

EXPERIMENTAL SETUPS FOR DIFFRACTION

ASPECTS AFFECTING DIFFRACTION EXPERIMENTS

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graph TD; A[ASPECTS AFFECTING DIFFRACTION EXPERIMENTS] --- B[COLLECTION GEOMETRIES]; A --- C[RECORDING ARCHITECTURES]; A --- D[RADIATION SOURCES]; B --> E[RELATED TO DIFFRACTOMETERS, I.E. INSTRUMENT'S SETUP]; C --> F[RELATED TO DETECTORS]; D --> G[CONVENTIONAL SOURCES versus LARGE SCALE FACILITIES (synchrotron & neutrons)];
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**COLLECTION
GEOMETRIES**



RELATED TO
DIFFRACTOMETERS,
I.E. INSTRUMENT'S
SETUP

**RECORDING
ARCHITECTURES**



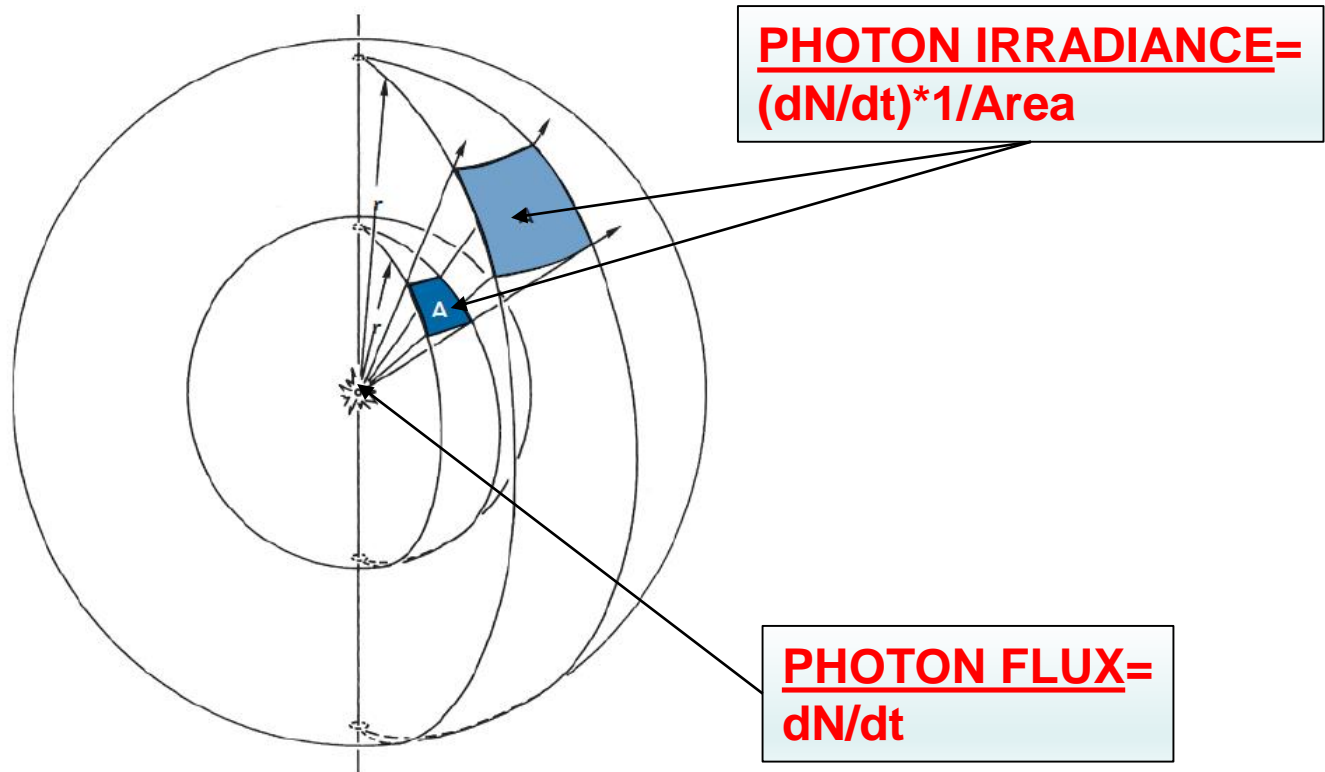
RELATED TO
DETECTORS

**RADIATION
SOURCES**



CONVENTIONAL
SOURCES *versus*
LARGE SCALE
FACILITIES
(synchrotron &
neutrons)

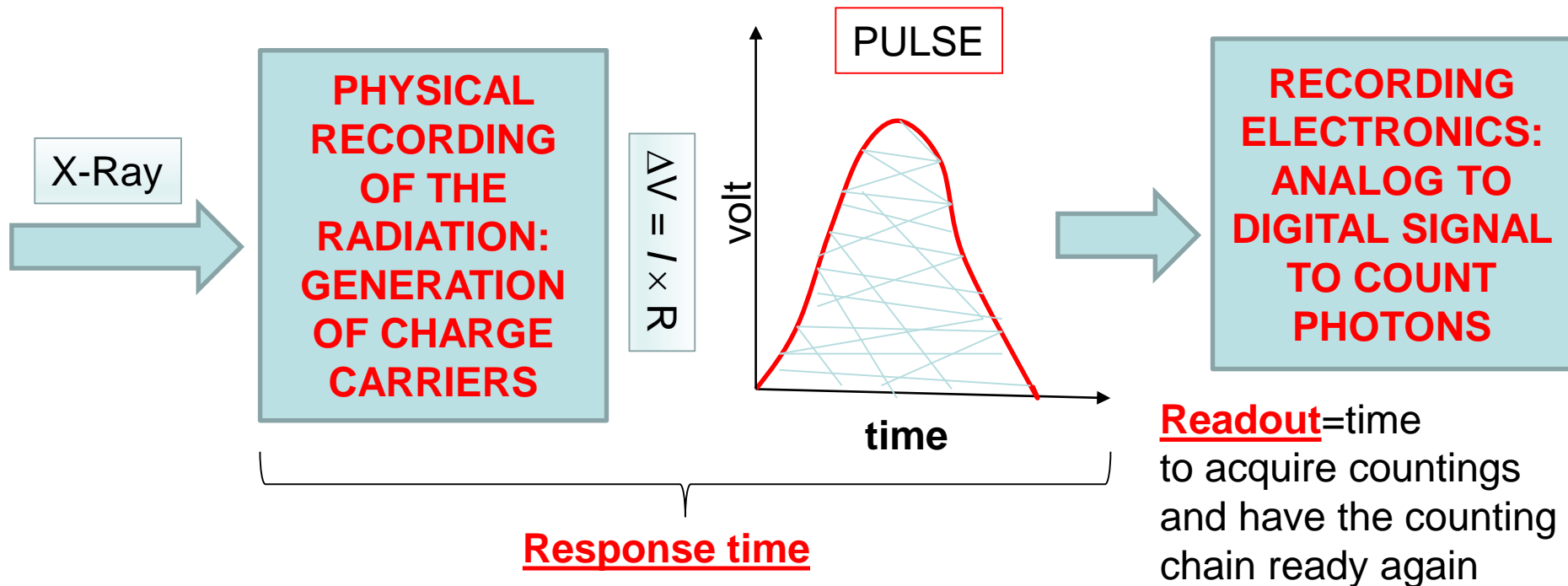
FUNDAMENTAL PHOTON-EMISSION QUANTITIES



WHAT IS A DETECTOR?

Some detector features/parameters

Sensitivity=efficacy to convert radiation into pulse



Dead time=time interval between two events during which a detector is not able to work

Response function=relationship between counted photons and output signal intensity. For instance: linear response

Some detector parameters

Energy resolution = $\Delta E, \Delta E/E$; Capacity to discriminate between photons with a ΔE difference

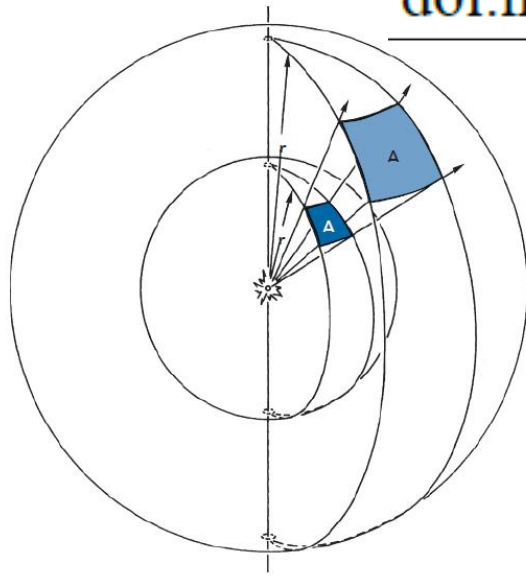
Total Efficiency

Intrinsic efficiency

$$\epsilon_{\text{int eff}} = \frac{N(\text{photons recorded})}{N(\text{photons on detector})}$$

Geometrical acceptance ϵ_{geom}

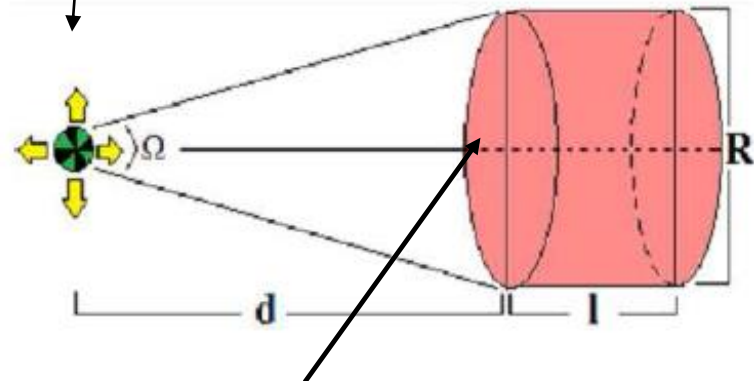
$$\epsilon_{\text{total}} = \frac{N(\text{photons recorded})}{N(\text{photons produced})} = \epsilon_{\text{int eff}} * \epsilon_{\text{geom}}$$



Geometrical acceptance

Total efficiency

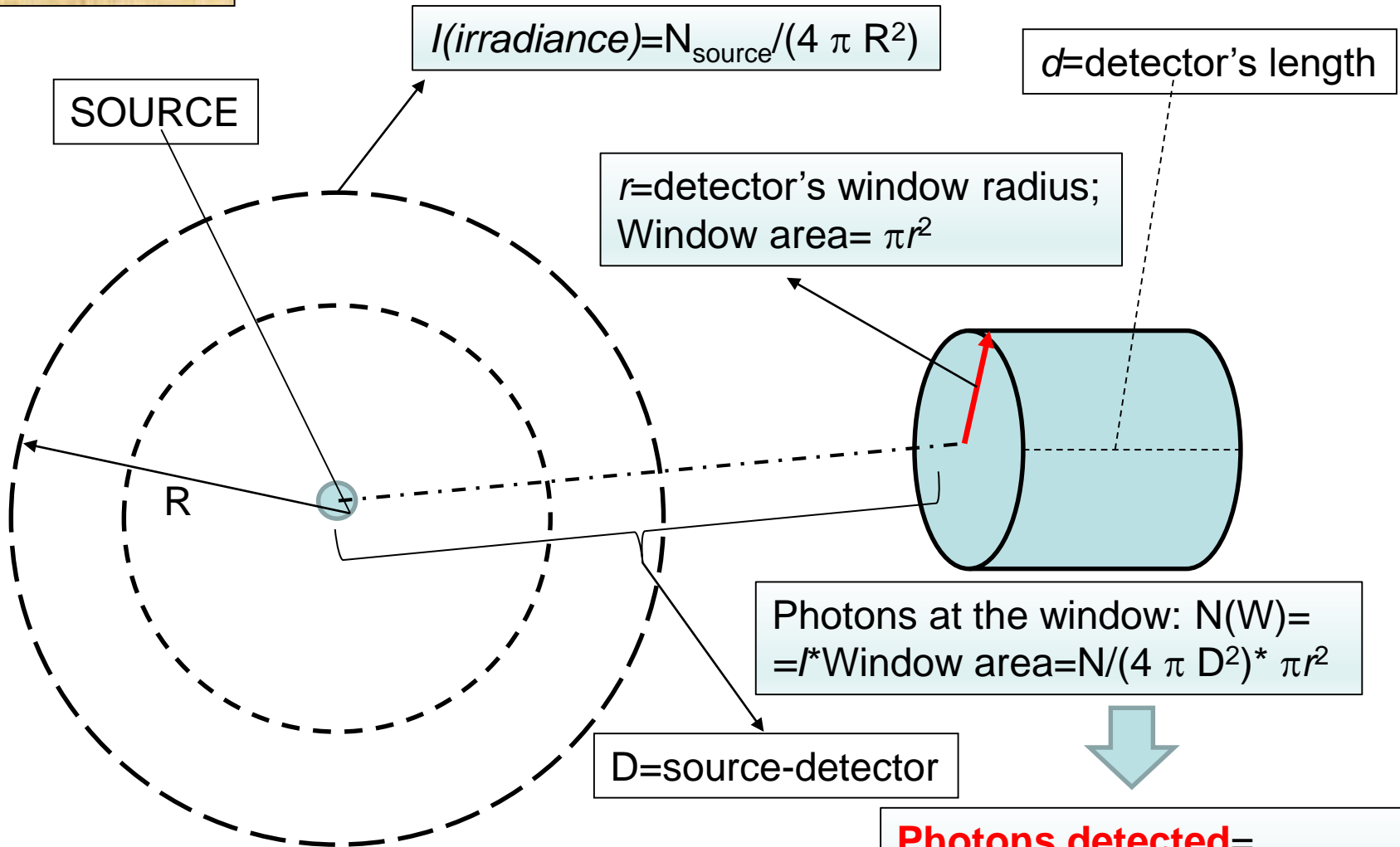
DOI: 10.12693/APhysPolA.128.B-332



SENSITIVE AREA
EFFECTIVE SENSITIVE AREA, I.E. HOMOGENEOUS RESPONSIVITY

Intrinsic efficiency=it is related to the incident photons' energy and detecting mechanism

AN EXAMPLE (a)



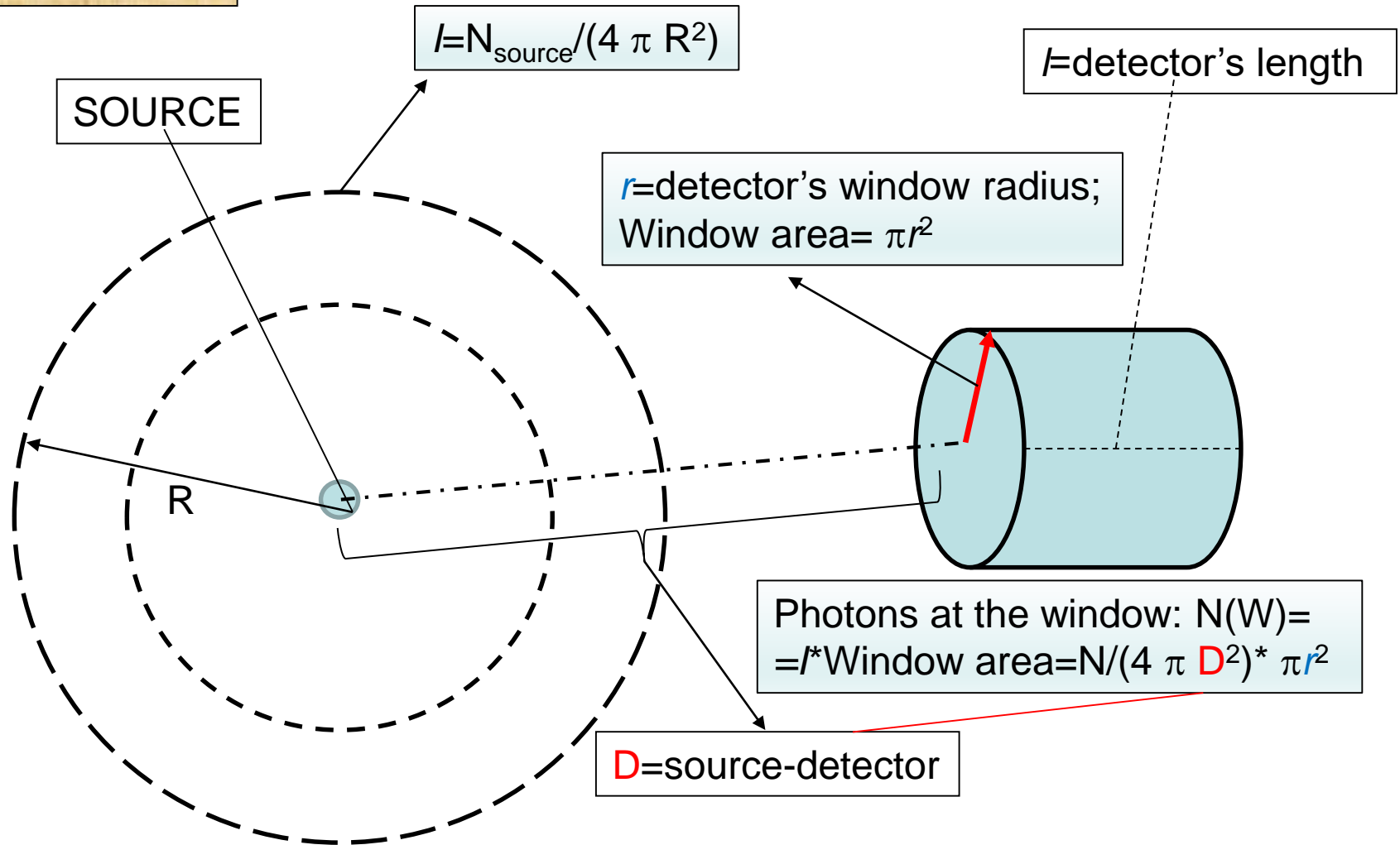
Photons detected=
 $N(W) * \text{prob. being recorded} =$
 $N / (4 \pi D^2) * \pi r^2 * [1 - \exp(-\mu d)]$

$\mu(\lambda)$

Total efficiency=
 Photons detected/
 Photons of source

Total efficiency~
 $(1/4 r^2/D^2) \times [1 - \exp(-\mu d)]$

AN EXAMPLE (b)



Geometrical acceptance $= \pi r^2 / (4 \pi D^2)$

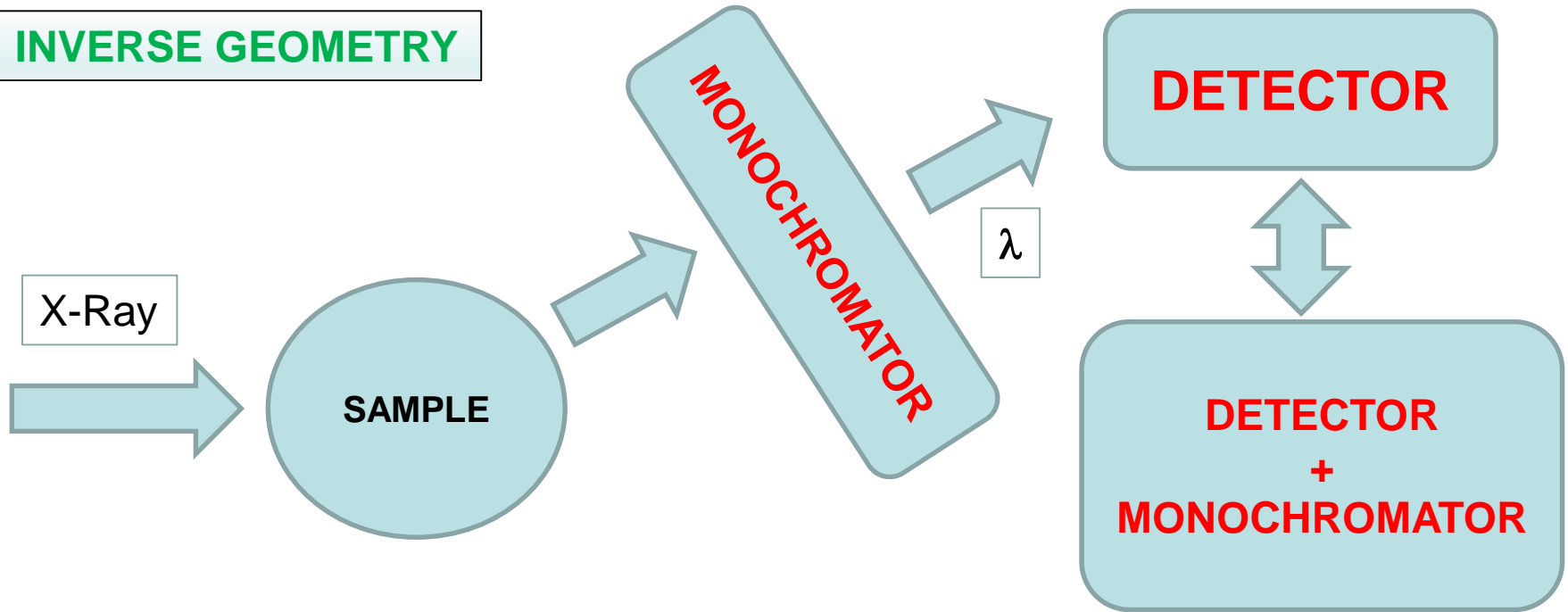
Intrinsic efficiency \sim

$1 - \exp(-\mu l) = \text{probability that a photon is absorbed}$

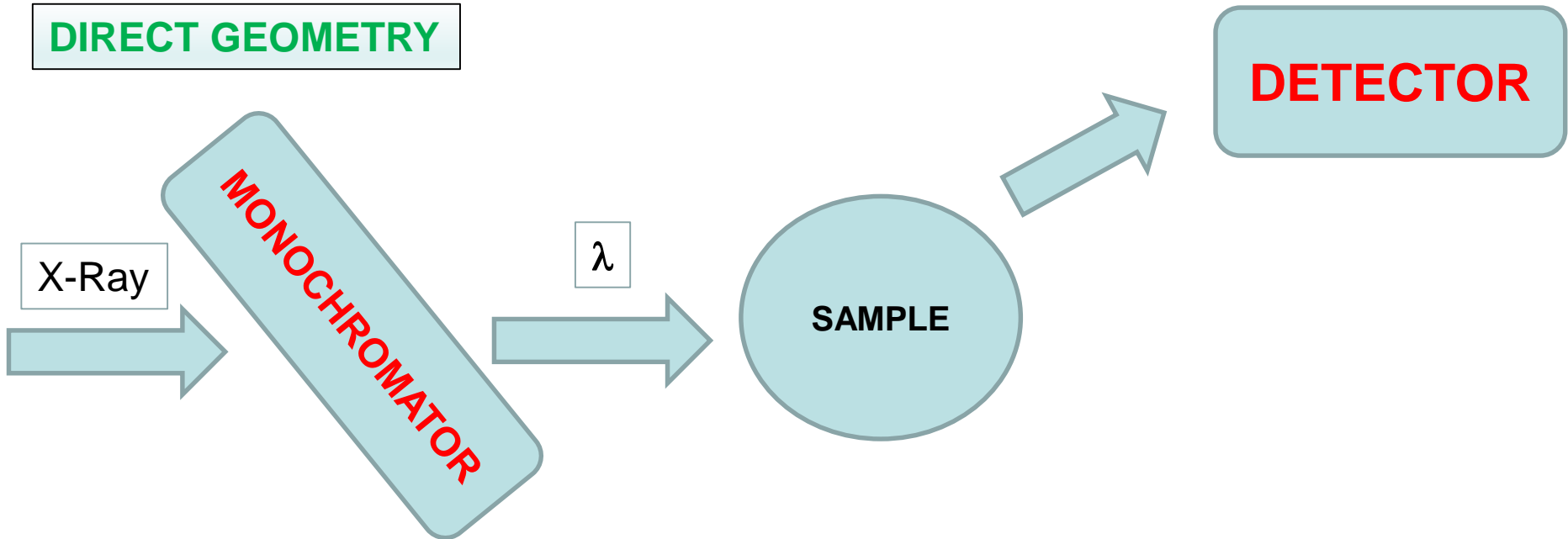
Total efficiency $\sim (1/4) r^2 / D^2 \times [1 - \exp(-\mu l)]$

$\mu(\lambda)$

INVERSE GEOMETRY



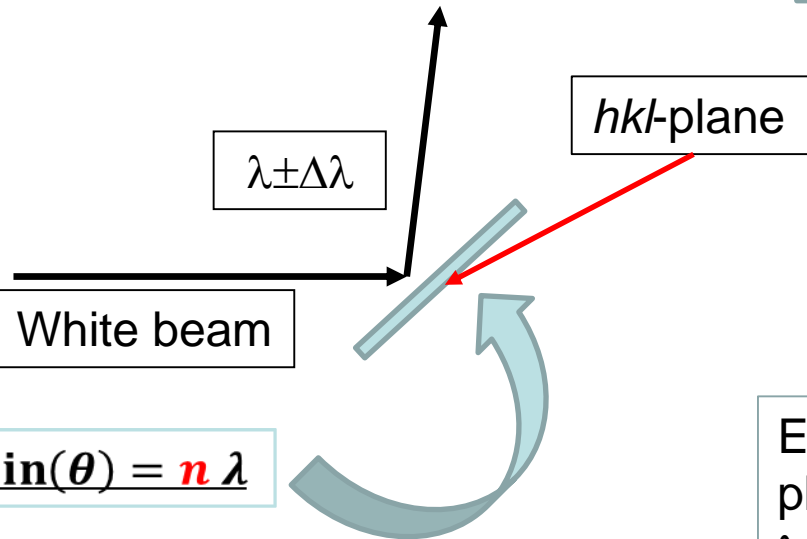
DIRECT GEOMETRY



MONOCHROMATOR

CRYSTAL DISCRIMINATOR

ELECTRONIC DISCRIMINATION



(constructive interference between waves)

Electronics to discriminate between photons and select those having λ Around a given value

