

# Design and Characterization of Photonic Crystal Membrane Reflector Based Vertical Cavity Surface Emitting Lasers on Silicon

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Silicon-based light source integrated in photonics and electronics circuits with low cost and high efficiency has been an attractive research and development direction worldwide. The hybrid approach, in which silicon is integrated with a III–V gain medium, is an effective way. Using a transfer-printing and multilayer semiconductor nanomembrane stacking process, an optically pumped surface-emitting laser on silicon is realized, which is sandwiched between two single-layer silicon photonic crystal Fano resonance membrane reflectors (MRs). Here we review the design and characteristics of this Si based laser cavity, including the principle, design and phase properties of the membrane reflector, the cavity design and mode analysis, and experimental demonstration of the MR reflections as well as performance and the lasing behavior.

**KEYWORDS:** Vertical Cavity Surface Emitting Laser, Si Nanomembrane Reflector, Photonic Crystal, Fano Resonance.

## CONTENTS

|  |    |
|--|----|
| 1. Introduction  | 77 |
| 2. SI MR Reflector   | 80 |
| 2.1. Principle and Design Towards Broadband and High Reflectance           | 80 |
| 2.2. Phase, Energy and Phase Penetration Properties in Membrane Reflectors | 81 |
| 3. MR-VCSEL Design   | 82 |
| 4. MR-VCSEL Optical Characteristics  | 83 |
| 4.1. MR Reflection   | 83 |
| 4.2. Half Cavity Characteristics   | 84 |
| 4.3. Lasing Behaviors  | 85 |
| 5. Summary   | 86 |
| Acknowledgments  | 87 |
| References and Notes   | 87 |

## 1. INTRODUCTION

Among various types of lasers, vertical-cavity surface-emitting lasers (VCSELs) are the one of the popular type for a wide range of applications which require low threshold, high wall plug-efficiency, high modulation speed, and low cost large volume production.<sup>1–5</sup> Traditional VCSELs consist of two distributed Bragg reflectors (DBRs) as top and bottom mirrors which provide the optical feedback to form the cavity, as shown in Figure 1. Due to the very

short gain lengths in the center of VCSELs cavity, a very high reflectivity (> 99%) is always required in the DBRs to lower the lasing threshold.<sup>2,6</sup> DBRs are mostly fabricated by using monolithically grown technology and the constrained index difference of the alternating materials is small. Therefore, the DBRs are typically very thick. While the DBR fabrication technology is mature for GaAs-based VCSELs, it is still a big challenge for InP-based longer wavelength VCSELs, due to the lack of the lattice-matched alternative materials with large index contrast.<sup>7</sup>

Single thin layer structures with one-dimensional (1D) subwavelength grating (SWG) and 2D photonic crystal (PC) patterns can also offer very high reflectivity,<sup>8–12</sup> which can replace the DBRs of traditional VCSELs. In 2007, electrically and optically pumped VCSELs have been reported by replacing the top DBR with 1D SWG reflector.<sup>13,14</sup> whose cavity structures are shown in Figures 2(a) and (b) respectively. In these VCSELs, the growth method is involved to form the cavity and the devices are processed on the III–V native substrates. In 2012, by replacing both top and bottom DBRs, optically-pumped VCSELs on Si were realized by using two different techniques.<sup>15,16</sup> Utilizing the III–V/SiO<sub>2</sub> molecular bonding processes and amorphous Si deposition processes, Viktorovitch et al. formed the VCSEL cavity with two 1D Si membrane grating reflectors shown in Figure 3(a). By employing transfer printing technology, we reported optically pumped MR-VCSELs on Si by sandwiching an InGaAsP QW active cavity in

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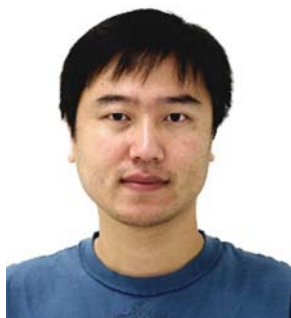
between two 2D photonic crystal Fano resonance membrane reflectors (MRs), shown in Figure 3(b).

Due to different mechanisms, the Fano resonance PCMRs have different phase and energy penetration characteristics.<sup>17–20</sup> Additionally, in the MR-VCSEL cavity, two MRs also act as two couplers which can excite

the waveguide (WG) modes in QW layer if the coupling condition is satisfied.<sup>21,22</sup> The WGs will lead to an additional lateral loss if it overlaps with the cavity mode. These unique characteristics of MRs are very important and should be taken into consideration carefully in the MR-VCSEL cavity design.



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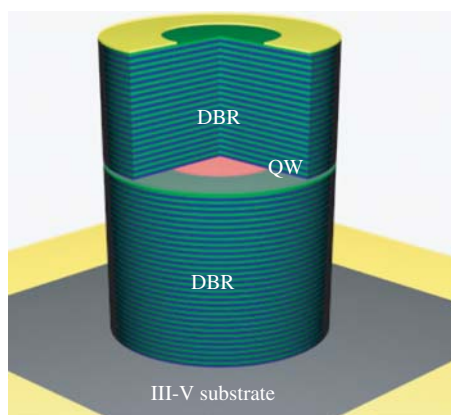
electronic devices, CMOS integrations with lasers and with micro-/nano electromechanical systems (MEMS/NEMS), nanophotonics based on transferable semiconductor membranes, high-speed flextronics, nanoscale semiconductor devices, unconventional multispectral imaging, photovoltaics, isotope betavoltaics, and high frequency RF integrated circuits.



