

ISTANBUL TECHNICAL UNIVERSITY ★ GRADUATE SCHOOL

**CONDITION MONITORING AND
FAULT DIAGNOSIS OF VFD-FED
INDUCTION MOTORS**

M.Sc. THESIS

Alper SENEM

Department of Mechatronics Engineering

Mechatronics Engineering Programme

JUNE 2021

ISTANBUL TECHNICAL UNIVERSITY ★ GRADUATE SCHOOL

**CONDITION MONITORING AND
FAULT DIAGNOSIS OF VFD-FED
INDUCTION MOTORS**

M.Sc. THESIS

**Alper SENEM
(518181003)**

Department of Mechatronics Engineering

Mechatronics Engineering Programme

Thesis Advisor: Prof. Dr. Şeniz ERTUĞRUL

JUNE 2021

İSTANBUL TEKNİK ÜNİVERSİTESİ ★ LİSANSÜSTÜ EĞİTİM ENSTİTÜSÜ

**DEĞİŞKEN FREKANSLI SÜRÜCÜ
İLE BESLENEN ASENKRON MOTORLARDA
DURUM İZLEME VE ARIZA TANILAMA**

YÜKSEK LİSANS TEZİ

**Alper SENEM
(518181003)**

Mekatronik Mühendisliği Anabilim Dalı

Mekatronik Mühendisliği Programı

Tez Danışmanı: Prof. Dr. Şeniz ERTUĞRUL

HAZİRAN 2021

Alper SENEM, a M.Sc. student of ITU Graduate School student ID 518181003, successfully defended the thesis entitled “CONDITION MONITORING AND FAULT DIAGNOSIS OF VFD-FED INDUCTION MOTORS”, which he/she prepared after fulfilling the requirements specified in the associated legislations, before the jury whose signatures are below.

Thesis Advisor : **Prof. Dr. Şeniz ERTUĞRUL**
Istanbul Technical University

Jury Members : **Prof. Dr. Name SURNAME**
Middle East Technical University

Prof. Dr. Name SURNAME
Boğaziçi University

Prof. Dr. Name SURNAME
Bilkent University

Prof. Dr. Name SURNAME
Sabancı University

Prof. Dr. Name SURNAME
Koç University

Date of Submission : 11 June 2021

Date of Defense : 11 June 2021

To my family,

FOREWORD

For the foreword, 1 line spacing must be set. The foreword, written as a first page of the thesis must not exceed 2 pages.

The acknowledgments must be given in this section.

After the foreword text, name of the author (right-aligned), and the date (as month and year) must be written (left-aligned). These two expressions must be in the same line.

The foreword is written with 1 line spacing.

June 2021

Alper SENEM
(Mechanical Engineer)

TABLE OF CONTENTS

	<u>Page</u>
FOREWORD.....	ix
TABLE OF CONTENTS.....	xi
ABBREVIATIONS	xiii
SYMBOLS.....	xv
LIST OF TABLES	xvii
LIST OF FIGURES.....	xix
SUMMARY	xxi
ÖZET	xxiii
1. INTRODUCTION	1
1.1 Overview	1
1.2 Objectives of Research	2
1.3 Organization of Thesis.....	3
2. CONDITION MONITORING OF INDUCTION MOTORS: BACK- GROUND	5
2.1 Introduction of Induction Motors	5
2.1.1 Principle of operation.....	5
2.1.2 VFD-fed induction motors.....	6
2.1.3 Need for condition monitoring.....	8
2.1.4 Maintenance strategies.....	8
2.2 Induction Motor Fault Types	10
2.2.1 Bearing related faults	11
2.2.2 Stator related faults	12
2.2.3 Rotor related faults.....	14
2.3 Condition Monitoring Techniques.....	16
2.3.1 Temperature monitoring.....	16
2.3.2 Vibration monitoring.....	16
2.3.3 Motor current monitoring	17
3. EXPERIMENTAL SETUP AND METHODOLOGY	19
REFERENCES.....	23
APPENDICES	27
CURRICULUM VITAE	29

ABBREVIATIONS

AIC	: Akaike Information Criteria
ANN	: Artificial Neural Network
App	: Appendix
BP	: Backpropagation
CGI	: Common Gateway Interface
ESS	: Error sum-of-squares
GARCH	: Generalized Autoregressive Conditional Heteroskedasticity
GIS	: Geographic Information Systems
HCA	: Hierarchical Cluster Analysis
Mbps	: Megabits per second
St	: Station
SWAT	: Soil and Water Assessment Tool
UMN	: University of Minnesota

SYMBOLS

C	: Capacitance
H	: The amount of heat
M_x, M_y	: Torque Components
N_x, N_y, N_z	: Normal Power Components
q	: Phase load
t	: Time
u, v	: Displacement Vector Components
w	: Angular velocity
XC	: Capacitive reactance
XL	: Inductive reactance
α	: Angle of deviation from the direction of the principal stresses
ρ	: Density
$\sigma_x, \sigma_y, \sigma_{xy}$: Shell internal stresses

