

ISTW 2022

The 21st International Spherical Torus Workshop

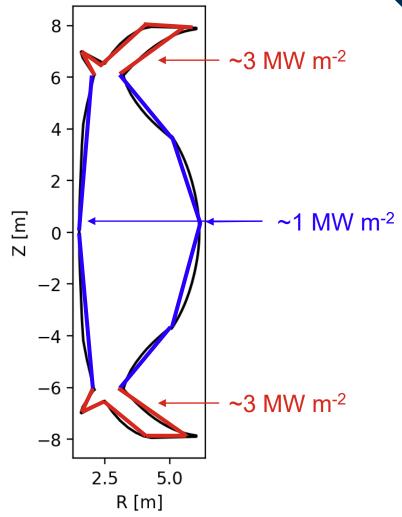
STEP's steady-state α particle losses

A. P. K. Prokopyszyn, H. J. C. Oliver, K. G. McClements, D. A. Ryan and the STEP team

Aims

ISTW UK Atomic Energy Authority

- Calculate steady-state α flux on wall of latest STEP design
- Model losses in:
 - Axisymmetric/2.5D magnetic field
 - 3D field:
 - > Toroidal field (TF) coil's ripple field
 - Resonant magnetic perturbation (RMP) field
- Discuss:
 - How we calculate the results
 - Importance of 3D effects



Approximate, steady-state maximum tolerable heat loads



(Lorentz Orbit Code for Use in Stellarators and Tokamaks)

Solves:

$$m_{He} \frac{d^2 \mathbf{r}_j}{dt^2} = \underbrace{2e \frac{d \mathbf{r}_j}{dt} \times \mathbf{B}(\mathbf{r}_j)}_{Lorentz\ force} + \underbrace{\mathbf{F}_{\alpha,i}(\mathbf{r}_j) + \mathbf{F}_{\alpha,e}(\mathbf{r}_j)}_{\alpha-ion+\alpha-electron\ collision\ force}$$

where j = marker #

- We use GPU hardware
- Follow $\sim 0.5 \times 10^6$ markers
- Until thermalisation/collision with wall (< 1s)
- $\Delta t = 1 \text{ ns} (2\pi/\omega_{c,\alpha} \approx 20-50 \text{ ns}) \implies \# \text{ timeteps} \approx 10^9$
- ~10−40 hours with 4 Nvidia A100 GPUs
- See e.g. Akers et al. (2018) and Ward et al. (2021)



Setting up LOCUST



(Lorentz Orbit Code for Use in Stellarators and Tokamaks)

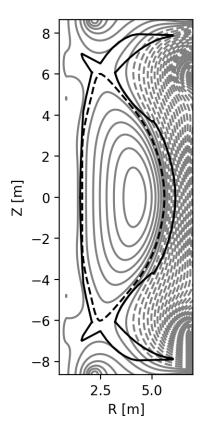
Input:

- Wall
- Magnetic field
 - Axisymmetric field (2D)
 - Ripple field (3D)
 - RMP field (3D)
- Temperature and density profiles
- $x_{
 m initial}$ and $v_{
 m initial}$



Output:

• $x_{
m final}$ and $v_{
m final}$



Obtained from the FIESTA code (SPR-045-6.5)

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(Lorentz Orbit Code for Use in Stellarators and Tokamaks)

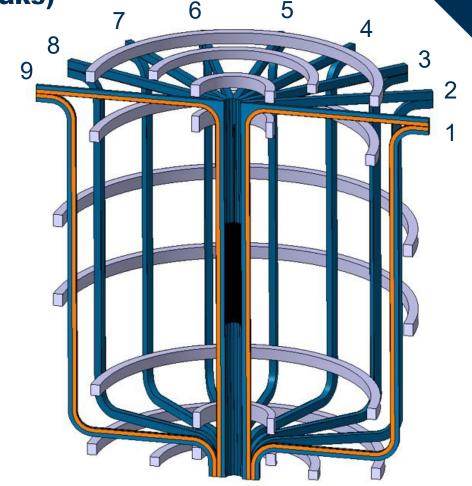
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Courtesy of Aziz Zaghloul and the STEP magnet and design team



(Lorentz Orbit Code for Use in Stellarators and Tokamaks)

