

I. Problem:

Moment-Curvature relationship curve of a reinforced concrete beam of different cases with parameters as follows:

General Cases

Cases	As	As'
Case 1	Asb	0
Case 2	0.5Asb	0
Case 3	Asb	0.5Asb

Beam Properties

Property	Value	Unit
f'c	21	MPa
fy	275	MPa
$f_r = 0.7 \sqrt{f'c}$	3.208	MPa
Es	200,000	MPa
$E_c = (4,700 \sqrt{f'c})$	21538.10	MPa
β_1	0.85	
$\eta = E_s / E_c$	9.28	
b (beam width)	300	mm
h (beam height)	450	mm
d (effective depth)	400	mm
d' (compression steel location)	50	mm

II. Solutions / Methodology

As a general solution to the problem, analysis as doubly reinforced beam is applied to address all the cases (singly or doubly reinforced). The following are the steps used:

1. Compute for the balanced steel at tension.

$$Asb = 4,539.92mm^2$$

2. Steel area is assigned to both tension and compression side as indicated in the general cases.
3. For the 3 stages of the behavior of the beam:

Stage 1 : Cracking point of concrete in tension

1. Neutral axis location (kd) from the compression fiber of concrete is calculated by transforming area of steel to area of concrete using the modular ratio η :

a. Uncrack section (Case 1 : Doubly Reinforced)

Particulars	Calculated Values
$As(transformed) = (\eta - 1)As$	37,617.24 mm^2
$As'(transformed) = (\eta - 1)As'$	18,808.62 mm^2
By taking moment of areas of concrete and steel to topmost fiber:	
kd	242.19 mm

2. Calculation of M_{cr} and ϕ_{cr}

Particulars	Calculated Values
I_{cr}	$3.949 \times 10^9 mm^4$
$M_{cr} = fr \frac{I_{cr}}{h - kd}$	$60.97 \times 10^6 kN - m$
$\phi_{cr} = \frac{fr}{Ec * (h - kd)}$	$7.167e - 07 rad/mm$

3. Calculate the curvature ϕ_c right after cracking

The neutral axis will shift after the crack, so taking moment of area for transformed steel in tension (ηAs) and compression ($(\eta - 1)As$) and concrete at the compressive area into the neutral axis:

$$b * kd * \frac{kd}{2} + (\eta - 1)As' * (kd - d') = \eta As(d - kd) \quad (1)$$

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# Imports
from sympy import *
import math
import matplotlib.pyplot as plt

# Define parameters
b = 300                                     # Beam width
h = 450                                     # Beam height
clearance = 50                             # Clearance from tension steel to bottom of
concrete                                   # d - Effective depth
d = h - clearance                          # d' - Distance from compression steel to concrete
d_prime = 50                               compression fiber
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fcprime = 21 # f'c - Concrete compressive strength
fy = 275 # fy - Steel tensile strength
fr = 0.7 * math.sqrt(fcprime) # Modulus of fracture
Es = 200000 # Modulus of elasticity of steel
Ec = 4700 * math.sqrt(fcprime) # Modulus of elasticity of concrete
β1 = 0.85 # Beta
η = Es / Ec # Modular ratio

# As balance
pb = (0.85 * fcprime * β1 * 600) / (fy * (600 + fy)) # Balance concret-steel ratio
Asb = pb * b * d # As balance

# Cases
As = [Asb, 0.5*Asb, Asb] # Tension reinforcements
AsPrime = [0.0, 0.0, 0.5*Asb] # Compression reinforcements

# Data holders
M = ([], [], []) # Array of moments for the 3 cases
φ = ([], [], []) # Array of curvature for the 3 cases
I = ([], [], []) # Array of all computed moment of inertias
kd = ([], [], []) # Array of values of neutral axis to compression
fiber
fsm = ([], [], []) # Array of strains in concrete
yield_pts = []

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# =====
# Utilities
# =====
def solveLo(case_no, λ):
    if case_no == 1:
        return 0.85 / 3 * λ * (3 - λ)
    else:
        return 0.85 * (3*λ - 1) / (3 * λ)

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# Insert initial values for moment and curvature
for i in range(3):
    M[i].append(0.0)
    φ[i].append(0.0)

for i in range(3):
    print('=====')
    print('Case No.', i+1)
    print('=====')
    # ===== #
    # Calculation before cracking #
    # ===== #
    # Calculate for kd of each case
    At = b * h # Concrete alone
    At += (η-1) * As[i] # Concrete plus transformed
    tension steel
    At += (η-1) * AsPrime[i] # Plus transformed compression
    steel