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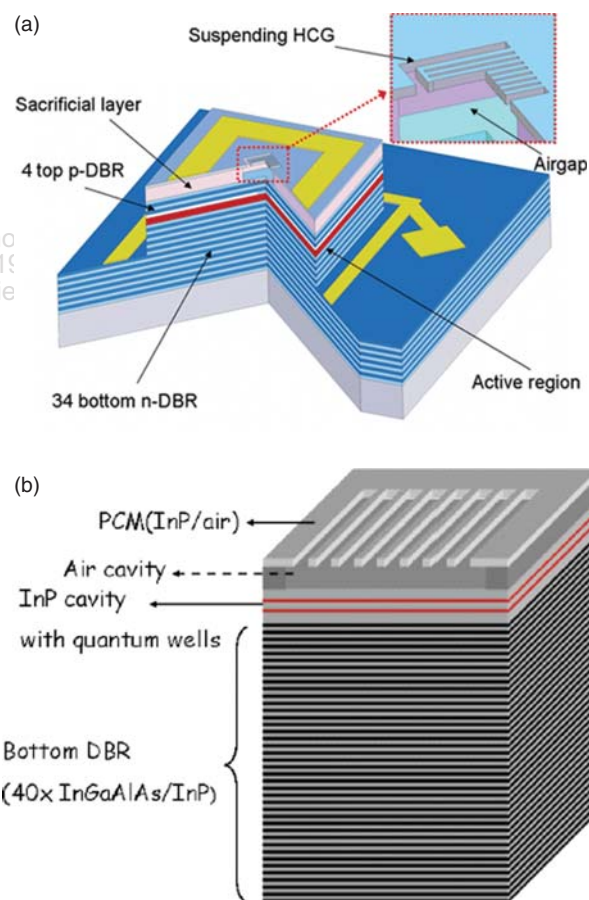
Figure 4 shows the sketch of the MR-VCSEL cavity which consists of a III–V InGaAsP quantum well (QW) disk, sandwiched in between two single-layer Si photonic crystal (PC) Fano resonance membrane reflectors (Si-MRs). Two low index buffer layers ( $\text{SiO}_2$ , layers  $t_2$  and  $t_4$ ) are inserted to ensure proper index contrast to the top and bottom Si-MRs. The complete MR-VCSEL cavity ( $t_1$  to  $t_5$ ) is built on the top of a silicon-on-insulator (SOI) substrate with  $\text{SiO}_2$  buried oxide (BOX) layer thickness of  $t_0$ . In order to achieve lasing with low threshold in such a cavity, it is highly desirable to design MR-VCSEL cavity with the following characteristics: (a) Both top and bottom MRs should have broadband reflection bands, with reflections greater than 99%; (b) The cavity should be designed such that the cavity mode is spectrally separated from the waveguide modes; (c) The cavity mode should match with QW emission peak spectrally with or without spectral detuning; and (d) The cavity mode should have an optimal field distribution spatially matched with QW active region for high confinement factors and low lasing thresholds.

In this paper, we report a systematic review on designs and characteristics of MR and MR-VCSEL cavity. First, we discuss the MR reflection principle, design and phase properties. Next, we present MR-VCSELs cavity design



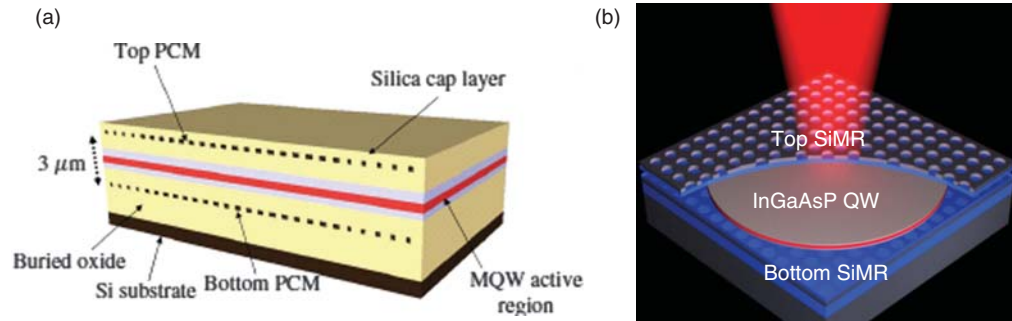
**Fig. 1.** Schematic of a traditional DBR based VCSEL with top and bottom DBRs grown on III–V substrate.

and cavity mode analysis. In the fourth section, we experimentally demonstrate the MR reflections and the lasing behavior. The conclusion and the further applications of the MR-VCSEL are discussed at the end.



**Fig. 2.** VCSELs with top MR/bottom DBR: (a) electrically pump, and GaAs 1D SWG reflector grown on GaAs substrate; and (b) optically pump, and InP 1D SWG grown on InP substrate. Reproduced with permissions from [13, 14], M. C. Y. Huang, et al., A surface-emitting laser incorporating a high-index-contrast subwavelength grating 1, 119 (2007), *Nat. Photonics* 1, 297 (2007). © 2007, Nature Publishing Group. S. Boutami, et al., Compact and polarization controlled 1.55  $\mu\text{m}$  vertical-cavity surface-emitting laser using single-layer photonic crystal mirror. *Appl. Phys. Lett.* 91, 13 (2007). © 2007, AIP.





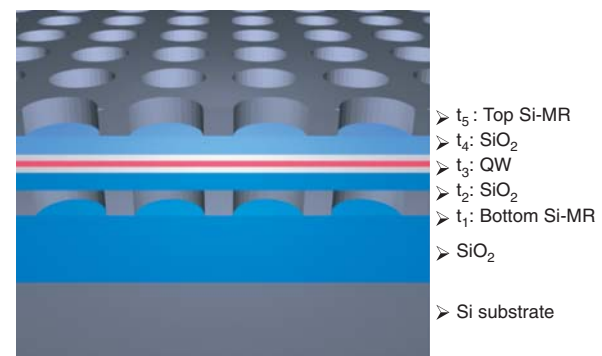
**Fig. 3.** Schematics of VCSELs with (a) double SWGs and (b) double 2D PC MRs. Reproduced with permission from [15, 16] C. Sciancalepore, et al., CMOS-compatible ultra-compact 1.55- $\mu\text{m}$  emitting VCSELs using double photonic crystal mirrors. *Photonics Technology Letters, IEEE* 24, 455 (2012). © 2012, IEEE. H. Yang, et al., Transfer printing stacked nanomembrane lasers on silicon. *Nat. Photonics* 25, 658 (2012). © 2012, Macmillan Publishers Limited.