LIST OF TABLES

	<u>Page</u>
Table 2.1 : Table with single row and centered columns.	10
Table 3.1 : Equipments used in experimental-setup.	19
Table 3.2 : Nominal Values of WAT Motor 3-phase Induction Motor.	20
Table 3.3 : Table with single row and centered columns.	20

LIST OF FIGURES

	<u>Page</u>
Figure 2.1 : Steady-state torque-speed curve of an induction motor, adapted from [1].	5
Figure 2.2 : Squirrel cage induction motor structure, courtesy of WAT Motor Co.	6
Figure 2.3 : (a) Torque–speed curves for different voltages in line-start operation and (b) Torque–speed curves for different voltages and frequencies in VFD-fed operation, adapted from [1].	7
Figure 2.4 : Maintenance types, adapted from [2].	9
Figure 2.5 : The P-F curve shows the point where the fault started, became observable and the fault occurred, adapted from [3].	10
Figure 2.6 : Star-connected stator winding faults, adapted from [4].	13
Figure 3.1 : Experiment setup, courtesy of WAT Motor Co.	19
Figure 3.2 : Typical induction motor label, courtesy of WAT Motor Co.	20
Figure 3.3 : Schematic of test system.	21

CONDITION MONITORING AND FAULT DIAGNOSIS OF VFD-FED INDUCTION MOTORS

SUMMARY

1 line spacing must be set for summaries. For theses in Turkish, the summary in Turkish must have 300 words minimum and span 1 to 3 pages, whereas the extended summary in English must span 3-5 pages.

For theses in English, the summary in English must have 300 words minimum and span 1-3 pages, whereas the extended summary in Turkish must span 3-5 pages.

A summary must briefly mention the subject of the thesis, the method(s) used and the conclusions derived. References, figures and tables must not be given in Summary.

Above the Summary, the thesis title in first level title format (i.e., 72 pt before and 18 pt after paragraph spacing, and 1 line spacing) must be placed. Below the title, the expression **ÖZET** (for summary in Turkish) and **SUMMARY** (for summary in English) must be written horizontally centered.

It is recommended that the summary in English is placed before the summary in Turkish.

DEĞİŞKEN FREKANSLI SÜRÜCÜ İLE BESLENEN ASENKRON MOTORLARDA DURUM İZLEME VE ARIZA TANILAMA

ÖZET

Özet hazırlanırken 1 satır boşluk bırakılır. Türkçe tezlerde, Türkçe özet 300 kelimedenden az olmamak kaydıyla 1-3 sayfa, İngilizce genişletilmiş özet de 3-5 sayfa arasında olmalıdır.

İngilizce tezlerde ise, İngilizce özet 300 kelimedenden az olmamak kaydıyla 1-3 sayfa, Türkçe genişletilmiş özet de 3-5 sayfa arasında olmalıdır.

Özetlerde tezde ele alınan konu kısaca tanıtılarak, kullanılan yöntemler ve ulaşılan sonuçlar belirtilir. Özetlerde kaynak, şekil, çizelge verilmez.

Özetlerin başında, birinci dereceden başlık formatında tezin adı (önce 72, sonra 18 punto aralık bırakılarak ve 1 satır aralıklı olarak) yazılacaktır. Başlığın altına büyük harflerle sayfa ortalanarak (Türkçe özet için) **ÖZET** ve (İngilizce özet için) **SUMMARY** yazılmalıdır.

Türkçe tezlerde Türkçe özetin İngilizce özetten önce olması önerilir.

1 line spacing must be set for summaries. For theses in Turkish, the summary in Turkish must have 300 words minimum and span 1 to 3 pages, whereas the extended summary in English must span 3-5 pages. For theses in English, the summary in English must have 300 words minimum and span 1-3 pages, whereas the extended summary in Turkish must span 3-5 pages. A summary must briefly mention the subject of the thesis, the method(s) used and the conclusions derived. References, figures and tables must not be given in Summary. Above the Summary, the thesis title in first level title format (i.e., 72 pt before and 18 pt after paragraph spacing, and 1 line spacing) must be placed. Below the title, the expression **ÖZET** (for summary in Turkish) and **SUMMARY** (for summary in English) must be written horizontally centered. It is recommended that the summary in English is placed before the summary in Turkish.

1. INTRODUCTION

1.1 Overview

Electric motors extensively employed in a system that converts electrical power into mechanical power in not only industrial applications but also residential, agricultural and transportation purposes. Taken together with systems they drive, electric motors use more than 40% of all electricity consumption and almost twice as much as the next largest user lighting [5]. Considering only industrial usage, electric motors dominate and account for close to 70% of the total electricity consumption [5,6].

