

Fragility Function Uncertainty Quantification in Infilled RC Frame Buildings

Speaker:

Al Mouayed Bellah Nafeh – IUSS Pavia

When:

12th June 2023

Where:

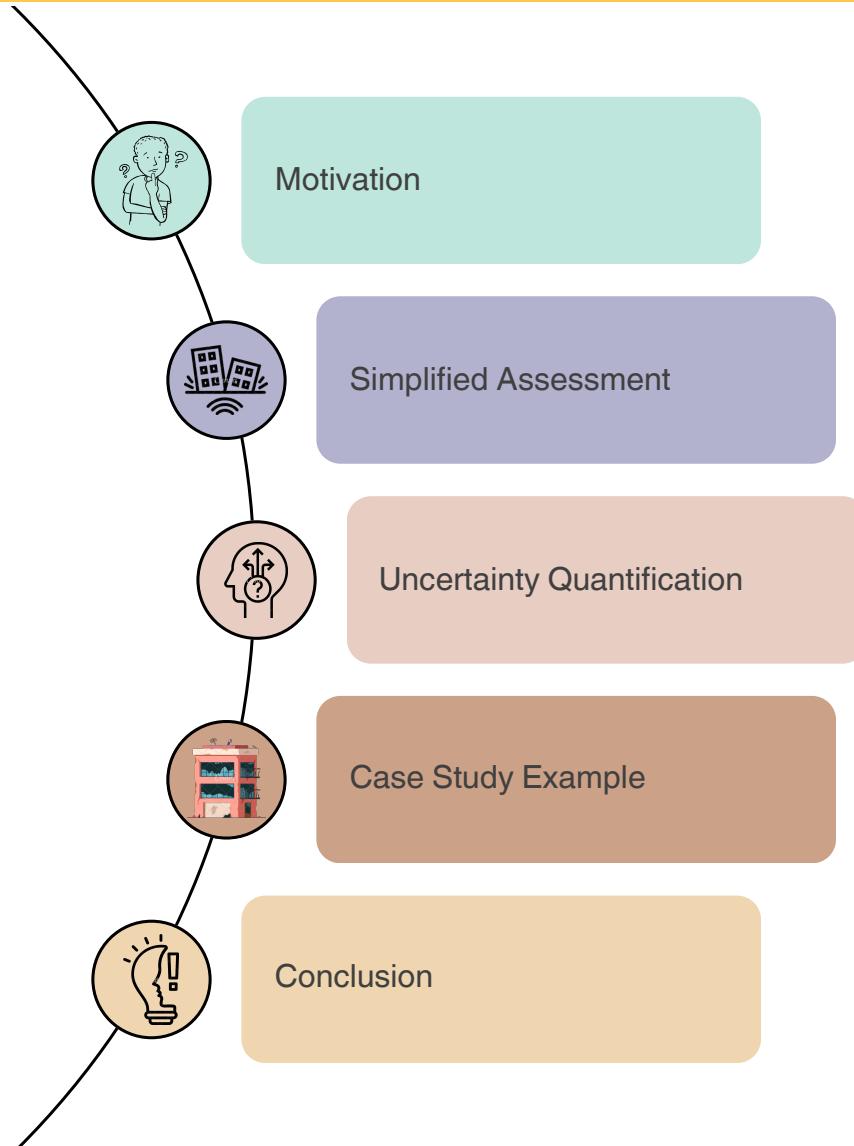
Athens, Greece

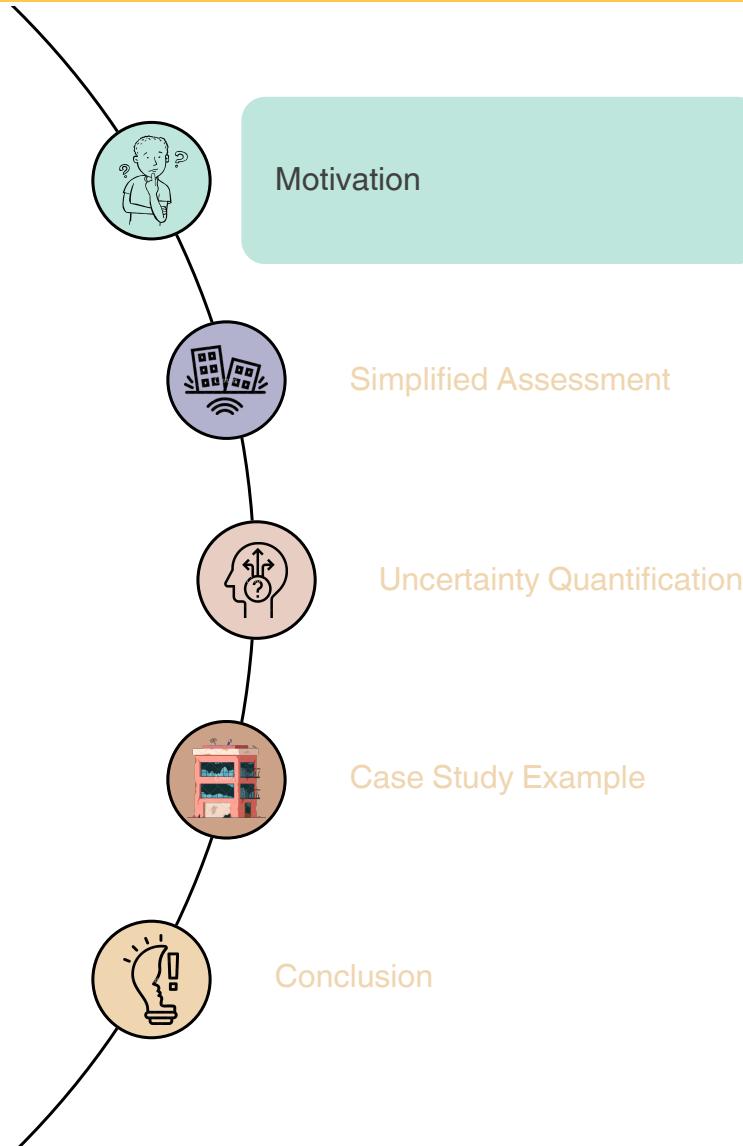


IUSS

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Centre for Training and Research
on Reduction of Seismic Risk
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High Vulnerability to Ground-Shaking Events



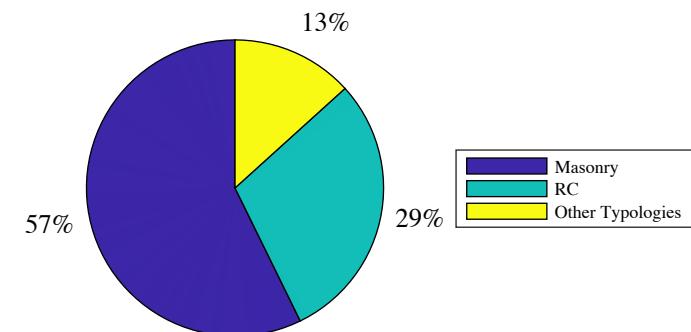
Accurate Response Characterisation



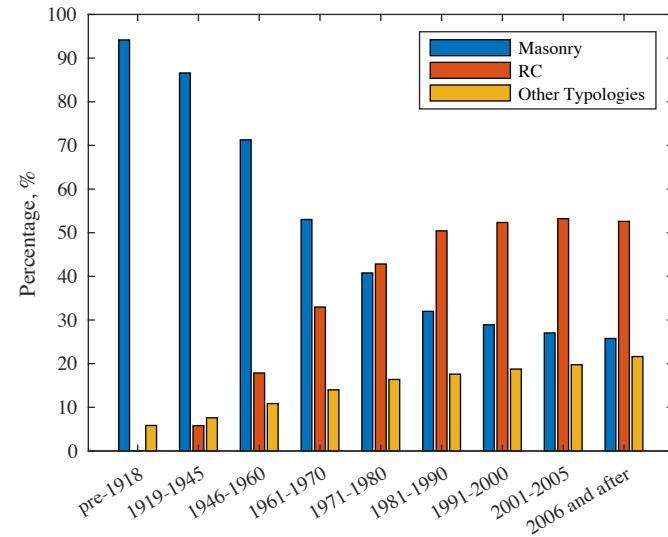
Reduction of Uncertainty in Risk- and Loss-Based Applications



Improved Decision-Making and Overall Community Resilience



Residential buildings by construction material



*Residential buildings by period of construction
and construction material*



Statistical Significance in Regional Building Stocks



High Vulnerability to Ground-Shaking Events



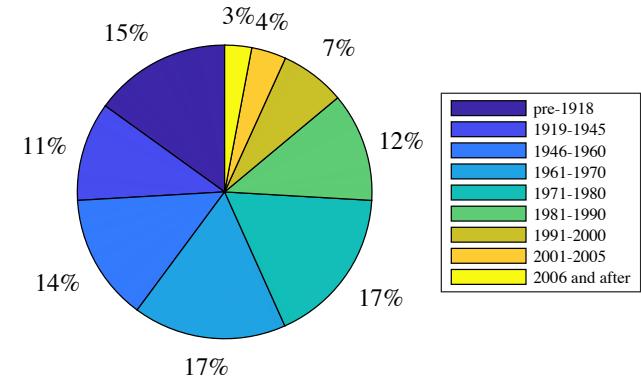
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Damage observations following earthquake events



Statistical Significance in Regional Building Stocks



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Reduction of Uncertainty in Risk- and Loss-Based Applications