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        Ma = (b * h) * (h / 2) # Moment of area of concrete to
compression fiber
        Ma += (η-1) * As[i] * d # Moment of tension reinf. to
compression fiber
        Ma += (η-1) * AsPrime[i] * d_prime # Moment of compression reinf.
to compression fiber
        kdCalculated = Ma / At
        kd[i].append(kdCalculated) # Insert to list of kd

# Calculate for moment of inertia of each case
Ic = (b * kdCalculated**3 / 12) + (b * kdCalculated * (kdCalculated / 2)**2)
Ic += (b * (h - kdCalculated)**3 / 12) + (b * (h - kdCalculated) * ((h -
kdCalculated) / 2)**2)
Ic += (η-1) * As[i] * (d - kdCalculated)**2
Ic += (η-1) * AsPrime[i] * (kdCalculated - d_prime)**2
I[i].append(Ic) # Insert to list of I

# Calculate the cracking moment
Mcr = fr * Ic / (h - kdCalculated) # Cracking moment
M[i].append(Mcr) # Insert to list of M

# Calculate the curvature
φc = fr / (Ec * (h - kdCalculated)) # Curvature right before
cracking
φ[i].append(φc) # Insert to list of φ
print('Mcr = ', round(Mcr / 1000**2, 2), 'φc = ', φc, 'kd = ', kdCalculated)

# ===== #
# Calculation after cracking #
# ===== #
# Finding the neutral axis using equilibrium of moment of areas
# b(kd)(kd/2) + (n-1)As'(kd-d') = nAs(d-kd)
# -- solve the quadratic equation
qa = b
qb = 2 * ((η-1) * AsPrime[i] + η * As[i])
qc = -2 * ((η-1) * AsPrime[i] * d_prime + η * As[i] * d)
qd = (qb**2) - (4 * qa * qc) # Discriminant
kdCalculated = (-1 * qb + math.sqrt(qd)) / (2 * qa) # Neutral axis after cracking
kd[i].append(kdCalculated)

# Calculate moment of inertia
Ic = (b * kdCalculated**3 / 12) + (b * kdCalculated * (kdCalculated / 2)**2)
Ic += (η) * As[i] * (d - kdCalculated)**2
Ic += (η-1) * AsPrime[i] * (kdCalculated - d_prime)**2
I[i].append(Ic)

# Calculate the curvature
φc = M[i][1] / (Ec * Ic) # Curvature right after
cracking

M[i].append(Mcr)
φ[i].append(φc)

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print('Mcr = ', round(Mcr / 1000**2, 2), 'φc = ', φc, 'kd = ', kdCalculated, "After
cracking...")

# ===== #
# Calculation at yield point #
# ===== #
fc = 0.5 * fcprime
εc = fc / Ec

qa = 0.5 * fc * b
qb = (Es * εc) * (AsPrime[i] + As[i])
qc = -(Es * εc) * (AsPrime[i] * d_prime + As[i] * d)
qd = (qb**2) - (4 * qa * qc) # Discriminant
kdCalculated = (-1 * qb + math.sqrt(qd)) / (2 * qa)

fs = (Es * εc) * (d - kdCalculated) / kdCalculated
fsPrime = Es * εc / kdCalculated * (kdCalculated - d_prime)
if fs > fy:
    fs = fy

if fsPrime > fy:
    fsPrime = fys

Mc = 0.5 * fc * b * kdCalculated * (d - kdCalculated / 3) + \
    AsPrime[i] * fsPrime * (d - d_prime)
φc = εc / kdCalculated

M[i].append(Mc)
φ[i].append(φc)
print('Myield = ', round(Mc / 1000**2, 2), 'φc = ', φc, 'εc = ', εc, 'kd = ',
kdCalculated)

yield_pts.append((φc*1000, Mc / 1000**2))

# ===== #
# Calculation at inelastic behaviour #
# ===== #
# Calculate for εo
εo = 2 * 0.85 * fcprime / Ec

# Iterator increment
iterator_increment = 0.0002

# For 0 < εc < εo
εc = 0.5 * εo # My setting for starting
strain iteration
print('For 0 < εc < εo')
# For case 0 < εc < εo
while (εc + iterator_increment) <= εo:
    εc = εc + iterator_increment
    λo = εc / εo
    k2 = 1 / 4 * (4 - λo) / (3 - λo)
    Lo = solveLo(1, λo)

