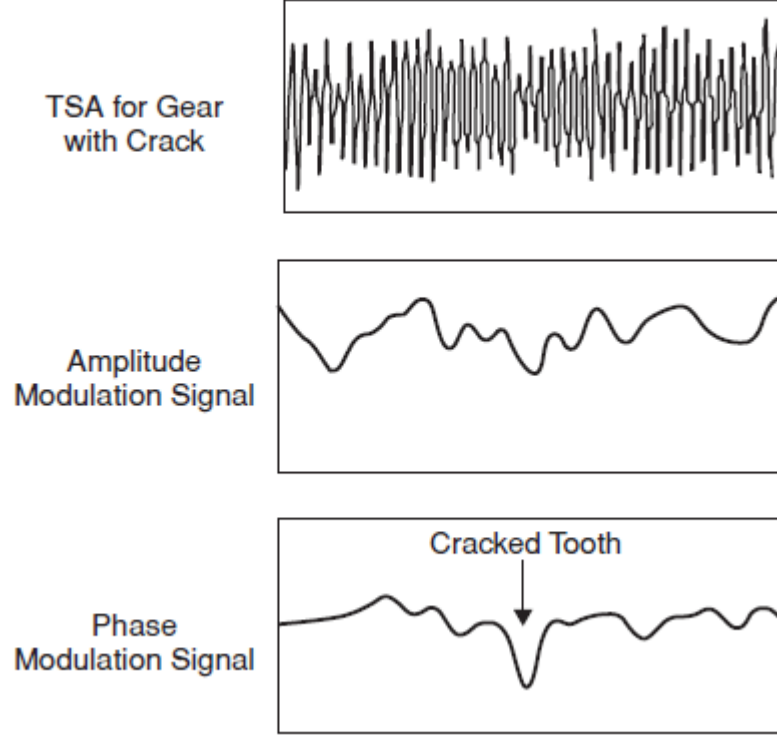


Figure 2.3: Demodulation of the second harmonic of the gearmesh frequency for a cracked gear [13]

their faulty type and damage extent. One example is introduced in [13]. It use Hilbert transform to demodulate the second harmonic of gearmesh frequency of the TSA signal. As seen in Figure 2.3, the phase modulation signal of the TSA signal clearly shows the cracked tooth. It is even able to be known which tooth is in fault with certain phase information.

Cepstrum analysis is another important method to investigate the sidebands and transfer function. Cepstrum is the inverse Fourier transform of a logarithmic spectrum, which is Fourier transformed from a time signal. It is then:

$$\hat{x}(\tau) = IF[\log(X(f))] \quad (2.8)$$

Where $X(f)$ is the spectrum signal.

Time-frequency-domain Methods

Time-frequency domain methods is a combination of time and frequency domains in one plot. Methods such as Wigner-Ville distribution and wavelets analysis are studied recently as another choice in vibration diagnostics. Meltzer *et al.* [16] [17] conducted this method on an automobile planetary gearbox.

Other Methods

Some other effective methods exist in this area, for example modeling method and intelligent method.

...

2.3 ~~Variable Speed~~

Most of the methods mentioned in the former part are developed for constant speed and load conditions. When there are minor speed fluctuations, performing of order tracking would eliminate this effect. But when it comes to wider speed range, as much as ± 30 percent, besides frequency modulation, amplitude modulation caused by passage of resonances, frequency response function and variation of torque comes into consideration. These effects could not be compensated by order tracking. Then the residual signal of TSA under these conditions would include much of the amplitude variation of the deterministic part as well as the random noise. [14] One possible method is to find sections with relatively steady speed. R. Randall [14] suggested another way to perform pre-processing of cepstrum modification to compensate the resonance part before order tracking and TSA.

2.3.1 Cepstrum-Resonance Compensation

The cepstrum is obtained by inverse Fourier transform of the log spectrum. If the log spectrum includes phase part, it is complex cepstrum. If the log spectrum only has amplitude, then it is real or power cepstrum. The logarithmic conversion of the spectrum transform the multiplication relationship between the forcing function and transfer function into an additive one.[3] It is also more evident to see the families of harmonics and sidebands in the log spectrum. Due to these characteristics, cepstrum analysis is able to be applied for collecting uniformly spaced sidebands and separating forcing functions from transfer functions.