## 2. SI MR REFLECTOR

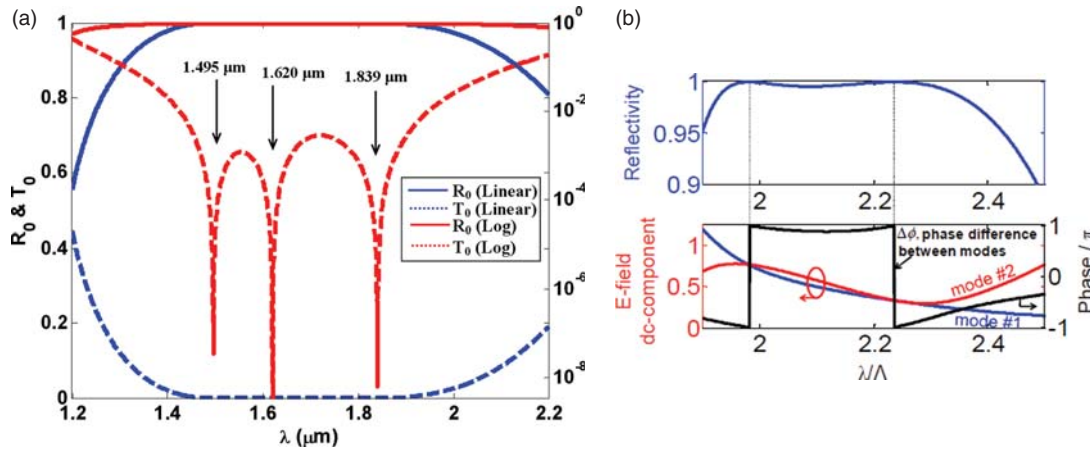
### 2.1. Principle and Design Towards Broadband and High Reflectance

Single layer nanomembrane with 1D or 2D photonic crystal pattern can be functioned as broad band reflectors, whose high reflection mechanism originate from the Fano- or guided-resonances effect and is completely different from the traditional DBR.<sup>23–25</sup> The spectral bandwidth and reflection properties of DBRs have been well studied.<sup>19</sup> The high reflectivity attributes to the multiple reflections with constructive interference among these reflected waves by each thin layer inside of DBR. And the larger index difference gives rise to a broader reflection band. For 1D SWG and 2D PC mirrors, the reflection mechanism comes from Fano or Guided mode resonance effect and the destructive interference effect. In Ref., Magnusson et al.<sup>24</sup> attributed the broadband reflection of SWG to the in-plane guided-mode excitation based on phase matching conditions. The wave then reradiates at one edge with a zero phase difference and at another edge with a  $\pi$  phase difference. The broad reflection spectral band originates from the cooperating of the several adjacent guided mode resonances. As shown in Figure 5(a), in a Si-based SWG design with target reflection band over 1.45–2.0  $\mu\text{m}$  for TM polarization, the very broadband reflection bandwidth of 520 nm for 99% reflection is supported by a blend of three guided mode resonances (transmission dips) located inside this band. On the other hand, in Ref. [25] Karagodsky et al. presented an analytic analysis on the ultra-high reflectivity of subwavelength high contrast grating reflectors based on double grating modes model. The double modes exhibit perfect cancellation at the output plane of SWG, i.e.,  $\pi$  phase difference or completely destructive interference. As clearly shown in Figure 5(b), the average  $E$ -fields of the first two grating modes are plotted with their phase difference. At the points of 100% reflectivity the modes have anti-phase with equal intensities, which means that perfect cancellation occurs. If two such 100% reflectivity points are located at close spectral vicinity, a broad-band of high reflectivity is achieved.

According to the principle of MRs, to achieve broadband high reflection, the first thing is to choose the structure parameters, including membrane thickness “ $t$ ,” PC lattice “ $a$ ,” air hole radius “ $r$ ,” and substrate index “ $n$ ,” which can support Fano/guided-mode resonances in the target spectral band, then one can tune the parameter to find optimized one. Sang et al. presented a systematical design guideline in a Ref. [26]. Using the trial-and-error approaches based on the complete 3D computational tools, such as RCWA and FDTD techniques, the different designs for high Q filters (narrow band reflector) and broadband MRs can be done. It was found that the Q factor (spectral line width) can be controlled by varying the radius once the proper membrane thickness is found. Very small  $r/a$  values ( $\sim 0.1$ ) favor high Q filter design and large  $r/a$  values (0.28–0.49) favor broadband reflector design. Other design parameters include the lattice structure and the air hole shape, the surrounding buffer, and the effective indices inside PC pattern region, etc. From the previous works,<sup>9, 27–29</sup> the thickness of 340 nm is found to be a better parameter of a single crystalline Si



**Fig. 4.** Membrane reflector VCSEL (MR-VCSEL) schematic of a complete MR-VCSEL cut-out view: an InGaAsP QW sandwiched in between two single layer Si Fano resonance photonic crystal membrane reflectors (SiMRs), stacked on a Si substrate. Low index SiO<sub>2</sub> buffer layers are inserted to ensure high reflection of MRs. The whole cavity consists of five layers ( $t_1$ – $t_5$ ). Reproduced with permission from [21], D. Zhao, et al., Design of photonic crystal membrane reflector based VCSELs. *IEEE Photonics Journal* 4, 2169 (2012). © 2012, IEEE.



**Fig. 5.** (a) Physical basis for broadband reflection in 1D gratings: Zero-order reflectance and transmittance spectra of broadband reflectors operating in (a) TM polarizations. For clarity, the spectra are plotted on both linear and logarithmic scales. Reproduced with permission from [24], R. Magnusson and M. Shokooch-Saremi, Physical basis for wideband resonant reflectors. *Opt. Express* 16, 3456 (2008). © 2008, OSA. (b) Double-mode solution exhibits perfect cancellation at the SWG output plane leading to 100% reflectivity. At the wavelengths of 100% reflectivity both modes have the same magnitude and opposite phases  $\pi$ . Reproduced with permission from [25], V. Karagodsky, et al., Theoretical analysis of subwavelength high contrast grating reflectors. *Opt. Express* 18, 16973 (2010). © 2010, OSA.

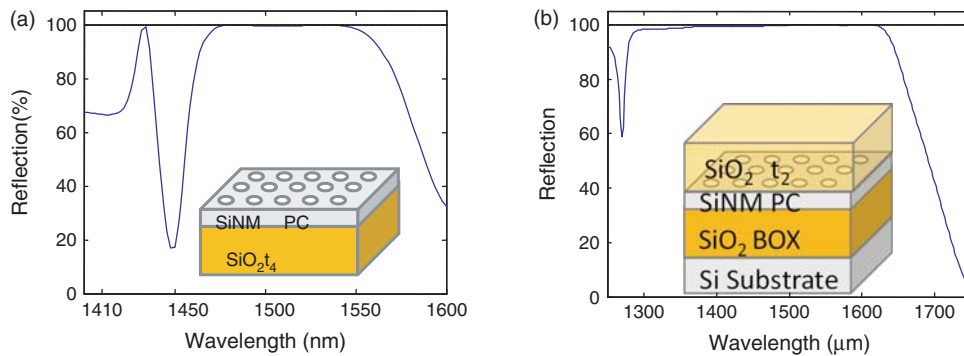
nanomembrane with index  $n = 3.48$  to design MRs with broad band spectral and high reflection in the optical communication band around 1550 nm. Here we present two good group designs with medium ( $r = 0.3a$ ) and larger ( $r = 0.45a$ ) air hole for top MR (on glass substrate,  $a = 1010$  nm) and bottom MR (on SOI,  $a = 880$  nm, BOX thickness  $t_0 = 2\mu\text{m}$ ), as shown in Figures 6(a) and (b), respectively. For the bottom MR, another layer of  $\text{SiO}_2$  low index buffer layer ( $t_2$ ) is also incorporated in the design, as part of the complete MR-VCSEL as shown in Figure 4. During  $\text{SiO}_2$  deposition, air hole will be partially filled. So the effective index inside air hole region ( $n_f$ ) should be considered. According to earlier theoretical and experiment results<sup>28</sup> the effective index for the air hole region ( $n_f$ ) is about 1.2 for Si-MRs with larger air hole design ( $r/a > 0.4$ ). One can see the bottom MR reflection band cover from 1300 to 1600 nm with  $R > 99\%$ . Through adjusting main parameters, ( $t$ ,  $a$ ,  $r$ ), MRs for different band range can be obtained. Qiang et al. reported

