

# Coordinate system for Tokamaks

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## 1 Basic definitions

### 1.1 Eulerian coordinates

Consider our traditional Euclidian coordinate system given by coordinates  $(x^1, x^2, x^3)$  and unit vectors  $\mathbf{x}_1, \mathbf{x}_2, \mathbf{x}_3$ . The position vector is  $\mathbf{x} = x^1\mathbf{x}_1 + x^2\mathbf{x}_2 + x^3\mathbf{x}_3$ .

### 1.2 Curvilinear Coordinates

We will now define a new coordinate system, a curvilinear coordinate system, in relation to the standard Euclidian coordinates. To do so we first define the transformation

$$\hat{u}^i = \hat{u}^i(x^1, x^2, x^3). \quad (1)$$

and we label its inverse as

$$\hat{x}^i = \hat{x}^i(u^1, u^2, u^3) \quad (2)$$

Thus, we can write

$$\hat{x}^i(\hat{u}^1, \hat{u}^2, \hat{u}^3) = x^i \quad (3)$$

$$\hat{u}^i(\hat{x}^1, \hat{x}^2, \hat{x}^3) = u^i \quad (4)$$

We can now take the derivative of either eq. (3) or eq. (4). For example, the derivative  $d/du^j$  of eq. (4) gives

$$\left( \frac{\partial \hat{u}^i}{\partial x^k} \right)_{x^i=\hat{x}^i} \frac{\partial \hat{x}^k}{\partial u^j} = \delta_j^i. \quad (5)$$

We can evaluate the above at  $u^i = \hat{u}^i$ , so that

$$\frac{\partial \hat{u}^i}{\partial x^k} \left( \frac{\partial \hat{x}^k}{\partial u^j} \right)_{u^i=\hat{u}^i} = \delta_j^i. \quad (6)$$

We now define two basis vectors as follows

$$\mathbf{e}_i = \left( \frac{\partial \hat{x}^1}{\partial u^i} \right)_{u^i=\hat{u}^i} \mathbf{x}_1 + \left( \frac{\partial \hat{x}^2}{\partial u^i} \right)_{u^i=\hat{u}^i} \mathbf{x}_2 + \left( \frac{\partial \hat{x}^3}{\partial u^i} \right)_{u^i=\hat{u}^i} \mathbf{x}_3 \quad (7)$$

$$\mathbf{e}^i = \frac{\partial \hat{u}^i}{\partial x^1} \mathbf{x}^1 + \frac{\partial \hat{u}^i}{\partial x^2} \mathbf{x}^2 + \frac{\partial \hat{u}^i}{\partial x^3} \mathbf{x}^3 \quad (8)$$

The dot product of these two vectors is given by

$$\mathbf{e}^i \cdot \mathbf{e}_j = \delta_j^i. \quad (9)$$

The two coordinate bases are not necessarily constant, orthogonal, of unit length, or dimensionless.

**At the end, one way to think about it is that for every point  $[x^1, x^2, x^3]$  in the Euclidian coordiante system, there is a coresponding coordinate given by  $[\hat{u}^1, \hat{u}^2, \hat{u}^3]$ , and that at every point of these new coordinates, there are two coordinate bases, given by eq. (7) and eq. (8). The latter basis is typically expresses as  $\nabla \hat{u}^1, \nabla \hat{u}^2$ , and  $\nabla \hat{u}^3$ .**

### 1.3 Vectors

Since there are two coordinate bases, one can define two types of vectors at every point in the domain. One is a vector in terms of contravariant components  $v^i$

$$\mathbf{v} = v^1 \mathbf{e}_1 + v^2 \mathbf{e}_2 + v^3 \mathbf{e}_3, \quad (10)$$

and the other a vector in terms of covariant components  $v_i$

$$\mathbf{v} = v_1 \mathbf{e}^1 + v_2 \mathbf{e}^2 + v_3 \mathbf{e}^3. \quad (11)$$

Note that, due to eq. (9), we have  $v^i = \mathbf{v} \cdot \mathbf{e}^i$  and  $v_i = \mathbf{v} \cdot \mathbf{e}_i$ .

