

NERS 551

Nuclear Reactor Kinetics

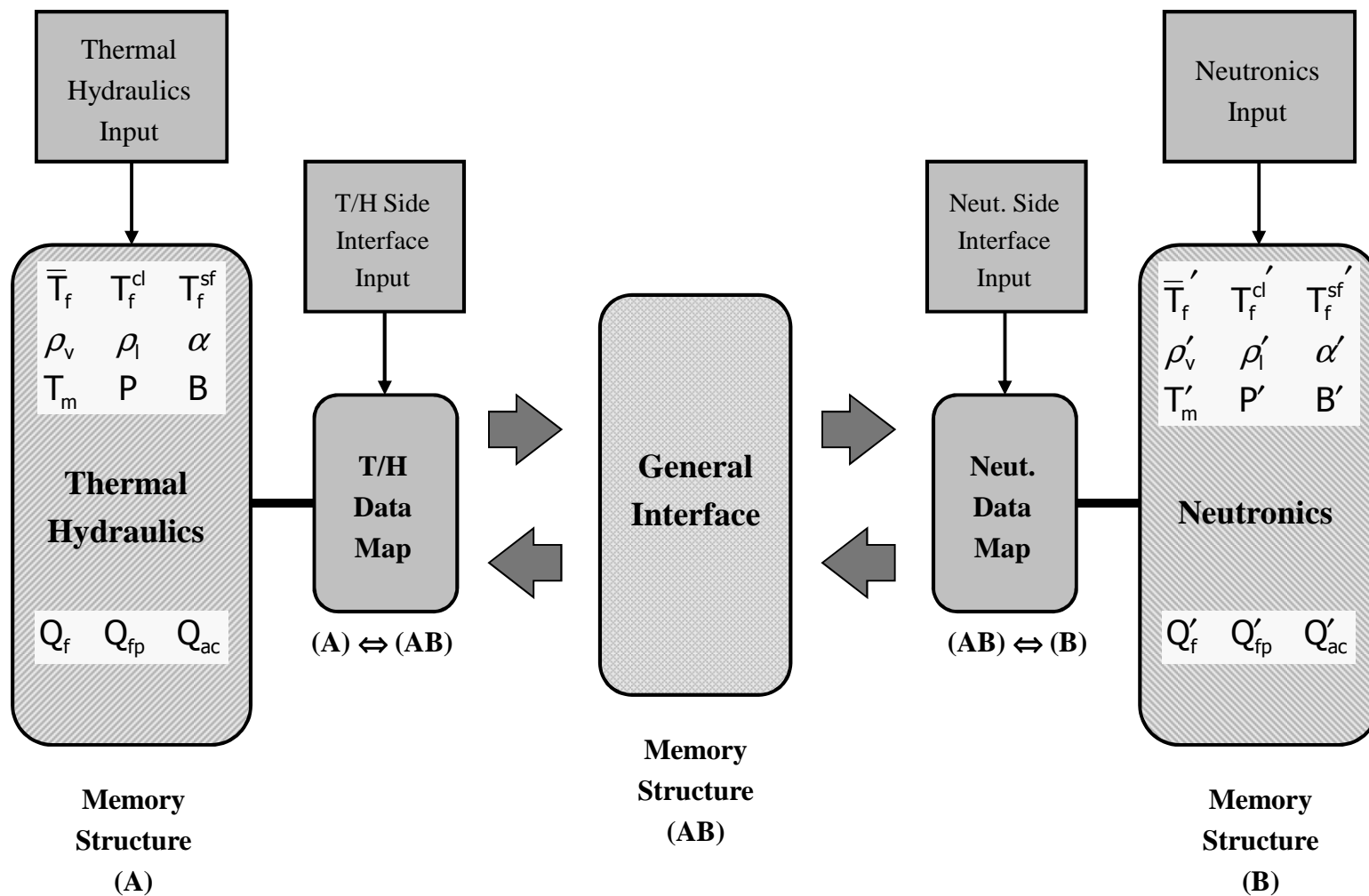
4-8-2011

Yunlin Xu
Thomas J. Downar

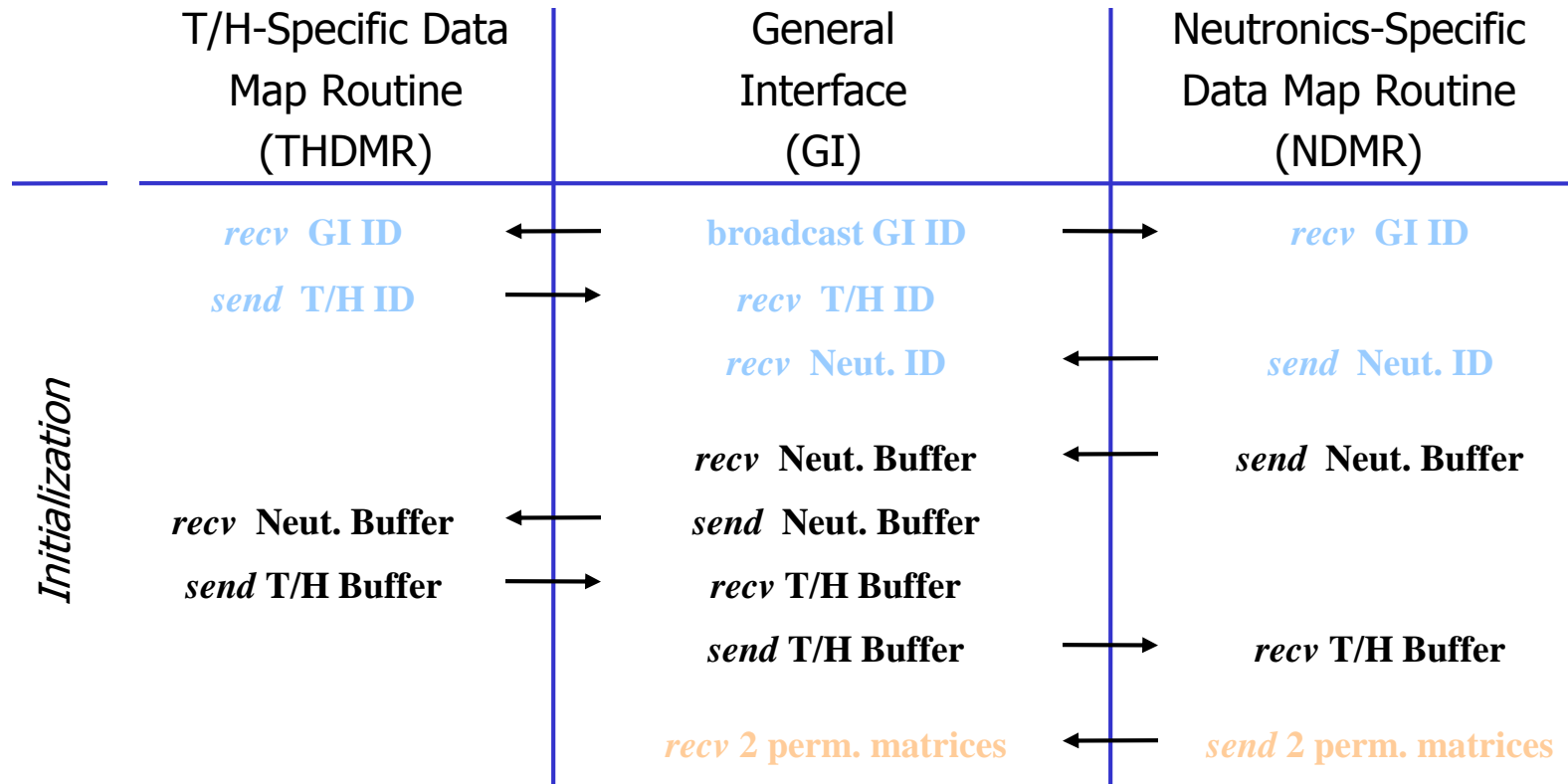
Outline for Today's Class