In the variable speed gearbox diagnosis application, cepstrum is utilized to perform resonance compensation. Randall indicated in [21] that low-frequency region of the cepstrum is contributed by both excitation and transfer function, while the high-frequency region is dominated by forcing function. So it is able to use liftering in cepstrum to remove the forcing function part, or on the contrary remove the transfer function component. In [14], modal information is obtained by applying exponential window to lifter the cepstrum. Removing the modal part in cepstrum and transfer back to spectrum and further to time domain, it should be able to seen a more uniform waveform. This means the amplitude variation due to passing resonances is compensated.

2.3.2 Ordertracking and TSA

Followed by the pre-processing of resonance compensation, 'order tracking' and TSA is now able to be performed. These two method have already been discussed in chapter 2.2.3. Cepstrum modification removed the amplitude modulation caused by resonance. The next step is to deal with the phase modulation caused by varying speed. 'Order tracking' is a phase demodulation technique based on a reference phase-locked signal. It resample the constant time interval signal to a constant phase increment signal. 'Order tracking' is used to avoid smearing of frequency component in its spectrum. Only after the application of order tracking, it is able to perform TSA.

As discussed in the former part, TSA is averaging together many signal segments corresponding to same period of synchronising signal. It is always performed for one or two rotation of the shaft. The averaged signal, as seen in Figure 2.2 and 2.3 would illustrate the fault in gears. A further investigation could be performed on the TSA or its residual signal. For example, the McFadden method perform a more complicated TSA and check the Kurtosis of the residual signal. The Hilbert transform technique could be performed to examine the amplitude and phase modulation signal as shown in Figure 2.3.

2.4 Summary

By reviewing of the literatures above, it is acknowledged that vibration analysis of gearboxes has been widely researched. Plenty of methods and techniques have been developed in this area. But most of these techniques are focused on fix axis gearboxes and constant speed conditions. Most of these methods fail to work for planetary gearboxes in varying speed conditions, which would be much more universal and widely performed. The complexity of planetary gearbox and amplitude modulation due to speed passing resonance bring a lot of challenge to this task. The suggested process is:

1. Perform cepstrum modification for resonance compensation;
2. Order tracking to compensate the speed variation;
3. TSA to investigate the fault.

Chapter 3

Methodology



In this chapter, the test equipment and experiment procedures are presented. The experiment is based on the planetary test rig in UNSW. Vibration signals are collected by a National Instrument data acquisition system and analysed in Matlab.

3.1 Equipment

The test equipment include the planetary gearbox test rig, control system and the data acquisition system.

3.1.1 Planetary Gearbox Test Rig

The UNSW planetary gearbox test rig was firstly built by Sweeney in parallel configuration and then modified to planetary configuration. Seen from the layout in Figure 3.1, the test rig is driven by a 3 Phase AC induction motor and a hydraulic pump provided the resistance torque. Two flywheels are mounted on input and output shaft to minimize speed fluctuation. Power is transfered through the planetary gearbox in the center. The planetary has a parallel stage and a planetary stage. The input of the parallel stage is a 42-tooth pinion gear, and the output is a 55-tooth spur gear fixed to