We now define the metric coefficients  $g_{ij}$  and  $g^{ij}$  as

$$g_{ij} = \mathbf{e}_i \cdot \mathbf{e}_j \quad (12)$$

$$g^{ij} = \mathbf{e}^i \cdot \mathbf{e}^j \quad (13)$$

$$(14)$$

Thus, the dot product of two vectors in the curvilinear reference frame simplifies to the following

$$\mathbf{v} \cdot \mathbf{w} = v^i w_i = v_i w^i = g_{ij} v^i w^j = g^{ij} v_i w_j. \quad (15)$$

The cross product can be computed as

$$\mathbf{v} \times \mathbf{w} = \epsilon_{ijk} \sqrt{g} v^i w^j \mathbf{e}^k \quad (16)$$

$$\mathbf{v} \times \mathbf{w} = \epsilon^{ijk} \frac{1}{\sqrt{g}} v_i w_j \mathbf{e}_k, \quad (17)$$

where  $g = \det(g_{ij})$ . One can also define  $g^{-1} = \det(g^{ij})$ .

## 2 Calculus

### 2.1 Integration

- Volume integrals: Define  $dV_u$  as an infinitesimal volume in curvilinear coordinates,  $\Omega_u$  as a finite volume of integration in curvilinear coordinates, and  $f_u$  as a function whose input is in curvilinear coordinates, that is,  $f_u = f_u(u^1, u^2, u^3)$ . Then, the volume integral can be computed using

$$\int_{\Omega_u} f_u dV_u = \int_{\Omega_u} f_u |\det(J_{ij})| du^1 du^2 du^3, \quad (18)$$

where  $J_{ij} = \partial \hat{x}^i / \partial u^j$  is the Jacobian. Given that Eulerian coordinates can be thought of as an instance of curvilinear coordinates, we have

$$\int_{\Omega_u} f_u dV_u = \int_{\Omega_x} f_x dV_x = \int_{\Omega_x} f_x dx^1 dx^2 dx^3 \quad (19)$$

One thing to note is that  $f_x(x^1, x^2, x^3)$  and  $f_u(u^1, u^2, u^3)$  are equal when evaluated at the same point in space. In other words, these functions satisfy

$$f_u(u^1, u^2, u^3) = f_x(\hat{x}^1, \hat{x}^2, \hat{x}^3). \quad (20)$$

Equating eqs. (18) and (19) allows us to write the standard rule for integration by substitution

$$\int_{\Omega_x} f_x(x^1, x^2, x^3) dx^1 dx^2 dx^3 = \int_{\Omega_u} f_x(\hat{x}^1, \hat{x}^2, \hat{x}^3) |\det(J_{ij})| du^1 du^2 du^3. \quad (21)$$

- Surface integrals: Define  $dS_u$  as an infinitesimal surface in curvilinear coordinates,  $\Gamma_u$  as a finite surface of integration in curvilinear coordinates that belongs to the  $u^1 = \text{constant}$  surfaces, and  $f_u$  as a function whose input is defined using curvilinear coordinates. Then, a surface integral can be computed using

$$\int_{\Gamma_u} f_u dS_u = \int_{\Gamma_u} f_u J |\nabla \hat{u}^1| du^2 du^3. \quad (22)$$

Note that now we can write

$$\begin{aligned} \int_{\Omega_u} f_u dV_u &= \int_{u_l^1}^{u_u^1} \int_{\Gamma_u} f_u J du^1 du^2 du^3 = \\ &= \int_{u_l^1}^{u_u^1} \int_{\Gamma_u} f_u \frac{J |\nabla \hat{u}^1| du^2 du^3}{|\nabla \hat{u}^1|} du^1 = \int_{u_l^1}^{u_u^1} \int_{\Gamma_u} f_u \frac{dS_u}{|\nabla \hat{u}^1|} du^1. \end{aligned} \quad (23)$$

## 2.2 Differentiation

### 2.2.1 The grad operator

Consider the function  $f_x = f_x(x^1, x^2, x^3)$  and the grad operator, which is

$$\nabla f_x = \frac{\partial f_x}{\partial x^1} \mathbf{x}_1 + \frac{\partial f_x}{\partial x^2} \mathbf{x}_2 + \frac{\partial f_x}{\partial x^3} \mathbf{x}_3. \quad (24)$$