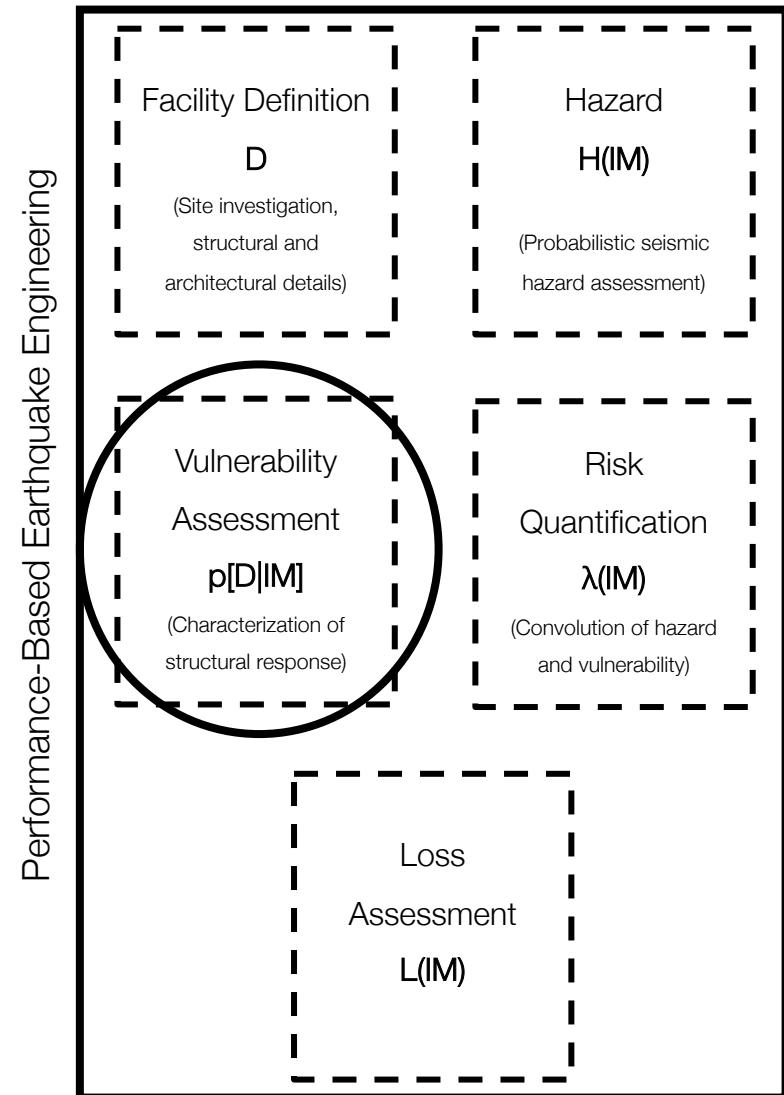


Improved Decision-Making and Overall Community Resilience



Predicted ≈ Observed

Analytical >> Empirical





**Statistical Significance in
Regional Building Stocks**



**High Vulnerability to Ground-
Shaking Events**



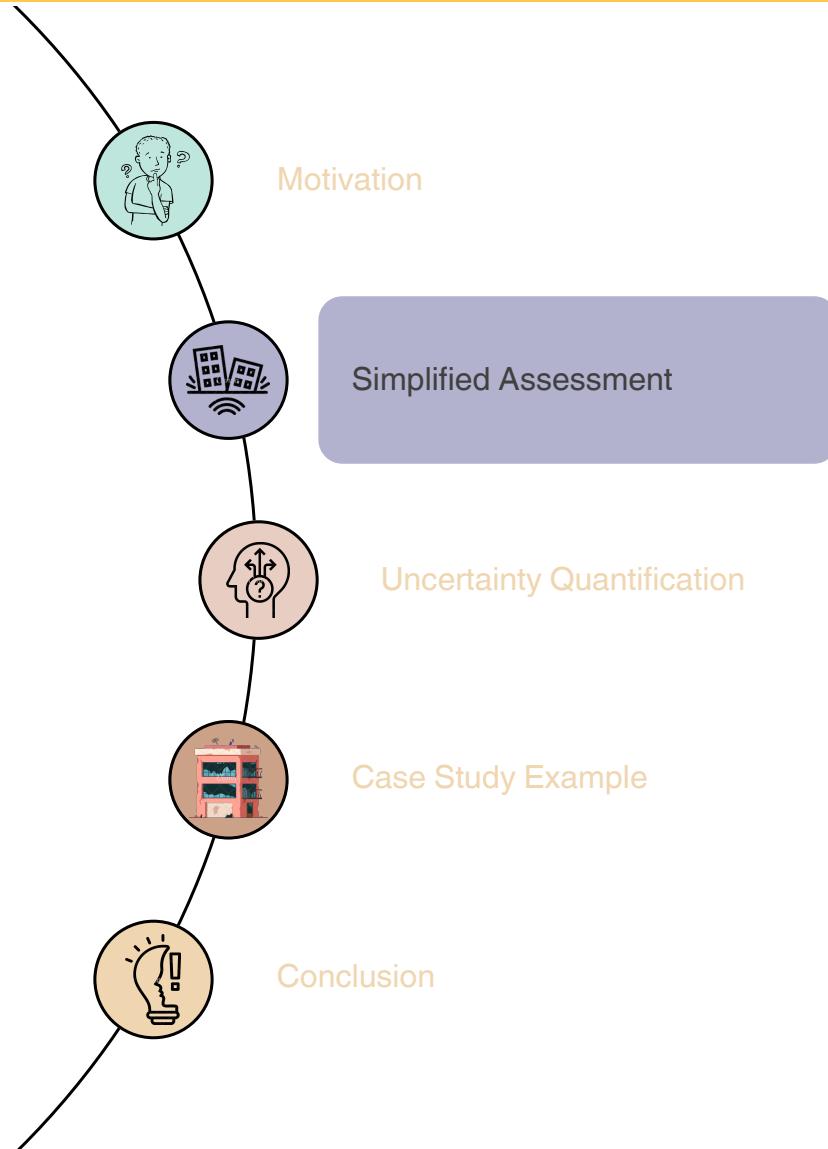
**Accurate Response
Characterisation**



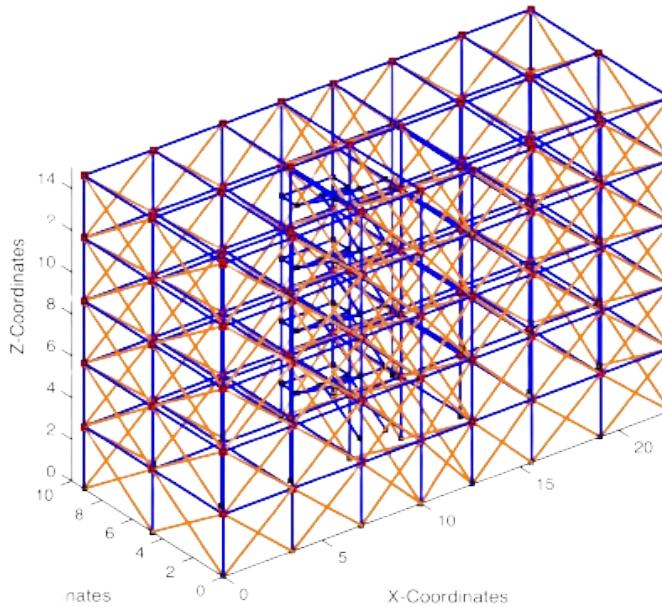
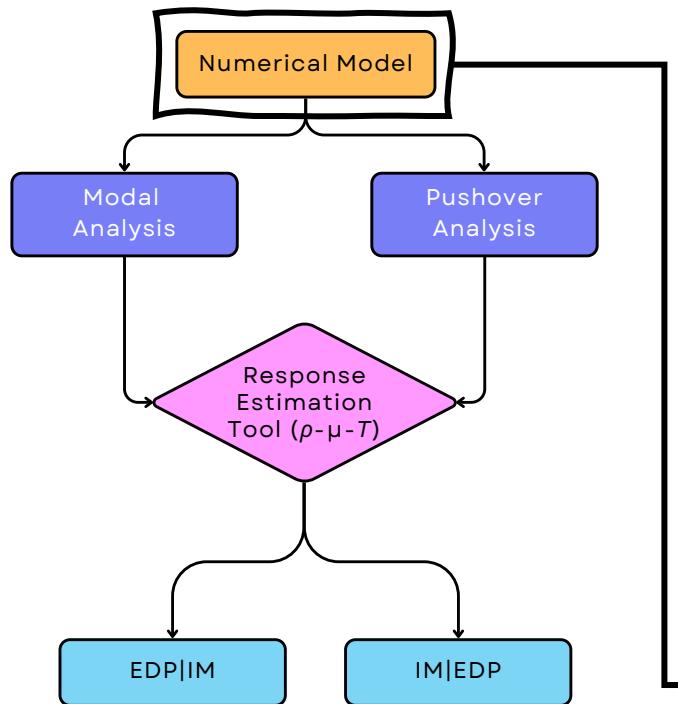
**Reduction of Uncertainty in Risk-
and Loss-Based Applications**



- *Adequate characterization of structural response*
- *Reduction and mitigation of seismic risk*
- *Drafting prioritization schemes and policies*
- *Retrofitting and structural rehabilitation*
- *Adequate allocation of resources*
- *Minimization of direct and indirect seismic losses*

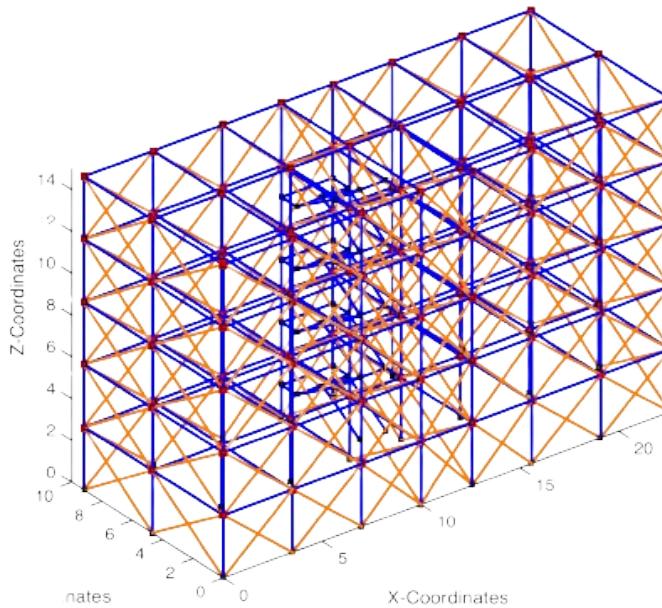
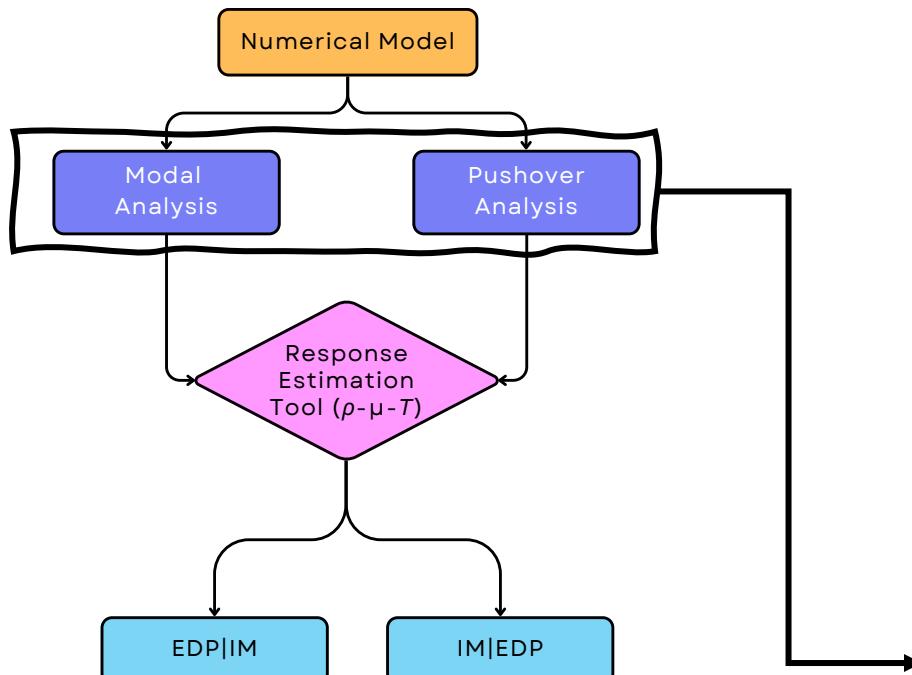


