Linear Quadratic Integral Differential Game applied to the Real-time Control of a Quadrotor Experimental setup

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Abstract.

The accurate attitude control of a quadrotor is necessary, especially when facing disturbance. Moreover, all the flight states of the quadrotor are not measured in practice. In this study, a linear quadratic Gaussian with integral action based on the differential game theory is implemented on the quadrotor experimental setup. A continuous state-space model of the setup is derived using the linearization of nonlinear equations of motion, and its parameters are identified with the experimental results. Then, the variables of the quadrotor setup are estimated based on an extended Kalman filter to compensate in the controller structure. Next, the attitude control commands of the quadrotor are derived based on two players; one finds the best attitude control command, and the other creates the disturbance by mini-maximizing a quadratic criterion, defined as the sum of outputs plus the weighted control effort and disturbance. The performance of the proposed structure is investigated in level flight and compared to the linear quadratic regulator controller. Results demonstrate that the proposed approach has an excellent performance in dissipating the disturbances.

Keywords: Linear Quadratic Gaussian, Differential Game, Quadrotor, State Estimation, 3DoF Experimental setup, Optimal Control, Robust Control.

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1 Introduction

A quadrotor is a type of helicopter with four rotors that plays a significant role in today's society (Fathoni, 2021), including research, military, imaging, recreation, and agriculture. The performance of the quadrotor relies on the control system, including attitude, altitude, and position subsystems. In the attitude control of the quadrotor, it is vital to maintain the attitude outputs at the desired level using control commands such as the rotational speed of the rotors (Sharifi, 2019), when the disturbances occur suddenly. Therefore, much research is being conducted on the automatic control of the attitudes' quadrotor in facing the disturbance.

In (H. Bolandi, 2013) (Abdul Salam, 2019), a Proportional Integral Derivative (PID) controller is used to regulate the quadrotor attitude. However, the control objectives have not been effectively achieved with this controller when the disturbance occurs. To solve this problem the model-based approaches (Bouzid, 2020) (Wang, 2020) are utilized for controller design. These controllers work based on information from the quadrotor's attitude model and disturbance to produce the best control command.

Various model-based controllers can be found within the literature, the most well-known of which are intelligent control, the nonlinear control, robust control, and optimal control to reduce the disturbance effect in the attitude control and provide a faster control algorithm in facing the modeling error. In the intelligent controller category, the artificial intelligence computing approaches like fuzzy logic (K.

Liu, 2022) iterative learning (L. V. Nguyen, 2021) machine learning (C. Nicol, 2008), reinforcement learning (C.-H. Pi, 2021), and evolutionary computation (P. Ghiglino, 2013) have been utilized to regulate the quadrotor's attitude.

Nonlinear control methods such as Feedback Linearization (FBL) (A. Aboudonia, 2016), Sliding Mode Control (SMC) (Chen, 2014) and Synergetic Control (Chara, 2022) have been applied to control the roll, pitch, and yaw angles of the quadrotor. Moreover, robust control strategies such as H_{∞} (Azar, 2020) (El-Badawy) and μ- synthesis (Dean, 2017) have been implemented to stabilize the quadrotor attitudes based on the worst-case scenario and large uncertainty ranges. In the optimal controller category, a Linear Quadratic Regulator (LQR) (Z. Shulong, 2013) and Linear Quadratic Gaussian (LQG) (E. Barzanooni, 2015) have been implemented on the quadrotor based on the minimization of a quadratic criterion, including regulation performance and control effort to provide optimally controlled feedback gains.

Linear Quadratic Regulator Differential Game (LQR-DG) control approach (Engwerda J. C., 2006), (Engwerda J. , 2022) is a class of optimal and robust controller methods that controls the outputs of a system based on its linear model and mini-maximization of a cost function. This approach has been utilized to stabilize and control various nonlinear and complex systems such as a ship controller (Zwierzewicz, 2014) (Li, 2011). Moreover, in the LQR-DG control method, the control commands are analytically generated based on a pursuit-evasion of two players, one tracks the best control command, and the other creates the disturbance. This is one of the distinctive features of the LQR-DG controller and an important difference from other optimal control methods.

In this study, a LQG controller method based on the differential game theory, with an integral action called Linear Quadratic Integral Gaussian Differential Game (LQIG-DG) controller, is proposed to generate the most efficient control command for an experimental setup of the quadrotor when facing the disturbance. Since the LQIG-DG is affected by an accurate model of the system, first, the dynamic of the three-degree-of-freedom setup of the quadrotor is modeled. Then, the linear state-space form the quadrotor model is extracted using the linearization of the nonlinear equations of motion to utilize in the proposed control problem. Moreover, the model's parameters are identified and verified against the experimental values. Next, the flight states of the quadrotor setup are estimated based on an Extended Kalman Filter (EKF) (Kunwu Zhang, 2016) (Azid, 2021) and then compensated using the LQIG-DG controller architecture. Finally, the LQIG-DG technique is applied to the experimental setup of the quadrotor to reduce the effect of disturbance. The performance of the suggested controller is examined when the disturbance occurs. The results show the successful performance of the LQIR-DG scheme in reducing the disturbance.

In the remainder of this study, the problem is defined in section 2. In sections 3, the dynamics model for the experimental setup of the quadrotor and the estimation problem are derived in details, respectively. In section , the LQIR-DG architecture is denoted. Finally, in sections 5 and 6, numerical results and conclusion are provided, respectively.

2 Problem Statement

Here, a nonlinear dynamic is presented for the setup of the quadrotor, as illustrated in Fig. 1. The quadrotor is free to rotate about its roll, pitch, and yaw axes. The Euler angles and angular velocities along three orthogonal axes are measured using the Attitude and Heading Reference Systems (AHRS). These noisy measurements are utilizes in the LQIR-DG for control of the Euler angles. The block diagram of the controller structure is illustrated in Fig. 2.

Fig. 1. 3DoF setup of the quadrotor.

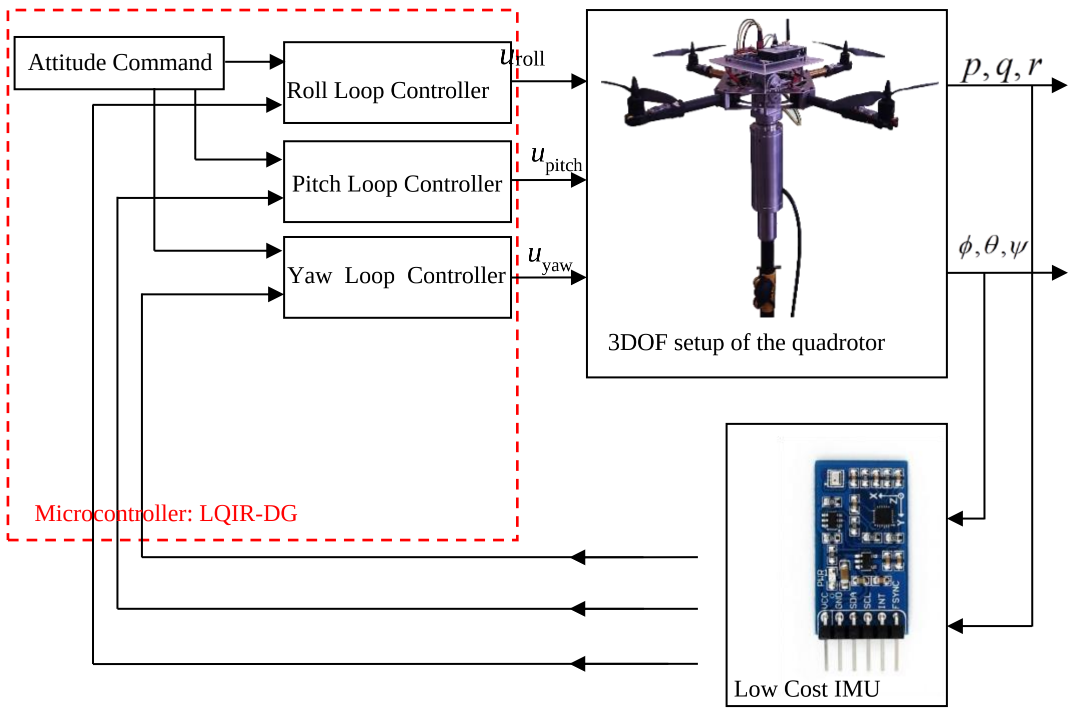


Fig. 2. Block diagram of the LQIG-DG controller structure.

