

L05: Motion and sensor model

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1 Introduction to motion models

$$x_t = g(x_{t-1}, u_t, \varepsilon_t)$$
 in general Non-linear. (1)

As designers we should find the right Transition function $g(\cdot)$ that better describes our system.

Ex: $\begin{array}{c} \text{free point 2D, 3D} \\ \text{wheeled robot} \end{array} \right\} \quad \text{Introduction for today.} \\ \text{car,} \\ \text{airplane,} \\ \text{quadrotor} \\ \text{serial manipulator,} \cdots \end{array}$

2 Free point 2D: Kinematics

$$x_t = \begin{bmatrix} x \\ y \end{bmatrix} \quad u_t = \begin{bmatrix} v_x \\ v_y \end{bmatrix}$$
 velocity (2)



Figure 1: Free point 2D: Kinematics

This corresponds to a free moving point, for now deterministic model (no noise). There are two approaches:

Discrete-time model $x_t = g(x_{t-1}, u_t, \varepsilon_t)|_{\varepsilon_t=0}$ Continuous-time model $\dot{x}_t = f(x, u)$ (Transition eq.)

$$\dot{x} = u = \begin{bmatrix} v_x(t) \\ v_y(t) \end{bmatrix}$$
 cont-time velocities (3)

$$x(t) = x(0) + \int_0^t f(x, u)dt'$$
 continuous-time trajectory (4)



2.1 Numerical method: Euler method, 1st order method

$$\dot{x} = \frac{dx}{dt} \simeq \frac{x(\Delta t) - x(0)}{\Delta t} \tag{5}$$

$$x(\Delta t) \simeq x(0) + \Delta t \cdot \dot{x} = x(0) + \Delta t \cdot f(x(0), u(0)) \tag{6}$$

An alternative to the Euler method are Runge-Kutta methods: which are higher order integration methods.

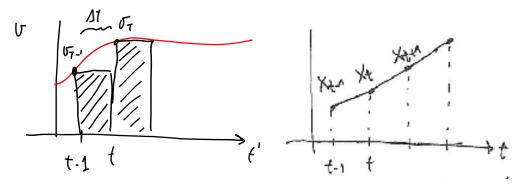


Figure 2: Euler method. On the left, piece-wise constant integration of velocity. On the right, piece-wise linear trajectory.

As a result, the 2D Kinematic point:

$$x_{t} = x_{t-1} + \Delta t \cdot f(x, u) = x_{t-1} + \Delta t \underbrace{\begin{bmatrix} v_{x} \\ v_{y} \end{bmatrix}}_{u}$$
 (Transition function)
$$A = I_{2 \times 2} \qquad B = \Delta t \cdot I_{2 \times 2}$$

2.2 Probabilistic model 2D Kinematic point

$$x_t = x_{t-1} + \Delta t \cdot \begin{bmatrix} v_x \\ v_y \end{bmatrix} + \varepsilon, \qquad \varepsilon \sim \mathcal{N}(0, R)$$
 (8)

Noise is added to the state space (ProbRob p.127)

$$R = \begin{bmatrix} \alpha_1 v_x^2 + \alpha_2 v_y^2 & 0\\ 0 & \alpha_3 v_x^2 + \alpha_4 v_y^2 \end{bmatrix}$$
 (9)

Sometimes, the noise variable is more convenient to be added in the action space:

$$x_{t} = I \cdot x_{t-1} + \Delta t \cdot I \begin{bmatrix} v_{x} + \varepsilon'_{x} \\ v_{y} + \varepsilon'_{y} \end{bmatrix} = x_{t-1} + \Delta t \begin{bmatrix} v_{x} \\ v_{y} \end{bmatrix} + \underbrace{\Delta t \begin{bmatrix} \varepsilon'_{x} \\ \varepsilon'_{y} \end{bmatrix}}_{}$$
(10)

where $\varepsilon' \sim \mathcal{N}(0, M)$ can also be expressed in the action space if we transform the r.v. such as $\varepsilon \sim \mathcal{N}(0, BMB^T)$. It will be crucial to check in which space the noise is defined.