We now introduce the function  $f_u = f_u(u^1, u^2, u^3)$  and note that  $f_x = f_u(\hat{u}^1, \hat{u}^2, \hat{u}^3)$ . Thus

$$\frac{\partial f_x}{\partial x^1} = \left( \frac{\partial f_u}{\partial u^1} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^1}{\partial x^1} + \left( \frac{\partial f_u}{\partial u^2} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^2}{\partial x^1} + \left( \frac{\partial f_u}{\partial u^3} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^3}{\partial x^1}, \quad (25)$$

$$\frac{\partial f_x}{\partial x^2} = \left( \frac{\partial f_u}{\partial u^1} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^1}{\partial x^2} + \left( \frac{\partial f_u}{\partial u^2} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^2}{\partial x^2} + \left( \frac{\partial f_u}{\partial u^3} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^3}{\partial x^2}, \quad (26)$$

$$\frac{\partial f_x}{\partial x^3} = \left( \frac{\partial f_u}{\partial u^1} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^1}{\partial x^3} + \left( \frac{\partial f_u}{\partial u^2} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^2}{\partial x^3} + \left( \frac{\partial f_u}{\partial u^3} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \frac{\partial \hat{u}^3}{\partial x^3}. \quad (27)$$

Using the definition of  $\mathbf{e}^i$ , the grad operator can be written as

$$\nabla f_x = \left( \frac{\partial f_u}{\partial u^1} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \mathbf{e}^1 + \left( \frac{\partial f_u}{\partial u^2} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \mathbf{e}^2 + \left( \frac{\partial f_u}{\partial u^3} \right)_{\mathbf{u}=\hat{\mathbf{u}}} \mathbf{e}^3. \quad (28)$$

This shows the equivalence between the grad operator in Eulerian coordinates and curvilinear coordinates.

### 2.2.2 The divergence operator

### 2.2.3 The curl operator

The curl is given by

$$\nabla \times A = \epsilon^{ijk} \frac{1}{\sqrt{g}} \frac{\partial A_j}{\partial u^i} \mathbf{e}_k \quad (29)$$

## 3 Flux coordinates

Imagine that Euclidian space is permeated by a set of surfaces, which we call flux surfaces. Each of those surfaces is labeled with a different value of the variable  $\psi$ . We also note that the flux surfaces are not stationary, they can move around as time progresses.

We now introduce the function  $\hat{\psi} = \hat{\psi}(t, x^1, x^2, x^3)$ . This function is defined in such a way that for all values  $x^1, x^2, x^3$  that are part of a given flux surface at a specific time  $t$ , then  $\hat{\psi}$  will evaluate to the value of  $\psi$  corresponding to that flux surface. The velocity of the flux surfaces is given by  $\mathbf{V}_\psi = \mathbf{V}_\psi(t, x^1, x^2, x^3)$ . Thus, by definition

$$\frac{\partial \hat{\psi}}{\partial t} + \mathbf{V}_\psi \cdot \nabla \hat{\psi} = 0. \quad (30)$$

A flux coordinate is defined as one in which  $\hat{u}^1 = \hat{\psi}$ .

### 3.1 Flux-surface averaging

To begin, we define the following.  $D(\psi, t)$  is the volume enclosed at time  $t$  by the flux surface labelled by  $\psi$ . The surface of  $D(\psi, t)$  is labelled as  $\partial D(\psi, t)$ . Additionally,  $\Delta(\psi, t) = D(\psi + \Delta\psi, t) - D(\psi, t)$ .