SINGLE CRYSTAL DIFFRACTION

RADIATION COLLECTION ARCHITECTURES

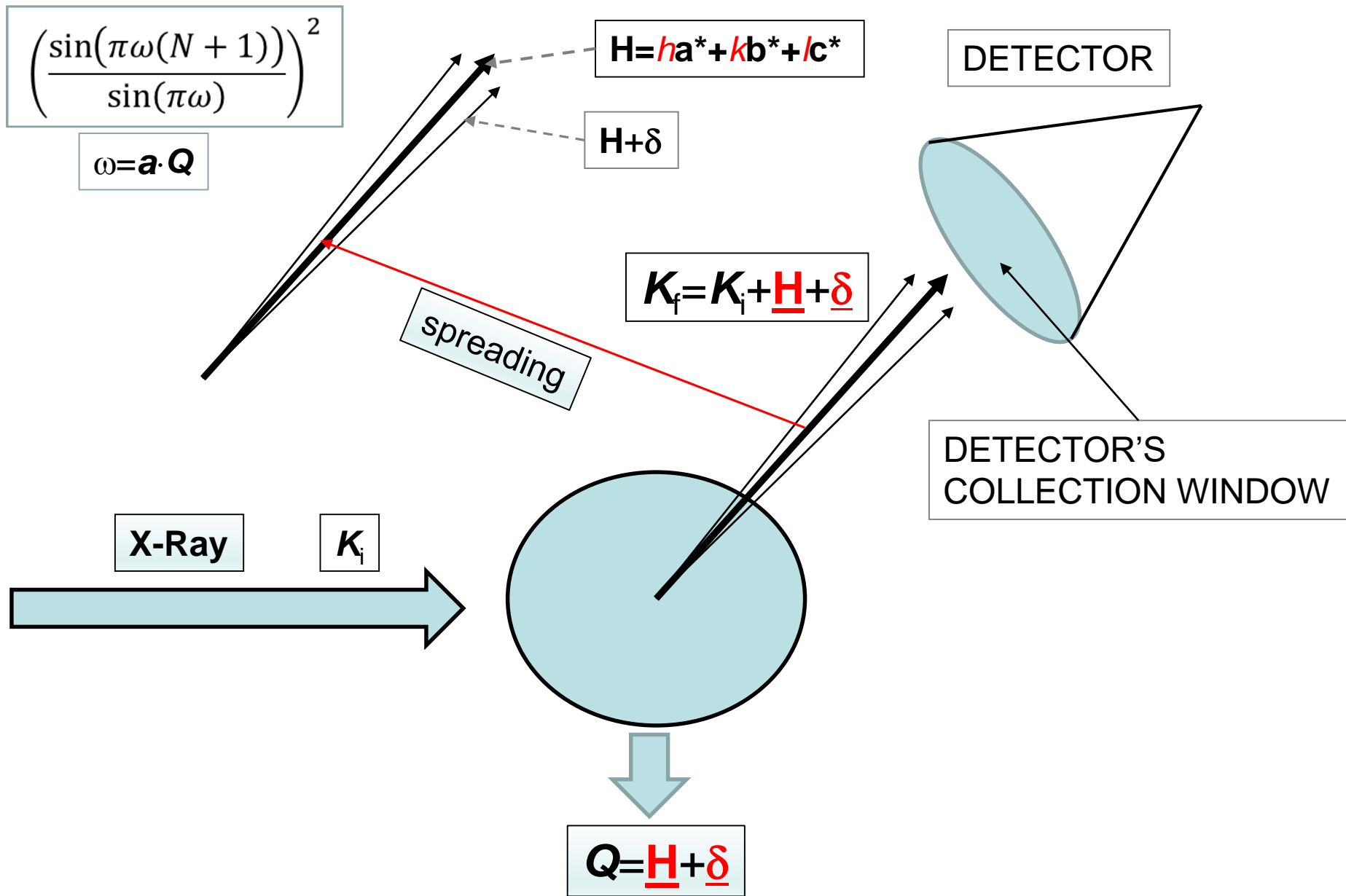
SINGLE CRYSTAL

OLD APPROACH:
POINT
DETECTORS

**ONE DIFFRACTED
BEAM AT A TIME**

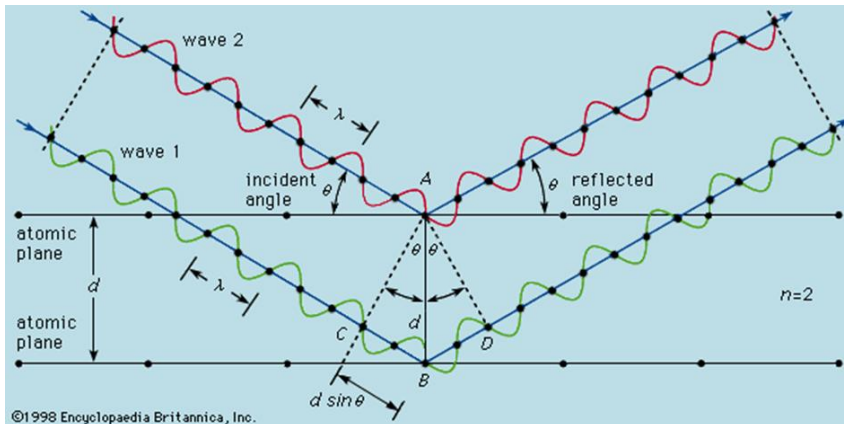
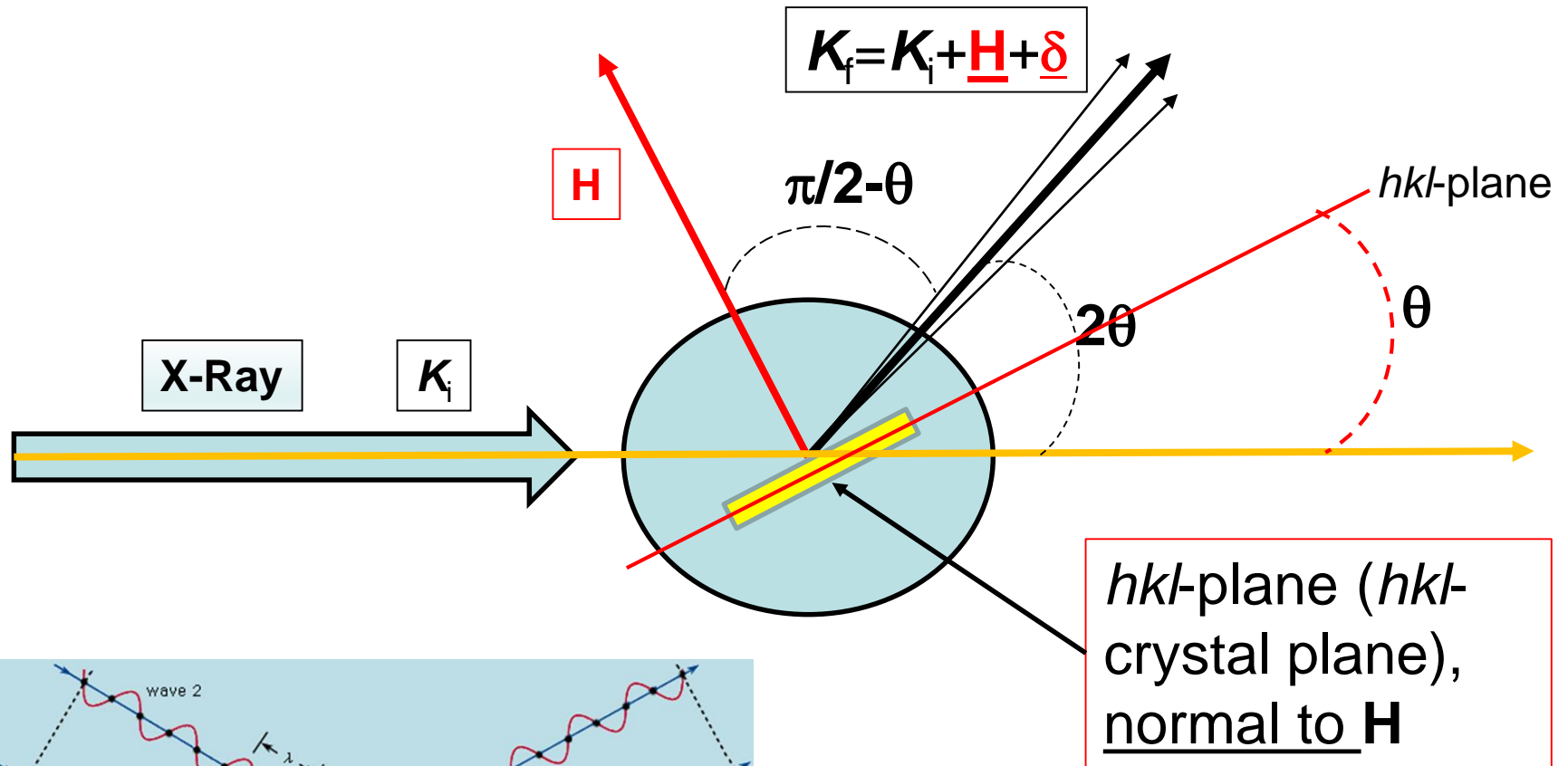
NOWADAYS: POSITION
SENSITIVE/AREA
DETECTORS

**MANY DIFFRACTED
BEAMS AT A TIME**

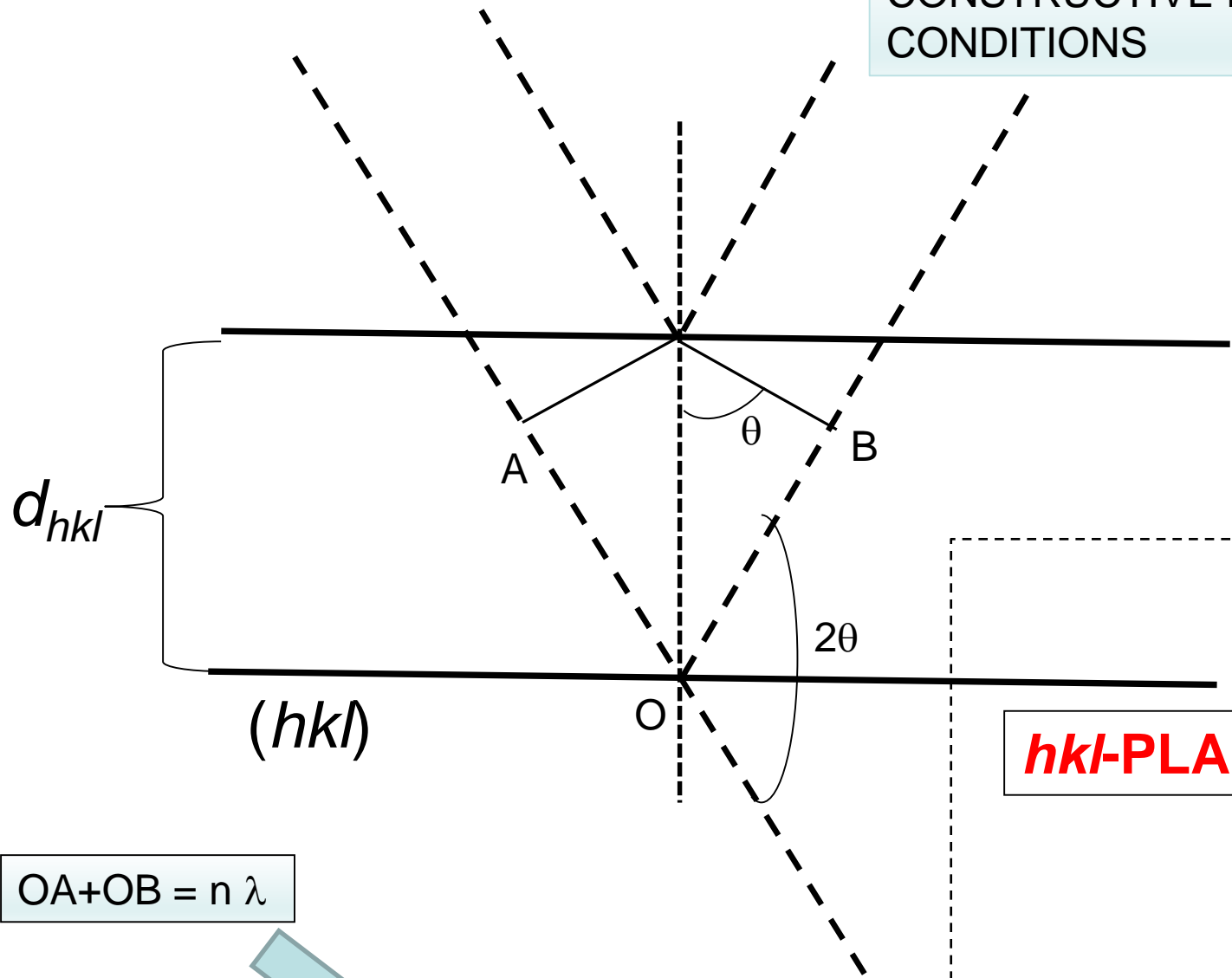


X-RAY SINGLE CRYSTAL EXPERIMENTAL PHENOMENOLOGY

BRAGG DIFFUSION & *hkl*-PLANES

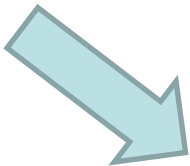


CONSTRUCTIVE INTERFERENCE
CONDITIONS



hkl -PLANE FAMILY

$OA + OB = n \lambda$



$2 d_{hkl} \sin(\theta) = \lambda$

Diffracted beam

Normal to plane

$$2 d_{hkl}^0 \sin(\theta^0) = \lambda$$

$$\pi/2 - \theta^0$$

Incident beam

d_{hkl}^0

(hkl^0) -family

**HOW DO TWO
 hkl -FAMILIES
BEHAVE?**

$$2 d_{hkl}^1 \sin(\theta^1) = \lambda$$

(hkl^1) -family

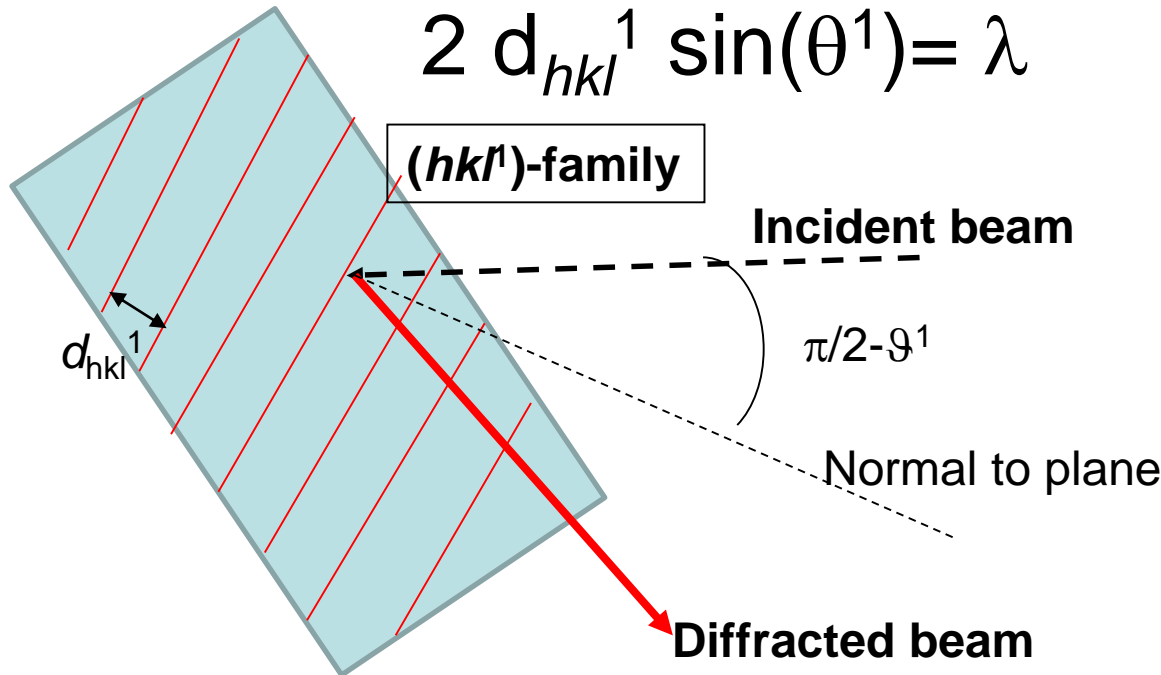
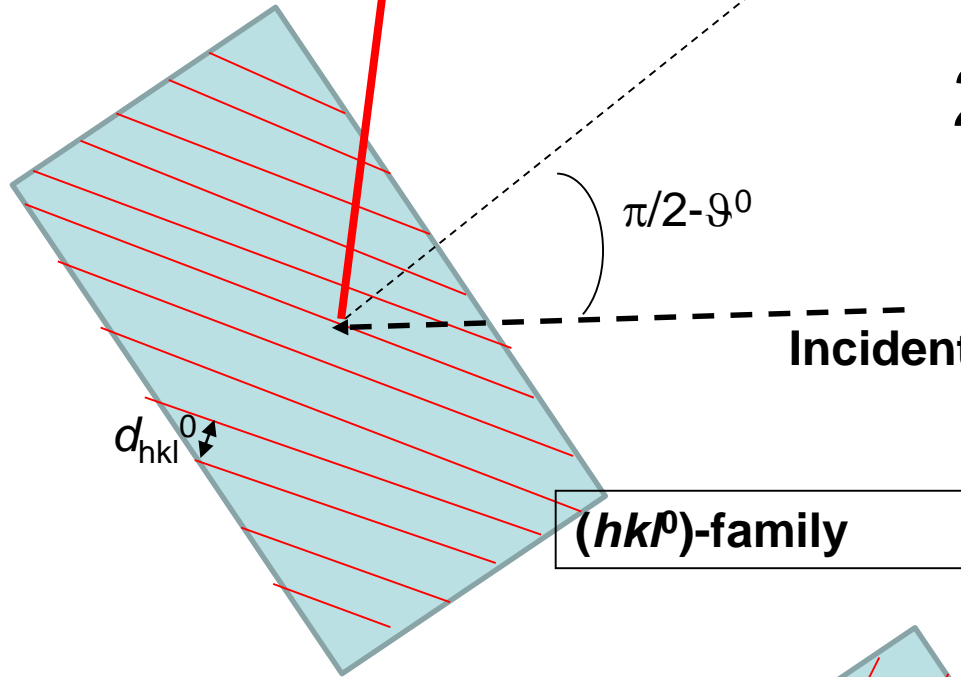
Incident beam

$$\pi/2 - \theta^1$$

Normal to plane

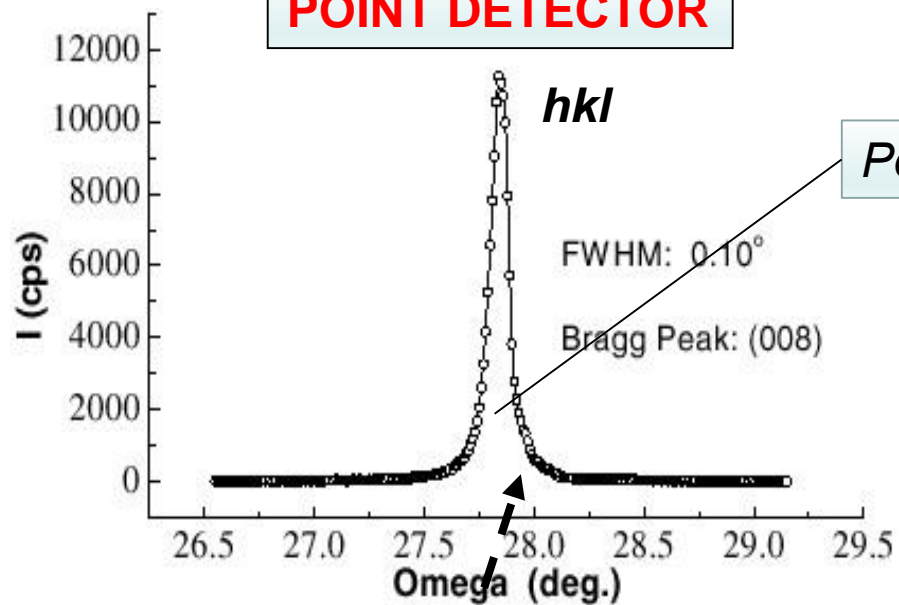
d_{hkl}^1

Diffracted beam



SINGLE CRYSTAL DIFFRACTION

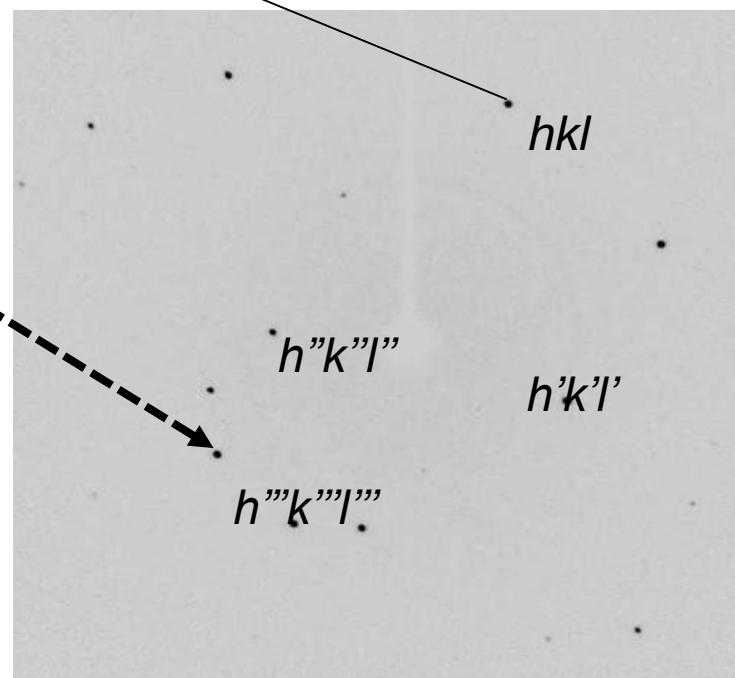
POINT DETECTOR



Peak's area

Reflection Intensity

Spot's area



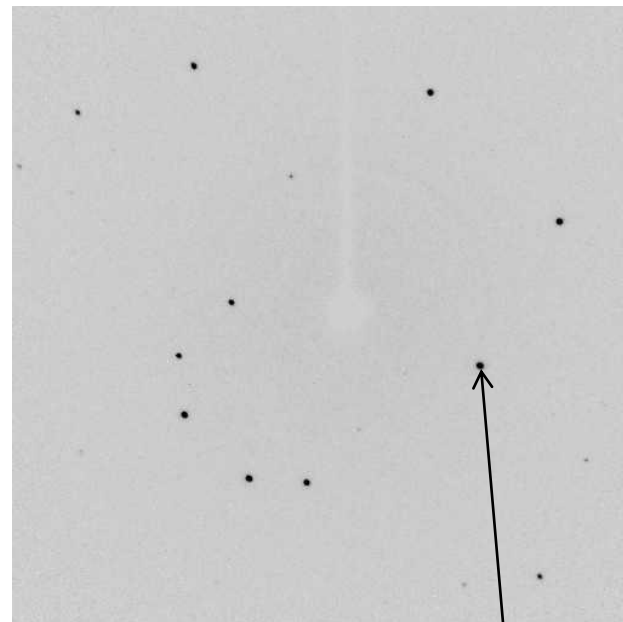
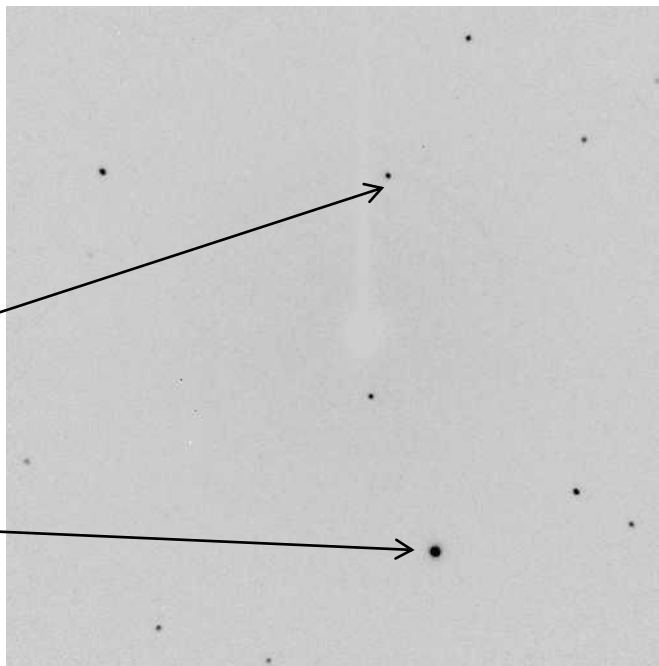
AREA DETECTOR

SINGLE CRYSTAL DIFFRACTION

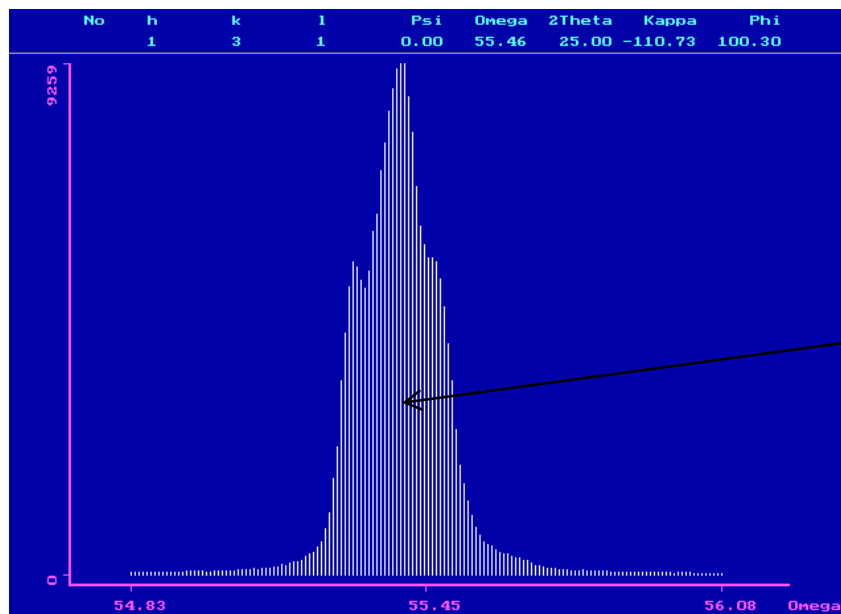
Area detector

$h'k'l'$

hkl

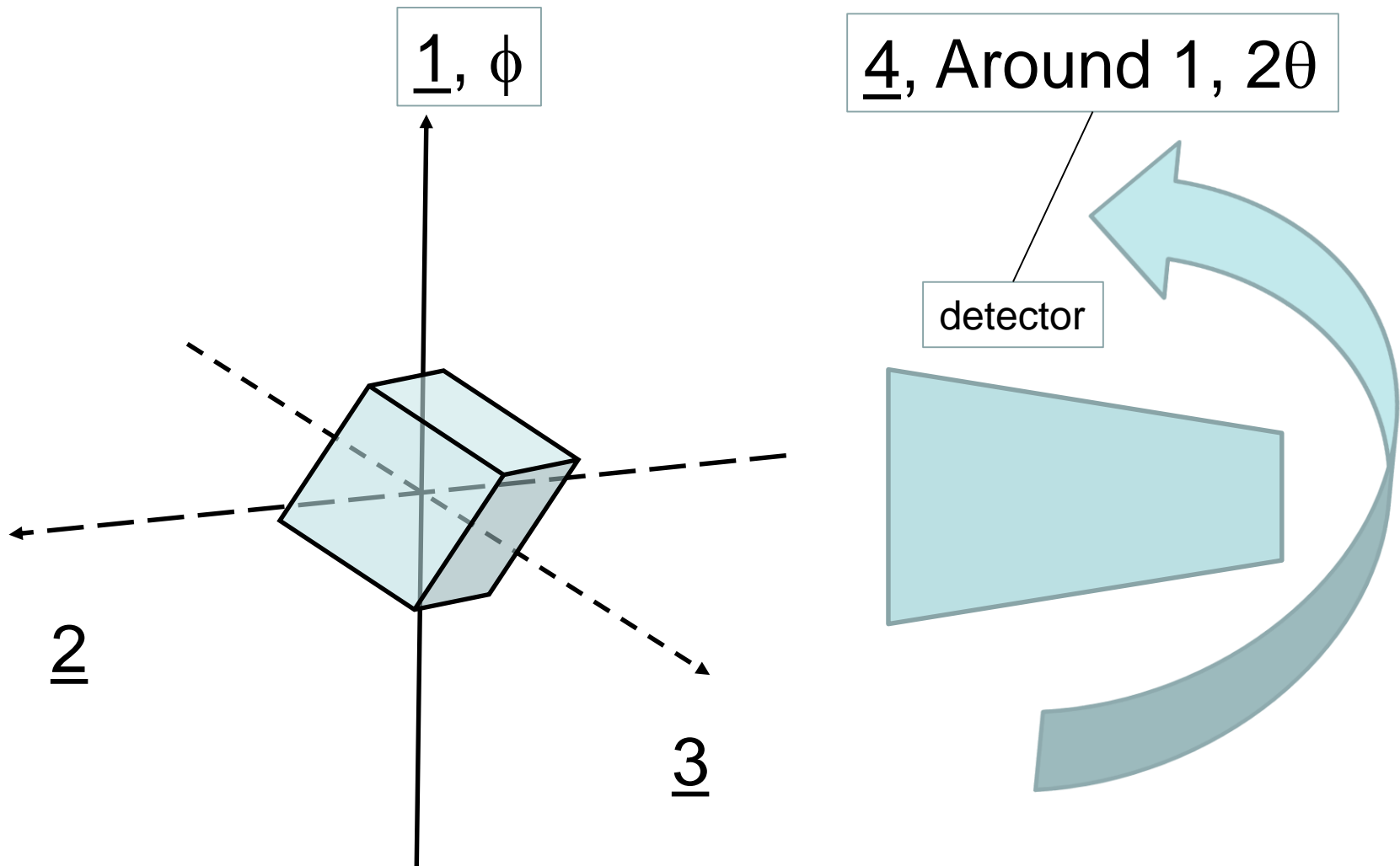


$h''k''l''$



Point detector

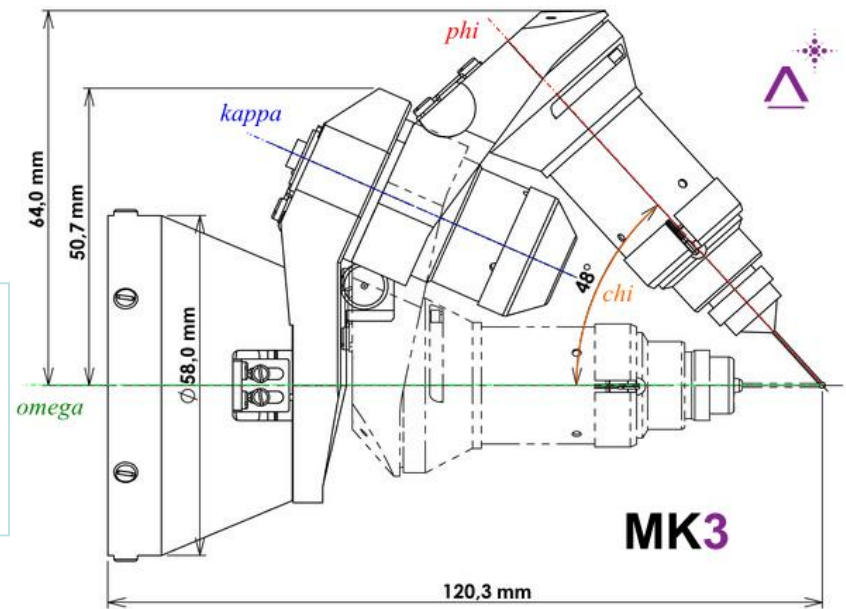
hkl



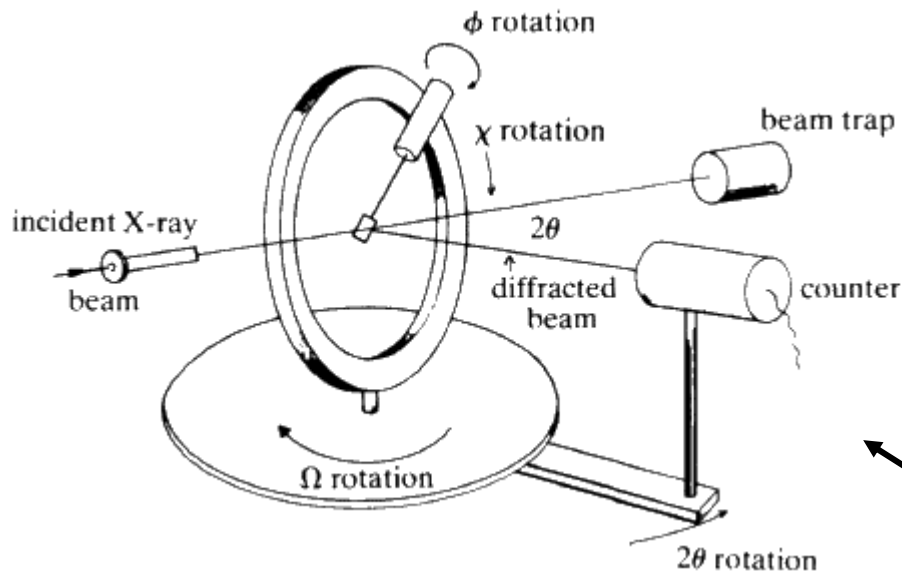
FOUR AXES PRINCIPLE FOR SINGLE CRYSTAL DIFFRACTION

