

Recall:

- Maxwell's Equation (from 7.3.3. Maxwell's Equations)
 - $\nabla \cdot \mathbf{E} = \rho / \epsilon_0$: Gauss's law for electric field (ρ is charge density)
 - $\nabla \cdot \mathbf{B} = 0$: Gauss's law for magnetic field
 - $\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$: Faraday's law
 - $\nabla \times \mathbf{B} = \mu_0 \mathbf{J} + \mu_0 \epsilon_0 \frac{\partial \mathbf{E}}{\partial t}$: Ampere's law (\mathbf{J} is current density)
- Constitutive relation
 - $\mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P}$: \mathbf{P} is polarization density (from 4.3 The Electric Displacement)
 - $\mathbf{H} = \left(\frac{1}{\mu_0}\right) \mathbf{B} - \mathbf{M}$: \mathbf{M} is magnetization density (from 6.3 The Auxiliary Field \mathbf{H})
- Maxwell's Equation (from 7.3.5 Maxwell's Equations in Matter)
 - $\nabla \cdot \mathbf{D} = \rho_f$: Gauss's law for electric field (ρ_f is (free) charge density)
 - $\nabla \cdot \mathbf{B} = 0$: Gauss's law for magnetic field
 - $\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$: Faraday's law
 - $\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t} + \mathbf{J}_f$: Ampere's law (\mathbf{J}_f is (free) current density)

Linear and Isotropic Material

- Constitutive relation in linear and isotropic material
 - Polarization (from 4.4 Linear Dielectrics)
 - $\mathbf{P} = \epsilon_0 \chi_e \mathbf{E}$: χ_e is called electric susceptibility
 - ➔ $\mathbf{D} = \epsilon_0 \mathbf{E} + \mathbf{P} = \epsilon_0 (1 + \chi_e) \mathbf{E}$
 - By defining permittivity of the medium $\epsilon \equiv \epsilon_0 (1 + \chi_e)$
 - ➔ $\mathbf{D} \equiv \epsilon \mathbf{E}$
 - $\frac{\epsilon}{\epsilon_0} = 1 + \chi_e = \epsilon_r$ is also called as relative permittivity or more frequently dielectric constant
 - Magnetization (from 6.4 Linear and Nonlinear Media)
 - $\mathbf{M} = \chi_m \mathbf{H}$: χ_m is called magnetic susceptibility
 - ➔ $\mathbf{B} = \mu_0 (\mathbf{H} + \mathbf{M}) = \mu_0 (1 + \chi_m) \mathbf{H}$
 - By defining permeability of the medium $\mu \equiv \mu_0 (1 + \chi_m)$
 - ➔ $\mathbf{B} \equiv \mu \mathbf{H}$ or more frequently $\mathbf{H} = \frac{1}{\mu} \mathbf{B}$

9.3.1 Propagation in Linear Media

- Gauss's laws for linear and isotropic medium

- $\nabla \cdot \mathbf{D} = \rho_f$

- $\nabla \cdot \mathbf{B} = 0$

- $\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$

- $\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t} + \mathbf{J}_f$

- No charge & no current: $\rho = \mathbf{J} = 0$

- (i) $\nabla \cdot \mathbf{E} = 0$

- (ii) $\nabla \cdot \mathbf{B} = 0$

- (iii) $\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$

- (iv) $\nabla \times \mathbf{B} = \mu\epsilon \frac{\partial \mathbf{E}}{\partial t}$

- What is the difference from the last lecture?

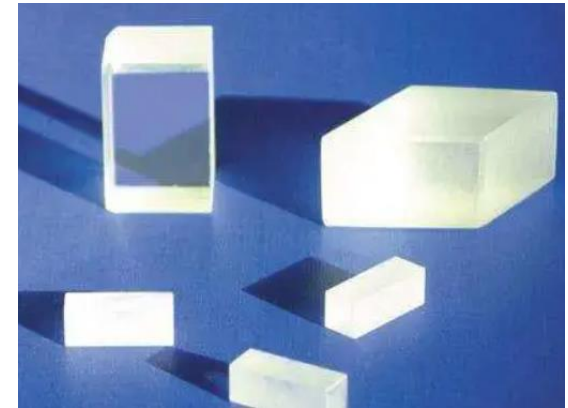
- (i) $\nabla \cdot \mathbf{E} = 0$

- (ii) $\nabla \cdot \mathbf{B} = 0$

- (iii) $\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$

- (iv) $\nabla \times \mathbf{B} = \mu_0\epsilon_0 \frac{\partial \mathbf{E}}{\partial t}$

- What is the speed of the light in the linear medium?



Picture of KTP

From <https://hncrystal.en.made-in-china.com/productimage/ovBJzghUaPYu-zf1jooenEQPWtRRCrG/China-Potassium-Titanyl-Phosphate-KTiOPO4-KTP-160-.html>

9.3.1 Propagation in Linear Media

- Speed of light in the linear media
 - $v = \frac{1}{\sqrt{\epsilon\mu}} = \frac{c}{n}$
 - $n = \sqrt{\frac{\epsilon\mu}{\epsilon_0\mu_0}}$: refractive index
 - For most of materials, $n \approx \sqrt{\epsilon_r}$
 - ϵ_r is almost always greater than 1 → light travels more slowly in matter
- Vacuum → Linear media: $\epsilon_0 \rightarrow \epsilon, \mu_0 \rightarrow \mu$ and $c \rightarrow v$
 - Energy density: $u = \frac{1}{2} \left(\epsilon E^2 + \frac{1}{\mu} B^2 \right) = \frac{1}{2} (\mathbf{E} \cdot \mathbf{D} + \mathbf{B} \cdot \mathbf{H})$
 - Poynting vector: $\mathbf{S} = \frac{1}{\mu} (\mathbf{E} \times \mathbf{B}) = (\mathbf{E} \times \mathbf{H})$
 - Intensity: $I = \frac{1}{2} \epsilon v E_0^2$
 - Proof: Prob. 8.15



Reflection and Transmission at the Boundary

- Behavior of field at the interface between two materials
 - Transmission
 - Familiar with refraction of the light by the water
 - Equilateral prisms (or dispersion prism)
 - Partial reflection by glass
 - Modeling of partial mirror in quantum optics (Hong-Ou-Mandel interference)
 - Polarization dependence
 - Sunglass
 - Brewster's angle
 - Total internal reflection
 - Dove prism
 - Fresnel rhoms
 - Multi-mode fiber
 - Mirrors
 - Dielectric mirrors vs metal mirrors



Transition of Notation

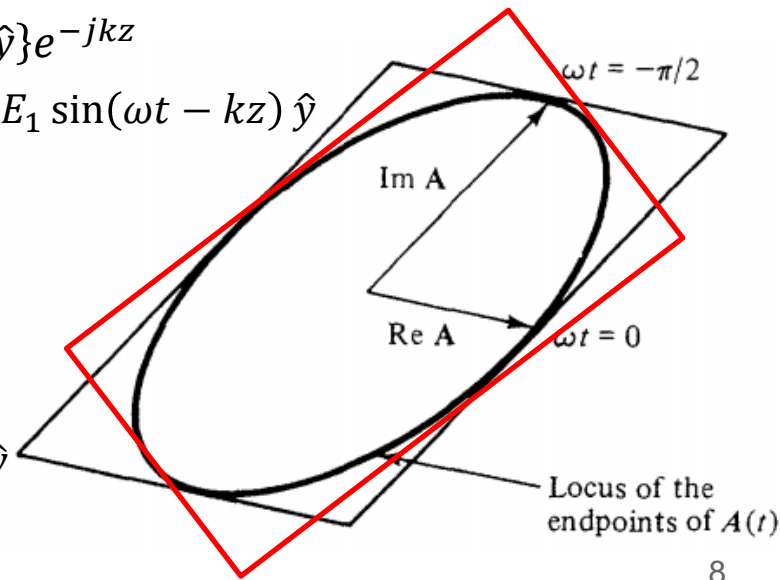
- From now on, I will switch from Griffiths book to Haus and Cheng books.
 - Griffiths: "Introduction to Electrodynamics", David. J. Griffiths, 3rd ed. (1999)
 - Haus: "Waves and Fields in Optoelectronics", Hermann A. Haus (1984)
 - Cheng: "Field and Wave Electromagnetics", David K. Cheng 2nd ed. (1989)
- Major changes of notations
 - Griffiths book
 - \mathbf{E}, \mathbf{B} are the fundamental fields, and \mathbf{D}, \mathbf{H} will be calculated, if necessary.
 - Exponential part of the primary field: $e^{i\mathbf{k}\cdot\mathbf{r}-i\omega t+i\phi}$
 - Complex field: $\tilde{\mathbf{E}}(\mathbf{r}, t) = (E_0 e^{i\delta} \hat{x}) e^{i(\mathbf{k}\cdot\mathbf{r}-\omega t)} \equiv \tilde{\mathbf{E}}_0 e^{i(\mathbf{k}\cdot\mathbf{r}-\omega t)}$
 - Haus and Cheng
 - \mathbf{E}, \mathbf{H} are the fundamental fields, and \mathbf{D}, \mathbf{B} will be calculated, if necessary.
 - Exponential part of the primary field: $e^{j\omega t-j\mathbf{k}\cdot\mathbf{r}+j\phi}$
 - Complex field: $\tilde{\mathbf{E}}(\mathbf{r}, t) = (E_0 e^{i\delta} e^{i\mathbf{k}\cdot\mathbf{r}} \hat{x}) e^{i\omega t} \equiv \mathbf{E}(\mathbf{r}) e^{i\omega t}$
 - We will mainly use $\mathbf{E}(\mathbf{r})$ only to represent electric field assuming the frequency is fixed → phasor (impedance calculation) used in electric circuits