- Neutronic/Fluid Coupling
 - Data transfer and Mapping
 - Notes on PVM
 - Coupled calculation procedure
 - MSLB
-

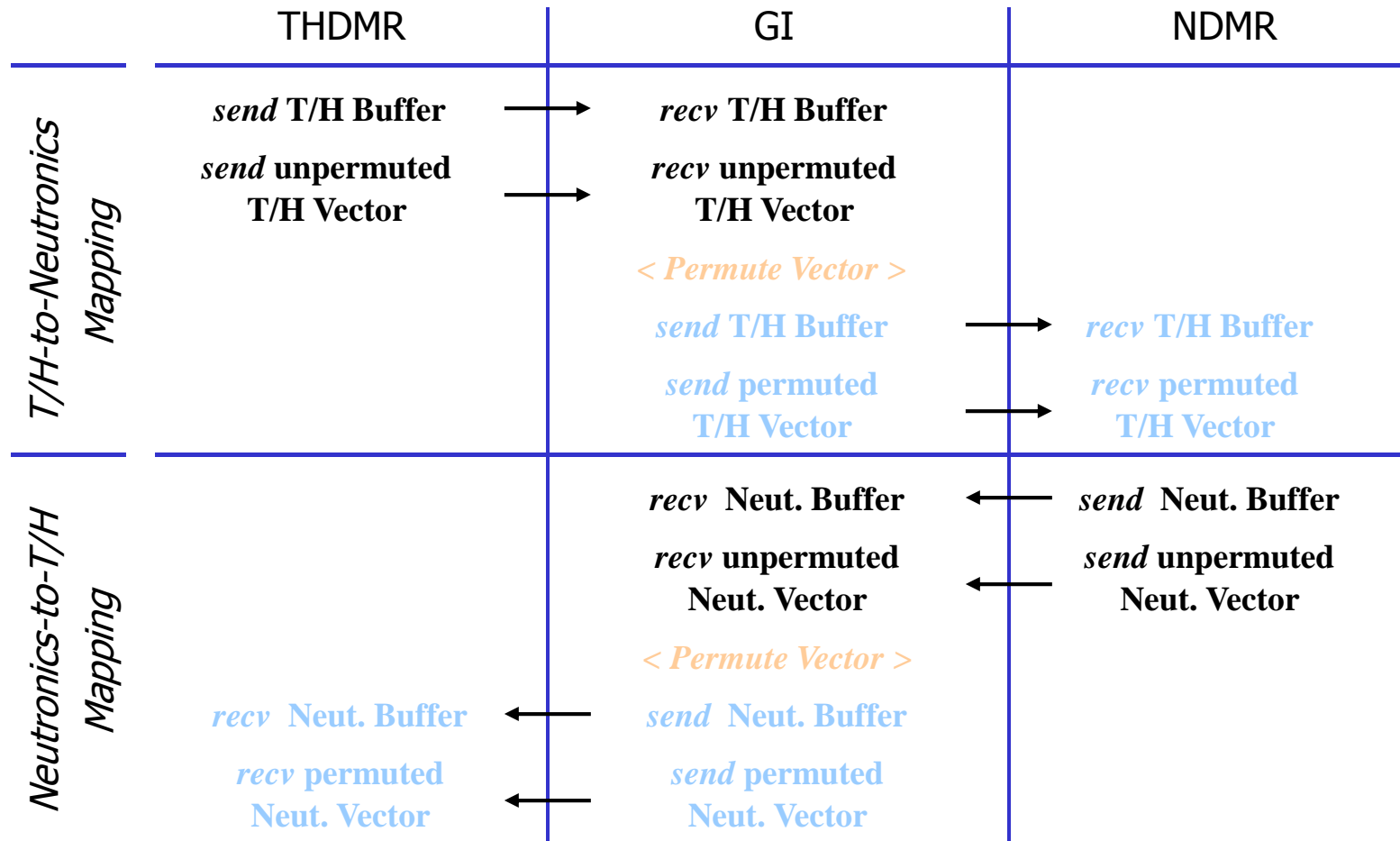
Neutronic/Thermal-Hydraulic Code Coupling