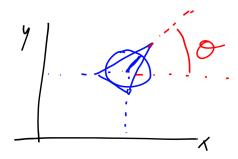


Figure 3: 2D pose. Position and orientation (or heading)

2D pose: Position and orientation (or heading) 3

$$x = \begin{bmatrix} x \\ y \\ \theta \end{bmatrix}$$
 is the state variable. $\dot{x} = \underbrace{\begin{bmatrix} v_x \\ v_y \\ \omega \end{bmatrix}}$ is the control variable.

$$x_{t} = x_{t-1} + \Delta t \cdot u = \begin{bmatrix} x \\ y \\ \theta \end{bmatrix}_{t-1} + \Delta t \begin{bmatrix} v_{x} \\ v_{y} \\ \omega \end{bmatrix}_{t}$$

$$(11)$$

Q: are the heading and position variables decoupled?

There are 3 control variables for 3 state variables $\Rightarrow \forall x \in X$ is reachable.

Linear approximation \rightarrow build probabilities model as before.

Wheeled robots in 2D

$$x_t = \begin{bmatrix} x \\ y \\ \theta \end{bmatrix}$$
 State is a pose: position and orientation

Why not 3D? Wheeled robots (normally) stay on the ground, which we locally approximate as a plane (2D)

Kinematic Unicycle 4

We have already presented the c-t transition equation $\dot{x} = f(x, u)$. This is a deterministic function. Wheels add constraints: heading and velocity are related, see Fig. 4.

$$\frac{dy}{dx} = \tan(\theta) \tag{12}$$

$$\frac{\dot{y}}{\dot{x}} = \frac{\sin \theta}{\cos \theta} \quad \Rightarrow \quad (-\dot{x}\sin \theta + \dot{y}\cos \theta) \cdot v = 0$$

$$\Rightarrow \quad \frac{\dot{x} = v \cdot \cos \theta}{\dot{y} = v \cdot \sin \theta} \quad \text{proof:} -v \cos \theta \sin \theta + v \sin \theta \cos \theta = 0$$
(13)

$$\Rightarrow \begin{array}{c} \dot{x} = v \cdot \cos \theta \\ \dot{y} = v \cdot \sin \theta \end{array} \quad \text{proof:} -v \cos \theta \sin \theta + v \sin \theta \cos \theta = 0 \tag{14}$$

$$\dot{x} = f(x, u) = \begin{bmatrix} v \cdot \cos \theta \\ v \cdot \sin \theta \\ \omega \end{bmatrix} \qquad u = \begin{bmatrix} v \\ \omega \end{bmatrix}$$



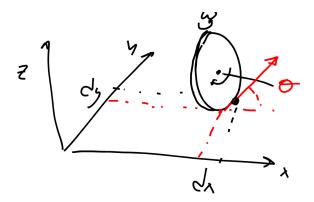


Figure 4: Kinematic Unicycle. Imagine a large disk, it can only move on the theta direction for infinitesimally small increments. Therefore, the constraints to the system follow from this fact.

Still $\forall x \in X$ is reachable. (Proof in Lavalle book).

$$x_{t} = \underbrace{\begin{bmatrix} x_{t-1} + \Delta t \cdot v_{t} \cos \theta_{t-1} \\ y_{t-1} + \Delta t \cdot v_{t} \sin \theta_{t-1} \\ \theta_{t-1} + \Delta t \cdot \omega_{t} \end{bmatrix}}_{q(x_{t-1}, |x_{t}, \xi_{t}||_{x=0})} = I \cdot x_{t-1} + \begin{bmatrix} \Delta t \cdot \cos \theta_{t-1} & 0 \\ \Delta t \cdot \sin \theta_{t-1} & 0 \\ 0 & \Delta t \\ B(x) - \text{Non-linear} \end{bmatrix} \begin{bmatrix} v \\ \omega \end{bmatrix}$$
 (15)

4.1 Unicycle: probabilistic model

Let's first consider the taylor expansion of the non-linear function $g(\cdot)$:

$$x_t = g(x_{t-1}, u_t, \varepsilon_t)|_{\varepsilon_t = 0} \simeq g(\mu_{t-1}, u_t, \varepsilon_t)|_{\varepsilon_t = 0} + G_t(x_{t-1} - \mu_{t-1}) + V_t(\underbrace{\tilde{u}_t - u_t}_{\varepsilon_t}).$$
(16)

The given action u_t , could be seen as the mean, and we have defined in the previous calsses that this is a deterministic variable. The real action value after considering noise could also be defined as single random variable $\tilde{u}_t = u_t + \epsilon_t$, where the noise variable $\epsilon \sim \mathcal{N}(0, M)$. Note then that the Jacobian is necessary only for when the noise is in the action space.