3 Modeling of the Quadrotor Setup

Here, the model of the three-degree-of-freedom setup of the quadrotor is presented in details. For this purpose, first, the configuration of the quadrotor is denoted. Then, the nonlinear model of the attitude dynamics is derived to denote the state-space form. In the next step, the nonlinear model is linearized to utilize in the control purposes. Finally, the model parameters of the 3DOF experimental setup are identified based on the experimental data.

3.1 Configuration of the Quadrotor

Fig. 3 denotes the quadrotor schematic. Each rotor has an angular velocity, Ω_i, rotating about the z_B axis in the body coordinate system. Rotors 1 and 3 rotate counterclockwise, while rotors 2 and 4 rotate clockwise, to cancel yawing moment.

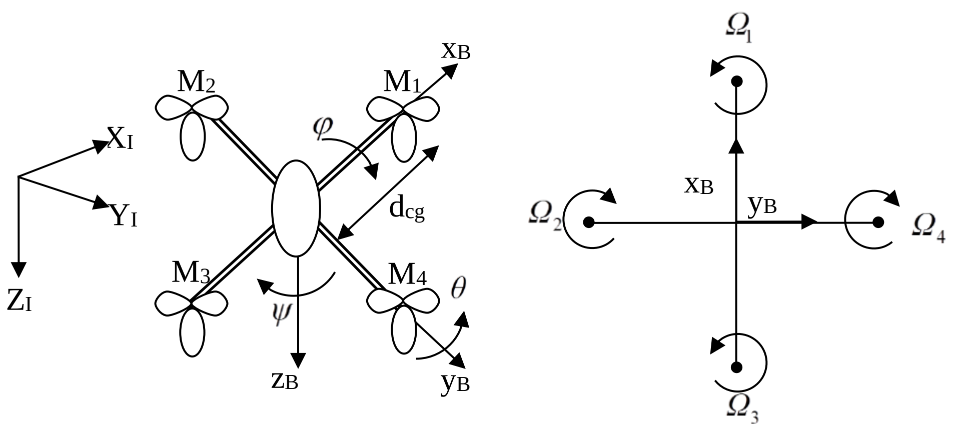


Fig. 3. Configuration of the quadrotor

3.2 Dynamic Model

The quadrotor kinetic model, derived using the Newton-Euler method, is stated as (Bouabdallah, 2007), (Siegwart, 2007)

$$\dot{p} = \frac{\mathrm{I}_{yy} - \mathrm{I}_{zz}}{\mathrm{I}_{xx}} qr + q\frac{\mathrm{I}_{rotor}}{\mathrm{I}_{xx}}\Omega_r + \frac{u_{roll}}{\mathrm{I}_{xx}} + \frac{d_{roll}}{\mathrm{I}_{xx}} \tag{1}$$

$$\dot{q} = \frac{\mathrm{I}_{zz} - \mathrm{I}_{zz}}{\mathrm{I}_{yy}} rp + p\frac{\mathrm{I}_{rotor}}{\mathrm{I}_{xx}}\Omega_r + \frac{u_{pitch}}{\mathrm{I}_{yy}} + \frac{d_{pitch}}{\mathrm{I}_{yy}} \tag{2}$$

$$\dot{r} = \frac{I_{xx} - I_{yy}}{I_{zz}} pq + \frac{u_{yaw}}{I_{zz}} + \frac{d_{yaw}}{I_{zz}} \tag{3}$$

where (p,q,r) are the angular velocities. d_{roll}, d_{pitch}, and d_{yaw} are the disturbances, generated in x_B, y_B. and z_B, respectively. Moreover, I_{xx}, I_{yy}, and I_{zz} are the principal moment of inertia and I_{rotor} is a rotor inertia about its axis. The relation between the angular body rates and the Euler angles rates are obtained as

$$\dot{\phi} = p + (q\sin(\phi) + r\cos(\phi))\tan(\theta) \tag{4}$$

$$\dot{\theta} = q\cos(\phi) - r\sin(\phi) \tag{5}$$

$$\dot{\psi} = (q\sin(\phi) + r\cos(\phi)) / \cos(\theta) \tag{6}$$

where (ϕ,θ,ψ) are roll, pitch, and yaw angles. Moreover, Ω_r, called the overall residual rotor angular velocity, is computed as

$$\Omega_r = -\Omega_1 + \Omega_2 - \Omega_3 + \Omega_4 \tag{7}$$

3.3 Control Commands

The control inputs u_{roll}, u_{pitch}, and u_{yaw} are roll, pitch, and yaw moments, obtained from the rotors, defined as

$$u_{roll} = \mathrm{bd_{cg}}(\Omega_2^2 - \Omega_4^2) \tag{8}$$

$$u_{pitch} = \mathrm{bd_{cg}}(\Omega_1^2 - \Omega_3^2) \tag{9}$$

$$u_{yaw} = \mathrm{d}(\Omega_1^2 - \Omega_2^2 + \Omega_3^2 - \Omega_4^2) \tag{10}$$

Also, d and b are, respectively, drag and thrust coefficients. d_{cg} is the distance of rotors from the gravity center . Hence, the angular velocity commands are obtained as

$$\Omega_{c,1}^2 = \Omega_{\mathrm{mean}}^2 + \frac{1}{2\mathrm{bd}_{\mathrm{cg}}} u_{\mathrm{pitch}} + \frac{1}{4\mathrm{d}} u_{\mathrm{yaw}} \tag{11}$$

$$\Omega_{c,2}^2 = \Omega_{\mathrm{mean}}^2 + \frac{1}{2\mathrm{bd}_{\mathrm{cg}}} u_{\mathrm{roll}} - \frac{1}{4\mathrm{d}} u_{\mathrm{yaw}} \tag{12}$$

$$\Omega_{c,3}^2 = \Omega_{\mathrm{mean}}^2 - \frac{1}{2\mathrm{bd}_{\mathrm{cg}}} u_{\mathrm{pitch}} + \frac{1}{4\mathrm{d}} u_{\mathrm{yaw}} \tag{13}$$

$$\Omega_{c,4}^2 = \Omega_{\mathrm{mean}}^2 - \frac{1}{2\mathrm{bd}_{\mathrm{cg}}} u_{\mathrm{roll}} - \frac{1}{4\mathrm{d}} u_{\mathrm{yaw}} \tag{14}$$

where Ω_{mean} is the nominal of the rotor angular velocities.