SINGLE CRYSTAL DIFFRACTOMETER

4 ROTATION AXES THAT ALLOW ONE
TO ORIENT A CRYSTAL IN ANY
POSSIBLE WAY WITH RESPECT TO
A DETECTOR

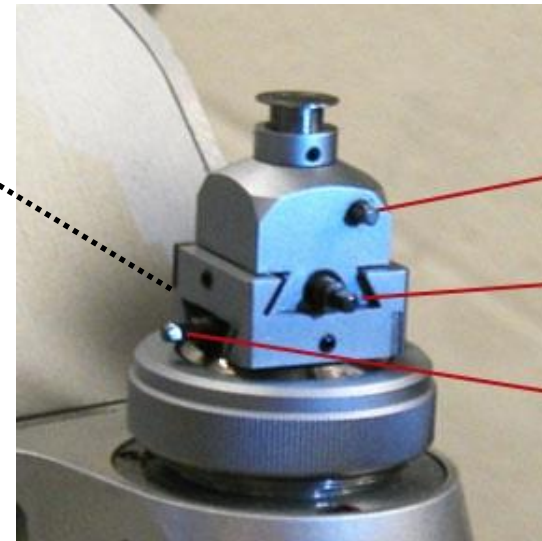
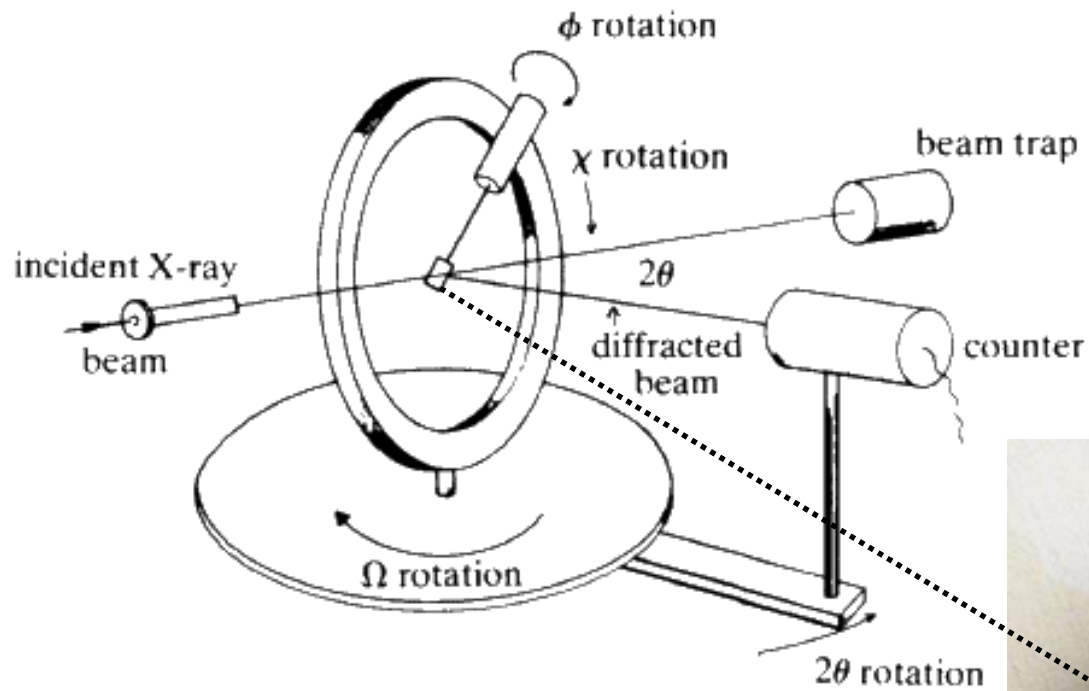


K-GEOMETRY



EULERIAN GEOMETRY

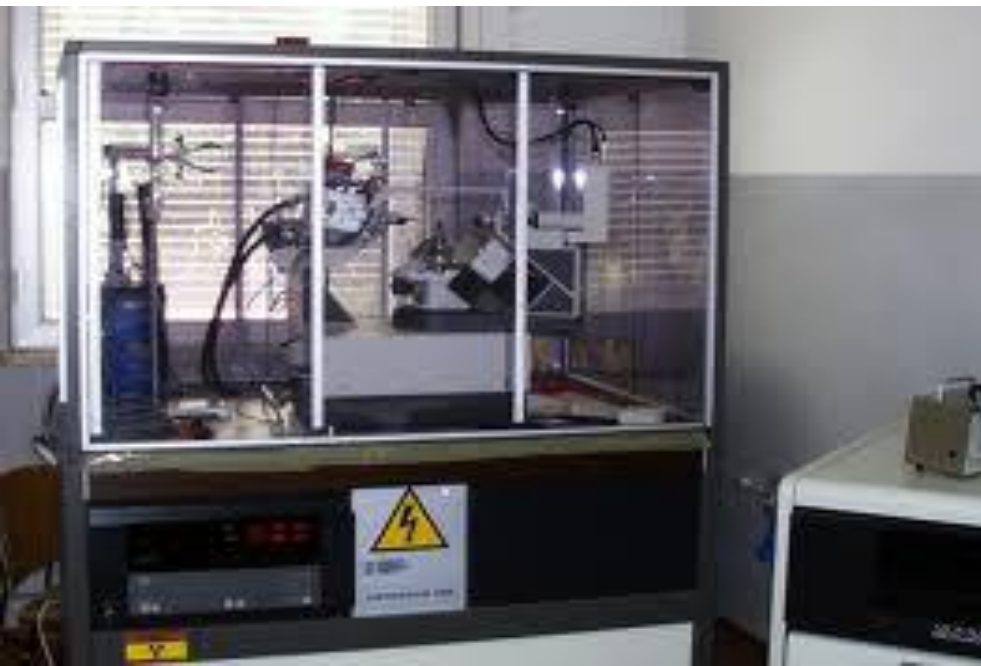
SINGLE CRYSTAL X-RAY DIFFRACTOMETERS



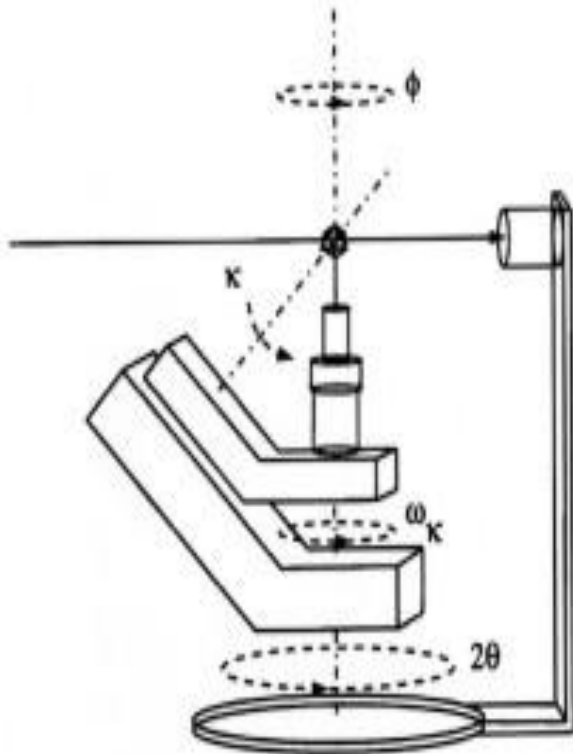
UP / DOWN

SIDE-to-SIDE

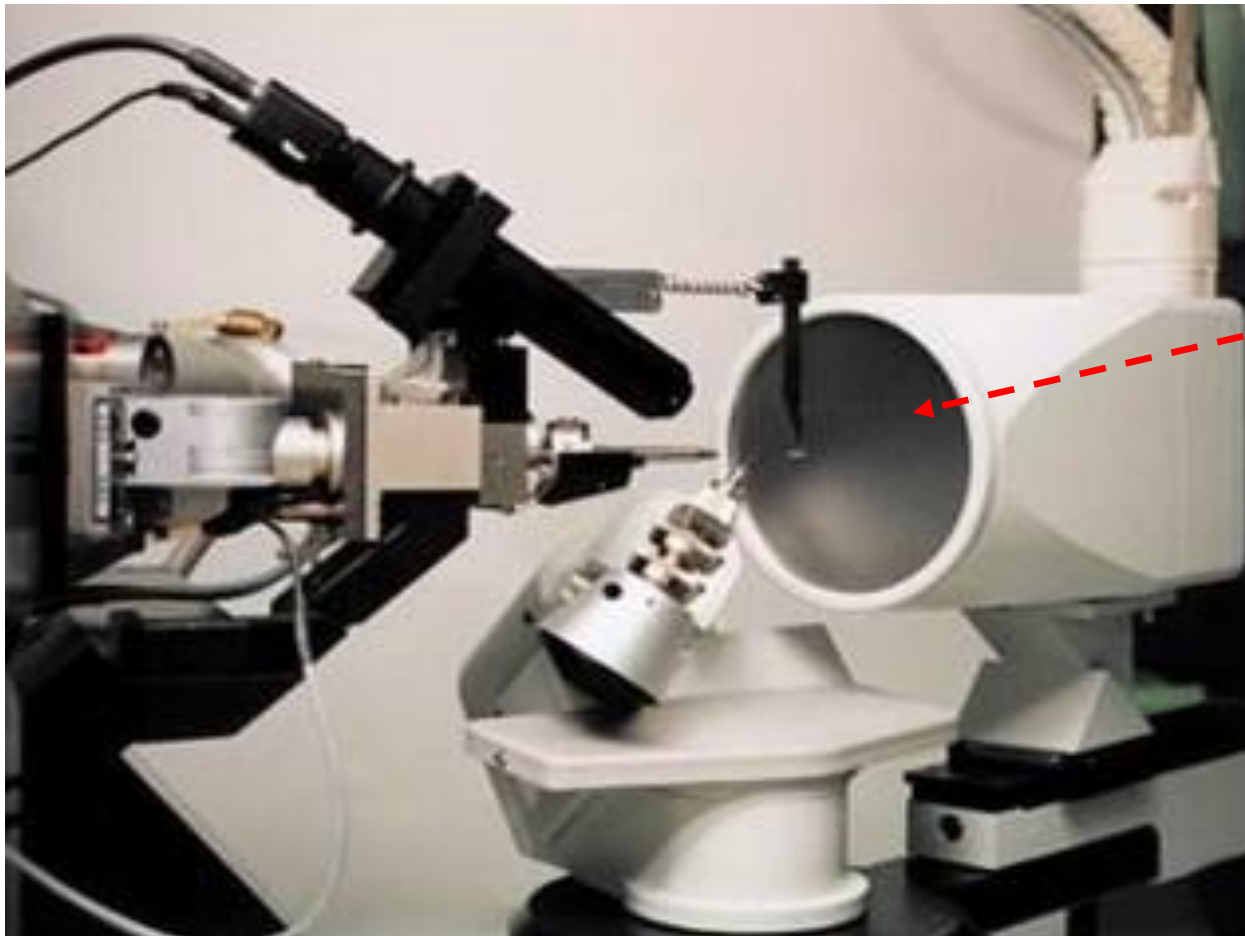
SIDE-to-SIDE



K-GEOMETRY



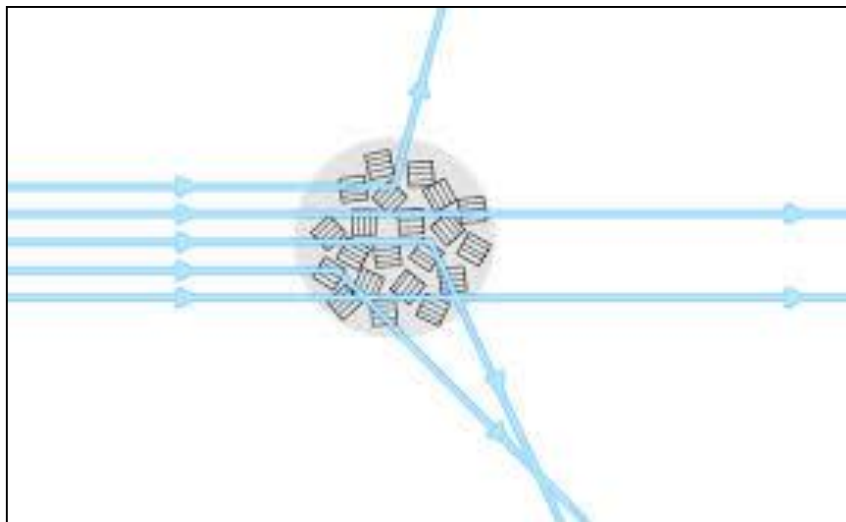
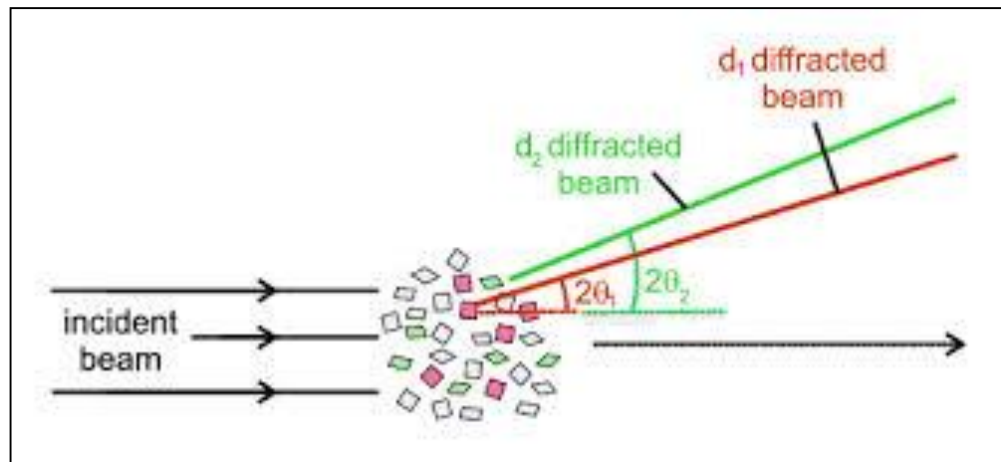
**POSITION SENSITIVE/AREA DETECTOR,
CHARGE COUPLED DEVICE (CCD)**



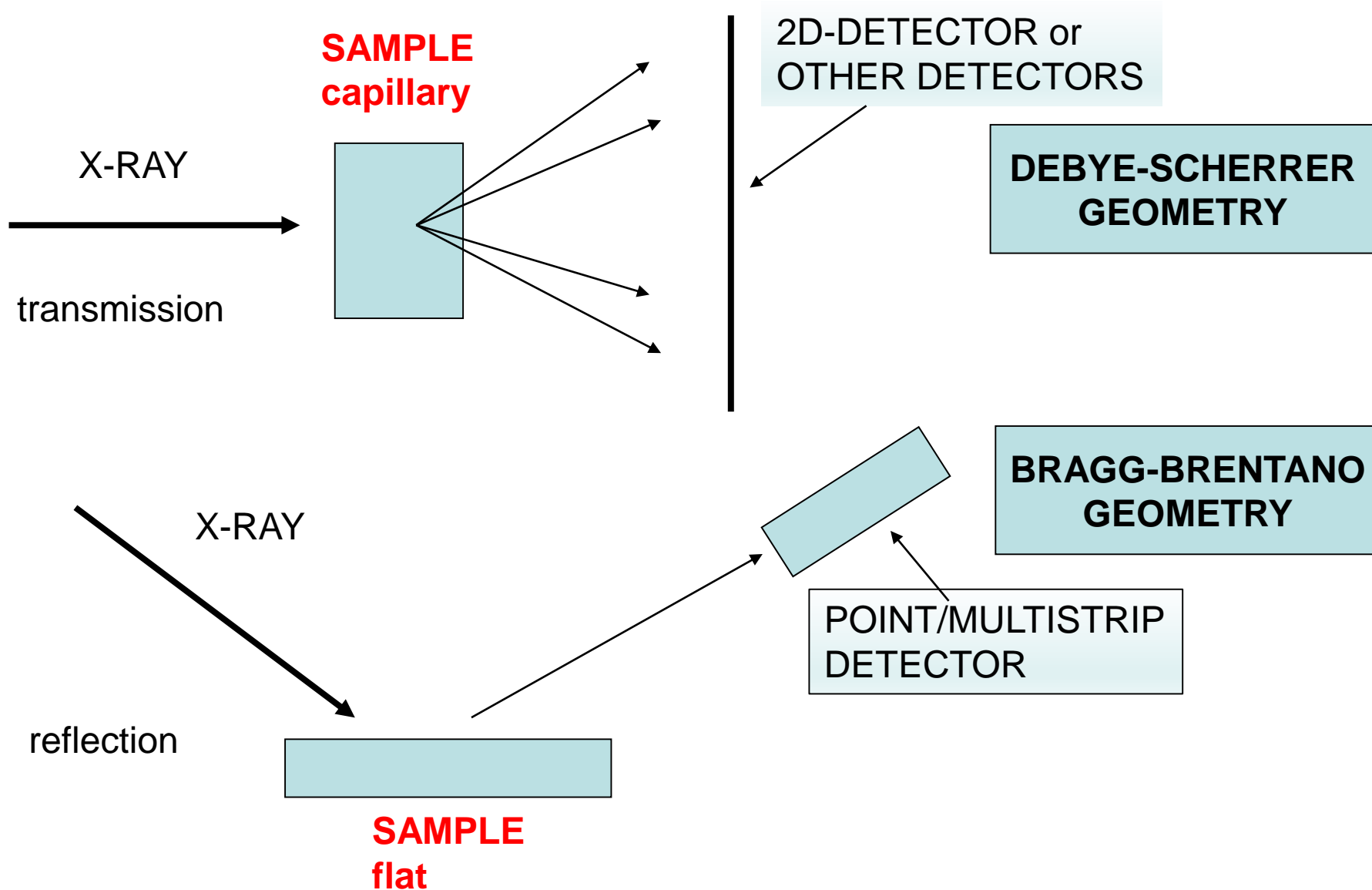
2D-DETECTOR

POWDER DIFFRACTION

POWDER DIFFRACTION

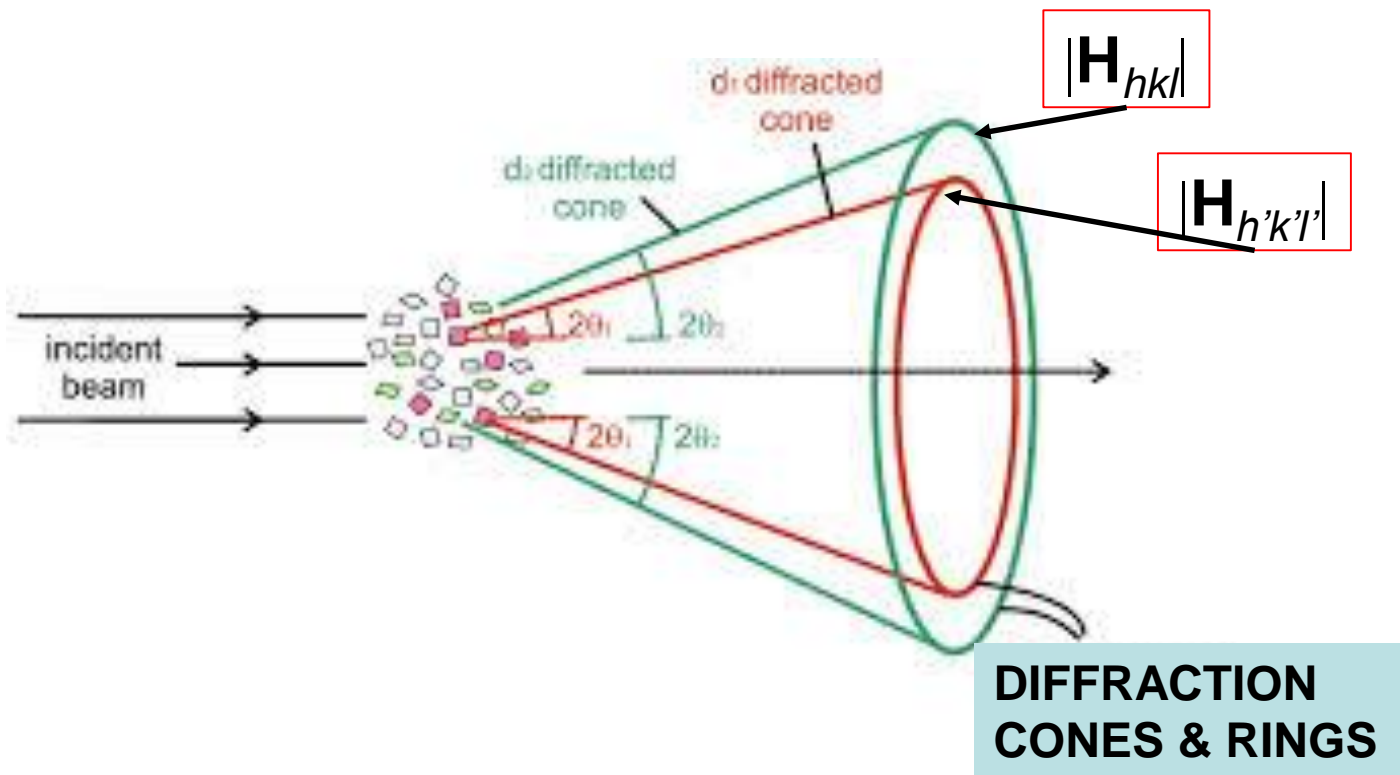


EXPERIMENTAL GEOMETRIES FOR POWDER DIFFRACTION



DEBYE-SCHERRER

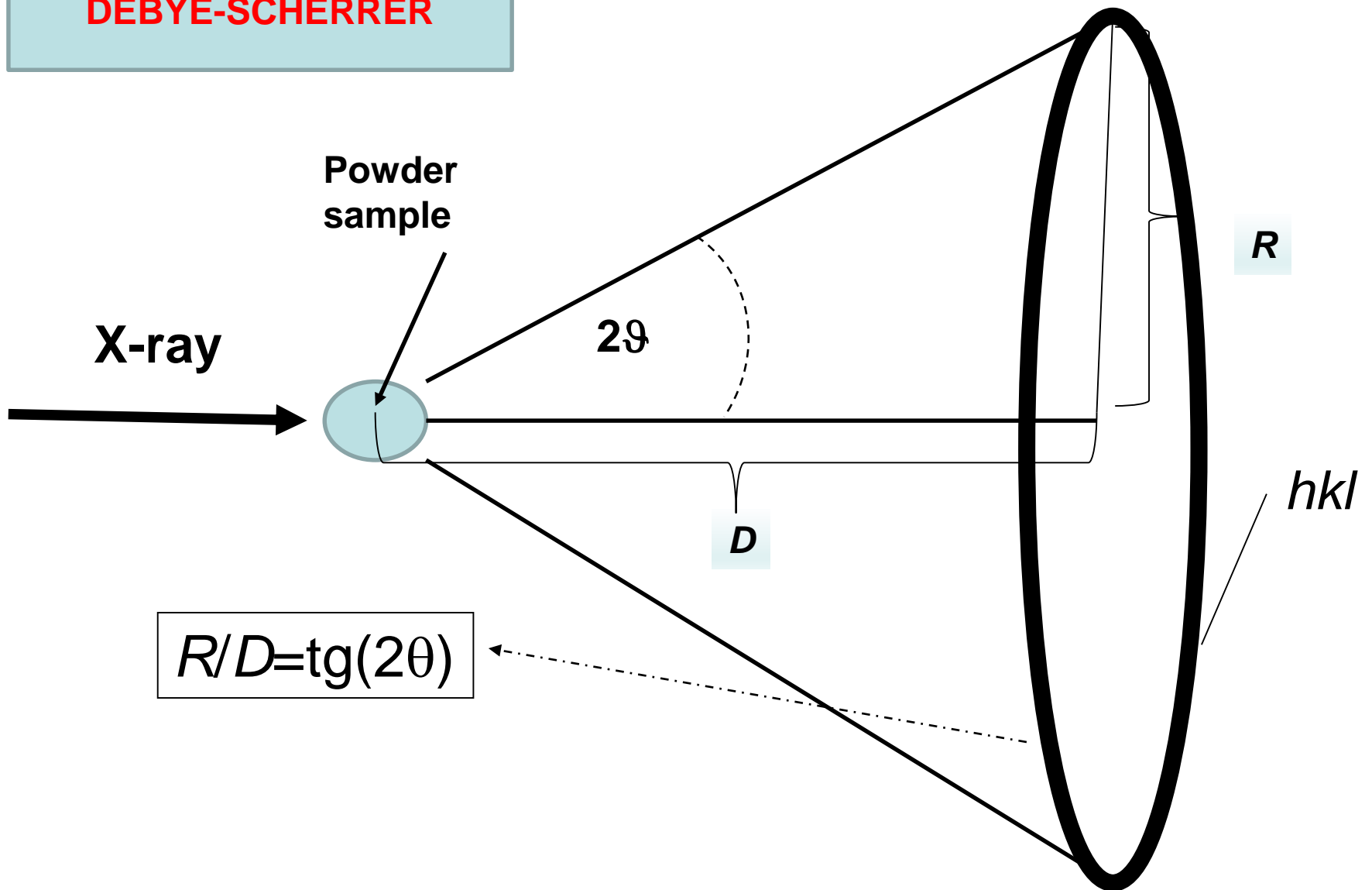
POWDER DIFFRACTION INTENSITY DISTRIBUTION



ON EACH CONE SURFACE LIE THE DIFFRACTED BEAMS CHARACTERISED BY THE SAME $|\mathbf{H}|$, I.E. SUCH AS TO FULFIL THE BRAGG LAW AT THE SAME 2θ ANGLE

$$\frac{2}{|\mathbf{H}|} \sin(\theta_{hkl}) = \lambda$$

POWDER DIFFRACTION
DEBYE-SCHERRER



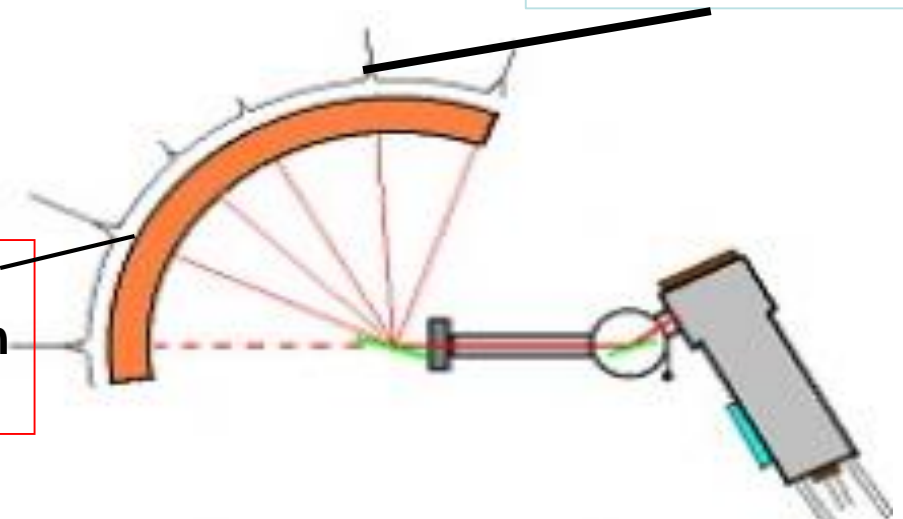
THE RESULTING PATTERN DEPENDS ON HOW A
DETECTOR INTERSECTS THE DIFFRACTION CONES

POWDER DIFFRACTION-POSITION SENSITIVE/AREA DETECTORS

A

INEL-geometry
Multi-channel design
«position sensitive»