There are many different motor types available in industrial facility operations, but asynchronous alternating current (AC) induction motors are the most preferred type because of their simple, reliable and rugged design. Relatively lost cost, low maintenance, high reliability and long lifespan are the most advantageous features of AC induction motors which drive core electro-mechanical systems such as material handling, material processing, pumping, ventilation and compressed air generation [7]. Especially HVAC (Heating, ventilation and air conditioning) sector requires special attention as they have the largest share of industrial electrical consumption and reasonably high saving potentials [7].

In recent years raised awareness about global warming demands more efficient systems including electric motor-driven systems. Policymakers such as the European Parliament and the European Council implementing new requirements to increase efficiency by encouraging the usage of high-efficiency premium motors and variable frequency drives (VFD) [6,8].

VFDs regulate the motor's output torque and speed to match the mechanical system loads and enables significant energy efficiency where variable mechanical power needed that have highly non-linear input power and output torque and speed such as pumps, fans and compressors. Previously Direct Current (DC) motors have

been dominant for variable motor speed control, yet developments in semiconductor technology became the driving force behind the prevalence usage of VFDs with AC motors [9]. Motor speed control is advantageous in terms of lower system energy costs, increased system reliability and less maintenance.

Considering 20-year in service, the power consumption of an electric motor depicts 90% of the total cost of ownership and followed by downtime costs as 5% and rebuild costs as 4% [5]. The initial purchase price represents only 1% of the total cost and it can be concluded that savings can be achieved by actions taken during operation of motor [5].

Industry 4.0 shaping industrial operations through automation and efficiency. Condition monitoring paves the way to Industry 4.0 through evaluating the state of the plant and/or equipment throughout its service life [2]. Maintenance can be defined as actions to retain or restore equipment in order to maintain its designed functions within the entire lifespan [2]. Traditional maintenance relies on periodically health checks to provide operability, but researches show that even if maintenance is done on time and correctly the vast majority of failures arises during operation state [10]. Condition monitoring and diagnostics can help to schedule maintenance to prevent such situations whilst avoiding unintended downtime and financial losses. Also, condition monitoring has the opportunity to build a database to understand better via trend analysis of the equipment or plant that leads more reliable system in the long run.

There are many condition monitoring methods available such as vibration, temperature, and current monitoring that can be used to assess insights into the health of equipment varying from bearings to electric motors and pumps. Current monitoring distinguishes itself from other methods since it is readily measured to control induction motor operation. VFDs are presenting a great potential to not only controlling the motor operation but also can be utilised as a connection to the Internet of Things structure to serve Industry 4.0.

1.2 Objectives of Research

This study aims to diagnose and identify mechanical and electrical faults of VFD-fed induction motors under various loads and speeds via monitoring only motor current.

As an outcome of this research comparative results among time-domain versus frequency-domain analysis and classical machine learning algorithms versus deep learning algorithms are presented. Also, these analyses investigated under single-fault and multiple-fault approaches.

The achievement of this study was facilitated by the following specific objectives:

- Analyse motor faults under VFD controlled motor current
- Investigate effects of various loads and speeds
- Build different feature engineering methods
- Benchmark Classical ML and Deep Learning algorithms
- Investigate single-fault scenarios and multiple-fault scenario

1.3 Organization of Thesis

Thesis organised in five chapters to achieve aforementioned objectives;

- Chapter-2 provides an in-depth background to condition monitoring and fault diagnosis of AC induction motors including general information about induction motors, fault types, condition monitoring and signal processing techniques followed by fault diagnosis methods.
- Chapter-3 presents the experimental testing system and used methodology.
- Chapter-4 discusses the diagnostics of faults via two different approaches: component-based and motor-based condition monitoring.
- Chapter-5 remarks obtained results with different approaches and concludes with future recommendations.

2. CONDITION MONITORING OF INDUCTION MOTORS: BACKGROUND

2.1 Introduction of Induction Motors

2.1.1 Principle of operation

Electric motors are divided into two classes depending on their power supply type: direct current (DC) or alternating current (AC). The latter can be broken into two classes as synchronous or induction according to their operating speed. Induction motors, which operates slightly lower than synchronous speed, are also sub-divided as wounded and squirrel-cage motors. In this study, squirrel-cage induction motors have been investigated by means of induction motors, since the squirrel-cage type is predominantly used in industrial applications.

