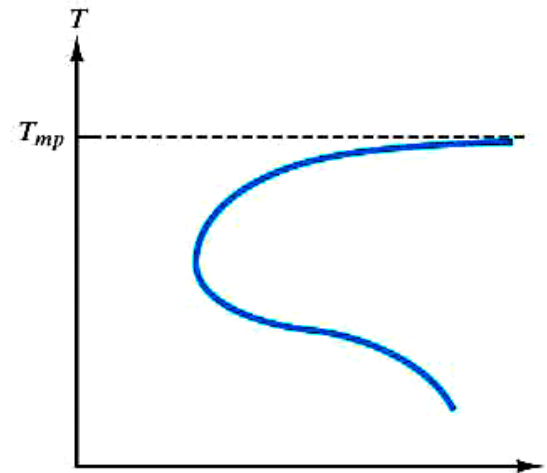
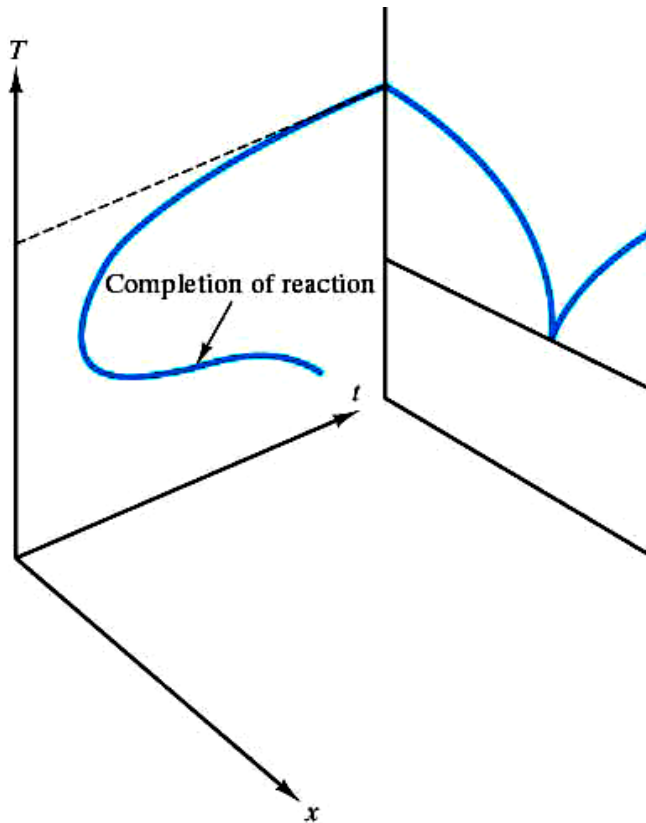


10. Phase Transformation

- phase transformation
thermodynamics, nucleation
interface, growth
- T-T-T curve
- martenstic transformation
- tempering

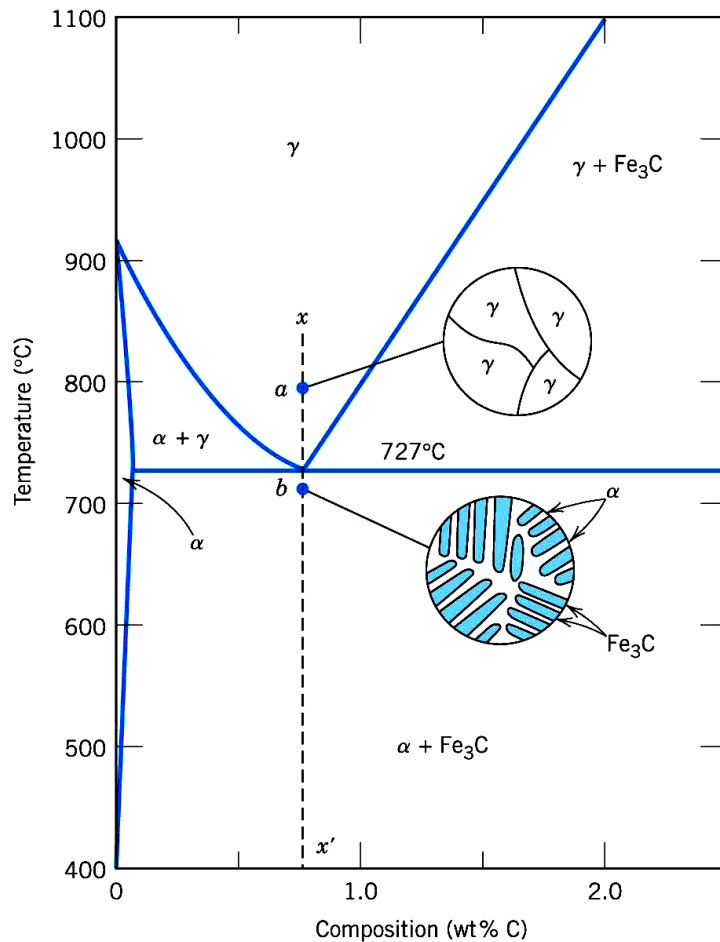
Fundamental Concepts

- ❑ phase diagram \leftarrow thermodynamic equilibrium
- ❑ real system \leftarrow non-equilibrium
- ❑ time \rightarrow kinetics
- ❑ phase transformation



Fundamental Concepts

- isothermal transformation– temperature–microstructure

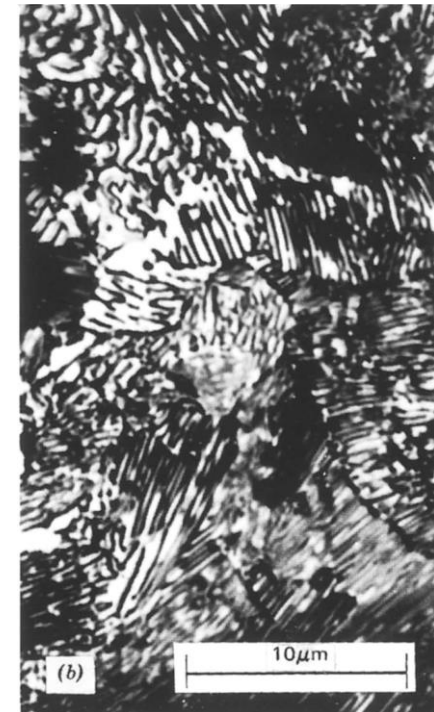


just below
eutectoid T



coarse
pearlite

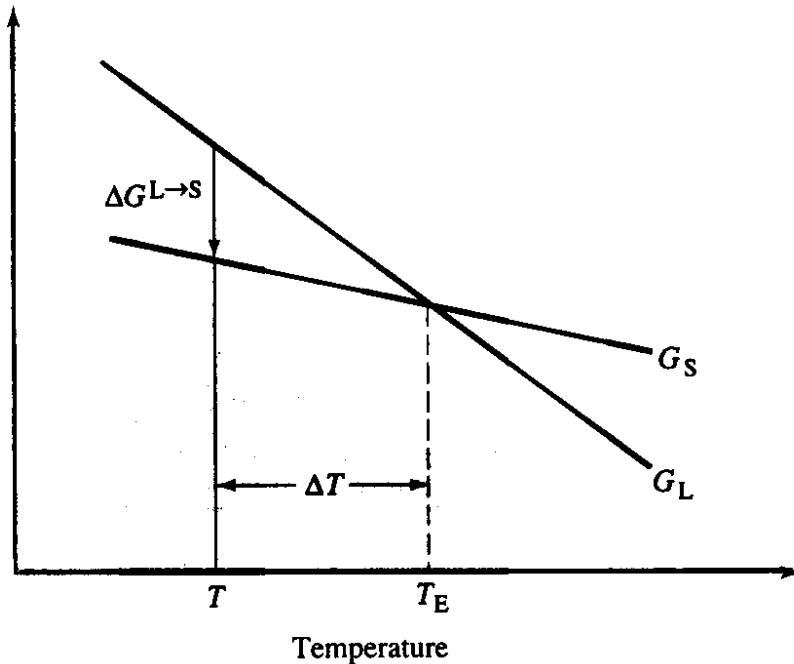
well below
eutectoid T



fine
pearlite

Phase Transformation

□ driving force: free energy change



$$\Delta G^{L \rightarrow S} = \Delta H^{L \rightarrow S} - T \Delta S^{L \rightarrow S}$$

$$(\Delta G^{L \rightarrow S} = G_S - G_L)$$

$$\text{at } T = T_E, \Delta G^{L \rightarrow S} = 0$$

$$\Delta S^{L \rightarrow S} = \frac{\Delta H^{L \rightarrow S}}{T_E}$$

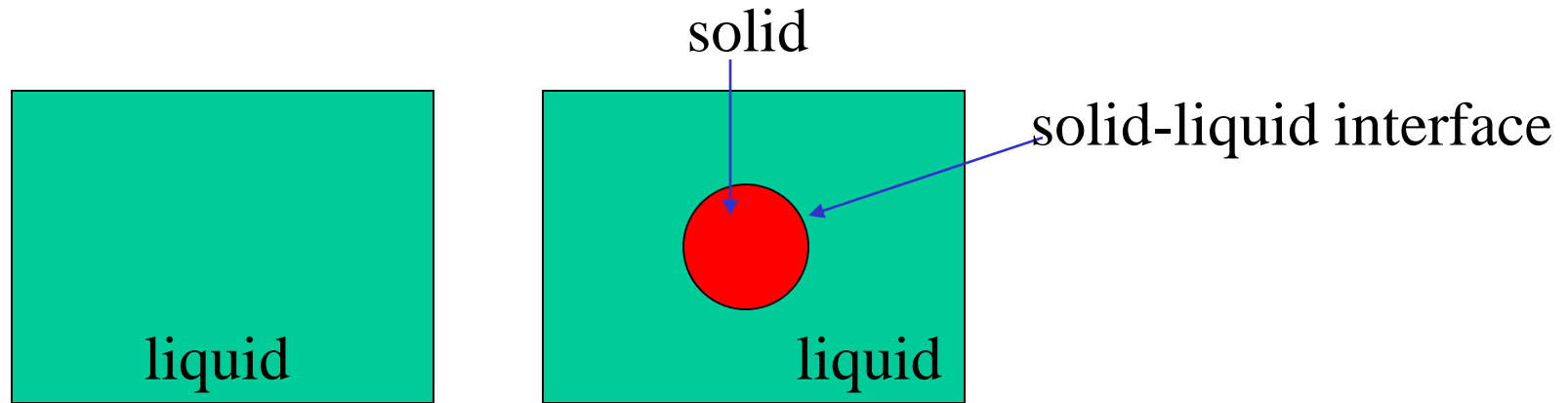
$$\Delta G^{L \rightarrow S} = \frac{\Delta H^{L \rightarrow S}}{T_E} \Delta T (= T_E - T)$$

For solidification, $\Delta H^{L \rightarrow S} < 0$ (exothermic)

$T < T_E$, $\Delta T > 0$, $\Delta G^{L \rightarrow S} < 0$ thermodynamically favorable

Phase Transformation

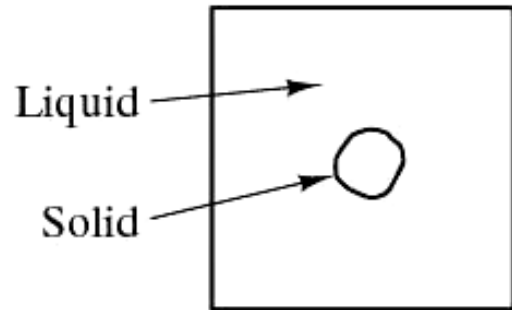
- opposing force: phase boundary



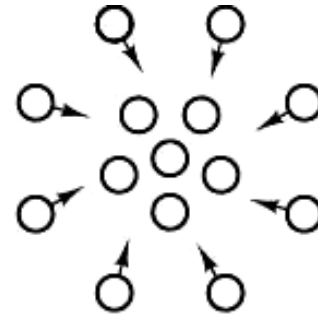
- phase boundary– a few atoms thick– 2-D defect
additional energy– interfacial energy
- undercooling → energy available to create the phase boundary

Phase Transformation

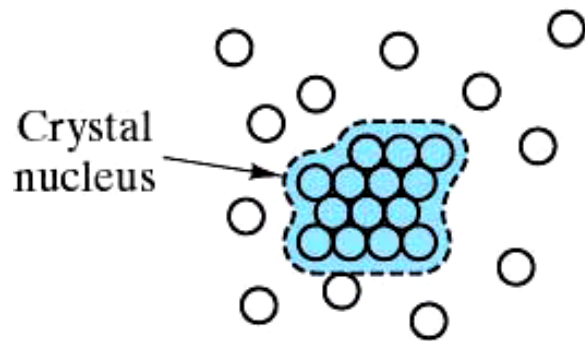
- ❑ nucleation: homogeneous or heterogeneous
- ❑ growth



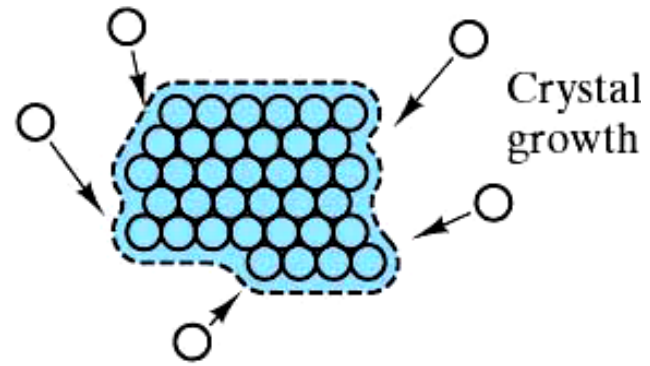
(a)



(b)

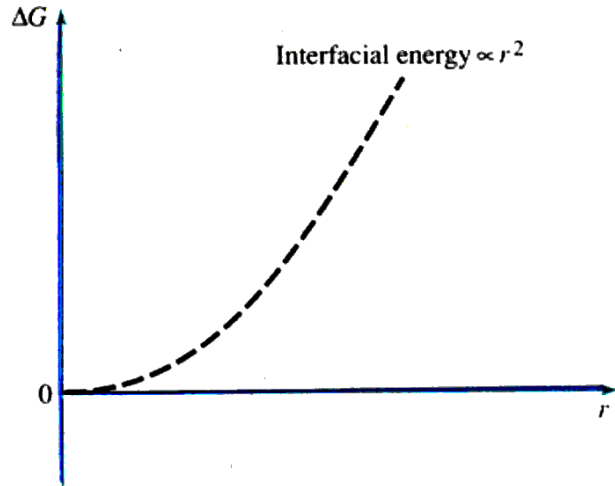


(c)