Resulting profile

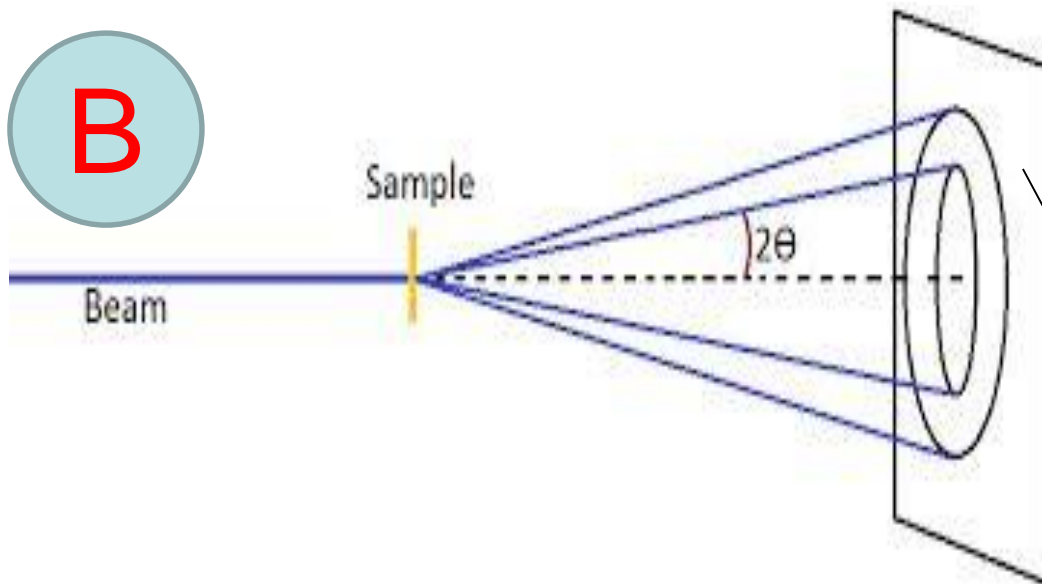


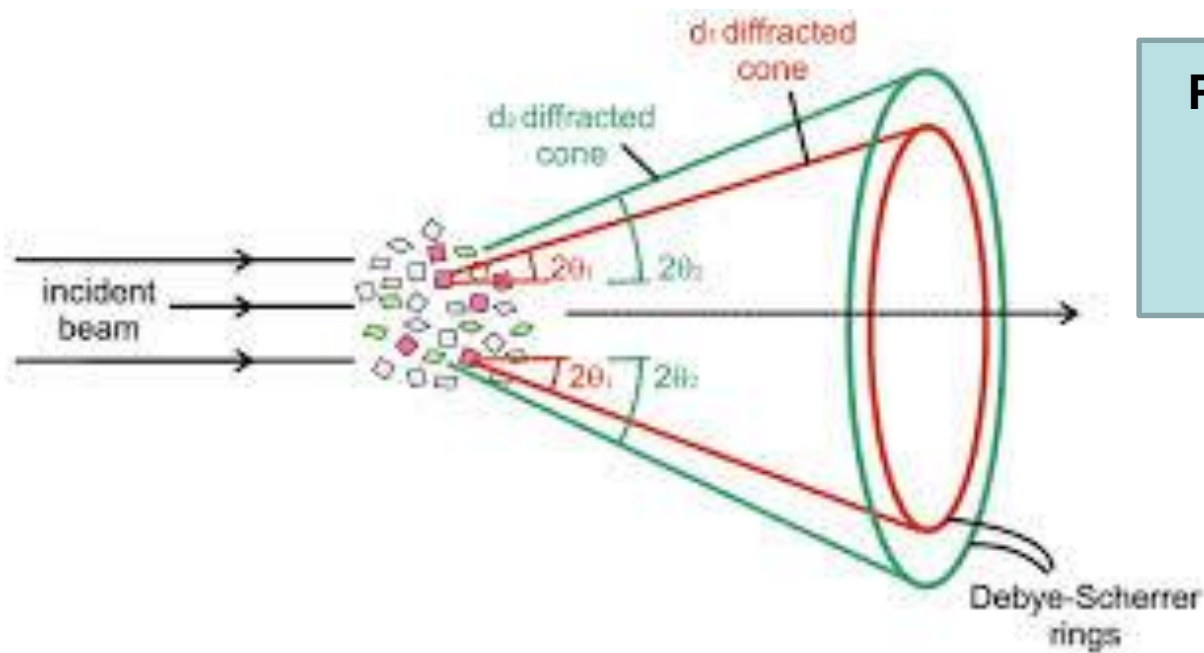
X-ray tube

B

Sample

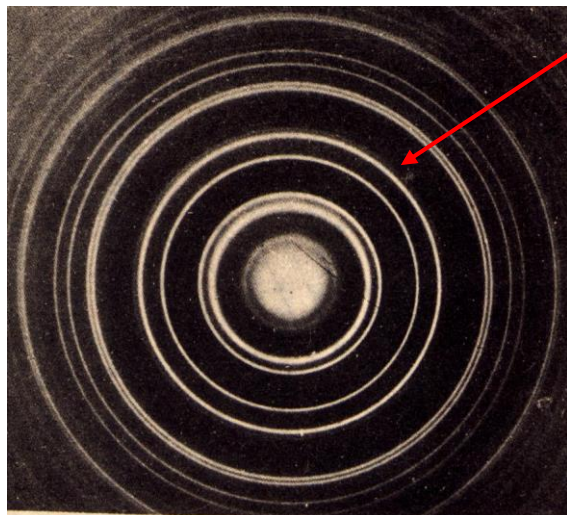
2D-detector



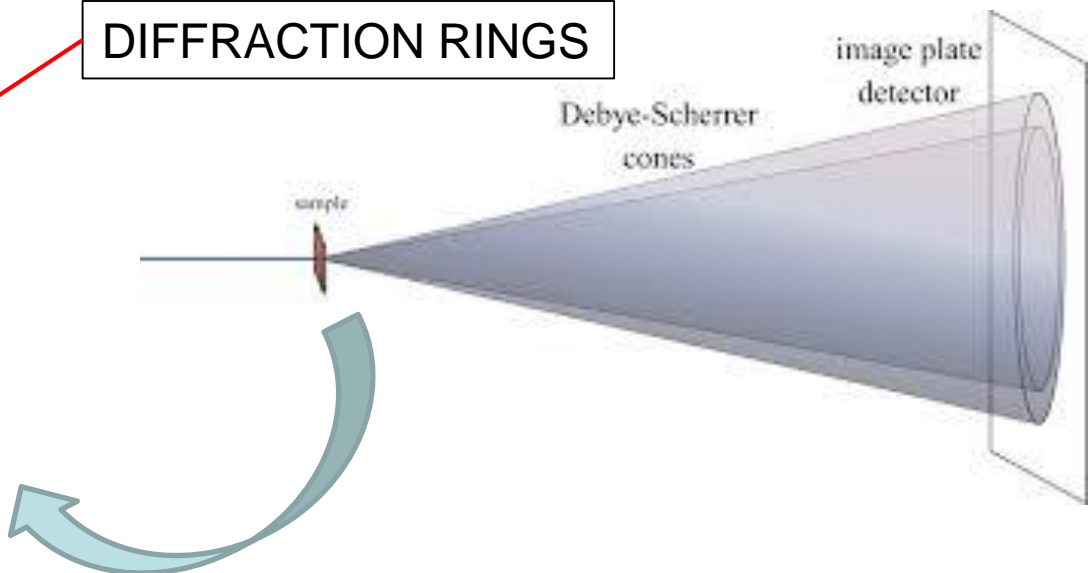


POWDER DIFFRACTION DEBYE-SCHERRER & 2D-DETECTOR

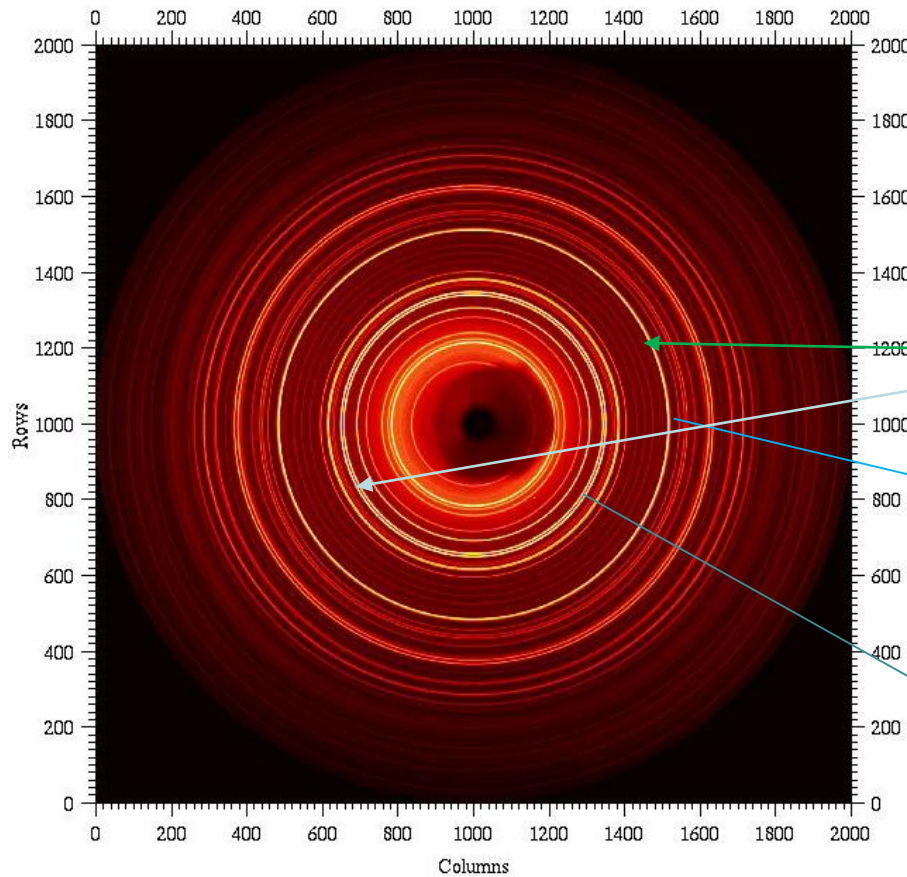
OUTPUT



DIFFRACTION RINGS



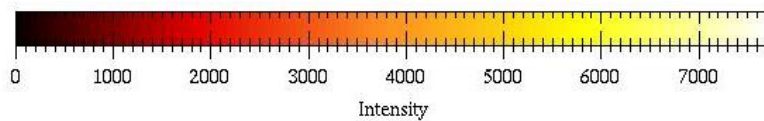
OLIVINE POWDER DIFFRACTION
PATTERN COLLECTED BY
A **DEBYE GEOMETRY**



DIFFRACTION RINGS

$2 d' \sin(\theta') = \lambda$

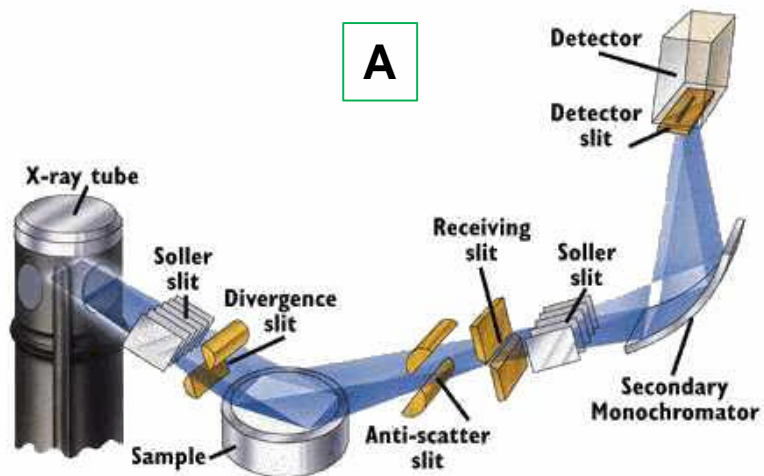
$2 d'' \sin(\theta'') = \lambda$



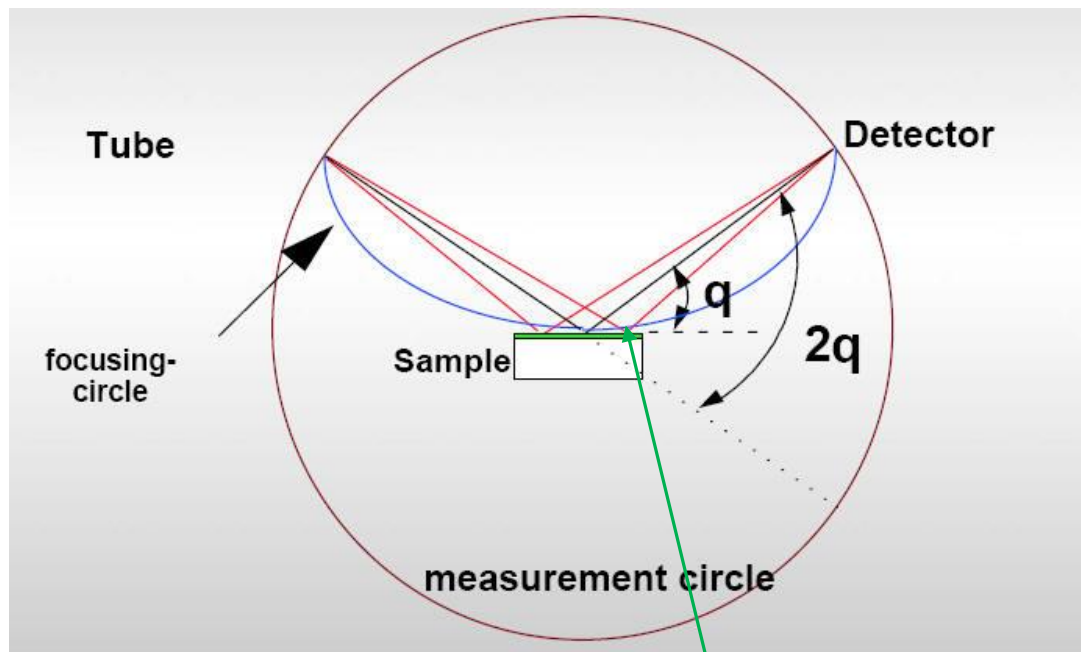
BRAGG-BRENTANO

BRAGG-BRENTANO GEOMETRY

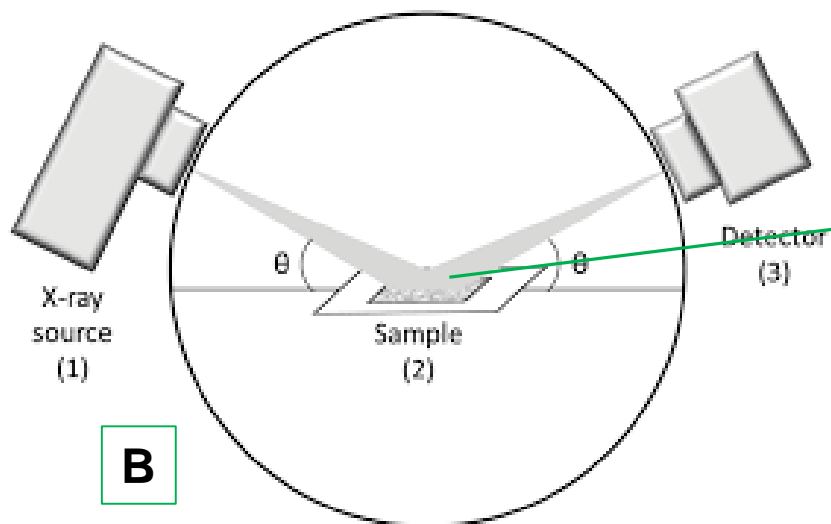
A



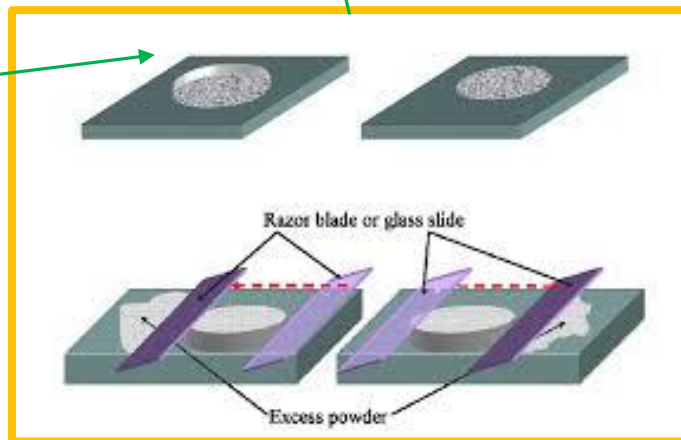
D



B



C



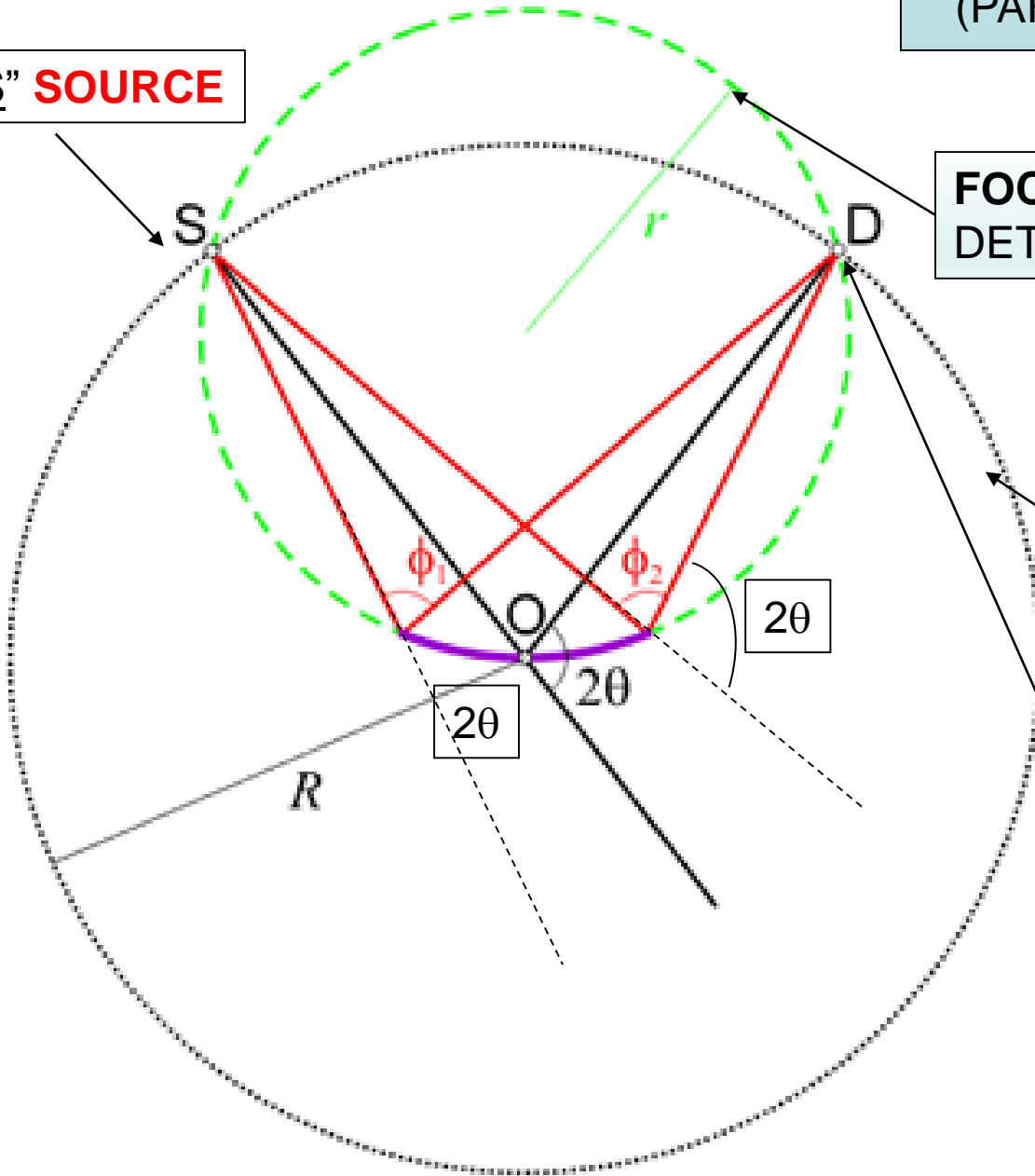
BRAGG-BRENTANO GEOMETRY (PARAFOCUSING GEOMETRY)

“S” SOURCE

FOCUSING CIRCLE: S-D-O
DETERMINE FOCUSING CIRCLE

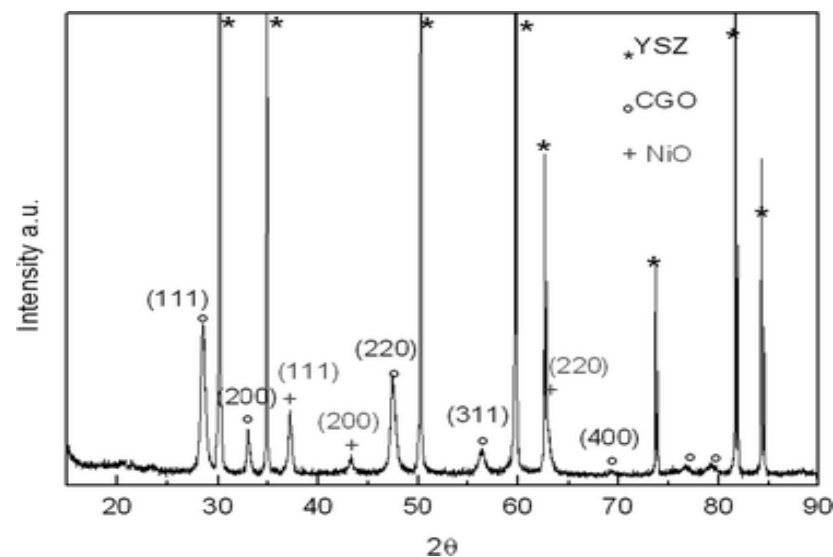
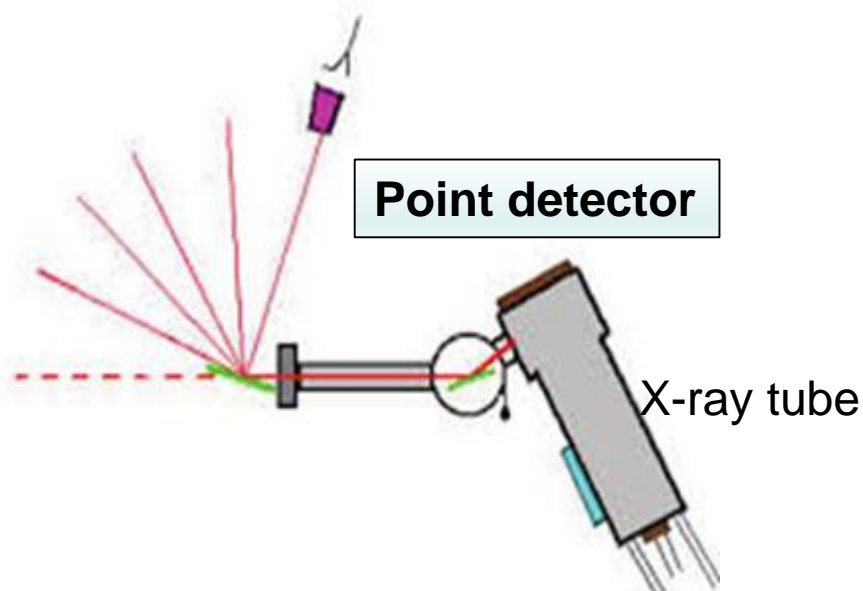
GONIOMETER CIRCLE:
CENTRED ON O; S and D
LIE ON

«D» (**DETECTOR**)
GATHERS ALL
SIGNALS SCATTERED
AT 2θ

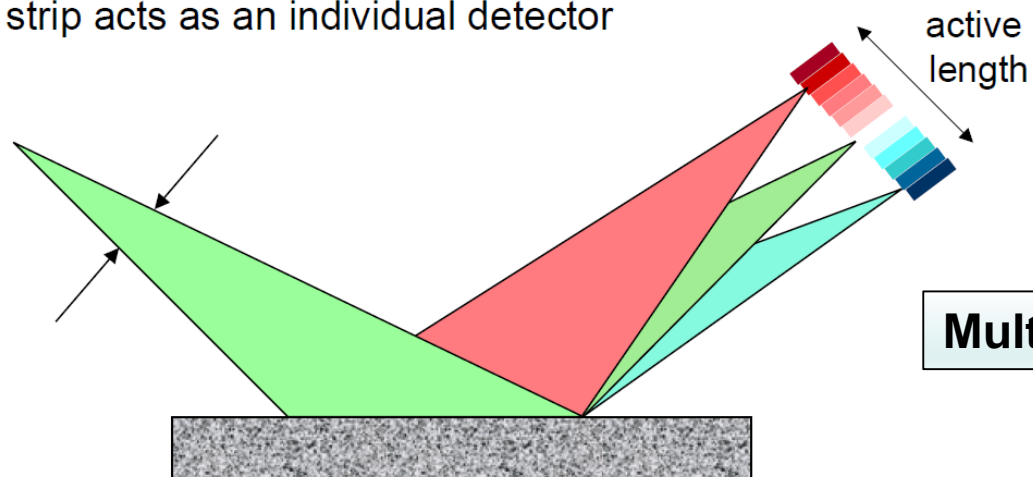


POWDER DIFFRACTION-POINT DETECTOR *versus* MULTI-STRIP DETECTORS

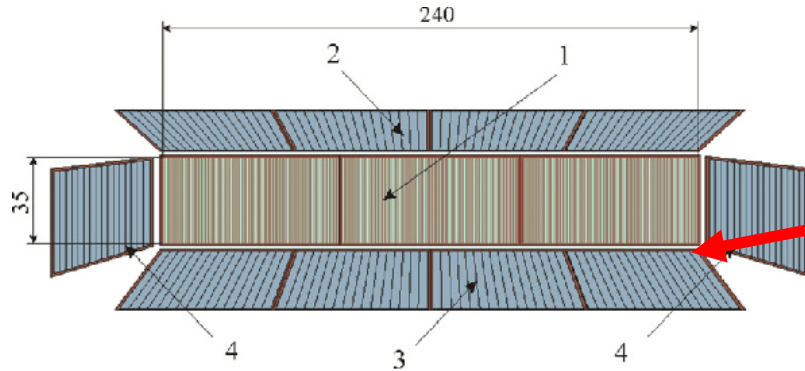
BRAGG-BRENTANO GEOMETRY



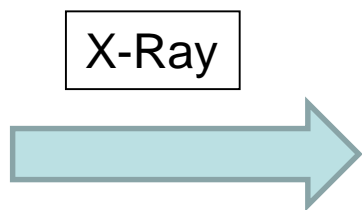
Each strip acts as an individual detector



Multi-strip detector

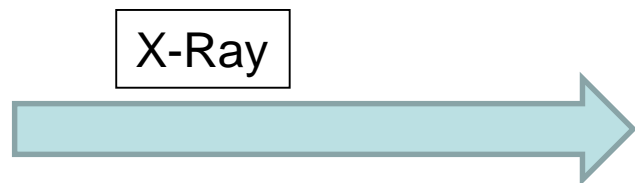


**MULTISTRIP
DETECTOR**



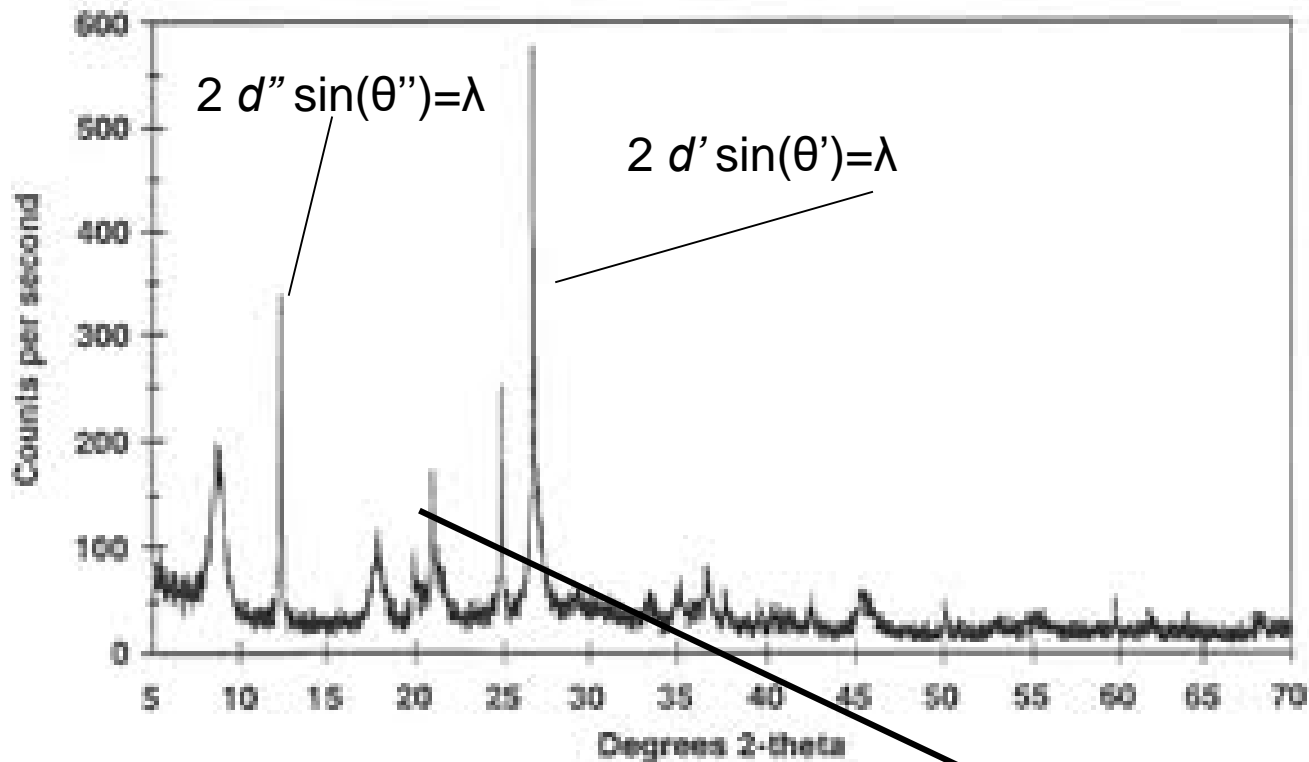
$N.CHANNELS * \Delta = \text{detector-width}$

