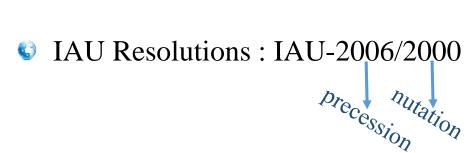
Transformation of ITRF to GCRF

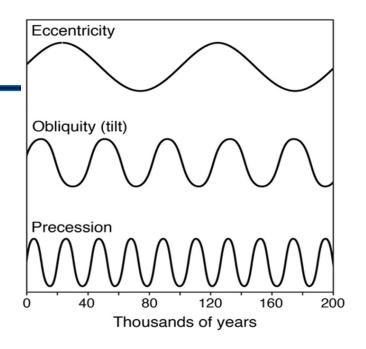
Orbit determination requires both celestial reference frames and terrestrial reference frames.

reduction formula (Earth orientation model) $\overset{\triangleright}{r}_{GCRF} = [P(t)][N(t)][R(t)][W(t)]\overset{\triangleright}{r}_{ITRF}$ Precession matrix of date t

Nutation matrix of date t

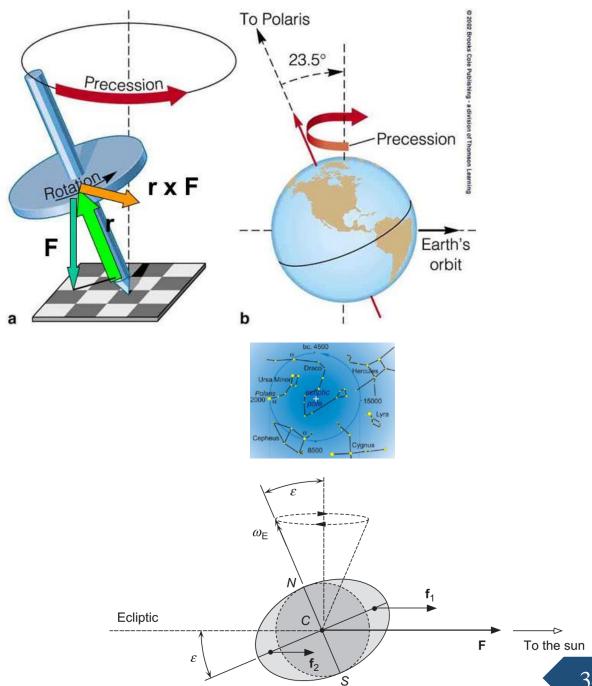
sidereal-rotation matrix of date t





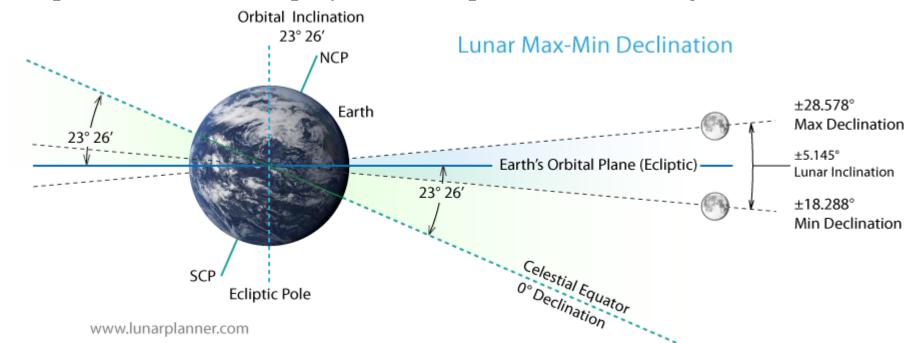
Precession

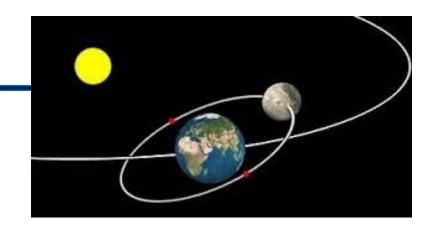
- Precession
 - precession of the ecliptic
 - o equinox precession to the west (12 "/century)
 - o Ecliptic obliquity reduction(47 "/century)
 - ☐ luni-solar precession
 - o Period: 26000 year (49.846 "/year)
 - general precession
 - o 50 "/year