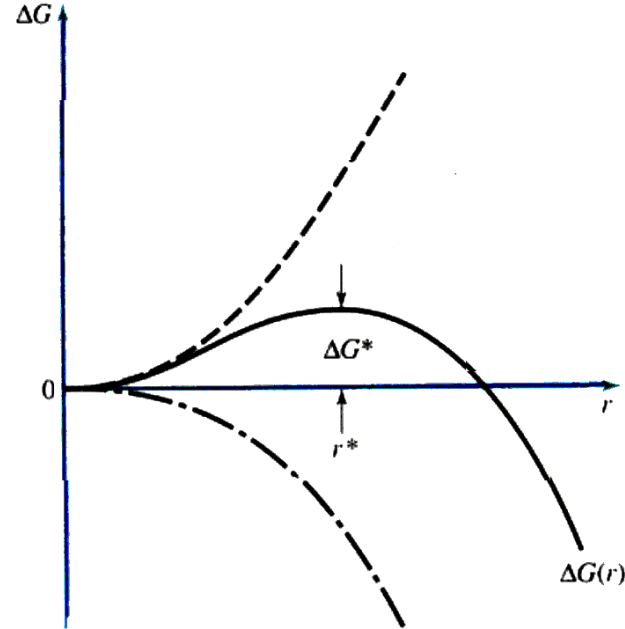


(d)

Homogeneous Nucleation

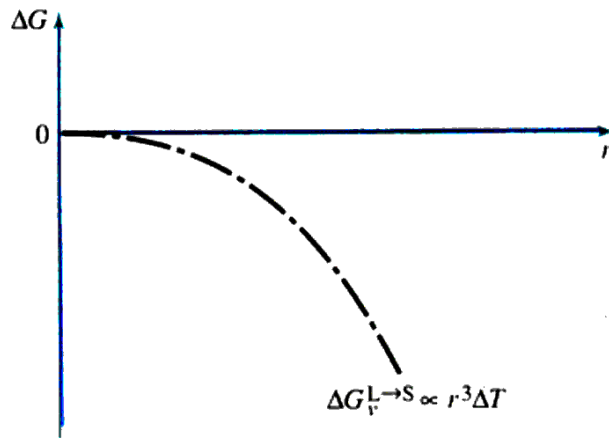


(a)

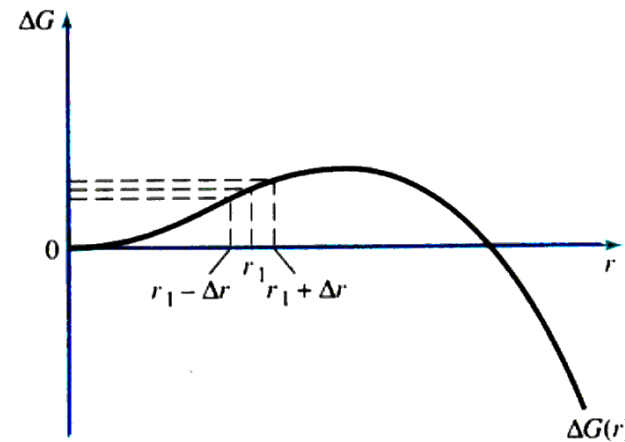


(c)

Assumption
 -isotropic interface energy
 -independent of size
 -spherical nucleus



(b)



(d)

Homogeneous Nucleation

- change in free energy as a function of r

$$\Delta G(r) = \left(\frac{4}{3}\pi r^3\right)\Delta G_V + (4\pi r^2)\gamma_{SL}$$

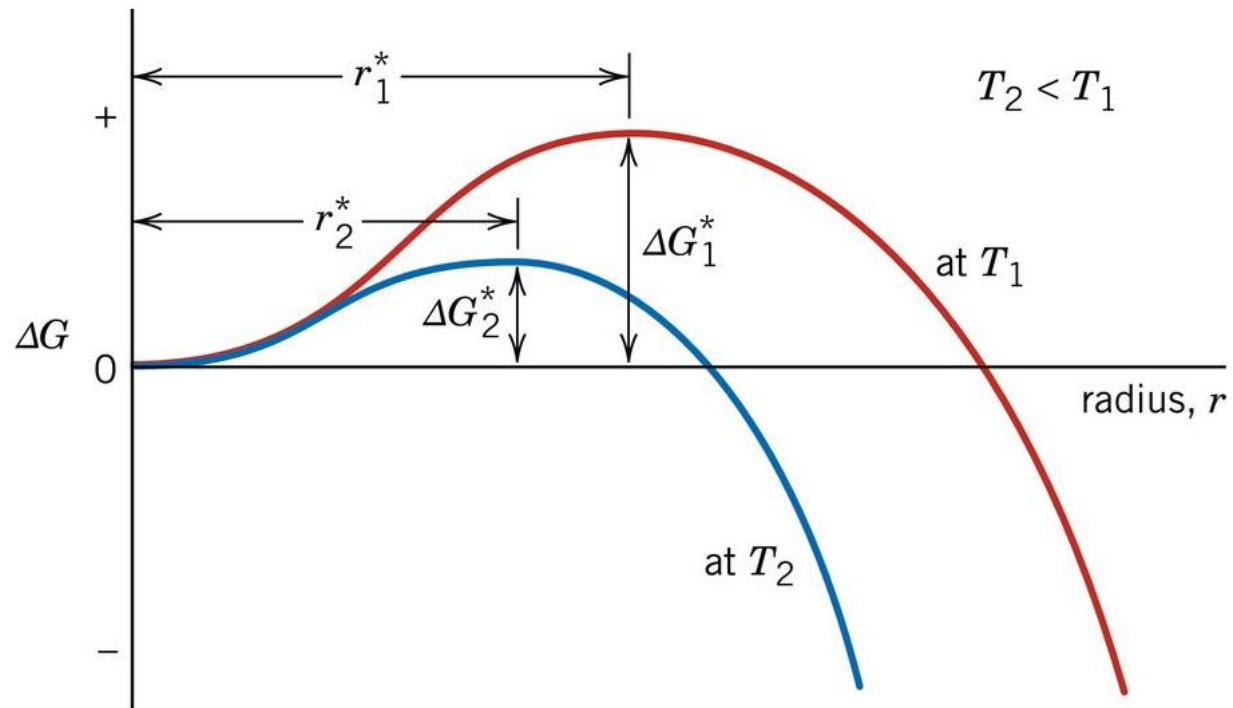
- critical radius r^*

$$\frac{d[\Delta G(r)]}{dr} = 0 = 4\pi r^2\Delta G_V + 8\pi r\gamma_{SL}$$

$$r^* = \frac{-2r_{SL}}{\Delta G_V} = \frac{-2\gamma_{SL}T_E}{\Delta H_V\Delta T} \quad (r^* \text{ decreases as undercooling increases})$$

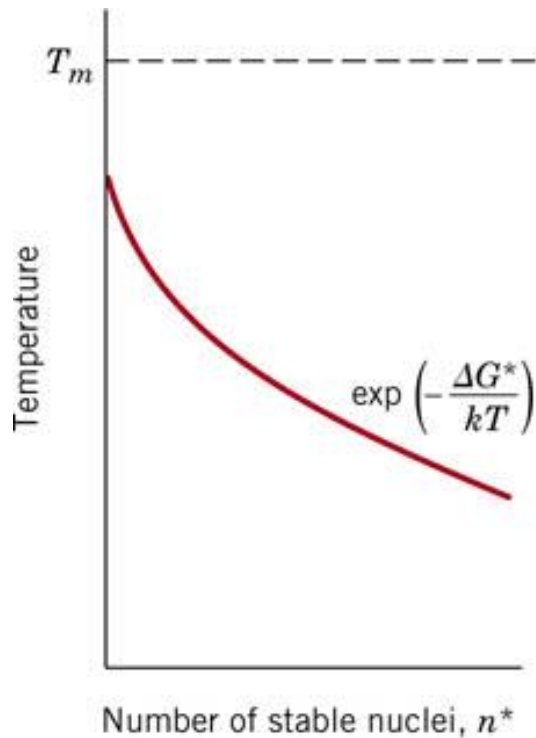
$$\Delta G^* = \frac{16\pi\gamma_{SL}^3T_E^2}{3\Delta H_V^2} \frac{1}{\Delta T^2} \quad (\text{energy barrier decreases as undercooling increases})$$

Homogeneous Nucleation

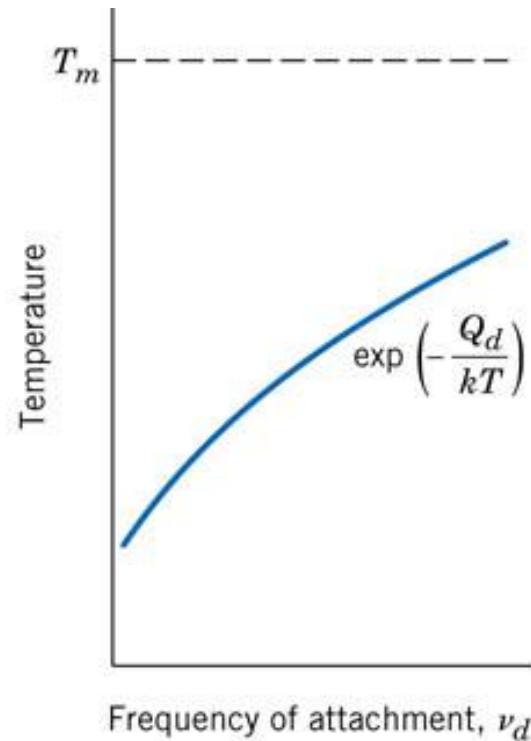


Homogeneous Nucleation

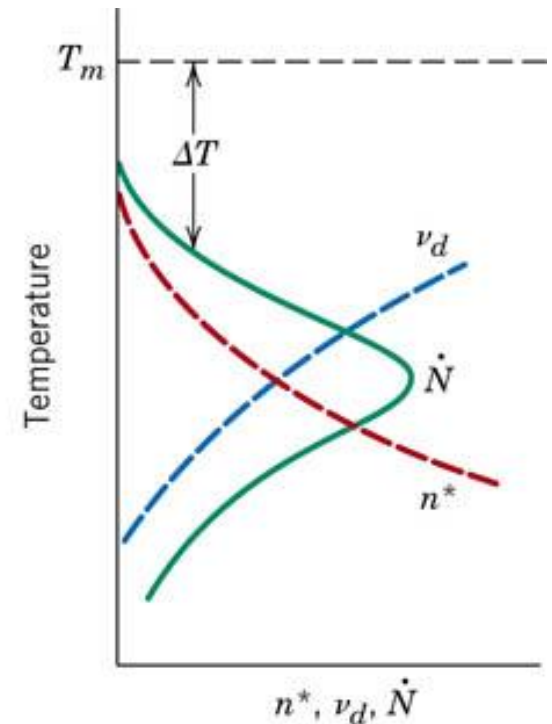
- for nucleation, atomic mobility should be considered in addition to nucleation barrier term



(a)



(b)

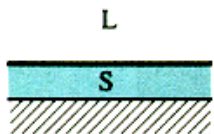
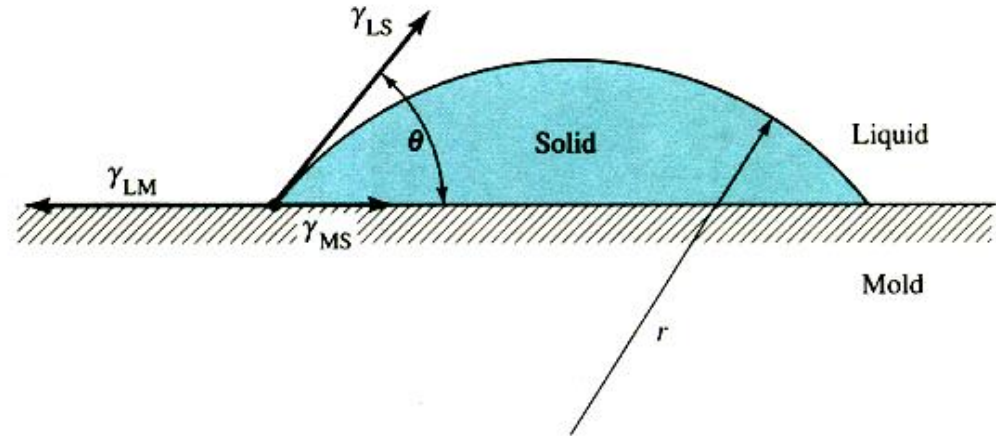


(c)

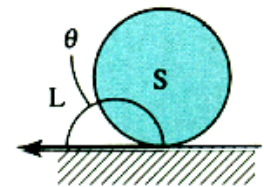
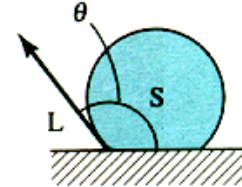
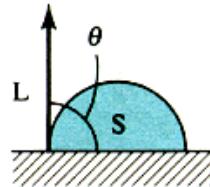
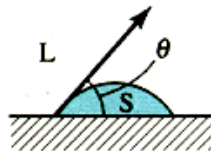
Heterogeneous Nucleation

$$\gamma_{LM} = \gamma_{MS} + \gamma_{LS} \cos \theta$$

θ : contact angle



Complete wetting.
No barrier to nucleation.



No wetting.
Nucleation indistinguishable from homogeneous nucleation.



