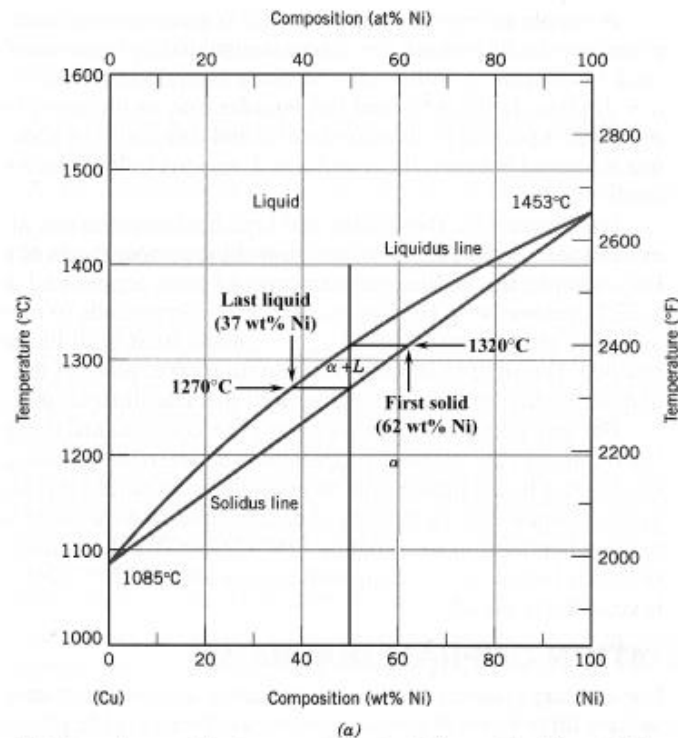


9.8 A 50 wt% Ni–50 wt% Cu alloy is slowly cooled from 1400°C to 1200°C.

- At what temperature does the first solid phase form?
- What is the composition of this solid phase?
- At what temperature does the liquid solidify?
- What is the composition of this last remaining liquid phase?

Solution

Shown below is the Cu–Ni phase diagram (Figure 10.3a) and a vertical line constructed at a composition of 50 wt% Ni–50 wt% Cu.



- The first solid phase forms at the temperature at which a vertical line at this composition intersects the  $L-(\alpha + L)$  phase boundary—i.e., at about 1320°C.
- The composition of this solid phase corresponds to the intersection with the  $L-(\alpha + L)$  phase boundary, of a tie line constructed across the  $\alpha + L$  phase region at 1320°C—i.e.,  $C_{\alpha} = 62$  wt% Ni–38 wt% Cu.
- Complete solidification of the alloy occurs at the intersection of this same vertical line at 50 wt% Ni with the  $(\alpha + L)-\alpha$  phase boundary—i.e., at about 1270°C.
- The composition of the last liquid phase remaining prior to complete solidification corresponds to the intersection with the  $L-(\alpha + L)$  boundary, of the tie line constructed across the  $\alpha + L$  phase region at 1270°C—i.e.,  $C_L$  is about 37 wt% Ni–63 wt% Cu.

9.21 For a lead–tin alloy of composition 80 wt% Sn–20 wt% Pb and at 180°C, do the following:

- (a) Determine the mass fractions of the  $\alpha$  and  $\beta$  phases.
- (b) Determine the mass fractions of primary  $\beta$  and eutectic microconstituents.
- (c) Determine the mass fraction of eutectic  $\beta$ .