more designs for MRs on SOI based on the control of vertical confinement with controlled refractive index for the buffer layers below and above the MR layer.<sup>28</sup>

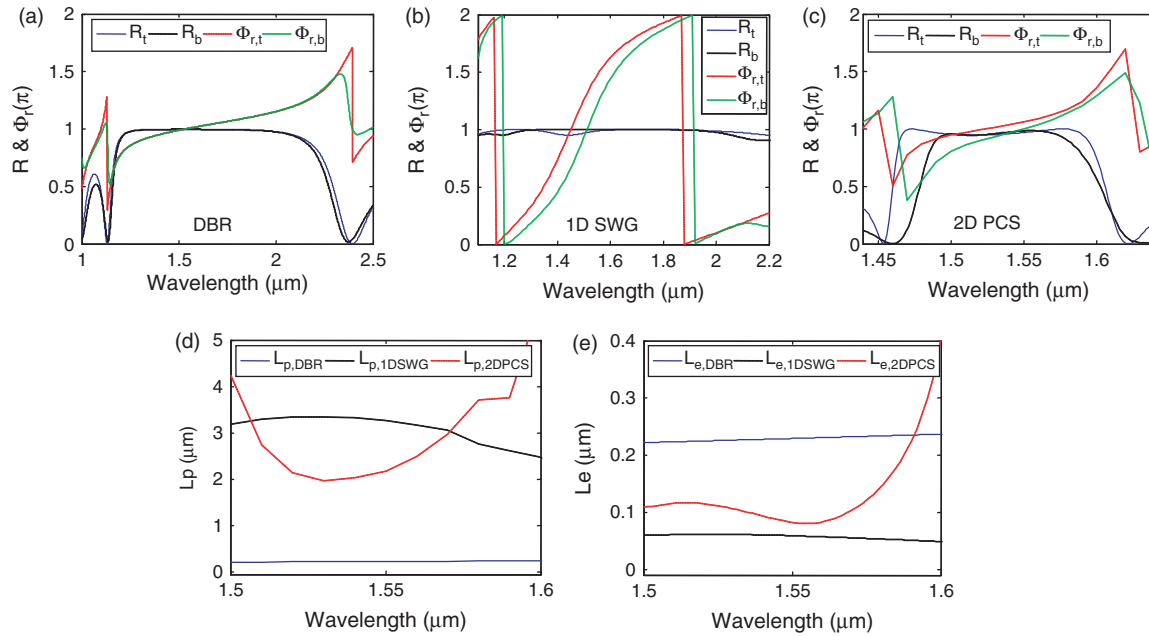
Experimentally, Boutami et al.<sup>30</sup> reported demonstration of 2D PCS based MRs with controlled polarization and broad reflection band of 200 nm at 1550 nm wavelength region. Later, Yang et al. reported detailed experimental investigations with index tuning range over 50 nm for both blue and red shifts, by controlling the buffer oxide index below with controlled etching and the index above with the controlled oxide deposition.<sup>27</sup>

## 2.2. Phase, Energy and Phase Penetration Properties in Membrane Reflectors

Under surface-normal incidence, DBR, 1D SWG, and 2D PCS reflectors can all exhibit similar reflection properties with extremely high reflection and broad reflection spectral band. However, the different reflection mechanisms lead to different phase and penetration properties.



**Fig. 6.** Simulated reflection of top and bottom MR. (a), Bottom MR based on SOI structure with  $\text{SiO}_2$  deposition as buffer layer with thickness  $t_2 \sim 400$  nm. (b), Top MR transferred on another  $\text{SiO}_2$  buffer layer with thickness  $t_4 \sim 400$  nm. Reproduced with permission from [21], D. Zhao, et al., Design of photonic crystal membrane reflector based VCSELs. *IEEE Photonics Journal* 4, 2169 (2012). © 2012, IEEE.



**Fig. 7.** (a)–(c) Simulated reflection and reflection phase change of three types of reflectors; (d) calculated phase penetration depths for three types of reflectors; and (e) the energy penetration depths for three types of reflectors. Reproduced with permission from [17], D. Y. Zhao, et al., Field penetrations in photonic crystal fano reflectors. *Opt. Express* 18, 14152 (2010). © 2010.