$\theta = 0$
 $f(\theta) = 0$

$\pi/4$
0.058

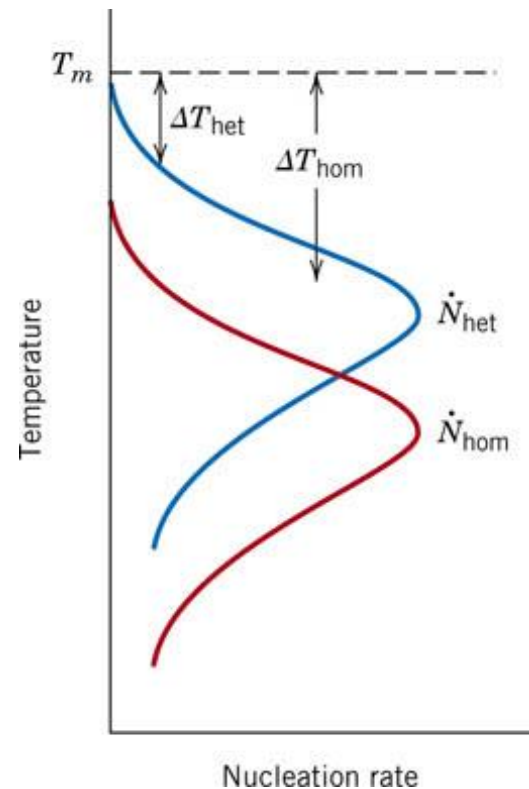
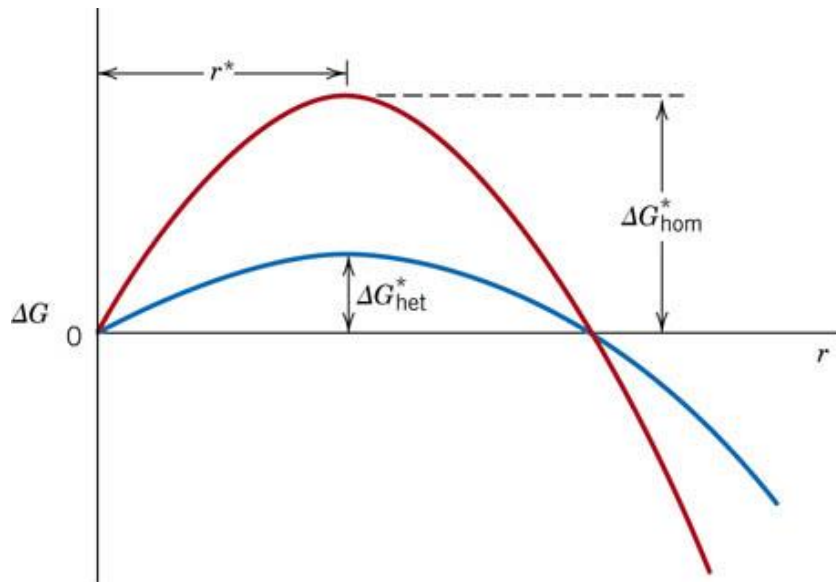
$\pi/2$
0.500

$3\pi/4$
0.943

π
1.000

Heterogeneous Nucleation

- $\Delta G_{het}^* \propto \Delta G_{hom}^* f(\theta)$, $0 < f(\theta) < 1$
- energy barrier for heterogeneous nucleation is **always lower** than that for homogeneous nucleation



Heterogeneous Nucleation



cast aluminum alloy

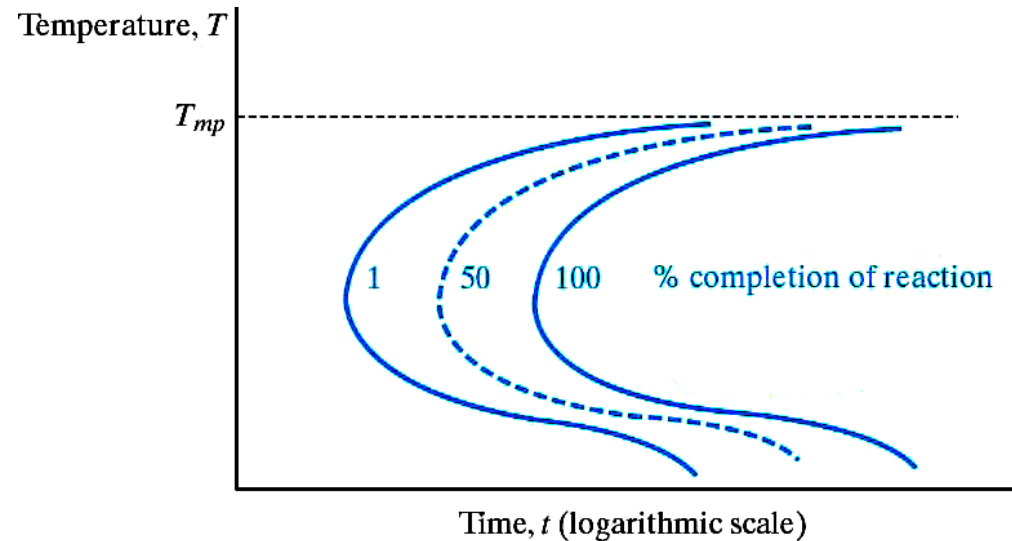
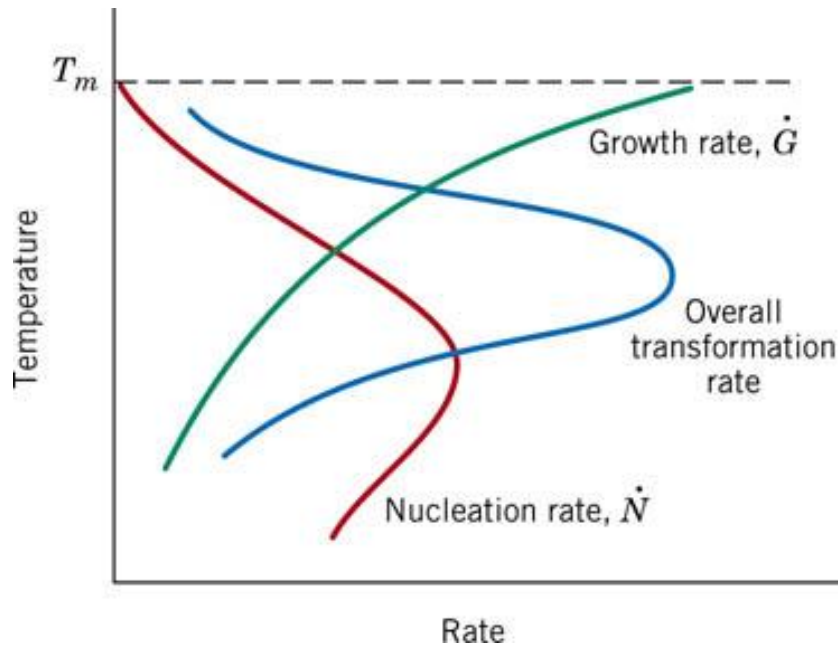
grain refiner (TiB₂)

Growth

- growth process is diffusional in nature

$$\dot{G} = Ce^{-Q/RT}$$

- overall transformation rate

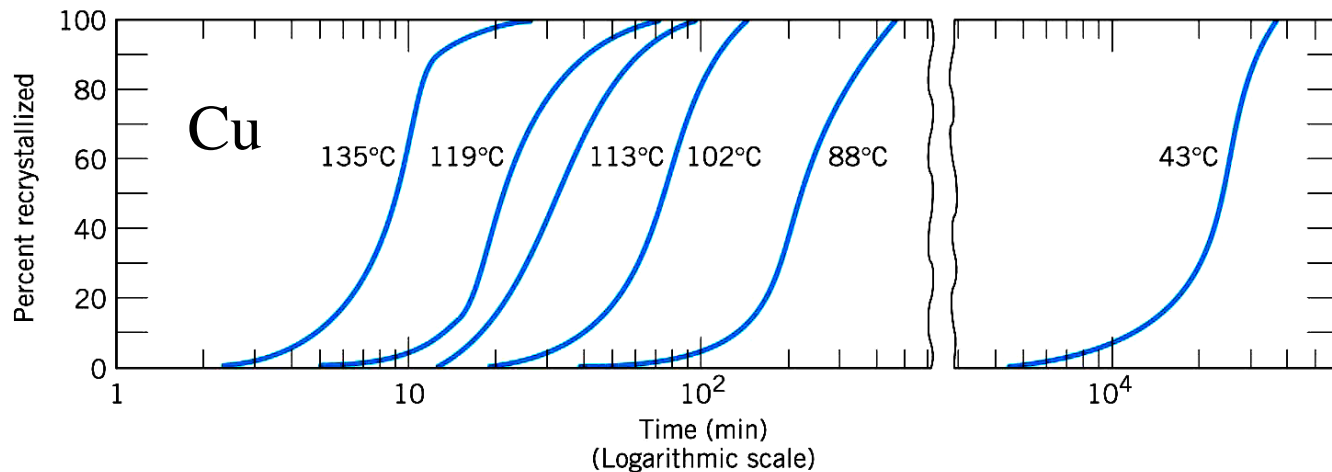
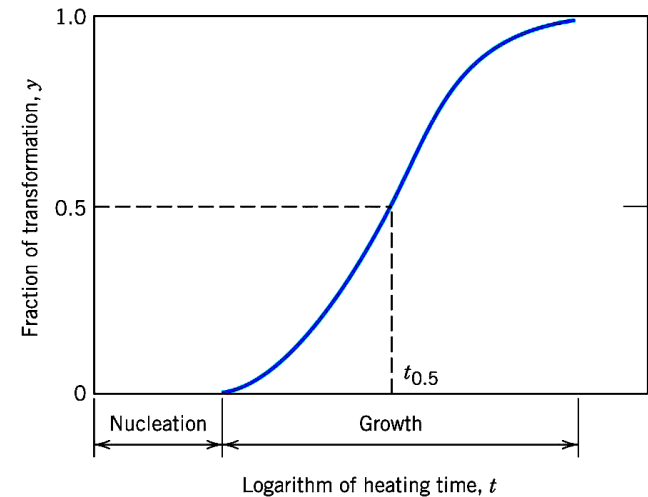
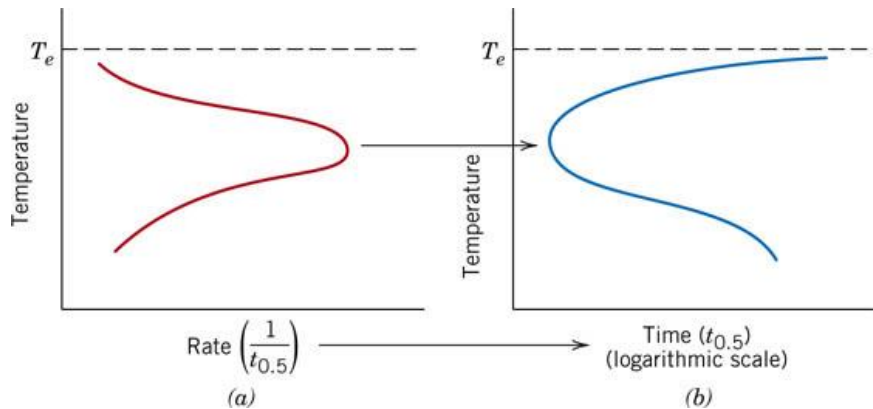