(Haus) 1.2 Complex Vectors

- Maxwell's equations in linear media → Linear
 - (i) $\nabla \cdot \mathbf{E} = \rho_f / \epsilon$ (ii) $\nabla \cdot \mathbf{H} = 0$
 - (iii) $\nabla \times \mathbf{E} = -\mu \frac{\partial \mathbf{H}}{\partial t}$ (iv) $\nabla \times \mathbf{H} = \epsilon \frac{\partial \mathbf{E}}{\partial t} + \mathbf{J}_f$
 - Sinusoidal excitation (e.g. a sinusoidal ρ_f or \mathbf{J}_f) at frequency ω
→ sinusoidal response (\mathbf{E} and \mathbf{B} change with frequency ω)
- Physical interpretation of complex vectors (phasors)
 - Example: complex scalar $V = |V|e^{j\phi}$
→ $v(t) = \text{Re}[Ve^{j\omega t}] = |V| \cos(\omega t + \phi)$
 - Complex vector $\mathbf{A} = A_x \hat{x} + A_y \hat{y} + A_z \hat{z}$
 $\mathbf{A} = |A_x|e^{j\phi_x} \hat{x} + |A_y|e^{j\phi_y} \hat{y} + |A_z|e^{j\phi_z} \hat{z} = \text{Re}[\mathbf{A}] + j\text{Im}[\mathbf{A}]$
where $\text{Re}[\mathbf{A}] = \text{Re}[A_x] \hat{x} + \text{Re}[A_y] \hat{y} + \text{Re}[A_z] \hat{z}$ & $\text{Im}[\mathbf{A}]$ are real vectors
→ $\mathbf{A}(t) = \text{Re}[\mathbf{A}e^{j\omega t}]$
 $= |A_x| \cos(\omega t + \phi_x) \hat{x} + |A_y| \cos(\omega t + \phi_y) \hat{y} + |A_z| \cos(\omega t + \phi_z) \hat{z}$
 $= \text{Re}[\mathbf{A}] \cos \omega t - \text{Im}[\mathbf{A}] \sin \omega t$

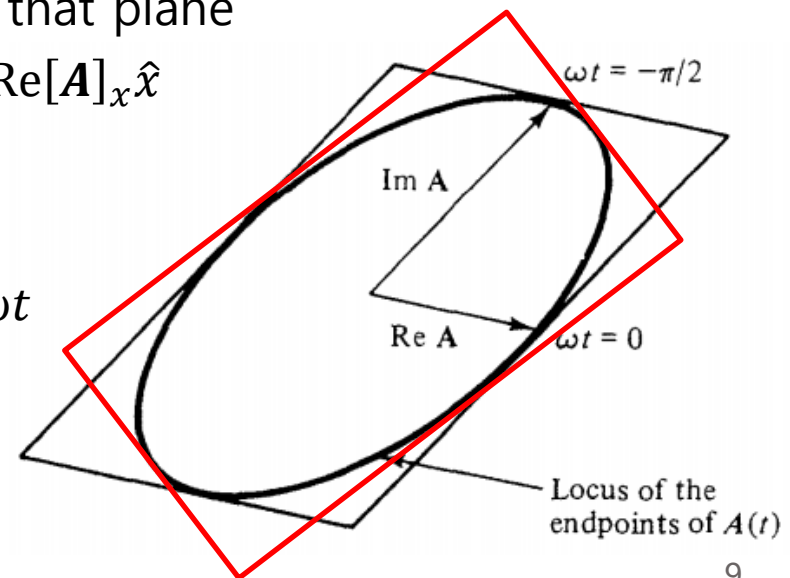
Representation of Polarization

- Recall
 - $\mathbf{E}(x, y, z, t) = E_0 \cos(\omega t - kz + \delta) \hat{x} = \text{Re}[\{E_0 e^{j(\delta - kz)} \hat{x}\} e^{j\omega t}] = \text{Re}[\tilde{\mathbf{E}}(x, y, z) e^{j\omega t}]$
- $\tilde{\mathbf{E}}(x, y, z) = \tilde{\mathbf{E}}(\mathbf{r}) = E_0 e^{j(-\frac{\pi}{2} - kz)} \hat{y}$
 - $\mathbf{E}(\mathbf{r}, t) = \text{Re}[\tilde{\mathbf{E}}(\mathbf{r}) e^{j\omega t}] = E_0 \sin(\omega t - kz) \hat{y}$
 - Linear polarization
- $\tilde{\mathbf{E}}(\mathbf{r}) = E_0 e^{j(-kz)} \hat{x} + E_0 e^{j(-\frac{\pi}{2} - kz)} \hat{y} = E_0 \{\hat{x} - j\hat{y}\} e^{-jkz}$
 - $\mathbf{E}(\mathbf{r}, t) = \text{Re}[\tilde{\mathbf{E}}(\mathbf{r}) e^{j\omega t}] = E_0 \{\cos(\omega t - kz) \hat{x} + \sin(\omega t - kz) \hat{y}\}$
 - Circular polarization
- $\tilde{\mathbf{E}}(\mathbf{r}) = E_0 e^{j(-kz)} \hat{x} + E_1 e^{j(\frac{\pi}{2} - kz)} \hat{y} = \{E_0 \hat{x} + jE_1 \hat{y}\} e^{-jkz}$
 - $\mathbf{E}(\mathbf{r}, t) = \text{Re}[\tilde{\mathbf{E}}(\mathbf{r}) e^{j\omega t}] = E_0 \cos(\omega t - kz) \hat{x} - E_1 \sin(\omega t - kz) \hat{y}$
 - Elliptical polarization
 - Are \hat{x} and \hat{y} special direction?
- Arbitrary polarization
 - $\mathbf{A} = |A_x| e^{j\phi_x} \hat{x} + |A_y| e^{j\phi_y} \hat{y} + |A_z| e^{j\phi_z} \hat{z}$
 - Non-orthogonal axis: $\mathbf{A} = \text{Re}[\mathbf{A}] + j\text{Im}[\mathbf{A}]$
 - Non- $\frac{\pi}{2}$ phase difference: $\mathbf{A} = |\alpha| \hat{n} + |\beta| e^{j\phi} \hat{m}$
 - What about both? $\mathbf{A} = |\alpha| \hat{n} + |\beta| e^{j\phi} \hat{m}$



(Haus) 1.2 Complex Vectors

- Physical interpretation of complex vectors (phasors)
 - The locus of $\mathbf{A}(t)$ for all t forms an ellipse
 - $\mathbf{A}(t) = \text{Re}[\mathbf{A}e^{j\omega t}] = \text{Re}[\mathbf{A}] \cos \omega t - \text{Im}[\mathbf{A}] \sin \omega t$
 - Both $\text{Re}[\mathbf{A}]$ and $\text{Im}[\mathbf{A}]$ are real vectors, but they are not necessarily orthogonal to each other
 - Vector $\mathbf{A}(t)$ must lie in the plane formed by $\text{Re}[\mathbf{A}]$ and $\text{Im}[\mathbf{A}]$.
 - 2D Cartesian coordinate system in that plane
 - Choose \hat{x} along $\text{Re}[\mathbf{A}] \rightarrow \text{Re}[\mathbf{A}] = \text{Re}[\mathbf{A}]_x \hat{x}$
 - $\text{Im}[\mathbf{A}] = \text{Im}[\mathbf{A}]_x \hat{x} + \text{Im}[\mathbf{A}]_y \hat{y}$
 - $\mathbf{A}(t) \equiv A_x(t) \hat{x} + A_y(t) \hat{y}$
 - $A_x(t) = \text{Re}[\mathbf{A}]_x \cos \omega t - \text{Im}[\mathbf{A}]_x \sin \omega t$
 - $A_y(t) = -\text{Im}[\mathbf{A}]_y \sin \omega t$



