# **BUCK CONVERTER TRANSFER FUNCTION DERIVATION**

### AVERAGE MODEL & SMALL SIGNAL CIRCUITS

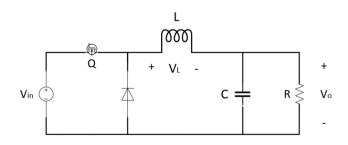
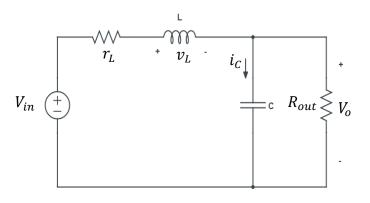
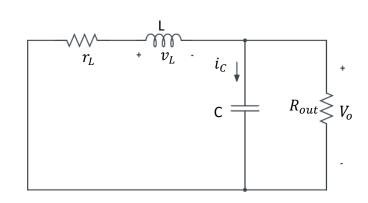


Figure 1. Buck Converter

#### *Interval I:* D

#### Interval II: 1 - D





#### 1. **Averaged, Small Signal Circuit Description**

D Interval:

$$v_L(t) = V_{in} - i_L(t)r_L - V_c$$

$$v_L(t) = V_{in} - i_L(t)r_L - V_o \qquad \parallel \qquad i_C(t) = i_L(t) - \frac{V_o}{R_{out}}$$

1 - D Inverval:

$$v_L(t) = -i_L(t)r_L - V_0$$

$$v_L(t) = -i_L(t)r_L - V_0$$
  $\parallel i_C(t) = i_L(t) - \frac{V_0}{R_{out}}$ 

## 2. Capacitor Charge & Volt. Second Balance Equations

$$L\frac{di_{L}}{dt} = D(V_{in} - i_{L}r_{L} - V_{o}) + (1 - D)(-i_{L}r_{L} - V_{o})$$

$$C\frac{dV_{C}}{dt} = D(i_{L} - \frac{V_{o}}{R_{out}}) + (1 - D)(i_{L} - \frac{V_{o}}{R_{out}})$$

## 3. Small Signal "hat" Terms ( $x(t) = X + \hat{x}$ )

Inductor:

$$L\frac{d(I_L + \hat{\imath}_L)}{dt} = \left( (D + \hat{d})(V_{in} + \hat{v}_{in}) - (I_L + \hat{\imath}_L)r_L - (V_o + \hat{v}_o) \right) + \left( \left( 1 - (D + \hat{d})\right) (-(I_L + \hat{\imath}_L)r_L - (V_o + \hat{v}_o) \right)$$

Single hat terms:

$$\begin{split} \boldsymbol{L}\frac{d(\hat{\imath}_{L})}{dt} &= \hat{d}V_{in} - \hat{d}I_{L}r_{L} - \hat{d}V_{o} + D\hat{v}_{in} - D\hat{\imath}_{L}r_{L} - D\hat{v}_{o} - \hat{\imath}_{L}r_{L} - \hat{v}_{o} + \hat{d}I_{L}r_{L} + \hat{d}V_{o} + D\hat{\imath}_{L}r_{L} \\ &\quad + D\hat{v}_{o} \\ \hline \boldsymbol{L}\frac{d(\hat{\imath}_{L})}{dt} &= \hat{d}V_{in} + D\hat{v}_{in} - \hat{\imath}_{L}r_{L} - \hat{v}_{o} \end{split} \quad \text{Averaged Small Signal}$$

DC Terms:

$$egin{aligned} L rac{d(I_L)}{dt} &= DV_{in} - DI_L r_L - DV_o - I_L r_L - V_o + DI_L r_L + DV_o \ \hline 0 &= DV_{in} - I_L r_L - V_o & ext{Averaged steady-state DC eqn.} \end{aligned}$$

Capacitor:

$$C\frac{d(V_C + \hat{v}_C)}{dt} = (D + \hat{d}) \left( (I_L + \hat{\imath}_L) - \frac{(V_O + \hat{v}_O)}{R_{out}} \right) + (1 - (D + \hat{d})) \left( (I_L + \hat{\imath}_L) - \frac{(V_O + \hat{v}_O)}{R_{out}} \right)$$