TTT diagram

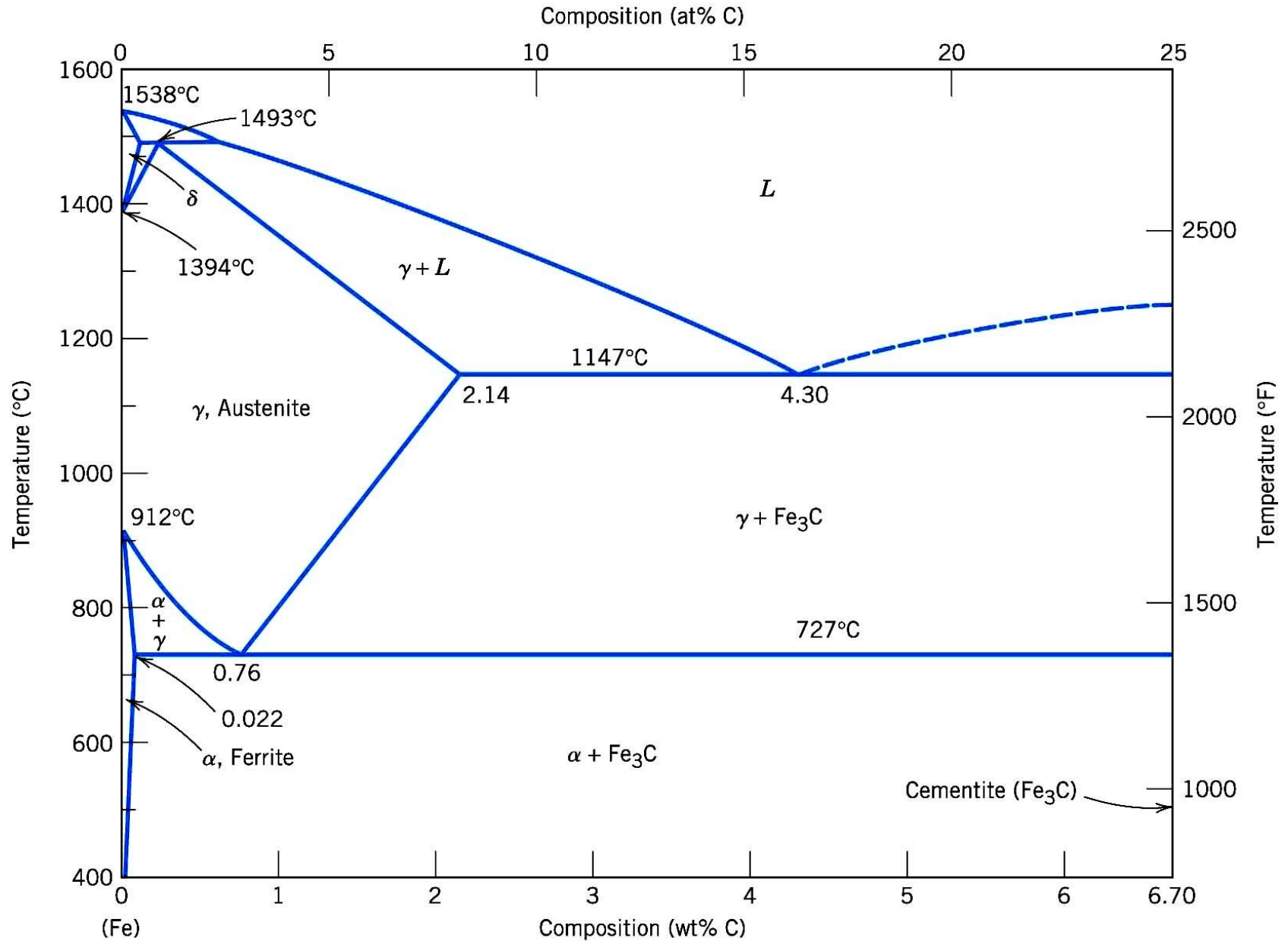
Phase Transformation

fraction of transformation

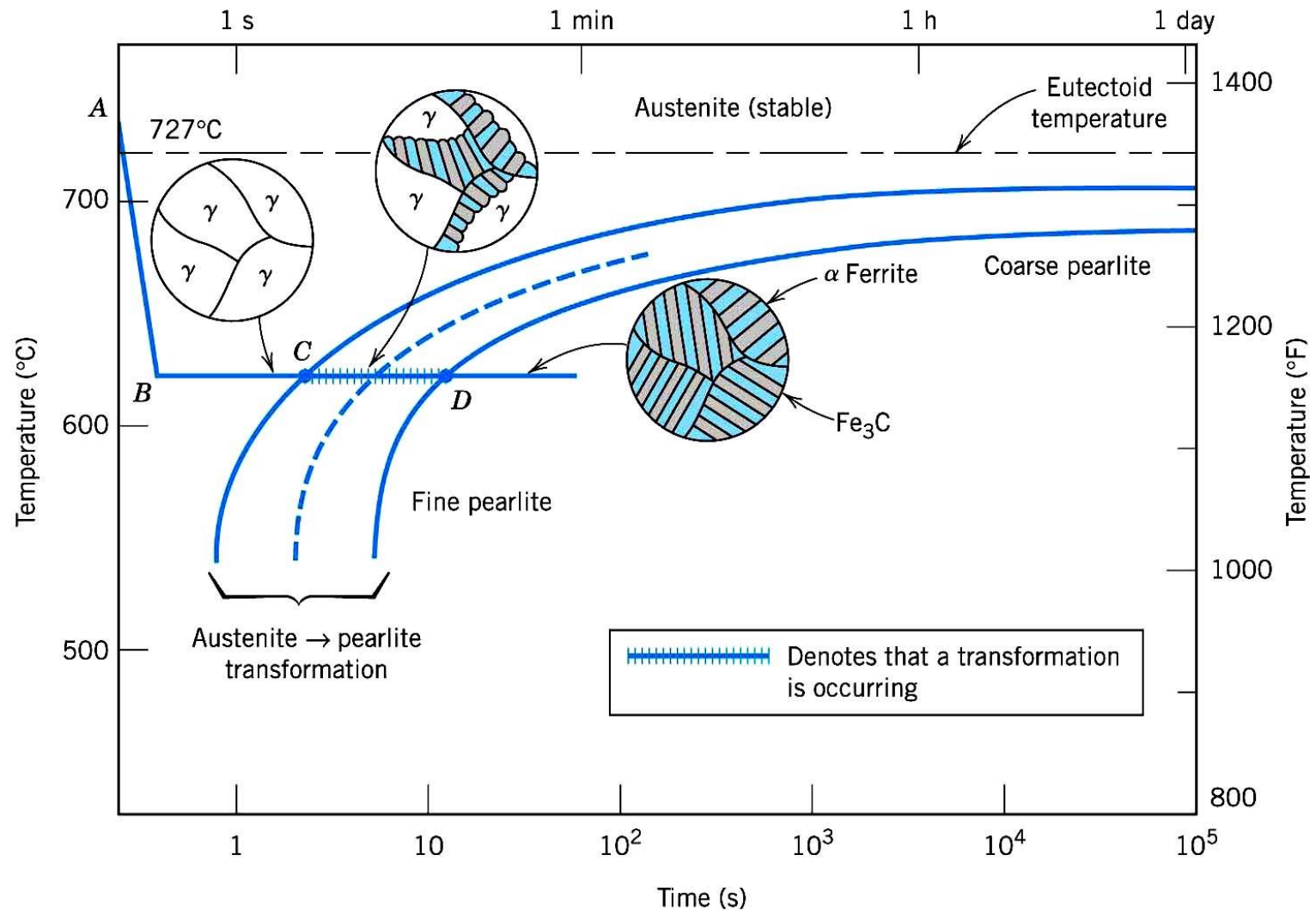
$$y = 1 - \exp(-kt^n)$$



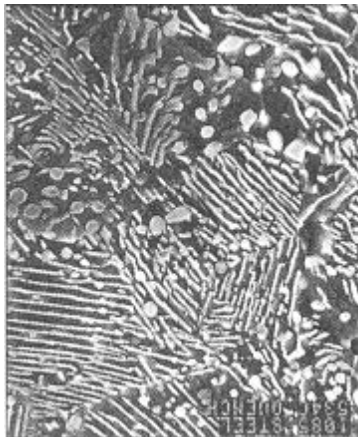
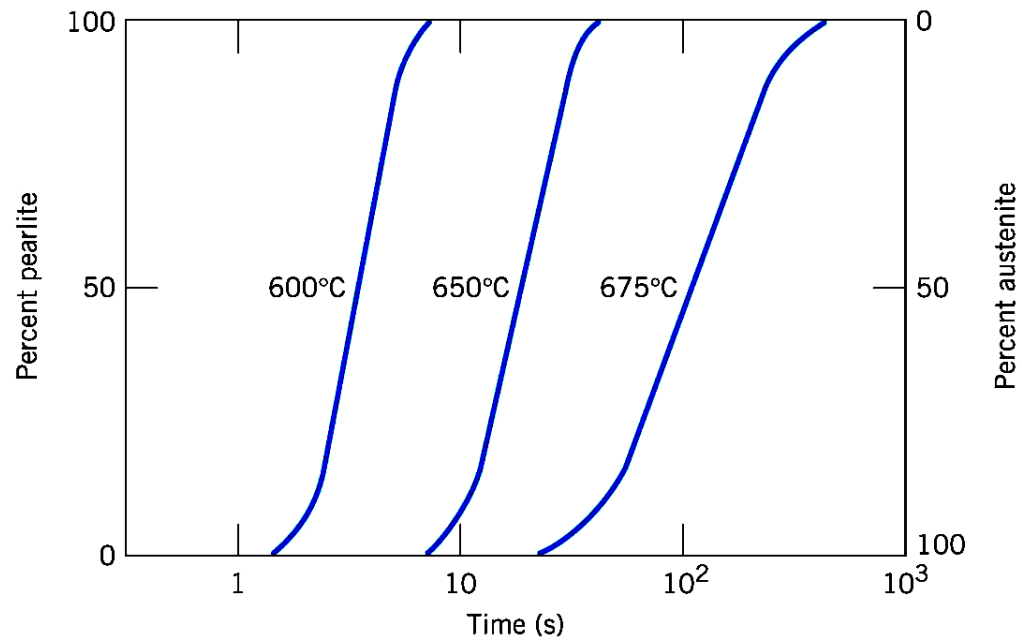
Fe-Fe₃C System



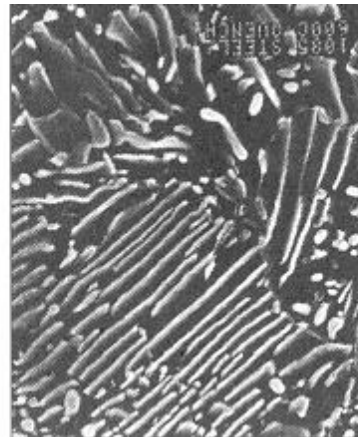
Isothermal Transformation Diagram



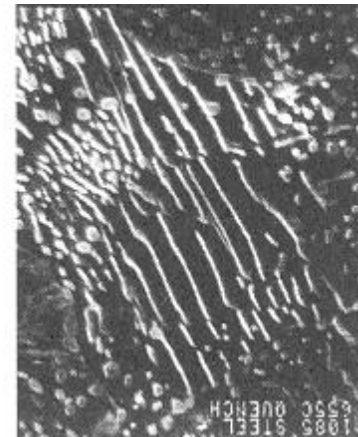
Eutectoid Steel



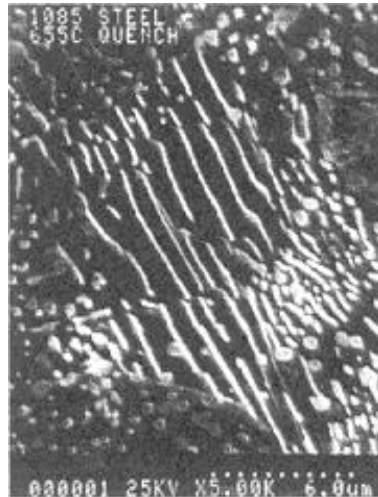
534°C



600°C



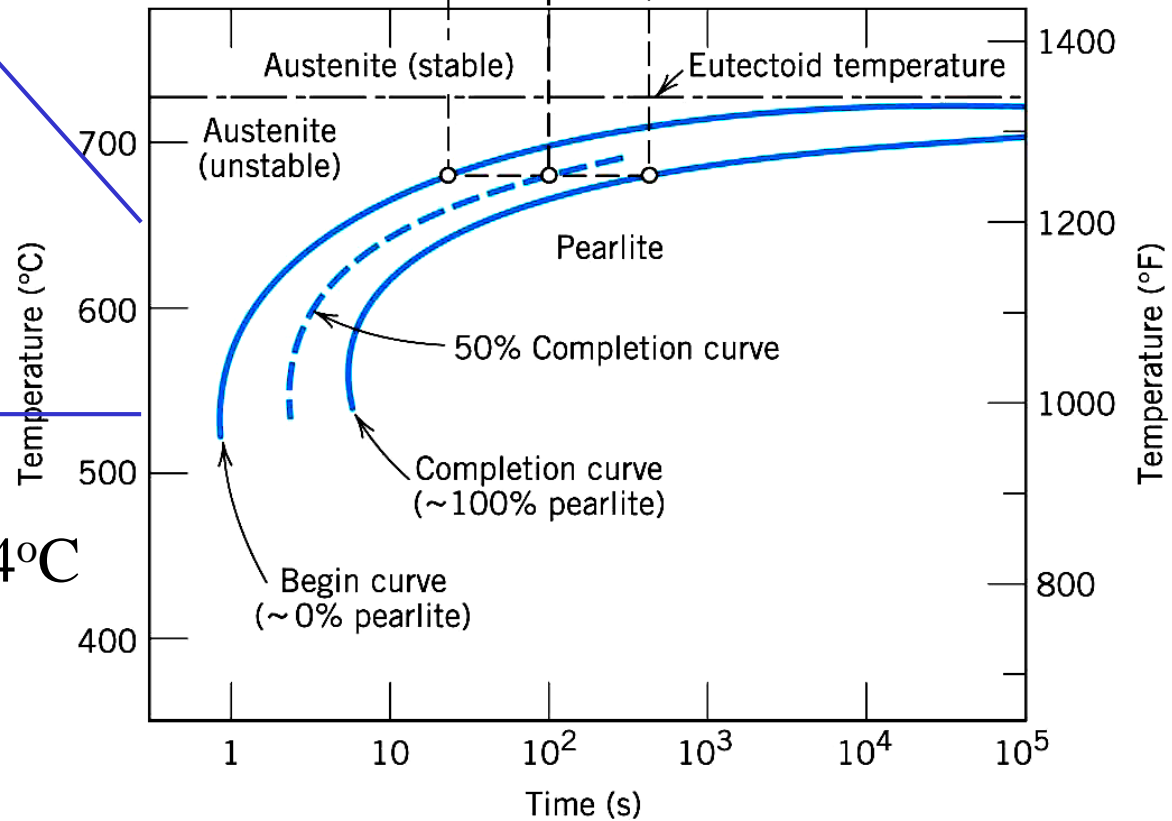
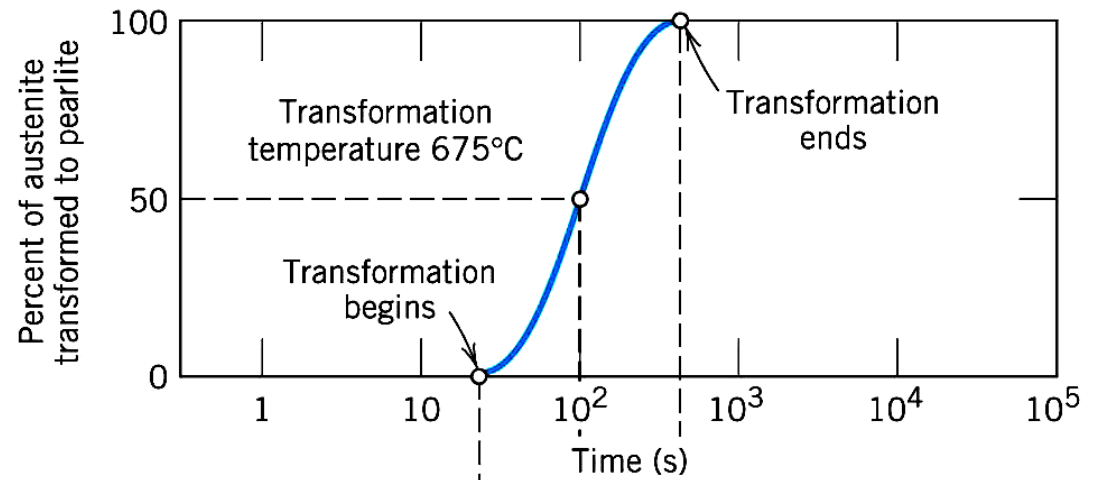
655°C

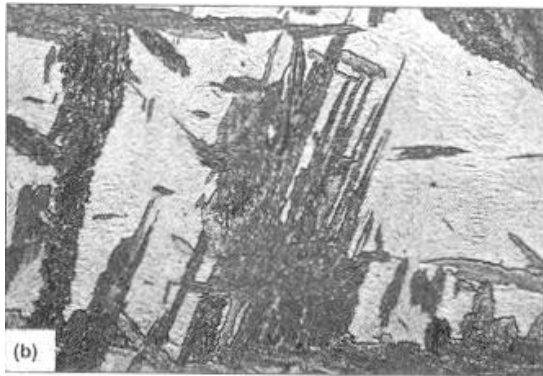
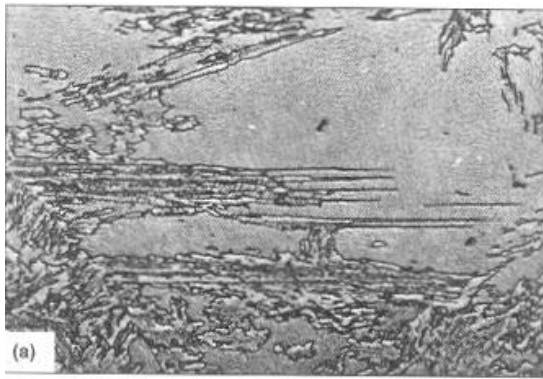