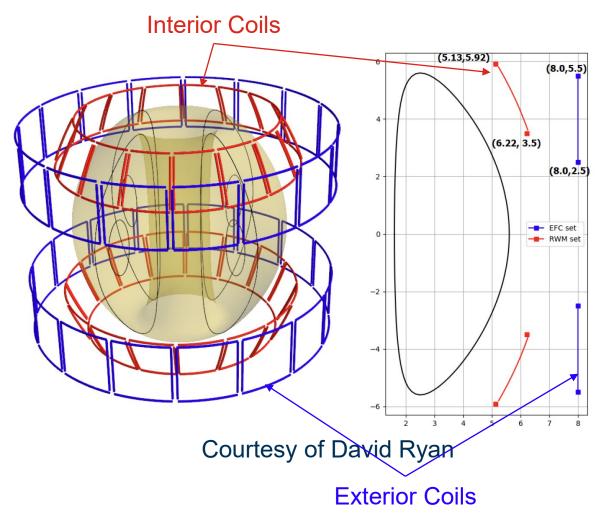
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(Lorentz Orbit Code for Use in Stellarators and Tokamaks)

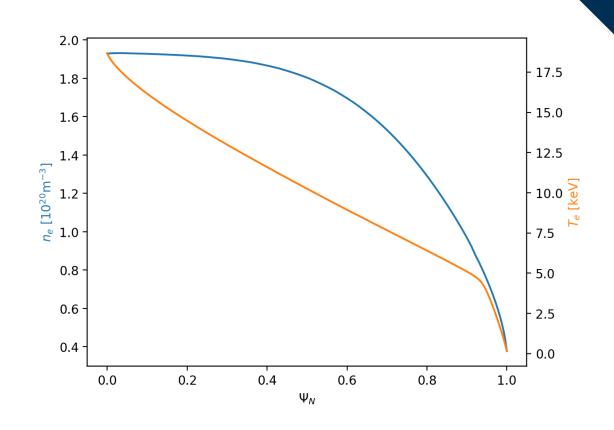
Input:

- Wall
- Magnetic field
 - Axisymmetric field (2D)
 - Ripple field (3D)
 - RMP field (3D)
- Temperature and density profiles
- $oldsymbol{x}_{
 m initial}$ and $oldsymbol{v}_{
 m initial}$



Output:

 $oldsymbol{v}_{ ext{final}}$ and $oldsymbol{v}_{ ext{final}}$



Obtained from the JETTO code (SPR-045-9)



(Lorentz Orbit Code for Use in Stellarators and Tokamaks)

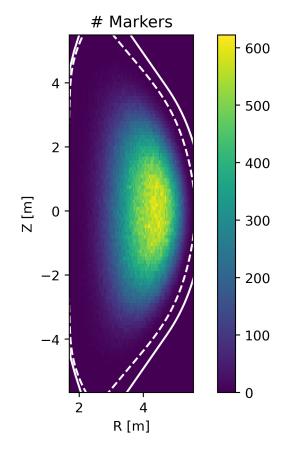
Input:

- Wall
- Magnetic field
 - Axisymmetric field (2D)
 - Ripple field (3D)
 - RMP field (3D)
- Temperature and density profiles
- $x_{
 m initial}$ and $v_{
 m initial}$



Output:

• $x_{\rm final}$ and $v_{\rm final}$



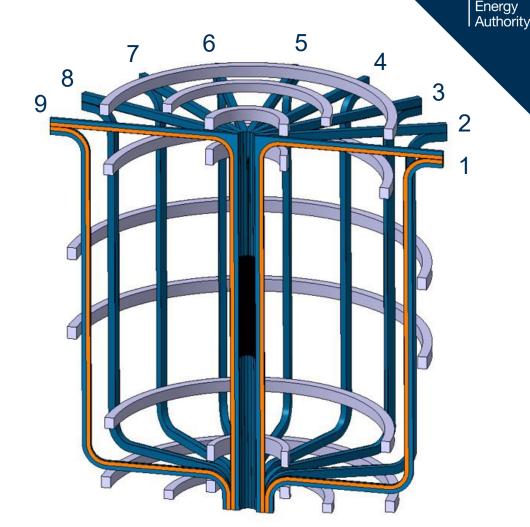
 Markers generated randomly with a probability given by the Bosch-Hale reactivity:

$$R \sim \frac{P^2 \langle \sigma v \rangle}{T^2}.$$

3D Fields

TF Ripple field

- Calculated numerically
- Amplitude $\propto \left(\frac{R}{R_{coil}}\right)^{N_{coil}}$
- Plasma response not included yet
- Ripple losses studied in e.g.:
 - Goldston and Towner (1981)
 - McClements (2005)
 - Yingfeng et al. (2022)