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fc = 0.85 * fcprime * (2 * λo - λo**2)
kdCalculated = (As[i] - AsPrime[i]) * fy / (Lo * fc * b)
fs = (Es * εc) * (d - kdCalculated) / kdCalculated
fsPrime = Es * εc / kdCalculated * (kdCalculated - d_prime)

if fs >= fy:                                     # Tension steel yields
    # Solve for the stress in compression steel
    if fsPrime < fy:
        # Compression steel does not yields
        qa = Lo * fc * b
        qb = (Es * εc) * AsPrime[i] - As[i] * fy
        qc = -(Es * εc) * AsPrime[i] * d_prime
        qd = (qb**2) - (4 * qa * qc)              # Discriminant
        kdCalculated = (-1 * qb + math.sqrt(qd)) / (2 * qa)
        fs = (Es * εc) * (d - kdCalculated) / kdCalculated
        fsPrime = Es * εc / kdCalculated * (kdCalculated - d_prime)
        print('Tension steel yields but compression steel did not.')
    else:
        # fs and fs' > fy
        kdCalculated = (As[i] - AsPrime[i]) * fy / (Lo * fc * b)
        fs = fy
        fsPrime = fy
        print('Both tension and compression steel yields.')
else:
    print('Tension steel did not yield.')
    qa = Lo * fc * b
    qb = AsPrime[i] * fy + As[i] * Es * εc
    qc = -As[i] * Es * εc * d
    qd = (qb**2) - (4 * qa * qc)                  # Discriminant
    kdCalculated = (-1 * qb + math.sqrt(qd)) / (2 * qa)
    fs = (Es * εc) * (d - kdCalculated) / kdCalculated
    fsPrime = Es * εc / kdCalculated * (kdCalculated - d_prime)

Mc = Lo * fc * b * kdCalculated * (d - k2 * kdCalculated) + \
    AsPrime[i] * fsPrime * (d - d_prime)
φc = εc / kdCalculated

M[i].append(Mc)
φ[i].append(φc)

print('Mc = ', round(Mc / 1000**2, 2), 'φc = ', round(φc, 8), 'εc = ',
      round(εc, 5), 'kd = ', round(kdCalculated, 0), 'fc = ', fc)

print("For εo < εc < εcu")
# For case εo < εc < εcu
εc = εo + 0.0001
while (εc + iterator_increment) <= 0.003:
    εc = εc + iterator_increment
    ζc = εo / εc
    λo = 1 / ζc
    Lo = solveLo(2, λo)
    k2 = (6 * λo**2 - 4 * λo + 1) / (4 * λo * (3 * λo - 1))
    fc = 0.85 * fcprime

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kdCalculated = (As[i] - AsPrime[i]) * fy / (Lo * fc * b)
fs = (Es * εc) * (d - kdCalculated) / kdCalculated
fsPrime = Es * εc / kdCalculated * (kdCalculated - d_prime)

if fs >= fy:                                     # Tension steel yields
    # Solve for the stress in compression steel
    if fsPrime < fy:
        # Compression steel does not yields
        qa = Lo * fc * b
        qb = (Es * εc) * AsPrime[i] - As[i] * fy
        qc = -(Es * εc) * AsPrime[i] * d_prime
        qd = (qb**2) - (4 * qa * qc)                # Discriminant
        kdCalculated = (-1 * qb + math.sqrt(qd)) / (2 * qa)
        fs = (Es * εc) * (d - kdCalculated) / kdCalculated
        fsPrime = Es * εc / kdCalculated * (kdCalculated - d_prime)
        print('Tension steel yields but compression steel did not.')
    else:
        # fs and fs' > fy
        kdCalculated = (As[i] - AsPrime[i]) * fy / (Lo * fc * b)
        fs = fy
        fsPrime = fy
        print('Both tension and compression steel yields.')
else:
    print('Tension steel did not yield.')
    qa = Lo * fc * b
    qb = AsPrime[i] * fy + As[i] * Es * εc
    qc = -As[i] * Es * εc * d
    qd = (qb**2) - (4 * qa * qc)                # Discriminant
    kdCalculated = (-1 * qb + math.sqrt(qd)) / (2 * qa)
    fs = (Es * εc) * (d - kdCalculated) / kdCalculated
    fsPrime = Es * εc / kdCalculated * (kdCalculated - d_prime)