Simplified Assessment



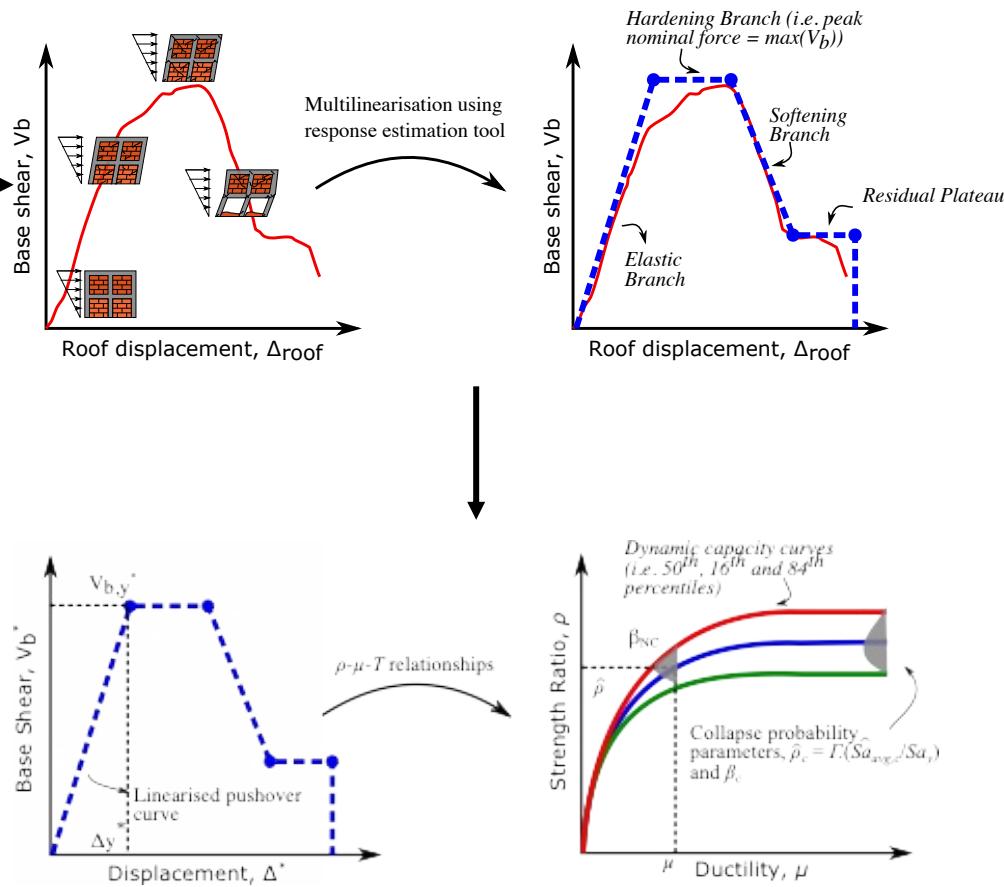
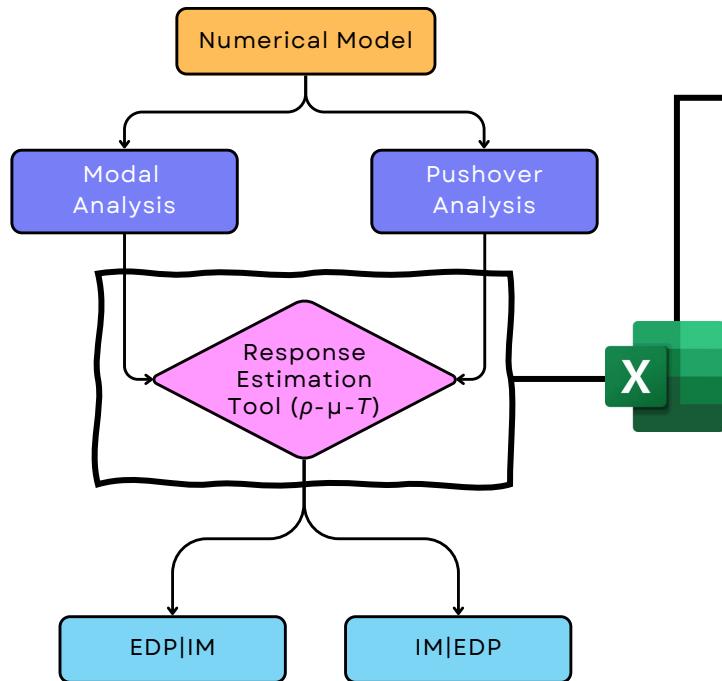
- Detailed numerical model;
- Must account for all possible inelastic mechanisms and failure modes;

Response Evaluation Tool

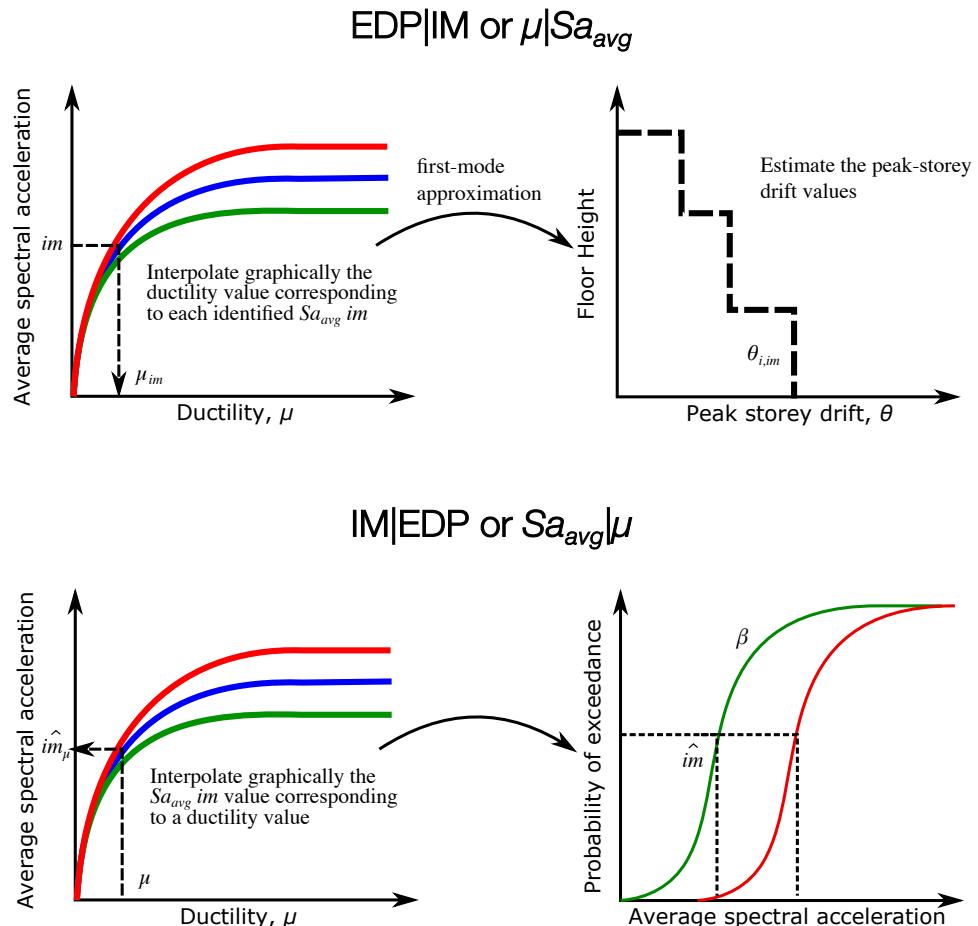
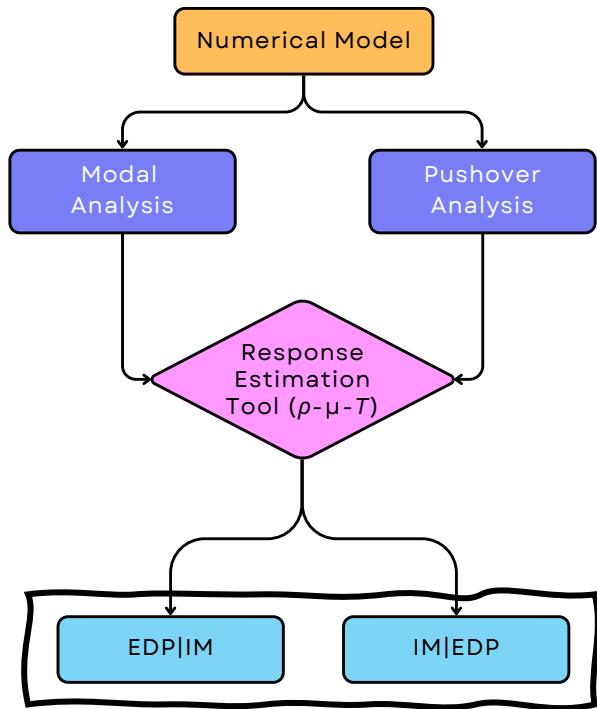


- Perform eigenvalue analysis to extract first-mode shape ordinates;
- Perform nonlinear static pushover to characterize the lateral response of the MDOF system (i.e., base-shear vs roof displacement);