$$G_{t} = \frac{\partial g(x_{t-1}, u_{t})}{\partial x_{t-1}} \bigg|_{\mu_{t-1}} = \begin{bmatrix} 1 & 0 & -\sin\theta_{t-1} \cdot \Delta t v_{t} \\ 0 & 1 & \cos\theta_{t-1} \cdot \Delta t v_{t} \\ 0 & 0 & 1 \end{bmatrix}$$

$$\frac{\partial}{\partial x} \frac{\partial}{\partial y} \frac{\partial}{\partial \theta}$$
(17)

$$V_{t} = \frac{\partial g(x_{t-1}, u_{t})}{\partial u_{t}} \bigg|_{u_{t}} = \begin{bmatrix} \cos\theta_{t-1} \cdot \Delta t & 0\\ \sin\theta_{t-1} \cdot \Delta t & 0\\ 0 & \Delta t \end{bmatrix}$$
(18)

Add noise in the state space:

$$x_t = g(x_{t-1}, u_t, \varepsilon_t) = g(x_{t-1}, u_t, 0) + \varepsilon_t$$
 (19)

where we want to emphasyze the fact that the transition function will produce a new state and the noise is added directly to this state x_t .

$$x_{t-1} \sim \mathcal{N}(\mu_{t-1}, \Sigma_{t-1})$$
 , $\varepsilon_t \sim \mathcal{N}(0, R)$ (state space noise)

$$\Rightarrow x_t \sim N(g(\mu_{t-1}, u_t, 0), G_t \Sigma G_t^T + R)$$
(20)

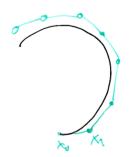


Figure 5: Circular path. In the first order approximation we use linear segments, which has associated some error.

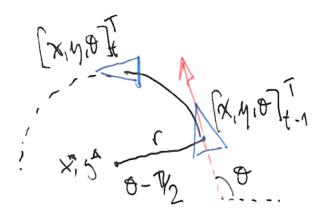


Figure 6: Approximation of the unicycle. In this approach there is a center of rotation (x^*, y^*) , from which the robot describes an arc.

Q: Show this at home.

Example: Circular path give the controls $\theta = 1, \omega = 1$.

Can we do better than Euler Integration? ProbRob Ch5.3 uses a sequence of arcs to approximate the unicycle:

$$\begin{bmatrix} x \\ y \\ \theta \end{bmatrix}_{t} = \begin{bmatrix} x \\ y \\ \theta \end{bmatrix}_{t-1} + \begin{bmatrix} -\frac{v}{\omega}\sin\theta + \frac{v}{\omega}\sin(\theta + \omega\Delta t) \\ \frac{v}{\omega}\cos\theta - \frac{v}{\omega}\cos(\theta + \omega\Delta t) \\ \omega\Delta t + \underbrace{\gamma\Delta t}_{\text{Extra term: final orientation}} \end{bmatrix}_{t} = g(x_{t-1}, u_{t}, 0)$$
 (21)

4.2 Probabilistic Arc Kinematic motion model

$$\begin{bmatrix} \hat{v} \\ \hat{\omega} \end{bmatrix} = \begin{bmatrix} v + \varepsilon_v \\ \omega + \varepsilon_\omega \end{bmatrix} , \quad \varepsilon \sim \mathcal{N}(0, M) \quad \text{(Jacobians in ProbRob p.127)}$$

$$x_t \sim \mathcal{N}(g(\mu_{t-1}, u_t, 0), \quad G_t \Sigma_{t-1} G_t^T + V_t M V_t^T). \quad (22)$$

5 Odometry model

Counts of increments on spinning wheels (observation) more accurate than velocity models.

$$u = \begin{bmatrix} \delta_{rot1} \\ \delta_{trans} \\ \delta_{rot2} \end{bmatrix} = \begin{bmatrix} atan2(y_t - y_{t-1}, x_t - x_{t-1}) \\ \sqrt{(x_t - x_{t-1})^2 + (y_t - y_{t-1})^2} \\ \theta_t - \theta_{t-1} - \delta_{rot1} \end{bmatrix}$$
(23)



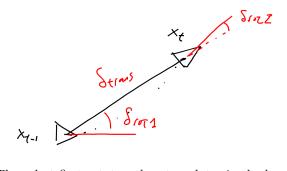


Figure 7: Odometry model. The robot first rotates, then translates in the heading direction and translates a second time to reach any possible end configuration.