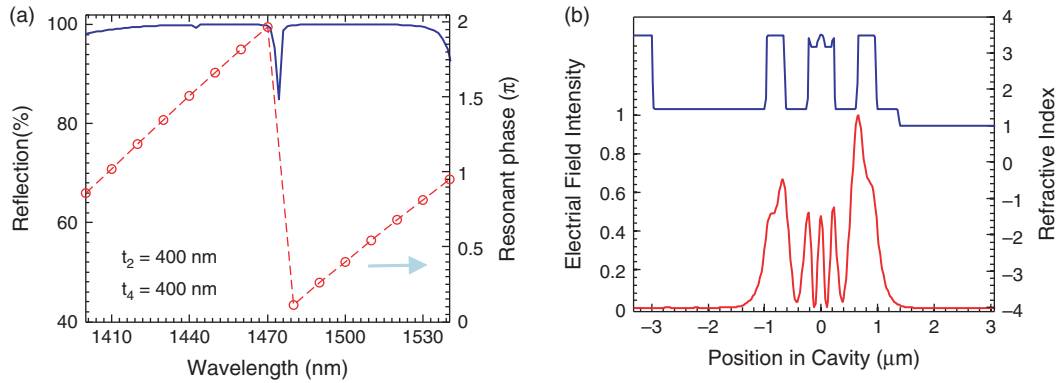
In Ref. [31] the authors reported the phase discontinuity  $\Phi_r$  and the energy penetration depth ( $L_e$ ) according to the mode spacing in the Fabry-Perot (FP) cavity. In 2009, the in-plane optical property of 2D PCS was reported by Sauvan et al.<sup>20</sup> With fully vectorial calculations, in heterostructure mirrors, the penetration length associated with the delay is much larger than the characteristic damping length of the energy distribution inside the mirror. This amazing property evidences that these two characteristic lengths are not necessarily correlated. Consequently, the usual trade-off between short damping lengths and large penetration lengths that is encountered in classical DBRs can be overcome with carefully designed PC structures. Later Zhao et al.<sup>17</sup> investigated in more details the phase and energy penetration depths, and field distributions of 1D SWG and 2D PCS reflectors, as shown in Figure 7. Figures 7(a)–(c) show the reflection phase change of DBR, 1D SWG and 2D PCS, respectively. One can see  $\Phi_r$  of 1D SWG and 2D PCS reflectors rapidly vary in the high reflection ( $R > 0.95$ ) spectral band, much faster than those of DBRs.

In dielectric mirrors, the reflection is not an instantaneous process. It includes a reflection time delay ( $\tau$ ) or phase penetration depth ( $L_p$ ) and energy storage in the mirrors. The phase penetration depth ( $L_p$ ) is always directly related to the reflection phase shift  $\Phi_r$ , so  $L_p$  of 1D SWG and 2D PCS are much larger than DBR, as shown in Figure 7(d). The energy penetration depth ( $L_e$ ) is related to the energy storage. Figure 7(e) shows  $L_e$  comparison of these three mirrors. One can see  $L_e$  of 1D SWG and 2D PCS are much smaller than DBR. In addition, for 1D SWG

and 2D PCS,  $L_p$  is much larger than  $L_e$ , while  $L_p$  and  $L_e$  of DBR are close to each other. Therefore, comparing to the DBR reflectors, these new types of single layer ultra-compact broadband reflectors can have more complicated larger phase delays and smaller energy penetration properties, which can be engineered via dispersion engineering for large spectral dependent phase delays, and ultra-small energy penetration depths. This phase information is important and helpful in the following cavity design.

### 3. MR-VCSEL DESIGN

Once two good MRs with high reflectivity and broader overlapped spectral band are obtained, a multi-layer Si-MR/QW/Si-MR MR-VCSEL cavity can be built up. Here, we need to decide the cavity resonant (longitudinal) mode by selecting a suitable cavity length, i.e., the thickness of the buffer layers between Si-MR and QW. Figure 8(a) shows the reflection spectrum (blue line) of one designed MR-VCSEL cavity with  $t_0 = 2 \mu\text{m}$ ,  $t_1 = t_5 = 340 \text{ nm}$ ,  $t_2 = t_4 = 400 \text{ nm}$ ,  $t_3 = 465 \text{ nm}$ ,  $a = 860 \text{ nm}$ ,  $r_t = 0.46a$  and  $r_b = 0.45a$ . The resonant cavity mode appears at 1478 nm. To make the field distribution more symmetric inside cavity, another  $\text{SiO}_2$  layer with  $t_6 = 400 \text{ nm}$  or thicker is assumed to be deposited on the top of MR-VCSEL and  $n_f = 1.2$  is also considered. To further confirm this cavity mode, the phase resonant condition (total phase change of one round-trip in cavity is equal to integer times of  $2\pi$ ) is also calculated according to the reflection phase change ( $\phi$ ) of the top and bottom MR, which is plotted as red dotted line in Figure 8(a). One can find the mode located at



**Fig. 8.** Characteristics of designed MR-VCSEL cavity. (a), Calculated cavity resonance mode based on cavity reflection and phase resonant condition. (b), Field distribution of cavity mode. Reproduced with permission from [21], D. Zhao, et al., Design of photonic crystal membrane reflector based VCSELs. *IEEE Photonics Journal* 4, 2169 (2012). © 2012, IEEE.

1478 nm has a  $m \cdot 2\pi$  phase change, which means 1478 nm is a real cavity mode.

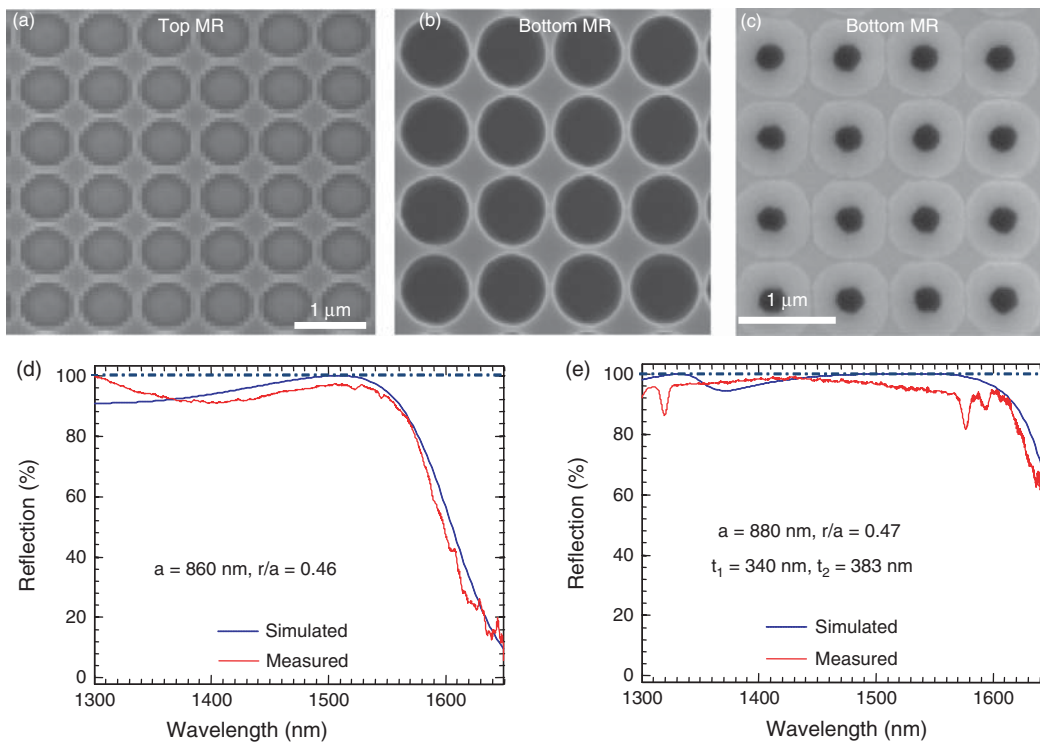
By employing FDTD, a short temporal Gaussian pulse is used to excite the cavity modes and the quality factor of the cavity mode 1478 nm is calculated to be 4300 according to  $Q = Re(\omega) / -2 \cdot Im(\omega)$ .<sup>32</sup> Then a longer temporal Gaussian pulse is used to excite the single cavity mode and the stable field is recorded. The  $E$ -field distribution is demonstrated in Figure 8(b) with red line, where the cavity index profile is also plotted with blue line. One of  $E$ -field peak is located at QW well region and the calculated confinement factor is about  $\Gamma = 5.6\%$ .