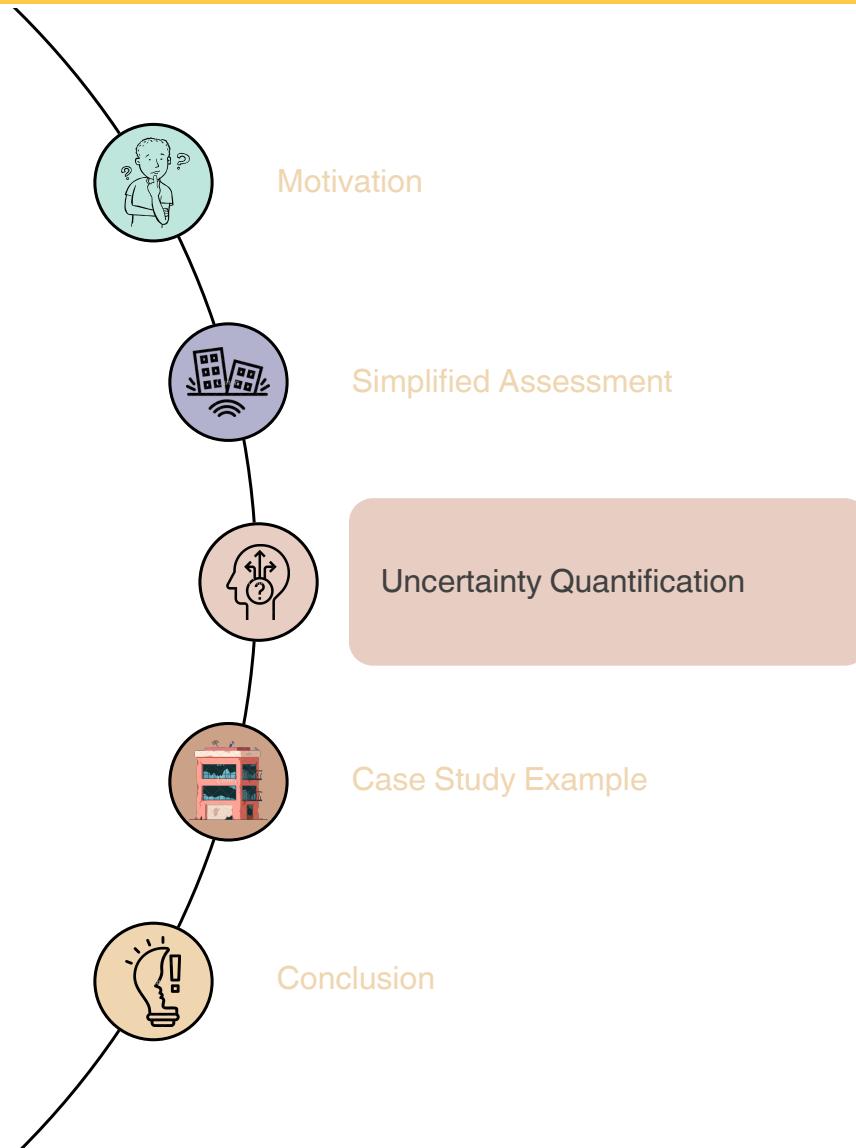
Response Evaluation Tool



Response Evaluation Tool

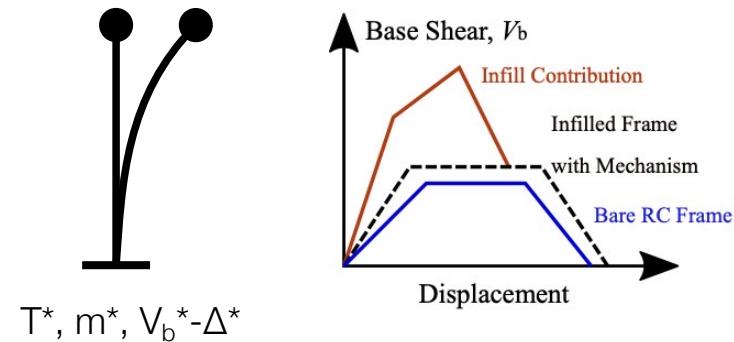
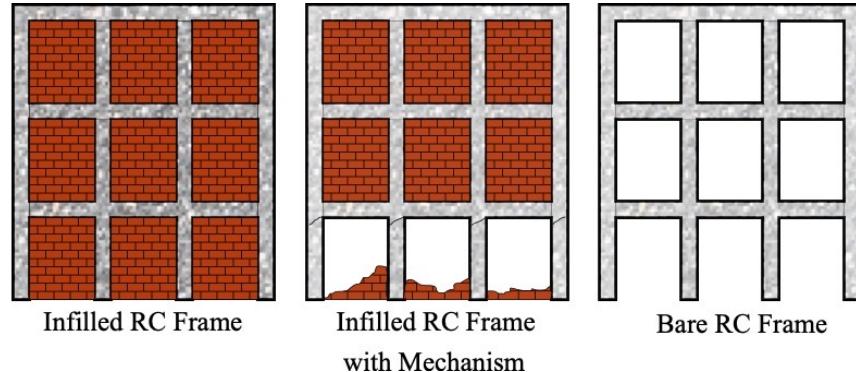
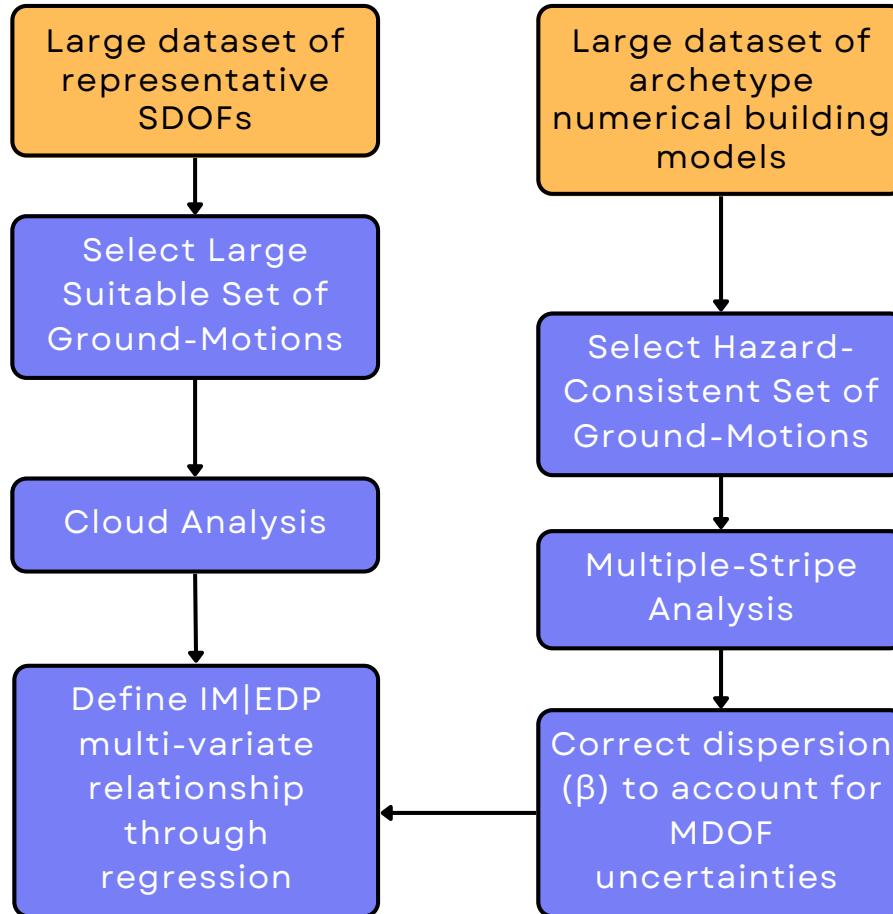


Uncertainty Quantification



Uncertainty Quantification

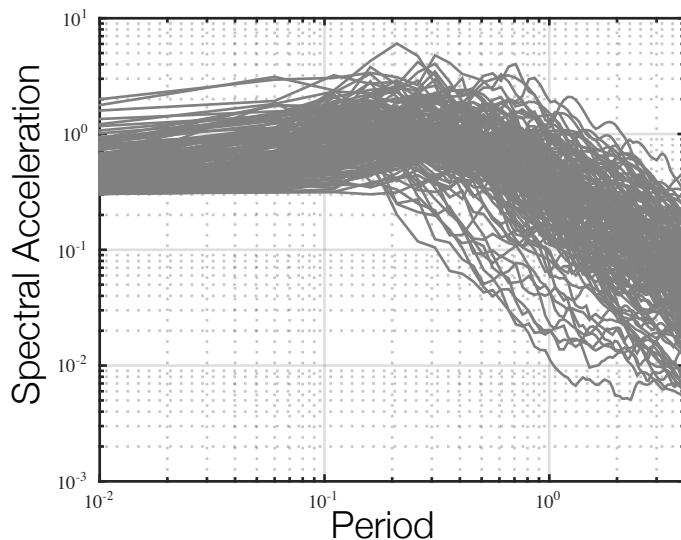
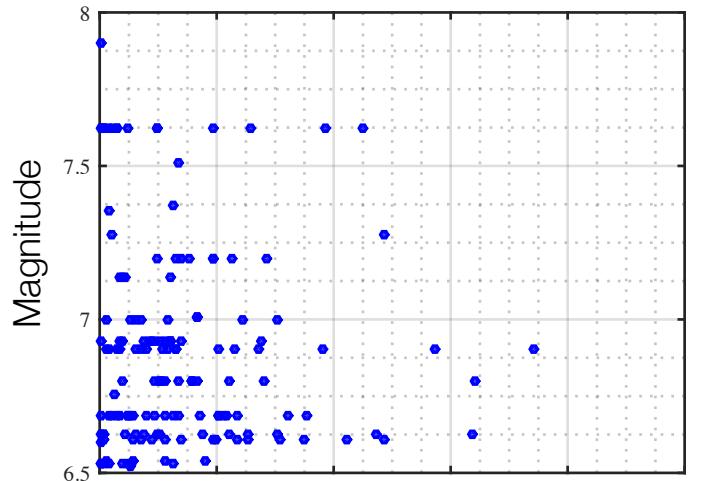
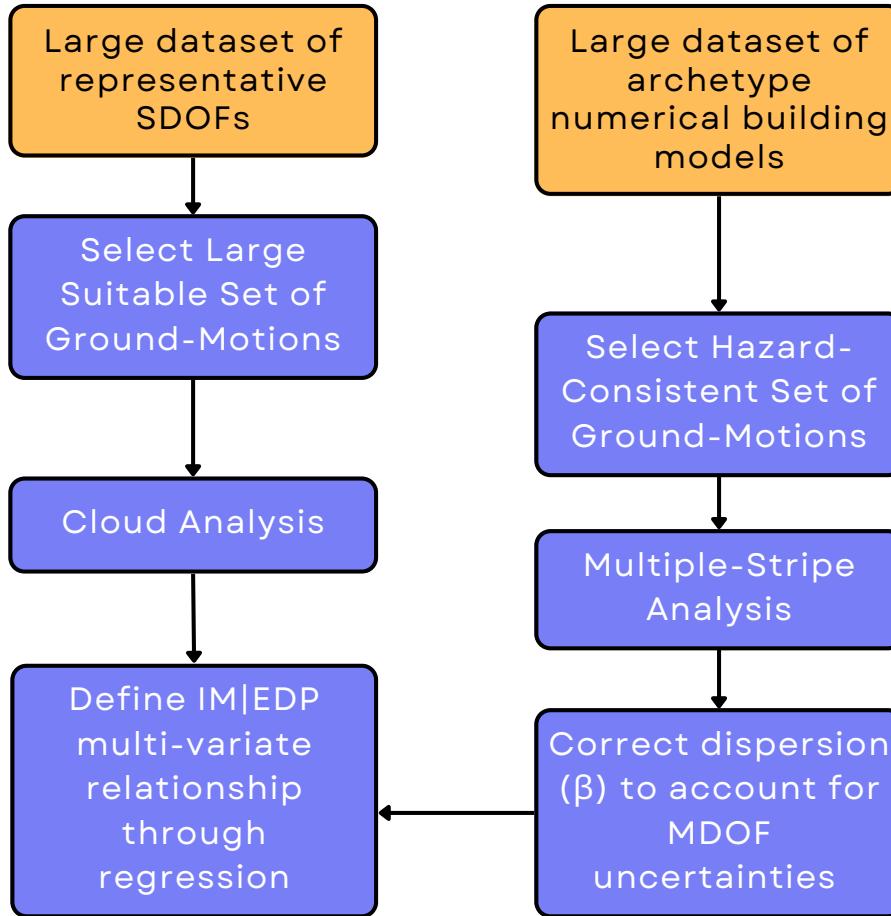
Initial Approach