3.4 State-Space Form

Here, the state-space model is presented for the control purposes. By defining $x_1 = p$, $x_2 = q$, $x_3 = r$, $x_4 = \phi$, $x_5 = \theta$, and $x_6 = \psi$; the model of in state-space form are denoted as

$$\dot{x}_1 = \Gamma_1 x_2 x_3 + \Gamma_2 x_2 \Omega_r + \Gamma_3 u_{\mathrm{roll}} + \Gamma_3 d_{\mathrm{roll}} \tag{15}$$

$$\dot{x}_2 = \Gamma_4 x_1 x_3 - \Gamma_5 x_1 \Omega_r + \Gamma_6 \left(u_{\mathrm{pitch}} + d_{\mathrm{pitch}} \right) \tag{16}$$

$$\dot{x}_3 = \Gamma_7 x_1 x_2 + \Gamma_8 \left(u_{\mathrm{yaw}} + d_{\mathrm{yaw}} \right) \tag{17}$$

$$\dot{x}_4 = x_1 + (x_2 \sin(x_4) + x_3 \cos(x_4)) \tan(x_5) \tag{18}$$

$$\dot{x}_5 = x_2 \cos(x_4) - x_3 \sin(x_4) \tag{19}$$

$$\dot{x}_6 = (x_2 \sin(x_4) + x_3 \cos(x_4)) / \cos(x_5) \tag{20}$$

Moreover, Γ_i (i=1,…,8) is defined as

$$\begin{aligned}
&\Gamma_1 = \frac{\mathrm{I_{yy}} - \mathrm{I_{zz}}}{\mathrm{I_{xx}}}; \Gamma_2 = \frac{\mathrm{I_{rotor}}}{\mathrm{I_{xx}}}; \Gamma_3 = \frac{1}{\mathrm{I_{xx}}};\\
&\Gamma_4 = \frac{\mathrm{I_{zz}} - \mathrm{I_{zz}}}{\mathrm{I_{yy}}}; \Gamma_5 = \frac{\mathrm{I_{rotor}}}{\mathrm{I_{yy}}}; \Gamma_6 = \frac{1}{\mathrm{I_{yy}}};\\
&\Gamma_7 = \frac{\mathrm{I_{xx}} - \mathrm{I_{yy}}}{\mathrm{I_{zz}}}; \Gamma_8 = \frac{1}{\mathrm{I_{zz}}};
\end{aligned} \tag{21}$$

The measurement model is written as

$$\mathrm{z} = \begin{bmatrix} p_m & q_m & r_m & \phi_m & \theta_m & \psi_m \end{bmatrix}^{\mathrm{T}} \tag{22}$$

3.5 Linear Model

The continuous-time linear model is utilized to drive the control commands on the quadrotor. The linear state-space model is denoted as

$$\dot{\mathrm{x}}(t) = \mathrm{Ax}(t) + \mathrm{Bu}(t) + \mathrm{B_d d}(t) \tag{23}$$

where A, B, and $\mathrm{B_d}$ are the system, input and disturbance matrices, respectively. Moreover, d is the disturbance. The measurements equation is stated as

$$\mathrm{z}(t) = \mathrm{x}(t) \tag{24}$$

According to Eqs.(15)-(20) the linear dynamic model around the equilibrium points $(\mathrm{x}_e = 0 \text{ and } \mathrm{u}_e = 0)$ of. the quadrotor setup is denoted as

$$\dot{\mathbf{x}} = \begin{bmatrix} \dot{\mathbf{x}}_{\text{roll}} \\ \dot{\mathbf{x}}_{\text{pitch}} \\ \dot{\mathbf{x}}_{\text{yaw}} \end{bmatrix} = \begin{bmatrix} \mathbf{A}_{\text{roll}} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{A}_{\text{pitch}} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{A}_{\text{yaw}} \end{bmatrix} \begin{bmatrix} \mathbf{x}_{\text{roll}} \\ \mathbf{x}_{\text{pitch}} \\ \mathbf{x}_{\text{yaw}} \end{bmatrix} + \begin{bmatrix} \mathbf{B}_{\text{roll}} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{B}_{\text{pitch}} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{B}_{\text{yaw}} \end{bmatrix} \begin{bmatrix} \mathbf{u}_{\text{roll}} \\ \mathbf{u}_{\text{pitch}} \\ \mathbf{u}_{\text{yaw}} \end{bmatrix} + \begin{bmatrix} \mathbf{B}_{\text{roll}} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{B}_{\text{pitch}} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{B}_{\text{yaw}} \end{bmatrix} \begin{bmatrix} \mathbf{d}_{\text{roll}} \\ \mathbf{d}_{\text{pitch}} \\ \mathbf{d}_{\text{yaw}} \end{bmatrix} \tag{25}$$

where $\mathrm{x}_{\text{roll}} = [p \quad \phi]^{\mathrm{T}}$, $\mathrm{x}_{\text{pitch}} = [q \quad \theta]^{\mathrm{T}}$, and $\mathrm{x}_{\text{yaw}} = [r \quad \psi]^{\mathrm{T}}$. Moreover, the state and input matrices are presented as

$$\mathrm{A}_{\text{roll}} = \mathrm{A}_{\text{pitch}} = \mathrm{A}_{\text{yaw}} = \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix} \tag{26}$$

$$\mathrm{B}_{\text{roll}} = \begin{bmatrix} \Gamma_3 \\ 0 \end{bmatrix} . \mathrm{B}_{\text{pitch}} = \begin{bmatrix} \Gamma_6 \\ 0 \end{bmatrix} ; \mathrm{B}_{\text{yaw}} = \begin{bmatrix} \Gamma_8 \\ 0 \end{bmatrix} \tag{27}$$

3.6 Identification of the Setup Parameters

In this section, the optimization technique based on the Nonlinear Least Squares (NLS) method is utilized to estimate the model parameters ($\mathbf{\Gamma}$) for the 3DOF experimental setup from experimental data. Here, the NLS algorithm, that is based on the trust-region reflective least squares (TRRLS) method, finds iteratively the values of the model parameters based on the minimization of the cost function, so that the input/output signals provided by the simulation model are very similar to the experimental ones. Therefore, the least squares problem consists in finding a vector $\mathbf{\Gamma}$ that minimizes a sum of squares function [?], as follows:

$$\min_{\Gamma_i} \left(\| e(\Gamma_i) \|^2 \right) = \min_{\Gamma_i} \left(\sum_{i=1}^{n} (y_i - \hat{y}_i)^2 \right) \tag{28}$$

where $\min_{\rho}\left(\|e(\rho)\|^2\right)=\min_{\rho}\left(\sum_{i=1}^{n}(y_i-\hat{y}_i)^2\right)$ and $\min_{\rho}\left(\|e(\rho)\|^2\right)=\min_{\rho}\left(\sum_{i=1}^{n}(y_i-\hat{y}_i)^2\right)$ are the simulated and experimental outputs, when the same input signals are applied ones. Moreover, a vector $\boldsymbol{\rho}$ has upper and lower bound constraints, ub and lb, respectively, with lb $lb \le \rho \le ub$. The structure of the proposed identification approach is illustrated in Figure 1.

Figure 4. Structure of TRRLS identification approach.

4 Formulation of the Controller Design

In the LQIR-DG controller structure, an integral action is added to the LQR-DG controller to cancel the steady-state errors for reference tracking. For this purpose, first, the augmented state space of the linear quadrotor model is defined to utilize in the controller architecture. Then, the LQR-DG controller design procedure is presented to produce the best control commands for the experimental setup of the quadrotor.

4.1 Augmented State Space Formulation

To add the integral action to the controller structure, the augmented states are defined as follows:

$$\mathrm{x}_{\mathrm{a_i}}=\begin{bmatrix}\mathrm{x_i} & \int \mathrm{x_i}\end{bmatrix}^{\mathrm{T}} \tag{29}$$

where i = roll, pitch, and yaw.

Then, the quadrotor dynamics model, denoted by Eq.(**23**), is denoted in the augmented state-space model as

$$\dot{\mathrm{x}}_{\mathbf{a}}(t) = \mathrm{A_a x_a}(t) + \mathrm{B_a u}(t) + \mathrm{B_{d_a} d}(t) \tag{30}$$

where matrices $\mathrm{A_a}$ and $\mathrm{B_a}$ are defined as follows:

$$\mathrm{A_a} = \begin{bmatrix} \mathrm{A} & \mathbf{0} \\ \mathrm{I} & \mathbf{0} \end{bmatrix} \tag{31}$$

$$\mathrm{B_a} = \mathrm{B_{d_a}} = \begin{bmatrix} \mathrm{B} \\ \mathbf{0} \end{bmatrix} \tag{32}$$

In the above equation I denotes the identity matrix.