(Haus) 1.2 Complex Vectors

- (cont'd) Physical interpretation of complex vectors (phasors)
 - What is the equation for ellipse?
 - $\alpha x^2 + \beta y^2 = \gamma$ whose major axis and minor axis are aligned along x - and y -axis and $\alpha, \beta, \gamma > 0$
 - $\begin{bmatrix} x & y \end{bmatrix} \begin{bmatrix} \alpha & 0 \\ 0 & \beta \end{bmatrix} \begin{bmatrix} x \\ y \end{bmatrix} = \gamma$
 - From $A_y(t) = -\text{Im}[\mathbf{A}]_y \sin \omega t$, $\sin \omega t = -\frac{A_y(t)}{\text{Im}[\mathbf{A}]_y}$
 - From $A_x(t) = \text{Re}[\mathbf{A}]_x \cos \omega t - \text{Im}[\mathbf{A}]_x \sin \omega t$, $\cos \omega t = \frac{1}{\text{Re}[\mathbf{A}]_x} \left\{ A_x(t) - \frac{\text{Im}[\mathbf{A}]_x}{\text{Im}[\mathbf{A}]_y} A_y(t) \right\}$
 - $\sin^2 \omega t + \cos^2 \omega t = 1 \rightarrow \left\{ \frac{A_y(t)}{\text{Im}[\mathbf{A}]_y} \right\}^2 + \frac{1}{\text{Re}[\mathbf{A}]_x^2} \left\{ A_x(t) - \frac{\text{Im}[\mathbf{A}]_x}{\text{Im}[\mathbf{A}]_y} A_y(t) \right\}^2 = 1$
 - $\rightarrow \text{Re}[\mathbf{A}]_x^2 A_y(t)^2 + \text{Im}[\mathbf{A}]_y^2 A_x(t)^2 - 2\text{Im}[\mathbf{A}]_y \text{Im}[\mathbf{A}]_x A_x(t) A_y(t) + \text{Im}[\mathbf{A}]_x^2 A_y(t)^2 = \text{Im}[\mathbf{A}]_y^2 \text{Re}[\mathbf{A}]_x^2$
 - $\rightarrow \{ \text{Re}[\mathbf{A}]_x^2 + \text{Im}[\mathbf{A}]_x^2 \} A_y(t)^2 - 2\text{Im}[\mathbf{A}]_y \text{Im}[\mathbf{A}]_x A_x(t) A_y(t) + \text{Im}[\mathbf{A}]_y^2 A_x(t)^2 = \text{Im}[\mathbf{A}]_y^2 \text{Re}[\mathbf{A}]_x^2$
 - $\begin{bmatrix} A_y(t) & A_x(t) \end{bmatrix} \begin{bmatrix} \text{Re}[\mathbf{A}]_x^2 + \text{Im}[\mathbf{A}]_x^2 & -\text{Im}[\mathbf{A}]_y \text{Im}[\mathbf{A}]_x \\ -\text{Im}[\mathbf{A}]_y \text{Im}[\mathbf{A}]_x & \text{Im}[\mathbf{A}]_y^2 \end{bmatrix} \begin{bmatrix} A_y(t) \\ A_x(t) \end{bmatrix} = \text{Im}[\mathbf{A}]_y^2 \text{Re}[\mathbf{A}]_x^2$
 - Symmetric matrix \rightarrow diagonalizable with orthogonal transform
 - $\det \begin{bmatrix} a - \lambda & -b \\ -b & c - \lambda \end{bmatrix} = (\lambda - a)(\lambda - c) - b^2 = \lambda^2 - (a + c)\lambda + ac - b^2 = (\lambda - \lambda_1)(\lambda - \lambda_2)$
 - If positive (semi-)definite, $\lambda_1, \lambda_2 \geq 0 \Rightarrow (a + c) \geq 0, ac - b^2 \geq 0$
 - $ac - b^2 = \{ \text{Re}[\mathbf{A}]_x^2 + \text{Im}[\mathbf{A}]_x^2 \} \text{Im}[\mathbf{A}]_y^2 - \text{Im}[\mathbf{A}]_y^2 \text{Im}[\mathbf{A}]_x^2 = \text{Im}[\mathbf{A}]_y^2 \{ \text{Re}[\mathbf{A}]_x^2 + \text{Im}[\mathbf{A}]_x^2 - \text{Im}[\mathbf{A}]_x^2 \} \geq 0$
 - $\begin{bmatrix} A_y(t) & A_x(t) \end{bmatrix} \mathbb{O} \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \mathbb{O}^T \begin{bmatrix} A_y(t) \\ A_x(t) \end{bmatrix} = \gamma$

(Haus) 1.2 Complex Vectors

- Time average
 - Time average of products of sinusoidally time-dependent scalars
 - Example: $V = |V|e^{j\phi_V}, I = |I|e^{j\phi_I}$
➔ $v(t) = \text{Re}[Ve^{j\omega t}] = |V| \cos(\omega t + \phi_V), i(t) = \text{Re}[Ie^{j\omega t}] = |I| \cos(\omega t + \phi_I)$

$$\begin{aligned}\langle v(t)i(t) \rangle &= \frac{1}{T} \int_0^T v(t)i(t) dt \\&= \frac{1}{T} \int_0^T \frac{1}{2} (Ve^{j\omega t} + V^*e^{-j\omega t}) \frac{1}{2} (Ie^{j\omega t} + I^*e^{-j\omega t}) dt \\&= \frac{1}{4T} \int_0^T \{V I e^{j2\omega t} + V I^* + V^* I + (V I)^* e^{-j2\omega t}\} dt \\&= \frac{1}{4T} T (V I^* + V^* I) = \frac{1}{2} \frac{V I^* + V^* I}{2} = \frac{1}{2} \text{Re}[V I^*]\end{aligned}$$

|| (Haus) 1.2 Complex Vectors

- (cont'd) Time average
 - Time average of products of sinusoidally time-dependent vectors

$$\begin{aligned}\langle \mathbf{A}(t) \times \mathbf{B}(t) \rangle &= \frac{1}{T} \int_0^T \mathbf{A}(t) \times \mathbf{B}(t) dt \\&= \frac{1}{T} \int_0^T \frac{1}{2} (\mathbf{A} e^{j\omega t} + \mathbf{A}^* e^{-j\omega t}) \times \frac{1}{2} (\mathbf{B} e^{j\omega t} + \mathbf{B}^* e^{-j\omega t}) dt \\&= \frac{1}{4T} \int_0^T \{ (\mathbf{A} \times \mathbf{B}) e^{j2\omega t} + \mathbf{A} \times \mathbf{B}^* + \mathbf{A}^* \times \mathbf{B} + (\mathbf{A}^* \times \mathbf{B}^*) e^{-j2\omega t} \} dt \\&= \frac{1}{4T} T (\mathbf{A} \times \mathbf{B}^* + \mathbf{A}^* \times \mathbf{B}) = \frac{1}{2} \frac{\mathbf{A} \times \mathbf{B}^* + \mathbf{A}^* \times \mathbf{B}}{2} = \frac{1}{2} \text{Re}[\mathbf{A} \times \mathbf{B}^*]\end{aligned}$$



1.4 The Complex Form of Maxwell's Eqs

- $\mathbf{E}(\mathbf{r}, t), \mathbf{B}(\mathbf{r}, t), \mathbf{J}(\mathbf{r}, t), \rho(\mathbf{r}, t) \rightarrow \mathbf{E}(\mathbf{r})e^{j\omega t}, \mathbf{B}(\mathbf{r})e^{j\omega t}, \mathbf{J}(\mathbf{r})e^{j\omega t}, \rho(\mathbf{r})e^{j\omega t}$
 - ▣ $\nabla \cdot (\epsilon \mathbf{E}(\mathbf{r}, t)) = \rho \quad \rightarrow \nabla \cdot (\epsilon \mathbf{E}(\mathbf{r})) = \rho$
 - ▣ $\nabla \cdot (\mu \mathbf{H}(\mathbf{r}, t)) = 0 \quad \rightarrow \nabla \cdot (\mu \mathbf{H}(\mathbf{r})) = 0$
 - ▣ $\nabla \times \mathbf{E}(\mathbf{r}, t) = -\mu \frac{\partial \mathbf{H}(\mathbf{r}, t)}{\partial t} \quad \rightarrow \nabla \times \mathbf{E}(\mathbf{r}) = -j\omega \mu \mathbf{H}(\mathbf{r})$
 - ▣ $\nabla \times \mathbf{H}(\mathbf{r}, t) = \epsilon \frac{\partial \mathbf{E}(\mathbf{r}, t)}{\partial t} + \mathbf{J}(\mathbf{r}, t) \quad \rightarrow \nabla \times \mathbf{H}(\mathbf{r}) = j\omega \epsilon \mathbf{E}(\mathbf{r}) + \mathbf{J}(\mathbf{r})$
- No charge & no current ($\rho = \mathbf{J} = 0$) & spatially uniform ϵ, μ
 - ▣ $\nabla \times (\nabla \times \mathbf{E}(\mathbf{r})) = -j\omega \mu (\nabla \times \mathbf{H}(\mathbf{r})) = \omega^2 \mu \epsilon \mathbf{E}(\mathbf{r})$
 - ▣ $\nabla \times (\nabla \times \mathbf{E}(\mathbf{r})) = \nabla(\nabla \cdot \mathbf{E}(\mathbf{r})) - \nabla^2 \mathbf{E}(\mathbf{r})$
 - ▣ $\nabla^2 \mathbf{E}(\mathbf{r}) + \omega^2 \mu \epsilon \mathbf{E}(\mathbf{r}) = 0$
- For plane wave,
 - ▣ $\mathbf{E}(\mathbf{r}) = \mathbf{E}_+ e^{-jk \cdot \mathbf{r}} \text{ \& } \mathbf{H}(\mathbf{r}) = \mathbf{H}_+ e^{-jk \cdot \mathbf{r}}$