Equivalent SDOF Definition

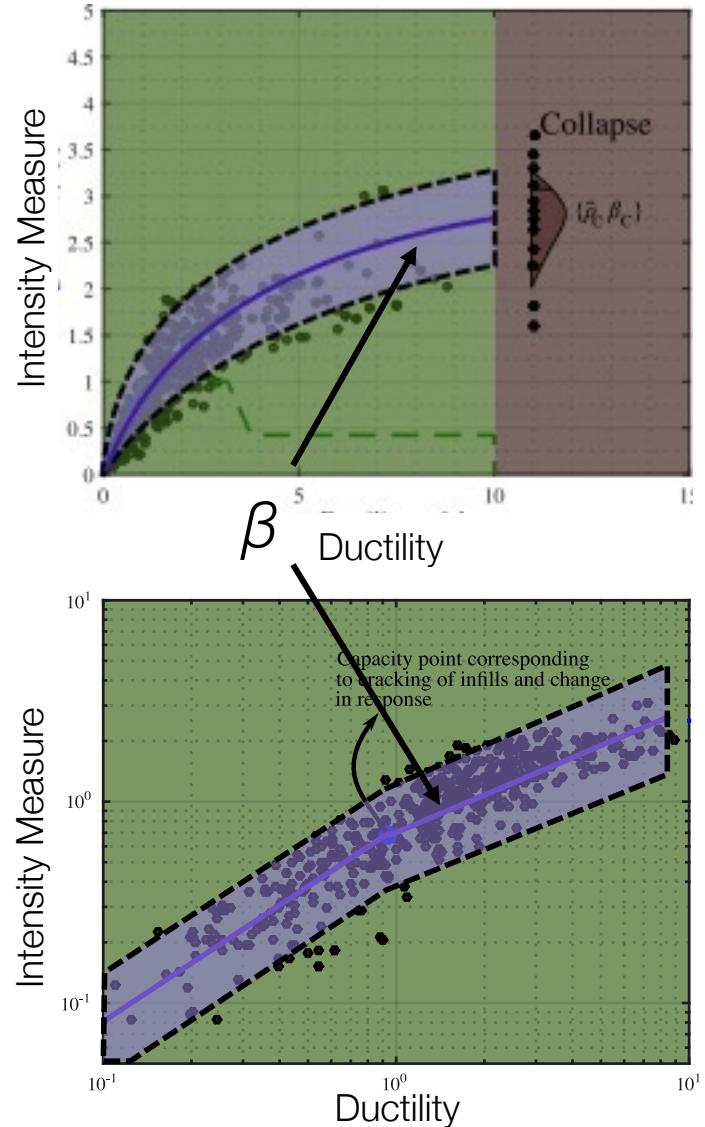
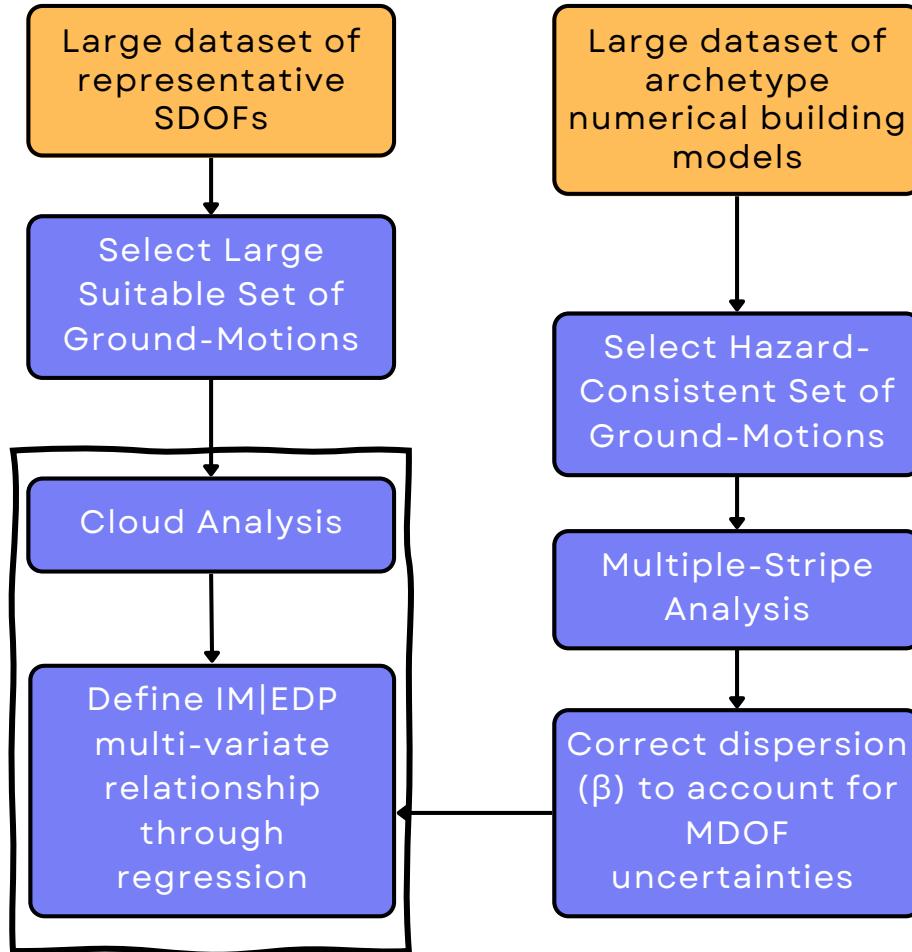
Uncertainty Quantification

Initial Approach

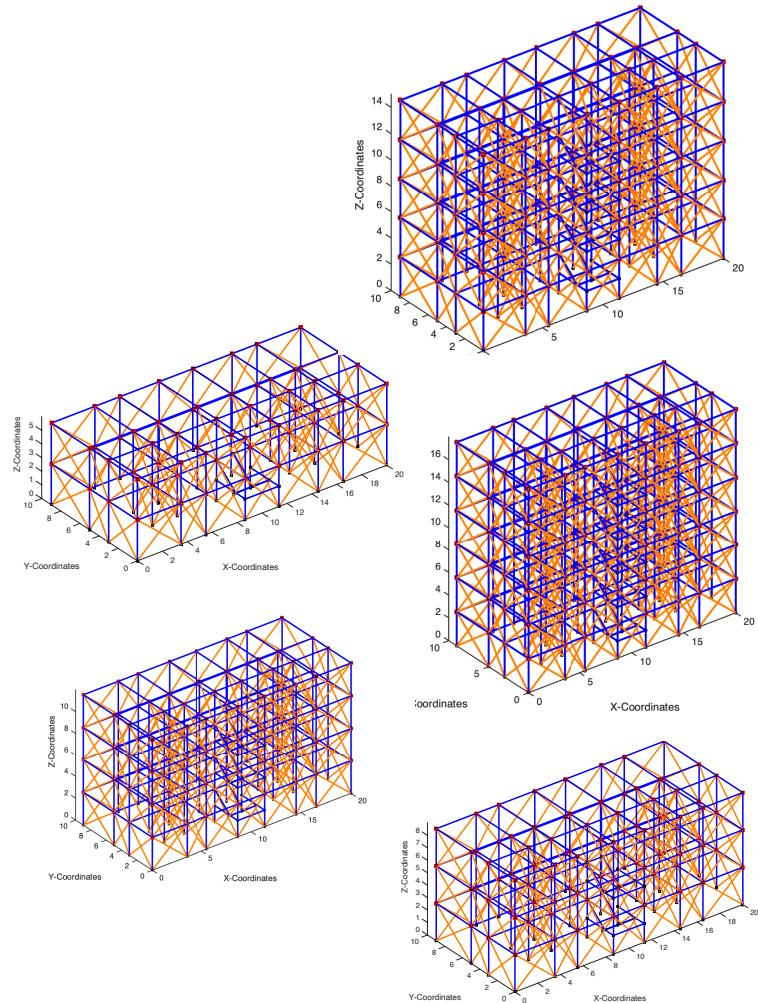
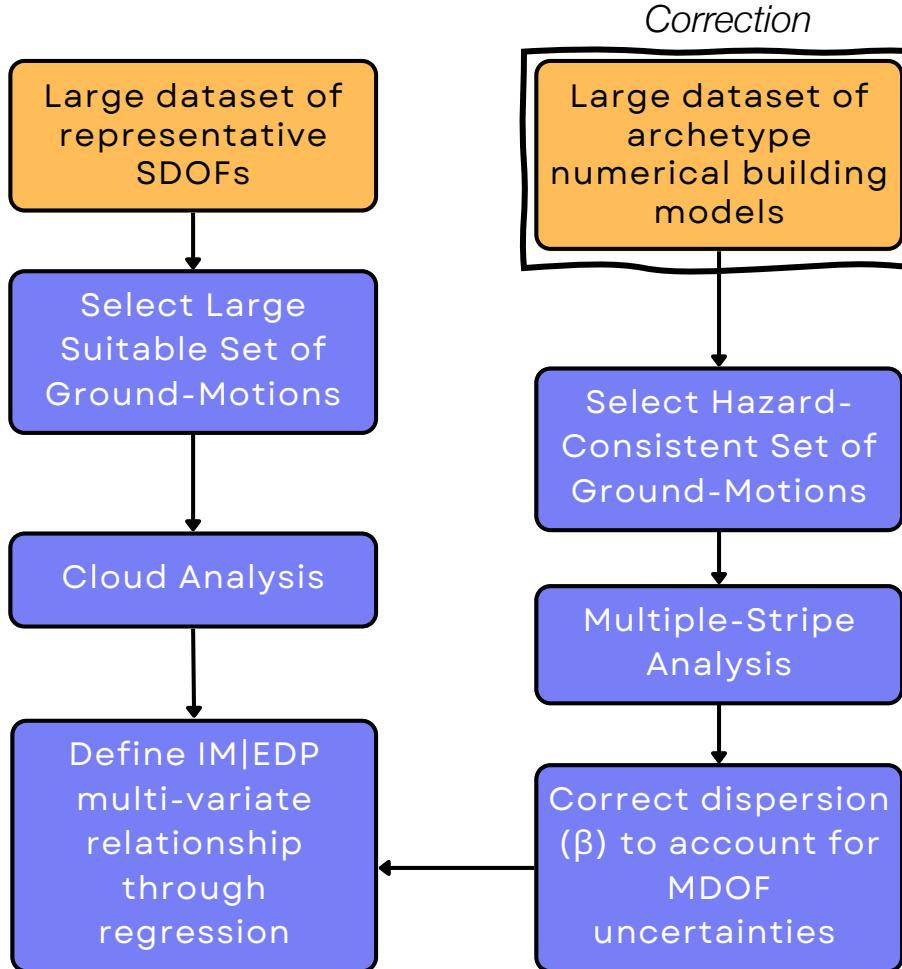