Discrete-time transition function:

$$x_{t} = g(x_{t-1}, u_{t}, \varepsilon_{t})|_{\varepsilon_{t}=0} = \begin{bmatrix} x_{t-1} + \delta_{trans} \cos(\theta + \delta_{rot1}) \\ y_{t-1} + \delta_{trans} \sin(\theta + \delta_{rot1}) \\ \theta_{t-1} + \delta_{rot1} + \delta_{rot2} \end{bmatrix}$$
(24)

5.1 Probabilistic odometry model

$$x_{t} = g(x_{t-1}, u_{t}, \varepsilon_{t}) \qquad \begin{array}{c} \text{(noise in action space)} \\ \varepsilon_{t} \sim \mathcal{N}(0, M) & \text{(ProbRob p.139)} \end{array}$$

$$\varepsilon_{t} = \begin{bmatrix} \varepsilon_{\delta_{rot1}} \\ \varepsilon_{\delta_{trans}} \\ \varepsilon_{\delta_{rot2}} \end{bmatrix} \sim \mathcal{N} \begin{pmatrix} 0, \begin{bmatrix} \alpha_{1}\delta_{rot1}^{2} + \alpha_{2}\delta_{trans}^{2} & 0 & 0 \\ 0 & \alpha_{3}\delta_{trans}^{2} + \alpha_{4}(\delta_{rot1}^{2} + \delta_{rot2}^{2}) & 0 \\ 0 & 0 & \alpha_{1}\delta_{rot2}^{2} + \alpha_{2}\delta_{trans}^{2} \end{bmatrix} \end{pmatrix}$$

$$(25)$$

5.2 Jacobian for odometry model

$$G_{t} = \frac{\partial g(x_{t-1}, u_{t}, \varepsilon_{t})}{\partial x_{t-1}} \bigg|_{\mu_{t-1}, \varepsilon_{t} = 0} = \begin{bmatrix} 1 & 0 & -\delta_{trans} \sin(\theta + \delta_{rot1}) \\ 0 & 1 & \delta_{trans} \cos(\theta + \delta_{rot1}) \\ 0 & 0 & 1 \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial \theta} \end{bmatrix}$$
(26)

$$V_{t} = \frac{\partial g(x_{t-1}, u_{t}, \varepsilon_{t})}{\partial u_{t}} \bigg|_{\mu_{t-1}, \varepsilon_{t} = 0} = \begin{bmatrix} -\delta_{trans} \cdot \sin(\theta + \delta_{rot1}) & \cos(\theta + \delta_{rot1}) & 0\\ \delta_{trans} \cdot \cos(\theta + \delta_{rot1}) & \sin(\theta + \delta_{rot1}) & 0\\ 1 & 0 & 1\\ \frac{\partial}{\partial \delta_{rot1}} & \frac{\partial}{\partial \delta_{trans}} & \frac{\partial}{\partial \delta_{rot2}} \end{bmatrix}$$
(27)

6 2D-Rigid Body Transformations

2D poses can be interpreted as a transformation between coordinate frames \rightarrow XYT parameterization. In the example below, between the global frame g and the robot frame r.

$${}^{g}x_{r} = \left[\begin{array}{c} x \\ y \\ \theta \end{array} \right]$$

We need to project point p in the local frame (or robot frame) to the global frame q.

$${}^{g}p = \begin{bmatrix} x_{local} \cdot \cos \theta_{g} - y_{local} \sin \theta_{g} + t_{x} \\ x_{local} \cdot \sin \theta_{g} + y_{local} \cos \theta_{g} + t_{y} \end{bmatrix} = \begin{bmatrix} \cos \theta_{g} & -\sin \theta_{g} & t_{x} \\ \sin \theta_{g} & \cos \theta_{g} & t_{y} \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x_{local} \\ y_{local} \\ 1 \end{bmatrix}$$
(28)



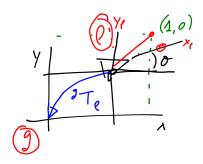


Figure 8: 2D-Rigid Body Transformation. From the local frame to the world frame. This transformation is expressed as a 2D pose.