655°C

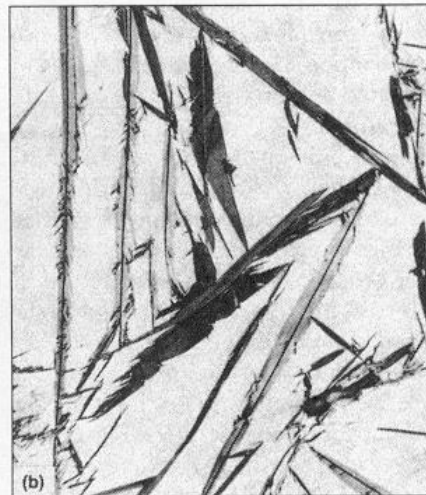
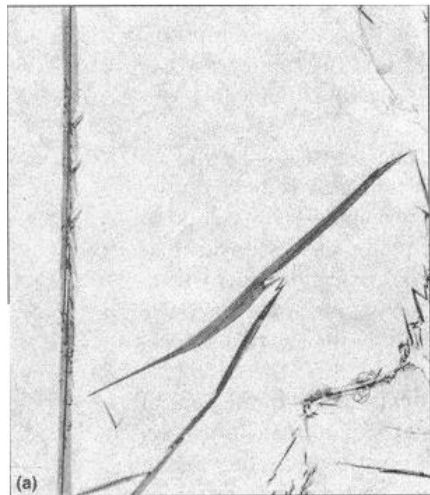
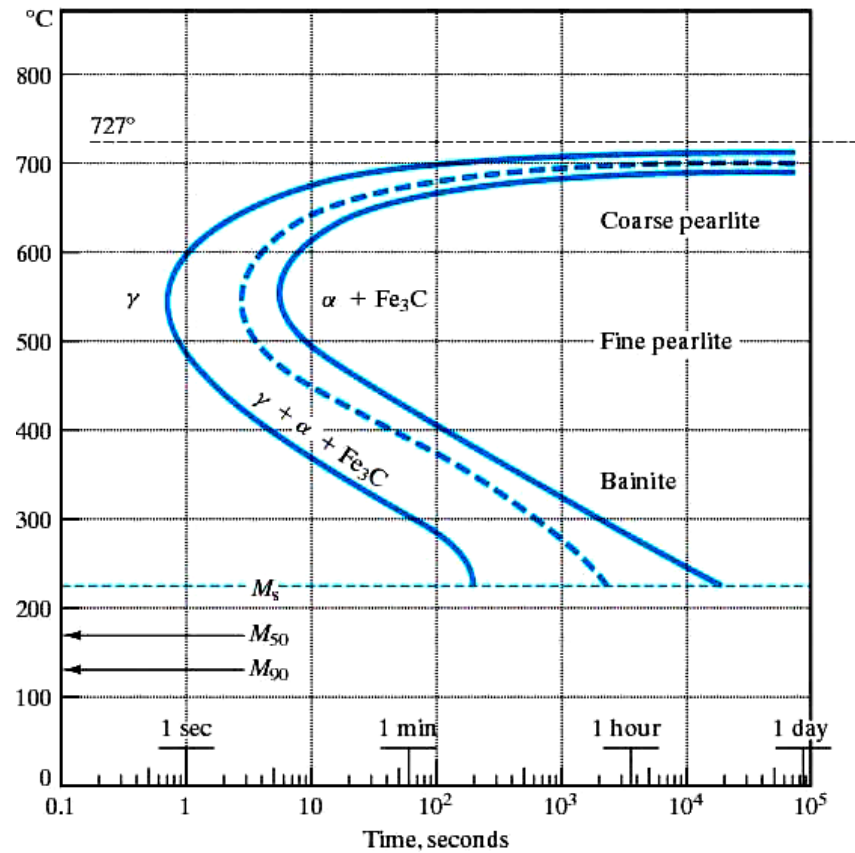


534°C





bainite

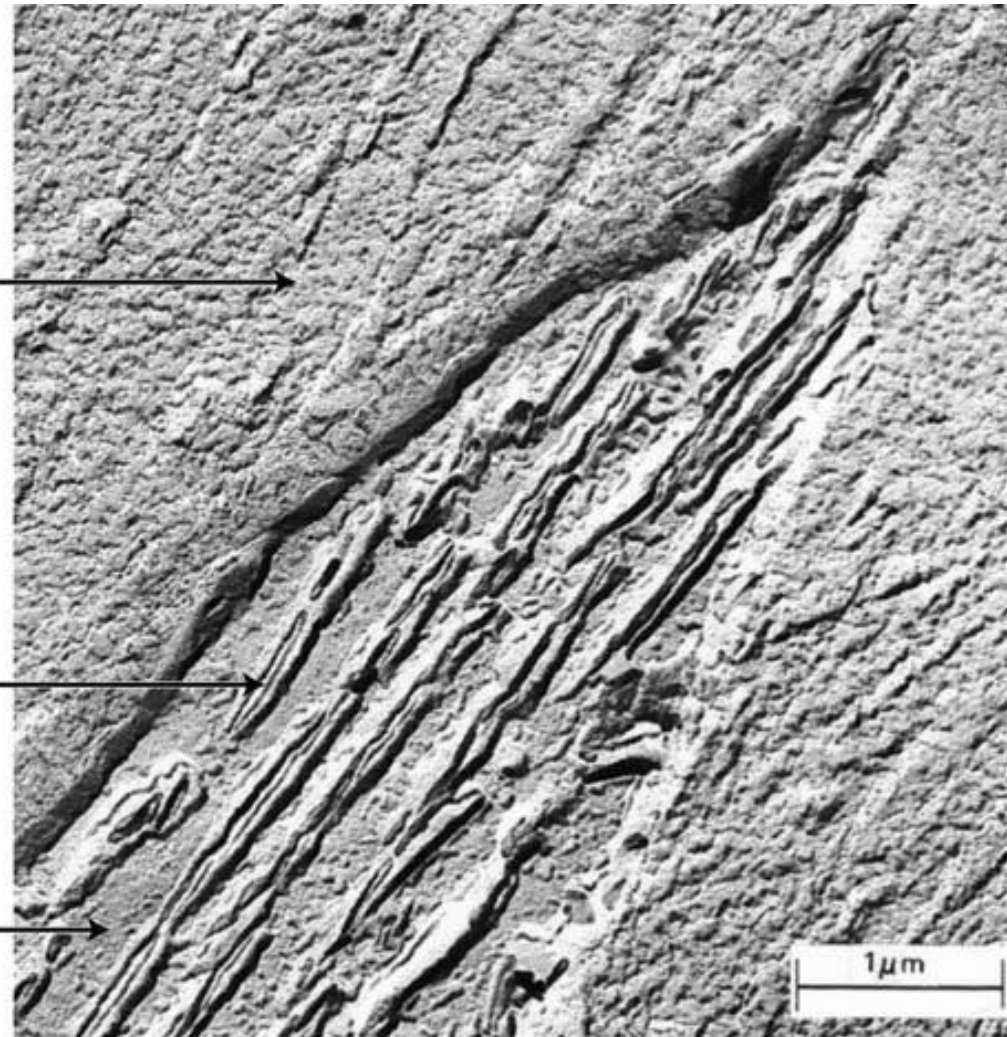


martensite
habit plane
habit direction

Martensite

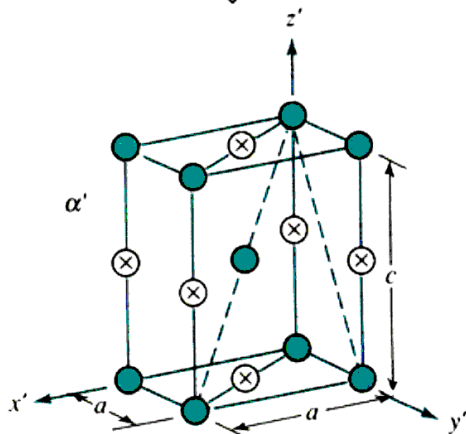
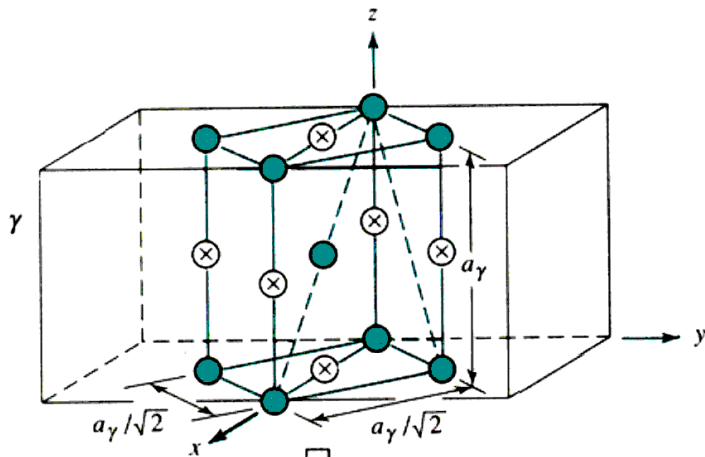
Cementite

Ferrite

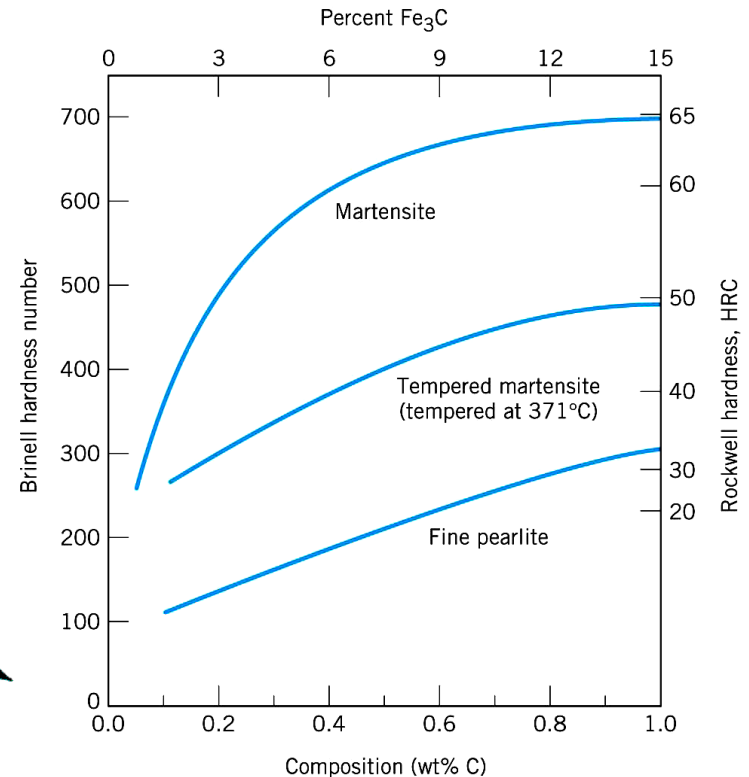
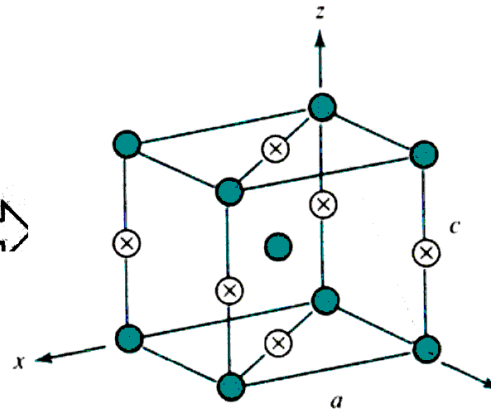


Martensitic Transformation

- FCC \rightarrow BCT
- bain distortion
 - c contracts by 20%, a expands by 12%
 - volume increases, internal stress
 - cracking
- rotation