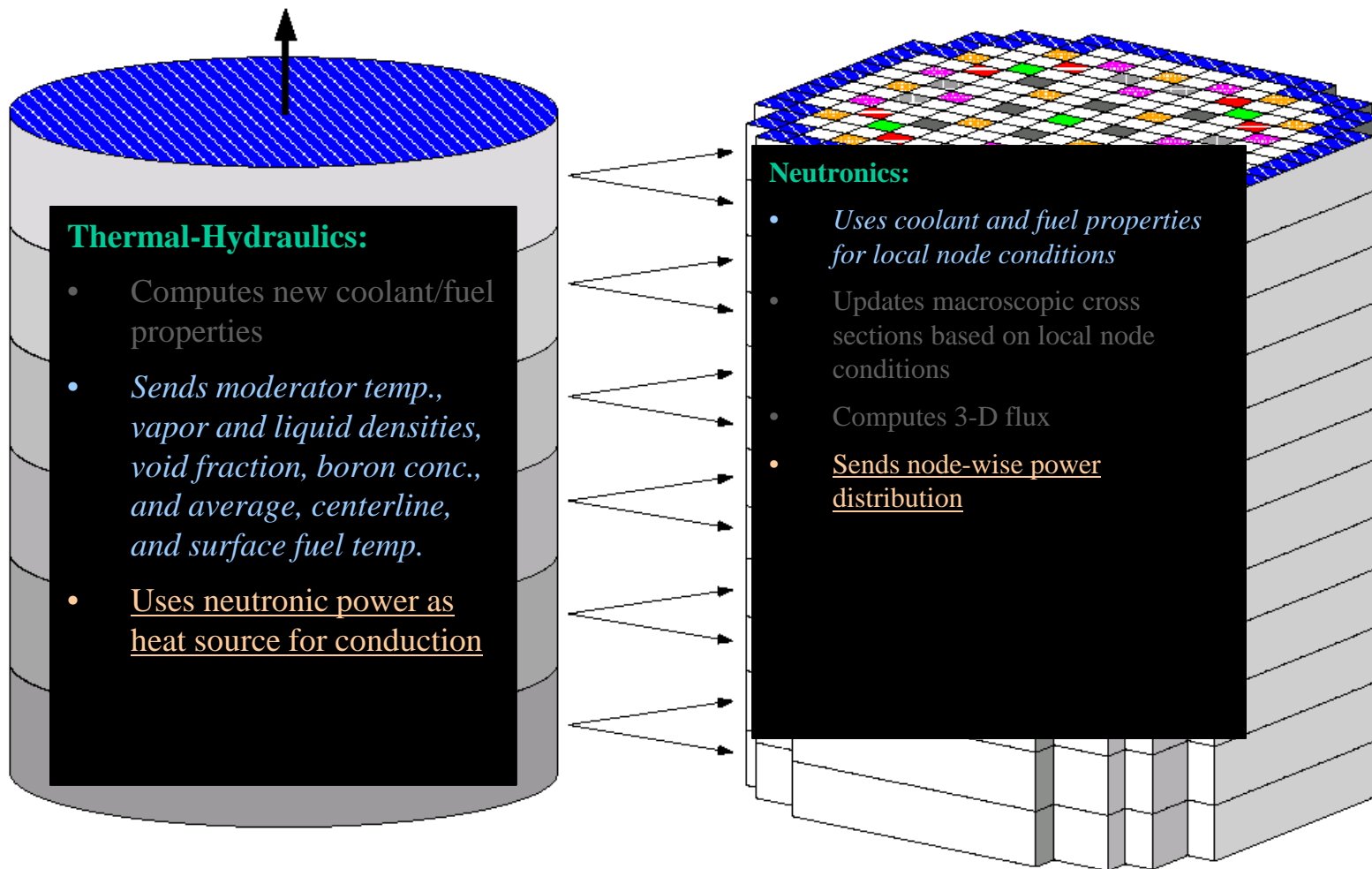
Calculation Control



Calculation Control



Spatial Coupling



General Idea of Spatial Mapping

- Mapping determines
 - where to deposit NK node power in the T/H node
 - Part of NK power goes to TH cell for direct moderator heating
 - Part of NK power goes to HS cell for fuel heat source
 - where to deposit TH cell properties in NK code
 - T/H and HS sends temperatures/densities feedback to NK node
- Weight specifies the fraction of the total neutronic power generated in a particular node that is deposited into its associated TH and HS cell
- Weights are geometric volume fractions determined by what fraction of neutronic node lies in the volume of corresponding TH and HS cell

Important notes on mapping

- Sum of weights for each neutronic node MUST sum up to 1.0
- All neutronic nodes have to be mapped somewhere in the T/H code
- Mapping non-conforming meshes is possible, but makes mapping difficult, for example very coarse T/H mesh to very fine neutronic mesh

Reflector mapping

- Radial reflector:
 - additional heat structure with no power mapped to the TH (bypass) channel should be used
- Axial reflector
 - Heat structures should have additional axial elevation, but the upper and lower ones will have no power (representing axial reflector for mapping)
 - TH-channels should also have additional axial elevations but only from 2 to N-1 represents the active core

MAPTAB format: RELAP5

- NRC didn't want to include it in the manual, so the only guide is from sample problems
- RELAP5 MAPTAB format is much easier than TRACE

%DOPL

same as TRACE

%TRIP

same as TRACE

%TABLE1

pipe_cell_number	PARCS_node	weight
------------------	------------	--------

%TABLE2

hs_cell_number	PARCS_node	weight
----------------	------------	--------

Coupled calculation procedure

- 3-step procedure
 - 1. Steady-state **stand-alone** T/H calculation
 - 2. Steady-state **coupled** TH-NK calculation
 - 3. Transient **coupled** TH-NK calculation
 - Reason: develop flow and good initial guess for fuel and moderator temperature before starting coupled calculation
- 2-step procedure
 - 1. Steady-state **coupled** TH-NK calculation
 - 2. Transient **coupled** TH-NK calculation
 - Reason: “easy” problems can be coupled even with bad initial guess

Notes on PVM

- PVM is necessary to compile PARCS
 - Even the most recent integrated TRACE/PARCS requires PVM for compilation, but NOT for execution
 - This “feature” will be fixed in the future
- PVM 3.4.3 or newer should be used
- PVM will not work properly under Windows if default temporary directory is used!
 - Use simple path for PVM temporary directory, for example:
 - C:\temp
 - C:\tmp
 - And make sure this directories exist!
- PVM can be run as “PVM Console” or “PVM Daemon”, I recommend running it as “PVM Console” as it is easier to monitor PVM status
- PVM Console has to be shut down with “halt” command, otherwise, follow procedure below to fix PVM problems
- If you get PVM errors during coupled run, do following:
 - Reboot computer
 - Go to PVM’s temporary directory (C:\temp or C:\tmp)
 - Exact path is set by PVM_TMP environment variable
 - Remove “pvmd.*” and “pvml.*” files
 - Reboot computer
 - Start “PVM Console”