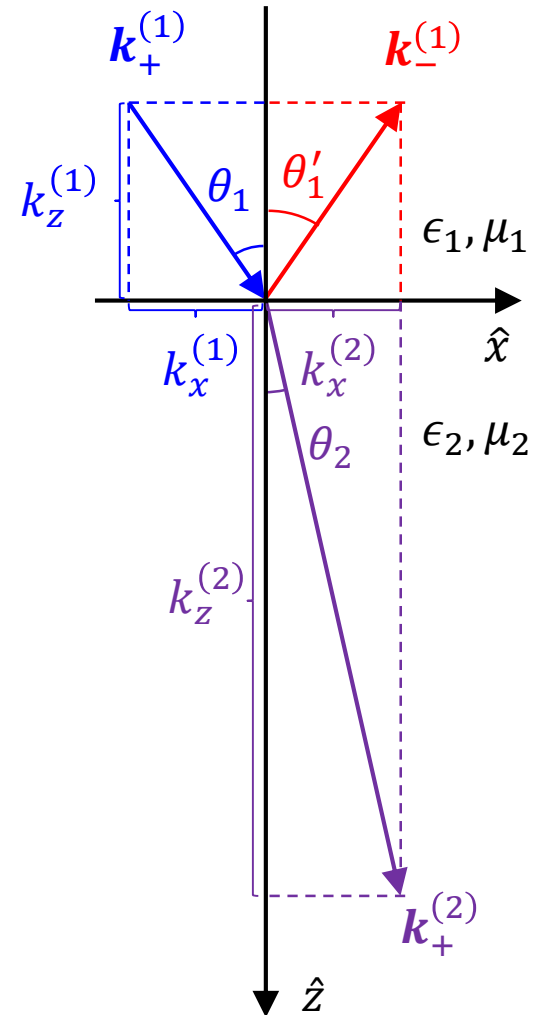


1.4 The Complex Form of Maxwell's Eqs

- Plane wave in source-free medium
 - $\mathbf{E}(\mathbf{r}) = \mathbf{E}_+ e^{-j\mathbf{k} \cdot \mathbf{r}}$ & $\mathbf{H}(\mathbf{r}) = \mathbf{H}_+ e^{-j\mathbf{k} \cdot \mathbf{r}} \rightarrow \nabla$ is replaced by $-j\mathbf{k}$
 - $\nabla \cdot \mathbf{E}(\mathbf{r}) = 0 \quad \rightarrow -j\mathbf{k} \cdot \mathbf{E}_+ = 0$
 - $\nabla \cdot \mathbf{H}(\mathbf{r}) = 0 \quad \rightarrow -j\mathbf{k} \cdot \mathbf{H}_+ = 0$
 - $\nabla \times \mathbf{E}(\mathbf{r}) = -j\omega\mu\mathbf{H}(\mathbf{r}) \quad \rightarrow -j\mathbf{k} \times \mathbf{E}_+ = -j\omega\mu\mathbf{H}_+$
 - $\nabla \times \mathbf{H}(\mathbf{r}) = j\omega\epsilon\mathbf{E}(\mathbf{r}) \quad \rightarrow -j\mathbf{k} \times \mathbf{H}_+ = j\omega\epsilon\mathbf{E}_+$
 - $\mathbf{k} \times (\mathbf{k} \times \mathbf{E}_+) = \mathbf{k}(\mathbf{k} \cdot \mathbf{E}_+) - \mathbf{E}_+(\mathbf{k} \cdot \mathbf{k}) = \mathbf{k} \times (\omega\mu\mathbf{H}_+) = -\omega^2\mu\epsilon\mathbf{E}_+$
 - $\mathbf{E}_+ k^2 = \omega^2\mu\epsilon\mathbf{E}_+ \rightarrow k^2 = \omega^2\mu\epsilon$ called dispersion relation
 - $\mathbf{H}_+ = \frac{1}{\omega\mu} \mathbf{k} \times \mathbf{E}_+ = \sqrt{\frac{\epsilon}{\mu}} \hat{\mathbf{k}} \times \mathbf{E}_+$
 - (Intrinsic) impedance of medium: $\eta = \frac{|E|}{|H|} = \sqrt{\frac{\mu}{\epsilon}}$

Reflection and Transmission

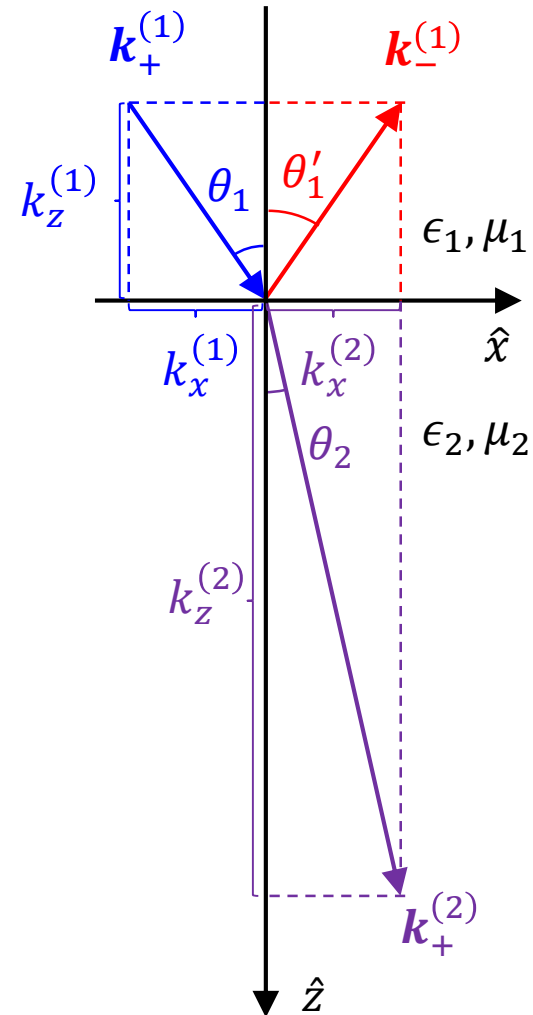
- Boundary conditions (no charge, no current)
 - $D_1^\perp - D_2^\perp = 0, \mathbf{E}_1^\parallel - \mathbf{E}_2^\parallel = 0$
 - $B_1^\perp - B_2^\perp = 0, \mathbf{H}_1^\parallel - \mathbf{H}_2^\parallel = 0$
- Monochromatic, plane wave
 - Plane of incidence
 - Incident wave: $E_+^{(1)} e^{j(\omega_+^{(1)} t - \mathbf{k}_+^{(1)} \cdot \mathbf{r})}$
 - Reflected wave: $E_-^{(1)} e^{j(\omega_-^{(1)} t - \mathbf{k}_-^{(1)} \cdot \mathbf{r})}$
 - Transmitted wave: $E_+^{(2)} e^{j(\omega_+^{(2)} t - \mathbf{k}_+^{(2)} \cdot \mathbf{r})}$
 - $\omega_+^{(1)} = \omega_-^{(1)} = \omega_+^{(2)} = \omega$
 - Tangential E & H continuous at all points on the boundary
 - ➔ $k_{x+}^{(1)} = k_{x-}^{(1)} = k_{x+}^{(2)} = k_x$
 - ➔ $k_{y+}^{(1)} = k_{y-}^{(1)} = k_{y+}^{(2)} = k_y$
 - What determines $k_z^{(2)}$?



Reflection and Transmission

Consequences

- 1) All waves have the same ω
- 2) All wave vectors are in one plane \rightarrow plane of incidence
- 3) The angle of reflection θ'_1 is the same as angle of incidence θ_1
 - $k_+^{(1)} \sin \theta_1 = k_-^{(1)} \sin \theta'_1 \rightarrow \theta'_1 = \theta_1$
- 4) The angle of transmission θ_2 is related to the angle of incidence θ_1 by $k_+^{(1)} \sin \theta_1 = k_+^{(2)} \sin \theta_2$
 - $k_+^{(1)} = k_-^{(1)} = k^{(1)} = \omega \sqrt{\mu_1 \epsilon_1} = \omega \frac{n_1}{c}$
 - $k_+^{(2)} = k^{(2)} = \omega \sqrt{\mu_2 \epsilon_2} = \omega \frac{n_2}{c}$
 - $n_1 \sin \theta_1 = n_2 \sin \theta_2$ or $\sqrt{\mu_1 \epsilon_1} \sin \theta_1 = \sqrt{\mu_2 \epsilon_2} \sin \theta_2 \rightarrow$ Snell's law



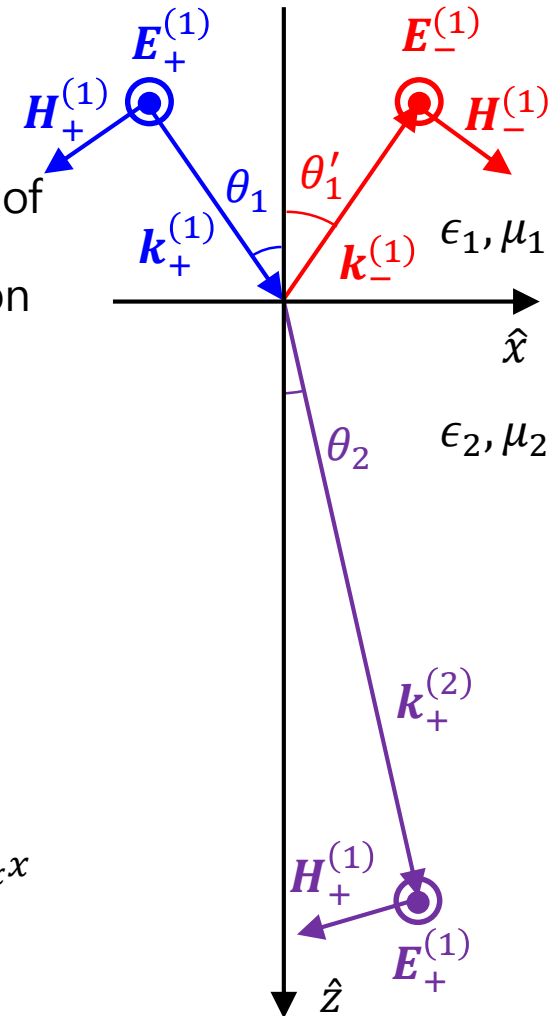
(Haus) 2.1 TE Wave Reflected from Boundary

■ Transverse electric wave reflected from boundary

- Consider a plane wave with E -field polarized parallel to the surface of an interface between two media
 - What should be the electric polarization direction of the reflected and transmitted fields?
 - What should be the magnetic polarization direction of the reflected and transmitted fields?