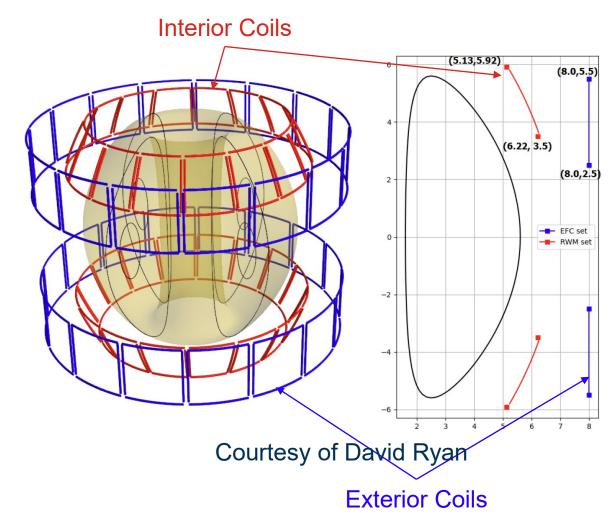
UK Atomic

Courtesy of Aziz Zaghloul and the STEP magnet and design team

RMP (Resonant Magnetic Perturbation) field



- Used to suppress ELMs (Edge Localised Modes), see e.g.
 - Ryan et al. (2015)
 - Haskey et al. (2014)
- Plasma response modelled using MARS code, see e.g.
 - Liu et al. (2015)
- Alpha particle losses in an RMP field studied in e.g.:
 - Sanchis et al. (2018)
 - Ward et al. (2022)

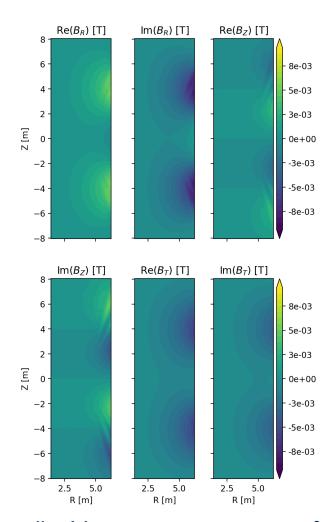






field

- RMP field components given by: $Re[Re[B_R(R,Z)] + i Im[B_R(R,Z)])e^{in\phi}$
- Parameters:
 - Toroidal number (*n*)
 - Exterior vs interior coils
 - Coil current [kAt]
 - Phase difference between upper and lower coil sets $(\Delta \phi)$
 - Vacuum vs plasma response



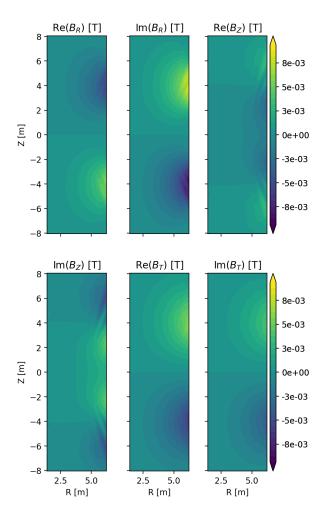
(Exterior coils, Vacuum n=3, $\Delta \phi=0^{\circ}$, 182 kAt)





field

- RMP field components given by: $Re[Re[B_R(R,Z)] + i Im[B_R(R,Z)])e^{in\phi}$
- Parameters:
 - Toroidal number (n)
 - Exterior vs interior coils
 - Coil current [kAt]
 - Phase difference between upper and lower coil sets $(\Delta \phi)$
 - Vacuum vs plasma response



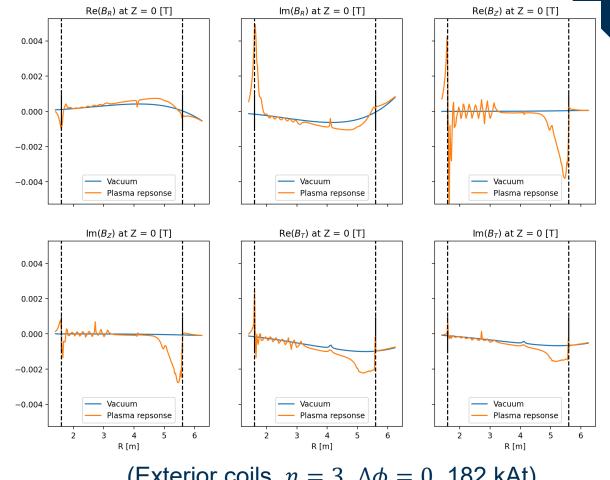
(Exterior coils, Vacuum n=3, $\Delta \phi=180^{\circ}$, 182 kAt)