Uncertainty Quantification

Initial Approach

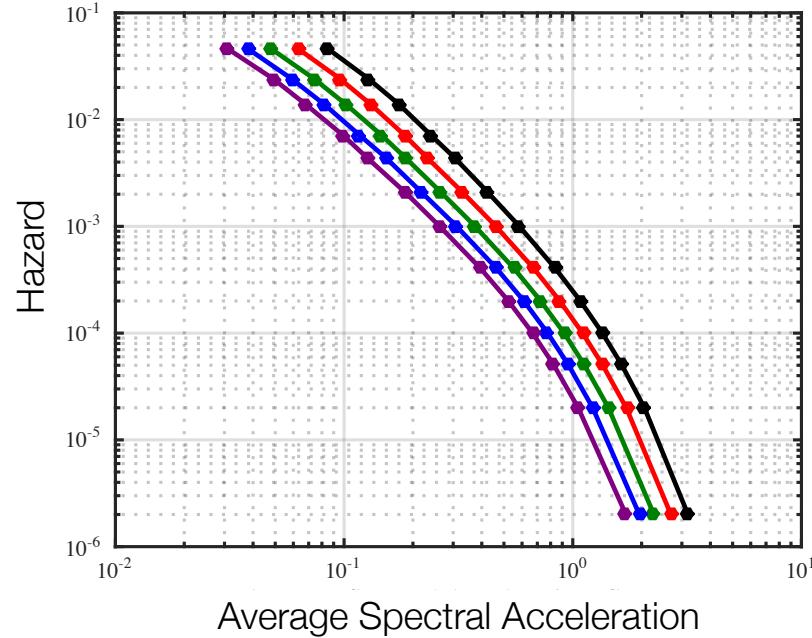
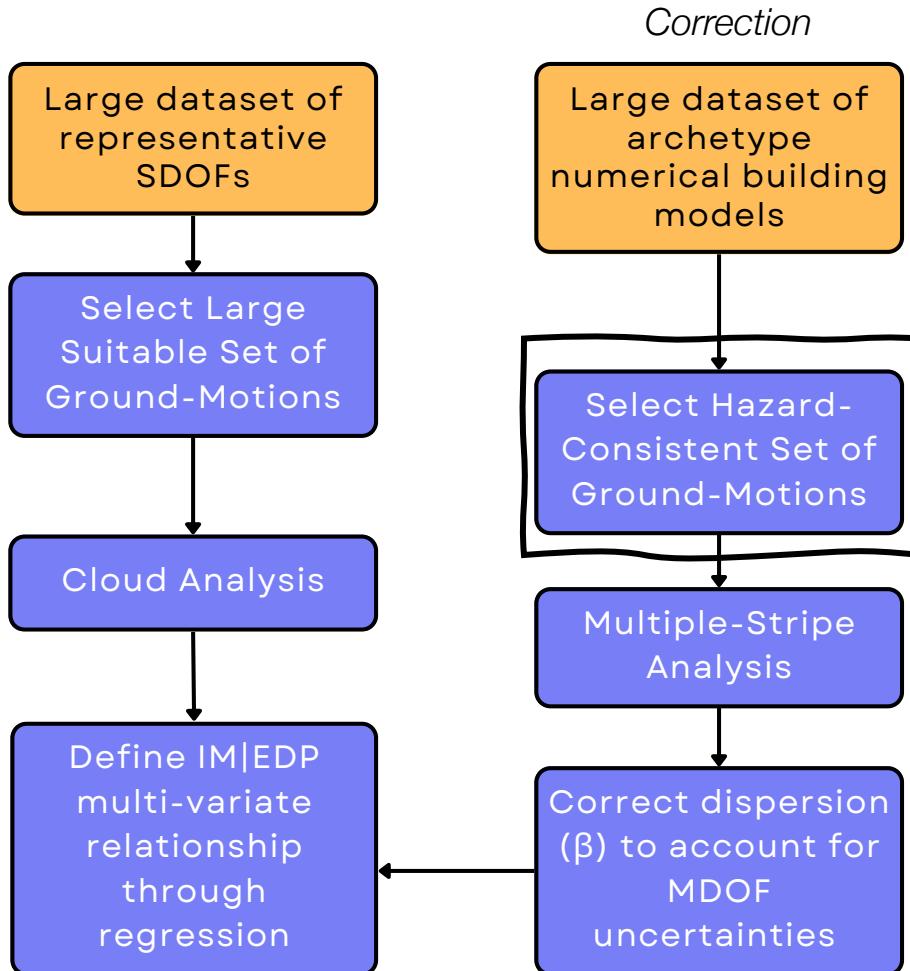


Uncertainty Quantification



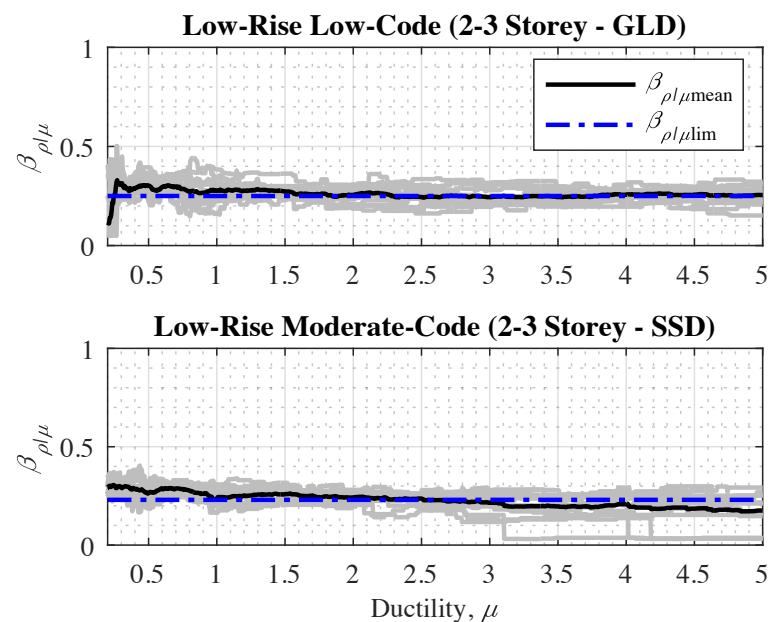
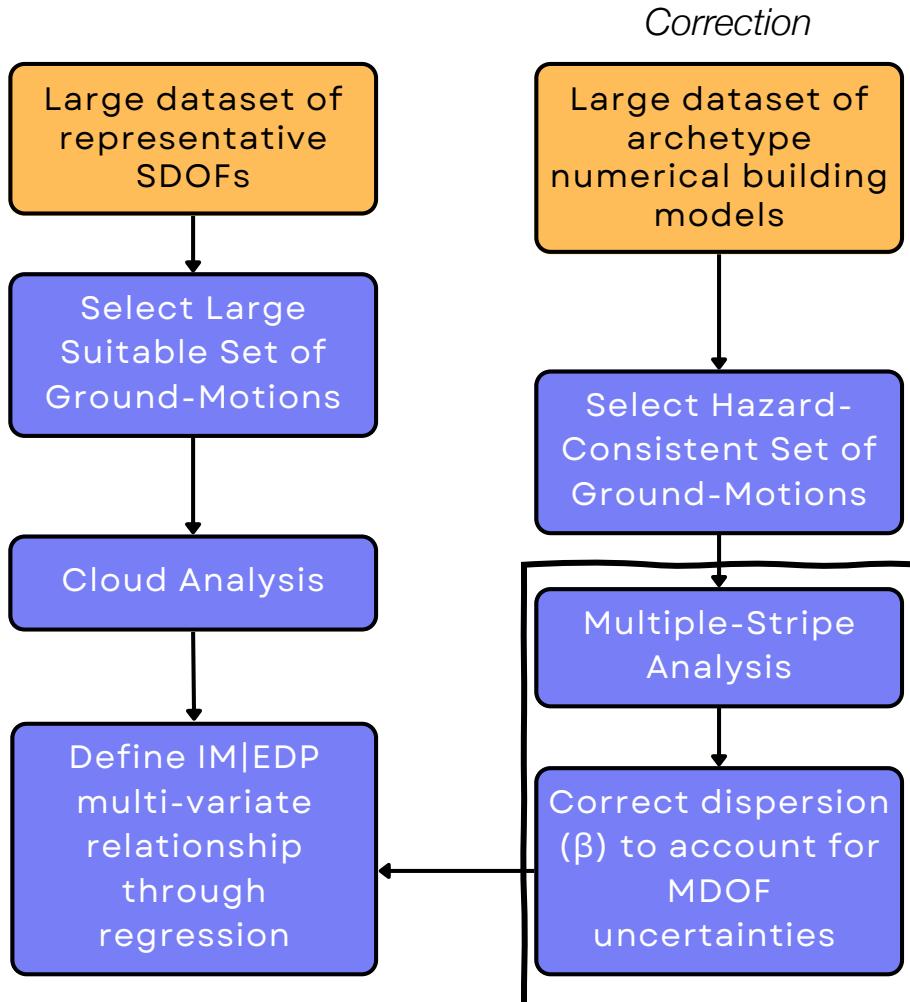
Total 105 low-rise and mid-rise infilled RC building archetypes

Uncertainty Quantification

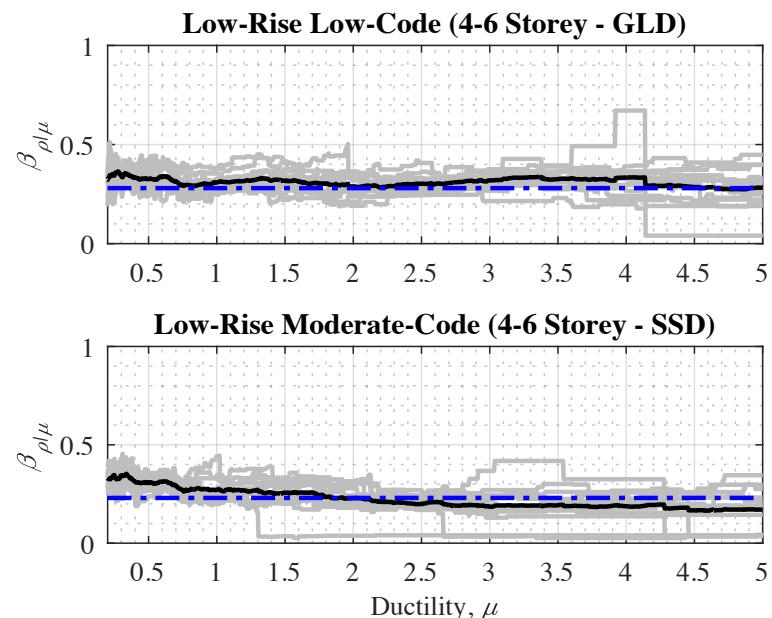
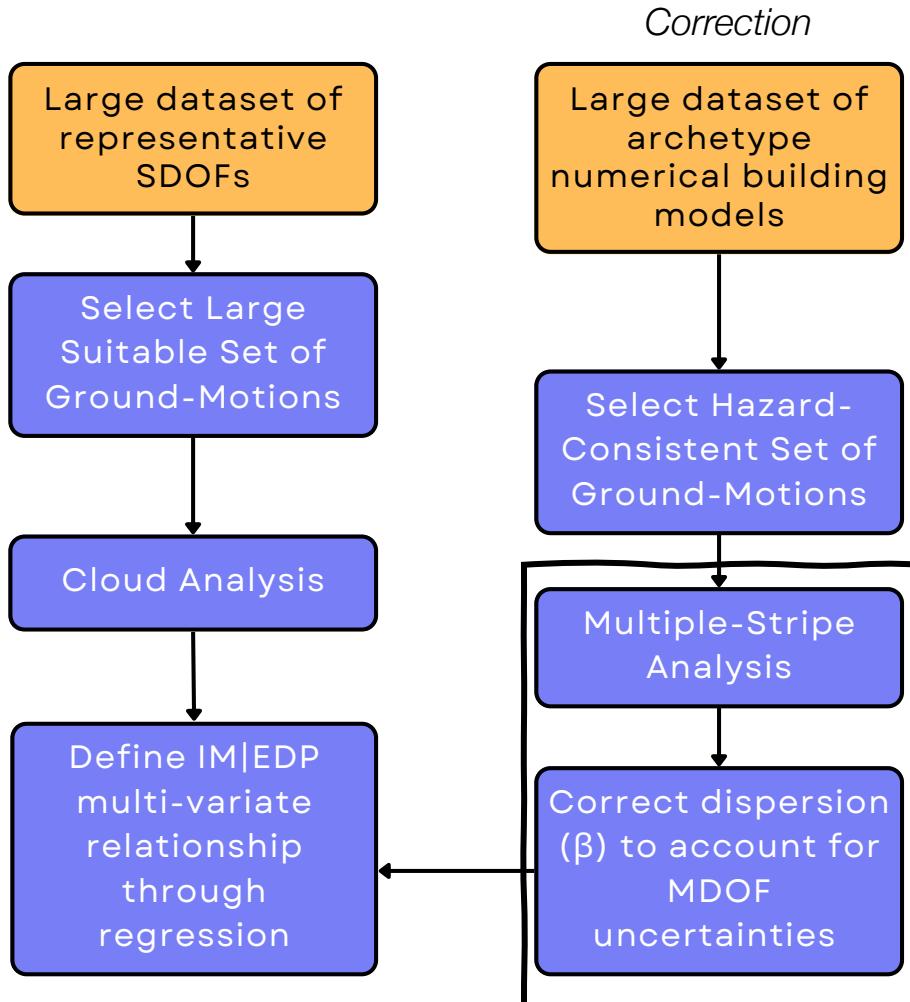