→ determined by boundary conditions

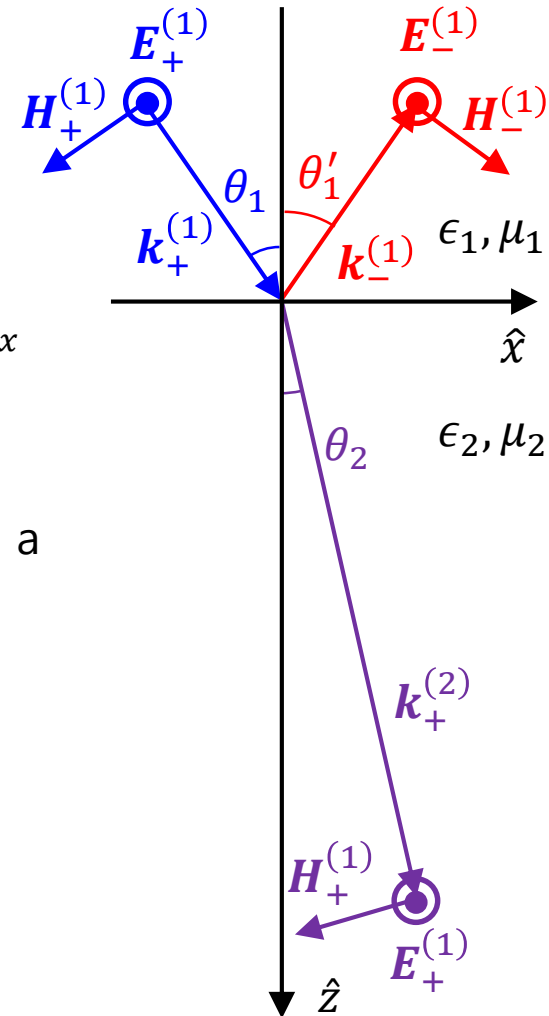
- $k_{x+}^{(1)} = k_{x-}^{(1)} = k_{x+}^{(2)} = k_x$
- $k_{z+}^{(1)} = k_{z-}^{(1)} = k_z^{(1)}$
- Incident: $\hat{y}E_+^{(1)}e^{-jk_+^{(1)} \cdot \mathbf{r}} = \hat{y}E_+^{(1)}e^{-jk_z^{(1)}z}e^{-jk_xx}$
- Reflected: $\hat{y}E_-^{(1)}e^{-jk_-^{(1)} \cdot \mathbf{r}} = \hat{y}E_-^{(1)}e^{jk_z^{(1)}z}e^{-jk_xx}$
- Transmitted: $\hat{y}E_+^{(2)}e^{-jk_+^{(2)} \cdot \mathbf{r}} = \hat{y}E_+^{(2)}e^{-jk_z^{(2)}z}e^{-jk_xx}$
- Region 1: $E_y^{(1)} = (E_+^{(1)}e^{-jk_z^{(1)}z} + E_-^{(1)}e^{jk_z^{(1)}z})e^{-jk_xx}$
- Region 2: $E_y^{(2)} = E_+^{(2)}e^{-jk_z^{(2)}z}e^{-jk_xx}$



(Haus) 2.1 TE Wave Reflected from Boundary

- Region 1: $E_y^{(1)} = \left(E_+^{(1)} e^{-jk_z^{(1)} z} + E_-^{(1)} e^{jk_z^{(1)} z} \right) e^{-jk_x x}$
- Region 2: $E_y^{(2)} = E_+^{(2)} e^{-jk_z^{(2)} z} e^{-jk_x x}$
- In general, from $\nabla \times \mathbf{E} = -j\omega\mu\mathbf{H}$,

$$H_x = -\frac{1}{j\omega\mu} [\partial_y E_z - \partial_z E_y] = \frac{(jk_z)}{j\omega\mu} E_y = \frac{(k_z)}{\omega\mu} E_y$$
- Region 1: $H_x^{(1)} = \frac{k_z^{(1)}}{\omega\mu} \left(-E_+^{(1)} e^{-jk_z^{(1)} z} + E_-^{(1)} e^{jk_z^{(1)} z} \right) e^{-jk_x x}$
- Region 2: $H_x^{(2)} = -\frac{k_z^{(2)}}{\omega\mu} E_+^{(2)} e^{-jk_z^{(2)} z} e^{-jk_x x}$
- **Characteristic impedance** presented by medium 1 to a TE wave at inclination θ_1 with respect to the z axis:
 - For TE, $Z_0^{(1)} \equiv \frac{\omega\mu_1}{k_z^{(1)}} = \frac{\omega\mu_1}{\omega\sqrt{\epsilon_1\mu_1} \cos \theta_1} = \sqrt{\frac{\mu_1}{\epsilon_1}} \frac{1}{\cos \theta_1} \sim \frac{E_y}{H_x}$
 - cf) (**intrinsic**) **impedance** of medium: $\eta = \frac{|E|}{|H|} = \sqrt{\frac{\mu}{\epsilon}}$
- **Wave impedance** of TE: $Z(z) = -\frac{\text{Total } E_y(z)}{\text{Total } H_x(z)}$



(Haus) 2.1 TE Wave Reflected from Boundary

Region 1

- $$E_y^{(1)} = (E_+^{(1)} e^{-jk_z^{(1)} z} + E_-^{(1)} e^{jk_z^{(1)} z}) e^{-jk_x x}$$
- $$H_x^{(1)} = -\frac{k_z^{(1)}}{\omega\mu} (E_+^{(1)} e^{-jk_z^{(1)} z} - E_-^{(1)} e^{jk_z^{(1)} z}) e^{-jk_x x}$$

Region 2

- $$E_y^{(2)} = E_+^{(2)} e^{-jk_z^{(2)} z} e^{-jk_x x}$$
- $$H_x^{(2)} = -\frac{k_z^{(2)}}{\omega\mu} E_+^{(2)} e^{-jk_z^{(2)} z} e^{-jk_x x}$$

- Characteristic impedance of TE: $Z_0^{(1)} \equiv \frac{\omega\mu_1}{k_z^{(1)}} = \sqrt{\frac{\mu_1}{\epsilon_1}} \frac{1}{\cos \theta_1}$

- At $z = 0$ for all x values, $E_y^{(1)} = E_y^{(2)}, H_x^{(1)} = H_x^{(2)}$

- $$E_+^{(1)} + E_-^{(1)} = E_+^{(2)}$$
- $$\frac{1}{Z_0^{(1)}} (E_+^{(1)} - E_-^{(1)}) = \frac{1}{Z_0^{(2)}} E_+^{(2)}$$

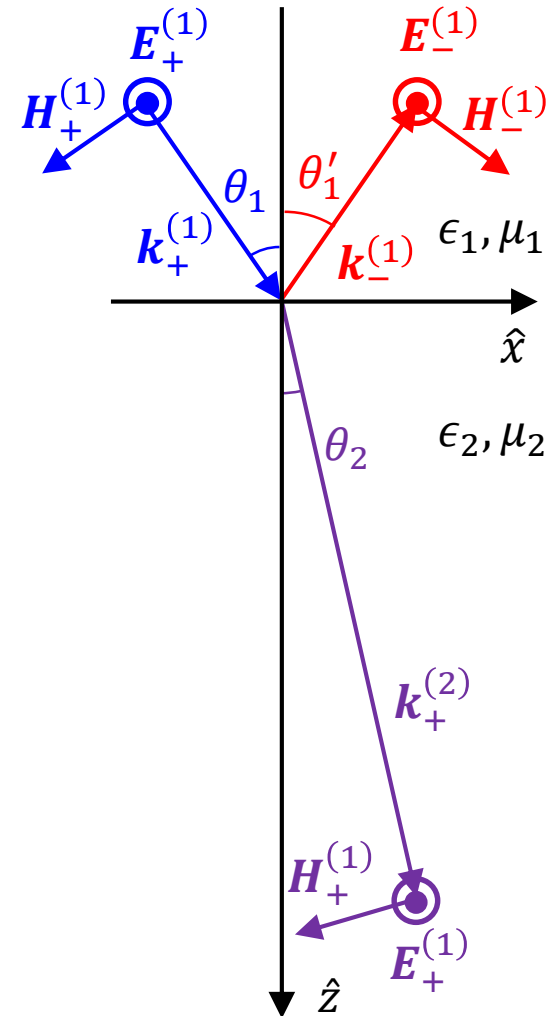
- Reflection coefficient: $\Gamma \equiv E_-^{(1)} / E_+^{(1)}$

- Transmission coefficient: $T \equiv E_+^{(2)} / E_+^{(1)}$

- $$1 + \Gamma = T$$

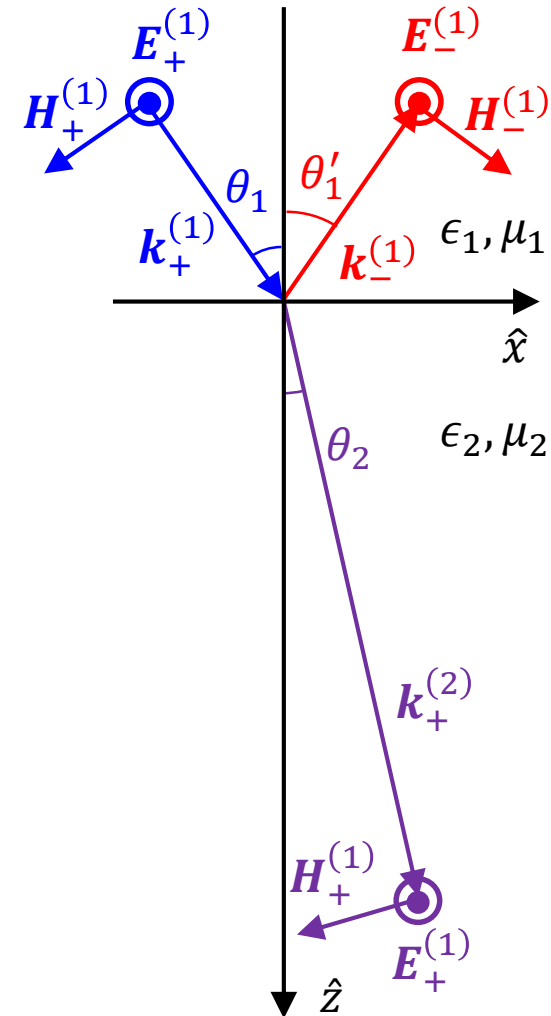
- $$\frac{1}{Z_0^{(1)}} (1 - \Gamma) = \frac{1}{Z_0^{(2)}} T$$

$$\rightarrow T = \frac{2Z_0^{(2)}}{Z_0^{(2)} + Z_0^{(1)}}, \Gamma = \frac{Z_0^{(2)} - Z_0^{(1)}}{Z_0^{(2)} + Z_0^{(1)}}$$