Solution

(a) This portion of the problem asks that we determine the mass fractions of  $\alpha$  and  $\beta$  phases for an 80 wt% Sn–20 wt% Pb alloy (at 180°C). In order to do this, it is necessary to employ the lever rule using a tie line that extends entirely across the  $\alpha + \beta$  phase field. From Figure 9.8 and at 180°C,  $C_\alpha = 18.3$  wt% Sn,  $C_\beta = 97.8$  wt% Sn, and  $C_{\text{eutectic}} = 61.9$  wt% Sn. Therefore, the two lever-rule expressions are as follows:

$$W_\alpha = \frac{C_\beta - C_0}{C_\beta - C_\alpha} = \frac{97.8 - 80}{97.8 - 18.3} = 0.224$$

$$W_\beta = \frac{C_0 - C_\alpha}{C_\beta - C_\alpha} = \frac{80 - 18.3}{97.8 - 18.3} = 0.776$$

(b) Now it is necessary to determine the mass fractions of primary  $\beta$  and eutectic microconstituents for this same alloy. This requires that we utilize the lever rule and a tie line that extends from the maximum solubility of Pb in the  $\beta$  phase at 180°C (i.e., 97.8 wt% Sn) to the eutectic composition (61.9 wt% Sn). Thus, mass fractions of primary  $\beta$  and eutectic microconstituents (denoted by  $W_{\beta'}$  and  $W_e$ , respectively) are determined using the following lever-rule expressions:

$$W_{\beta'} = \frac{C_0 - C_{\text{eutectic}}}{C_\beta - C_{\text{eutectic}}} = \frac{80.0 - 61.9}{97.8 - 61.9} = 0.504$$

$$W_e = \frac{C_\beta - C_0}{C_\beta - C_{\text{eutectic}}} = \frac{97.8 - 80.0}{97.8 - 61.9} = 0.496$$

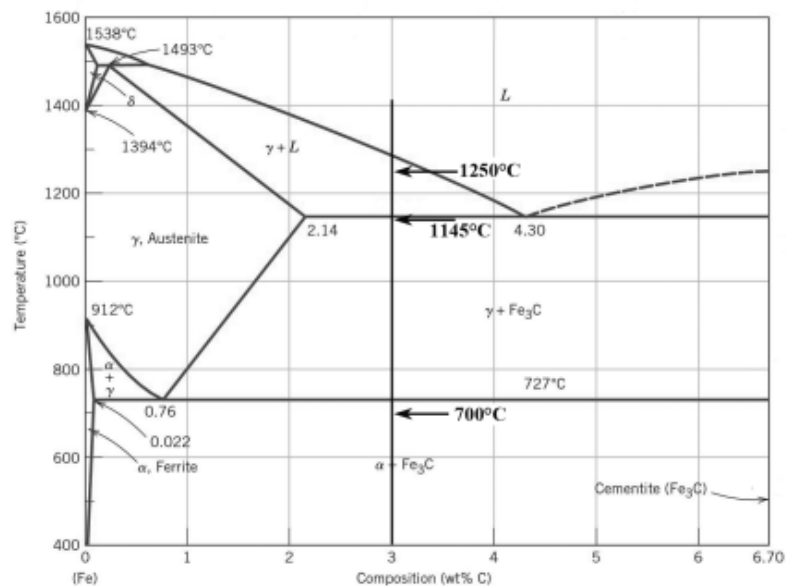
(c) And, finally, we are asked to compute the mass fraction of eutectic  $\beta$ ,  $W_{e\beta}$ . This quantity is simply the difference between the mass fractions of total  $\beta$  and primary  $\beta$  as follows:

$$\begin{aligned} W_{e\beta} &= W_\beta - W_{\beta'} \\ &= 0.776 - 0.504 = 0.272 \end{aligned}$$

9.43 For an iron-carbon alloy of composition 3 wt% C–97 wt% Fe, make schematic sketches of the microstructure that would be observed for conditions of very slow cooling at the following temperatures: 1250°C, 1145°C, and 700°C. Label the phases and indicate their compositions (approximate).

Solution

Below is shown the Fe-Fe<sub>3</sub>C phase diagram with a vertical line constructed at 3 wt% C; also along this line noted temperatures of 1250°C, 1145°C, and 700°C.



Schematic microstructures for this iron-carbon alloy at the three temperatures are shown below; approximate phase compositions are also indicated.