

In The Name of God



Sharif University of Technology  
Department of Aerospace Engineering

# **45-784: Advanced Orbital Mechanics**

## CH#4: Orbit Representation Methods

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# Satellite State Representations

- 🌐 We need six quantities to define the translational state of a satellite in space. These quantities may take on many equivalent forms:

- 🌐 Cartesian (inertial) coordinates


$$\mathbf{X} = [\mathbf{r}^T \quad \mathbf{v}^T]^T = [x \quad y \quad z \quad \dot{x} \quad \dot{y} \quad \dot{z}]^T$$

- 🌐 True classical element set

$$\mathbf{X} = [a \quad e \quad i \quad \Omega \quad \omega \quad t]^T$$

Singular at  $e = 0$  or  $1$ ,  $i = 0$  or  $\pi$

- 🌐 Modified classical element set

$$\mathbf{X} = [a \quad e \quad i \quad \Omega \quad \omega \quad \theta]^T$$


M

Singular at  $e = 0$  or  $1$ ,  $i = 0$  or  $\pi$

# Satellite State Representations

## Flight elements (ADBARV elements)

| Spherical elements | Geographic elements | Flight elements |
|--------------------|---------------------|-----------------|
| $\alpha$           | $h$                 | $\alpha$        |
| $\delta$           | $\lambda$           | $\delta$        |
| $\alpha_v$         | $\phi_{gc}$         | $\beta$         |
| $\delta_v$         | $v$                 | $A$             |
| $r$                | $\gamma$            | $r$             |
| $v$                | $A$                 | $v$             |

Singular at poles

$$\sin(\alpha) = \frac{y}{\sqrt{x^2 + y^2}}, \quad \sin(\delta) = \frac{z}{r}, \quad r = \sqrt{x^2 + y^2 + z^2}, \quad v = \sqrt{\dot{x}^2 + \dot{y}^2 + \dot{z}^2}$$

# Satellite State Representations

$$[\mathbf{v}]^{SEZ} = T^{SEZ-GCRF} [\mathbf{v}]^{GCRF} = T^{SEZ-GCRF} \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix}$$

$$T^{SEZ-GCRF} = R_2(90 - \delta) R_3(\alpha)$$

$$[\mathbf{v}]^{SEZ} = \begin{bmatrix} v_s \\ v_E \\ v_z \end{bmatrix} = v \begin{bmatrix} -\cos A \cos \gamma \\ \sin A \cos \gamma \\ \sin \gamma \end{bmatrix}$$

$$\sin \gamma = \frac{v_z}{v}, \quad \sin A = \frac{v_E}{\sqrt{v_s^2 + v_E^2}}$$

$$\sin \phi_{gc} = \frac{r_z}{r}, \quad \tan \lambda = \frac{r_y}{r_x}$$

$$\text{where } [\mathbf{r}]^{ITRF} = T^{ITRF-GCRF} [\mathbf{r}]^{GCRF} \rightarrow \begin{bmatrix} r_x \\ r_y \\ r_z \end{bmatrix} = T^{ITRF-GCRF} \begin{bmatrix} x \\ y \\ z \end{bmatrix}$$

# Satellite State Representations

🌐 Nonsingular ( $e < 1$ ) Euler parameters  $\mathbf{X} = [a \quad e \quad q_1 \quad q_2 \quad q_3 \quad M]^T$

$$T^{GCRF-PCS} = R_3(-\Omega)R_1(-i)R_3(-\omega)$$

$$= \begin{bmatrix} q_1^2 - q_2^2 - q_3^2 + q_4^2 & 2(q_1q_2 - q_3q_4) & 2(q_1q_3 + q_2q_4) \\ 2(q_1q_2 + q_3q_4) & -q_1^2 + q_2^2 - q_3^2 + q_4^2 & 2(q_2q_3 - q_1q_4) \\ 2(q_1q_3 - q_2q_4) & 2(q_2q_3 + q_1q_4) & -q_1^2 - q_2^2 + q_3^2 + q_4^2 \end{bmatrix}$$

where  $\mathbf{q} = [q_1 \quad q_2 \quad q_3 \quad q_4]^T$ ,  $\mathbf{q}^T \mathbf{q} = 1$

$$q_4 = \frac{1}{2} \sqrt{1 + t_{11} + t_{22} + t_{33}} = \cos \frac{i}{2} \cos \frac{\Omega + \omega}{2}$$

Undefined for  $e \geq 1$ .

$$q_1 = \frac{t_{32} - t_{23}}{4q_4} = \sin \frac{i}{2} \cos \frac{\Omega - \omega}{2}$$

$$q_2 = \frac{t_{13} - t_{31}}{4q_4} = \sin \frac{i}{2} \sin \frac{\Omega - \omega}{2},$$

$$q_3 = \frac{t_{21} - t_{12}}{4q_4} = \cos \frac{i}{2} \sin \frac{\Omega + \omega}{2}$$

# Quaternions

- How to compute unit quaternion from a given DCM?