4.2 LQIR-DG Controller Method

The LQIR-DG controller is an optimal and robust method based on the differential game theory. This controller consists of two essential players: one finds the best control command, and the other creates the worst disturbance.

For this purpose, the first player tries to minimize a cost function; while the second player is assumed to maximize it. Therefore, the quadratic cost function equation is denoted using min-max operators as follows:

$$\min_u \max_d J(\mathrm{x_{a_i}}, u_i, d_i) = J(\mathrm{x_{a_i}}, u_i^*, d_i^*) = \min_u \max_d \int_0^{\mathrm{t_f}} \left(\mathrm{x_{a_i}^T Q_i x_{a_i}} + u_i^{\mathrm{T}} R u_i - d_i^{\mathrm{T}} R_d d_i \right) \mathrm{d}t \tag{33}$$

where R and R_d are symmetric nonnegative definite matrices and $\mathrm{Q_i}$ is a symmetric positive definite matrix. Moreover, $\mathrm{t_f}$ is the final time. To solve this problem, connections between the general optimal problem and the LQIR problem are considered (Engwerda J. C., 2006) and consequently the optimum control effort is computed for the each control loop as follows:

$$u_i(t) = -\mathrm{K}_{\mathbf{i}}(t)\mathrm{x}_{\mathrm{a_i}}(t) \tag{34}$$

$$d_i(t) = \mathrm{K}_{\mathbf{i}}(t)\mathrm{x}_{\mathrm{a_i}}(t) \tag{35}$$

where $\mathrm{K_i}$ and $\mathrm{K_{d_i}}$ are a time varying gain, given by

$$\mathrm{K_i} = R^{-1}\mathrm{B}^{\mathrm{T}}_{\mathbf{a_i}}\mathrm{P}_{\mathbf{a_i}}(t) \tag{36}$$

$$\mathrm{K_{d_i}} = R_d^{-1}\mathrm{B}^{\mathrm{T}}_{\mathbf{a_{d_i}}}\mathrm{P}_{\mathbf{a_{d_i}}}(t) \tag{37}$$

where $\mathrm{P}_{\mathbf{a_i}}(t)$ and $\mathrm{P}_{\mathbf{a_{d_i}}}(t)$ satisfy

$$\dot{\mathrm{P}}_{\mathbf{a_i}}(t) = -\mathrm{A}_{\mathrm{a}}^{\mathrm{T}}\mathrm{P}_{\mathrm{a_i}}(t) - \mathrm{P}_{\mathrm{a_i}}(t)\mathrm{A}_{\mathrm{a}} - \mathrm{Q_i} + \mathrm{P}_{\mathrm{a_i}}(t)\mathrm{S}_{\mathrm{a_i}}(t)\mathrm{P}_{\mathrm{a_i}}(t) + \mathrm{P}_{\mathrm{a_i}}(t)\mathrm{S}_{\mathrm{a_{d_i}}}(t)\mathrm{P}_{\mathrm{a_{d_i}}}(t) \tag{38}$$

$$\dot{\mathrm{P}}_{\mathbf{a_{d_i}}}(t) = -\mathrm{A}_{\mathrm{a}}^{\mathrm{T}}\mathrm{P}_{\mathrm{a_{d_i}}}(t) - \mathrm{P}_{\mathrm{a_{d_i}}}(t)\mathrm{A}_{\mathrm{a}} - \mathrm{Q_i} + \mathrm{P}_{\mathrm{a_{d_i}}}(t)\mathrm{S}_{\mathrm{a_{d_i}}}(t)\mathrm{P}_{\mathrm{a_{d_i}}}(t) + \mathrm{P}_{\mathrm{a_{d_i}}}(t)\mathrm{S}_{\mathrm{a_i}}(t)\mathrm{P}_{\mathrm{a_i}}(t) \tag{39}$$

where $\mathrm{S_{a_i}} = \mathrm{B_{a_i}}R^{-1}\mathrm{B}^{\mathrm{T}}_{\mathbf{a_i}}$ and $\mathrm{S_{a_{d_i}}} = \mathrm{B}_{\mathbf{a_{d_i}}}R_d^{-1}\mathrm{B}^{\mathrm{T}}_{\mathbf{a_{d_i}}}$.

In this study, the steady-state values of the above equations $(\mathrm{P\ as\ t_f} \to \infty)$ are utilized to generate a feedback control law.

5 Result and Discussion

Here, the results of the LQIR-DG controller method are devoted to the control loops of the roll, pitch, and yaw of the experimental setup of the quadrotor. First, the controller parameters are tuned using the results of numerical simulations. Moreover, the performance of the LQIR-DG controller is compared to an LQR control strategy. The quadrotor parameters are shown in **Table 1**. Moreover, the parameters of LQIR-DG controller weight are denoted in **Table 2**.

Table 1. The Parameter of the Quadrotor.

Parameter	Unit	Value
I_{xx}	$kg.m^2$	0.02839

I_{yy}	$kg.m^2$	0.03066
I_{zz}	$kg.m^2$	0.0439
I_{rotor}	$kg.m^2$	4.4398×10^{-5}
b	$N.sec^2 /rad^2$	3.13×10^{-5}
d	$N.m.sec^2 /rad^2$	3.2×10^{-6}
Ω_{mean}	rpm	3000
d_{cg}	m	0.2

Table 2. The Parameters of the LQIR-DG Controller.

Control Loop	Weight	Value
Roll	Q_{roll}	diag([7.91,0.01,631.85, 214.28])
Pitch	Q_{pitch}	diag([9853.09, 0.12, 0.01, 873.93])
Yaw	Q_{yaw}	diag([1.81e-4, 4.5e-4, 3e-6, 1.7e-5])
-	R	1
-	R_d	1.2577

5.1 Identification of the 3DoF experimental setup model

As denoted in section ?, the parameters of the quadrotor setup are Γ_i (i=1,…,8) that need to be identified based on the NRS algorithm. The NLS-TRRLS algorithm is performed in the Matlab R2022a®. In order to increase accuracy identification of parameters, three scenarios, according to ~~**Error! Reference source not found.**~~, are considered and performed. When the stopping condition of the NLS algorithm is reached, the best values of the quadrotor parameters are computed, shown in Table 3. Moreover, the intelligent movement of the parameters during the optimization process for finding the true values is shown in Figure 5.

In the first scenario, according to the Figure ?, the quadrotor is able to rotate about only one axis (roll, pitch or yaw axes) to identify G_3, G_6 and G_8 parameters. In the second scenario, Figure ? shows G_2 and G_5 parameters are estimated based on the experimental setup, that is free to rotate around its roll and pitch axes. Finally, in the last scenario, according to the Figure ?, G_1, G_4 and G_7 parameters of the UAV model are identified by rotate the quadrotor setup around three axis. These results illustrate that the outputs of the simulation results for the quadrotor model are consistent with reality.

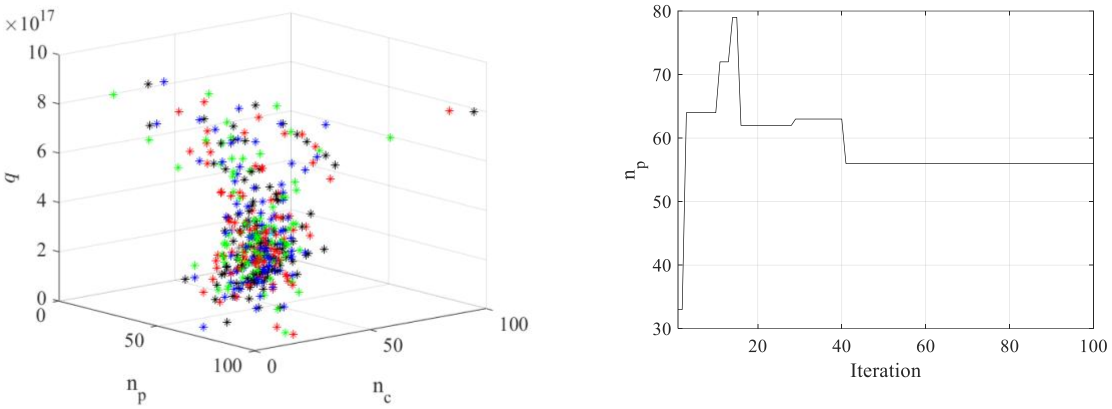
Tabel :Scenarios for identification of quadrotor model.