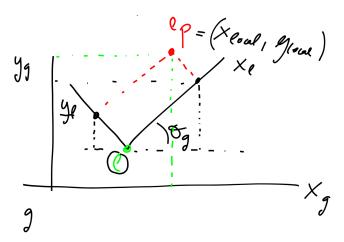


Figure 9: 2D-Rigid Body Transformations 2

We can express this transformation more compactly as a linear transformation of homogeneous coordinates:

$${}^{g}p = \begin{bmatrix} {}^{g}R_{l}(\theta_{g}) & & t \\ 0_{1\times 2} & & 1 \end{bmatrix} \cdot {}^{l}p = {}^{g}T_{l} \cdot {}^{l}p = {}^{g}p.$$
 (29)

Note that the superscript with the point coordinates, has to match the subcript of the transformation, and as a result the new frame of the point is the global frame.

7 RBT composition

Two solutions to transform the same point, one directly from $b \to g$ and the second $b \to a \to g$:

$$g_p = g_b T_b \cdot p_b$$

$$g_p = g_b T_b \cdot p_b$$

$$g_p = g_b T_a \cdot p_b T_a \cdot T_b \cdot p_b$$

8 Sensor models

$$p(z_t|x_t)$$
 Observation distribution (Lecture 4)
 $z_t = h(x_t, \delta_t)$ Observation function

Example: Accelerometer, sensor, radar, Lidar, camera, ...

We will propose a sensor model, but any function relating state and observation is a valid sensor model.

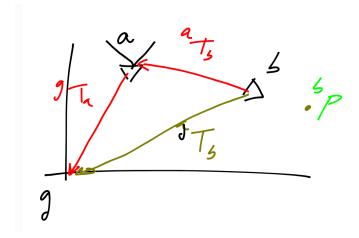


Figure 10: RBT composition. Two solution to transform the point ${}^{b}p$.

8.1 Feature-based measurements model

The idea is to extract features f from observations $f(z_t) = \{f_1, f_2, \dots f_n\}$. **Example:** lines, corners, point description, objects, etc...

Landmark definition: feature which corresponds to physical objects.

$$(2D) \quad f_i = \left[\begin{array}{c} \text{'range'} \\ \text{'bearing'} \\ \text{'signature'} \end{array} \right] = \left[\begin{array}{c} r \\ \phi \\ s \end{array} \right] \qquad \text{s is optional to alleviate data association problem.}$$

$$(\text{color, size, } \mathbb{R}^{60} \text{ embedding, etc ...})$$

each feature corresponds to a location $[m_{i,x}, m_{i,y}]^T$

$$\begin{bmatrix} r_t^j \\ \phi_t^j \\ s_t^j \end{bmatrix} = \begin{bmatrix} \sqrt{(m_{i,x} - x)^2 + (m_{i,y} - y)^2} \\ atan2(m_{i,y} - y, m_{i,x} - x) - \theta \\ s_i \end{bmatrix} + \begin{bmatrix} \delta_{\sigma_r^2} \\ \delta_{\sigma_\phi^2} \\ \delta_{\sigma_z^2} \end{bmatrix} , \quad \delta \sim \mathcal{N}(0, \Sigma_\delta)$$
 (30)

The data association problem: the i^{th} map location m_i corresponds to the j^{th} feature.

$$f^j = h(x_t, m_i) + \delta_t \tag{31}$$

$$f \sim \mathcal{N}(f(z_t); h(\mu_t, m_i), \Sigma_{\delta})$$
 Probabilistic model (32)

Sampling x_t from m_i in ProbRob 180.

9 Summary

- Transition function: $x_t = g(x_{t-1}, u_t)$, discrete-time model obtained by integrating $\dot{x} = f(x, u)$ (NL)
- Probabilistic model:
 - Add noise to the state/action space
 - Linearize $g(\cdot)$
 - Covariance transformation: $x_t \sim N(g(\mu_{t-1}, u_t), G_t \Sigma G_t^T + R))$
- RBT 2D: $p={}^gT_l\cdot{}^lp={}^gT_a\cdot{}^aT_l\cdot{}^lp$ chain of transformations



• Observation function \rightarrow Landmarks:

$$m_i = \begin{bmatrix} m_{i,x} & m_{i,y} \end{bmatrix}^T$$

(features from sensor data:)
$$z = h(x, m_i) = \begin{bmatrix} r & \phi & s \end{bmatrix}^T$$

- range, bearing, appearance

$$p(z|x) \sim N(z; h(\mu_x, m), \Sigma_z)$$