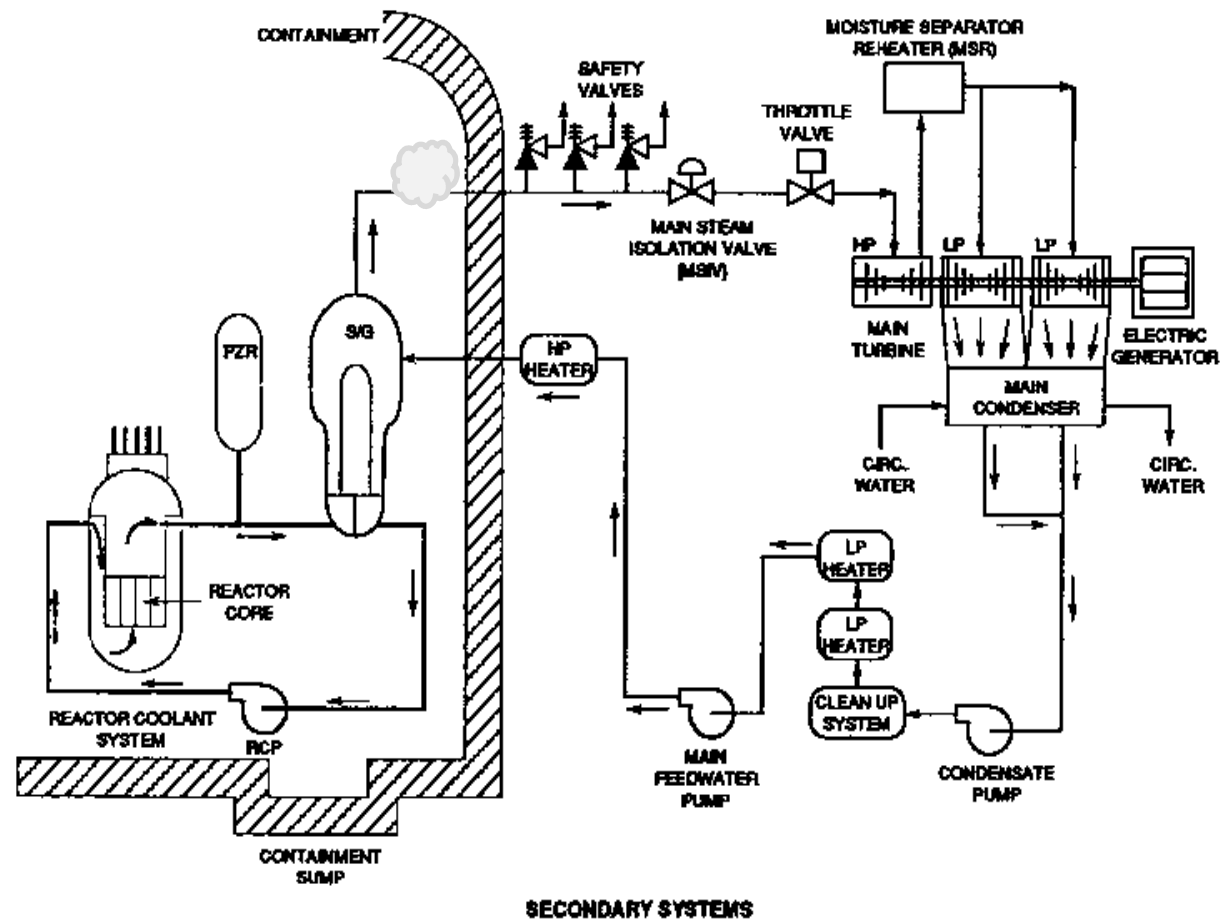
OECD/NEA MSLB Benchmark

- Based on B&W TMI1 reactor in Pennsylvania, a PWR
- Accident Scenario
 - Break of a Main Steam Line in a Secondary Loop
 - Sudden (Secondary Side) Pressure Decrease in Steam Generator
 - Enhanced Heat Removal from Primary to Secondary
- *Coolant Temperature Reduction in Core Inlet (One Side Only)*
- Positive Reactivity Feedback / Core Power Increase
- *High Flux (114%) Trip Set Point / Reactor Scram / Highest Worth Rod Stuck*
- Continuous Coolant Overcooling and Positive Reactivity Insertion
- Distorted Radial Power Distribution Over Time
 - *Over-Cooling in One Side of Core*
 - *Mainly Due to the Stuck Rod Assumption*
 - *Requires 3D Kinetics*