- Form the symmetric matrix

$$\mathbf{K} = \frac{1}{3} \begin{bmatrix} t_{11} - t_{22} - t_{33} & t_{21} + t_{12} & t_{31} + t_{13} & t_{23} - t_{32} \\ t_{21} + t_{12} & -t_{11} + t_{22} - t_{33} & t_{32} + t_{23} & t_{31} - t_{13} \\ t_{31} + t_{13} & t_{32} + t_{23} & -t_{11} - t_{22} + t_{33} & t_{12} - t_{21} \\ t_{23} - t_{32} & t_{31} - t_{13} & t_{12} - t_{21} & t_{11} + t_{22} + t_{33} \end{bmatrix}$$

- Solve the eigenvalue problem  $\mathbf{K}\mathbf{e} = \lambda\mathbf{e}$  for the largest eigenvalue ( $\lambda_{\max}$ ). The corresponding eigenvector is the quaternion.

# Satellite State Representations

🌐 Nonsingular ( $e < 1$ ) quaternion element set:  $\mathbf{X} = [\mathbf{q}^T \quad e_x \quad e_y]^T$

$$q_1 = p^{\frac{1}{4}} \sin \frac{i}{2} \cos \frac{\Omega - \omega - M}{2}$$

$$q_2 = p^{\frac{1}{4}} \sin \frac{i}{2} \sin \frac{\Omega - \omega - M}{2}$$

$$q_3 = p^{\frac{1}{4}} \cos \frac{i}{2} \sin \frac{\Omega + \omega + M}{2}$$

$$q_4 = p^{\frac{1}{4}} \cos \frac{i}{2} \cos \frac{\Omega + \omega + M}{2}$$

$$e_x = e \cos M$$

$$e_y = e \sin M$$

# Satellite State Representations

- Equinoctial elements:  $\mathbf{X} = [a \ h \ k \ p \ q \ \lambda]^T$

$$a = a$$

$$h = e \sin(\omega + f_r \Omega)$$

$$k = e \cos(\omega + f_r \Omega)$$

$$f_r = \begin{cases} +1 & : \text{Prograde orbits} \\ -1 & : \text{Retrograde orbits} \end{cases}$$

$$p = \tan^{f_r} (i / 2) \sin \Omega = \frac{\sin i \sin \Omega}{1 + \cos^{f_r} i}$$

Undefined for  $e \geq 1$ .

$$q = \tan^{f_r} (i / 2) \cos \Omega = \frac{\sin i \cos \Omega}{1 + \cos^{f_r} i}$$

$$\lambda = M + \omega + \Omega: \text{ mean longitude}$$

- Modified Equinoctial elements:  $\mathbf{X} = [p \ f \ g \ h \ k \ L]^T$

$$p = a(1 - e^2)$$

$$h = \tan^{f_r} (i / 2) \cos(\Omega)$$

Nonsingular for all eccentricities and inclinations

$$f = e \cos(\omega + f_r \Omega)$$

$$k = \tan^{f_r} (i / 2) \sin(\Omega)$$

$$g = e \sin(\omega + f_r \Omega)$$

$$L = \omega + f_r \Omega + \theta$$



# Satellite State Representations

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- 🌐 Classical OE from MEOE

$$e = \sqrt{f^2 + g^2}$$

$$a = \frac{p}{1 - e^2}$$

Assuming  $f_r = 1$ :  $\tan(i / 2) = \sqrt{h^2 + k^2}$

$$\tan \Omega = \frac{k}{h}$$

$$\omega = \tan^{-1}(g / f) - \Omega$$

$$\theta = L - (\Omega + \omega)$$

# Satellite State Representations

- 🌐 Delaunay elements:  $\mathbf{X} = [M \quad \Omega \quad \omega \quad L \quad h \quad H]^T$

$$L = \sqrt{\mu a}$$

Singular at  $e = 0$  or  $1$ ,  $i = 0$  or  $\pi$

$$H = \sqrt{\mu p} \cos i$$

- 🌐 Poincaré elements:  $\mathbf{X} = [\Lambda \quad \xi \quad \eta \quad u \quad v \quad \lambda]^T$

$$\Lambda = \sqrt{\mu a}$$

$$\xi = e \sin(\Omega + \omega) \sqrt{2\Lambda / (1 + \sqrt{1 - e^2})}$$

$$\eta = e \cos(\Omega + \omega) \sqrt{2\Lambda / (1 + \sqrt{1 - e^2})}$$

$$u = \sin i \sin \Omega \sqrt{2\Lambda \sqrt{1 - e^2} / (1 + \cos i)}$$

$$v = \sin i \cos \Omega \sqrt{2\Lambda \sqrt{1 - e^2} / (1 + \cos i)}$$

$$\lambda = M + \Omega + \omega$$

Nonsingular for small eccentricities and inclinations

Undefined for  $e \geq 1$ .