$\Delta = \text{CHANNEL WIDTH}$



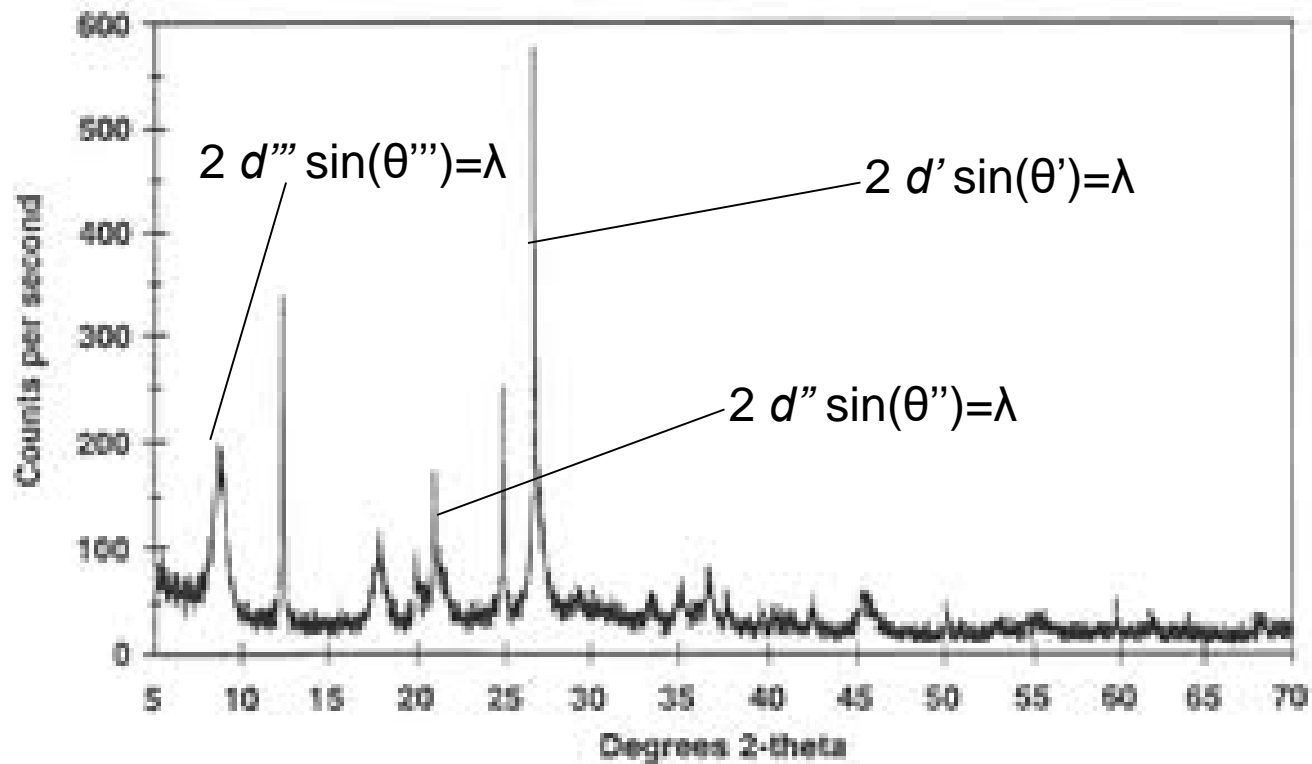
DATA COLLECTION
OVER AN ARC

DIFFRACTION PATTERN COLLECTED BY A
BRAGG-BRENTANO GEOMETRY

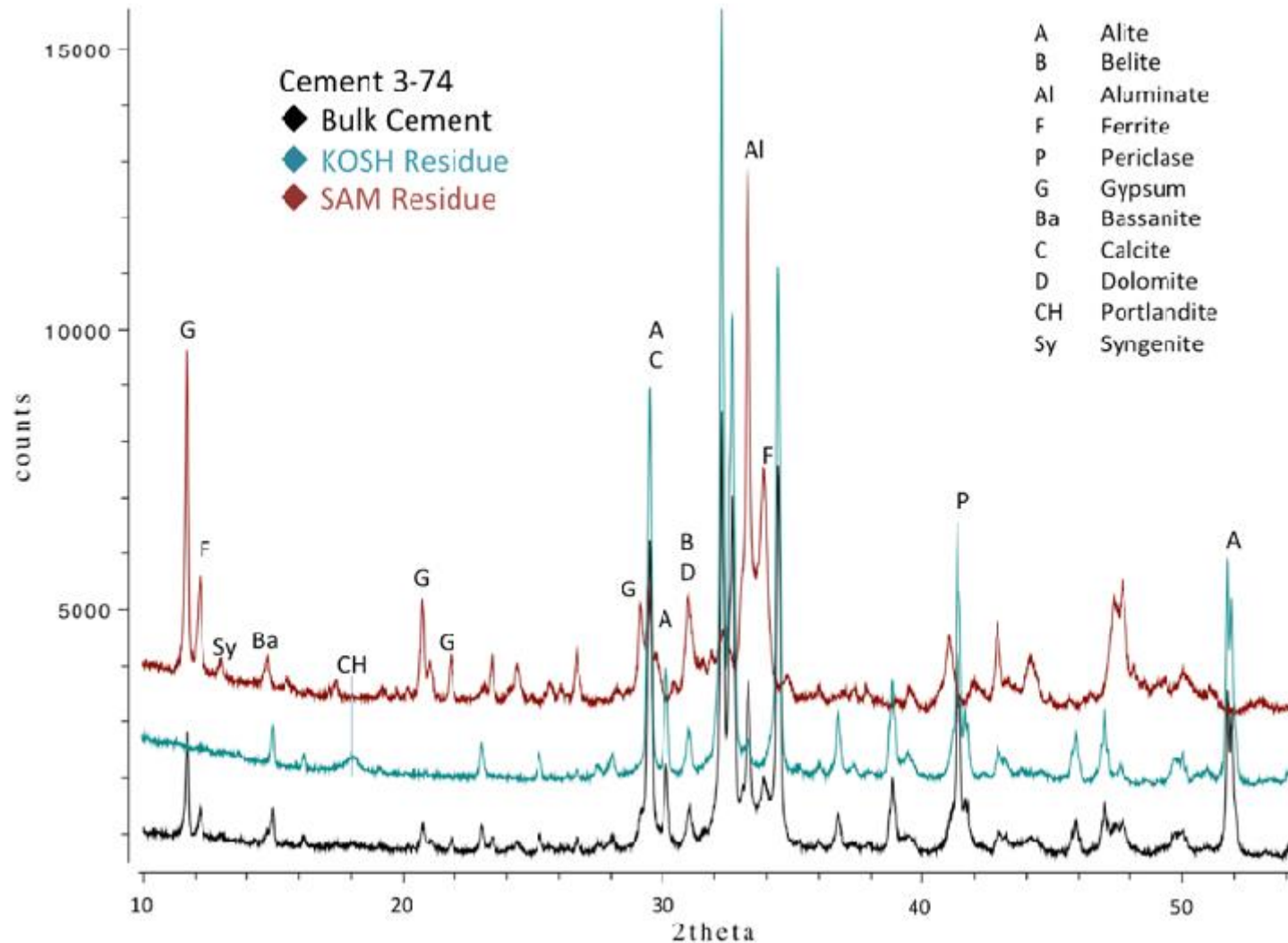


$$2 d_{hkl} \sin(\theta) = \lambda$$

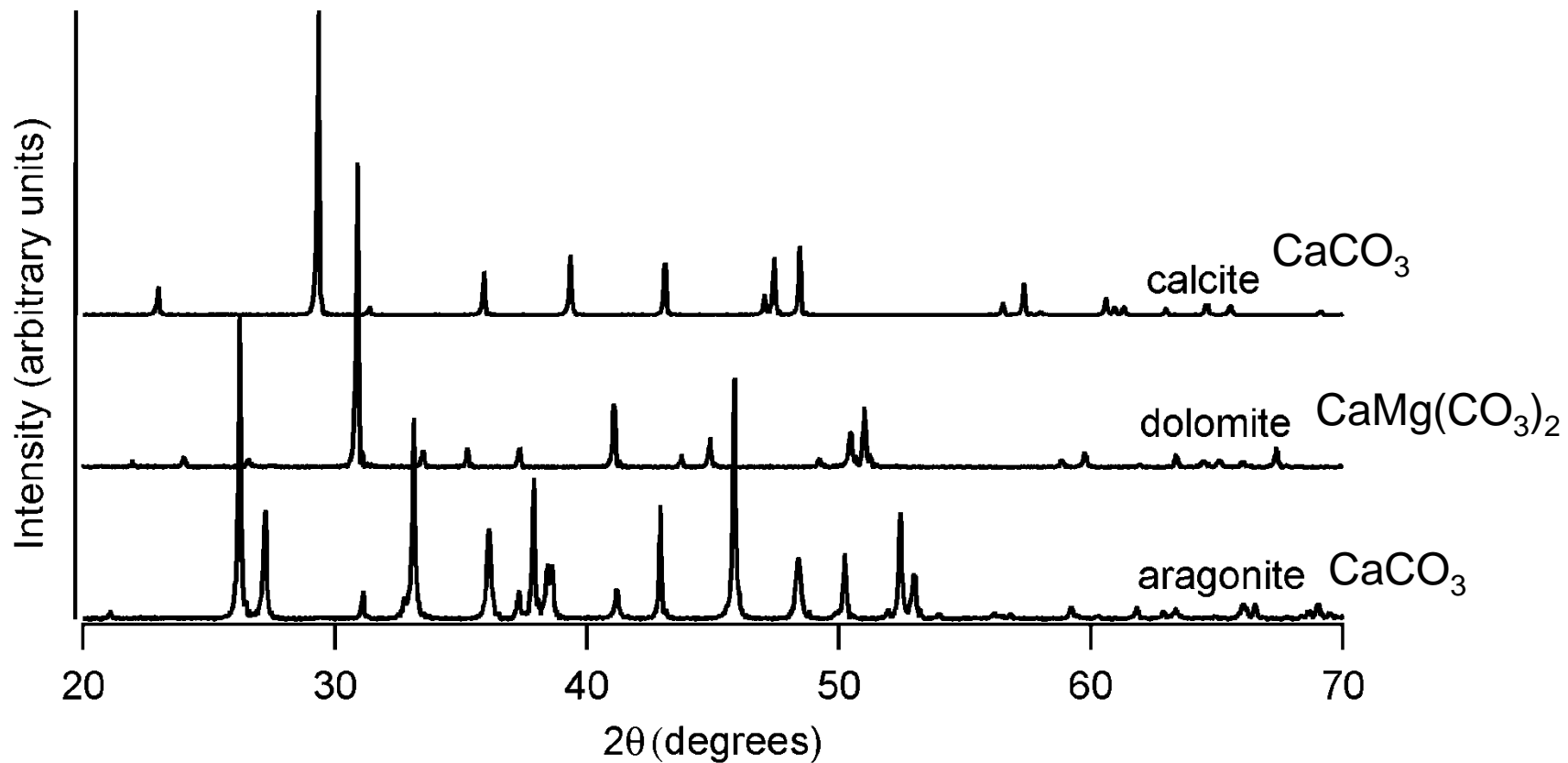
DIFFRACTION RINGS CAN BE TURNED INTO STANDARD BRAGG-BRENTANO PROFILE



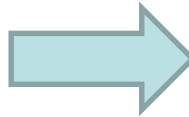
Every phase has its own diffraction pattern. In a mixture, the diffraction patterns of the occurring phases sum up, proportionally to the amount of each phase



DIFFERENCES BETWEEN POWDER DIFFRACTION PATTERNS



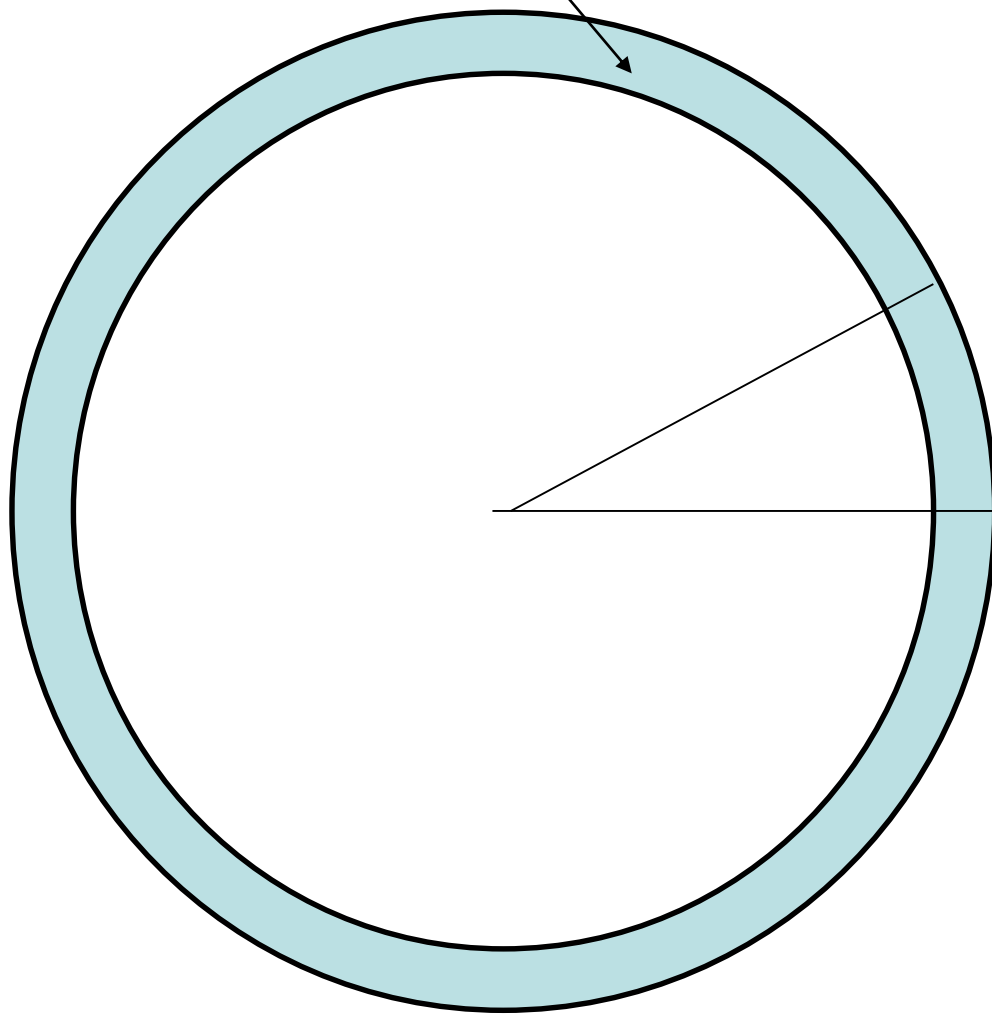
DEBYE-SCHERRER



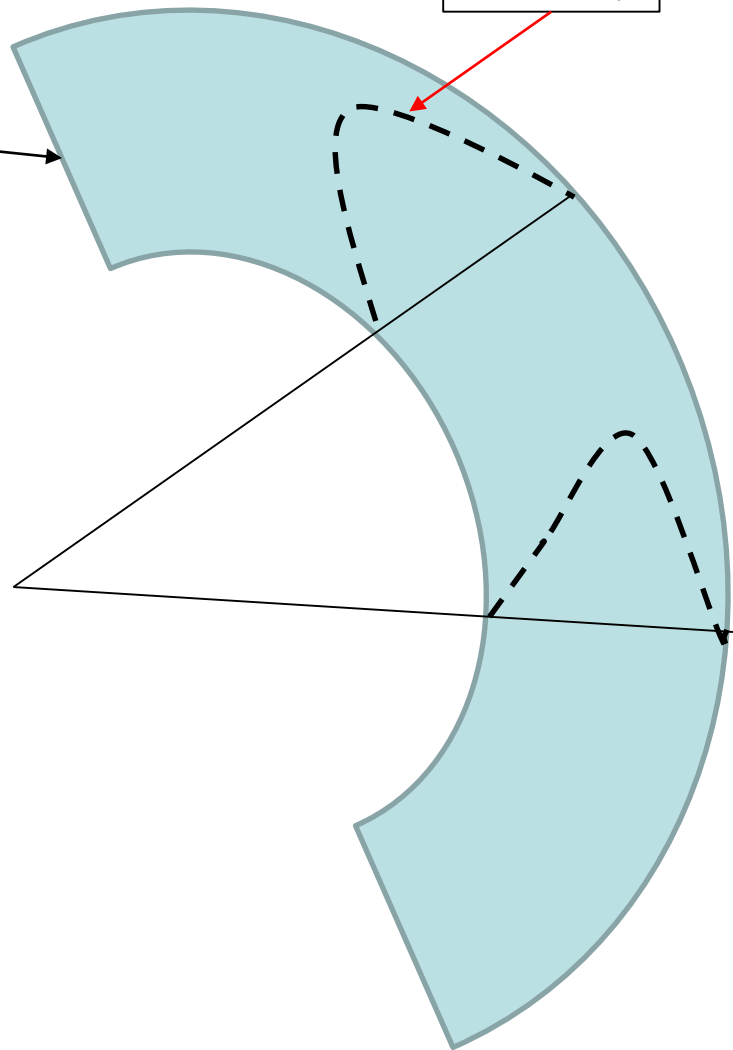
BRAGG-BRENTANO

THE DEBYE-SCHERRER-LIKE OUTPUT (**DIFFRACTION RINGS**) CAN BE
TURNED INTO BRAGG-BRENTANO LIKE OUTPUT (**PROFILE PATTERN**)

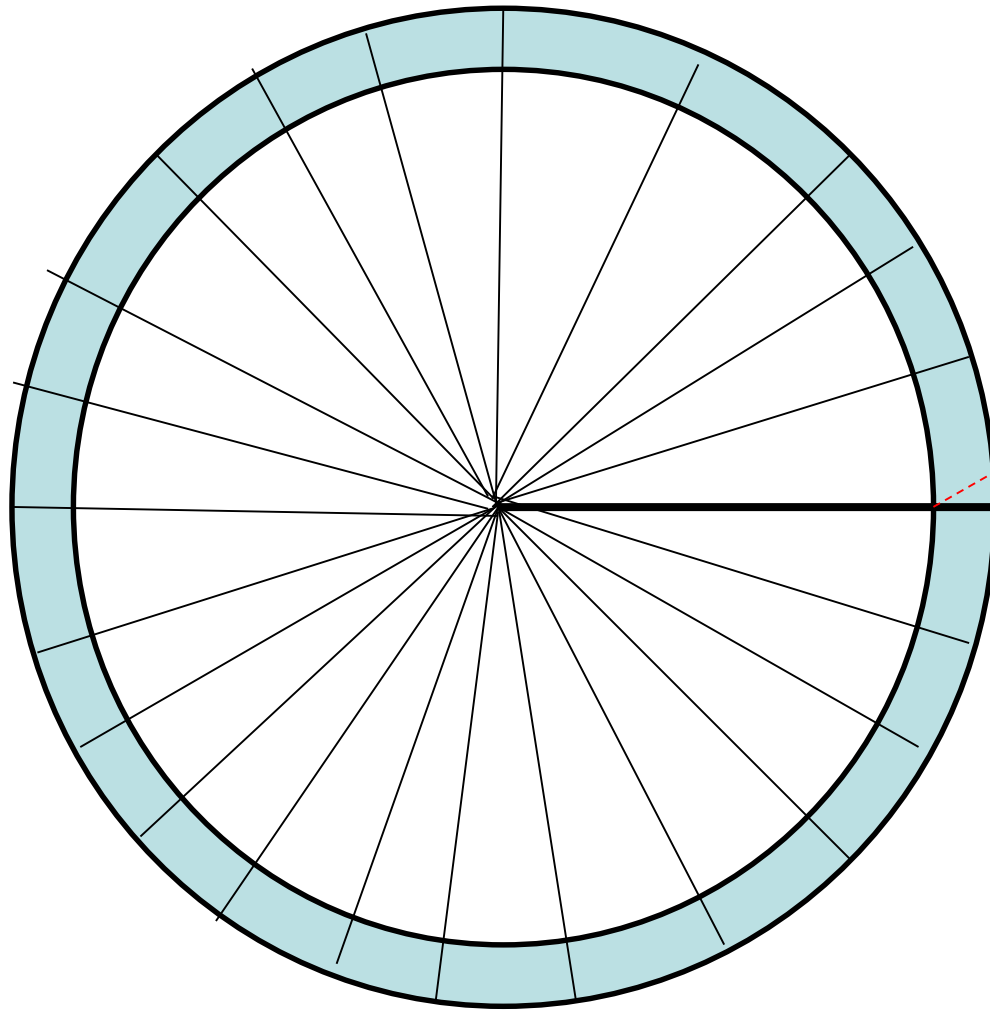
DIFFRACTION RING'S THICKNESS



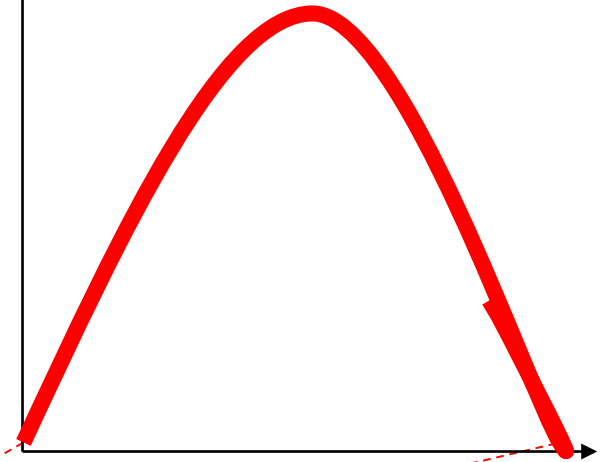
intensity



DIFFRACTION RING'S THICKNESS



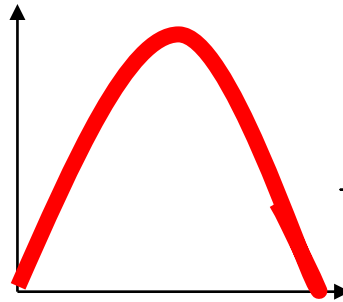
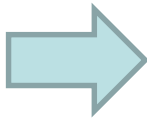
INTENSITY



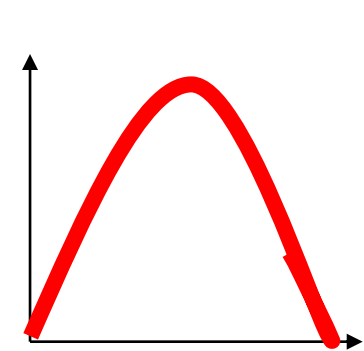
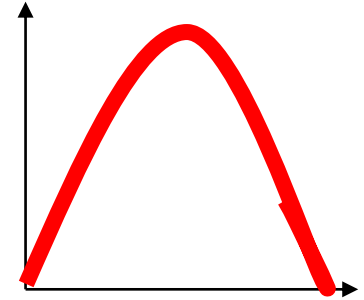
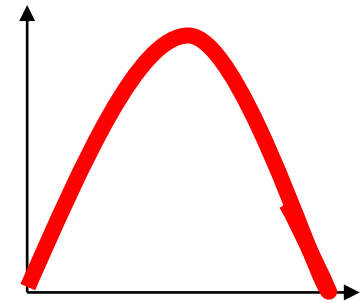
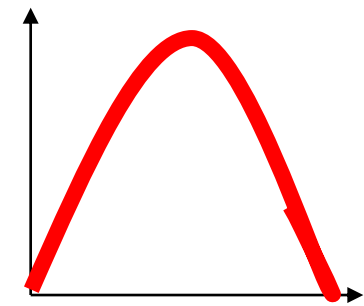
RADIAL POSITION

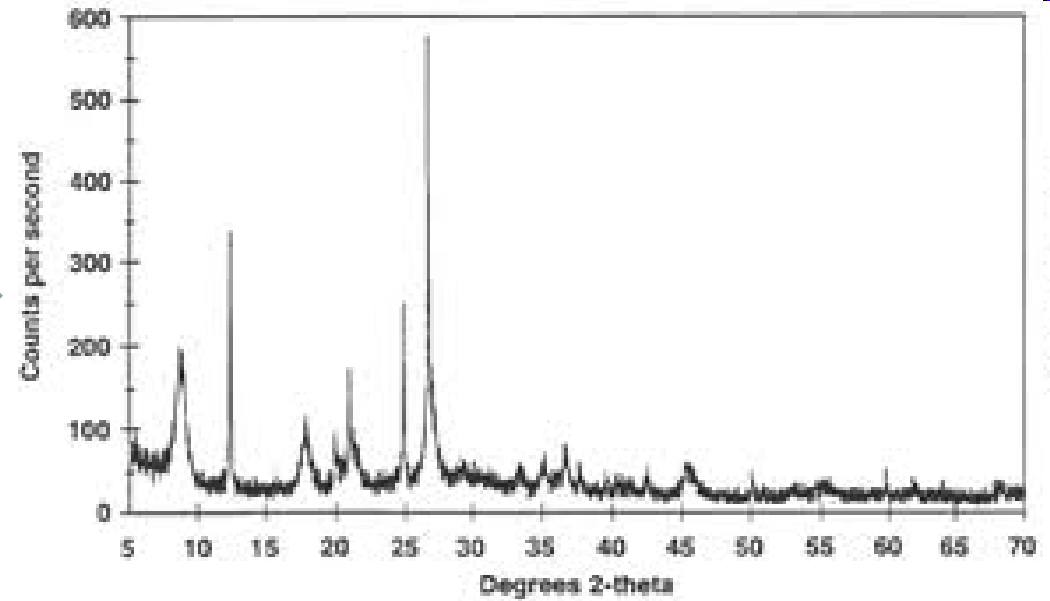
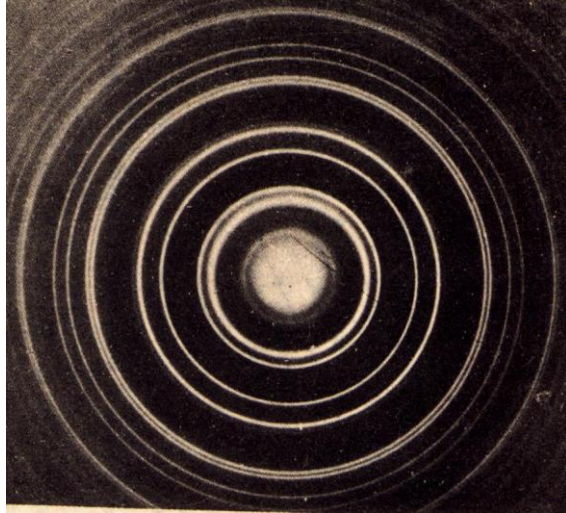
$= 2\theta$

