

EE414 Supplementary Problem Solutions

Problem 1:

For $L_d = 0$

$$(a) L_{eff} = L - 2L_d - X_d = 0.9 \mu m$$

$$|I_0| = 200 \mu A \text{ for } M_5 - M_8$$

$$|I_0| = 100 \mu A \text{ for } M_1 - M_4$$

$$\frac{dX_d}{dV_{DS}} = 0.02 \mu m/V \text{ (NMOS)}$$

$$= 0.04 \mu m/V \text{ (PMOS)}$$

$$\frac{1}{r_0} = \frac{\partial I_0}{\partial V_{DS}} = \frac{I_0}{L_{eff}} \frac{dX_d}{dV_{DS}}$$

$$1/r_{02} = 100 \mu A / 0.9 \mu m \cdot 0.04 \mu m/V = 4.44 \mu A/V$$

$$1/r_{01} = 100 \mu A / 0.9 \mu m \cdot 0.02 \mu m/V = 2.22 \mu A/V$$

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}} = \frac{3.9 \times 8.854 \times 10^{-12}}{80 \times 10^{-10}} = 4.32 \times 10^{-3} F/m^2$$

$$K_p' = \mu_p C_{ox} = 150 \times 10^{-4} \times 4.32 \times 10^{-3} = 64.7 \mu A/V^2$$

$$K_n' = \mu_n C_{ox} = 450 \times 10^{-4} \times 4.32 \times 10^{-3} = 194 \mu A/V^2$$

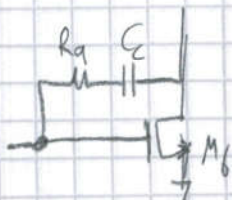
$$g_{m2} = \sqrt{2 \times 64.7 \times (150/0.9) \times 100} = 1.47 \text{ mA/V}$$

$$g_{m6} = \sqrt{2 \times 194 \times (100/0.9) \times 200} = 2.94 \text{ mA/V}$$

$$1/r_{07} = \frac{200 \mu A}{0.9 \mu m} \times 0.04 \mu m/V = 8.89 \mu A/V$$

$$1/r_{06} = \frac{200 \mu A}{0.9 \mu m} \times 0.02 \mu m/V = 4.44 \mu A/V$$

$$V_0/V_i = g_{m2} (r_{02} || r_{04}) \cdot g_{m6} (r_{06} || r_{07}) = \underline{\underline{48681}}$$



$$Z = \frac{1}{(1/g_{m6} - R_q)C_c}$$

cancel this zero by moving it to infinity.

$$R_q = \frac{1}{g_{m6}} = \frac{1}{2.94 \text{ m}} = 340.1 \Omega$$

$$1/R_q = K' \left(\frac{W}{L} \right)_q (V_{GSq} - V_{Tq} - V_{OSq}) \Rightarrow (V_{OSq} \approx 0)$$

Assume $\gamma = 0$

$$1/R_q = K' \left(\frac{W}{L} \right)_q (V_{Gq} - V_{SS} - V_{GS6} - V_{Tq})$$

$$\therefore V_{OV6} = \sqrt{\frac{2 \times 200}{194(100/29)}} = 0.136 \text{ V} \Rightarrow V_{GS6} = V_{OV6} + V_{T6} \overset{0.6 \text{ V}}{\downarrow} = 0.736 \text{ V}$$

$$\therefore 1/R_q = \frac{1}{340} = 194 \times 10^{-6} \left(\frac{W}{L} \right)_q (3 - 0.736 - 0.7) \Rightarrow \left(\frac{W}{L} \right)_q = 9.7$$

* M_q is in triode region, so $X_d = 0 \Rightarrow L_q = L_d - 2L_d - X_d = 1 \mu\text{m}$

$$\Rightarrow \underline{L_q = 1 \mu\text{m}}, \quad \underline{W_q = 9.7 \mu\text{m}}$$

$$\text{At } f_{\text{unity}} \Rightarrow |A(j\omega)| = \left| \frac{g_{m1}}{j\omega C_c} \right| = 1 \Rightarrow f_{\text{unity}} = \frac{g_{m1}}{C_c 2\pi} = \underline{46.8 \text{ MHz}}$$

$$SR = \frac{I_{\text{max}}}{C_c} = \frac{200 \mu\text{A}}{5 \text{ pF}} = \underline{40 \text{ V}/\mu\text{s}}$$

$$(b) 1/R_q = K' \left(\frac{W}{L} \right)_q (V_{GSq} - V_{Tq})$$

$$\text{Since } I_{D12} = I_{D6} \text{ and } \left(\frac{W}{L} \right)_{12} = \left(\frac{W}{L} \right)_6 \therefore V_{OV12} = V_{OV6} = 0.136 \text{ V}$$

$$\text{Therefore } V_{SB11} = V_{GS12} = V_{T12} + V_{OV12} = V_{SBq} = V_{GS6} = V_{T6} + V_{OV6}$$

Because $V_{T12} = V_{T6}$ (no body effect)

$$\text{Also: } V_{OV11} = V_{OV12} \text{ because } I_{D11} = I_{D12} \text{ and } \left(\frac{W}{L} \right)_{11} = \left(\frac{W}{L} \right)_{12}$$

$$\begin{aligned} \text{Therefore: } V_{GSq} &= V_{GS11} + V_{GS12} - V_{GS6} = V_{G11} + V_{OV11} + V_{G12} + V_{OV12} - V_{G6} - V_{OV6} \\ &= V_{G11} + V_{OV11} \end{aligned}$$

$$\therefore V_{GS9} - V_{T9} = V_{T11} + V_{OV11} - V_{T9} = V_{OV11}$$

Since $V_{GS9} - V_{T9} = V_{GS6} - V_{T6}$ and $1/R_9$ should be equal to g_{m6} to cancel the RHP zero.