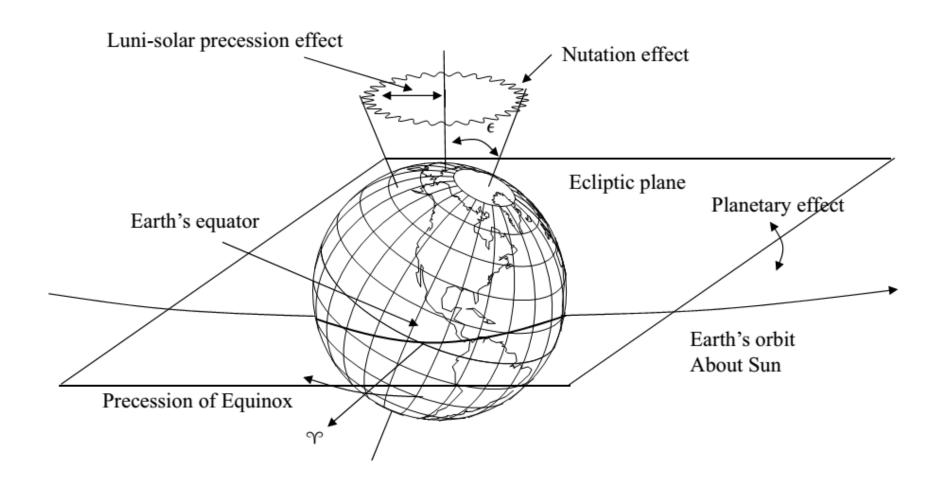
Nutation

- Nutation
 - period about 18.6 years
 - ☐ Precession of the equator/regression of the lunar node
 - ☐ Variation of the max torque direction
 - ☐ Max amplitude of 9" in obliquity of the ecliptic and 17" in longitude





Precession-Nutation



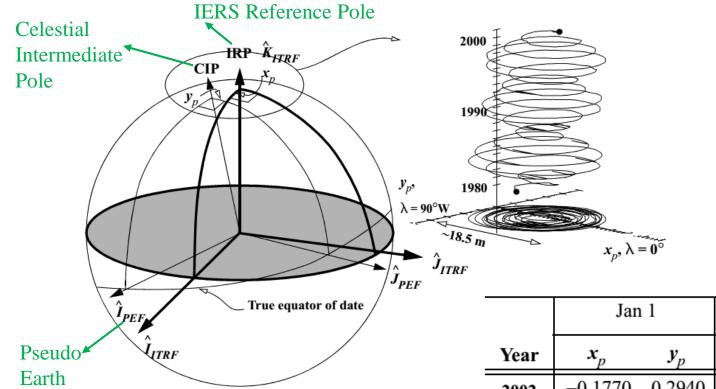
Some definitions

- ecliptic of date: ecliptic plane orientation (variable due to general precession) with an ideal inertial frame on a specific date.
- mean equator of date: modeled equator wobbling around the ecliptic
- wean equinox of date: the intersection of equator and ecliptic planes on a given date
- true equator of date: including the effect of nutation

Polar Motion

fixed

with respect to the crust of the Earth



0.1" = 0.000 028° = 3.09 m for the surface of the Earth

	Jan 1		Oct 1	
Year	x_p	y_p	x_p	y_p
2002	-0.1770	0.2940	0.1985	0.2005
2003	-0.0885	0.1880	0.2585	0.3040
2004	0.0313	0.1538	0.1985	0.4315
2005	0.1492	0.2380	0.0588	0.4169
2006	0.0527	0.3834	0.0327	0.2524

Williams

Theory

IAU 76/FK5

Rotation

Polar Motion (IAU-2006/2000, CIO based)

$$\dot{r}_{TIRS} = \text{ROT3}(-s')\text{ROT2}(x_p)\text{ROT1}(y_p)\dot{r}_{ITRF} = [\textbf{W}]_{ITRF-TIRS}\dot{r}_{ITRF}$$

$$s' = -0.0015" \left(\frac{a_c^2}{1.2} + a_a^2\right)T_{TT} \cong -0.000\ 047"T_{TT}$$