Scenario	Description	Initial Conditions	angular velocity Commands
I	Roll free	10	10
	Pitch free		
	Yaw free		

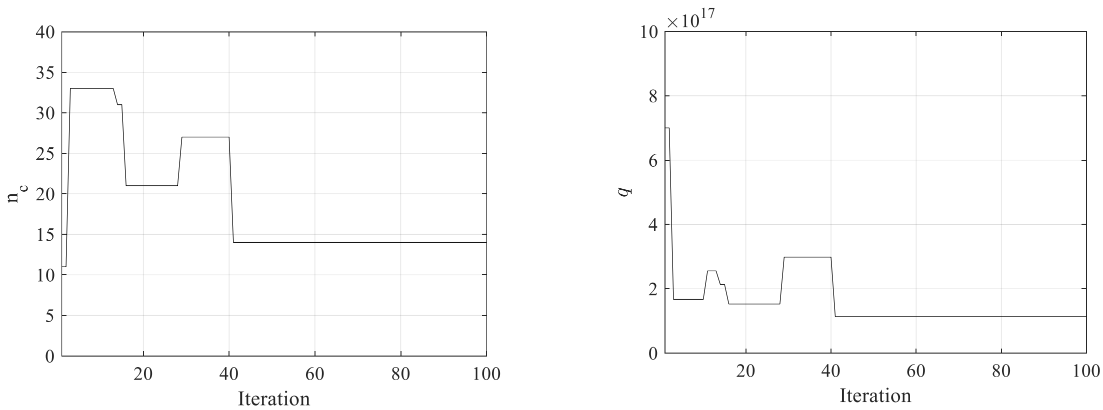
Ii	Roll & Pitch Free	10	5
Iii	Roll, Pitch and Yaw free	20	10

Table 3. True values of the quadrotor parameters.

Parameter	Value	Parameter	Value
Γ_1	69	Γ_i	
Γ_2	37	Γ_i	
Γ_i	7.96e15	Γ_i	
Γ_i	1	Γ_i	



(a)



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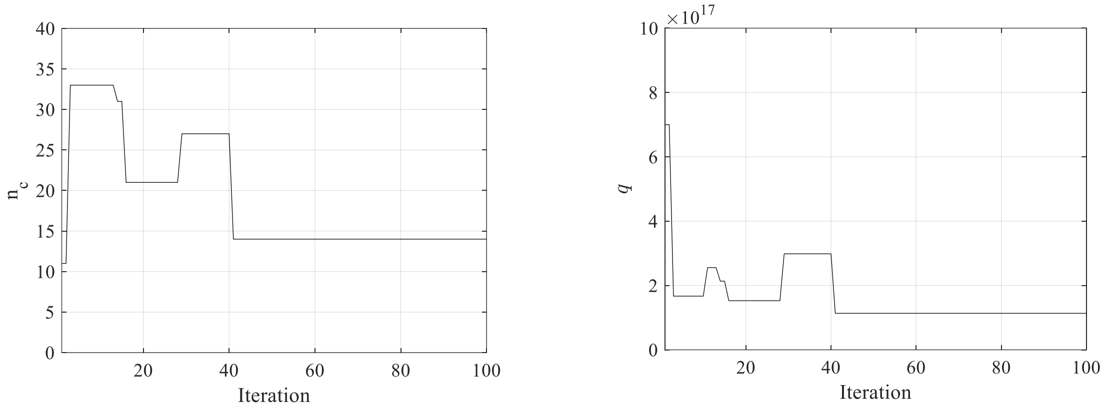
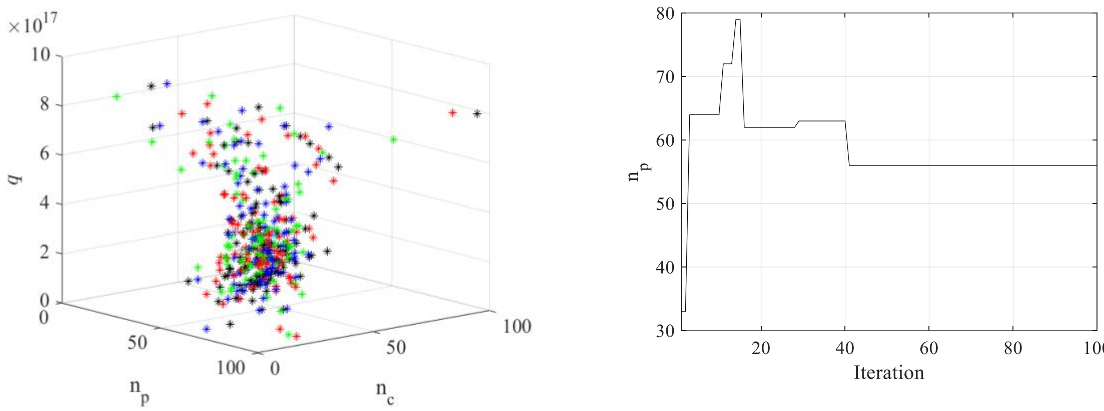
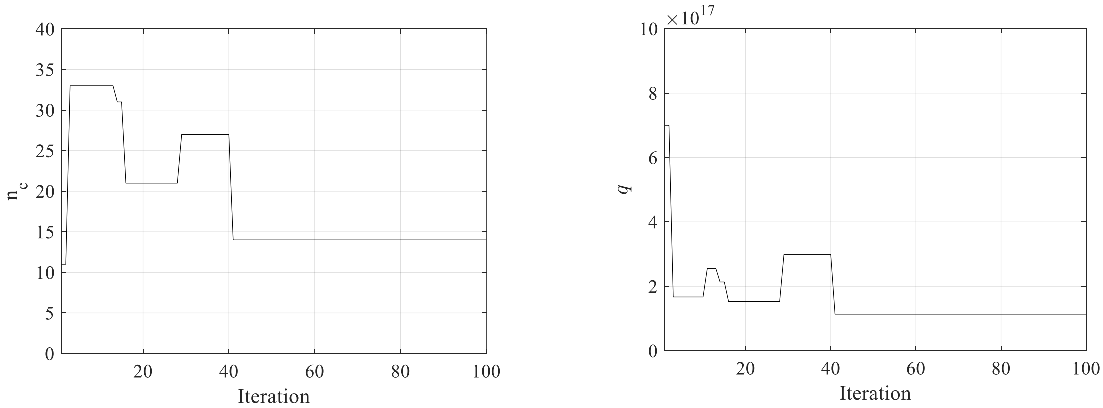


Figure 5. Identification process results when the quadrotor rotates about only one axis: (a) Identification of G_3 in free roll. (b) Identification of G_6 in free pitch. (c) Identification of G_3 in free yaw.



(a)



(b)

Figure 6. Identification process results when the quadrotor rotates about its roll and pitch axes: (a) Comparison of Simulation and experimental results. (b) Identification of G_3 and G_5.