Mc = Lo * fc * b * kdCalculated * (d - k2 * kdCalculated) + \
    AsPrime[i] * fsPrime * (d - d_prime)
φc = εc / kdCalculated

print('Mc = ', round(Mc / 1000**2, 2), 'φc = ', round(φc, 8), 'εc = ',
round(εc, 5), 'kd = ', round(kdCalculated, 0), 'fc = ', fc)
φ[i].append(φc)
M[i].append(Mc)

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Case No. 1
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Mcr = 54.57 φc = 7.970318780711861e-07 kd = 263.13649515099587
Mcr = 54.57 φc = 1.0428634969669626e-06 kd = 223.02262969808856 After cracking...
Myield = 114.39 φc = 2.1859129421746513e-06 εc = 0.0004875080526548766 kd =
223.0226296980886
For 0 < εc < εo
Tension steel did not yield.
Mc = 153.69 φc = 3.95e-06 εc = 0.00103 kd = 261.0 fc = 15.281428223688067
Tension steel did not yield.
Mc = 187.86 φc = 4.76e-06 εc = 0.00123 kd = 258.0 fc = 16.655591741493783

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Tension steel did not yield.
 Mc = 216.42 ϕ_c = 5.52e-06 ϵ_c = 0.00143 kd = 259.0 fc = 17.509990553417143
 Tension steel did not yield.
 Mc = 237.47 ϕ_c = 6.23e-06 ϵ_c = 0.00163 kd = 261.0 fc = 17.844624659458155
 For $\epsilon_o < \epsilon_c < \epsilon_{cu}$
 Tension steel did not yield.
 Mc = 259.5 ϕ_c = 7.3e-06 ϵ_c = 0.00196 kd = 268.0 fc = 17.849999999999998
 Tension steel did not yield.
 Mc = 269.74 ϕ_c = 7.93e-06 ϵ_c = 0.00216 kd = 272.0 fc = 17.849999999999998
 Tension steel did not yield.
 Mc = 278.35 ϕ_c = 8.54e-06 ϵ_c = 0.00236 kd = 276.0 fc = 17.849999999999998
 Tension steel did not yield.
 Mc = 285.68 ϕ_c = 9.14e-06 ϵ_c = 0.00256 kd = 280.0 fc = 17.849999999999998
 Tension steel did not yield.
 Mc = 292.0 ϕ_c = 9.73e-06 ϵ_c = 0.00276 kd = 283.0 fc = 17.849999999999998
 Tension steel did not yield.
 Mc = 297.51 ϕ_c = 1.032e-05 ϵ_c = 0.00296 kd = 287.0 fc = 17.849999999999998

Case No. 2

Mcr = 43.86 ϕ_c = 7.315136942596765e-07 kd = 246.40002452244482
 Mcr = 43.86 ϕ_c = 1.27052110091158e-06 kd = 177.01582310560858 After cracking...
 Myield = 95.07 ϕ_c = 2.7540365832947417e-06 ϵ_c = 0.0004875080526548766 kd = 177.01582310560858
 For $0 < \epsilon_c < \epsilon_o$
 Tension steel did not yield.
 Mc = 132.65 ϕ_c = 4.82e-06 ϵ_c = 0.00103 kd = 213.0 fc = 15.281428223688067
 Tension steel did not yield.
 Mc = 161.97 ϕ_c = 5.83e-06 ϵ_c = 0.00123 kd = 211.0 fc = 16.655591741493783
 Tension steel did not yield.
 Mc = 186.87 ϕ_c = 6.76e-06 ϵ_c = 0.00143 kd = 211.0 fc = 17.509990553417143
 Tension steel yields but compression steel did not.
 Mc = 201.24 ϕ_c = 7.85e-06 ϵ_c = 0.00163 kd = 208.0 fc = 17.844624659458155
 For $\epsilon_o < \epsilon_c < \epsilon_{cu}$
 Both tension and compression steel yields.
 Mc = 203.58 ϕ_c = 1.024e-05 ϵ_c = 0.00196 kd = 191.0 fc = 17.849999999999998
 Both tension and compression steel yields.
 Mc = 204.35 ϕ_c = 1.17e-05 ϵ_c = 0.00216 kd = 184.0 fc = 17.849999999999998
 Both tension and compression steel yields.
 Mc = 204.89 ϕ_c = 1.316e-05 ϵ_c = 0.00236 kd = 179.0 fc = 17.849999999999998
 Both tension and compression steel yields.
 Mc = 205.27 ϕ_c = 1.462e-05 ϵ_c = 0.00256 kd = 175.0 fc = 17.849999999999998
 Both tension and compression steel yields.
 Mc = 205.55 ϕ_c = 1.608e-05 ϵ_c = 0.00276 kd = 172.0 fc = 17.849999999999998
 Both tension and compression steel yields.
 Mc = 205.76 ϕ_c = 1.754e-05 ϵ_c = 0.00296 kd = 169.0 fc = 17.849999999999998