Induction motors run at a speed slightly lower than synchronous speed at the point where motor torque and load torque are equal [11]. The difference between the actual speed and synchronous speed is known as slip [9].

$$\text{Synchronous Speed} = \frac{120 \cdot \text{Frequency (Hz)}}{\text{number of poles}} \quad (2.1)$$

$$\text{Slip} = \frac{\text{Synchronous Speed} - \text{Rotor's Mechanical Speed}}{\text{Synchronous Speed}} \quad (2.2)$$

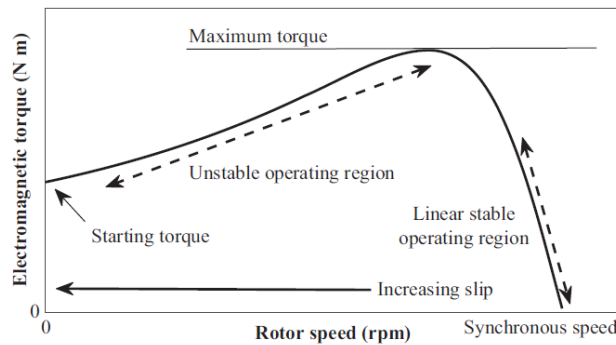


Figure 2.1 : Steady-state torque-speed curve of an induction motor, adapted from [1].

In Principle, induction motors transfer electrical energy into mechanical energy by interlinking two electrical components: stator as stationary part and rotor as rotational part. Electrical energy transmitted from stator to rotor via electromagnetic induction, then a mechanical component bearing guides rotor to provide mechanical power [4, 12].

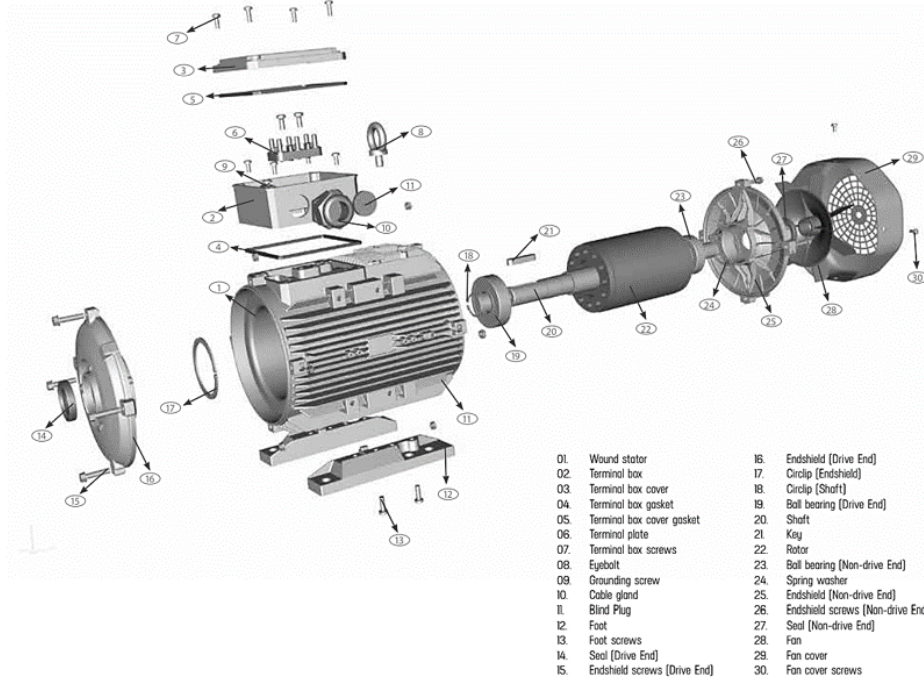


Figure 2.2 : Squirrel cage induction motor structure, courtesy of WAT Motor Co.

2.1.2 VFD-fed induction motors

A variable frequency drive, also called as adjustable-frequency drive (AFD), variable-speed drive (VSD) or inverter, fed motor system controls the rotation speed of the induction motor by controlling the supply frequency and voltage of the motor. The main difference between line-start and VFD-fed induction motors is that while in line-start mode supply voltage is the only controllable parameter, on the other hand, VFD-fed has the ability to control torque and speed easily [1].

From a historical point of view, DC motors have been utilised in speed control applications. However, as a result of advances in power semiconductor technology used in inverters, the performance of AC motors in terms of precision, response, and speed range began to exceed that of DC motors [8, 9]. As a driving force behind the induction motor control dominance today, VFDs generally have the following control strategies regarding speed and torque regulation [13, 14]:

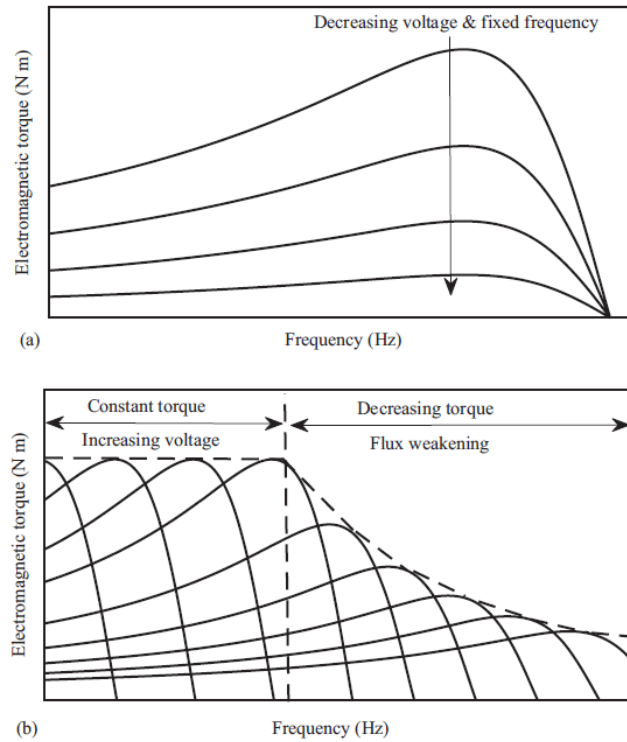


Figure 2.3 : (a) Torque–speed curves for different voltages in line-start operation and (b) Torque–speed curves for different voltages and frequencies in VFD-fed operation, adapted from [1].

- Voltage per Frequency Control (V/f)
- Field Oriented Control (FOC)
- Direct Torque Control (DTC)

The common idea behind these methods is based on controlling the torque and flux references applied to the motor separately, as in DC motor control [1]. In the scope of this thesis, only the V/f control strategy emphasized due to the widespread adoption of the control method in pump, compressor and fan applications.

V/f control can be employed in both open-loop and closed-loop modes. Open-loop V/f control, which is by far the most popular control due to its simplicity, as the name implies, creates a constant air-gap flux by keeping the ratio between the voltage and frequency applied to the induction motor constant, and as a result, it provides the opportunity to work at operating frequencies from zero to nominal frequency [15].

VFDs come with benefits such that energy savings, reliability and product quality, yet in concern of fault diagnosis they introduce a number of factors, which will be discussed later on, that increase the complexity.

2.1.3 Need for condition monitoring

Condition monitoring defined as measuring activities concerning characteristics and parameters of physical equipment at predetermined intervals either manually or automatically [2]. Leveraging rapid technological advancements in data storage, data process and network structure, condition monitoring became one of the driving force behind the industry 4.0 paradigm. The key goal behind this paradigm is to acquisition, transmission and analysis of data in order to predict future behaviours of machinery, or plant on a larger scale, to boost efficiency and reliability [16, 17].

Researchers from both academia and industry have devoted significant attention to condition monitoring of induction motors over decades. Even though induction motors renowned for robustness, environmental, electrical and mechanical effects may lead induction motors to failure. As a result, industrial processes subjected to potential losses in a manner of time and capital, so the desire to minimize or even prevent these losses emerges the need for condition monitoring.

2.1.4 Maintenance strategies

Maintenance can be defined as the combination of all technical and administrative actions taken to maintain or restore an item throughout its life cycle in a condition where it can fulfil its designed function [2]. A motor maintenance program should effectively address reliability, cost, and scheduling issues, as well as the causes of the most common motor failures. Essentially, there are two types of maintenance strategies: corrective and preventive.

Corrective maintenance is a type of maintenance performed after the induction motor failure to detect the fault and restore it to operational condition [2]. The main purpose of this type of maintenance is to get the equipment up and running as soon as possible by repairing or replacing the defective equipment. However, corrective maintenance as a failure-driven method contains a high-risk potential as faults may occur at unexpected times, can disrupt the operation. Since this type of maintenance approach does not take

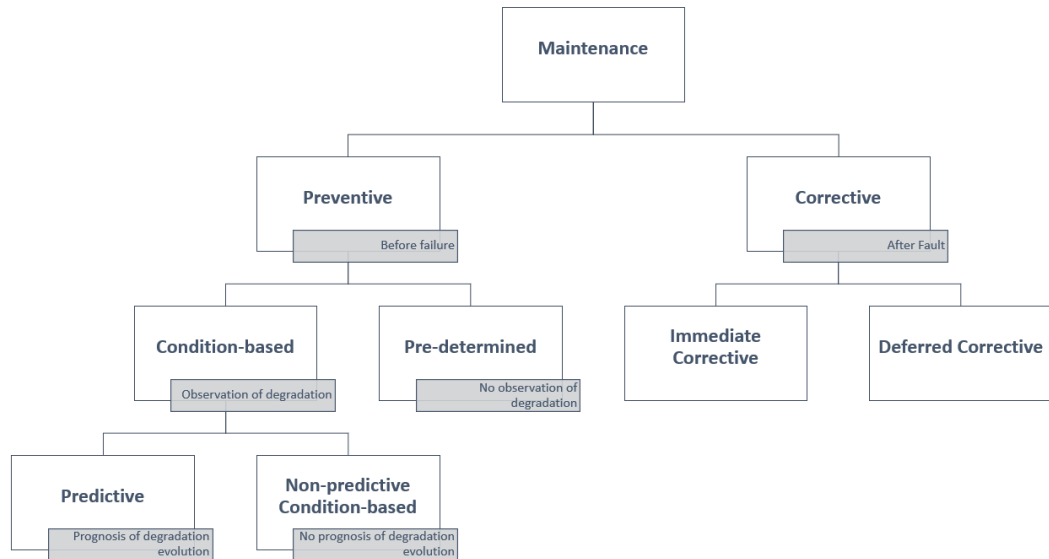


Figure 2.4 : Maintenance types, adapted from [2].

into account the damages that may occur, it may be suitable for equipment that is not critical to the business that does not pose a safety risk.