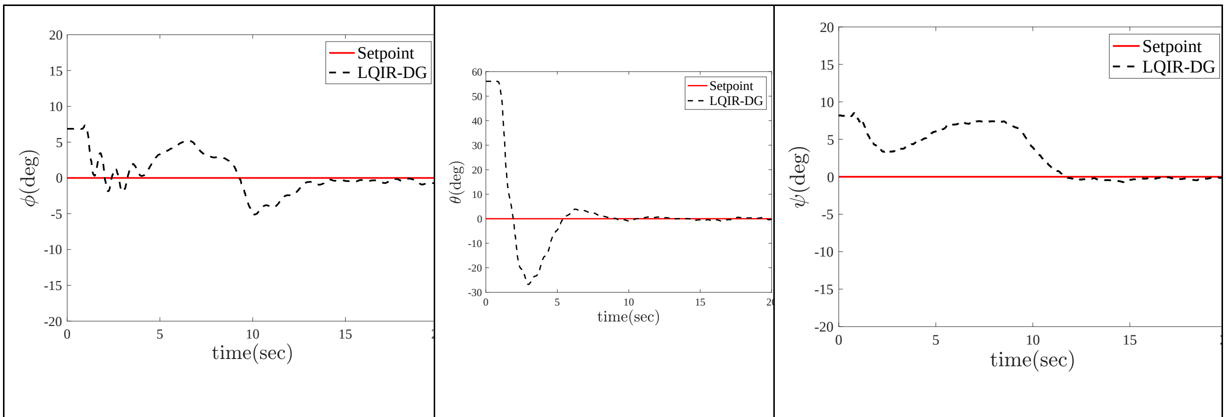
(a)		
(b)		

Figure 7. Identification process results when the quadrotor rotates about its roll, pitch and yaw axes: (a) Comparison of Simulation and experimental results. (b) Identification of G_1, G_4 and G_7 parameters.

5.2 Performance of the LQIR-DG Controller

Here, the performance of the LQIR-DG controller is evaluated. The desired and actual outputs, including the roll, pitch, and yaw angles, are compared in **Fig. 8**. The desired scenario of the simulator is considered as a level flight. These figures show that the attitude outputs of the quadrotor converge to the desired values in less than three seconds. Moreover, **Fig. 9** show the angular velocity command of the quadrotor, respectively. These results illustrate that the LQIR-DG approach appropriately controls the attitude of the experimental setup of the quadrotor.

Fig. 13 illustrates the performance of the LQIR-DG controller in the coupling mode of the roll and pitch channels to track the desired angle as a square wave with a frequency of 0.02 Hz and an amplitude of 20 degrees.



(a)	(b)	(c)

Fig. 8. Performance of the LQIR-DG controller (a) roll angle (b) pitch angle (c) yaw angle

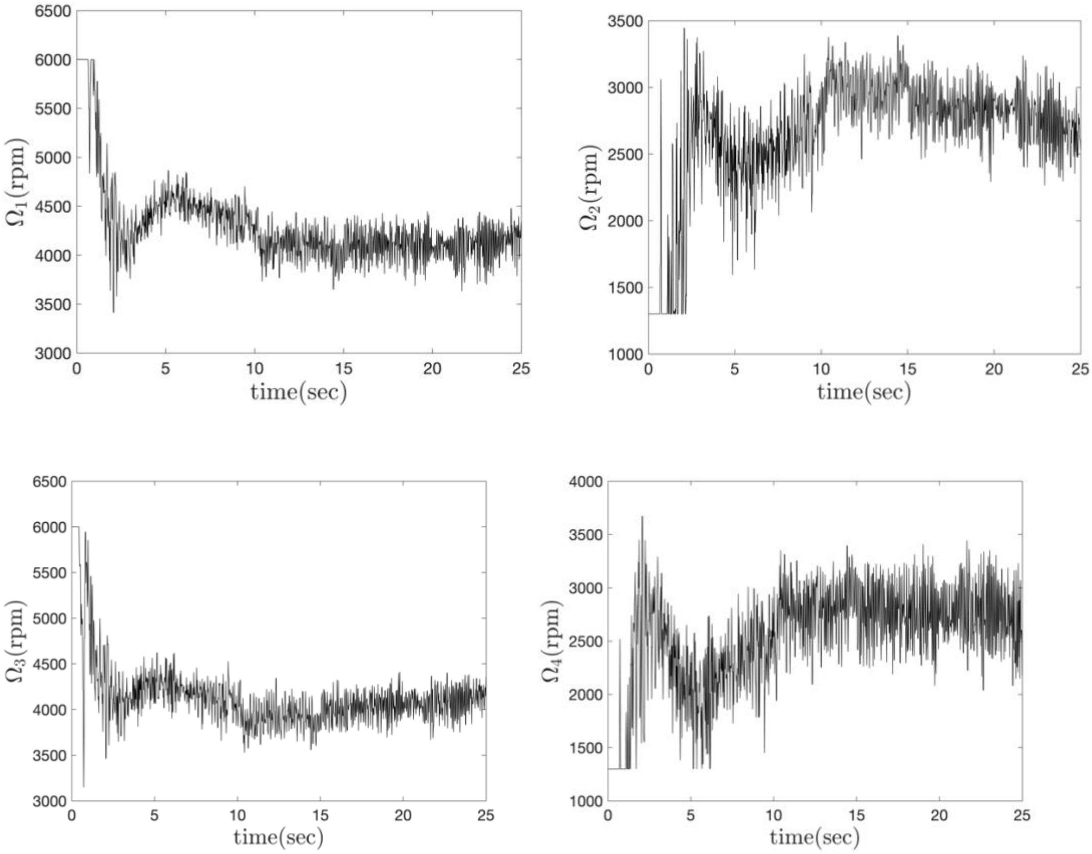
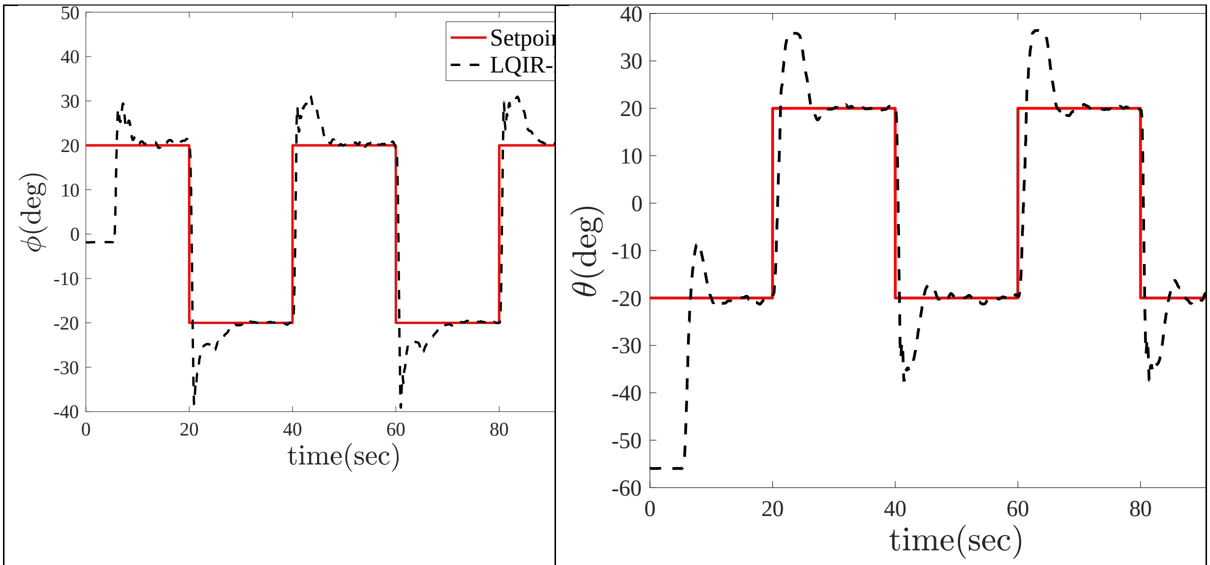


Fig. 9. Time history of angular velocity commands



(a)	(b)

Fig. 10. LQIR-DDG controller performance in order to track the desired angles in the two-degree-of-freedom coupling mode a) Comparison of the roll angle with the desired value b) Comparison of the pitch angle with the desired

5.3 Investigating the possibility of disturbance rejection

This section investigates the possible rejection of input disturbances by the LQIR-DG controller in regulation. For this purpose, a disturbance with an amplitude of 0.5 N is added to the input from 26 to 36 seconds. As shown in Fig. 7, the LQIR-DG controller performs well in coupling the roll and screw channels to remove the input disturbance. In Fig. 7 (a), the performance of this controller is checked by comparing the desired roll angle with the actual roll angle. Also, Fig. 7 (b) compares the desired turn angle with the actual pitch angle of the 3DoF experimental setup in removing the input disturbance. The results indicate the proper performance of the controller in removing the input disturbance.