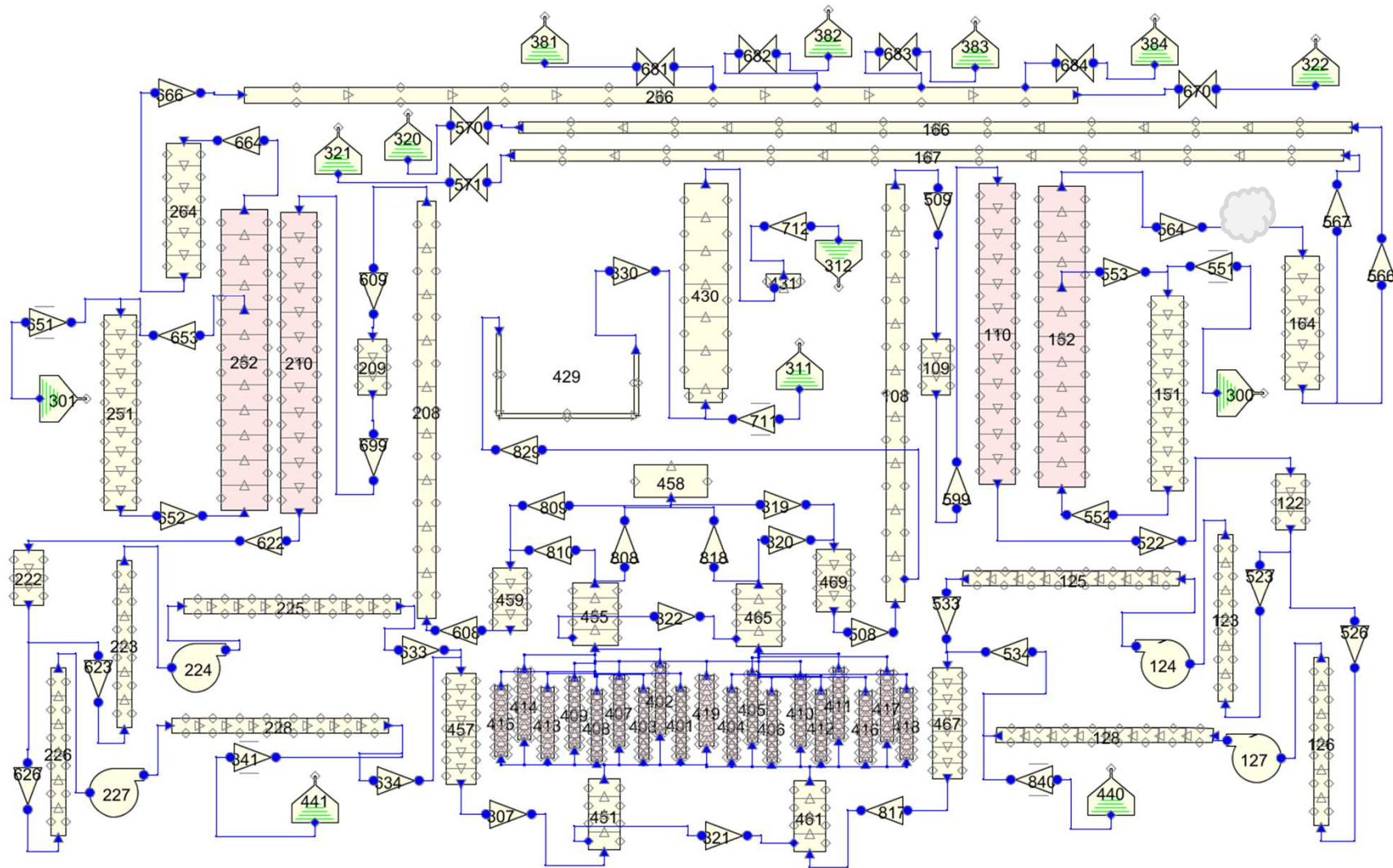


Nuclear Reactor Transient Analysis: Main Steam Line Break

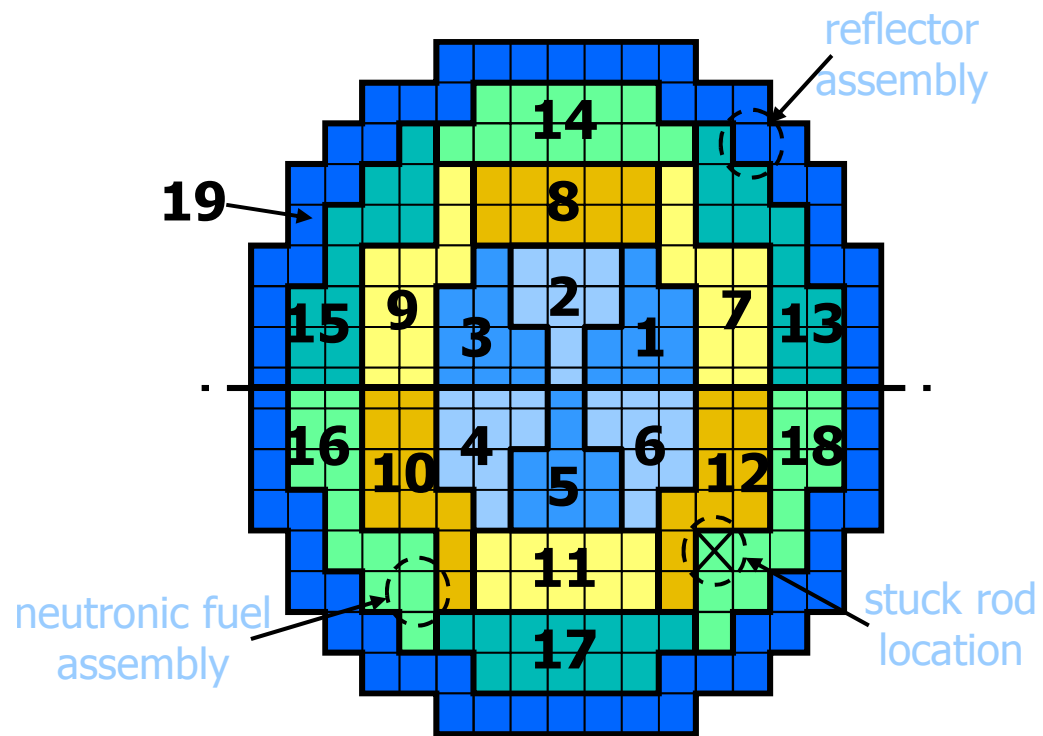
PWR Plant Schematic



RELAP Model

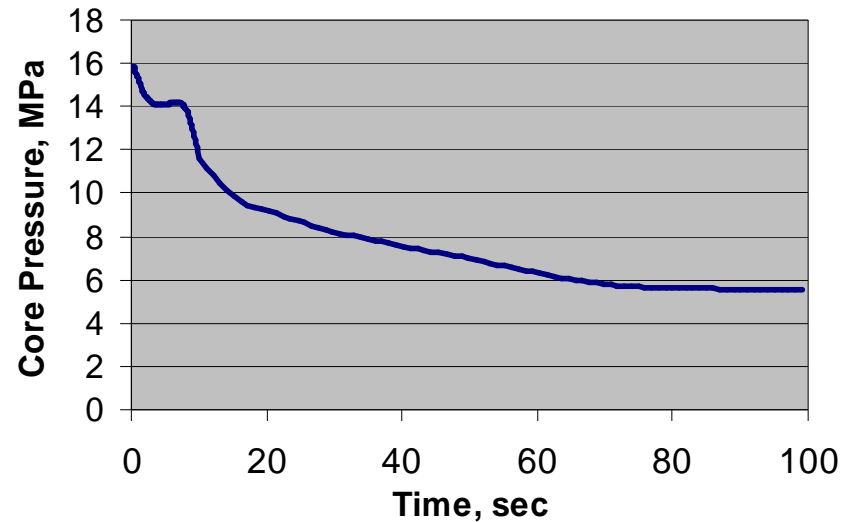
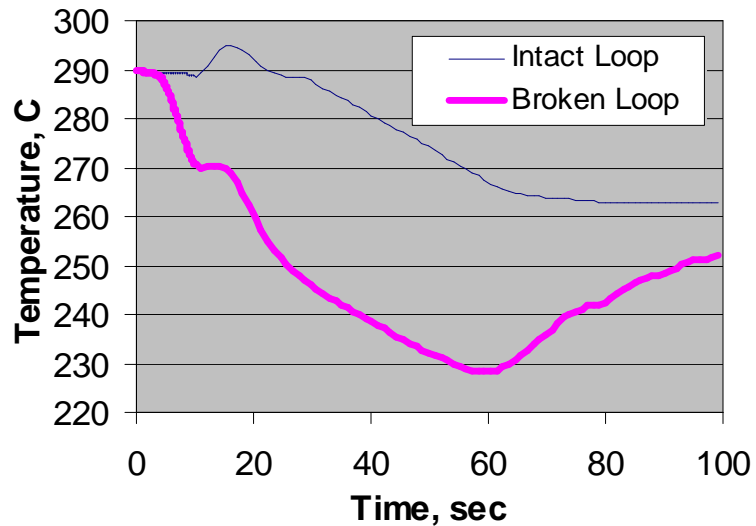