$$Profile(I, 2\theta) = \sum_{j=1, N} RADIAL\ PROFILE_j$$



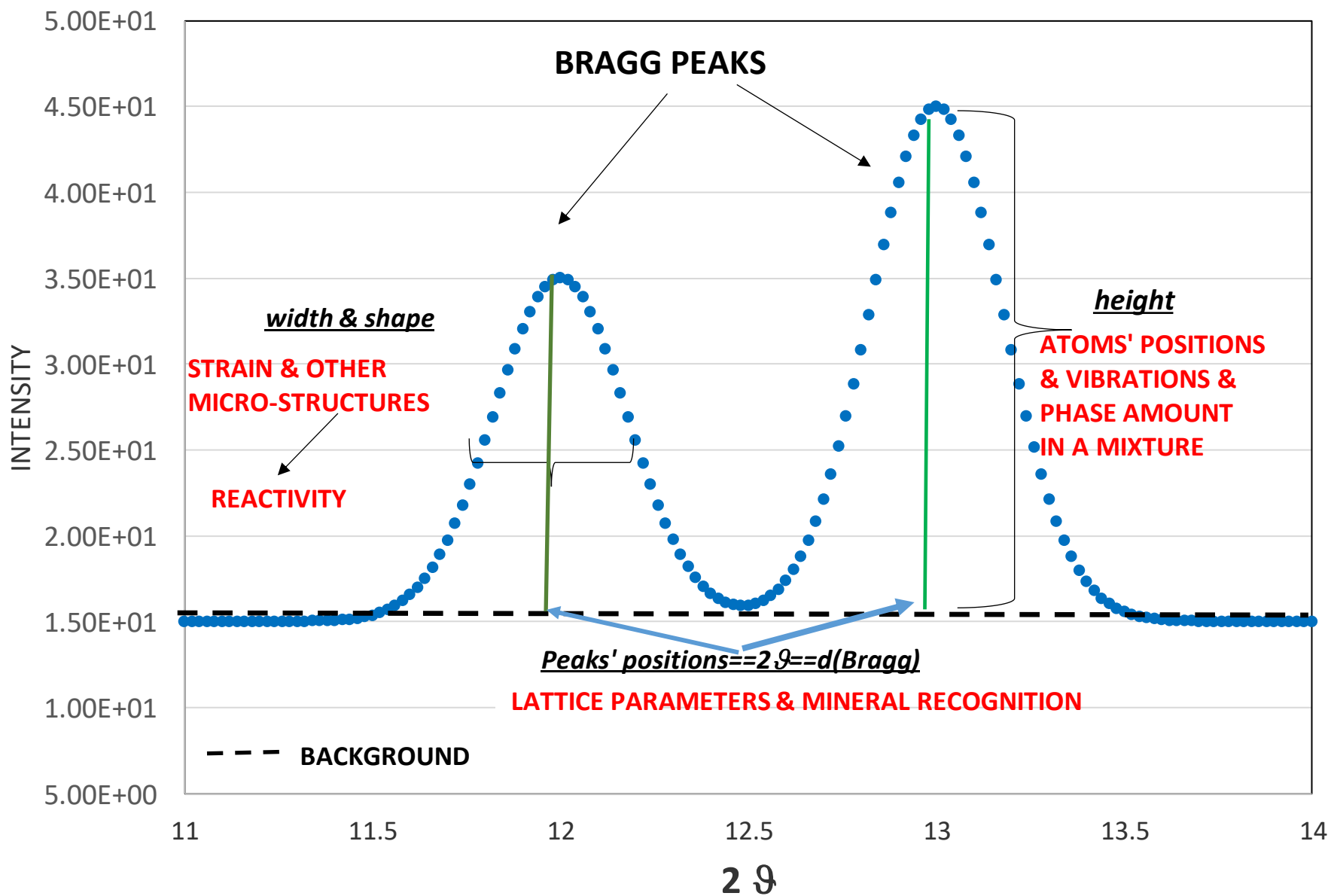
AVERAGE RADIAL PROFILE

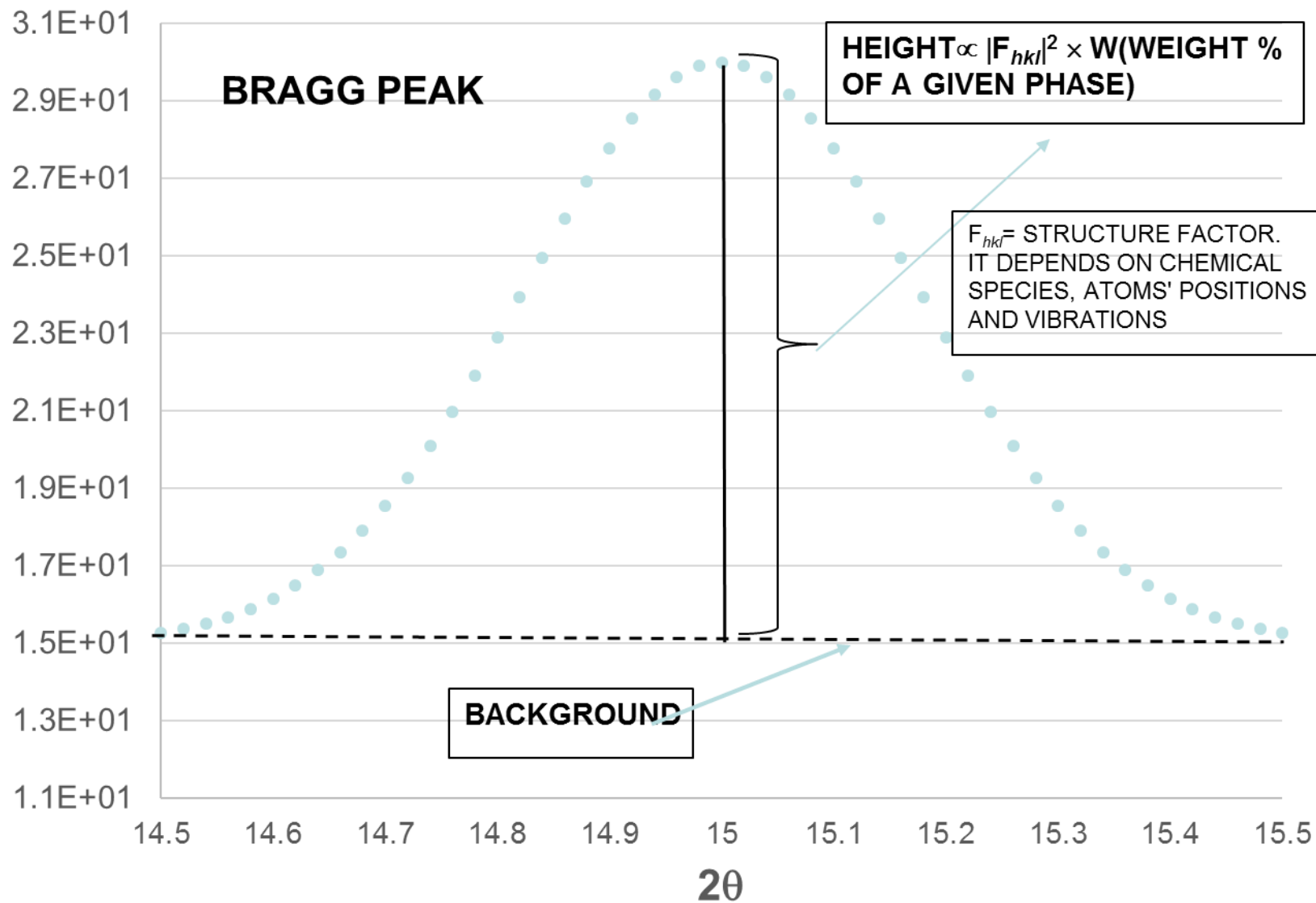




CONVERSION FROM DIFFRACTION RINGS TO 2θ -PATTERN

PHYSICAL MEANING OF BRAGG PEAK IN POWDER DIFFRACTION



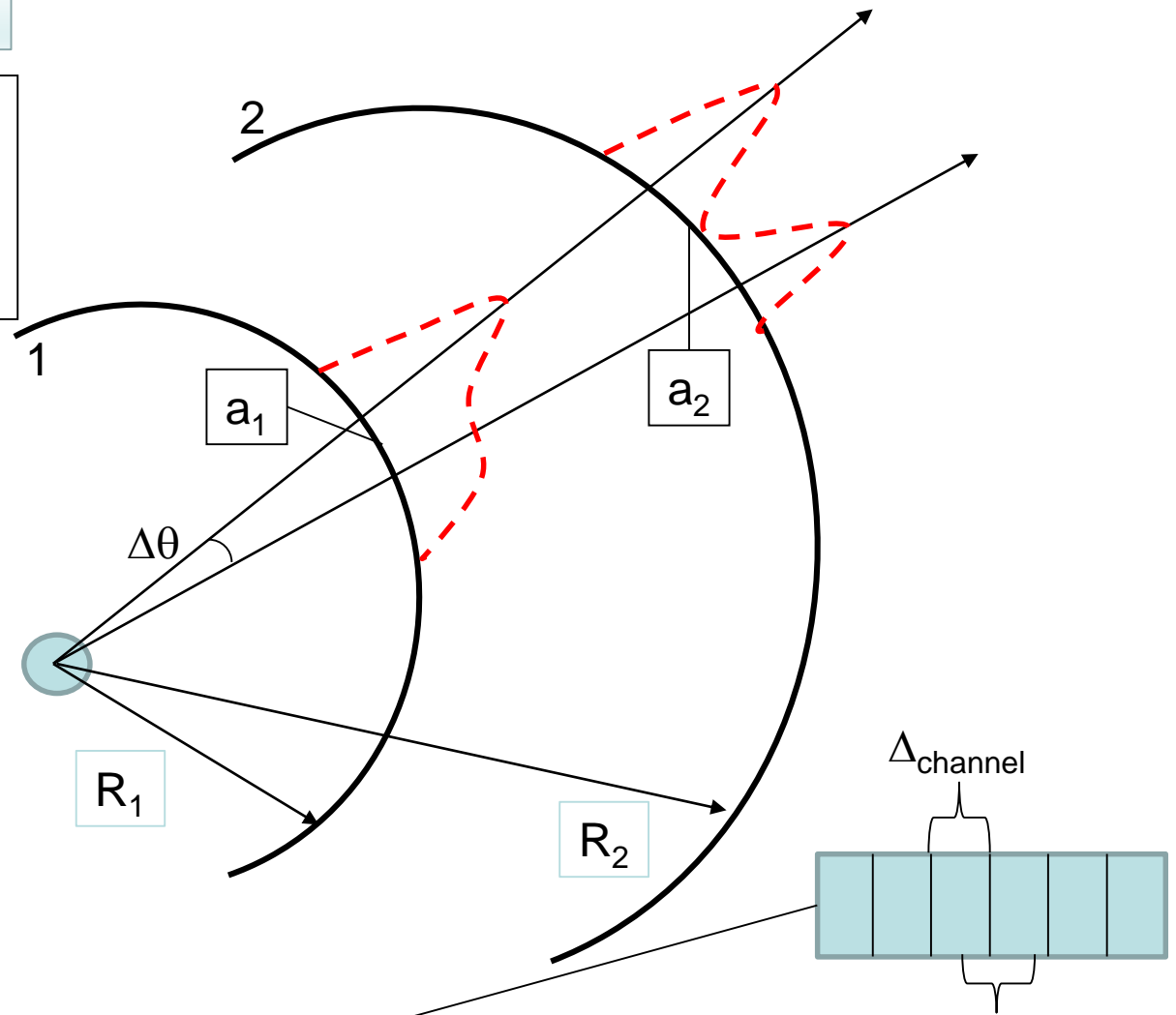


RESOLUTION

ANGULAR RESOLUTION

$a_{1,2}$ = physical distance of observation of the two peaks on detector
 \Rightarrow ANGULAR RESOLUTION

X-Ray



$$a_1 = R_1 \times \Delta\theta$$

$$a_2 = R_2 \times \Delta\theta$$



For multi-strip

$$\Delta\theta_{\min} = \Delta_{\text{channel}} / R$$

$\Delta\theta_{\min}$ = The smallest angular discrimination
 Δ_{channel} = Multi-strip channel's width

Δ_{channel}



MULTI-STRIP DETECTOR

R=detector-sample distance

$$\Delta\theta_{\min} = \Delta_{\text{channel}} / R$$

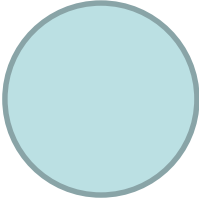
Angular resolution = $\Delta\theta_{\min}$

SAMPLE

YOU NEED A COMPROMISE!



THE LARGER THE SAMPLE-DETECTOR DISTANCE, THE BETTER THE ANGULAR RESOLUTION



THE LARGER THE SAMPLE-DETECTOR DISTANCE, THE WORSE THE TOTAL EFFICIENCY BECAUSE OF A REDUCTION OF PHOTON IRRADIANCE



TRY TO COMPENSATE THROUGH AN ENHANCEMENT OF INTRINSIC EFFICIENCY

COUNTING UNCERTAINTY

$$\sigma(N) \sim \sqrt{N}$$



$$\frac{\sigma}{N} \sim \frac{1}{\sqrt{N}}$$

END OF THE GENERAL PART

NEUTRON RADIATION

NEUTRONS

Mass = $1.67492729(28) \times 10^{-27}$ kg

De Broglie relationship

$$h = p \times \lambda$$

h = Planck constant = $6.62606896(33) \times 10^{-34}$ J.s

p

Particle-like

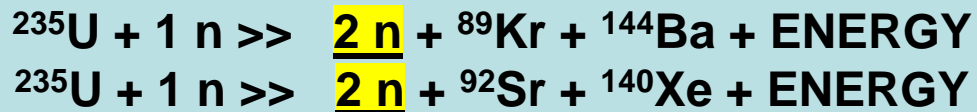
λ

Wave-like

NEUTRON PRODUCTION

FISSION

^{235}U
 ^{239}Pu



$n(\text{energy}) \sim 0.025\text{ eV}$
(*thermal* neutrons =
slow neutrons)

SPALLATION

COMPLEX NUCLEAR
REACTION PROCESS

EMBEDDING of
FAST NEUTRONS

EVAPORATION

Fast neutrons: energy greater than 1 eV, up to 0.1 MeV or approximately 1 MeV, depending on the definition.

Slow neutrons: energy less than or equal to 0.4 eV.

Epithermal neutrons: energy from 1 eV to 10 keV.

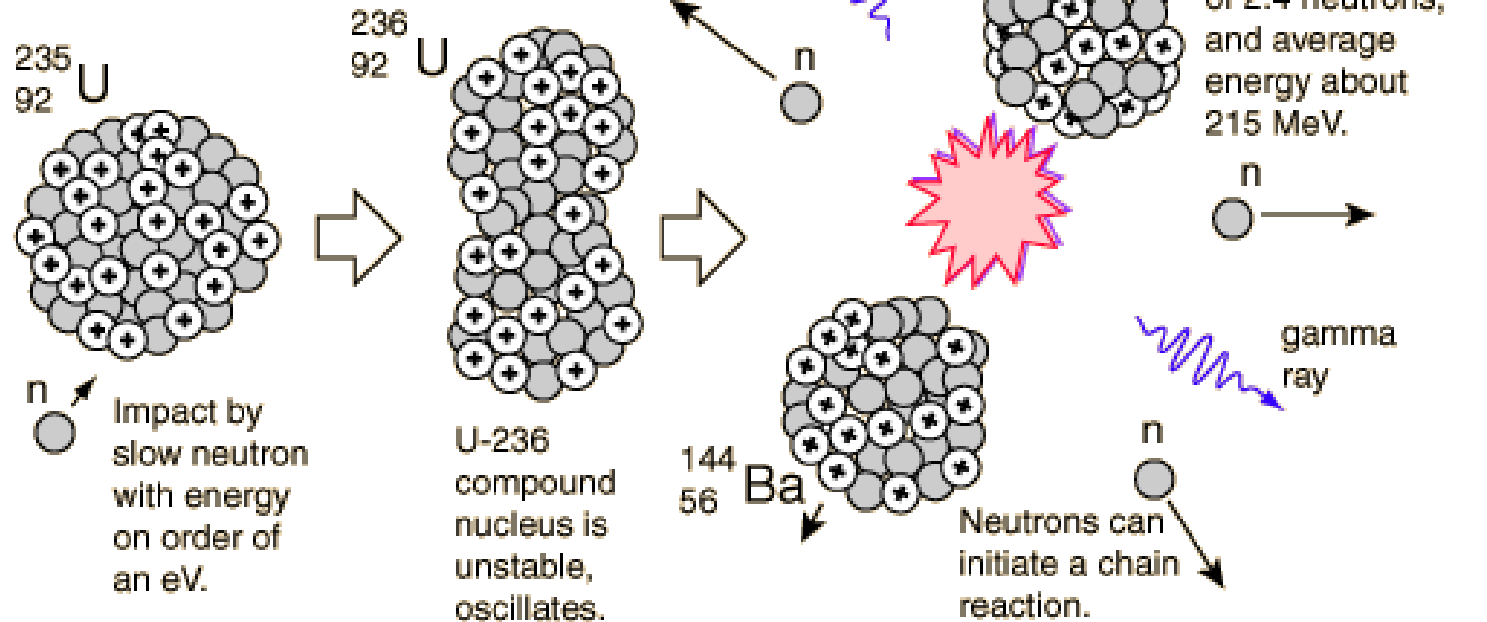
Hot neutrons: energy of about 0.2 eV.

Thermal neutrons: energy of about 0.025 eV

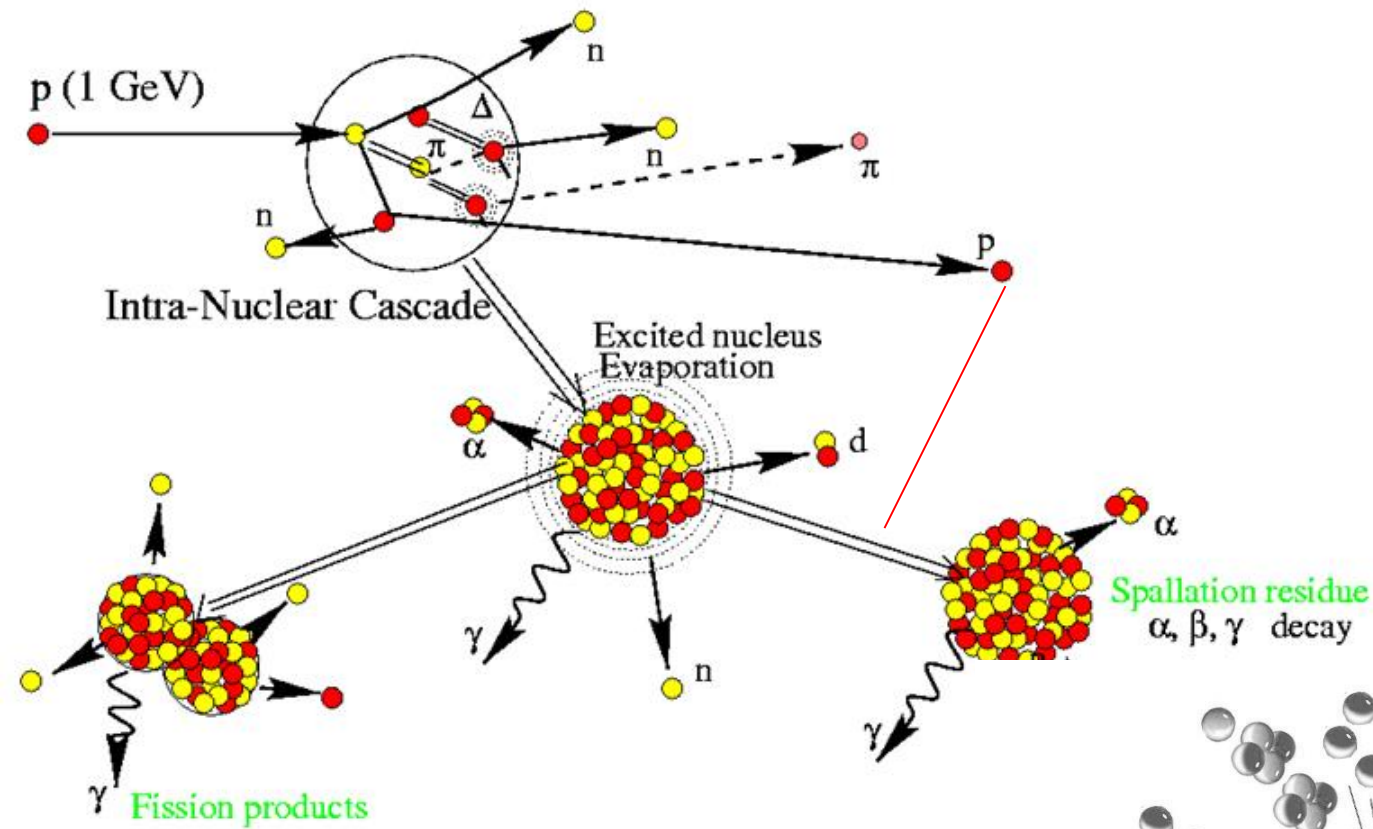
Cold neutrons: energy from 5×10^{-5} eV to 0.025 eV.

Very cold neutrons: energy from 3×10^{-7} eV to 5×10^{-5} eV.

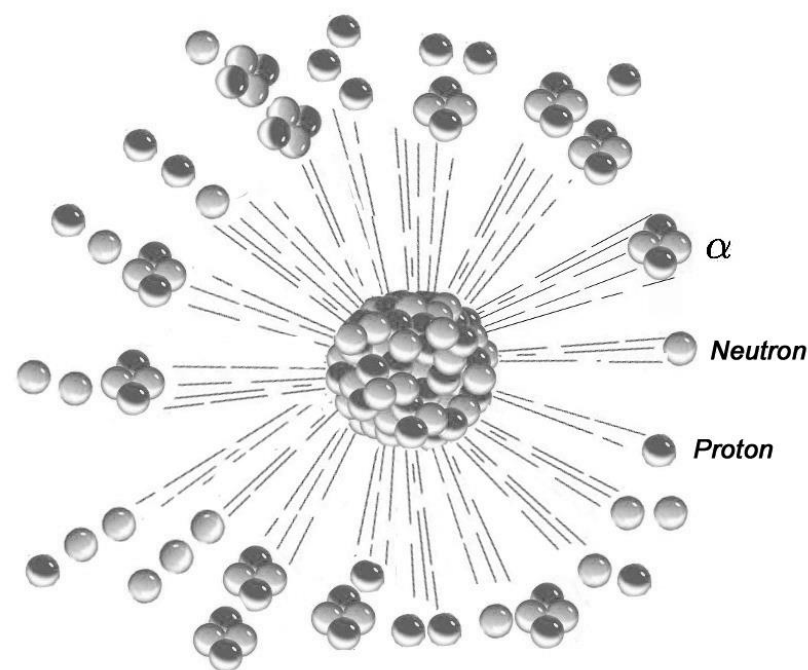
An example of one of the many reactions in the uranium-235 fission process.



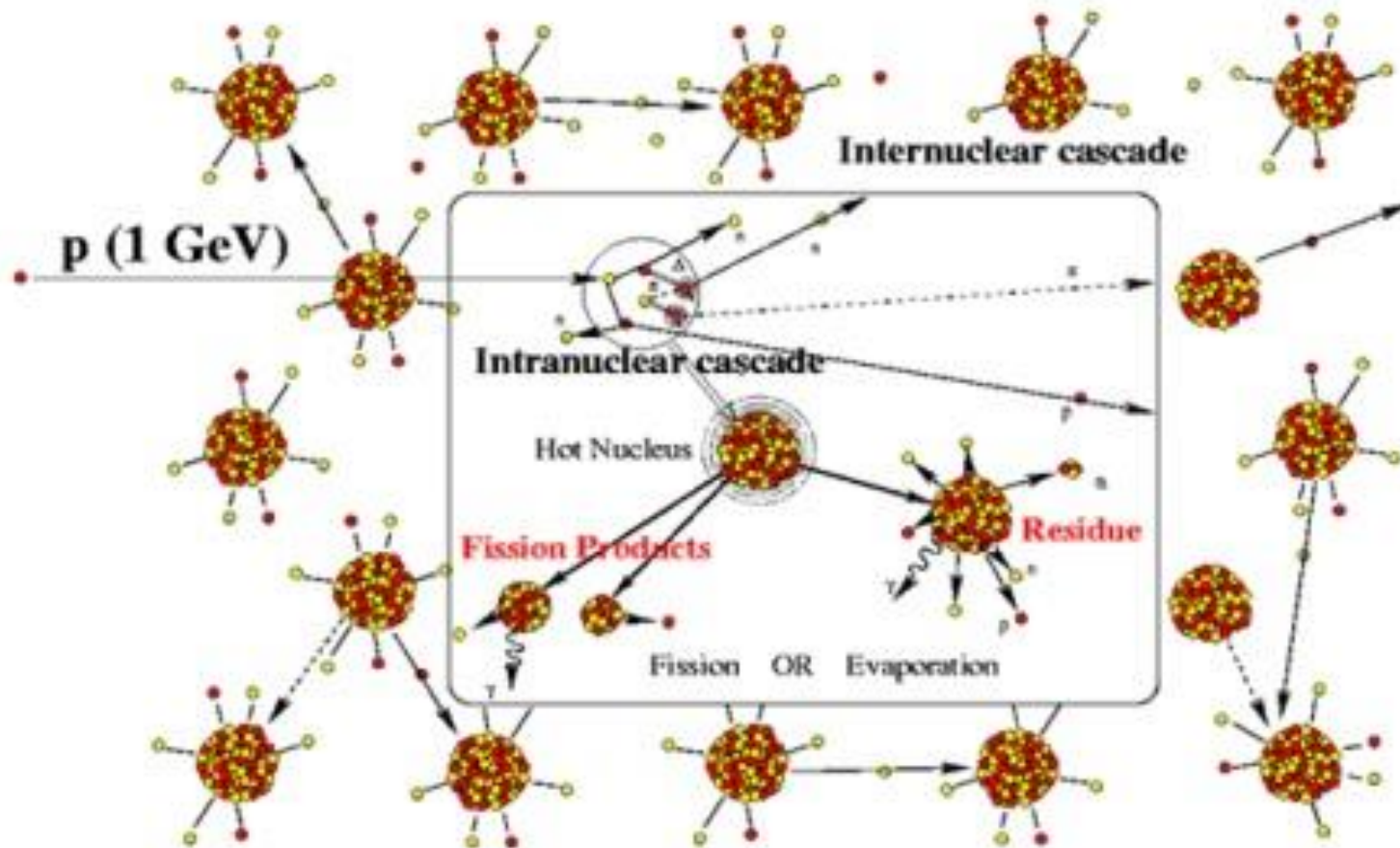
NUCLEAR FISSION



SPALLATION

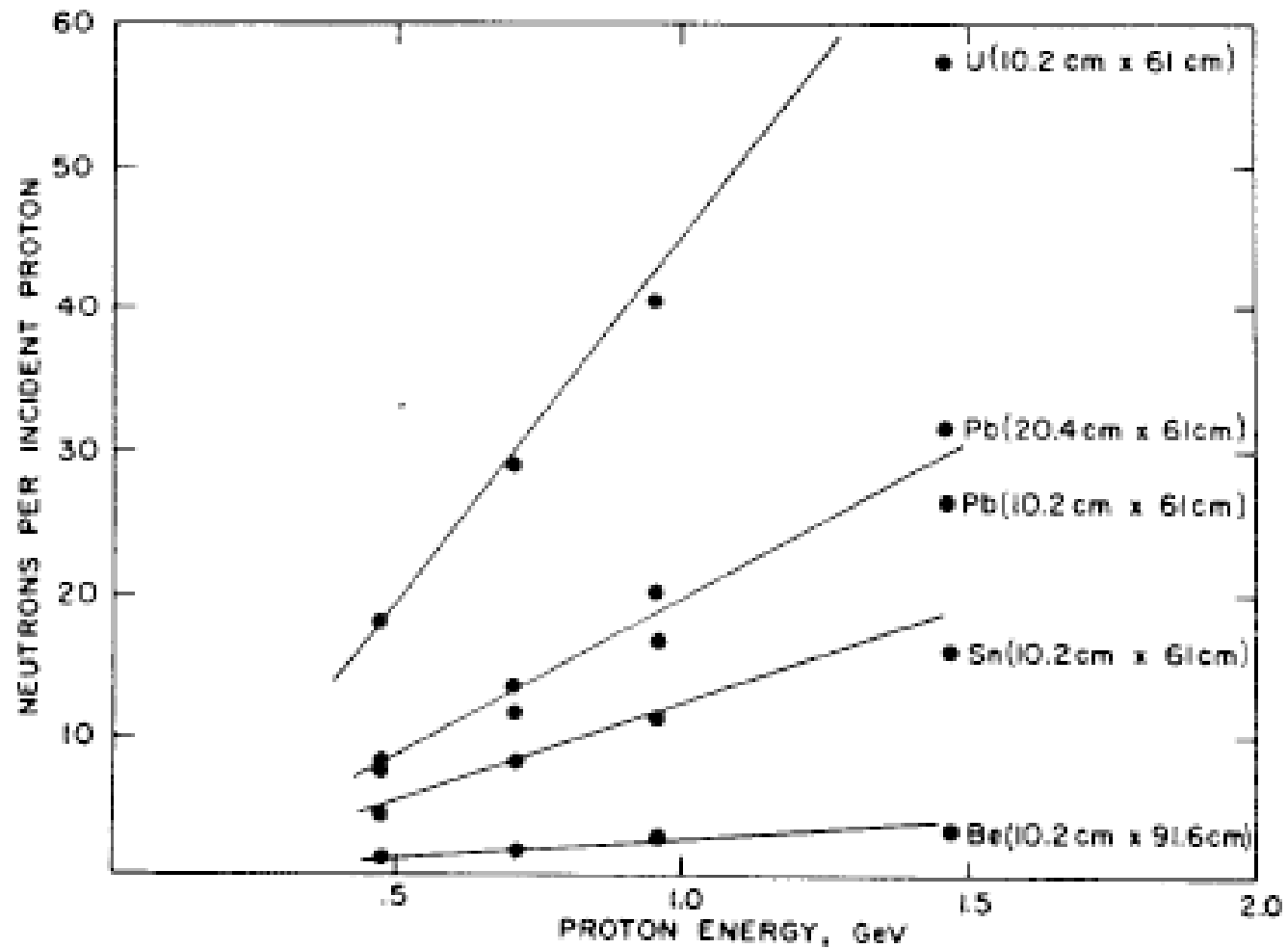


SPALLATION



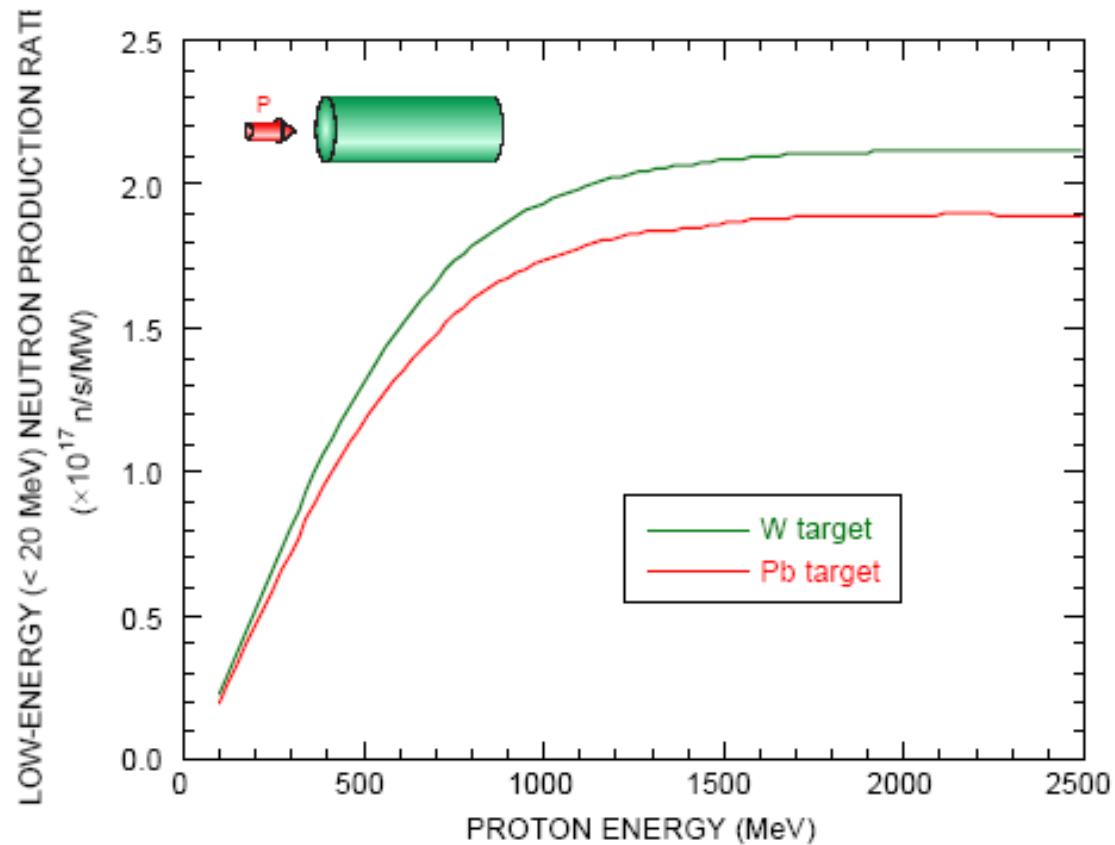
A spallation reaction consists of sending a high energy particle, often a proton, into a nucleus which then ejects different sorts of particles. Among these are many neutrons. These are then fired at the nuclei which we wish to transform and transmute. During transmutation, the excited nucleus effectively captures neutrons and then either it fissions or is evaporated by losing the most energetic particles.