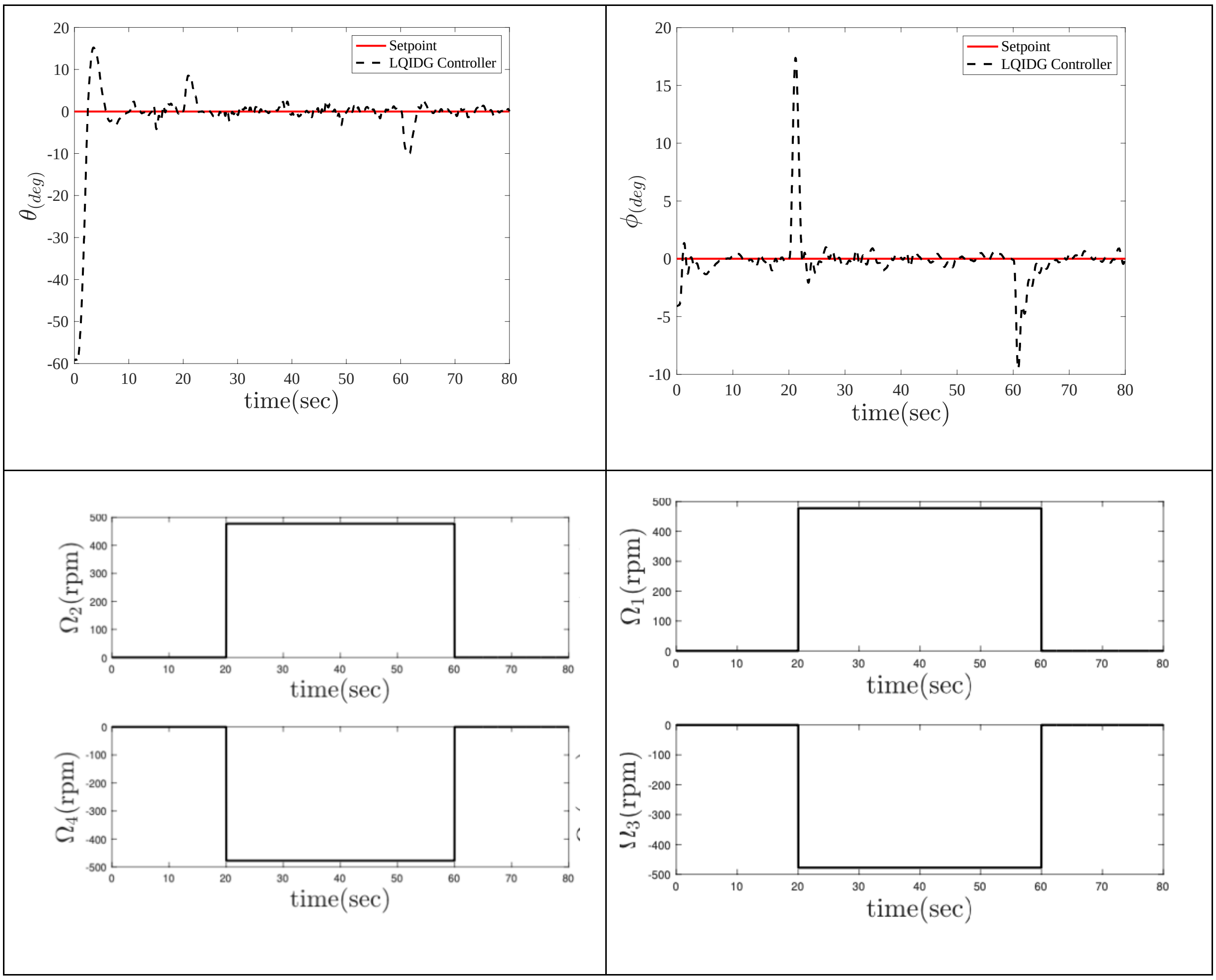
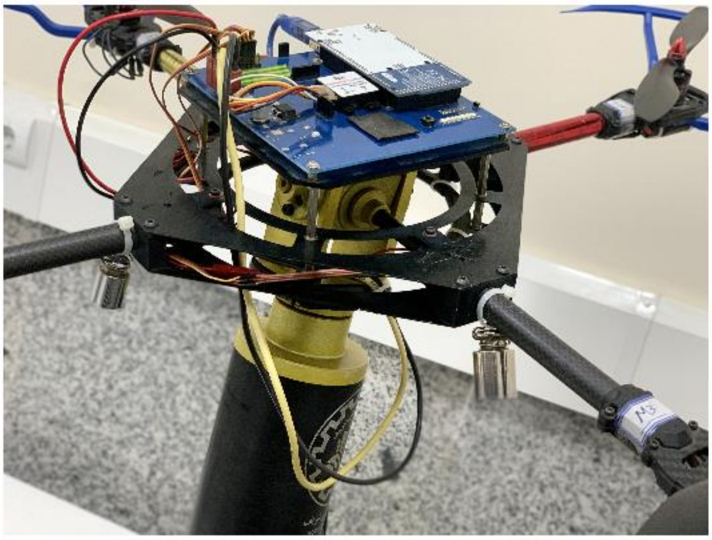


Fig. 11. The performance of the LQIR-DG controller in the presence of the input disturbance in the two-degree-of-freedom coupling mode a) Comparison of the desired roll angle with the actual value b) Comparison of the desired pitch angle with the actual value.

5.4 Investigating the impact of uncertainty in modeling

This section examines the performance of the LQIR-DG controller designed by considering the uncertainty in 3DoF experimental setup modeling. The performance of the sliding mode controller in the coupling mode of the roll, pitch, and yaw channels is checked by considering the uncertainty in the 3DoF experimental setup modeling in figure 17. For this purpose, 50 grams is added to the roll axis and 100 grams to the pitch axis. In figure 17 (a), the performance of this controller is checked by comparing the desired roll angle with the actual roll angle; In figure 17 (b), the performance of this controller is checked by comparing the desired pitch angle to the actual pitch angle. The implementation results indicate the proper efficiency of the LQIR-DG controller in pursuit of the desired value, taking into account the uncertainty in the values of the moments of inertia around each axis of the body coordinate system.