Neutronics Model and Mapping

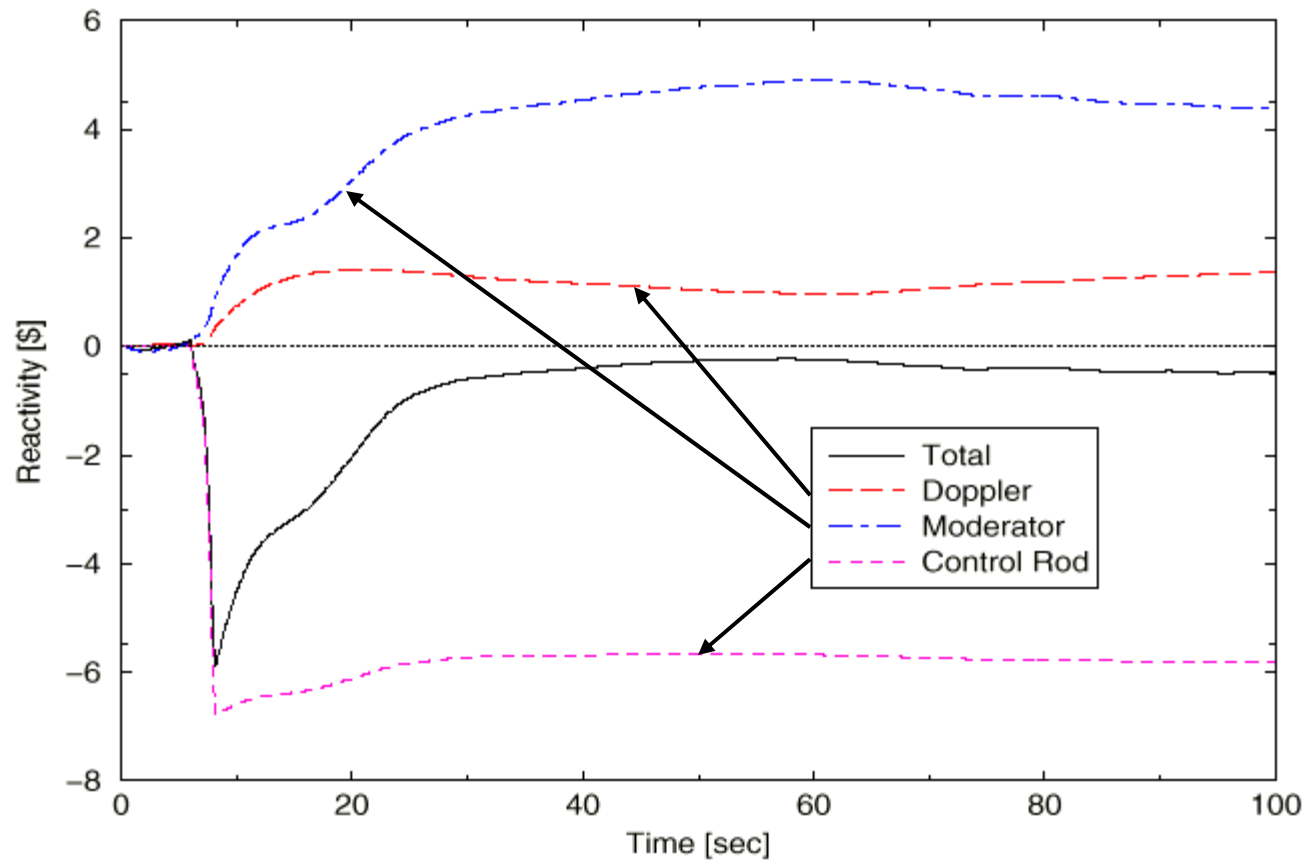


OECD/NEA MSLB Benchmark:

Temperature and Pressure

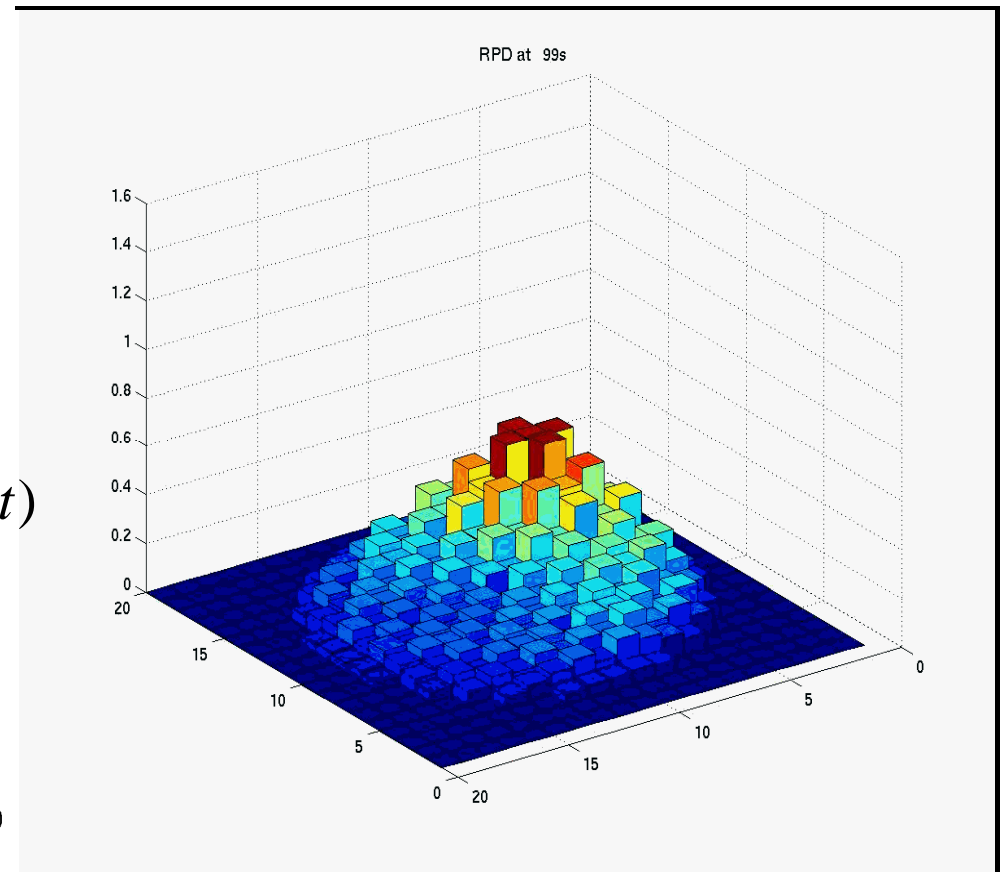
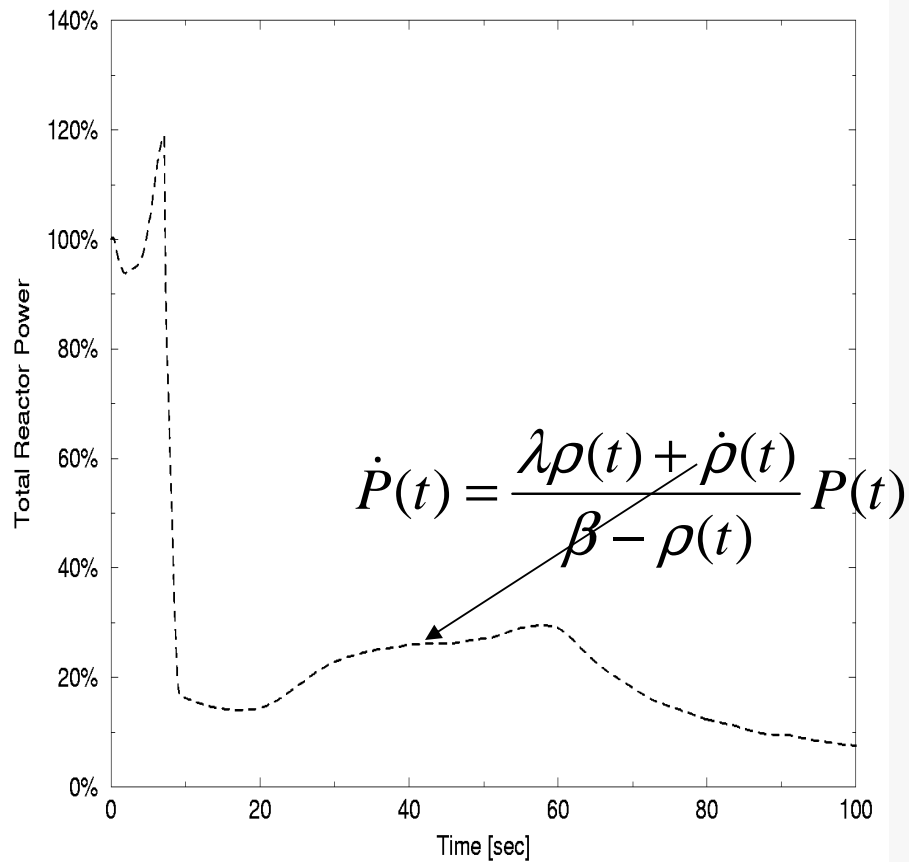