The flux surface average of a function is given by

$$\langle f \rangle_\psi = \lim_{\Delta\psi \rightarrow 0} \frac{\int_{\Delta(\psi, t)} f dV}{\int_{\Delta(\psi, t)} dV}. \quad (31)$$

This can be re-written as shown below

$$\langle f \rangle_\psi = \lim_{\Delta\psi \rightarrow 0} \frac{\frac{1}{\Delta\psi} \int_{\Delta(\psi, t)} f dV}{\frac{1}{\Delta\psi} \int_{\Delta(\psi, t)} dV} = \lim_{\Delta\psi \rightarrow 0} \frac{\frac{1}{\Delta\psi} \left( \int_{D(\psi+\Delta\psi, t)} f dV - \int_{D(\psi, t)} f dV \right)}{\frac{1}{\Delta\psi} \left( \int_{D(\psi+\Delta\psi, t)} dV - \int_{D(\psi, t)} dV \right)} = \frac{\frac{\partial}{\partial \psi} \int_{D(\psi, t)} f dV}{\frac{\partial}{\partial \psi} \int_{D(\psi, t)} dV}. \quad (32)$$

Defining  $V' = V'(\psi, t)$  as

$$V' = \frac{\partial}{\partial \psi} \int_{D(\psi, t)} dV. \quad (33)$$

the second expression for the flux surface average is written as

$$\langle f \rangle_\psi = \frac{1}{V'} \frac{\partial}{\partial \psi} \int_{D(\psi, t)} f dV. \quad (34)$$

A third expression for  $\langle g \rangle_\psi$  follows from using eq. (23) for the above. Thus,

$$\langle f \rangle_\psi = \frac{1}{V'} \frac{\partial}{\partial \psi} \int_0^\psi \int_{\partial D(\psi', t)} f \frac{dS}{|\nabla \hat{\psi}|} d\psi' = \frac{1}{V'} \int_{\partial D(\psi, t)} f \frac{dS}{|\nabla \hat{\psi}|}. \quad (35)$$

### 3.1.1 Average of spatial derivatives

We use the second definition of the flux-surface average, given by eq. (34), and then the divergence theorem to obtain

$$\langle \nabla \cdot \mathbf{A} \rangle_\psi = \frac{1}{V'} \frac{\partial}{\partial \psi} \int_{D(\psi, t)} \nabla \cdot \mathbf{A} dV = \frac{1}{V'} \frac{\partial}{\partial \psi} \int_{\partial D(\psi, t)} \mathbf{A} \cdot \frac{\nabla \hat{\psi}}{|\nabla \hat{\psi}|} dS. \quad (36)$$

We now use the third definition eq. (35) to obtain

$$\langle \nabla \cdot \mathbf{A} \rangle_\psi = \frac{1}{V'} \frac{\partial}{\partial \psi} V' \langle \mathbf{A} \cdot \nabla \hat{\psi} \rangle_\psi. \quad (37)$$

### 3.1.2 Average of time derivatives

Using the Reynolds transport theorem we show

$$\begin{aligned} \frac{\partial}{\partial t} \int_{D(\psi, t)} f dV &= \int_{D(\psi, t)} \frac{\partial f}{\partial t} dV + \int_{\partial D(\psi, t)} f \mathbf{V}_\psi \cdot \frac{\nabla \hat{\psi}}{|\nabla \hat{\psi}|} dS \\ &= \int_{D(\psi, t)} \frac{\partial f}{\partial t} dV + V' \langle f \mathbf{V}_\psi \cdot \nabla \hat{\psi} \rangle_\psi. \end{aligned} \quad (38)$$

We now take the derivative of both sides by  $\psi$  and then divide by  $V'$ .

$$\frac{1}{V'} \frac{\partial}{\partial t} V' \langle f \rangle_\psi = \left\langle \frac{\partial f}{\partial t} \right\rangle_\psi + \frac{1}{V'} \frac{\partial}{\partial \psi} V' \langle f \mathbf{V}_\psi \cdot \nabla \hat{\psi} \rangle_\psi. \quad (39)$$

Re-arranging and using eq. (30)

$$\left\langle \frac{\partial f}{\partial t} \right\rangle_\psi = \frac{1}{V'} \frac{\partial}{\partial t} V' \langle f \rangle_\psi + \frac{1}{V'} \frac{\partial}{\partial \psi} V' \left\langle f \frac{\partial \hat{\psi}}{\partial t} \right\rangle_\psi. \quad (40)$$