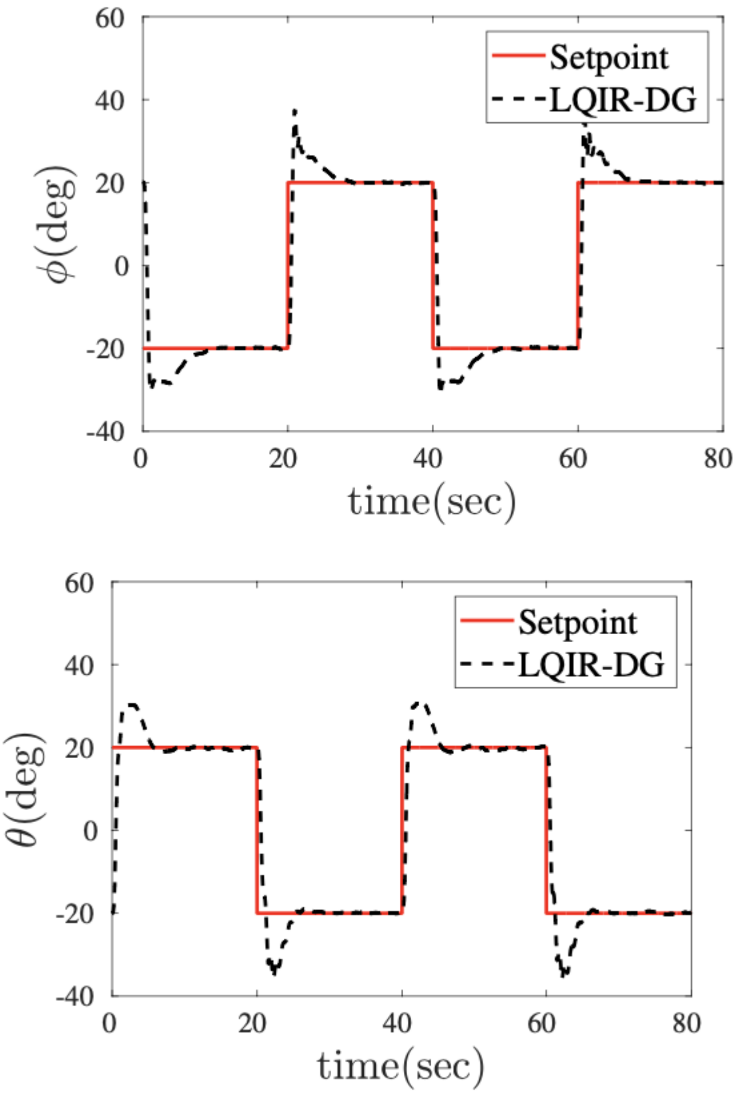
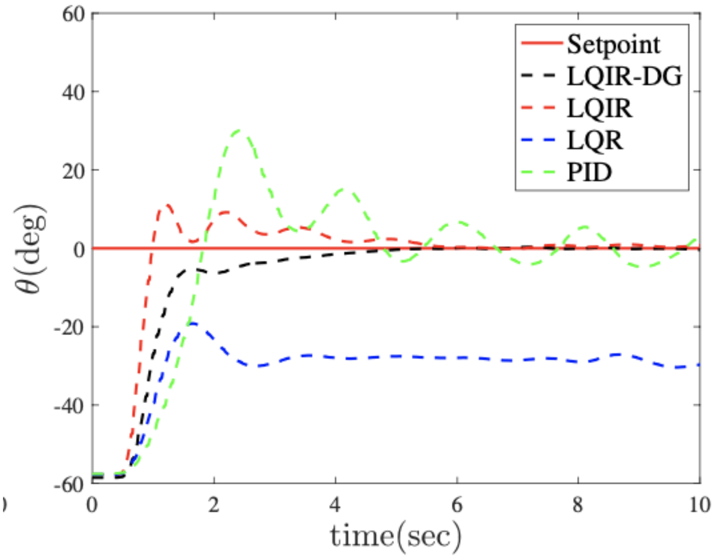


Fig. 12. The performance of the LQIR-DG controller by adding weight to each of the roll and pitch axes in the two-degree-of-freedom coupling mode (a) Comparison of the roll angle with the actual value (b) Comparison of the pitch angle with the actual value

5.5 Comparison with LQR, LQIR, and PID

Here, the LQIR-DG controller performance is compared with famous control strategies such as the LQR controller method. Figure18 compares the quadrotor's desired and actual pitch angle in the presence of these controllers. This result indicates that the LQIR-DG controller can provide high tracking performance, such as good transient response and high rapid convergence relative to the LQR controller for pitch angle control of the quadrotor setup.



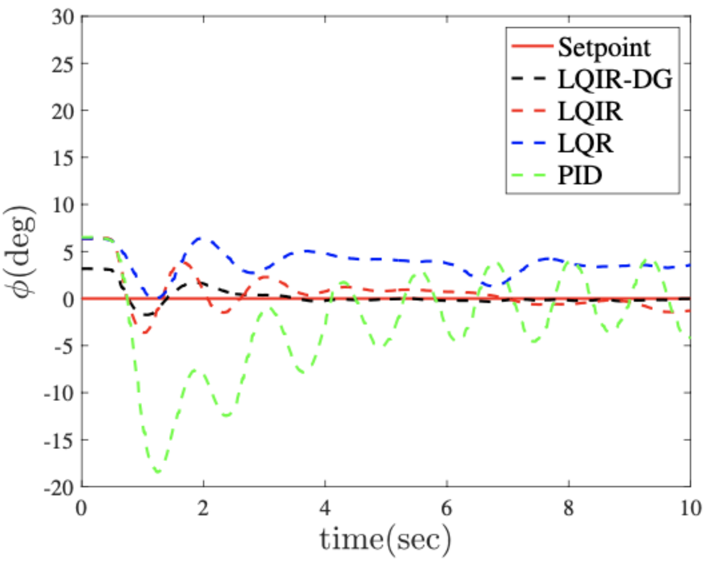


Fig. 13. The performance of the LQIR-DG controller by adding weight to each of the roll and pitch axes in the three-degree-of-freedom coupling mode (a) Comparison of the roll angle with the actual value (b) Comparison of the pitch angle with the actual value (c) Comparison of the yaw angle with the actual value

Figure 19: Comparison of the LQIR-DG to the PID quadratic cost function

Figure 19: Comparison of the LQIR-DG to the PID quadratic cost function

Figure 19: Comparison of the LQIR-DG to the PID quadratic cost function

Figure 19: Comparison of the LQIR-DG to the PID quadratic cost function

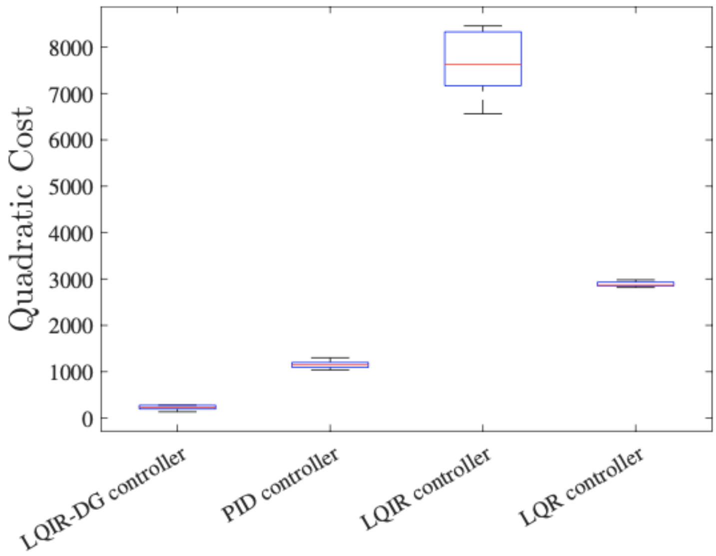


Figure 19: Comparison of the LQIR-DG to the PID quadratic cost function

6 Conclusion

In this study, a linear quadratic with integral action based on the differential game theory, called LQIR-DG, was implemented for level attitude control in an experimental setup of a quadrotor. To implement the proposed controller structure, first, an accurate model of the quadrotor was linearized in the state-space form, and then the model parameters were estimated. Next, two players were considered for each of the quadrotor's roll, pitch, and yaw channels. The first player found the best control command for each channel of the setup of a quadrotor based on the mini-maximization of a quadratic criterion; when the second player produced the worst disturbances. Finally, the performance of the proposed controller was investigated in level flight and compared to the LQR controller. The implementation results verify the successful performance of the LQIR-DG method in the level flight of the attitude control for the actual plant.

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