OECD/NEA MSLB Benchmark: Reactivity



MSLB Transient Analysis

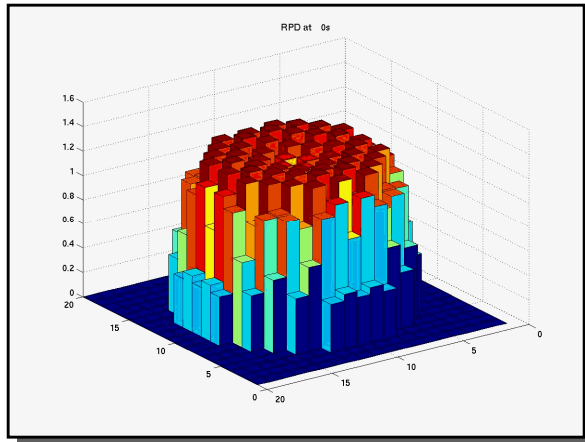
- Radial Power Evolution



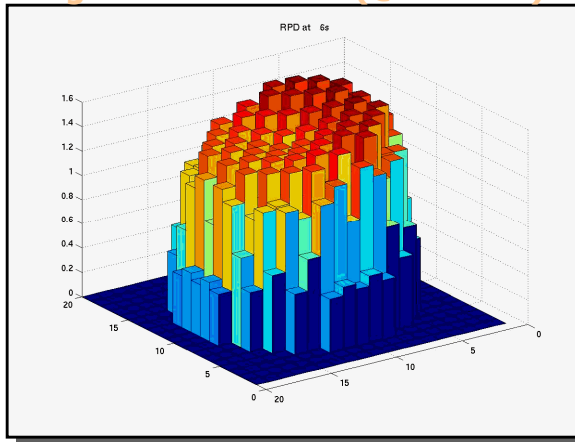
OECD/NEA MSLB Benchmark:

Radial Power

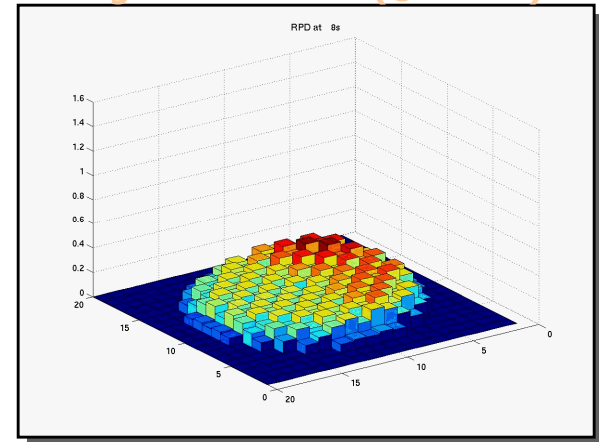
Initial HFP State



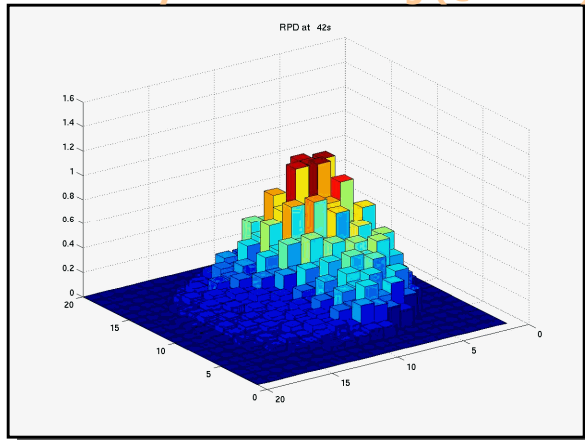
Right Before Scram (@6.03 sec)



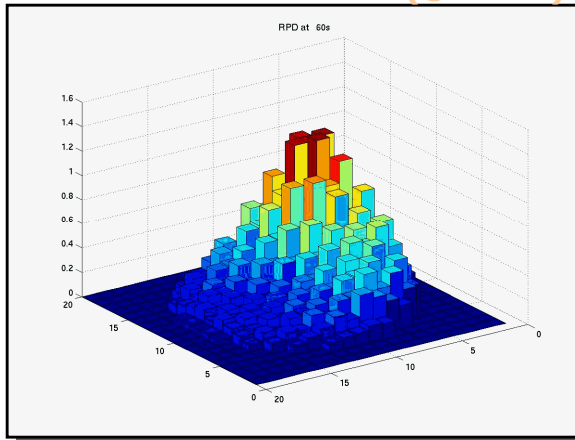
Right After Scram (@8.3 sec)



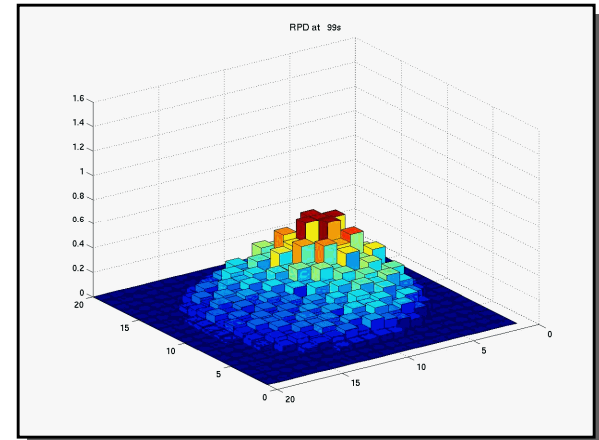
Max. Assy Power Peaking (@42 sec)