# Satellite State Representations

🌐 Alternate form of Poincaré elements:  $\mathbf{X} = [L \quad g_p \quad h_p \quad G \quad H \quad \lambda]^T$

$$L = \sqrt{\mu a}$$

$$g_p = \cos(\Omega + \omega) \sqrt{2L(1 - \sqrt{1 - e^2})}$$

$$h_p = \cos(\Omega) \sqrt{2L\sqrt{1 - e^2}(1 - \cos i)}$$

$$G = \sin(\Omega + \omega) \sqrt{2L(1 - \sqrt{1 - e^2})}$$

$$H = \sin(\Omega) \sqrt{2L\sqrt{1 - e^2}(1 - \cos i)}$$

$$\lambda = M + \Omega + \omega$$

Nonsingular for small eccentricities and inclinations

Undefined for  $e \geq 1$ .

# Satellite State Representations

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- 🌐 Two-line Element Set (TLE) is a data format encoding a list of orbital elements of an Earth-orbiting object for a given point in time.
- 🌐 A TLE set consists of two 69-character lines of data which can be used together with SGP4/SDP4 orbital model to determine the position and velocity of the associated satellite.

## ISS (ZARYA)

```
1 25544U 98067A 08264.51782528 -.00002182 00000-0 -11606-4 0 2927  
2 25544 51.6416 247.4627 0006703 130.5360 325.0288 15.72125391563537
```

- 🌐 Line 0 is a twenty-four character name.

# Satellite State Representations

## Line 1

1 25544U 98067A 08264.51782528 -.00002182 00000-0 -11606-4 0 2927

| Field | Columns | Content   | Example      |
|-------|---------|---|--------------|
| 1     | 01–01   | Line number of Element Data   | 1            |
| 2     | 03–07   | Satellite number  | 25544        |
| 3     | 08–08   | Classification (U=Unclassified)   | U            |
| 4     | 10–11   | International Designator (Last two digits of launch year)                                     | 98           |
| 5     | 12–14   | International Designator (Launch number of the year)  | 067          |
| 6     | 15–17   | International Designator (piece of the launch)  | A            |
| 7     | 19–20   | Epoch Year (last two digits of year)  | 08           |
| 8     | 21–32   | Epoch (day of the year and fractional portion of the day)                                     | 264.51782528 |
| 9     | 34–43   | First Time Derivative of the Mean Motion divided by two ( $\dot{n}/2$ )                       | -.00002182   |
| 10    | 45–52   | Second Time Derivative of Mean Motion divided by six (decimal point assumed) ( $\ddot{n}/6$ ) | 00000-0      |
| 11    | 54–61   | BSTAR drag term (decimal point assumed)   | -11606-4     |
| 12    | 63–63   | The number 0 (originally this should have been "Ephemeris type")                              | 0            |
| 13    | 65–68   | Element set number. Incremented when a new TLE is generated for this object                   | 292          |
| 14    | 69–69   | Checksum (modulo 10) (Letters, blanks, periods, plus signs = 0; minus signs = 1)              | 7            |

$$B^* = \frac{1}{2} \frac{c_D A}{m} \rho_o R_{\oplus} \longrightarrow BC = \frac{1}{12.741\,621\,B^*} \frac{\text{kg}}{\text{m}^2}$$

# Satellite State Representations

## Line 2

2 25544 51.6416 247.4627 0006703 130.5360 325.0288 15.72125391563537

| Field | Columns | Content   | Example     |
|-------|---------|---|-------------|
| 1     | 01–01   | Line number of Element Data                     | 2           |
| 2     | 03–07   | Satellite number                                | 25544       |
| 3     | 09–16   | Inclination (degrees)                           | 51.6416     |
| 4     | 18–25   | Right ascension of the ascending node (degrees) | 247.4627    |
| 5     | 27–33   | Eccentricity (decimal point assumed)            | 0006703     |
| 6     | 35–42   | Argument of perigee (degrees)                   | 130.5360    |
| 7     | 44–51   | Mean Anomaly (degrees)                          | 325.0288    |
| 8     | 53–63   | Mean Motion (revolutions per day)               | 15.72125391 |
| 9     | 64–68   | Revolution number at epoch (revolutions)        | 56353       |
| 10    | 69–69   | Checksum (modulo 10)                            | 7           |