(Haus) 2.1 TE Wave Reflected from Boundary

- $Z_0^{(1)} \equiv \frac{\omega \mu_1}{k_z^{(1)}} = \sqrt{\frac{\mu_1}{\epsilon_1}} \frac{1}{\cos \theta_1} \rightarrow \frac{Z_0^{(1)}}{Z_0^{(2)}} = \frac{\omega \mu_1 / k_z^{(1)}}{\omega \mu_2 / k_z^{(2)}} = \frac{\mu_1 k_z^{(2)}}{\mu_2 k_z^{(1)}}$
- $\Gamma = \frac{Z_0^{(2)} - Z_0^{(1)}}{Z_0^{(2)} + Z_0^{(1)}} = \frac{1 - Z_0^{(1)} / Z_0^{(2)}}{1 + Z_0^{(1)} / Z_0^{(2)}} = \frac{1 - (\mu_1 k_z^{(2)}) / (\mu_2 k_z^{(1)})}{1 + (\mu_1 k_z^{(2)}) / (\mu_2 k_z^{(1)})}$
- $T = \frac{2Z_0^{(2)}}{Z_0^{(2)} + Z_0^{(1)}} = \frac{2}{1 + Z_0^{(1)} / Z_0^{(2)}} = \frac{2}{1 + (\mu_1 k_z^{(2)}) / (\mu_2 k_z^{(1)})}$
- $\Gamma = \frac{1/Z_0^{(1)} - 1/Z_0^{(2)}}{1/Z_0^{(1)} + 1/Z_0^{(2)}} = \frac{\sqrt{\epsilon_1/\mu_1} \cos \theta_1 - \sqrt{\epsilon_2/\mu_2} \cos \theta_2}{\sqrt{\epsilon_1/\mu_1} \cos \theta_1 + \sqrt{\epsilon_2/\mu_2} \cos \theta_2}$
- Using $n = \sqrt{\epsilon/\epsilon_0}$ assuming $\mu_1 \approx \mu_2 \approx \mu_0$,
- $\Gamma = \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2}$
- From Snell's law $n_1 \sin \theta_1 = n_2 \sin \theta_2$,
 - $\sin \theta_2 = \frac{n_1}{n_2} \sin \theta_1$ or $\cos \theta_2 = \sqrt{1 - \left(\frac{n_1}{n_2}\right)^2 \sin^2 \theta_1}$
 - $n_2 \cos \theta_2 = \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}$
- $\Gamma = \frac{n_1 \cos \theta_1 - \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}{n_1 \cos \theta_1 + \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}, T = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}$





Power Flow

- $\mathbf{S} = \mathbf{E} \times \mathbf{H}^*$
- Density of power flow along z-axis: $S_z = E_x H_y^* - E_y H_x^*$
- Reflectance: ratio of the reflected to incident power flow
 - $r = -\hat{z} \cdot \mathbf{S}_{-}^{(1)} / \hat{z} \cdot \mathbf{S}_{+}^{(1)}$
 - $r = E_{y-}^{(1)} H_{x-}^{(1)*} / (-E_{y+}^{(1)} H_{x+}^{(1)*})$
 - $r = \left(\Gamma E_{y+}^{(1)} \right) \left(\frac{1}{Z_0^{(1)}} \Gamma E_{y+}^{(1)} \right)^* / \left(-E_{y+}^{(1)} \cdot \left(\frac{-1}{Z_0^{(1)}} E_{y+}^{(1)} \right)^* \right) = |\Gamma|^2$
- Transmittance: ratio of the transmitted to incident power flow
 - $t = \hat{z} \cdot \mathbf{S}_{+}^{(2)} / \hat{z} \cdot \mathbf{S}_{+}^{(1)}$
 - $t = (-E_{y+}^{(2)} H_{x+}^{(2)*}) / (-E_{y+}^{(1)} H_{x+}^{(1)*})$
 - $t = \left(T E_{y+}^{(1)} \right) \left(\frac{-1}{Z_0^{(2)}} T E_{y+}^{(1)} \right)^* / \left(E_{y+}^{(1)} \cdot \left(\frac{-1}{Z_0^{(1)}} E_{y+}^{(1)} \right)^* \right) = |T|^2 \frac{Z_0^{(1)}}{Z_0^{(2)}}$

Signs of Γ and T

- For TE waves,

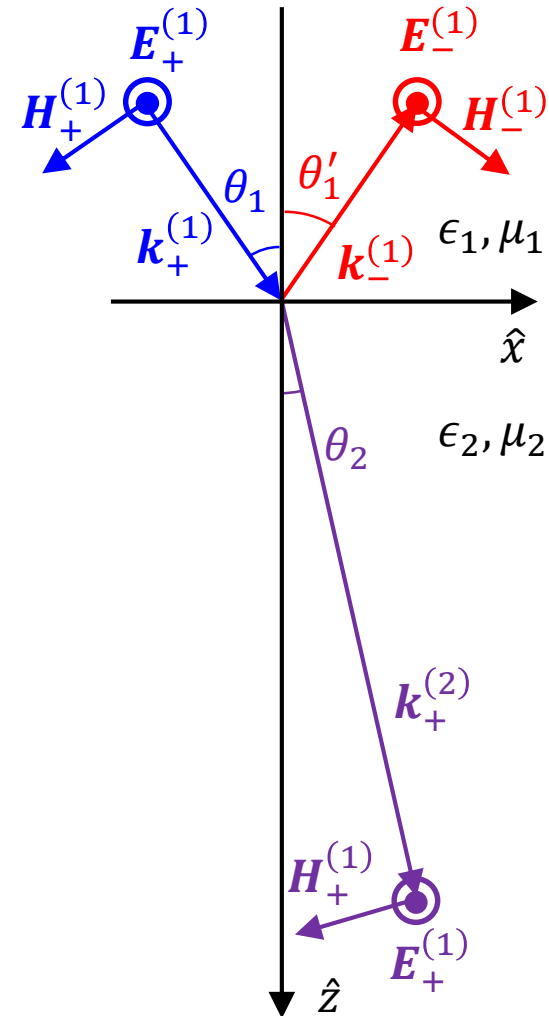
$$\Gamma = \frac{n_1 \cos \theta_1 - \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}{n_1 \cos \theta_1 + \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}, T = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}$$

- Sign of Γ

- Consider $n_2^2 - n_1^2 \sin^2 \theta_1 > 0$ case
- $(n_1 \cos \theta_1)^2 - (n_2^2 - n_1^2 \sin^2 \theta_1) = n_1^2 - n_2^2$
- If $n_1 < n_2$, medium 2 is called more dense
 - Reflection coefficient $\Gamma < 0 \rightarrow \mathbf{E}_{-}^{(1)} = \Gamma \mathbf{E}_{+}^{(1)}$
 - \rightarrow the phase of reflected beam is shifted by 180°
 - Propagation from 2 to 1 should be in-phase

- Sign of T

- $\mathbf{E}_{+}^{(2)} = T \mathbf{E}_{+}^{(1)} \rightarrow$ transmission is always in-phase



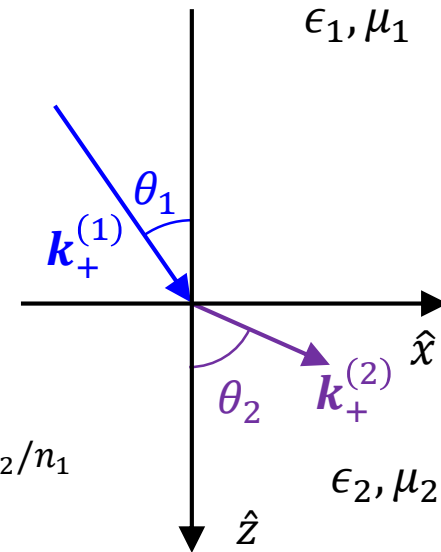
(Haus) 2.3 Total Internal Reflection

- For TE waves,

$$\Gamma = \frac{n_1 \cos \theta_1 - \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}{n_1 \cos \theta_1 + \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}, T = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}$$

- $n_2^2 - n_1^2 \sin^2 \theta_1 < 0$?

- It can happen only when $n_1 > n_2$.
- Ex) seen from inside of water \rightarrow total internal reflection (TIR)
- Snell's law $n_1 \sin \theta_1 = n_2 \sin \theta_2 \rightarrow \sin \theta_2 = \frac{n_1}{n_2} \sin \theta_1$
 \rightarrow problem when θ_1 becomes larger than the critical angle $\sin \theta_c = n_2/n_1$
- Interpretation with wave vectors
 - $k^2 = \omega^2 \mu \epsilon = \omega^2 \frac{1}{v^2} \rightarrow k = \frac{\omega}{v} = \frac{\omega}{c/n} = k_0 n$
 - $n_1 > n_2 \rightarrow k^{(1)} = k_0 n_1 > k^{(2)} = k_0 n_2$
- From boundary condition: $k_{x+}^{(1)} = k_{x+}^{(2)}$
 - When θ_1 becomes larger than $\sin \theta_c = n_2/n_1$, $k_{x+}^{(2)} > k^{(2)}$
 - From $k^{(2)} = \sqrt{(k_{x+}^{(2)})^2 + (k_{z+}^{(2)})^2}$,
 - $k_{z+}^{(2)}$ should become imaginary $k_{z+}^{(2)} = \pm \sqrt{(k^{(2)})^2 - (k_{x+}^{(2)})^2} = \pm j \alpha_z^{(2)}$



Phases of Γ and T

- For TE waves,

$$\Gamma = \frac{n_1 \cos \theta_1 - \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}}{n_1 \cos \theta_1 + \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}} = \frac{1/Z_0^{(1)} - 1/Z_0^{(2)}}{1/Z_0^{(1)} + 1/Z_0^{(2)}} = \frac{Y_0^{(1)} - Y_0^{(2)}}{Y_0^{(1)} + Y_0^{(2)}}$$

$$T = \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + \sqrt{n_2^2 - n_1^2 \sin^2 \theta_1}} = \frac{2/Z_0^{(1)}}{1/Z_0^{(1)} + 1/Z_0^{(2)}} = \frac{2Y_0^{(1)}}{Y_0^{(1)} + Y_0^{(2)}}$$