Max. Return to Power (@60 sec)



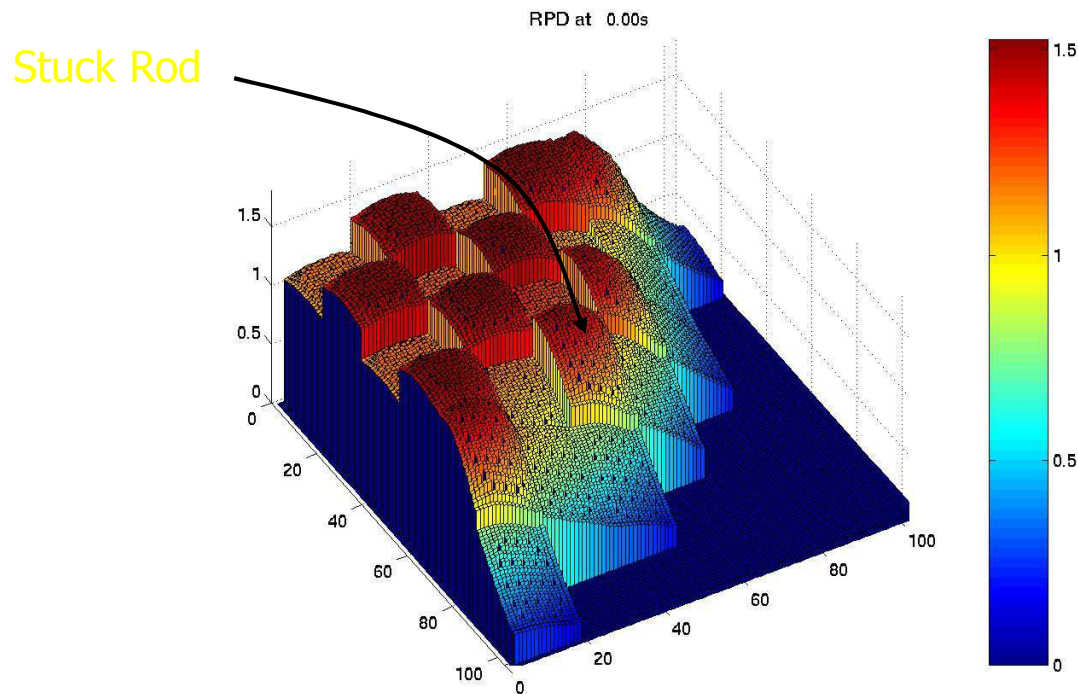
End of Transient



OECD/NEA MSLB Benchmark:

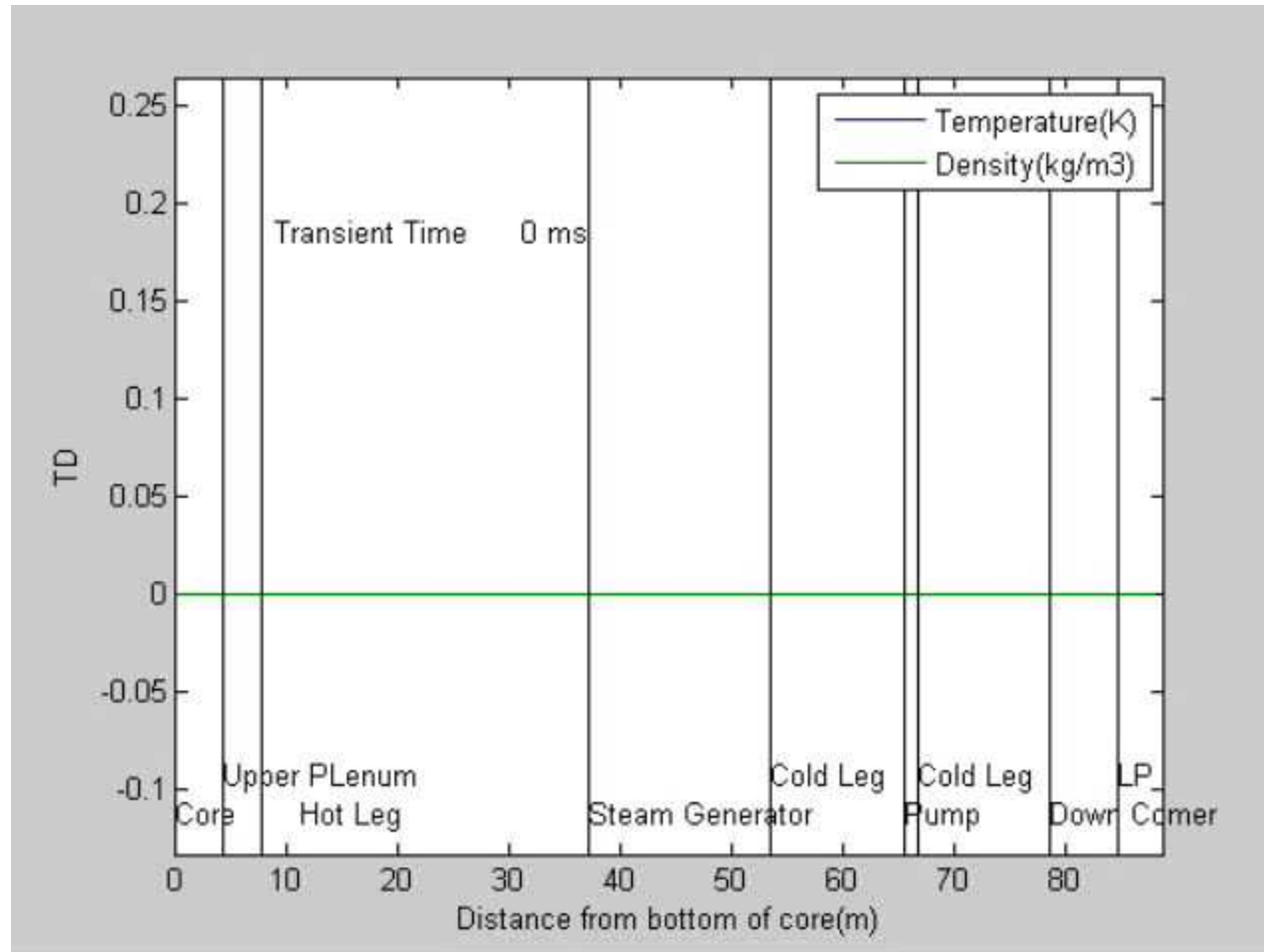
Pin Power

- Pin Power in Vicinity of Stuck Rod



OECD/NEA MSLB Benchmark:

- Temperature and Density Change in Primary Loop



OECD/NEA MSLB Benchmark:

- Pressure Change in Primary Loop