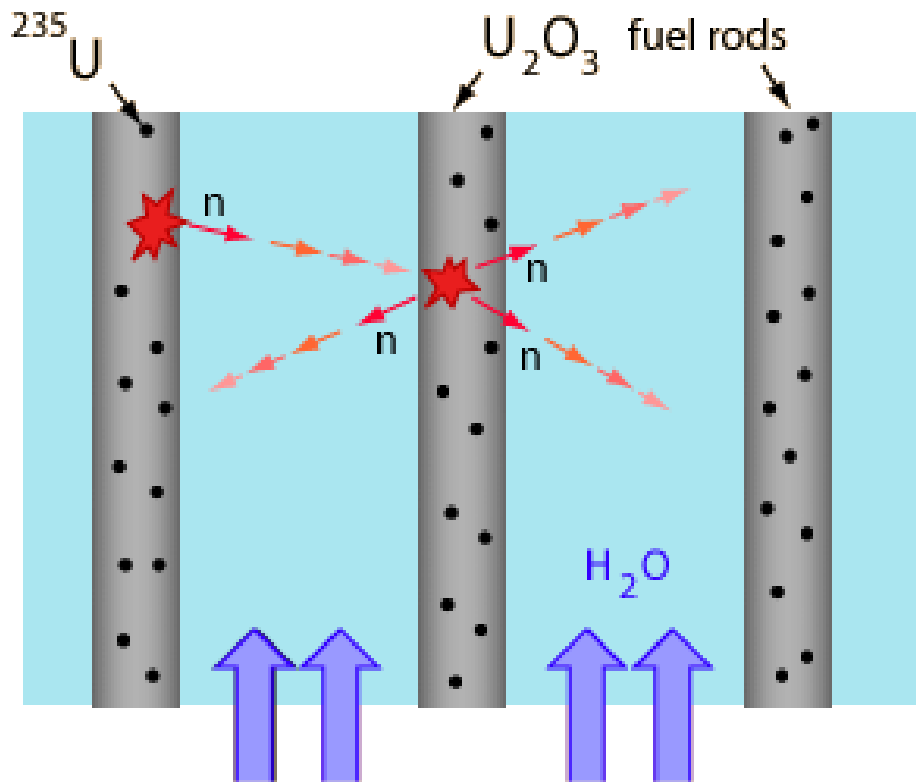
SPALLATION YIELD versus TARGET



PROTON ENERGY AND NEUTRON PRODUCTION BY SPALLATION: SATURATION

(50-cm-diam × 200-cm-long targets bombarded on axis by ~1-GeV protons)





Water as coolant and moderator flows between fuel rods.

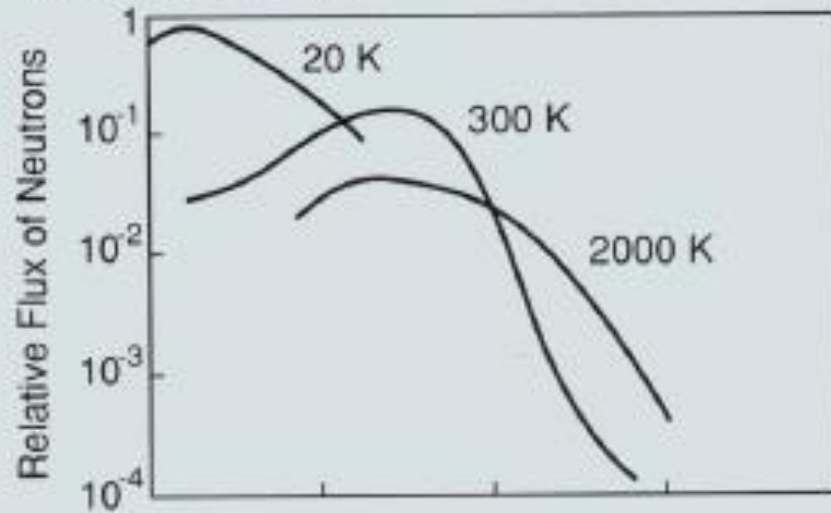
NEUTRONS MUST BE SLOWED DOWN BY MEANS OF A

MODERATOR

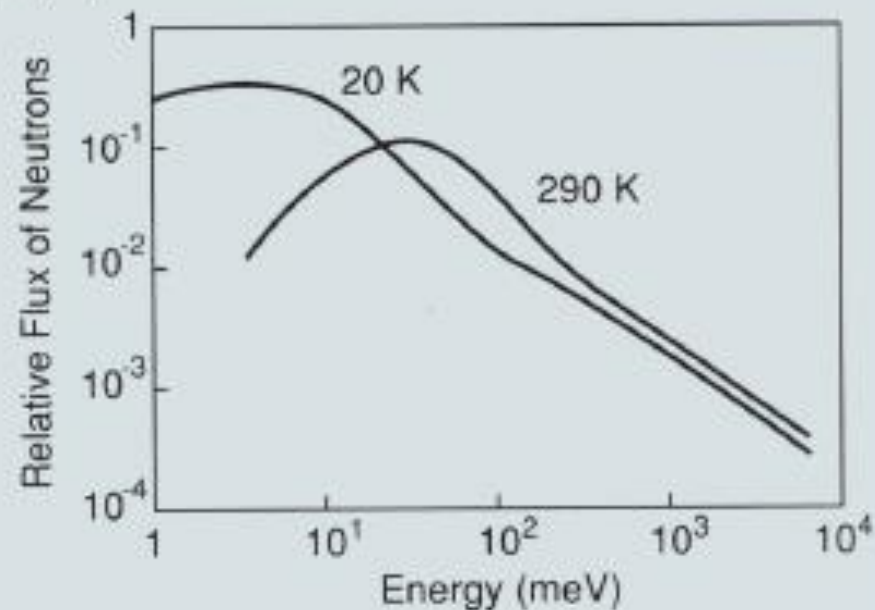
TO FEED FISSION

TO HAVE LOW ENERGY NEUTRONS

(a) Reactor Neutrons

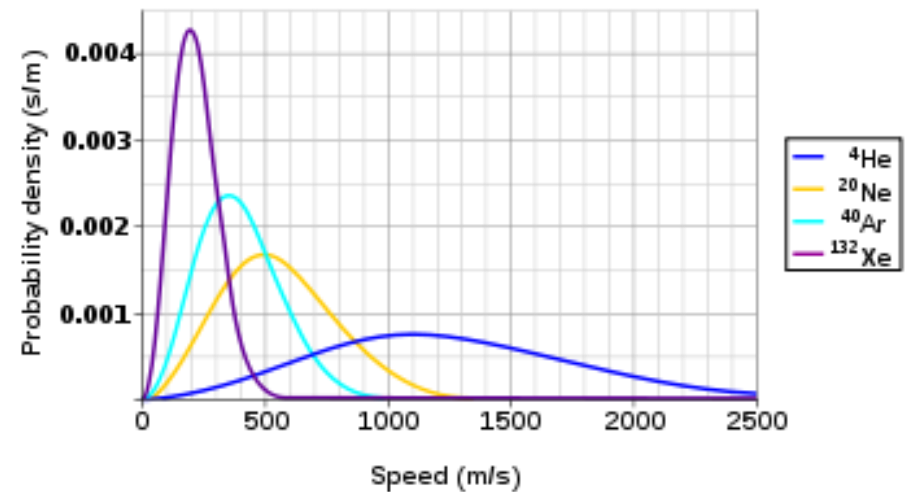


(b) Spallation Neutrons



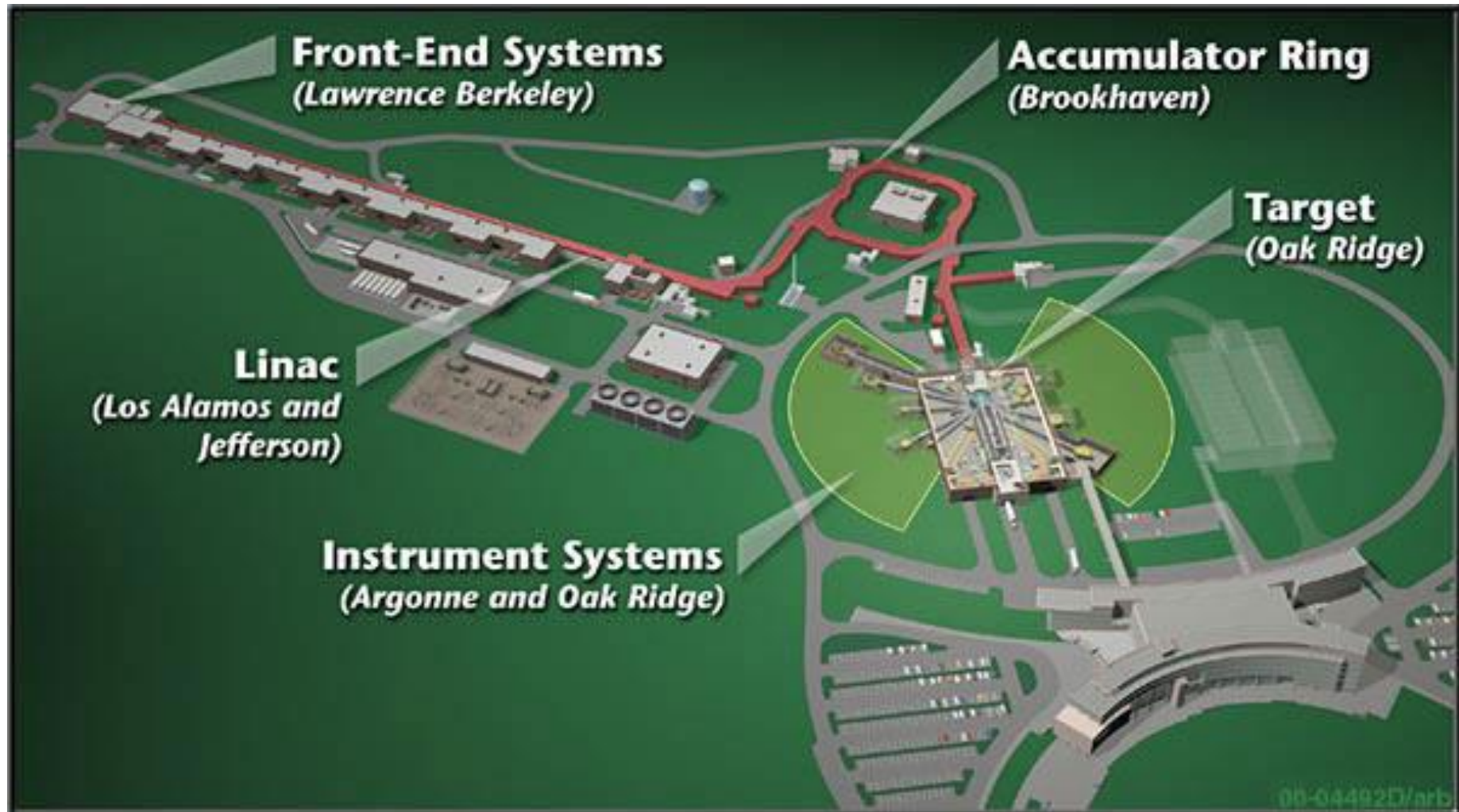
FLUX AS A FUNCTION
OF
MODERATOR

Maxwell-Boltzmann Molecular Speed Distribution for Noble Gases

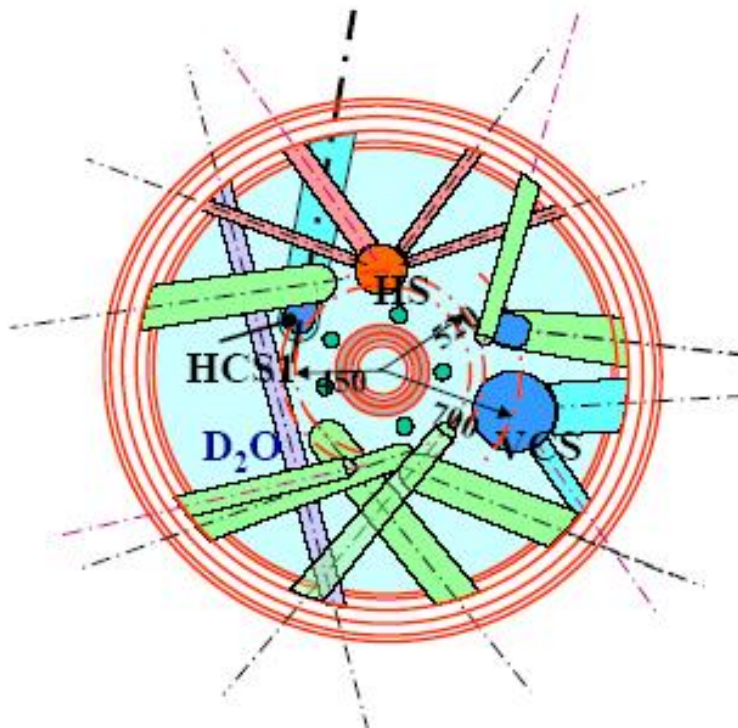


MAXWELL VELOCITY
DISTRIBUTION

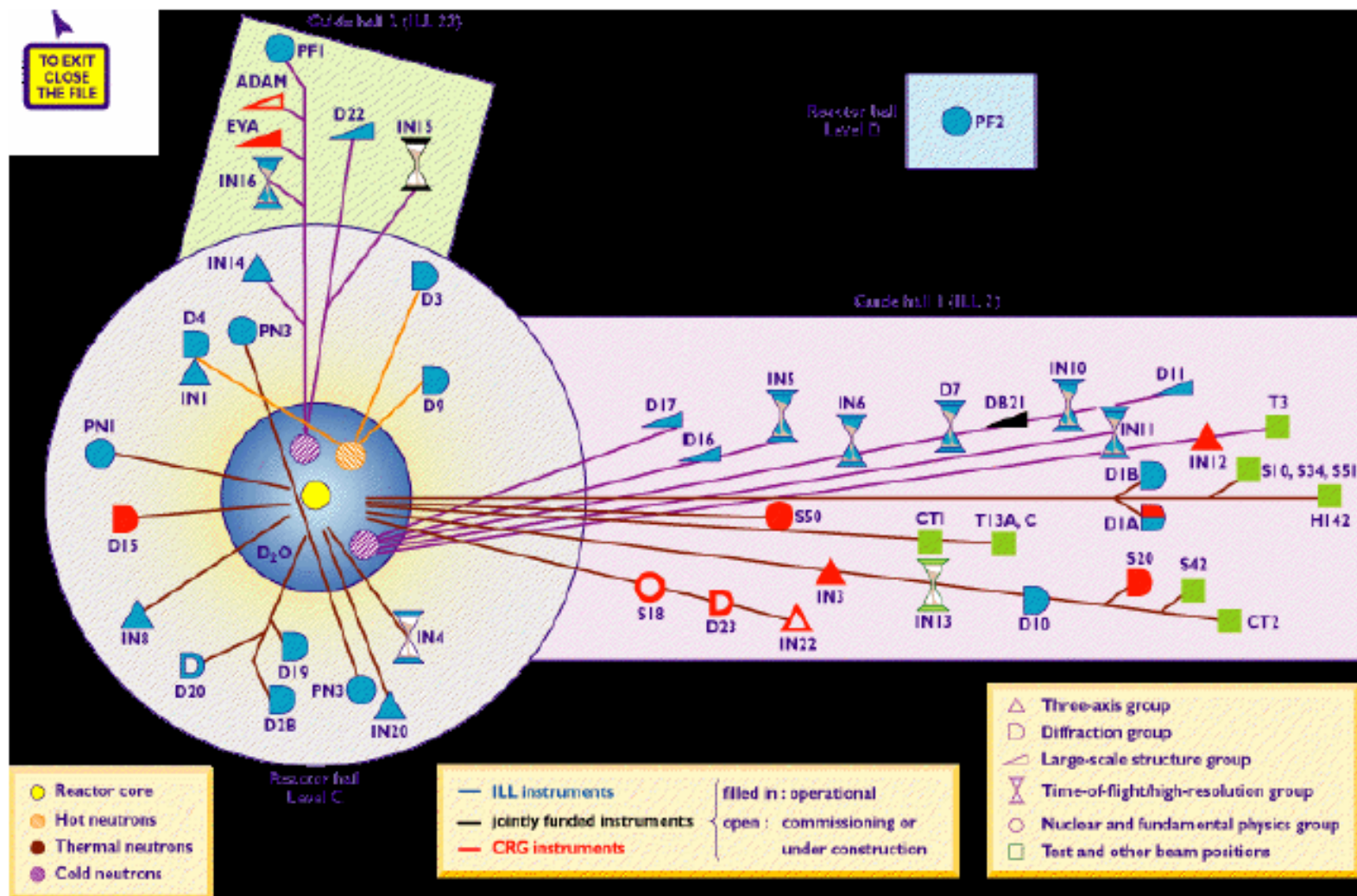
LAYOUT OF A SPALLATION SOURCE



REACTOR CORE OF SPALLATION



LAYOUT OF ILL: **STEADY SOURCE**



NEUTRON DETECTION

```
graph TD; A[NEUTRON DETECTION] --> B[RECOIL MECHANISM]; A --> C[NUCLEAR REACTIONS];
```

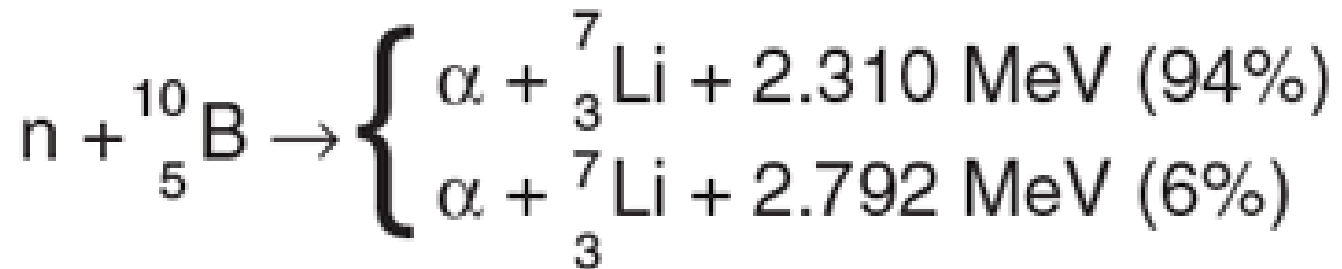
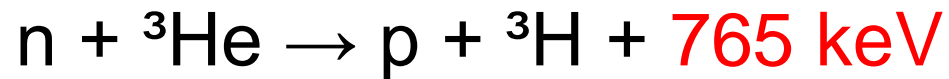
RECOIL MECHANISM

- IONIZATION BY COLLISION

NUCLEAR REACTIONS

- CAUSING NUCLEAR REACTIOS
WHICH PRODUCE DETECTABLE
ENERGY

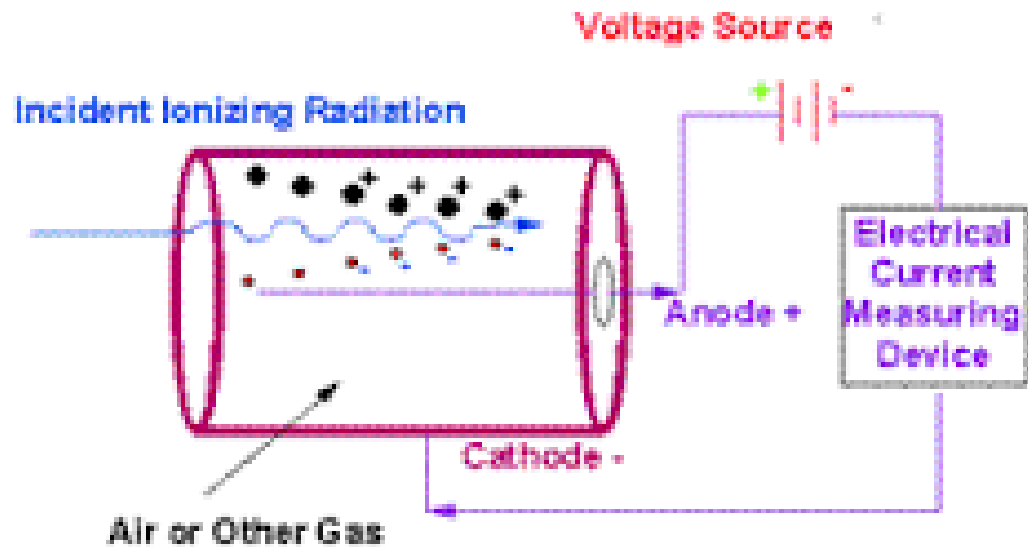
THE COMMONEST **NUCLEAR REACTIONS** FOR NEUTRON
DETECTION



DETECTORS

- **GAS FILLED (GAS)**
- **SCINTILLATORS (SOLID STATE)**
- **SEMI-CONDUCTORS (SOLID STATE)**

GAS-FILLED DETECTORS



GAS-FILLED DETECTORS LAYOUT

$^3\text{He} - \text{BF}_3$ – NEUTRON REACTIONS (THERMAL NEUTRONS)

$^4\text{He} - \text{CH}_4$ – RECOIL MECHANISM (FAST NEUTRONS)

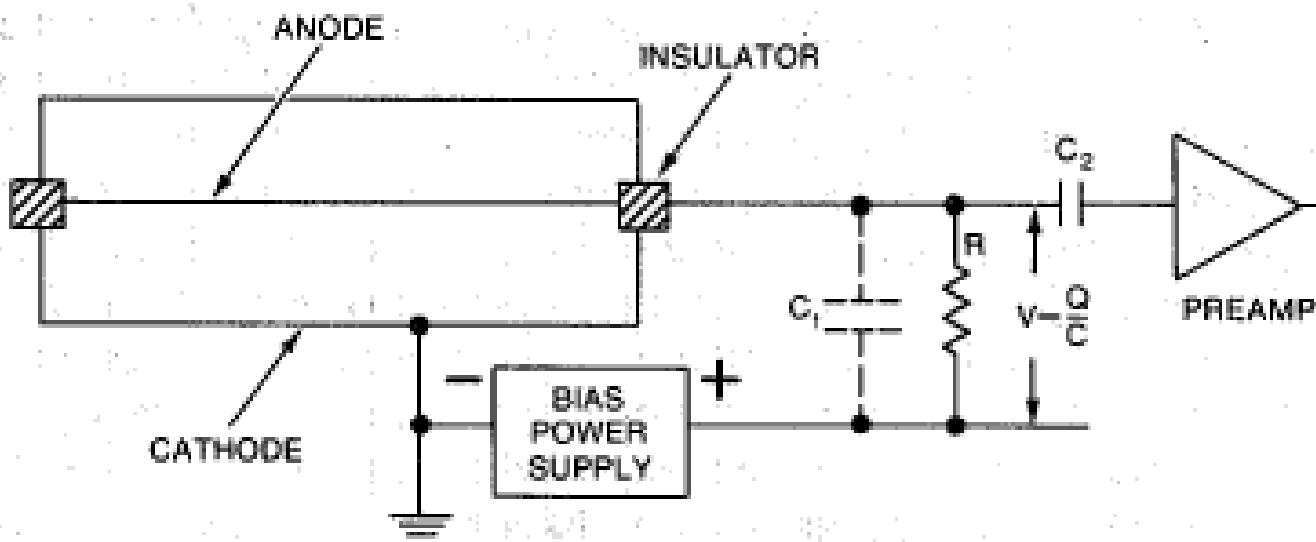
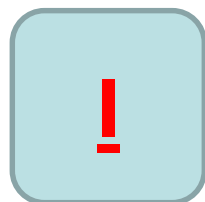


Fig. 13.1 Typical setup for gas-filled neutron detectors.

CROSS-SECTIONS OF SOME ELEMENTS AS A FUNCTION OF NEUTRON ENERGY

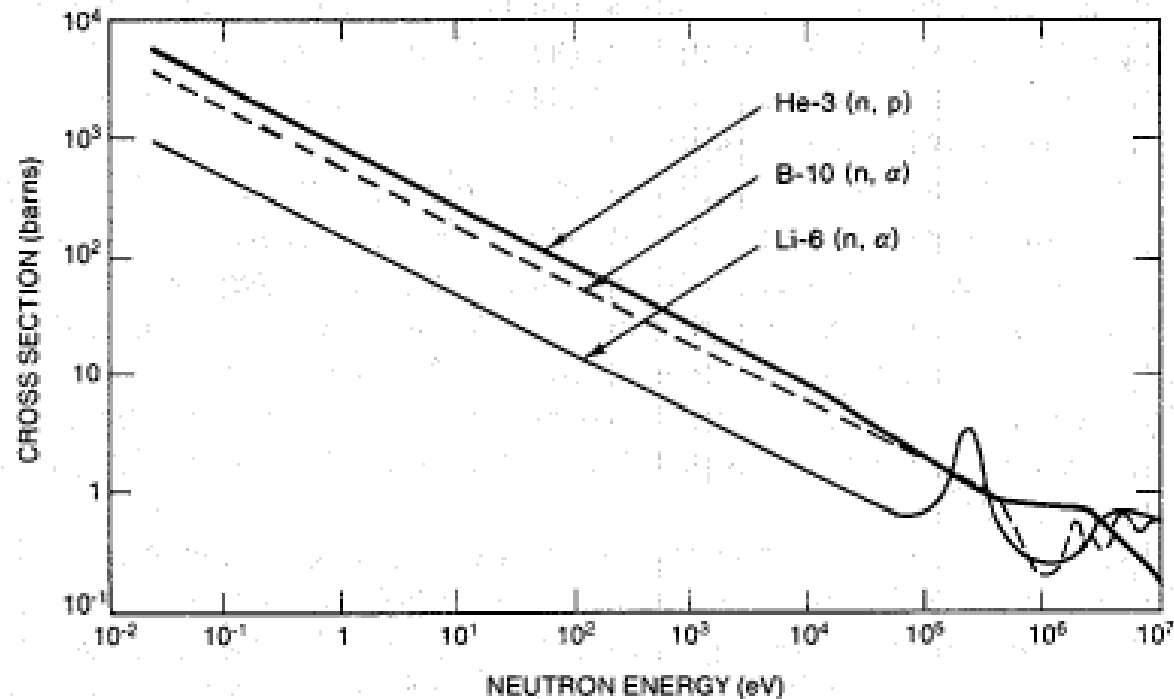
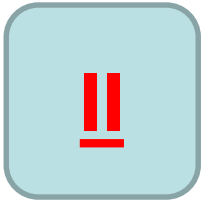
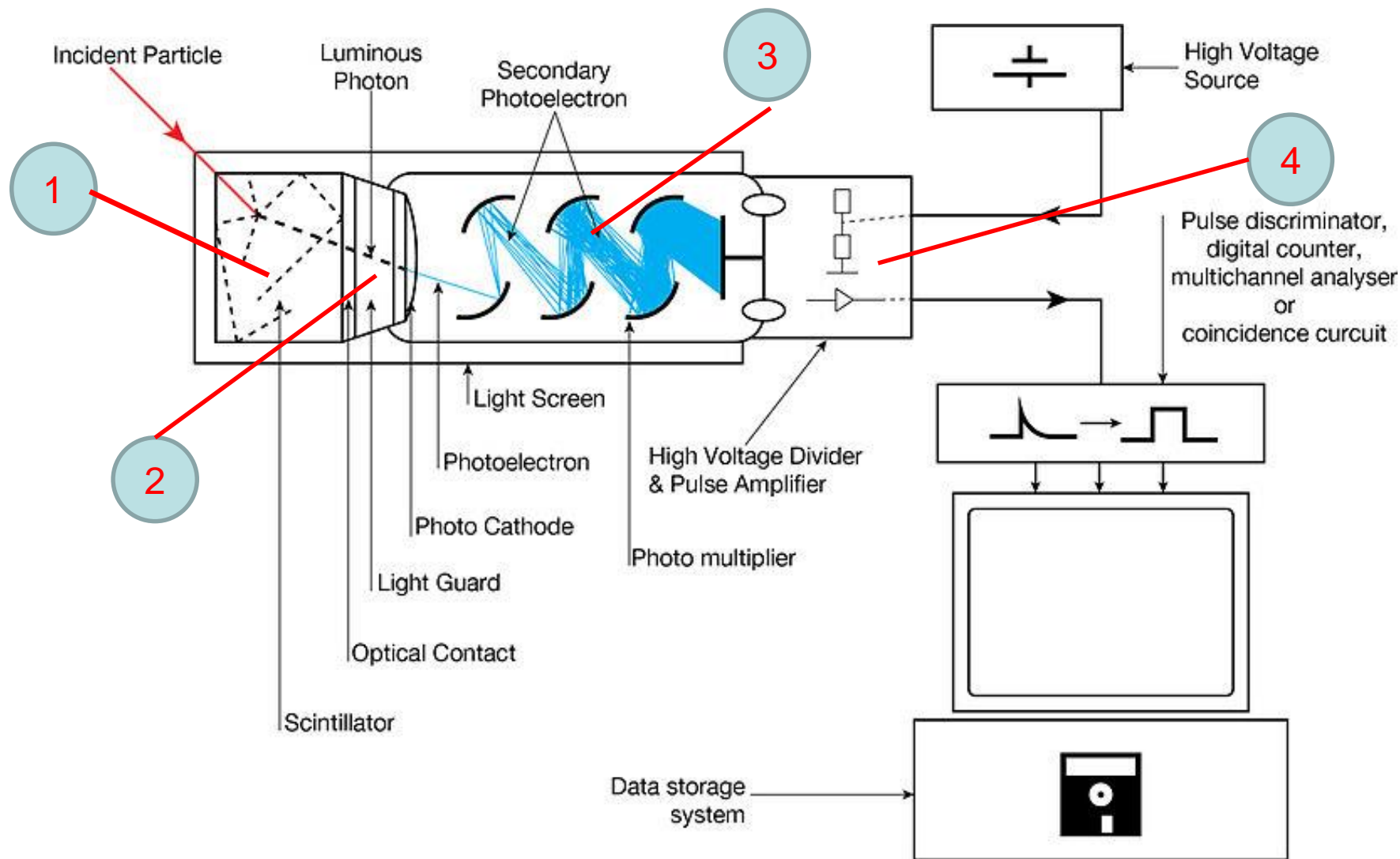


Fig. 13.4 $^3\text{He}(n,p)$, $^{10}\text{B}(n,\alpha)$, and $^6\text{Li}(n,\alpha)$ cross sections as a function of incident neutron energy (Ref. 7).



SCINTILLATOR DETECTOR LAYOUT





ORGANIC SCINTILLATORS

CRYSTALS:

ANTHRACENE, STILBENE, NAPHTHALENE (C_nH_m)

LIQUIDS:

P-TERPHENYL

PLASTIC:

ORGANIC SCINTILLATOR IS EMBEDDED INTO
A POLYMER MATRIX

And more.....