- Reflection coefficient

$$\Gamma = \frac{Y_0^{(1)} - jX_0^{(2)}}{Y_0^{(1)} + jX_0^{(2)}} = \frac{|A|e^{j\phi}}{|A|e^{-j\phi}} = e^{j2\phi} \rightarrow |\Gamma| = 1, \arg \Gamma = 2\phi(\theta_1, n_1, n_2)$$

- $\mathbf{E}_-^{(1)} = \Gamma \mathbf{E}_+^{(1)} \rightarrow$ the phase shift of reflected beam is determined by θ_1
 \rightarrow homework about Fresnel rohm phase retarder

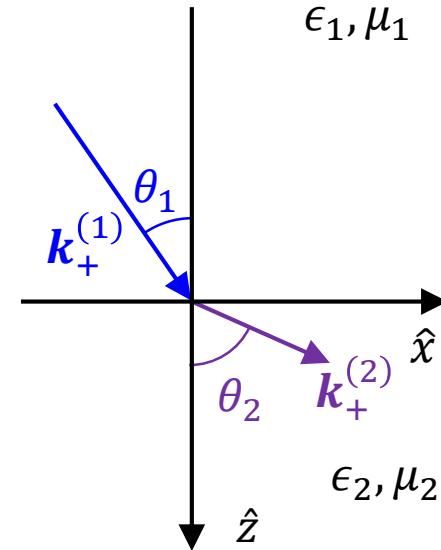
- Transmitted wave

$$T = \frac{2Y_0^{(1)}}{Y_0^{(1)} + jX_0^{(2)}} = |T|e^{j\phi}$$

$$\text{With } k_{x+}^{(1)} = k_{x+}^{(2)} = k_x \text{ and } k_{z+}^{(2)} = \sqrt{(k^{(2)})^2 - (k_x)^2} = -j\alpha_z^{(2)}$$

$$E_y^{(2)} = E_+^{(2)} e^{-jk_z^{(2)}z} e^{-jk_x x} = TE_+^{(1)} e^{-j(-j\alpha_z^{(2)})z} e^{-jk_x x} = |T|e^{j\phi} E_+^{(1)} e^{-\alpha_z^{(2)}z} e^{-jk_x x}$$

$$H_x^{(2)} = -\frac{k_z^{(2)}}{\omega\mu} E_+^{(2)} e^{-jk_z^{(2)}z} e^{-jk_x x} = \frac{\alpha_z^{(2)}}{\omega\mu} |T|e^{j\phi} E_+^{(1)} e^{-\alpha_z^{(2)}z} e^{-jk_x x}$$



(Haus) 2.2 TM Wave Reflected from Boundary

■ Transverse magnetic wave reflected from boundary

- Consider a plane wave with H -field polarized parallel to the surface of an interface between two media

- $\mathbf{H}_+^{(1)} \parallel \mathbf{H}_-^{(1)} \parallel \mathbf{H}_+^{(2)}$

- $k_{x+}^{(1)} = k_{x-}^{(1)} = k_{x+}^{(2)} = k_x$, $k_{z+}^{(1)} = k_{z-}^{(1)} = k_z^{(1)}$

- Region 1

- $H_y^{(1)} = \left(H_+^{(1)} e^{-jk_z^{(1)} z} + H_-^{(1)} e^{jk_z^{(1)} z} \right) e^{-jk_x x}$

- Ampere's law $\nabla \times \mathbf{H} = j\omega\epsilon\mathbf{E} \rightarrow E_x = \frac{1}{j\omega\epsilon} (-\partial_z H_y)$

- $E_x^{(1)} = \frac{k_z^{(1)}}{\omega\epsilon} \left(H_+^{(1)} e^{-jk_z^{(1)} z} - H_-^{(1)} e^{jk_z^{(1)} z} \right) e^{-jk_x x}$

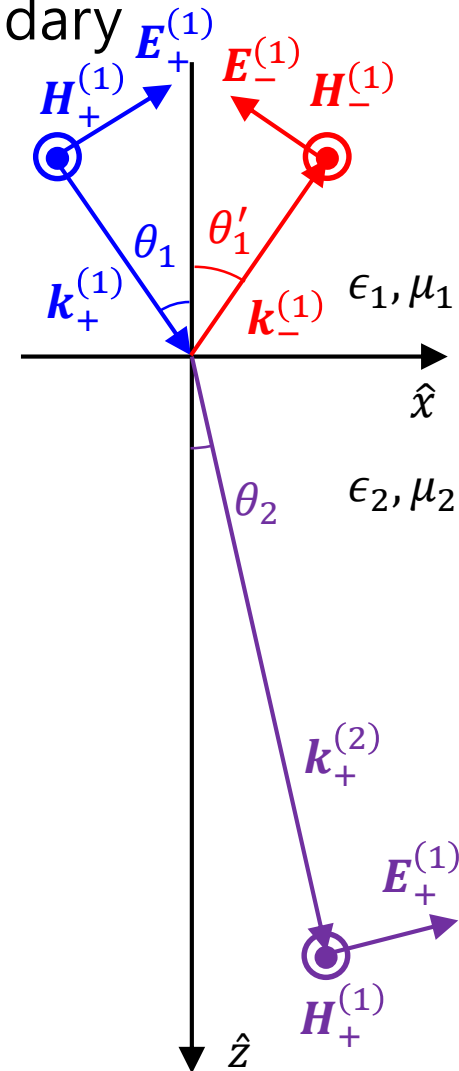
- Region 2

- $H_y^{(2)} = H_+^{(2)} e^{-jk_z^{(2)} z} e^{-jk_x x}$

- $E_x^{(2)} = \frac{k_z^{(2)}}{\omega\epsilon} H_+^{(2)} e^{-jk_z^{(2)} z} e^{-jk_x x}$

- **Characteristic impedance** presented by medium 1 to a TM wave at inclination θ_1 with respect to the z axis:

- For TM, $Z_0^{(1)} \equiv \frac{k_z^{(1)}}{\omega\epsilon} = \frac{\omega\sqrt{\epsilon\mu} \cos \theta_1}{\omega\epsilon} = \sqrt{\frac{\mu}{\epsilon}} \cos \theta_1 \sim \frac{E_x}{H_y}$



(Haus) 2.2 TM Wave Reflected from Boundary

Region 1

- $H_y^{(1)} = (H_+^{(1)} e^{-jk_z^{(1)} z} + H_-^{(1)} e^{jk_z^{(1)} z}) e^{-jk_x x}$
- $E_x^{(1)} = \frac{k_z^{(1)}}{\omega \epsilon} (H_+^{(1)} e^{-jk_z^{(1)} z} - H_-^{(1)} e^{jk_z^{(1)} z}) e^{-jk_x x}$

Region 2

- $H_y^{(2)} = H_+^{(2)} e^{-jk_z^{(2)} z} e^{-jk_x x}$
- $E_x^{(2)} = \frac{k_z^{(2)}}{\omega \epsilon} H_+^{(2)} e^{-jk_z^{(2)} z} e^{-jk_x x}$

- Characteristic impedance of TM: $Z_0^{(1)} \equiv \frac{k_z^{(1)}}{\omega \epsilon_1} = \sqrt{\frac{\mu_1}{\epsilon_1}} \cos \theta_1$

- At $z = 0$ for all x values, $H_y^{(1)} = H_y^{(2)}$, $E_x^{(1)} = E_x^{(2)}$

- $H_+^{(1)} + H_-^{(1)} = H_+^{(2)}$
- $Z_0^{(1)} (H_+^{(1)} - H_-^{(1)}) = Z_0^{(2)} H_+^{(2)}$

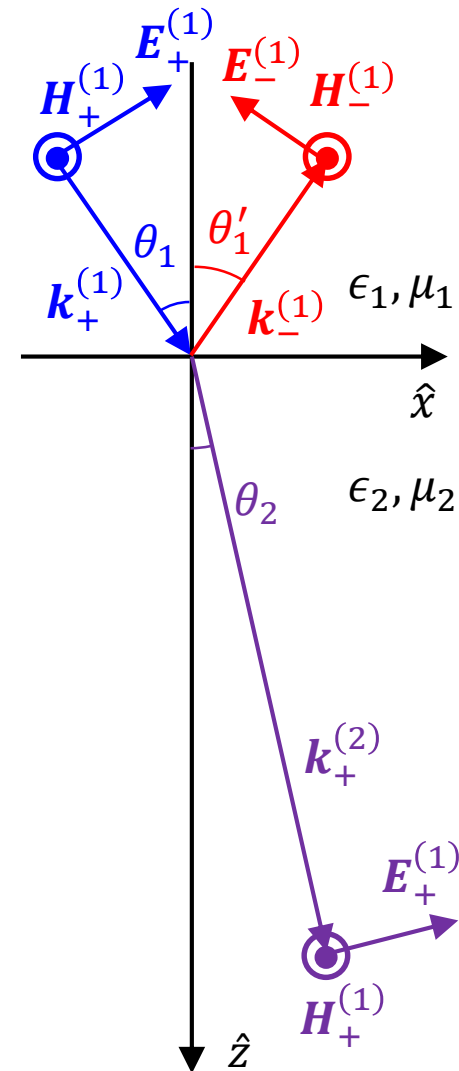
- Reflection coefficient of TM: $\Gamma^{\text{TM}} \equiv -H_-^{(1)} / H_+^{(1)}$