Another design concern should be taken care, i.e., separating the lasing cavity modes from the waveguide modes within the QW layer as mentioned in a Ref. [21]. Despite the relatively large field concentration in Si-MR layer, the lasing mode field confinement factor is 5.6% for MR-VCSELs, which is comparable to DBR-based VCSELs.

## 4. MR-VCSEL OPTICAL CHARACTERISTICS

### 4.1. MR Reflection

Using the designed Si-MR parameters discussed in the previous section, the top MR was first fabricated on SOI



**Fig. 9.** (a)–(c), SEM images of membrane reflectors (MRs). (d) and (e) the measured and simulated reflection of top and bottom MRs. Reproduced with permission from [16], H. Yang, et al., Transfer printing stacked nanomembrane lasers on silicon. *Nat. Photonics* 25, 658 (2012). © 2012, Macmillan Publishers Limited.



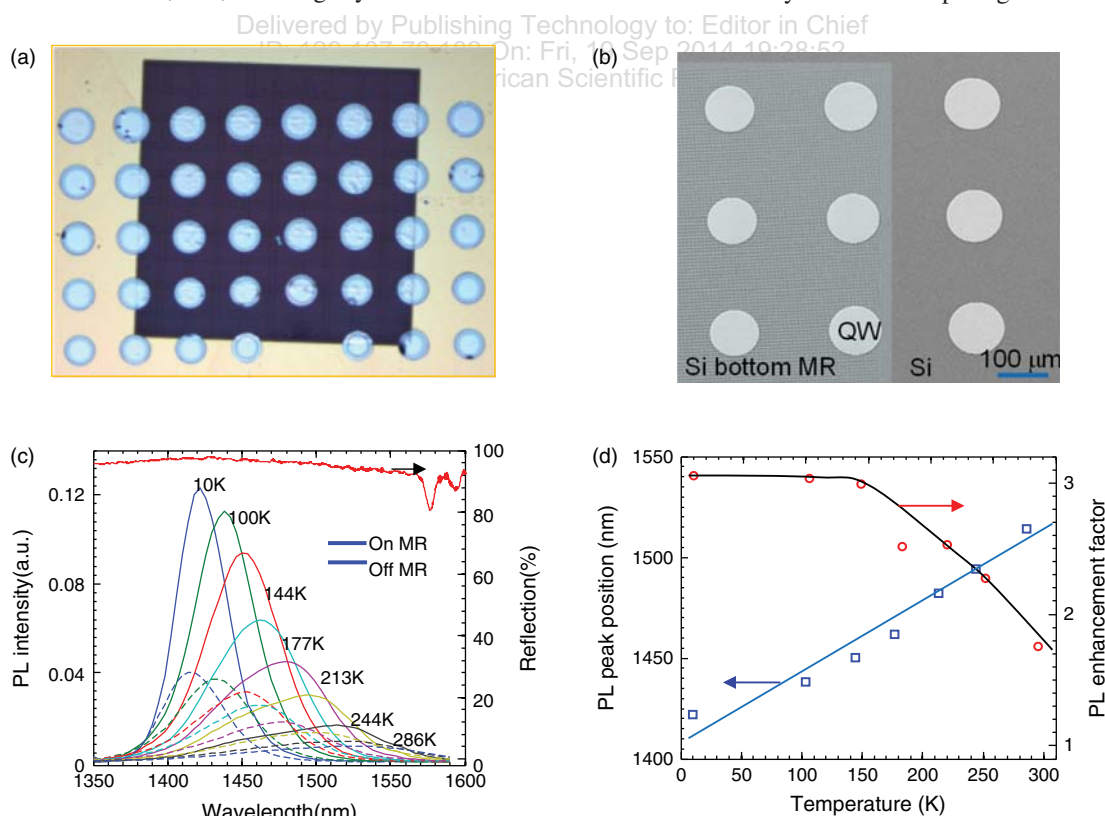
and then transferred onto a glass substrate employing the elastomeric stamp based transfer printing process.<sup>16</sup> Figure 9(a) is the scanning electron micrograph (SEM) image of the transferred top MR on glass substrate with  $a = 860$  nm and  $r/a = 0.46$ . The bottom SiMR with  $a = 860$  nm and  $r/a = 0.45$  is directly fabricated on a SOI substrate and followed by a deposition of a thin SiO<sub>2</sub> film on its top, with SiO<sub>2</sub> layer thickness  $t_2 \sim 383$  nm, to work as a cavity buffer layer. SEM images of two cases, before and after the top SiO<sub>2</sub> deposition, are shown in Figures 9(b) and (c), respectively. Due to the large  $r/a$ , air holes become smaller and not completely sealed by this thin SiO<sub>2</sub> deposition, which means SiO<sub>2</sub> is partially filled into the air holes and is considered in our designs by using an effective index in the air hole region.

The reflections of these two MRs are measured under normal incidence using a slightly focused white light beam and normalized with gold mirror. The simulation and measurement results of the top and the bottom MRs are plotted together in Figures 9(d) and (e). The reflectors designed to have peak reflection values  $> 99\%$ , with wide reflection bands. Also, the measured and simulated reflections are matched well. It should be noted that the small dip at the edge of high reflection band comes from the non-ideal normal incidence, i.e., the slightly focused beam

includes a small partial of oblique incident light around the beam edge.