Single hat terms:

$$C\frac{d(\hat{v}_C)}{dt} = \hat{d}I_L - \hat{d}\frac{V_o}{R_{out}} + D\hat{\imath}_L - D\frac{\hat{v}_o}{R_{out}} + \hat{\imath}_L - \frac{\hat{v}_o}{R_{out}} - \hat{d}I_L + \hat{d}\frac{V_o}{R_{out}} - D\hat{\imath}_L + D\frac{\hat{v}_o}{R_{out}}$$

$$C\frac{d(\hat{v}_C)}{dt} = \hat{\imath}_L - \frac{\hat{v}_o}{R_{out}}$$
Averaged Small Signal

DC Terms:

$$C\frac{d(V_C)}{dt} = DI_L - D\frac{V_o}{R_{out}} + I_L - \frac{V_o}{R_{out}} - DI_L + D\frac{V_o}{R_{out}}$$

$$C\frac{d(V_C)}{dt} = I_L - \frac{V_o}{R_{out}}$$
Averaged Steady-State DC eqn

**Input Current:** 

$$i_{in}(t) = (D + \hat{d}) < i_L(t) >$$
 Very small compared to DC values, ignored. 
$$I_{in} + \hat{\iota}_{in} = DI_L + \hat{d}I_L + D\hat{\iota}_L + \hat{d}\hat{\iota}_L$$

$$egin{align*} \widehat{\iota}_{in} &= \widehat{d}I_L + D\widehat{\iota}_L \ \hline I_{in} &= DI_L \ \hline \end{pmatrix} &
ightarrow ext{Averaged small signal} \ 
ightarrow ext{Steady-state DC signal} \ \end{array}$$

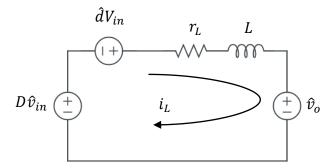
Small signal and steady-state DC signal analysis has been implemented. Now, they should be merged in one circuit to get the transfer function of the system.

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#### **Inductor:**

Small Signal Eqn:

$$L\frac{d(\hat{\imath}_L)}{dt} = \hat{d}V_{in} + D\hat{v}_{in} - \hat{\imath}_L r_L - \hat{v}_o$$



# Capacitor:

Small Signal Eqn:

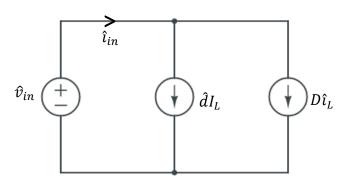
$$C\frac{d(\hat{v}_C)}{dt} = \hat{\iota}_L - \frac{\hat{v}_o}{R_{out}}$$

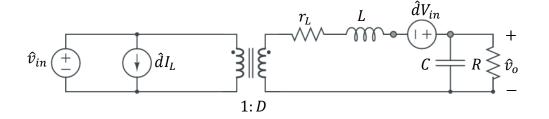
$$\hat{\iota}_L \qquad \qquad R \geqslant \hat{v}_o$$

# Input Current:

Small Signal Eqn:

$$\hat{\imath}_{in} = \hat{d}I_L + D\hat{\imath}_L$$





#### 4. Control-to-Output Transfer Function

$$\widehat{\boldsymbol{v}}_{o} = V_{in} \widehat{\boldsymbol{d}} \times \frac{\left(\frac{1}{sC}//R_{out}\right)}{r_{L} + sL + \left(\frac{1}{sC}//R_{out}\right)}$$

$$\frac{1}{sC}//R_{out} = \frac{\frac{R_{out}}{sC}}{R_{out} + \frac{1}{sC}} = \frac{R_{out}}{1 + sCR_{out}}$$

$$G_p = \frac{\hat{v}_o}{\hat{d}} = V_{in} \frac{\frac{R_{out}}{1 + sCR_{out}}}{r_L + sL + \frac{R_{out}}{1 + sCR_{out}}} \rightarrow \frac{R_{out}}{r_L + sLCR_{out} + sL + s^2R_{out}LC + R_{out}} \times \frac{\frac{1}{R_{out}}}{\frac{1}{R_{out}}}$$

$$\frac{\hat{v}_o}{\hat{d}} = V_{in} \frac{1}{s^2 LC + s(\frac{L}{R_{out}} + r_L C) + 1 + \frac{r_L}{R_{out}}}$$

If there is no resistance of the inductor, use this formula:

$$\frac{\hat{v}_o}{\hat{d}} = V_{in} \frac{1}{s^2 LC + s \frac{L}{R_{out}} + 1}$$

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