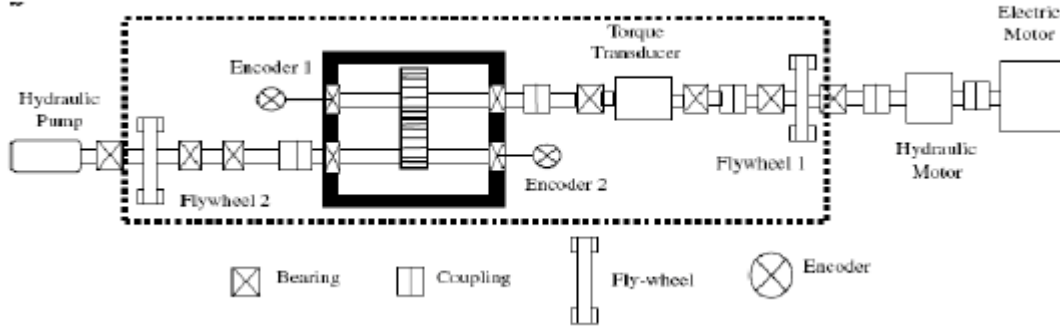


Figure 3.1: UNSW Planetary Gearbox Test Rig

the planet carrier. The planetary stage is driven by the planet carrier. It carries three planet gears which have 23 teeth each. The ring is fixed and has 80 teeth. The output sun gear has 34 teeth.

The gearbox is connected to the input and output shafts by belt couplings, which are not shown in the layout of Figure 3.1. Tension of the belts are adjusted by the sliding rails downside the gearbox housing. The planetary gearbox and the belt drives are illustrated in Figure 3.2.

A in-line torque transducer is used to measure the torque on the drive shaft. Its result is shown directly on The UNSW MK II transducer indicator. Due to the limitation of the belt transmission, the maximum torque is restricted to 70 Nm. A Hiedhan 426-36000 shaft encoder is mounted on the input shaft of the gearbox. Which is shown on the upper-left corner of Figure 3.2. The external accelerometer is fixed by stud to the outframe of the ring gear. There are two internal accelerometers, axial and radial, mounted inside the spur gear. The radial transducer rotate together with the carrier, and its signal is trasferred out through a Michigan Scientific B6-2 slip ring on the left side. Both the external and internal transducers are Bruel & Kjaer 4394 IEPE accelerometers.

The speed of the AC induction motor is controlled by a F RENIC-MEGA variable frequency drive (VFD), which allow us to run the variable speed tests. As this is a 8 pole induction moter, the input frequency displayed on the variable frequency drive

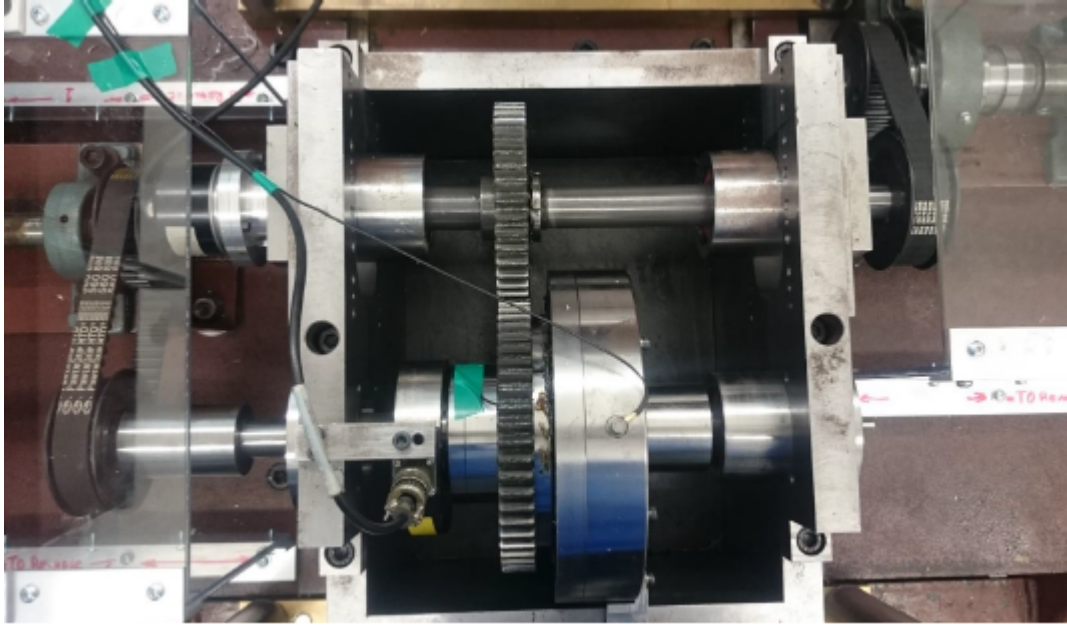


Figure 3.2: The Planetary Gearbox

should be divided by four to get the drive shaft running frequency.