Preventive maintenance, on the other hand, aims to detect faults at an early stage and correct them before they introduce risk to operation [2]. Preventive maintenance employed to increase efficiency and reliability by taking into account the probability of failure or the ageing of the equipment, at certain intervals or according to pre-planned scheduling. Although this approach is beneficial in cases where the wear-out characteristics are evident, it has disadvantages, especially in terms of not being able to use equipment lifespan efficiently and increasing the maintenance cost compared to the corrective maintenance approach [18].

Predictive maintenance is a condition-based approach to maintenance that is used to evaluate the parameters and characteristics of the equipment or to make predictions based on repeated analysis [2]. Compared to preventive maintenance, predictive maintenance maximizes equipment service-life whilst minimizing unnecessary maintenance. In 99% of machine failures, it is possible to observe indications that malfunctions will occur, in other words, the necessary measures can be taken before 99% of the faults occur by continuously monitoring the machine [18].

Under the predictive maintenance approach, decision-making can be divided into two: diagnosis, which is the analysis of the current situation, and prognosis, which is the

assessment of conditions measured over time [3]. A P-F curve can be used to better understand diagnostic and prognostic monitoring systems.

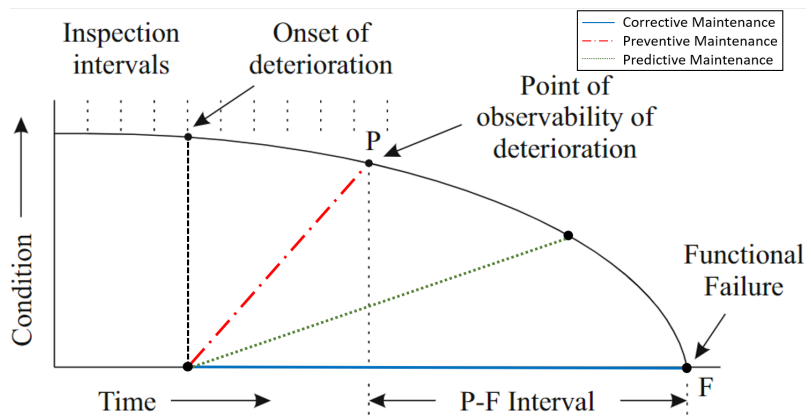


Figure 2.5 : The P-F curve shows the point where the fault started, became observable and the fault occurred, adapted from [3].

The downside of predictive maintenance is that it requires additional equipment and relatively high investment costs. But the advantage of VFDs also comes out here. As they currently monitor motor parameters in control applications, they have a high potential for predictive maintenance applications without the need for additional sensors and investments.

2.2 Induction Motor Fault Types

From a mechanical perspective, induction machines basically consist of three components: stator, rotor and bearing. Electrical, mechanical, and environmental disturbances constantly affect asynchronous motor components and cause most malfunctions [19]. Table 2.1 exhibits various surveys that studied and categorized the most common failures [10,20–23].

Table 2.1 : Table with single row and centered columns.

Component	IEEE	EPRI	Thorsen-Dalva	Bonnett-Yung
Bearing	44	41	51	69
Stator	26	37	16	21
Rotor	8	10	5	7
Other	22	12	28	3

As can be seen in Table 2.1, most of the faults associated with bearings followed by stator related faults. It also should be noted that these surveys do not include the effects of power electronics. A motor controlled by VFD is subjected to short and high voltage

pulses called PWM (Pulse Width Modulation), which are sent at a very high frequency, which can have a detrimental effect on the wire insulation and cause a burn on the stator [11]. Although this problem can be solved with high-quality insulation, PWM signals also create non-continuous electrical discharges on the bearings, causing wear which reduces bearing lifespan [24]. Therefore, it would not be wrong to conclude that bearing and stator failures will also have a high rate in VFD-fed induction motors.

2.2.1 Bearing related faults

In all kinds of electrical machines, the mechanical element positioned between the frame that initiates the movement and the rotating axis shaft is called a bearing. These mechanical elements, which help the rotational movement of the electric motor, are exposed to many internal and external destructive effects during their operation and failures arise as a result. Major sources of bearing failures are given below [19,25–29]:

Mechanical stresses: Fatigue, which mostly begins on the surface, turns into small-sized material ruptures at the beginning and later dimensional surface indentations and protrusions. Loose motor connection, misalignment where the motor shaft and load shaft are connected without aligning on the same axis, angular misalignment where the motor shaft and load shaft axes are connected at a certain angle, and unbalanced load connection, which is an unbalance condition where the centre of gravity of the load connected to the motor shaft is not on the rotation axis are other mechanical disturbances on the bearing.

