

# Marbl

June 23, 2023

## 1 Governing equations

We introduce the flow variables  $\rho = \rho(\mathbf{x}, t)$ ,  $\mathbf{u} = \mathbf{u}(\mathbf{x}, t)$ ,  $e = e(\mathbf{x}, t)$ , and  $p = p(\mathbf{x}, t)$ . The governing equations that dictate their evolution are

$$\frac{\partial \rho}{\partial t} + \mathbf{u} \cdot \nabla \rho = -\rho \nabla \cdot \mathbf{u}, \quad (1)$$

$$\rho \left( \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = -\nabla p, \quad (2)$$

$$\rho \left( \frac{\partial e}{\partial t} + \mathbf{u} \cdot \nabla e \right) = -p \nabla \cdot \mathbf{u}. \quad (3)$$

## 2 Finite element expansion

We introduce the coefficients  $R_i = R_i(t)$ ,  $\mathbf{U}_i = \mathbf{U}_i(t)$ ,  $E_i = E_i(t)$ ,  $P_i = P_i(t)$ , as well as the basis functions  $\phi_i = \phi_i(\mathbf{x}, t)$ , and  $w_i = w_i(\mathbf{x}, t)$ . We note that  $\mathbf{U}_i$  is a vector whose components are  $U_{i,\alpha} = U_{i,\alpha}(t)$  for  $\alpha = x, y, z$ . These coefficients are used in the following expansions

$$\rho = \sum_j^{N_\rho} R_j \phi_j, \quad (4)$$

$$\mathbf{u} = \sum_j^{N_u} \mathbf{U}_j w_j, \quad (5)$$

$$e = \sum_j^{N_e} E_j \phi_j, \quad (6)$$

$$p = \sum_j^{N_p} P_j \phi_j. \quad (7)$$

The basis functions are defined so that they satisfy

$$\frac{\partial \phi_j}{\partial t} + \mathbf{u} \cdot \nabla \phi_j = 0, \quad (8)$$

$$\frac{\partial w_j}{\partial t} + \mathbf{u} \cdot \nabla w_j = 0. \quad (9)$$

### 3 Semi-discrete momentum conservation

We begin by showing that

$$\begin{aligned}
\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} &= \sum_j^{N_u} \left( \frac{d\mathbf{U}_j}{dt} w_j + \mathbf{U}_j \frac{\partial w_j}{\partial t} \right) + \mathbf{u} \cdot \left( \sum_j^{N_u} \mathbf{U}_j \nabla w_j \right) \\
&= \sum_j^{N_u} \left[ \frac{d\mathbf{U}_j}{dt} w_j + \mathbf{U}_j \left( \frac{\partial w_j}{\partial t} + \mathbf{u} \cdot \nabla w_j \right) \right] \\
&= \sum_j^{N_u} \frac{d\mathbf{U}_j}{dt} w_j.
\end{aligned} \tag{10}$$

Define the domain of the problem under consideration as  $\Omega = \Omega(t)$ . The finite element formulation of the momentum equation is thus

$$\int_{\Omega} \rho \sum_j^{N_u} \frac{d\mathbf{U}_j}{dt} w_j w_i dV = \int_{\Omega} \sum_j^{N_p} P_j \phi_j \nabla w_i dV \quad \text{for } i = 1, \dots, N_u. \tag{11}$$

The above is re-written as

$$\sum_j^{N_u} \frac{d\mathbf{U}_j}{dt} m_{ij} = \sum_j^{N_p} P_j \mathbf{d}_{ji} \quad \text{for } i = 1, \dots, N_u. \tag{12}$$

where the mass bilinear form  $m_{ij}$  is given by

$$m_{ij} = \int_{\Omega} \rho w_i w_j dV, \tag{13}$$

and the derivative bilinear form  $\mathbf{d}_{ij}$  by

$$\mathbf{d}_{ij} = \int_{\Omega} \phi_i \nabla w_j dV. \tag{14}$$

Note that  $\mathbf{d}_{ij}$  is a vector whose components are  $d_{ij,\alpha}$ , for  $\alpha = x, y, z$ , where  $\alpha$  determines which component of the  $\nabla$  operator is being used. Equation (12) can thus be expanded as

$$\begin{aligned}
\sum_j^{N_u} \frac{dU_{j,x}}{dt} m_{ij} &= \sum_i^{N_p} P_j d_{ji,x} & \text{for } i = 1, \dots, N_u, \\
\sum_j^{N_u} \frac{dU_{j,y}}{dt} m_{ij} &= \sum_i^{N_p} P_j d_{ji,y} & \text{for } i = 1, \dots, N_u, \\
\sum_j^{N_u} \frac{dU_{j,z}}{dt} m_{ij} &= \sum_i^{N_p} P_j d_{ji,z} & \text{for } i = 1, \dots, N_u.
\end{aligned} \tag{15}$$

We'll now write the above in matrix notation. Introduce the vector  $\mathbf{U}_x = \mathbf{U}_x(t)$  whose components are  $U_{i,x}$  for  $i = 1, \dots, N_u$ . The analogous holds for  $\mathbf{U}_y$  and  $\mathbf{U}_z$ . Similarly, we introduce the matrix

$\mathbf{D}_x = \mathbf{D}_x(t)$  whose components are  $d_{ij,x}$ . The analogous holds for  $D_y$  and  $D_z$ . Finally, the matrix  $\mathbf{M} = \mathbf{M}(t)$  is that with components  $m_{ij}$  and the vector  $\mathbf{P} = \mathbf{P}(t)$  is that with components  $P_j$ . Equation (15) can now be written as

$$\begin{aligned} M \frac{d\mathbf{U}_x}{dt} &= \mathbf{D}_x^T \mathbf{P}, \\ M \frac{d\mathbf{U}_y}{dt} &= \mathbf{D}_y^T \mathbf{P}, \\ M \frac{d\mathbf{U}_z}{dt} &= \mathbf{D}_z^T \mathbf{P}. \end{aligned} \tag{16}$$