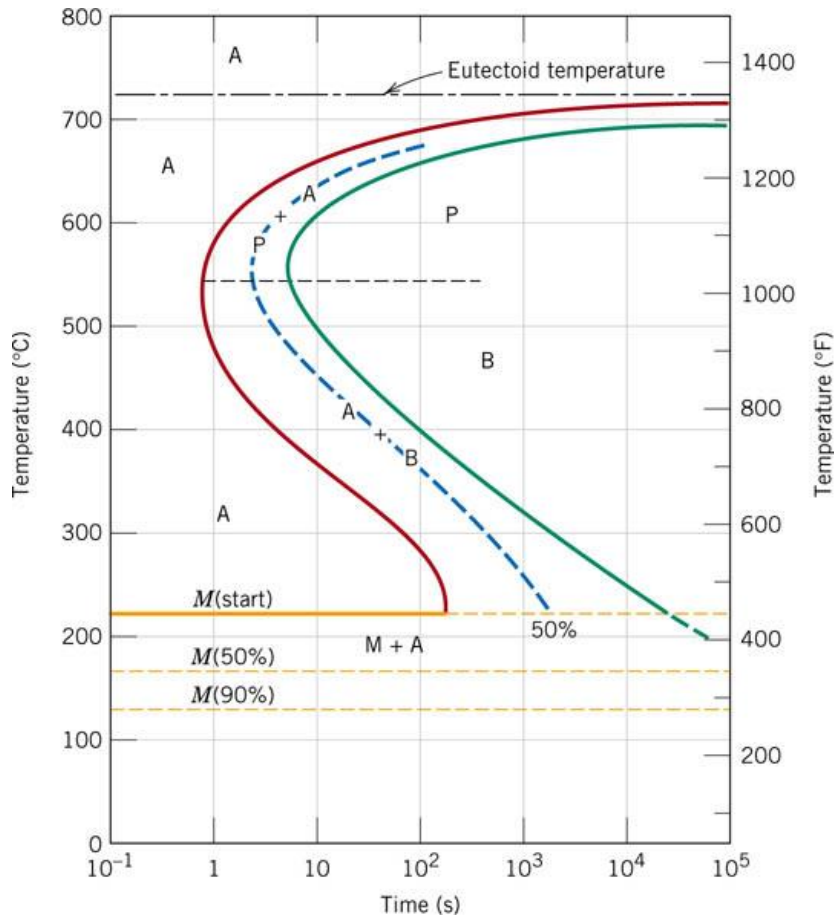


$$c/a \approx 1.4$$

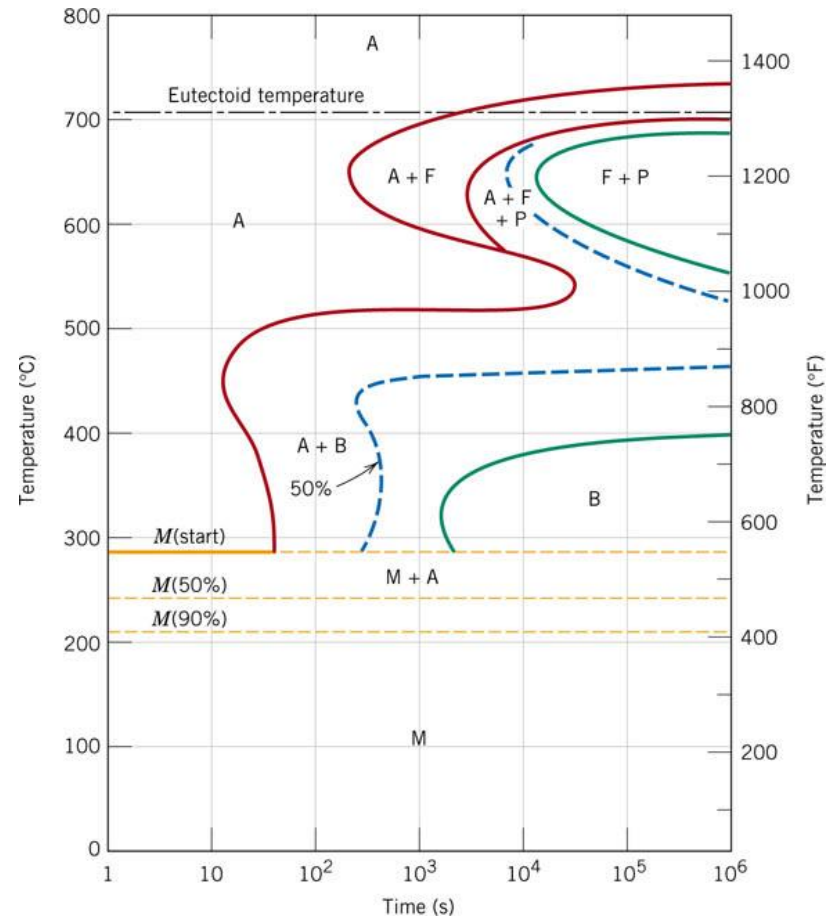


Effect of Alloying Elements

Cr, Ni, Mo, W

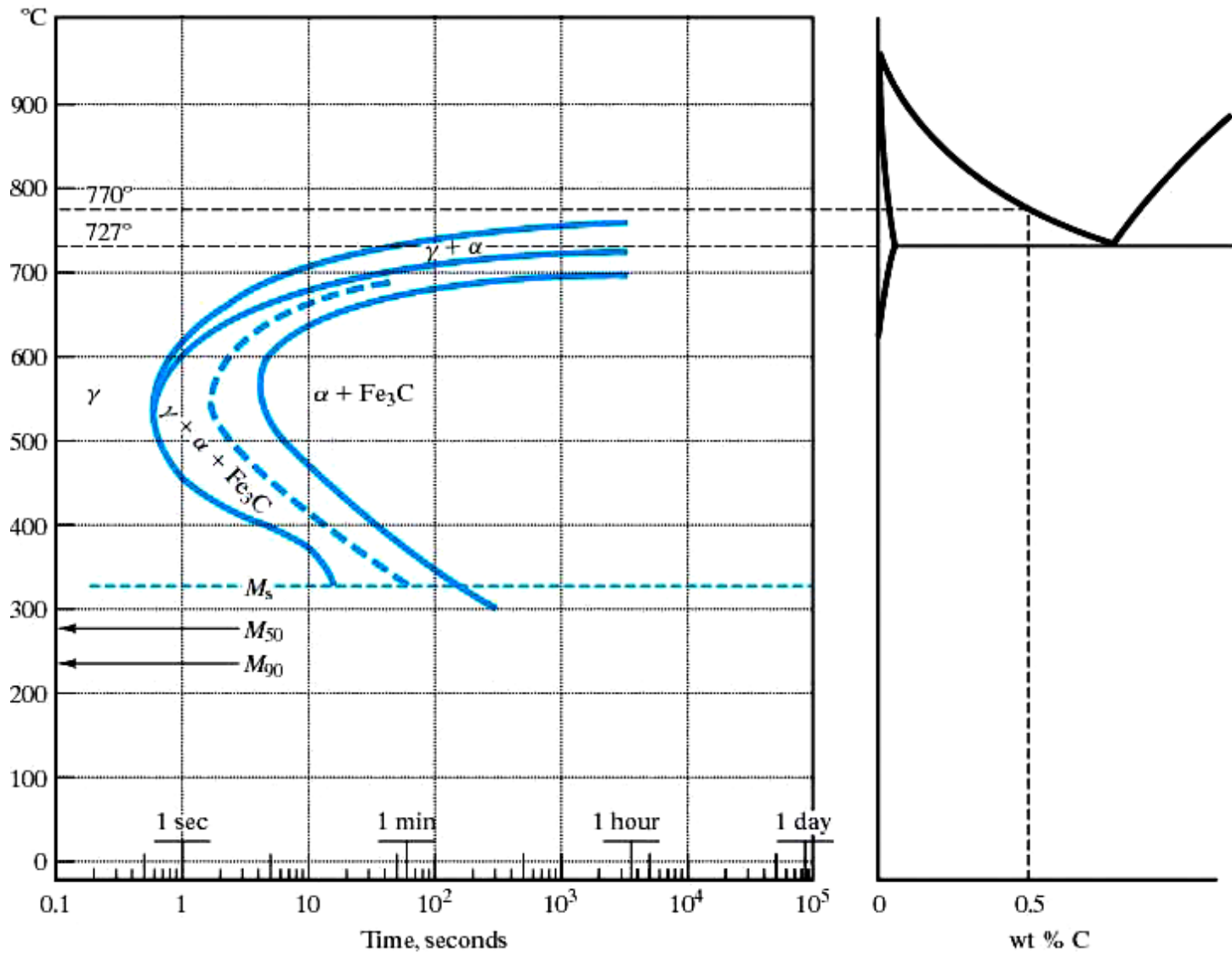


plain carbon steel

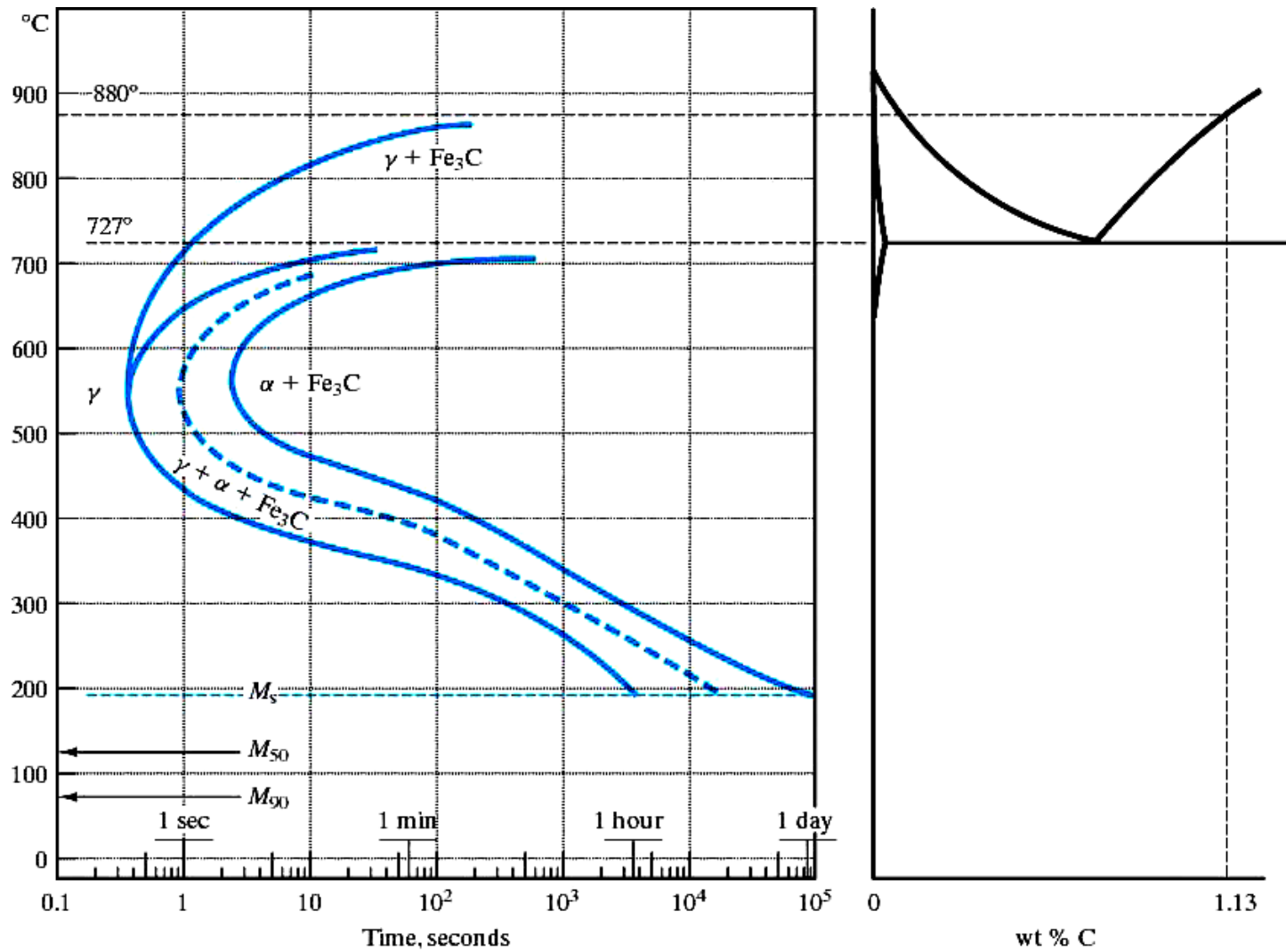


4340 alloy steel

Hypoeutectoid

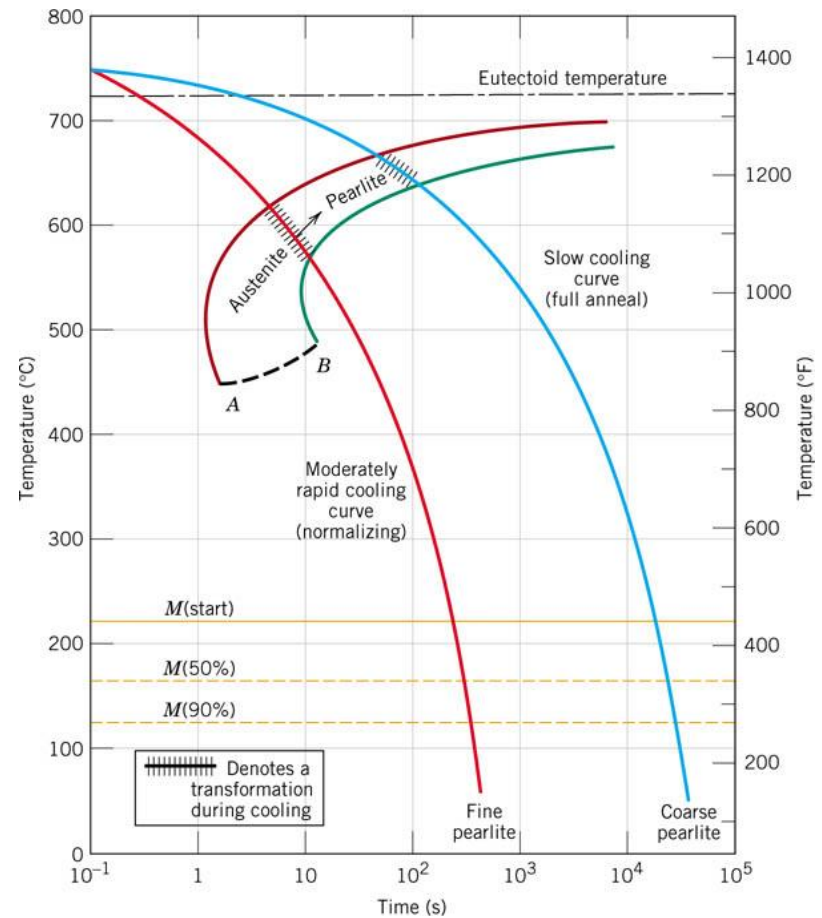
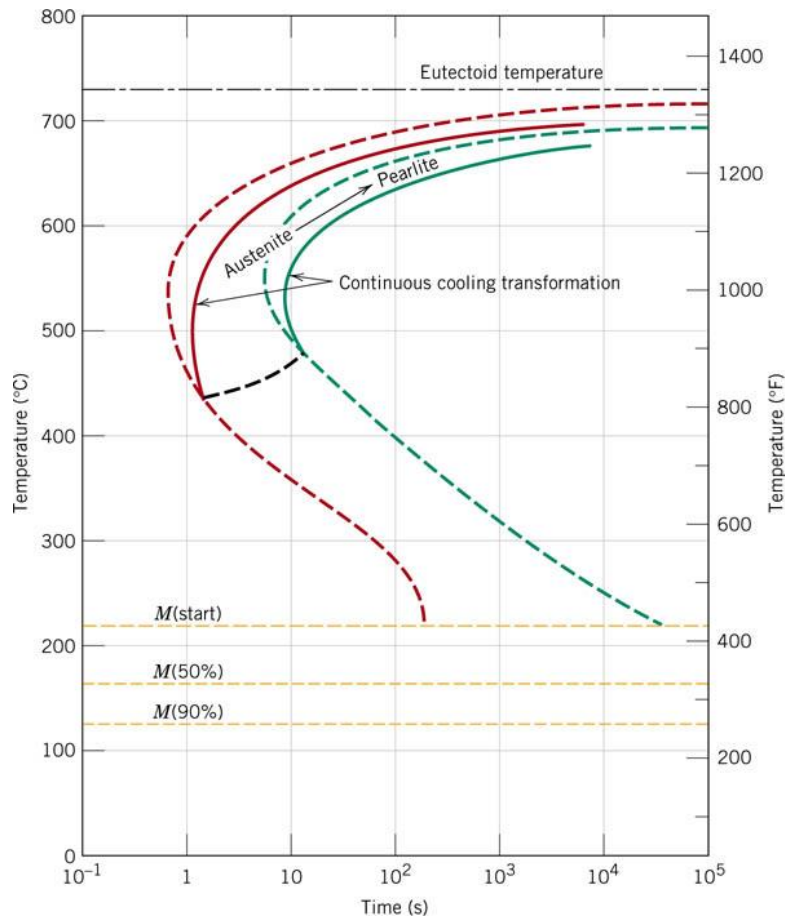