- Transmission coefficient: $T^{\text{TM}} \equiv H_+^{(2)} / H_+^{(1)}$

- $1 - \Gamma = T$

- $Z_0^{(1)} (1 + \Gamma) = Z_0^{(2)} T$

$$\rightarrow T = \frac{2Z_0^{(1)}}{Z_0^{(2)} + Z_0^{(1)}}, \Gamma = \frac{Z_0^{(2)} - Z_0^{(1)}}{Z_0^{(2)} + Z_0^{(1)}}$$



Duality

■ Duality

$$(i) \quad \nabla \cdot \mathbf{E}(\mathbf{r}) = 0 \quad (ii) \quad \nabla \times \mathbf{E}(\mathbf{r}) = -j\omega\mu\mathbf{H}(\mathbf{r})$$

$$(iii) \quad \nabla \cdot \mathbf{H}(\mathbf{r}) = 0 \quad (iv) \quad \nabla \times \mathbf{H}(\mathbf{r}) = j\omega\epsilon\mathbf{E}(\mathbf{r})$$

$$\square \quad \mathbf{E} \rightarrow \mathbf{H}, \quad \mathbf{H} \rightarrow -\mathbf{E}, \quad \mu \Leftrightarrow \epsilon$$

■ Transverse Electric wave

$$\square \quad Z_0^{(1)} \equiv \frac{\omega\mu_1}{k_z^{(1)}} = \sqrt{\frac{\mu_1}{\epsilon_1}} \frac{1}{\cos\theta_1}$$

$$\rightarrow \frac{Z_0^{(1)}}{Z_0^{(2)}} = \frac{\omega\mu_1/k_z^{(1)}}{\omega\mu_2/k_z^{(2)}} = \frac{\mu_1 k_z^{(2)}}{\mu_2 k_z^{(1)}}$$

$$\square \quad \Gamma^{\text{TE}} = \frac{Z_0^{(2)} - Z_0^{(1)}}{Z_0^{(2)} + Z_0^{(1)}} = \frac{1 - Z_0^{(1)}/Z_0^{(2)}}{1 + Z_0^{(1)}/Z_0^{(2)}} \\ = \frac{1 - (\mu_1 k_z^{(2)}) / (\mu_2 k_z^{(1)})}{1 + (\mu_1 k_z^{(2)}) / (\mu_2 k_z^{(1)})}$$

$$\square \quad T^{\text{TE}} = \frac{2Z_0^{(2)}}{Z_0^{(2)} + Z_0^{(1)}} = \frac{2}{1 + Z_0^{(1)}/Z_0^{(2)}} \\ = \frac{2}{1 + (\mu_1 k_z^{(2)}) / (\mu_2 k_z^{(1)})}$$

■ Transverse Magnetic wave

$$\square \quad Z_0^{(1)} \equiv \frac{k_z^{(1)}}{\omega\epsilon_1} = \sqrt{\frac{\mu_1}{\epsilon_1}} \cos\theta_1$$

$$\rightarrow \frac{Z_0^{(2)}}{Z_0^{(1)}} = \frac{k_z^{(2)}/\omega\epsilon_2}{k_z^{(1)}/\omega\epsilon_1} = \frac{\epsilon_1 k_z^{(2)}}{\epsilon_2 k_z^{(1)}}$$

$$\square \quad -\Gamma^{\text{TM}} = \frac{Z_0^{(1)} - Z_0^{(2)}}{Z_0^{(1)} + Z_0^{(2)}} = \frac{1 - Z_0^{(2)}/Z_0^{(1)}}{1 + Z_0^{(2)}/Z_0^{(1)}} \\ = \frac{1 - (\epsilon_1 k_z^{(2)}) / (\epsilon_2 k_z^{(1)})}{1 + (\epsilon_1 k_z^{(2)}) / (\epsilon_2 k_z^{(1)})}$$

$$\square \quad T^{\text{TM}} = \frac{2Z_0^{(1)}}{Z_0^{(2)} + Z_0^{(1)}} = \frac{2}{1 + Z_0^{(2)}/Z_0^{(1)}} \\ = \frac{2}{1 + (\epsilon_1 k_z^{(2)}) / (\epsilon_2 k_z^{(1)})}$$

Brewster's Angle

- Transverse Electric field
 - Define $\beta \equiv \frac{n_2}{n_1}$
 - For $\Gamma^{\text{TE}} = \frac{Z_0^{(2)} - Z_0^{(1)}}{Z_0^{(2)} + Z_0^{(1)}}$ to become zero, $Z_0^{(2)} = Z_0^{(1)}$
 - ➔ $\sqrt{\frac{\mu_1}{\epsilon_1}} \frac{1}{\cos \theta_1} = \sqrt{\frac{\mu_2}{\epsilon_2}} \frac{1}{\cos \theta_2} \rightarrow \sqrt{\epsilon_1} \cos \theta_1 = \sqrt{\epsilon_2} \cos \theta_2$
 - ➔ $\cos \theta_2 = \frac{\sqrt{\epsilon_1}}{\sqrt{\epsilon_2}} \cos \theta_1 = \left(\frac{n_1}{n_2}\right) \cos \theta_1 = \frac{1}{\beta} \cos \theta_1$
 - Snell's law $\sin \theta_2 = \left(\frac{n_1}{n_2}\right) \sin \theta_1 = \frac{1}{\beta} \sin \theta_1$
 - $1 = \cos^2 \theta_2 + \sin^2 \theta_2 = \frac{1}{\beta^2} \cos^2 \theta_2 + \frac{1}{\beta^2} \sin^2 \theta_2 = \frac{1}{\beta^2}$
 - $\beta = 1 \rightarrow$ impossible with two different materials
- Transverse Magnetic field
 - For $\Gamma^{\text{TM}} = \frac{Z_0^{(2)} - Z_0^{(1)}}{Z_0^{(2)} + Z_0^{(1)}}$ to become zero, $Z_0^{(2)} = Z_0^{(1)}$
 - ➔ $\sqrt{\frac{\mu_1}{\epsilon_1}} \cos \theta_1 = \sqrt{\frac{\mu_2}{\epsilon_2}} \cos \theta_2 \rightarrow \frac{1}{\sqrt{\epsilon_1}} \cos \theta_1 = \frac{1}{\sqrt{\epsilon_2}} \cos \theta_2$
 - ➔ $\cos \theta_2 = \left(\frac{n_2}{n_1}\right) \cos \theta_1 = \beta \cos \theta_1$
 - ➔ $1 = \cos^2 \theta_2 + \sin^2 \theta_2 = \beta^2 \cos^2 \theta_1 + \frac{1}{\beta^2} \sin^2 \theta_1$
 - ➔ $\beta^2 = \beta^4 \cos^2 \theta_1 + (1 - \cos^2 \theta_1)$
 - ➔ $\beta^2 - 1 = (\beta^4 - 1) \cos^2 \theta_1$
 - ➔ $\cos^2 \theta_1 = \frac{1}{\beta^2 + 1} \rightarrow 1 + \tan^2 \theta_1 = \frac{1}{\cos^2 \theta_1} = 1 + \beta^2$
 - ➔ $\tan \theta_B = \frac{n_2}{n_1}$

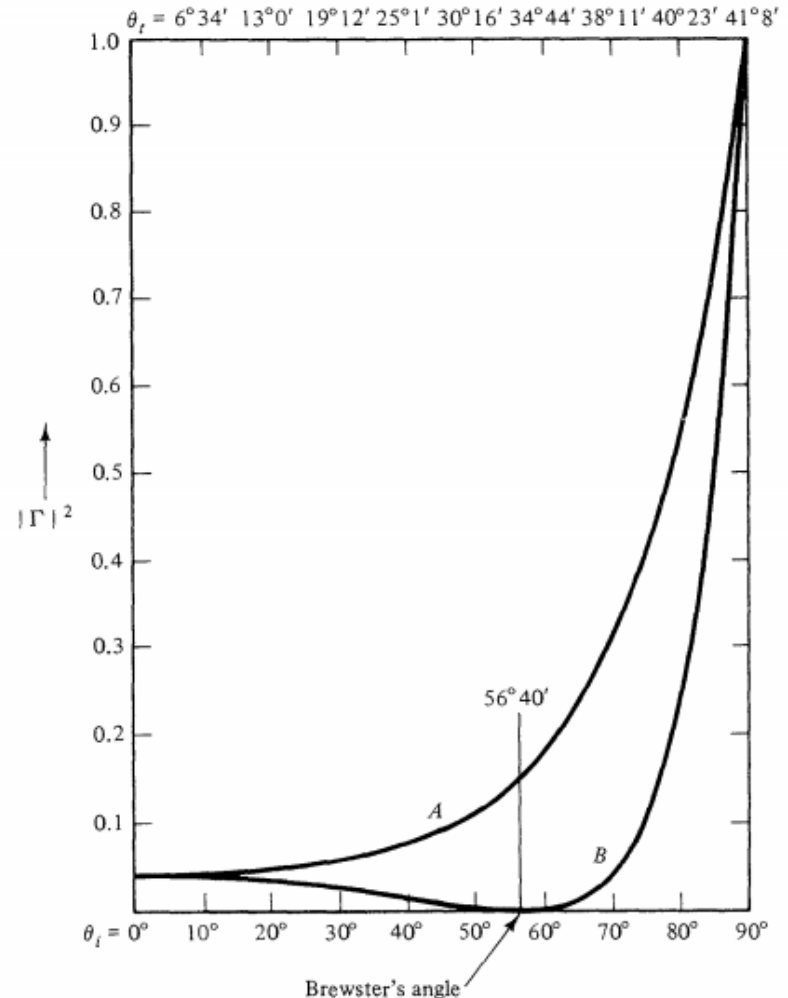


Figure 2.2 Square of reflection coefficient as a function of the angle of incidence: (a) curve A, TE; (b) curve B, TM. $n = 1.52$ index of glass. (After O. D. Chwolson, *Lehrbuch der Physik*, Vol. II, No. 2, 2nd ed., Braunschweig, Vieweg, 1922, p. 716.)