Chandler wobble ($a_c = 0.26$ ") annual wobble ($a_a = 0.12$ ")

$$\left[\textbf{\textit{W}} \right]_{\text{ITRF-TIRS}} = \begin{bmatrix} \cos(x_p)\cos(s') & -\cos(y_p)\sin(s') + \sin(y_p)\sin(x_p)\cos(s') & -\sin(y_p)\sin(s') - \cos(y_p)\sin(x_p)\cos(s') \\ \cos(x_p)\sin(s') & \cos(y_p)\cos(s') + \sin(y_p)\sin(x_p)\sin(s') & \sin(y_p)\cos(s') - \cos(y_p)\sin(x_p)\sin(s') \\ \sin(x_p) & -\sin(y_p)\cos(x_p) & \cos(y_p)\cos(x_p) \end{bmatrix}$$

Earth Rotation Angle (IAU-2006/2000, CIO based)

$$\begin{split} \theta_{ERA} &= 280.460\ 618\ 375\ 04^\circ + 360.985\ 612\ 288\ 808(JD_{UT1} - 2,451,545.0) \\ &= 2\pi(0.779\ 057\ 273\ 264\ 0 + 1.002\ 737\ 811\ 911\ 354\ 48(JD_{UT1} - 2,451,545.0)) \\ \mathring{r}_{CIRS} &= \text{ROT3}(-\theta_{ERA})\mathring{r}_{TIRS} \\ \mathring{v}_{CIRS} &= \text{ROT3}(-\theta_{ERA})\mathring{v}_{TIRS} + \mathring{\omega}_{\oplus} \times \mathring{r}_{TIRS} \end{split}$$

Precession-Nutation (IAU-2006/2000, CIO based)

$$\dot{r}_{GCRF} = [PN]\dot{r}_{CIRS}$$

$$= \begin{bmatrix} 1 - aX^2 & -aXY & X \\ -aXY & 1 - aY^2 & Y \\ -X & -Y & 1 - a(X^2 + Y^2) \end{bmatrix} ROT3(s)\dot{r}_{CIRS}$$