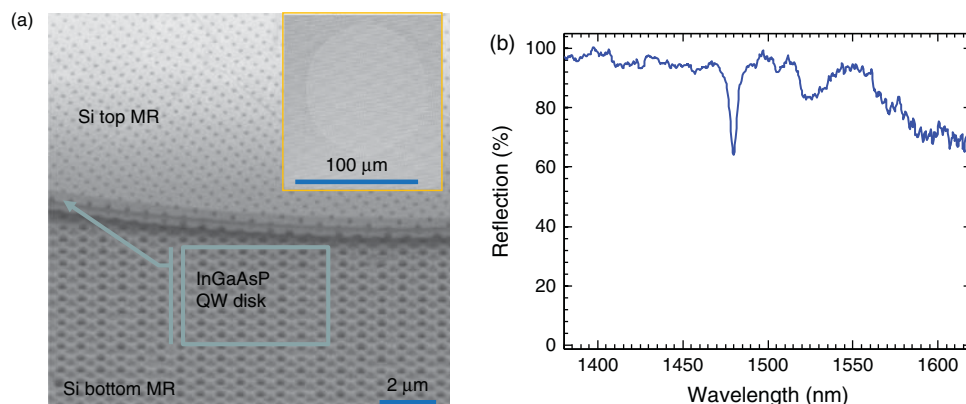
#### 4.2. Half Cavity Characteristics

The InGaAsP QW disks are transferred onto the bottom SiMR after the substrate removal. Figures 10(a) and (b) show the micrograph and SEM image of this half cavity without top MR. Some QW disks are transferred onto a patterned bottom Si-MR region, while the others are laid onto the unpatterned Si region. The diameter  $D$  of these QW disks (i.e., the active area of the MR-VCSELs) is  $100\ \mu\text{m}$ . The PL performances of QW disks on-MR and off-MR were tested under various temperature ( $T$ ) from 10 K to 300 K using a continuous wave (c.w.) green laser. Figure 10(c) shows the PL spectra of the disks on MR (solid lines) and off-MR (dashed lines) at different  $T$ , where the bottom MR reflection at 300 K is also plotted together as a reference. As  $T$  increases, the common PL features can be found, PL spectral shift towards longer wavelength, intensity reduces, and spectral becomes broader. In Figure 10(d), the linearly fitted PL peak location indicates PL peaks are red-shifted with a rate of  $0.43\ \text{nm/K}$ . Due to the high reflection of bottom Si-MR, the PL intensity is much enhanced. Shown in Figure 10(d) is the PL peak intensity enhancement factor as a function of  $T$ . For  $T < 150$  K, PL of QW disk on-MR is enhanced by 3 times comparing with off-MR, and

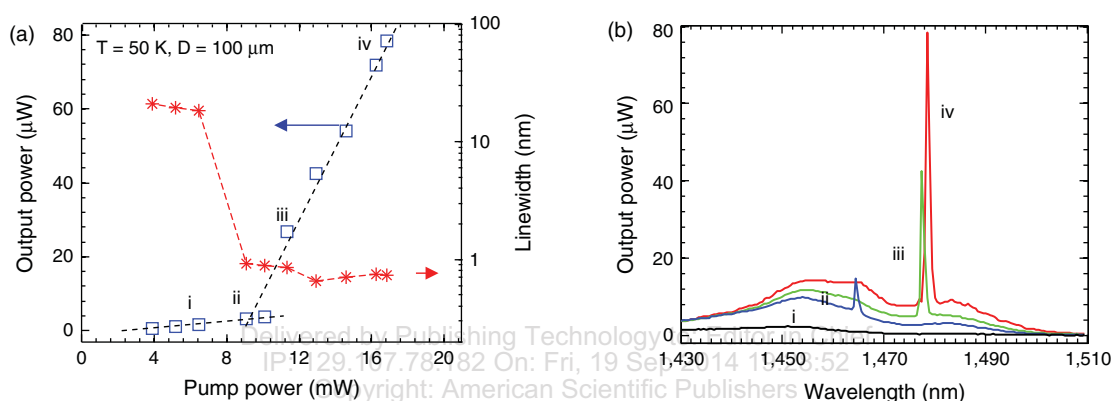


**Fig. 10.** (a) and (b) Micrograph and SEM images of half cavity (QW on bottom MR); Reproduced with permission from [16], H. Yang, et al., Transfer printing stacked nanomembrane lasers on silicon. *Nat. Photonics* 25, 658 (2012). © 2012, Macmillan Publishers Limited. (c) the PL spectral of the QW disk on and off-MR as function of temperature, where the bottom MR reflection is also plotted with red line; (d) PL peak location and intensity enhancement factor versus  $T$ .





**Fig. 11.** (a) SEM image of the complete MR-VCSEL; Reproduced with permission from [16], H. Yang, et al., Transfer printing stacked nanomembrane lasers on silicon. *Nat. Photonics* 25, 658 (2012). © 2012, Macmillan Publishers Limited. (b) The measured cavity reflections.



**Fig. 12.** (a), The L-L plot (light output for different pump powers) and the corresponding spectral linewidths at  $T = 50$  K; (b) The measured spectral outputs for pump powers below, at, and above thresholds. Reproduced with permission from [16], H. Yang, et al., Transfer printing stacked nanomembrane lasers on silicon. *Nat. Photonics* 25, 658 (2012). © 2012, Macmillan Publishers Limited.

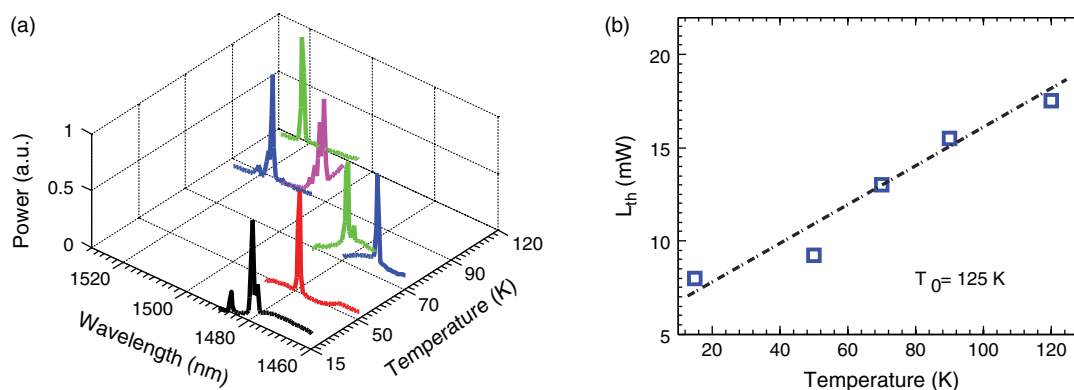
when  $T > 150$  K, the PL enhancement reduces down to 1.8 times because MR reflection at longer wavelength range becomes lower.