Probabilistic seismic hazard assessment expressing the hazard in L'Aquila, Italy in terms of the average spectral acceleration corresponding to conditioning periods of $T^=0.2\text{-}0.6\text{s}$*

Uncertainty Quantification



Uncertainty Quantification

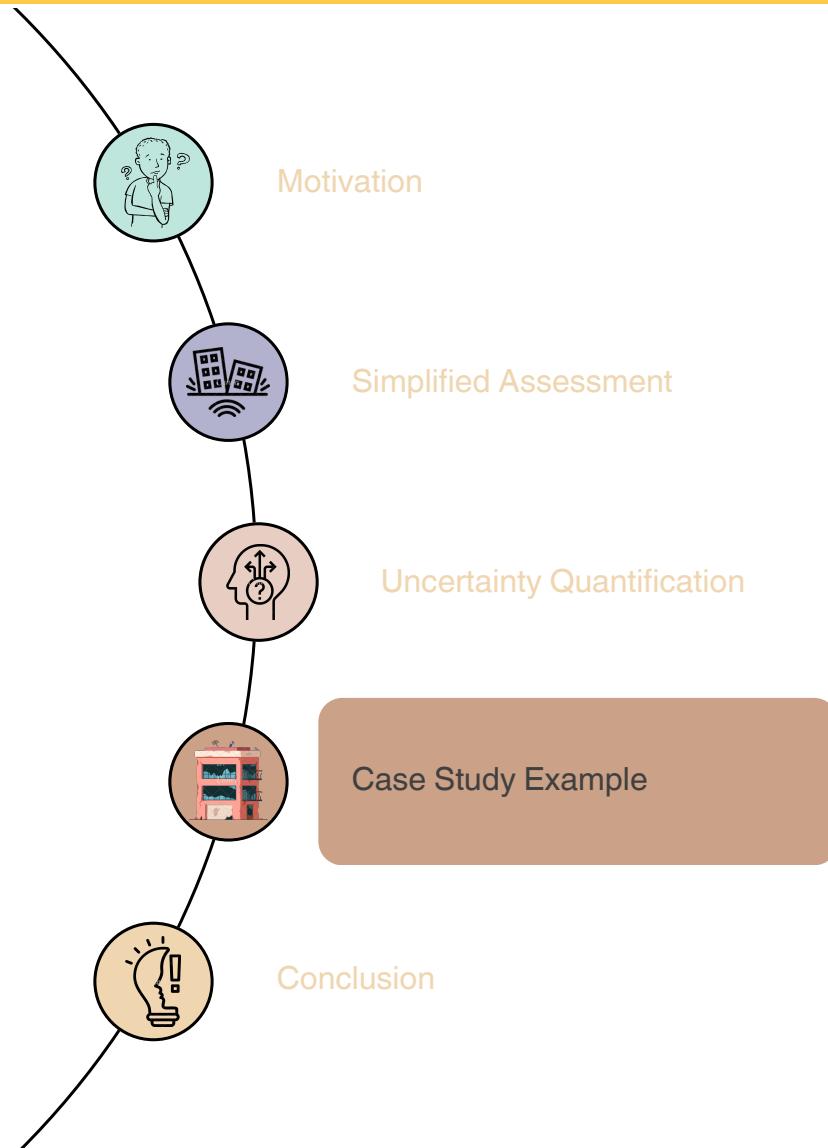


Suggested value of IM|EDP uncertainty for low and mid-rise infilled RC buildings

Seismic Code Level	Number of Stories	Taxonomy Code	Suggested Dispersion, β
Low (GLD)	Low-rise (2-3)	LC-LR	0.25
	Mid-rise (4-6)	LC-MR	0.23
Moderate (SSD)	Low-rise (2-3)	MC-LR	0.28
	Mid-rise (4-6)	MC-MR	0.23

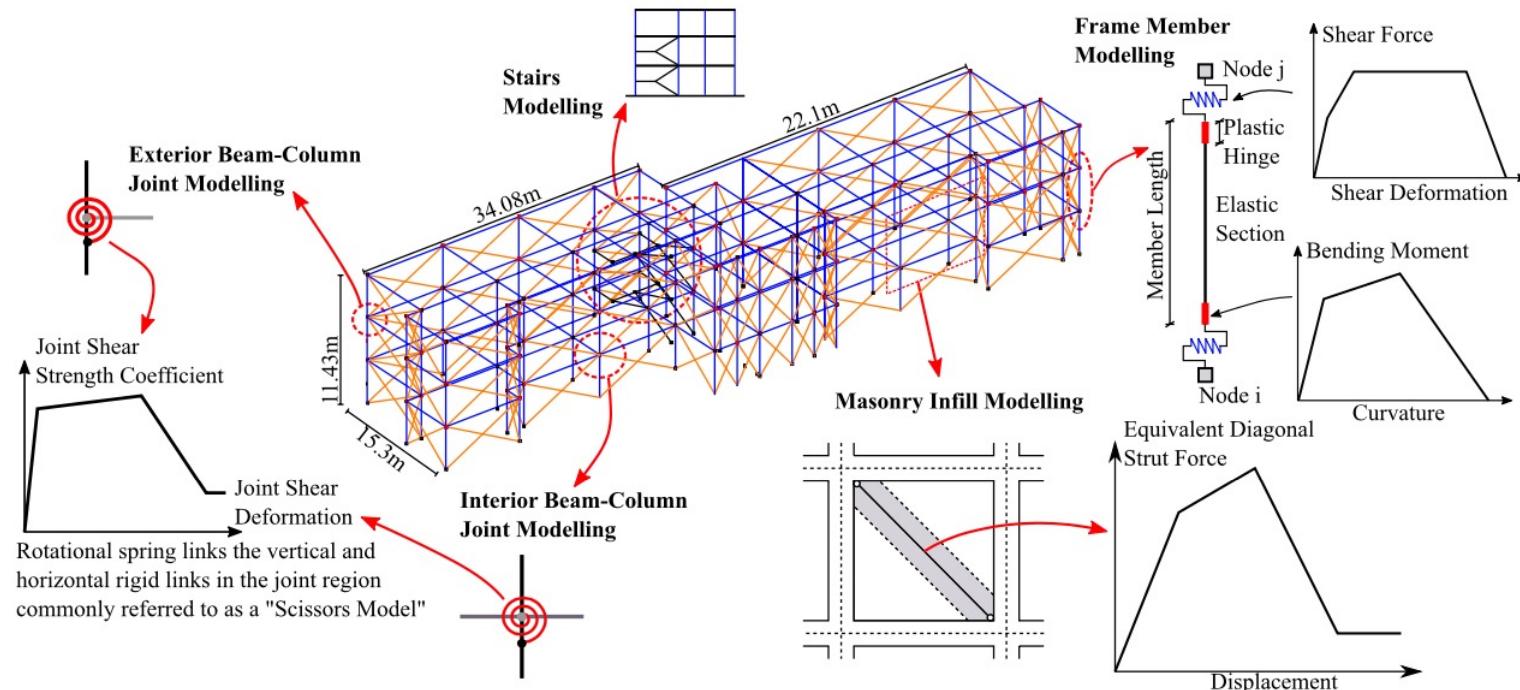
Uncertainty Quantification

9th International Conference on Computational Methods
in Structural Dynamics and Earthquake Engineering
June 12th - 14th 2023



Case Study Example

- Three-storey RC school building with masonry infills;
- Located in Napoli, Italy;
- Constructed in the 1960s, before the introduction of modern seismic design guidelines;



General layout and numerical modelling techniques of the case study school building.

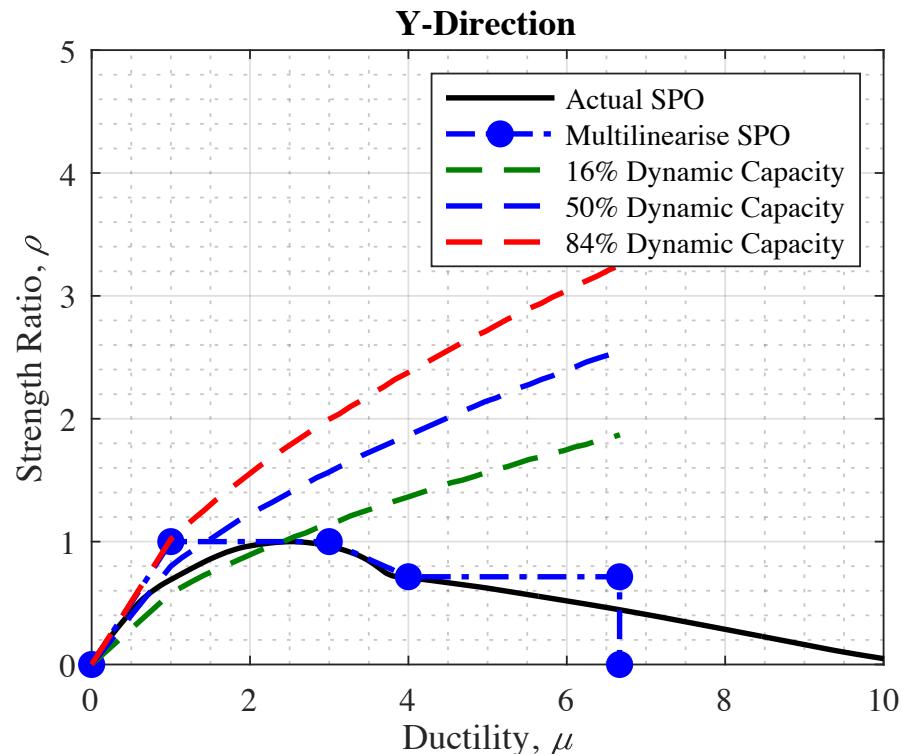
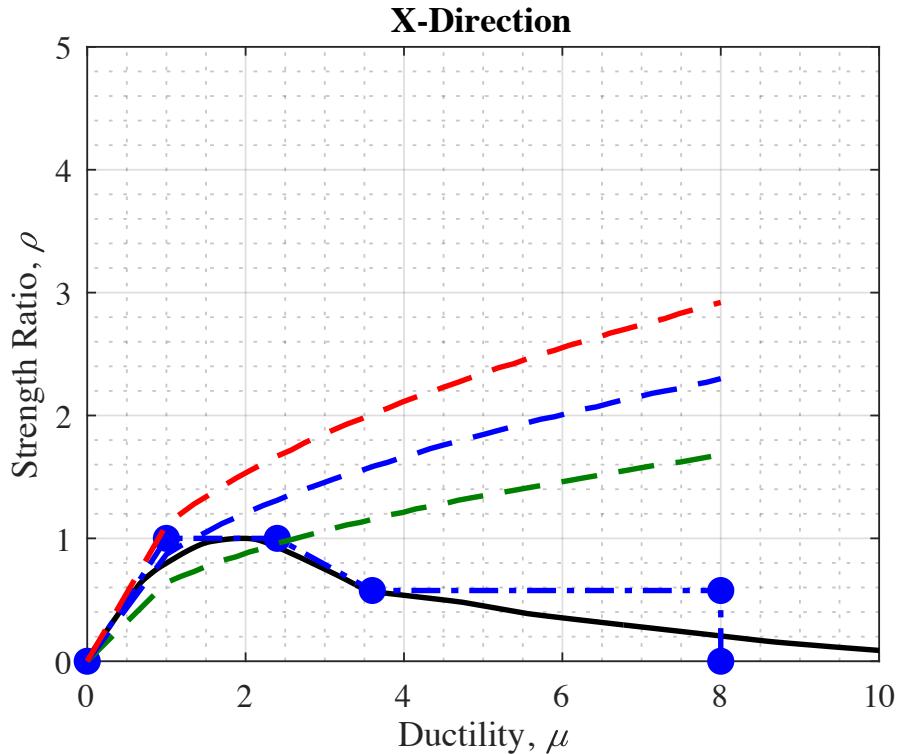
Case Study Example