RMP (Resonant Magnetic Perturbation)



field

- RMP field components given by: $\operatorname{Re}[(\operatorname{Re}[B_R(R,Z)] + i \operatorname{Im}[B_R(R,Z)])e^{in\phi}]$
- Parameters:
 - Toroidal number (n)
 - Exterior vs interior coils
 - Coil current [kAt]
 - Phase difference between upper and lower coil sets ($\Delta \phi$)
 - Vacuum vs plasma response



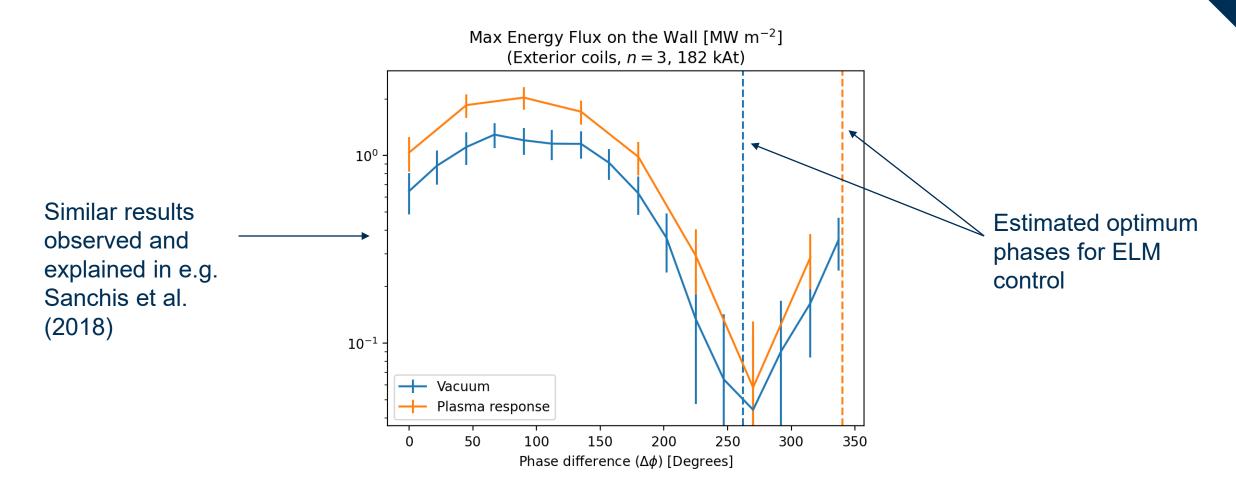
(Exterior coils, n = 3, $\Delta \phi = 0$, 182 kAt)

Results

3D Field	% α power lost	~ Peak flux on the wall	Peak flux location
None (axisymmetric)	0.15%	0.02 MW m ⁻²	Upper outer wall
TF Ripple ($R_{coil} \approx 7.5 \text{ m}$)	0.15%	0.02 MW m ⁻²	Upper outer wall
TF Ripple ($R_{coil} \approx 6.8 \text{ m}$)	0.50%	0.4 MW m ⁻²	Upper outer wall
TF Ripple ($R_{coil} \approx 6.5 \text{ m}$)	2.7%	2.2 MW m ⁻²	Upper outer wall
Ripple + RMP ($R_{coil} \approx 7.5$ m, Exterior-coil, $n=3$, Vacuum, $\Delta \phi = 270^\circ$, 182 kAt)	0.16%	0.04 MW m ⁻²	Upper outer wall
Ripple + RMP ($R_{coil} \approx 7.5$ m, Exterior-coil, $n=3$, Vacuum, $\Delta \phi = 45^\circ$, 182 kAt)	1.2%	1.1 MW m ⁻²	Upper inner wall
Ripple + RMP ($R_{coil} \approx 7.5$ m, Exterior-coil, $n=3$, Plasma Response, $\Delta \phi = 270^\circ$, 182 kAt)	0.19%	0.06 MW m ⁻²	Upper outer wall
Ripple + RMP ($R_{coil} \approx 7.5$ m, EFC, $n=3$, Plasma Response, $\Delta \phi = 45^\circ$, 182 kAt)	1.8%	1.9 MW m ⁻²	Lower outer wall
RMP (Interior Coil, $n=3$, Plasma Response, $\Delta \phi = 217^\circ, 84$ kAt)	0.96%	0.14 MW m ⁻²	Upper Inner wall
RMP (Exterior Coil, $n=1$, Plasma Response, $\Delta \phi = 217^\circ$, 60 kAt)	0.19%	0.02 MW m ⁻²	Upper outer wall