INORGANIC SCINTILLATORS

CRYSTALS:

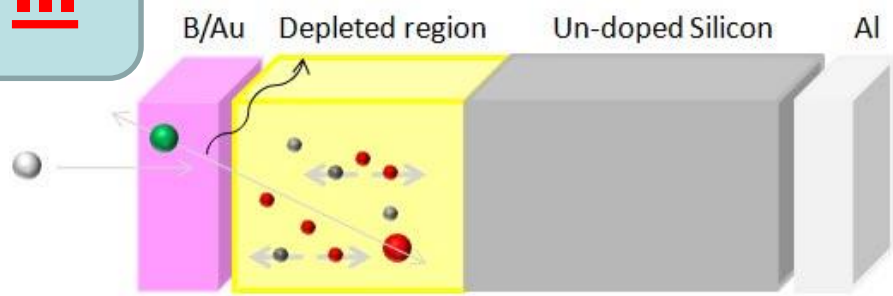
$ZnS(Ag)$, BaF_2 , $CaF_2(Eu)$

GLASSES:

Boron silicates

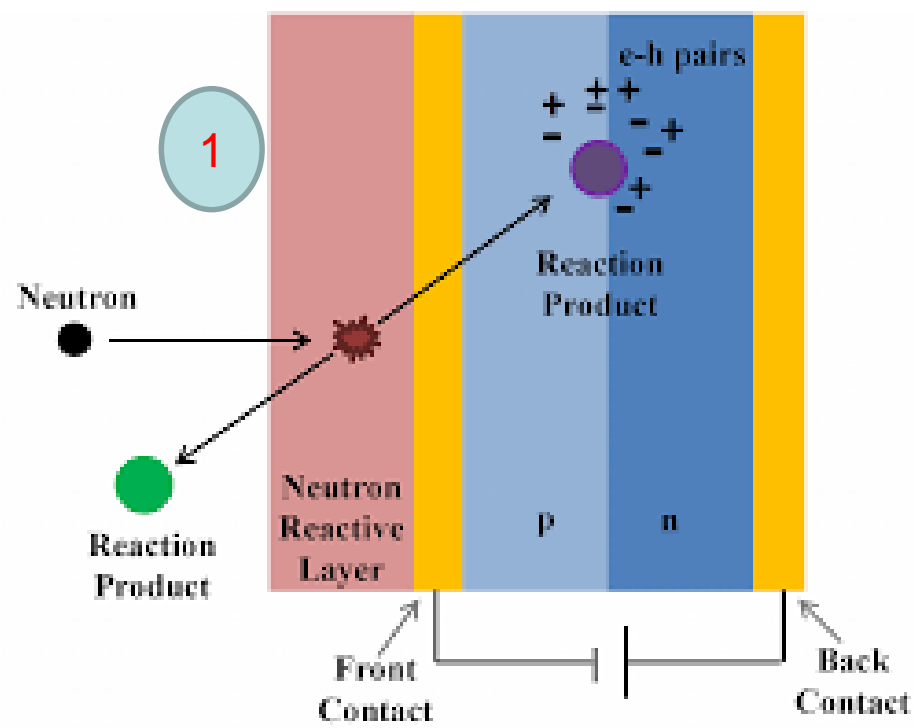


SEMICONDUCTOR-BASED NEUTRON DETECTORS

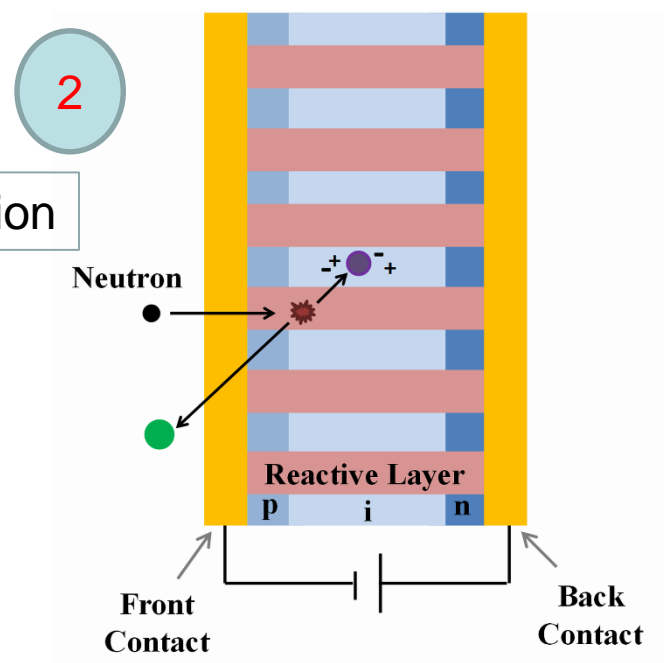


- Electron-hole pairs
- Neutrons
- Li/He from $B(n, \alpha)Li$

p-n junction



p-i-n junction



EXPERIMENTAL NEUTRON SCATTERING ARCHITECTURES

**TIME OF FLIGHT
(TOF)**



SPALLATION

- PULSED NEUTRONS PRODUCTION;
- WHITE BEAM

STEADY SOURCES



FISSION

- STEADY FLUX
- CONVENTIONAL

TIME OF FLIGHT (TOF) GEOMETRY

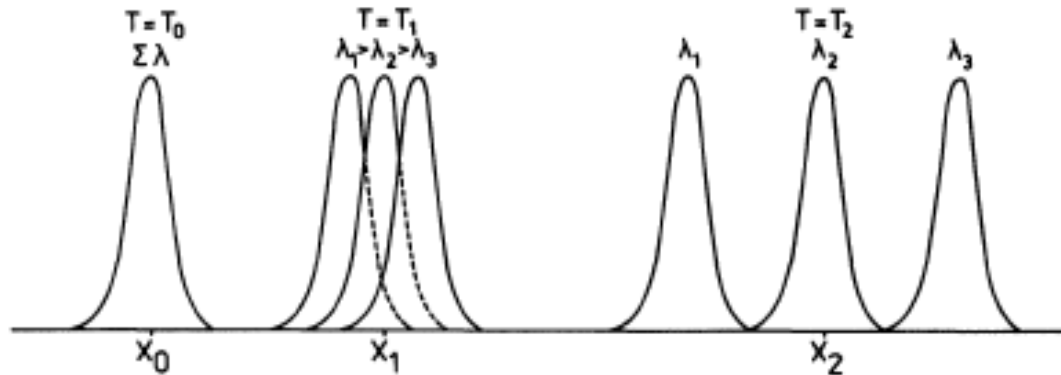
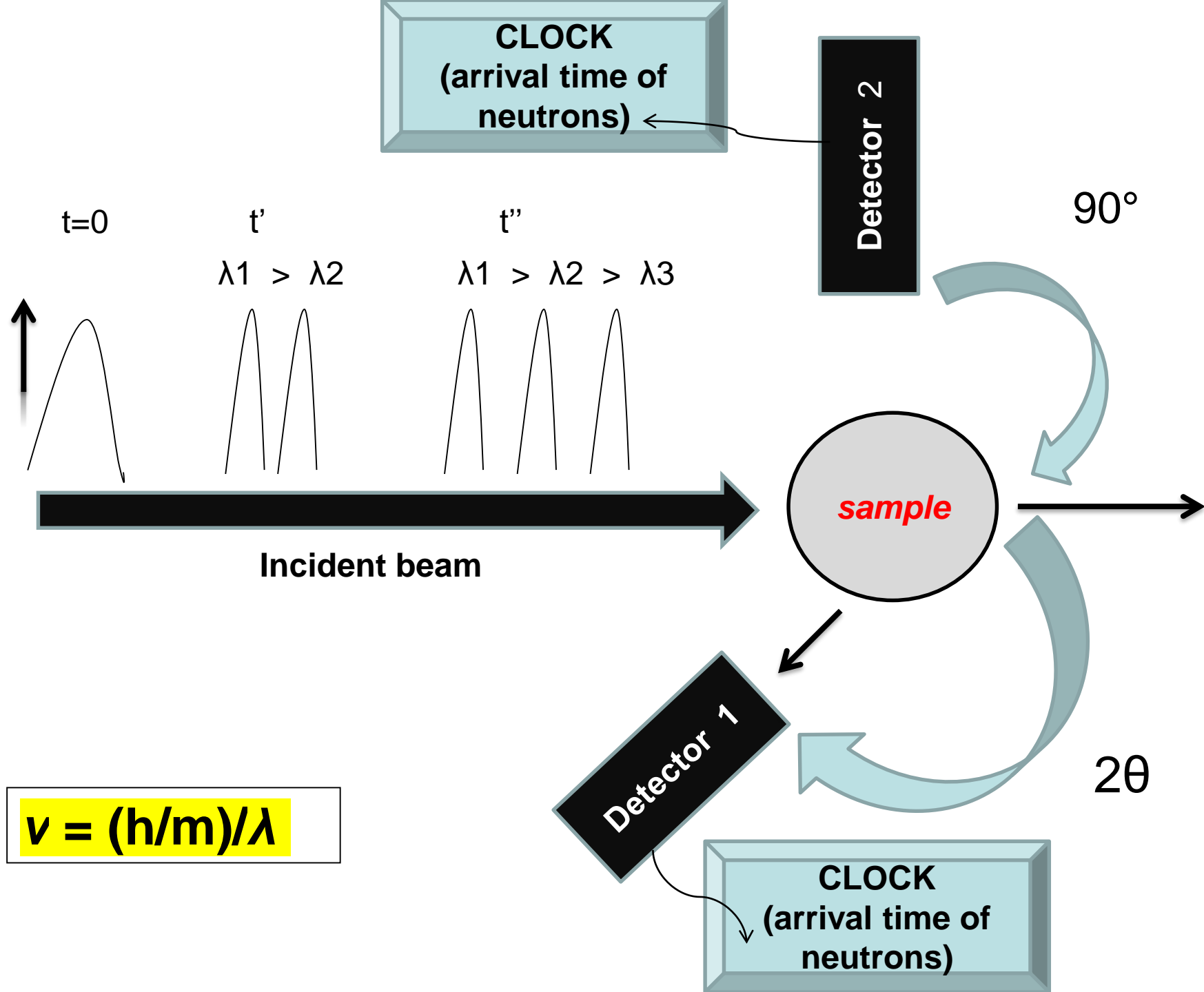


Figure 2 Behaviour of the polychromatic neutron pulse. At time T_0 the pulse leaves the moderator surface. It contains all wavelengths. After a short time T_1 the λ_2 -neutrons arrive at the point x_1 . The λ_3 -neutrons have passed it already, the λ_1 neutrons are slower. Passing a long flight path x_2 (long time T_2) the three different wavelength pulses are separated completely.

- NEUTRONS WITH DIFFERENT WAVELENGTHS HAVE DIFFERENT ARRIVAL TIMES AS A FUNCTION OF THEIR DIVERSE VELOCITIES!
- DETECTORS DISCRIMINATE ON THE BASIS OF A CLOCK REGISTERING NEUTRONS ARRIVAL AND SYNCHRONIZED WITH THE PULSE FROM THE SOURCE



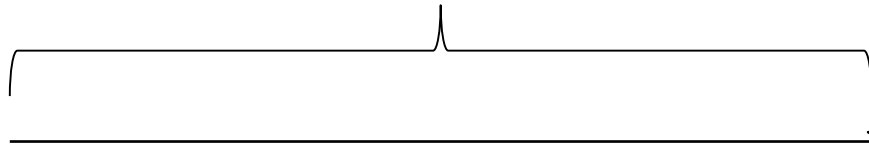
time = Time required by neutrons from their source to the detector, passing through the sample

$$v = (L_1 + L_0) / \text{time}$$

$$\lambda = h / (m v)$$

$$2 d \sin(\theta) = \lambda = (h/m) * \text{time} / (L_0 + L_1)$$

L_0



Neutrons «flying» \Rightarrow

Fixed geometry!

2θ

sample

L_1

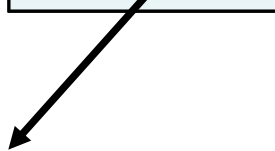
CLOCK
detector

$$d = \frac{h}{2 \sin(\theta_0) m_N} \frac{t}{(L_0 + L_1)}$$

Bragg-Law
with
TOF



RESOLUTION

$$R = \frac{\Delta d}{d}$$


Where Δd is obtained by differentiating the Bragg Law:

$$2 \times d \times \sin(\theta) = \lambda \text{ (standard)}$$

$$d = \frac{h}{2 \sin(\theta_0) m_N} \frac{t}{(L_0 + L_1)} \text{ (TOF)}$$

RESOLUTION WITH TIME OF FLIGHT

$$R = \frac{\Delta d}{d} \approx \frac{\Delta L(\textit{flight})}{L(\textit{flight})}$$

RESOLUTION WITH STEADY SOURCES

$$R = \frac{\Delta d}{d} \approx \textit{ctg}(\vartheta) \Delta \vartheta$$

INTERACTIONS OF NEUTRON WITH MATTER

```
graph TD; A[INTERACTIONS OF NEUTRON WITH MATTER] --> B[NUCLEAR]; A --> C[MAGNETIC]; B --> D[NUCLEUS - NEUTRON]; D --> E["A constant factor<br/>For each chemical species"]; C --> F["ATOMIC MAGNETIC<br/>FIELD – NEUTRON<br/>SPIN"]; F --> G["A function<br/>For each chemical species"];
```

NUCLEAR

MAGNETIC

NUCLEUS - NEUTRON

**ATOMIC MAGNETIC
FIELD – NEUTRON
SPIN**

A constant factor
For each chemical species

A function
For each chemical species

NUCLEAR SCATTERING

STRUCTURE FACTOR (DIFFRACTION of CRYSTALS) X-RAY VERSUS NEUTRONS

$$F_{hkl} = \sum f \left(\frac{\sin \vartheta}{\lambda} \right)_j \times \exp \left(-B_j \times \left(\frac{\sin \vartheta}{\lambda} \right)^2 \right) \times \exp [2\pi \times (h \cdot x_j + k \cdot y_j + l \cdot z_j)]$$

X-ray structure factor

X-ray scattering power is a function of $\sin(\vartheta)/\lambda$, whereas
Neutron scattering length is a constant
 Dependent on the chemical species only

$$F_{hkl} = \sum b_j \times \exp \left(-B_j \times \left(\frac{\sin \vartheta}{\lambda} \right)^2 \right) \times \exp [2\pi \times (h \cdot x_j + k \cdot y_j + l \cdot z_j)]$$

neutron structure factor
(nuclear contribution)

NEUTRON SCATTERING LENGTH

$$b = b_{\text{coherent}} \text{ \& } b_{\text{incoherent}}$$

CONTRIBUTES TO THE
BRAGG PEAKS

CONTRIBUTES TO THE
BACKGROUND

ORIGIN OF COHERENT SCATTERING AND INCOHERENT SCATTERING

$$I(Q) \propto \sum_{j=1}^{N_{atoms\ in\ Cry}} b_j e^{-B_j Q^2} e^{2\pi i \vec{Q} \cdot \vec{X}_j} \times \sum_{k=1}^{N_{atoms\ in\ Cry}} b_k e^{-B_k Q^2} e^{-2\pi i \vec{Q} \cdot \vec{X}_k}$$

$$\sum_{j,k=1}^{N_{atoms\ in\ Cry}} b_j b_k e^{-B_j Q^2} e^{-B_k Q^2} e^{2\pi i \vec{Q} \cdot (\vec{X}_j - \vec{X}_k)}$$

$$b_j = \langle b_{species\ in\ j} \rangle + \varphi_j \sigma_{species\ in\ j} \quad \langle \varphi_j \rangle = 0$$

$$\sum_{j,k=1}^{N_{atoms\ in\ Cry}} b_{j,coe} b_{k,coe} e^{-B_j Q^2} e^{-B_k Q^2} e^{2\pi i \vec{Q} \cdot (\vec{X}_j - \vec{X}_k)} + \sum_{k=1}^{N_{atoms\ in\ Cry}} \varphi_k^2 \sigma_k^2 e^{-2B_k Q^2}$$



$$\sum_{j,k=1}^{N_{atoms\ in\ EC}} b_{j,coe} b_{k,coe} e^{-B_j Q^2} e^{-B_k Q^2} e^{2\pi i \vec{Q} \cdot (\vec{X}_j - \vec{X}_k)} + \sum_{k=1}^{N_{atoms\ in\ EC}} b_{k,inc}^2 e^{-2B_k Q^2}$$

BRAGG COHERENT CONTRIBUTION

INCOHERENT CONTRIBUTION

MAGNETIC SCATTERING

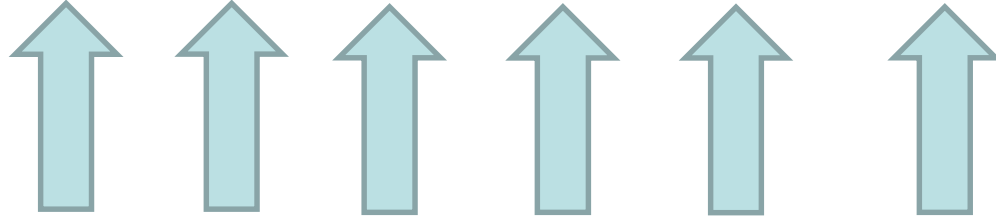
MAGNETIC SCATTERING ALLOWS US TO INVESTIGATE
MAGNETIC PROPERTIES OF MATTER, WHICH ARE RELATED
TO THE MAGNETIC MOMENTS OF THE ATOMS

MAGNETIC SCATTERING IS DUE TO INTERACTIONS BETWEEN

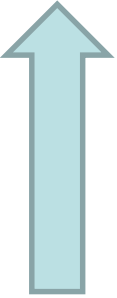
- NEUTRON MAGNETIC MOMENT
and
- MAGNETIC FIELD GENERATED BY ATOMIC ELECTRONS

ARRAYS OF MAGNETIC MOMENTS OF ATOMS

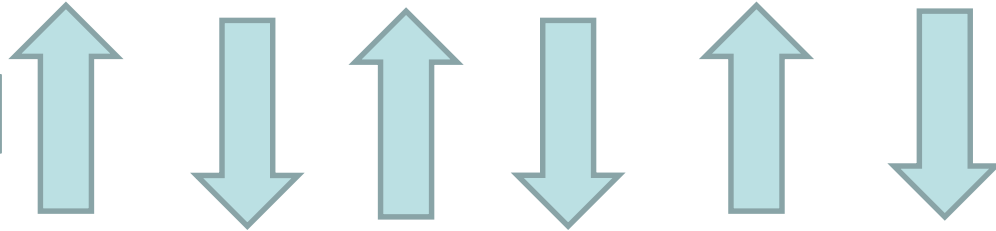
FERROMAGNET



$\Sigma =$

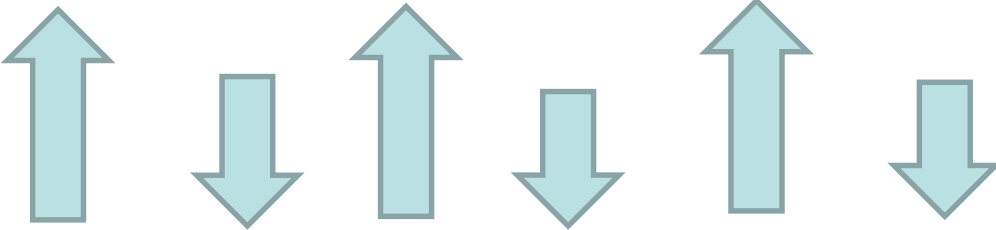


ANTIFERROMAGNET



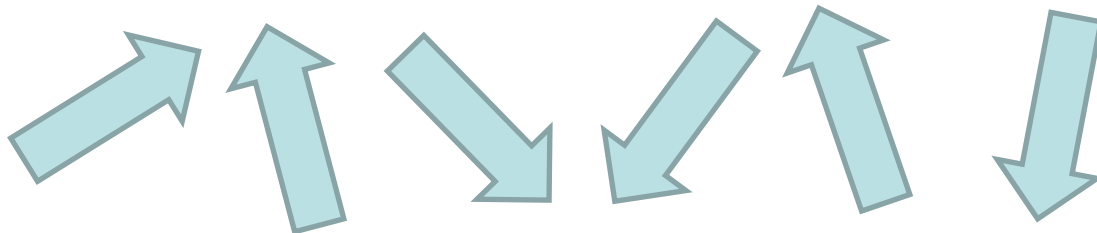
$\Sigma = 0$

FERRIMAGNET



$\Sigma =$ 

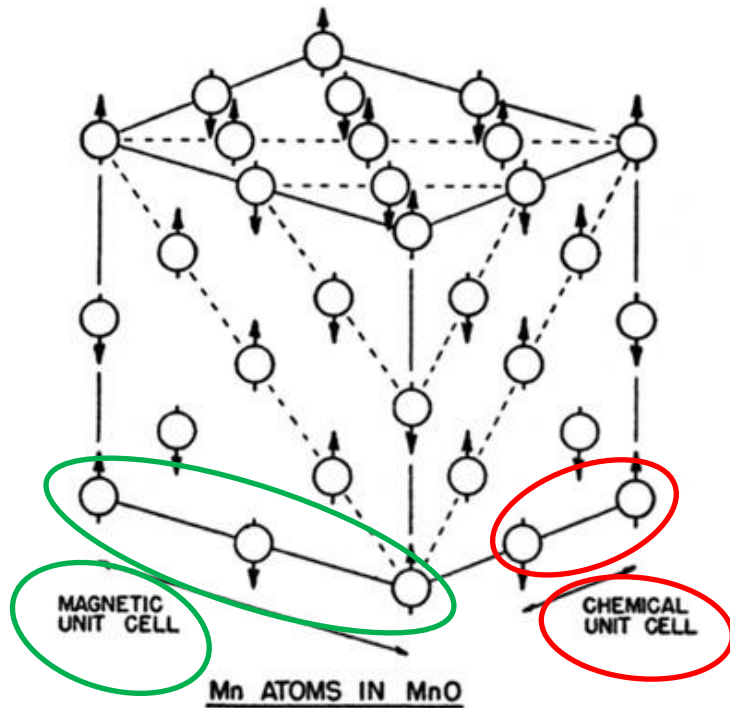
PARAMAGNET



$\Sigma = 0$

AND MORE....

MAGNETIC VERSUS CHEMICAL STRUCTURE



**ATOMS ARE EQUIVALENT
AS A FUNCTION OF THEIR
CHEMICAL SPECIES AND
MAGNETIC MOMENTS**

Equivalent by translation

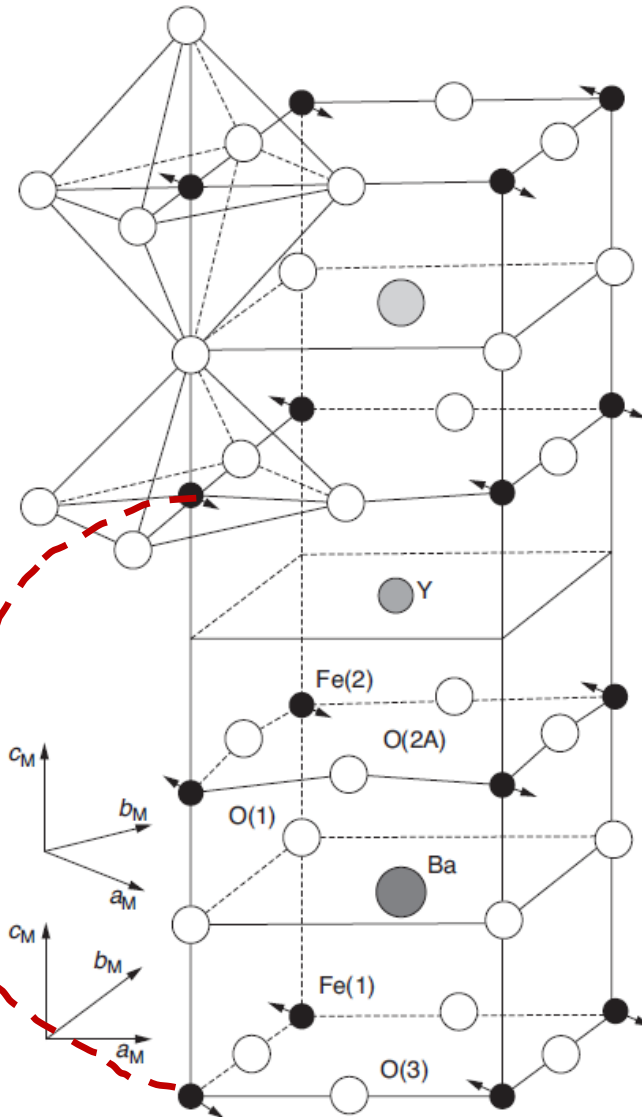


Figure 2. Crystal and magnetic structure for $\text{YBa}_2\text{Fe}_3\text{O}_8$ deduced from the data of Figure 1 (Huang et al., 1992).

MAGNETIC STRUCTURES

FERROMAGNETIC

FERRIMAGNETIC

If $T_{\text{Curie}} < T$

Fe₂O₃ 948 K
Fe₃O₄ 858 K
Fe 1043 K

PARAMAGNETIC

ANTIFERROMAGNETIC

If $T_{\text{Neel}} < T$

MnO 116 K
FeO 198 K
CoO 291 K

PARAMAGNETIC

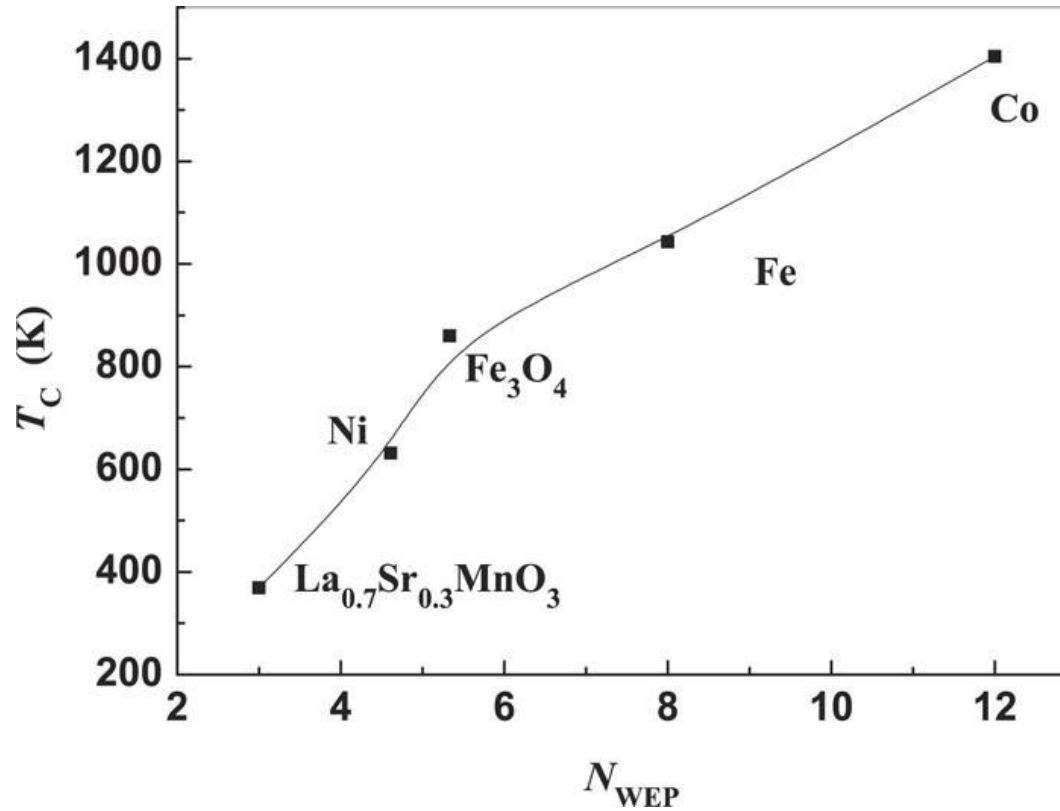


FIG. 2. Dependence of Curie temperature, T_C , on the average number, N_{WEP} of the bonds near one magnetic cation, at which WEPs can be found.

Weiss electron pair (WEP)

MAGNETIC STRUCTURE FACTOR

Magnetic Elementary Cell = MEC

$$F(\vec{Q})_{\text{Magnetic}} \propto \sum_{j=1}^{\text{Atoms in MEC}} \vec{\tau} \times [\vec{M}(\vec{\tau})_j \times \vec{\tau}] e^{-B_j Q^2} e^{2\pi i \vec{Q} \cdot \vec{X}_j}$$

$\vec{\tau}$ Versor parallel to \mathbf{Q}

$\vec{M}(\vec{\tau})_j$ Vector form factor of the j^{th} -atom

$$I(\vec{Q})_{\text{Magnetic}} \propto \left| F(\vec{Q})_{\text{Magnetic}} \right|^2$$

MAGNETIC STRUCTURE FACTOR

$$\vec{F}(\vec{Q})_{Magnetic} = \sum_{j=1}^{\text{atoms in magnetic cell}} \vec{\tau} \times [\vec{M}(\vec{Q})_j \times \vec{\tau}] e^{2\pi i \vec{Q} \cdot \vec{X}_j} e^{-Q^2 B_j}$$

$\vec{\tau}$ Versor parallel to \mathbf{Q}

$\vec{M}(\vec{Q})_j \times \vec{\tau}$ Vector form factor of the j^{th} -atom

$$I(\vec{Q})_{Magnetic} \propto |\vec{F}(\vec{Q})_{Magnetic}|^2$$

Magnetic Elementary Cell = MEC

- General scattering equation and its origin
- Lattice translation invariance: implications on scattering
(metric-component and physical-chemical component – full derivation not required)
- Reciprocal lattice: what is it?
- Structure factor (thermal vibrations; anomalous scattering; atomic scattering power);
- Occupancy factors; «practical expression» for F_{hkl}
- Relations between structure factor and experiments: i) structure refinements;
ii) structure solving (direct methods; charge flipping; MEM)
- X-ray Powder diffraction: experimental geometries (Debye-Scherrer/Bragg-Brentano)
- Rietveld method: what is it? How does it work? What information can we obtain from XRPD using the Rietveld method?
- Neutron scattering: nuclear contribution