Summary of the modal properties of the case study building in both principal directions

Floor No.	Mass, m_i [tonnes]	X-Direction			Y-Direction (Weaker Direction)		
		First-mode shape, Φ	Period, T_1 [s]	Yield spectral acceleration, S_{a_y} [g]	First-mode shape, Φ	Period, T_1 [s]	Yield spectral acceleration, S_{a_y} [g]
Base	0	0.00	0.62	0.42	0.00	0.36	0.40
First	985	0.22			0.22		
Second	960	0.56			0.57		
Third	806	1.00			1.00		

Case Study Example

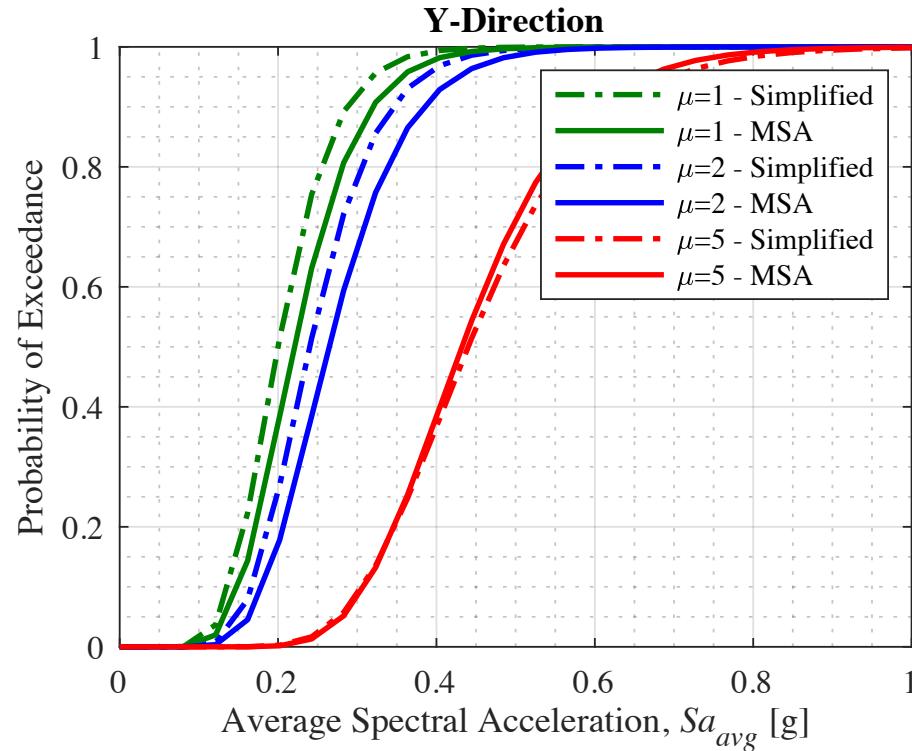
Summary of the static pushover analyses of the case study building in both principal directions



Summary of the fragility function comparisons

Ductility Thresholds	Simplified Assessment		Extensive Assessment (MSA)	
	Median intensity, Sa_{avg} [g]	Dispersion, β	Median intensity, Sa_{avg} [g]	Dispersion, β
$\mu=1$	0.20	0.25	0.22	0.28
$\mu=2$	0.24		0.27	0.26
$\mu=5$	0.44		0.43	0.26

Summary of the fragility function comparisons



Seismic Risk Calculation:

- Classical Approach:

$$\lambda = \int_0^{+\infty} P[\mu \geq \mu | IM = s] |dH(s)|$$

- Pushover-Based Risk Estimation (PB-Risk):

1. Second-order approximation of the hazard function:

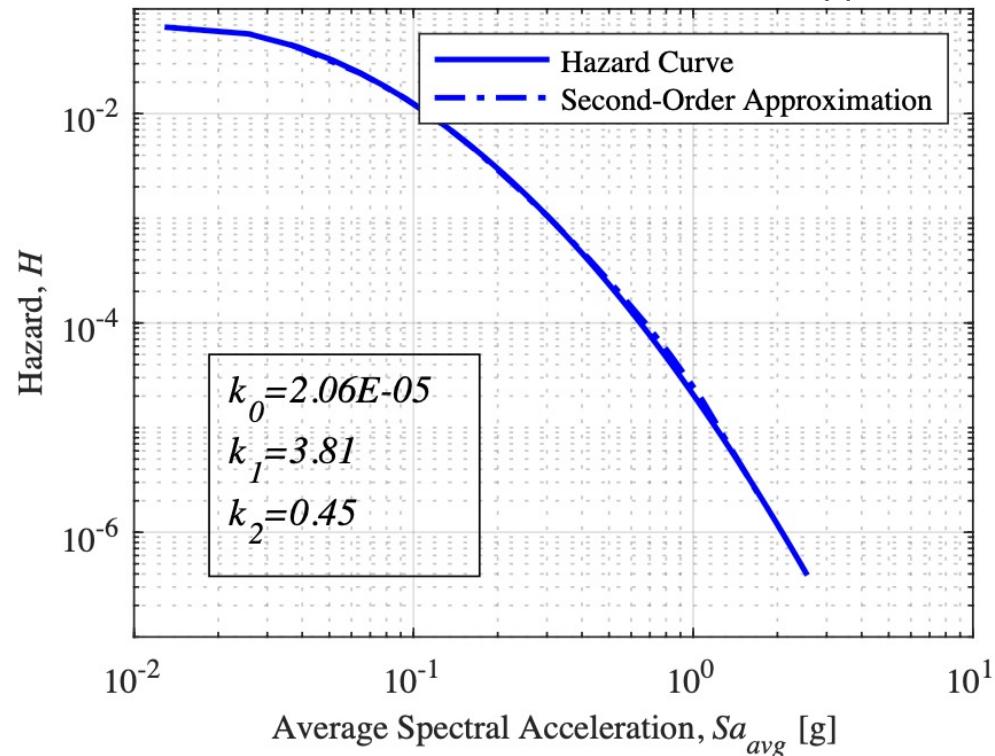
$$H(s) = k_0 \exp [-k_2 \ln^2(s) - k_1 \ln(s)]$$

2. Application of IM-based closed form expressions:

$$\lambda = \sqrt{p} k_0^{1-p} [H(s)]^p \exp \left[\frac{k_1^2}{4k_2} (1-p) \right]$$
$$p = \frac{1}{1 + 2k_2 \beta^2}$$

Case Study Example

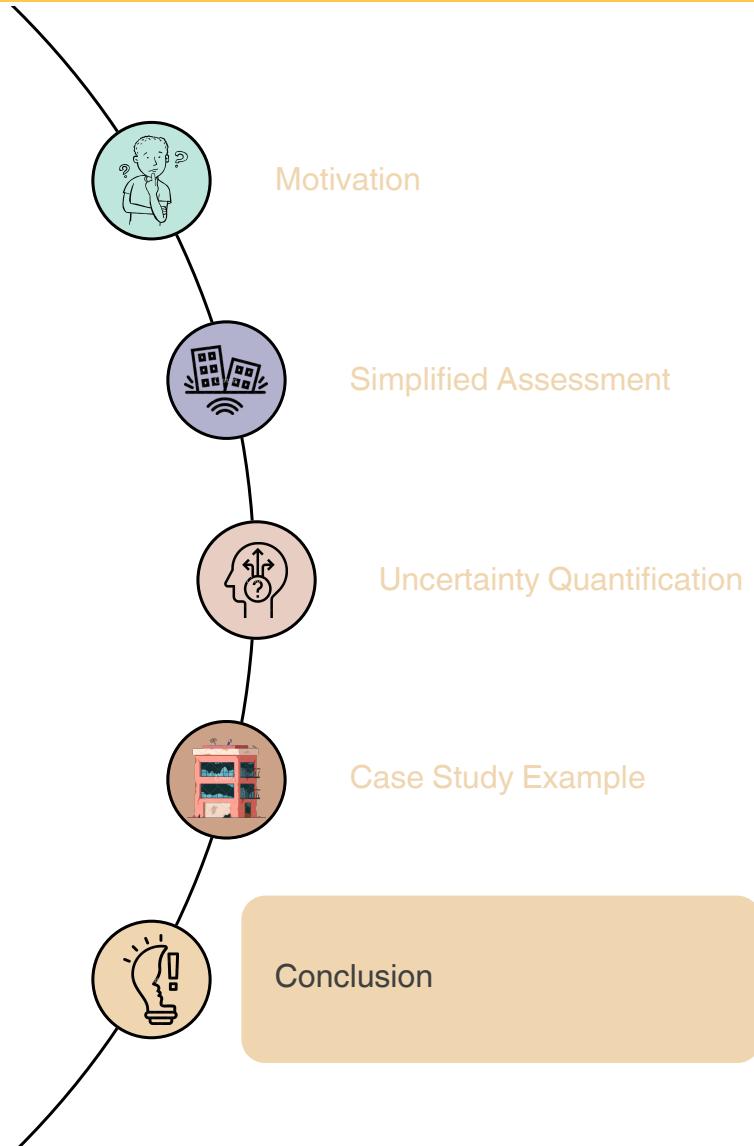
Seismic hazard characterization and second-order approximation



Summary of the risk assessment comparisons

Ductility Thresholds	PB-Risk	Classical	Error in MAFE estimation
	Mean annual frequency of exceedance (MAFE), λ		
$\mu=1$	0.0031	0.0029	6.89%
$\mu=2$	0.0021	0.0019	10.52%
$\mu=5$	4.92E-04	5.02E-04	1.6%

Conclusion



- A simplified tool for the seismic performance assessment of infilled RC frames was presented;
- The epistemic uncertainty associated with structural response ($IM|EDP$) was quantified for the infilled RC typology and different sub-taxonomies;
- The suggested values of the record-to-record variability could be incorporated with other simplified methodologies for the derivation of fragility functions or risk metrics (e.g. *PB-Risk*);
- The suggested values were validated on a case-study school buildings where an adequate match in terms of vulnerability and risk parameters was observed;
- Good agreement between the results of classical and simplified methodologies;

Links:

- Database of Archetype Building Models:

<https://github.com/gerardjoreilly/Infilled-RC-Building-Database>

- Response Estimation Tool for Infilled RC Frame Structures:

<https://github.com/gerardjoreilly/Infilled-RC-Building-Response-Estimation>

Publications:

- Nafeh A.M.B., O'Reilly G.J. (2022) Unbiased simplified seismic fragility estimation of non-ductile infilled RC structures. Soil Dynamics and Earthquake Engineering 157:107253. <https://doi.org/10.1016/j.soildyn.2022.107253>
- *PB-Risk*: Nafeh, A.M.B., O'Reilly, G.J. (2023) Simplified pushover-based seismic risk assessment methodology for existing infilled frame structures. Bulletin of Earthquake Engineering 21, 2337–2368 <https://doi.org/10.1007/s10518-022-01600-y>

Thank you for your attendance

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