Heat load vs. $\Delta \phi$

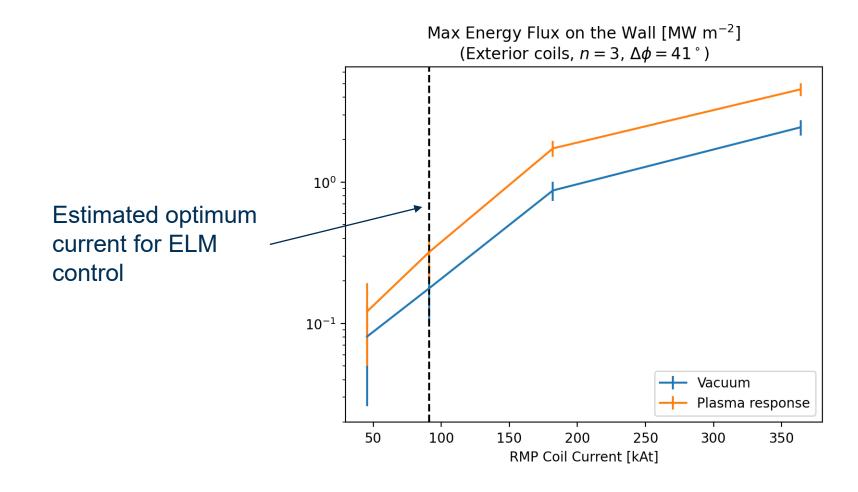




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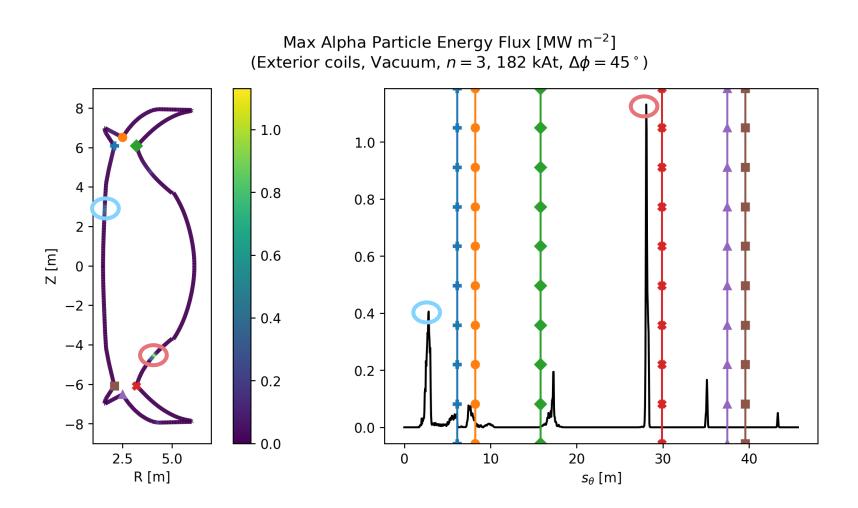
Heat load vs. coil current





Heat load distribution





Summary and further study



Summary:

- Results suggest α heat loads should be acceptable with refinement of parameters
- Axisymmetric peak flux ~ 0.02 MW m⁻²
- 3D peak flux can be as large as ~ 2 MW m⁻²
- Heat loads are sensitive to RMP parameters
- Changing $\Delta \phi$ can reduce heat load by a factor of 10

Further study:

- Why does changing $\Delta \phi$ have such a large affect on the α confinement?
- Will the RMP fields used on ASDEX Upgrade/DIII-D upgrade work for STEP?
- Include 3D field from ferromagnetic structures



Thank you for listening

谢谢!

References



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