Hypereutectoid

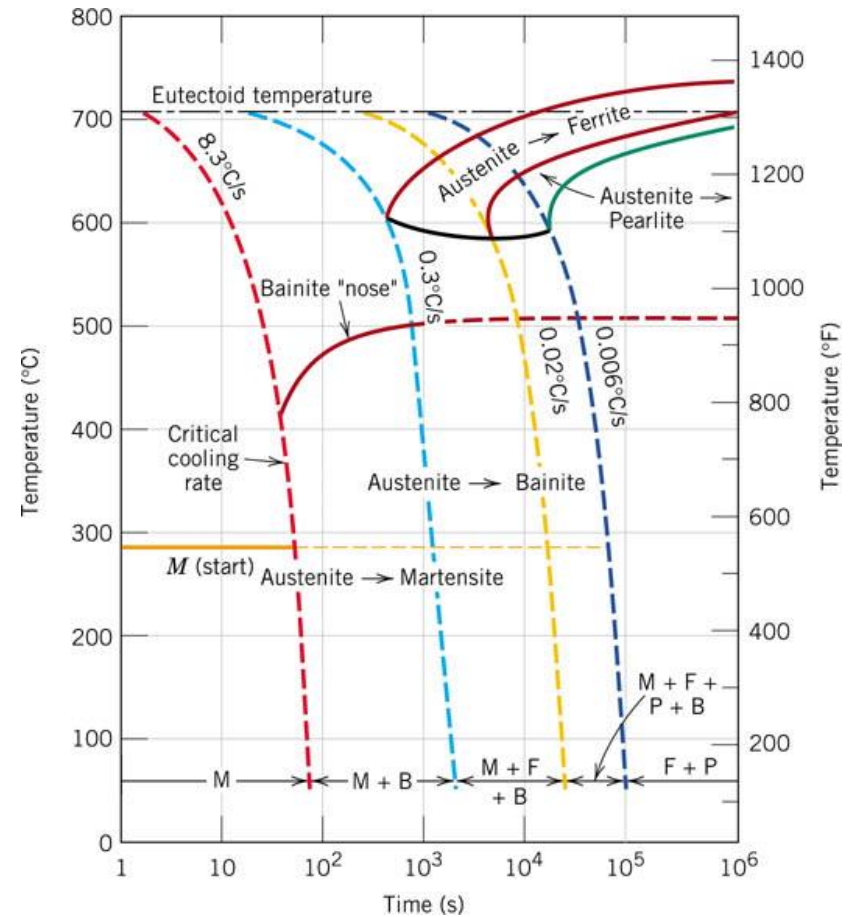
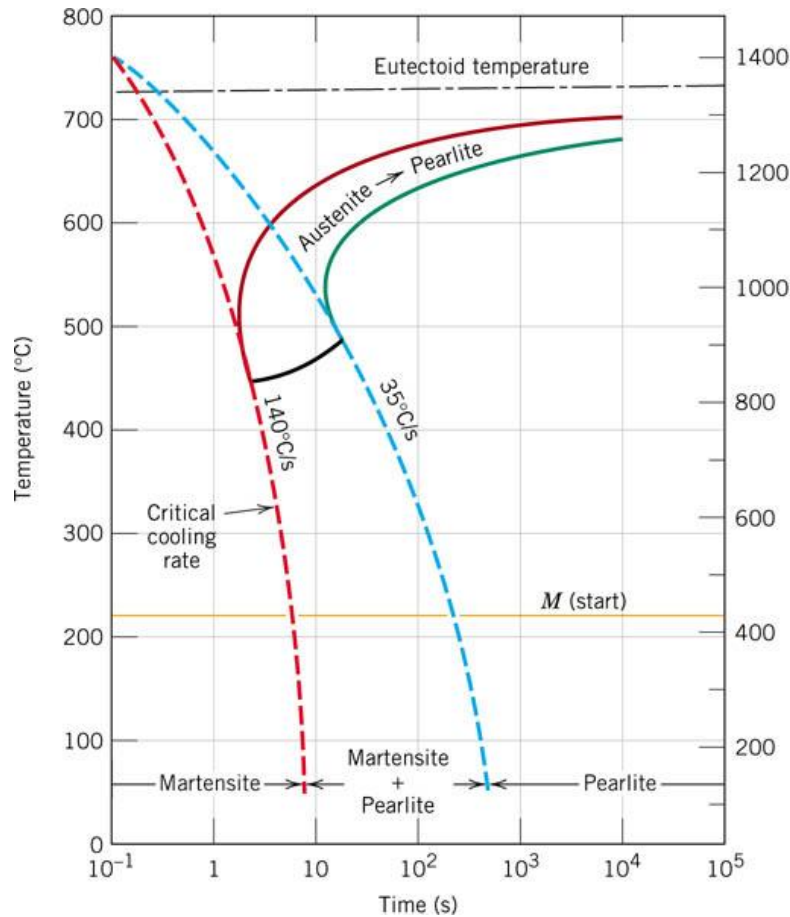


Continuous Cooling Transformation

- to shift transformation curve downward and toward the right



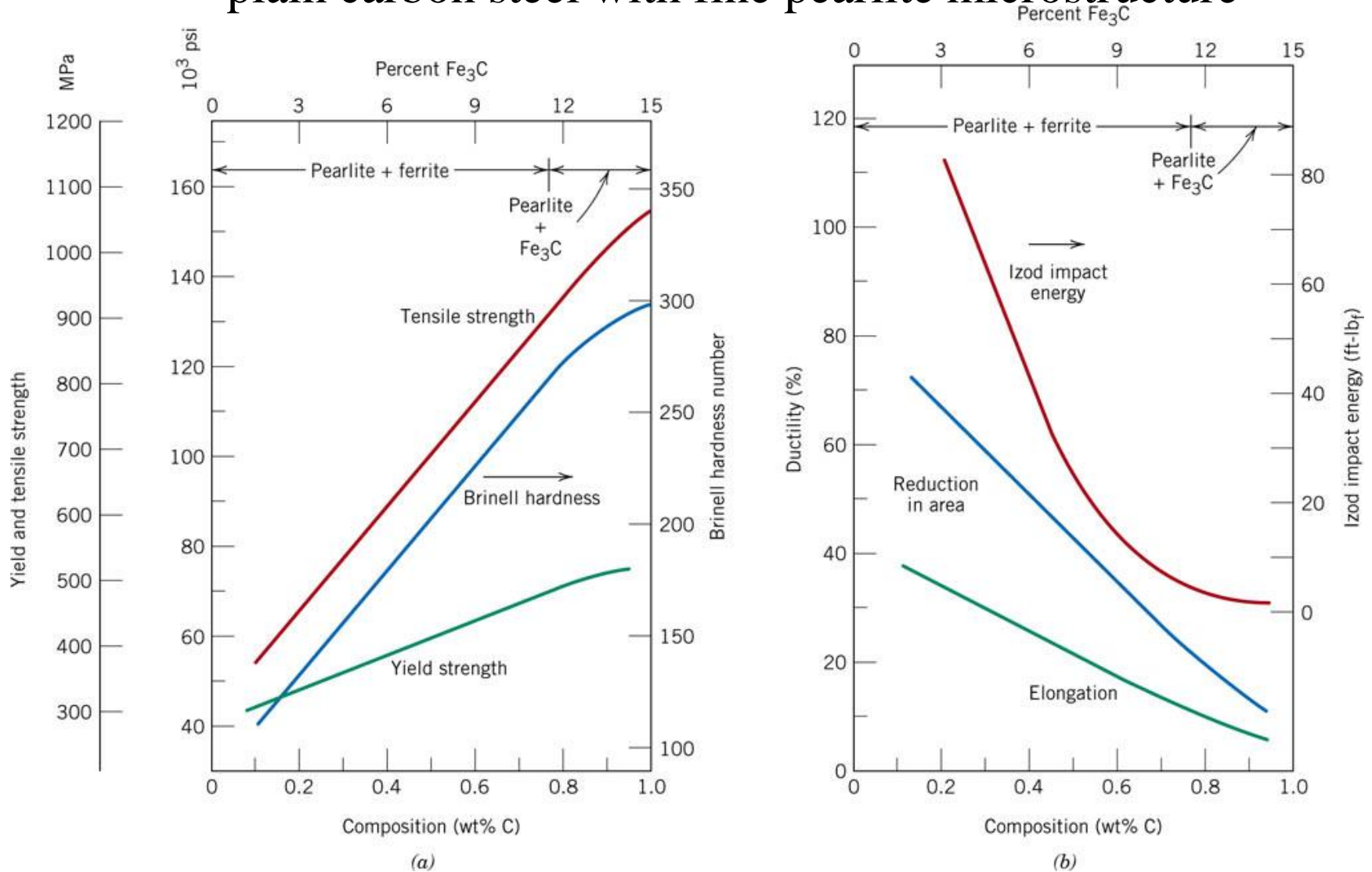
Continuous Cooling Transformation



4340 alloy steel

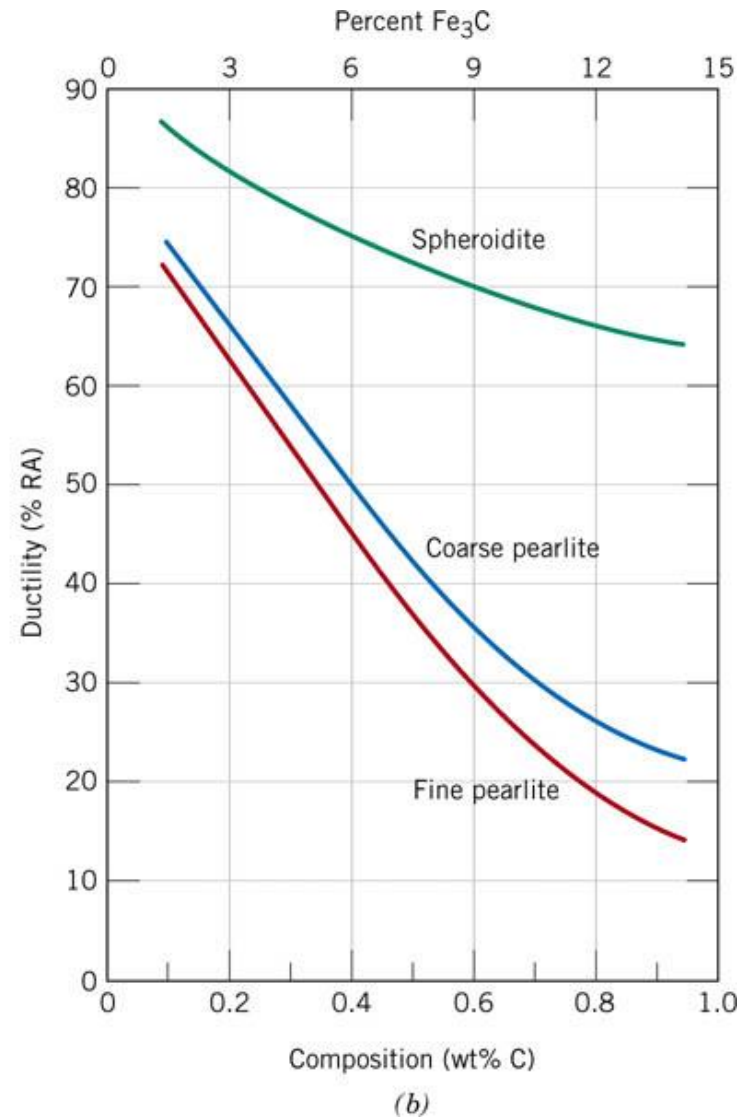
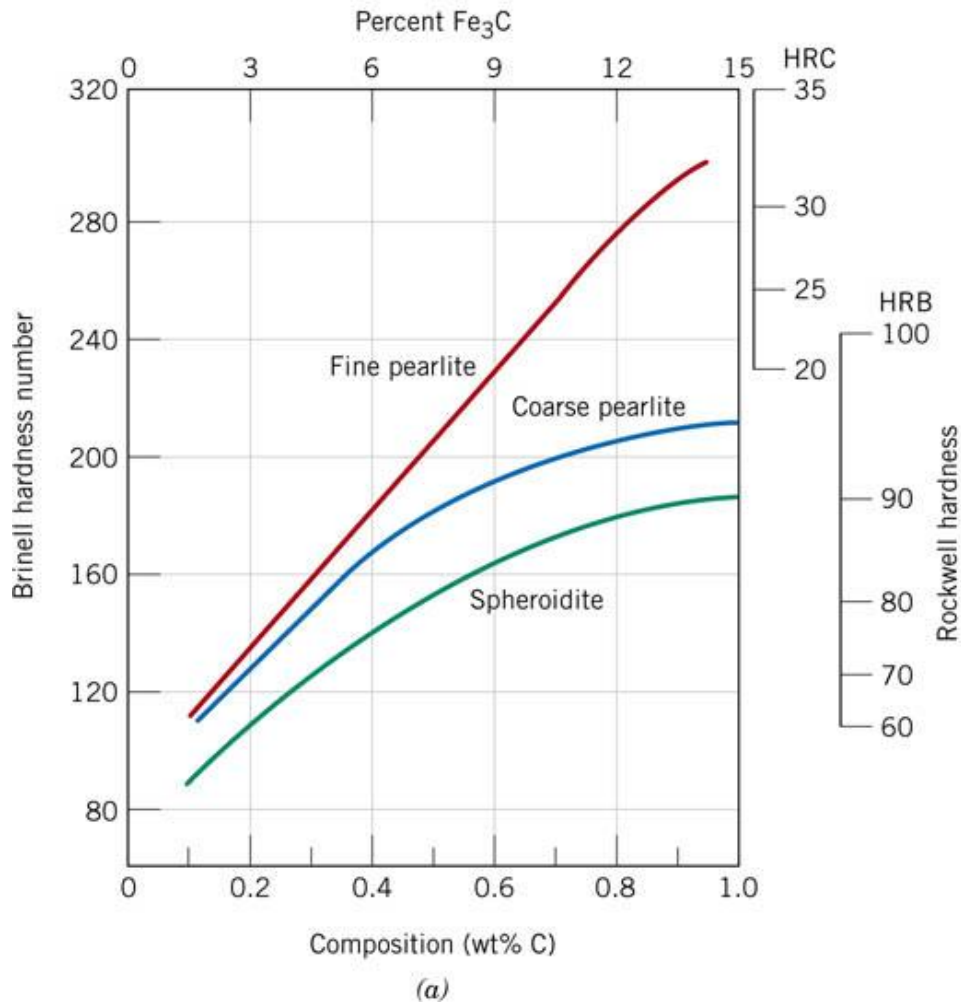
Mechanical Properties

plain carbon steel with fine pearlite microstructure



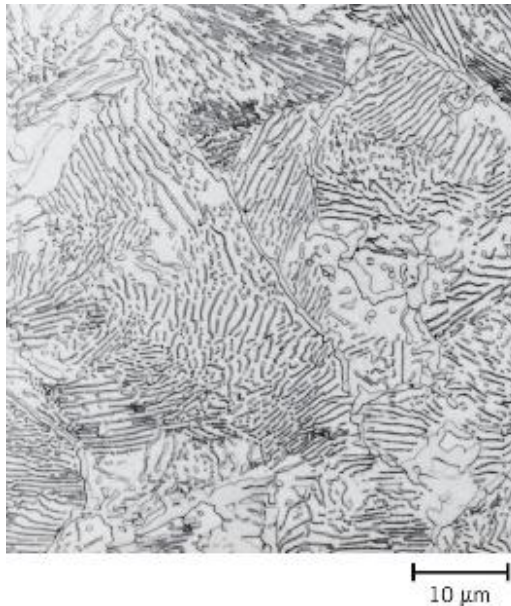
Mechanical Properties

plain carbon steel

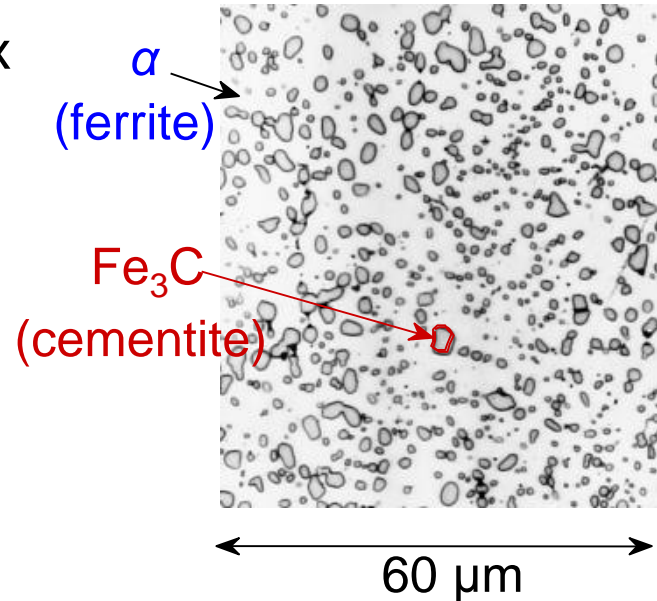


Spheroidite: Another Microstructure for the Fe-Fe₃C System

- Spheroidite:
 - Fe₃C particles within an α -ferrite matrix
 - formation requires diffusion
 - heat bainite or pearlite at temperature just below eutectoid for long times
 - driving force – reduction of α -ferrite/Fe₃C interfacial area