### 4.3. Lasing Behaviors

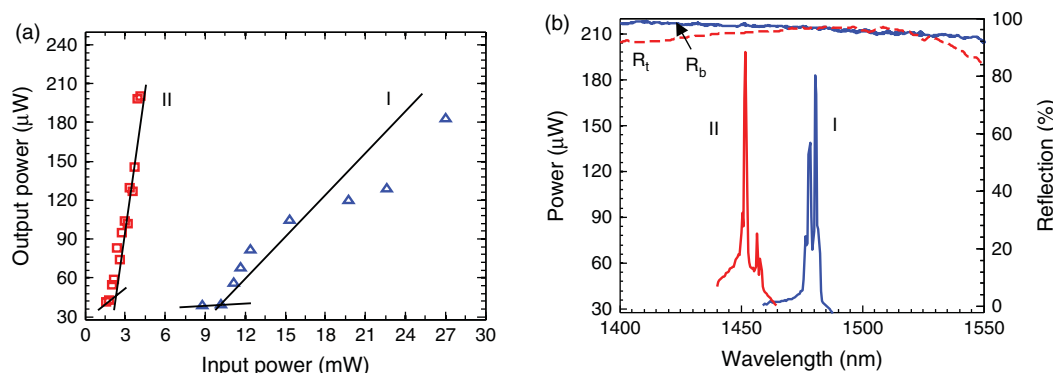
A complete MR-VCSEL structure is shown in Figure 11(a), where both the top and the bottom Si-MRs

are visible. The inset shows a single QW disk underneath the top Si-MR layer. Figure 11(b) is the cavity reflection measured with white light source at normal incidence. One can find the cavity mode is at around 1478 nm, which matches the cavity mode design.

The MR-VCSEL device was tested under PL setup using quasi-continuous wave (c.w.) 532 nm laser pumping



**Fig. 13.** (a) Measured lasing spectral at different temperatures under 530 nm laser pumping; (b) lasing threshold as a function of temperature. Reproduced with permission from [16], H. Yang, et al., Transfer printing stacked nanomembrane lasers on silicon. *Nat. Photonics* 25, 658 (2012). © 2012, Macmillan Publishers Limited.



**Fig. 14.** (a) L-L plot (light output for different pump powers) at  $T = 15$  K under 532 nm (I) and 980 nm (II) lasers pumping. (b) The corresponding lasing spectra and the measured reflections of top and bottom MRs.

(with 50% duty cycle). Shown in Figure 12(a) is the L-L plot (light output for different pump powers) and the corresponding spectral linewidths measured at  $T = 50$  K. The threshold pump power is  $\sim 8$  mW, or  $0.32$  KW/cm<sup>2</sup>. The measured spectral linewidths reduce from 30 nm below threshold to 0.6–0.8 nm above threshold. The measured spectral outputs are shown in Figure 12(b), for pump powers below, at, and above thresholds (points (i, ii, iii, iv) at L-L curve). The lasing spectral linewidth is  $\sim 8$  Å, which is limited by the measurable resolution of monochrometer. The relative peak location shift shown in Figure 12(b) from bias levels (ii) and (iii, iv) is mostly related to mode hopping and temperature rise inside the active region at higher pump power levels.

This MR-VCSEL LT device was also characterized at different temperatures up to 120 K. Figure 13(a) shows the normalized lasing spectra (arbitrary units, a.u.) above the threshold at  $T = 15$  K, 50 K, 70 K, 90 K, 120 K. The lasing peak red shifts as  $T$  increases and multimode lasing for most  $T$  cases at a rate  $(d\lambda_c/dT)$  close to the simulated 0.088 nm/K. There is a mode hopping occurred below and above the operation temperature of 80 K. As  $T$  rises higher than 125 K, there was no lasing any more, which is mainly limited by the MR reflector bandwidth except the QW emission becomes weak. The LT design cavity has three lasing wavelengths of 1448 nm (at 10 K), 1478 nm (at 50 K), and 1520 nm (at 120 K) which match well with the cavity resonances. Figure 13(b) shows the lasing threshold ( $L_{th}$ ) as a function of  $T$ .  $L_{th}$  lineally increases with  $T$ , which matches the QW PL efficiency lineally decreases as  $T$ .

By improving cavity design and thermal engineered layers for improved thermal performance, we were able to drastically reduce the lasing threshold.<sup>33</sup> The measured L-L plots are shown in Figure 14(a) for a MR-VCSEL device under two types of c.w. pumping laser sources at  $T = 15$  K. By switching the pumping laser sources from 532 nm to 980 nm, the lasing thresholds reduce from 10 mW to 1.9 mW. The reduction of the lasing threshold is largely contributed to the significantly reduced thermal heating inside the lasing cavity. This is evident from the

measured lasing spectral outputs, as shown in Figure 14(b), where the lasing spectral peaks shifts from 1482 nm (with 532 nm pump) to 1452 nm (with 980 nm pump). Such a large blue-shift in lasing wavelength is a strong evidence of much reduced heat dissipation. Further threshold reduction is possible with much improved cavity design and the incorporation of highly thermal conductive buffer layers. Also shown in Figure 14(b) is the measured reflection spectra of the top ( $R_t$ ) and bottom ( $R_b$ ) Si-MRs used for this MR-VCSEL.

We should point out that photonics and photonic crystals have many other applications and are under extensive investigation.<sup>34–38</sup> Here we just review and summarize the progress based on our own research group.

## 5. SUMMARY

In summary, we systematically reviewed the designs and characteristics of MR reflectors and MR-VCSEL cavity. Based on the careful design and analysis on the MR properties, the fabricated device shows the characteristics as it is expected by cavity design, which is confirmed by MR-VCSEL optical characteristic demonstrations. More design details should be considered in MR-based VCSEL than conventional DBR-VCSEL, such as larger reflection phase change and waveguide exaction in QW layer. The design procedure discussed in here is common for any kind of VCSEL using PC MRs. In addition, utilizing the advantage of transfer printing technique, the multi-layer membranes structure can have different types of interface control, so different material systems can be further integrated together with unlocked constraints in lattice mismatches and thermal mismatches, which is opening doors towards a wide range of applications in optoelectronic and photonic devices: MR-VCSEL can be further integrated with different functional photonic nanomembrane layers for modulation, routing, and 3D photonic/electronic integration; MR-VCSEL can be built and transferred onto any other flexible plastic substrates, making them attractive for applications in consumer electronics and biophotonics, etc.

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