Case No. 3

Mcr = 60.97 ϕ_c = 7.167101269032306e-07 kd = 242.19468984442693
 Mcr = 60.97 ϕ_c = 9.733433018711496e-07 kd = 196.764121236301 After cracking...
 Myield = 159.98 ϕ_c = 2.5125377830969175e-06 ϵ_c = 0.0004875080526548766 kd = 194.0301379484058


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For  $0 < \epsilon_c < \epsilon_o$ 
Tension steel did not yield.
Mc = 244.28  $\phi_c$  = 5.31e-06  $\epsilon_c$  = 0.00103 kd = 194.0 fc = 15.281428223688067
Tension steel did not yield.
Mc = 302.97  $\phi_c$  = 6.1e-06  $\epsilon_c$  = 0.00123 kd = 201.0 fc = 16.655591741493783
Tension steel did not yield.
Mc = 357.3  $\phi_c$  = 6.86e-06  $\epsilon_c$  = 0.00143 kd = 208.0 fc = 17.509990553417143
Tension steel yields but compression steel did not.
Mc = 414.18  $\phi_c$  = 7.27e-06  $\epsilon_c$  = 0.00163 kd = 224.0 fc = 17.844624659458155
For  $\epsilon_o < \epsilon_c < \epsilon_{cu}$ 
Both tension and compression steel yields.
Mc = 422.07  $\phi_c$  = 1.024e-05  $\epsilon_c$  = 0.00196 kd = 191.0 fc = 17.849999999999998
Both tension and compression steel yields.
Mc = 422.84  $\phi_c$  = 1.17e-05  $\epsilon_c$  = 0.00216 kd = 184.0 fc = 17.849999999999998
Both tension and compression steel yields.
Mc = 423.37  $\phi_c$  = 1.316e-05  $\epsilon_c$  = 0.00236 kd = 179.0 fc = 17.849999999999998
Both tension and compression steel yields.
Mc = 423.75  $\phi_c$  = 1.462e-05  $\epsilon_c$  = 0.00256 kd = 175.0 fc = 17.849999999999998
Both tension and compression steel yields.
Mc = 424.03  $\phi_c$  = 1.608e-05  $\epsilon_c$  = 0.00276 kd = 172.0 fc = 17.849999999999998
Both tension and compression steel yields.
Mc = 424.25  $\phi_c$  = 1.754e-05  $\epsilon_c$  = 0.00296 kd = 169.0 fc = 17.849999999999998

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# Convert the values of data to smaller figures
 $\phi\_converted$  = ([], [], [])
M_converted = ([], [], [])
for i in range(3):
    for curvature in  $\phi[i]$ :
         $\phi\_converted[i].append(curvature * 1000)$ 
    for moment in M[i]:
        M_converted[i].append(moment / 1000**2)

# Plot the curves
plt.figure(figsize=(10,8))
plt.title("Moment-Curvature")
plt.xlabel('Curvature  $\times 10^{-5}$  /mm')
plt.ylabel('Moment in kN-m')
plt.grid()

for yp in yield_pts:
    plt.text(yp[0], yp[1], 'Yield Point')

# Plot the converted values
case1, = plt.plot( $\phi\_converted[0]$ , M_converted[0], marker='s', label='Case 1 ( $A_s = A_{sb}$ )')
case2, = plt.plot( $\phi\_converted[1]$ , M_converted[1], marker='s', label='Case 2 ( $A_s = 0.5A_{sb}$ )')
case3, = plt.plot( $\phi\_converted[2]$ , M_converted[2], marker='s', label='Case 3 ( $A_s = 1.2A_{sb}$ ,  $A_s \setminus = 0.7A_{sb}$ )')
plt.legend(handles=[case1, case2, case3], loc='best', fontsize=14)
plt.show()

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