The VFD is installed on the control panel together with a switch and an emergency stop button. The control panel is shown in Figure 3.3. It also contains the hydraulic control valve and the hydraulic isolation valve. The resistance torque could be adjusted by the control valve.

3.1.2 Data Acquisition System

The test signals generated by the rig are collected by a National Instrument (NI) data acquisition system.

3.2 Test Setting

3.3 Processing and Analysis

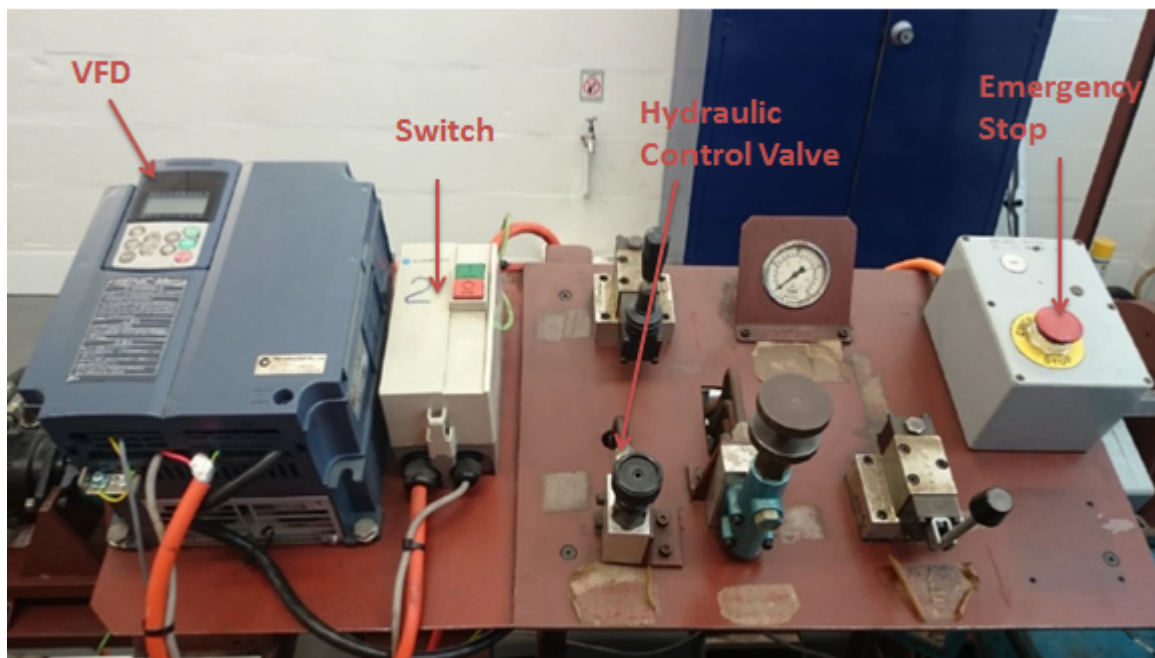


Figure 3.3: The Test Rig Control Panel

Chapter 4

Results and Discussion

This chapter is mainly provided for the purpose of showing a typical thesis structure. There are no more thesis requirements described.

4.1 Results

The result of this work is the present document, being both a L^AT_EX template and a thesis requirement specification.

4.2 Discussion

The Dual function of this document somewhat de-emphasises the primary purpose of the document, namely the thesis requirements. It would be better, if these could be stated on a few concise pages (cf Appendix 1, p21).

Chapter 5

Conclusion

A thesis requirements/template document has been created. This serves the dual purposes of giving students specific requirements to their theses — both style and content related — while providing a typical thesis structure in a L^AT_EX template.

5.1 Future Work

Extract the requirements from the template in order to have very concise requirements.

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Appendix 1

This section contains the options for the UNSW thesis class; and layout specifications used by this thesis.

Appendix 2

This section contains scads of supplementary data.

B.1 Data