$$1/R_9 = k' (W/L)_9 (V_{GS9} - V_{T9}) = g_{m6} = k' (W/L)_6 (V_{GS6} - V_{T6})$$

$$\Rightarrow (W/L)_9 = (W/L)_6 = \underline{\underline{100/1}}$$

(c) To get 45° phase margin set the second pole = unity gain freq.

$$\left(|P_2| = \frac{g_{m6} C_c}{C_L C_1 + C_c C_L + C_c C_c} \right) = \frac{g_{m2}}{C_c} \quad (C_c \text{ is the parasitic cap. at first stage output})$$

$$\therefore C_1 = \cancel{C_{OL2}} + \cancel{C_{OL4}} + C_{GS6} + \cancel{C_{OL9}} \approx C_{GS6} = \left(\frac{2}{3} 100 \mu\text{m} \cdot 0.9 \mu\text{m} \right) \cdot 4.32 \frac{\text{fF}}{\mu\text{m}^2}$$

$$C_1 = 259.2 \text{ pF}$$

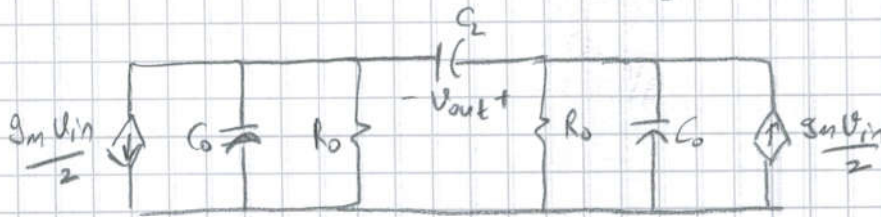
$$\frac{g_{m2}}{C_c} = \frac{147 \text{ MA/V}}{5 \text{ pF}} = 294 \text{ Mrad/s}$$

$$\therefore 294 \text{ Mrad/s} = \frac{2.94 \text{ mA/V} \cdot 5 \text{ pF}}{C_L 259.2 \text{ f} + C_L 59 + 259.2 \text{ f} \times 59}$$

$$\Rightarrow \underline{\underline{C_L = 9.26 \text{ pF}}}$$

Problem 2:

Let's first draw the small signal model of the circuit.



$$\frac{v_{out}}{v_{in}} = g_m r_o \quad \text{and} \quad \omega_{-3dB} = \frac{1}{(C_L + 0.5C_0) 2r_o}$$

$$g_m = \sqrt{2 \mu_n \left(\frac{W}{L} \right)_1 I_{D1}} = \sqrt{2 \cdot 110 \cdot 10.25 \text{ MA/V}} = 234.5 \text{ MA/V}$$

$$r_o \approx 1/g_{m3} \parallel r_{o1} \parallel r_{o3} \parallel r_{o5}, \quad g_{m3} = \sqrt{2 \mu_p \left(\frac{W}{L} \right)_3 I_{D3}} = \sqrt{2 \cdot 50 \cdot 2.5 \text{ MA/V}} = 31.62 \text{ MA/V}$$

$$r_{o1} = \frac{1}{\lambda I_{D1}} = \frac{1}{0.04 \cdot 25 \text{ MA}} = 1 \text{ M}\Omega, \quad r_{o3} = 4 \text{ M}\Omega, \quad r_{o5} = 0.8 \text{ M}\Omega$$

$$\therefore r_o = 31.623 \text{ k}\Omega \parallel 1 \text{ M}\Omega \parallel 4 \text{ M}\Omega \parallel 0.8 \text{ M}\Omega = 29.31 \text{ k}\Omega$$

$$C_0 \approx C_{gs3} + C_{bd1} + C_{bd3} + C_{bd5} \quad C_{gs3} = C_{gs0} W_5 + 0.67 C_{ox} W_5 L_5$$

$$= 220 \text{ pF/m} \cdot 2 \times 10^{-6} + 0.67 \times 24.7 \times 10^{-4} \text{ F/m}^2 \times 2 \text{ Mm}^2$$

$$C_{gs3} = 3.73 \text{ fF}$$

$$C_{bd1} = C_j A_S + C_{jsw} \cdot P_S = 770 \times 10^{-6} \text{ F/m}^2 \cdot 50 \text{ Mm}^2 + 380 \times 10^{-12} \text{ F/m} \cdot 30 \text{ Mm}$$

$$C_{bd1} = 38.5 \text{ pF} + 11.4 \text{ pF} = 49.9 \text{ pF}$$

$$C_{bd3} = C_{bd5} = 560 \times 10^{-6} \text{ F/m}^2 \cdot 10 \text{ Mm}^2 + 350 \times 10^{-12} \text{ F/m} \cdot 14 \text{ Mm} = 10.5 \text{ pF}$$

$$\therefore C_0 = 74.6 \text{ pF} \rightarrow \omega_{-3dB} = \frac{1}{(11073 \text{ pF}) 58.62 \text{ k}\Omega} = 16.45 \text{ Mrad/s}$$

$$f_{-3dB} = \underline{\underline{2.62 \text{ MHz}}}$$

$$A_v = \underline{\underline{6.873 \text{ V/V}}}$$