Environmental stresses: Corrosion occurs on the bearing surfaces used in high humidity working environments. Especially the moisture absorbed in the bearing oil initiates this process and the rust that occurs due to corrosion causes deterioration that turns into indentation and protrusion on the surface of the bearing element, and cracks in the later stages.

Thermal stresses: Insufficient lubrication generally causes problems with bearing components. Normally, there is a layer of oil in the bearing that prevents direct contact between the rotating elements so that their surfaces do not wear out quickly. In case of insufficient lubrication, excessive wear and subsequent material deterioration occur as a result of increased friction due to direct contact between metal surfaces.

Electrical stresses: the electrical discharge current effect occurs with a fault current flowing through the bearings from the motor frame to the ground in motors that do not have a suitable ground connection. Asymmetry of stator windings, permanent magnetism effect developing in the motor over time, electrostatic charge accumulation in the motor frame and application of voltage to the motor shaft from the outside, or common end voltages generated due to the high switching frequency of semiconductor power electronics (VFDs using PWM) are the factors that cause this malfunction. The irregular current will cause wear and tear on the bearing metal surface, and as a result, the degree of material rupture and surface deterioration increases.

Vibration in the motor causes the rotor to rotate irregularly or axially unbalanced in the motor air gap. Any axial misalignment that occurs in the motor air gap adversely affects the air gap flux density and causes the formation of harmonic components [1, 28, 29]. Consequently, this can induce harmonic components in the current drawn by the motor with frequencies given by formula [28]:

$$f_{bng} = f_e \pm m \cdot f_v \quad (2.3)$$

where,

f_e is the electrical supply frequency;

f_v is the rotational speed frequency of the rotor;

m is the harmonic number 1, 2, 3, ...;

f_{bng} is the current component frequency due to air gap changes.

2.2.2 Stator related faults

As researches have shown, stator faults occupy an important place among asynchronous motor faults after bearing [10, 20–23]. Mechanical, electrical, thermal and environmental factors cause malfunctions in the stator windings, as well as their laminations [4, 30]. Winding faults, as the most common stator faults, are winding short-circuit faults that are mostly the result of the aforementioned effects of the winding insulation. Types of winding faults are as follows [4, 30, 31]:

- Short-circuit between two turns in the same phase, (turn-turn failure)
- Short-circuit between two coils side by side in the same phase (coil-coil failure),

- Short-circuit between the turns of two phases (phase-phase failure),
- Short circuit consisting of all three-phase turns,
- Short-circuit between the conductor of the winding and the stator core (phase-ground short circuit),
- Open-circuit fault when winding gets break.

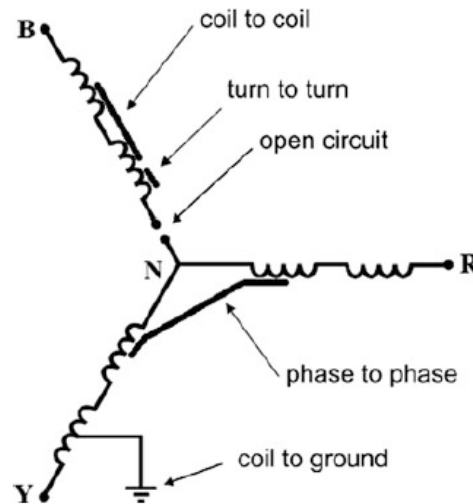


Figure 2.6 : Star-connected stator winding faults, adapted from [4].

The factors that cause the motor winding insulation to deteriorate are explained below [1,4,30,32]:

Mechanical stresses: While the motor is running, the rotor may rub or hit the inner surface of the stator due to motor shaft deterioration, bearing failures and misalignment. This force creates a turn-to-turn or a phase-to-earth short-circuit, causing the stator coil and the stator winding insulation to break down. On the other hand, winding breakage may occur due to vibration during operation and therefore the motor produces the open-circuit fault.

Environmental stresses: The environment in which the motor is running can be very hot, cold or humid. On the other hand, substances in the external environment can contaminate the windings, causing the heat dissipation to deteriorate and the insulation to be damaged. In addition, the airflow can be blocked and cannot absorb the air required for cooling. Therefore, it causes the motor windings to heat and consequently the insulation to deteriorate.

Thermal stresses: Thermal effects occur as a result of overloading or a motor failure. With motor overload, the motor temperature rises above the limit value of the insulation class and the insulation deteriorates. At this point, every 3.5% unbalance in the motor supply voltage increases the temperature of the motor by 10°C. In addition, every 10°C temperature increase above the limit temperature value of the insulation halves the life of the insulation.