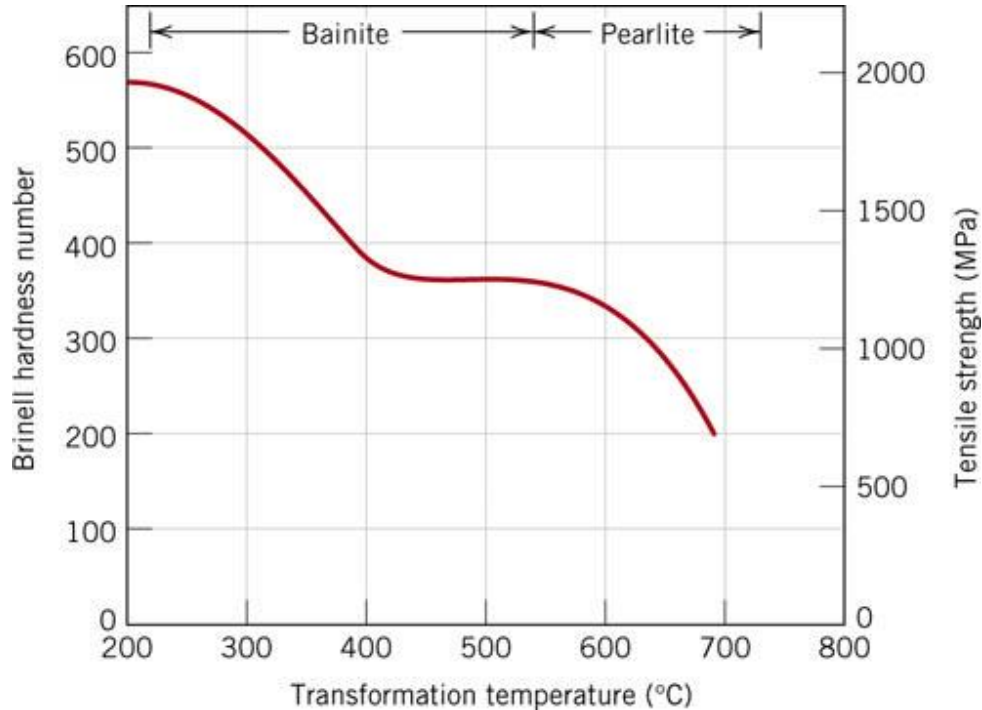
Courtesy of United States Steel Corporation.



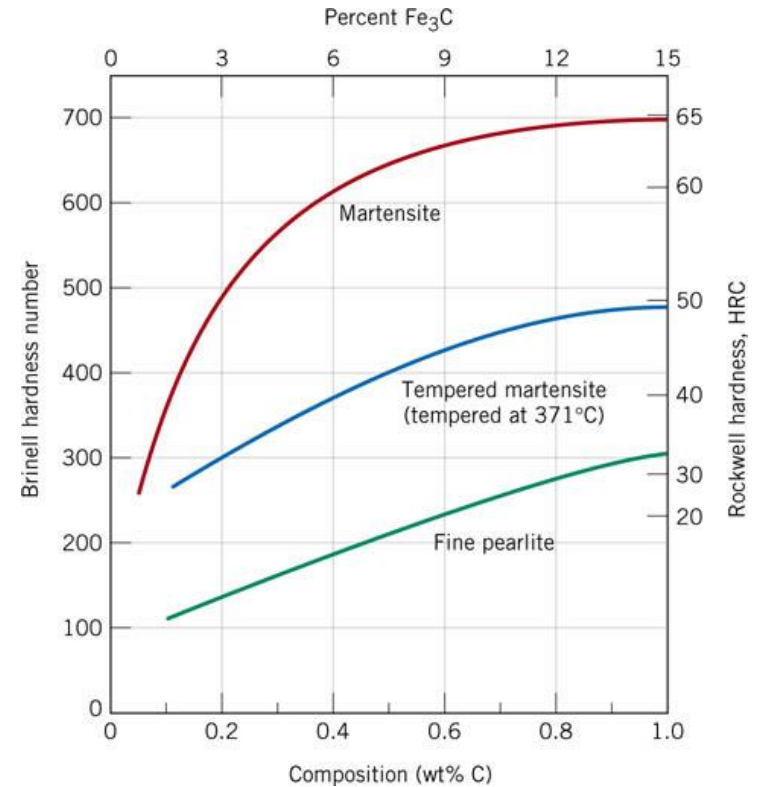
partially transformed to spheroidite

Mechanical Properties

plain carbon steel

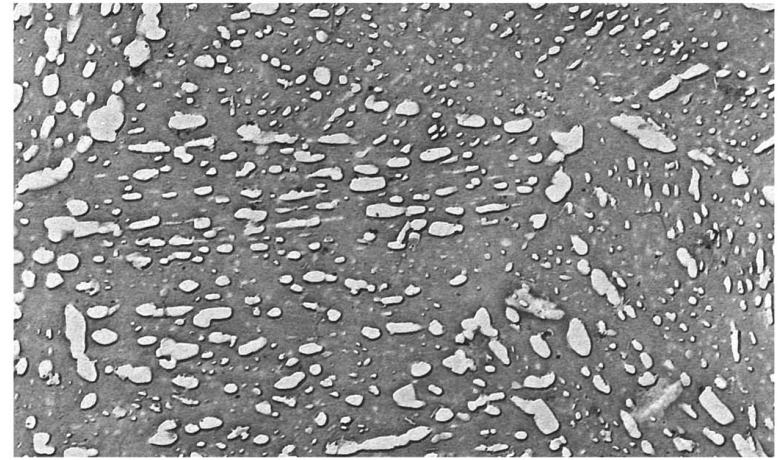
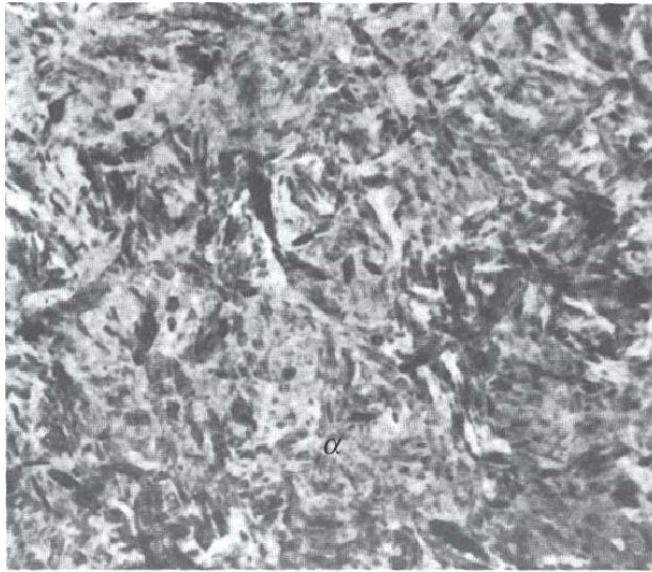
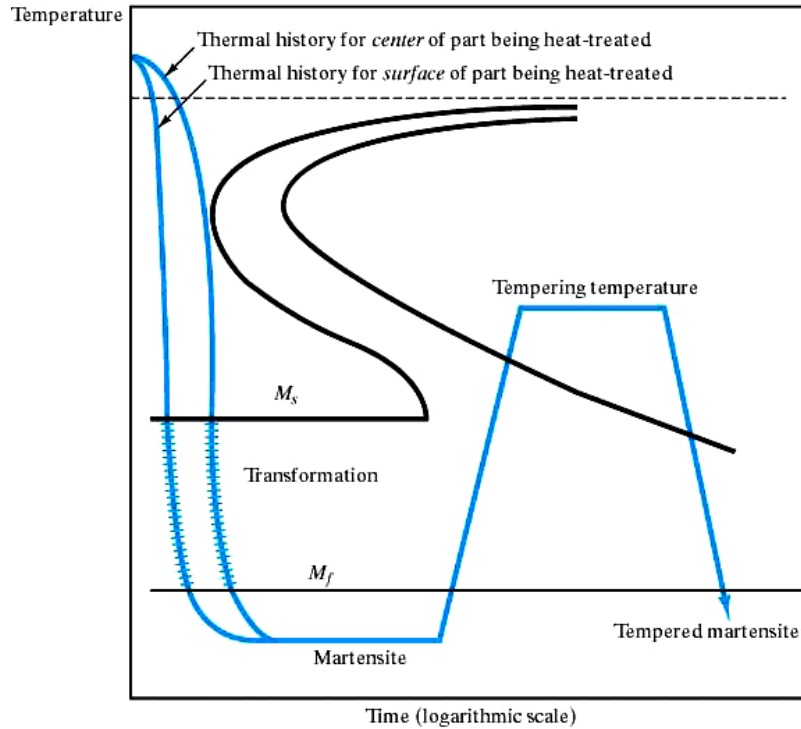


eutectoid composition

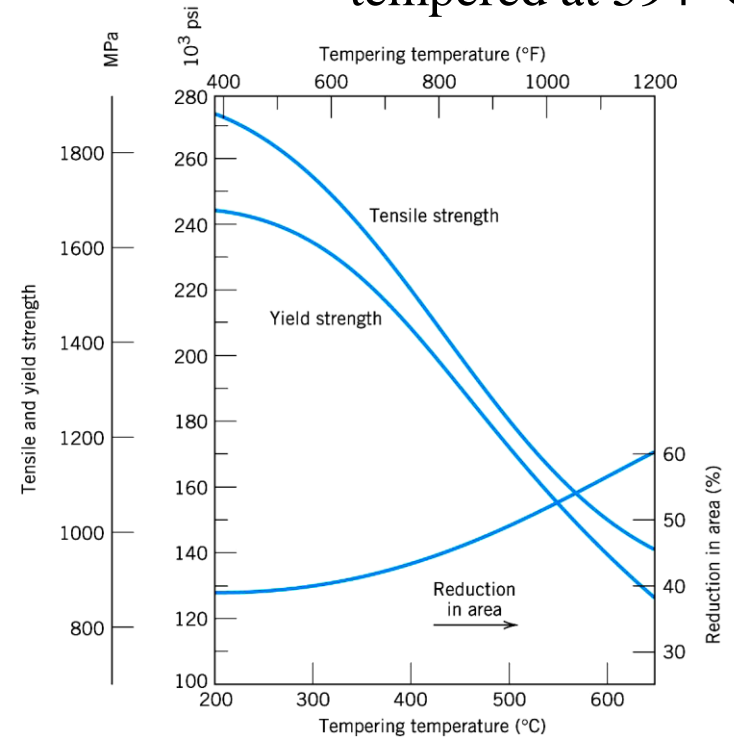


plain carbon steel

Tempering



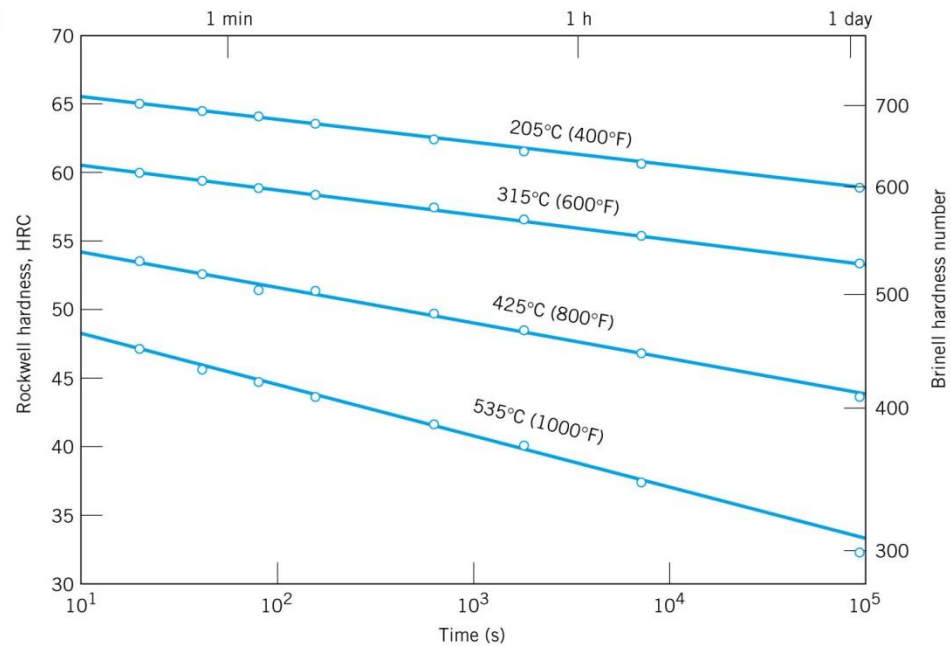
tempered at 594 °C



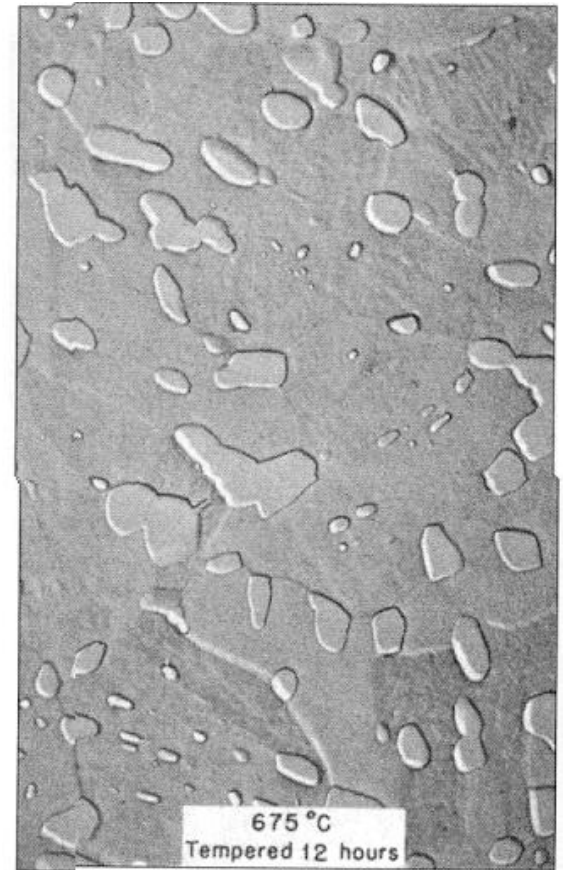
oil quenched alloy steel 4340 type

0.5 wt% C

FIGURE 10.26
 Hardness versus
 tempering time for a
 water-quenched
 eutectoid plain carbon
 (1080) steel. (Adapted
 from Edgar C. Bain,
*Functions of the
 Alloying Elements in
 Steel*, American
 Society for Metals,
 1939, p. 233.)



Spheroidite



0.7 wt% C

Summary: Processing Options