$$\begin{split} a &= \frac{1}{1 + \cos(d)} \cong \frac{1}{2} + \frac{1}{8}(X^2 + Y^2) \\ X &= -0.016\ 617'' + 2004.191\ 898\ T_{TT} - 0.429\ 782\ 9\ T_{TT}^2 - 0.198\ 618\ 34\ T_{TT}^3 \\ &+ 0.000\ 007\ 578\ T_{TT}^4 + 0.000\ 005\ 928\ 5\ T_{TT}^5 \\ 1306 & 253 \\ &+ \sum_{i=1}^{1306} [A_{xs0_i} \mathrm{SIN}(a_{p_i}) + A_{xc0_i} \cos(a_{p_i})] + \sum_{i=1}^{1306} [A_{xs1_i} \mathrm{SIN}(a_{p_i}) + A_{xc1_i} \cos(a_{p_i})] T_{TT} \\ &+ \sum_{i=1}^{136} [A_{xs2_i} \mathrm{SIN}(a_{p_i}) + A_{xc2_i} \cos(a_{p_i})] T_{TT}^2 + \sum_{i=1}^{136} [A_{xs3_i} \mathrm{SIN}(a_{p_i}) + A_{xc3_i} \cos(a_{p_i})] T_{TT}^3 \\ &+ \sum_{i=1}^{136} [A_{xs4_i} \mathrm{SIN}(a_{p_i}) + A_{xc4_i} \cos(a_{p_i})] T_{TT}^4 \end{split}$$

```
s = -\frac{XY}{2} + 0.000094'' + 0.00380865T_{TT} - 0.00012268T_{TT}^2 - 0.07257411T_{TT}^3
           -0.002\ 640\ 73\ \mathrm{SIN}(\Omega_{\mathcal{C}}) - 0.000\ 063\ 53\ \mathrm{SIN}(2\Omega_{\mathcal{C}})
           -0.000\ 011\ 75\ \mathrm{SIN}(2u_{M\%}-2D_{\bigodot}+3\Omega_{\circlearrowleft})-0.000\ 011\ 21\ \mathrm{SIN}(2u_{M\%}-2D_{\bigodot}+\Omega_{\circlearrowleft})
           +\ 0.000\ 004\ 57\ \mathrm{SIN}((2u_{M^{(\ell)}}-2D_{\odot}+2\Omega_{(\ell)})-0.000\ 002\ 02\ \mathrm{SIN}(2u_{M^{(\ell)}}+3\Omega_{(\ell)}))
           -0.000\ 001\ 98 \sin((2u_{M\mathcal{O}} + \Omega_{\mathcal{O}}) + 0.000\ 001\ 72 \sin(3\Omega_{\mathcal{O}}))
           + 0.000\ 001\ 41\ \sin((M_{\odot} + \Omega_{\odot}) + 0.000\ 001\ 26\ \sin(M_{\odot} - \Omega_{\odot}))
           +\ 0.000\ 000\ 63\ \mathrm{sin}((M_{\mathcal{Q}}+\Omega_{\mathcal{Q}})+0.000\ 000\ 63\ \mathrm{sin}(M_{\mathcal{Q}}-\Omega_{\mathcal{Q}}))
           +\,0.000\,001\,73\,T_{TT}\mathrm{SIN}(\Omega_{\mathcal{C}}) + 0.000\,003\,57\,T_{TT}\mathrm{cos}(2\Omega_{\mathcal{C}}) + 0.000\,743\,52\,T_{TT}^{2}\mathrm{SIN}(\Omega_{\mathcal{C}})
           + 0.000\ 056\ 91\ T_{TT}^2 \sin(2(u_{M\mathscr{Q}} - D_{\odot} + \Omega_{\mathscr{Q}})) + 0.000\ 009\ 84\ T_{TT}^2 \sin(2(u_{M\mathscr{Q}} + \Omega_{\mathscr{Q}}))
           -0.000\,008\,85\,T_{TT}^2\sin(2\Omega_{c})
 \begin{vmatrix} \dot{r}_{GCRF} = [PN][R][W]\dot{r}_{ITRF} \\ \dot{v}_{GCRF} = [PN][R] \left\{ [W]\dot{v}_{ITRF} + \dot{\omega}_{\oplus} \times \dot{r}_{TIRS} \right\} \end{vmatrix}
\Rightarrow \begin{cases} \dot{r}_{ITRF} = [\boldsymbol{W}]^T [\boldsymbol{R}]^T [\boldsymbol{P} \boldsymbol{N}]^T \dot{r}_{GCRF} \\ \dot{\boldsymbol{v}}_{ITRF} = [\boldsymbol{W}]^T \bigg\{ [\boldsymbol{R}]^T [\boldsymbol{P} \boldsymbol{N}]^T \dot{\boldsymbol{v}}_{GCRF} - \dot{\boldsymbol{\omega}}_{\oplus} \times \dot{\boldsymbol{r}}_{TIRS} \bigg\} \end{cases}
```

```
M_{\mathcal{C}} = 485868.249\ 036" + 1717915923.2178T_{TT} + 31.8792T_{TT}^2 + 0.051\ 635T_{TT}^3 - 0.000\ 244\ 70T_{TT}^4
 M_{\odot} = 1287104.79305'' + 129596581.0481 T_{TT} - 0.5532 T_{TT}^2 + 0.000 136 T_{TT}^3 - 0.000 011 49 T_{TT}^4
u_{M\%} = 335779.526\ 232" + 1739527262.8478 T_{TT} - 12.7512 T_{TT}^2 - 0.001\ 037 T_{TT}^3
         + 0.000 004 17 T_{TT}^4
 D_{\odot} = 1072260.70369'' + 1602961601.2090T_{TT} - 6.3706T_{TT}^{2} + 0.006593T_{TT}^{3} - 0.00003169T_{TT}^{4}
 \Omega_{\mathcal{C}} = 450160.398\ 036" - 6962890.5431T_{TT} + 7.4722T_{TT}^2 + 0.007702T_{TT}^3 - 0.000\ 059\ 39T_{TT}^4
\lambda_{M8} = 4.402608842 + 2608.7903141574T_{TT}
 \lambda_{M \odot} = 3.176 \, 146 \, 697 + 1021.328 \, 554 \, 621 \, 1 T_{TT}
 \lambda_{M\oplus} = 1.753470314 + 628.3075849991T_{TT}
 \lambda_{MS} = 6.203 480 913 + 334.061 242 670 0 T_{TT}
  \lambda_{M2l} = 0.599546497 + 52.9690962641T_{TT}
  \lambda_{Mb} = 0.874\,016\,757 + 21.329\,910\,496\,0T_{TT}
   \lambda_{M^{\odot}} = 5.481\ 293\ 872 + 7.478\ 159\ 856\ 7T_{TT}
   \lambda_{M\Psi} = 5.311 \, 886 \, 287 + 3.813 \, 303 \, 563 \, 8T_{TT}
  p_{\lambda} = 0.02438175T_{TT} + 0.00000538691T_{TT}^2
```