Electrical stresses: The main reason for this is sudden changes in supply voltage. Transients during commissioning and decommissioning and voltage fluctuations frequently occur, especially in asynchronous motors powered by variable frequency drives. Winding insulations deteriorate due to these voltage variations.

Under the inter-turn short-circuit condition, a significant deviation in rotor slot harmonics components, called as principle slot harmonics (PSH), occurs and can be obtained by given formula [33];

$$f_{st} = f_e \cdot \left[n \cdot \frac{(1-s)}{p} \pm k \right] \quad (2.4)$$

where,

f_e is the electrical supply frequency ;

p is the number of pole pairs of the motor ;

$n = 1, 2, 3 \dots (2p - 1)$;

s is the slip ;

k is the harmonic number 1, 2, 3,;

f_{st} is the principle slot harmonic frequencies.

2.2.3 Rotor related faults

There are several reasons why rotor bar faults can occur in an induction motor. In caged motors, breaking one cage bar does not significantly change the operating behaviour of the machine. However, due to the fracture that occurs, the current distribution, air gap flux, force balance and temperature distribution in the rotor deteriorate, and heating and strains increase [34]. If the rotor continues to run in this state, damage can also spread to the sidebars, causing multiple bars of the rotor to break. In this respect, it is very important to diagnose the condition when a rotor bar broken.

The main reasons of rotor broken bar of an induction motor can be mentioned as follows [30, 32, 34, 35];

Mechanical stresses: In cases that cause structural asymmetry such as rotor misalignment or bearing failure, the resultant of the normal direction forces in the air gap is not equal to zero and the force acting on the bars increases. In addition, dynamic effects such as impact forces due to sudden load change, centrifugal forces due to excessive acceleration also cause failure.

Environmental stresses: Dusty, wet and/or oily environment in which the electric motor operates negatively affects the engine and increases the possibility of malfunction.

Thermal stresses: Thermal stresses may occur during take-off and/or operation. The temperature limit values of the motor and rotor are different. In terms of the safe operation of the motor, the rotor temperature at start-up and the stator temperature during operation are decisive. Thermal stresses are generally caused by frequent starting, locking of the motor shaft, bearing failure, insufficient cooling, skin effect and current accumulation. It takes the form of partial warming in machines fed by power electronics.

Electrical stresses: The flux created by the current flowing through the rotor bars creates an electrodynamic force ($F \propto I^2$) acting from the rotor surface towards the shaft in quadratic proportion to the current. The bar vibrates at $2 \cdot s \cdot f_e$ and $4 \cdot s \cdot f_e$ frequencies and can therefore cause breakage in the rotor bars. In addition, since the rotor current at motor start-up is very high, the rotor bar is again exposed to high stresses.

Cracked or broken bar in the rotor cage produces a series of sideband frequencies in the stator current given by [4];

$$f_{brb} = f_e \cdot [1 \pm 2 \cdot k \cdot s] \quad (2.5)$$

where,

f_e is the electrical supply frequency ;

s is the slip ;

k is the harmonic number $1, 2, 3, \dots$;

f_{brb} is the broken rotor bar sideband frequencies.

2.3 Condition Monitoring Techniques

Condition monitoring is applied to the motor continuously or periodically, as a diagnostic tool for fault detection and as one of the fundamentals of maintenance planning. Sudden or unexpected changes in monitored parameters provide important information about the condition of the motor. Although the parameters to be monitored vary depending on the end-user, temperature, vibration and current magnitudes are widely used in the industry [36].

2.3.1 Temperature monitoring

One of the parameters that can be followed in order for electric motors to work safely and without failure for a long time is the motor temperature. By installing sensors such as Resistance Temperature Detectors, thermistors, thermocouples and thermostats, electrical or mechanical faults can be detected [36]. These sensors are usually placed in the stator windings, bearings and frame [37]. In addition, temperature monitoring can be performed by parameter estimation over the stator supply current without using any temperature sensor [38].

As mentioned before, thermal stresses resulting from effects such as overloading and bearing lubrication problems may damage various components of the motor. While bearing temperatures provide useful information about possible friction problems, the coolant bulk outlet temperature is frequently monitored, especially when the machine is forced beyond its nominal values, and winding temperature monitoring is also useful in the event of overheating due to overload [39]. Continuously monitoring of temperature will give an indication of potential failures to avoid catastrophic incidents.

2.3.2 Vibration monitoring

Due to their working principles, rotating gears, electric fields and shafts periodically generate vibrations [40]. Since the produced vibration signals contain information about the condition of the machine and can be followed without interfering with the operation of the motor, it is mostly preferred in condition monitoring studies. Vibration

monitoring has the ability to track sudden changes in the machine condition that enables monitor the condition of the equipment continuously or intermittently.

Vibration can be measured in units of displacement, velocity, and acceleration. The displacement type is generally used in the measurement of rotor vibration, while the velocity type is used in motor housing vibration measurements associated with machine fatigue [36]. With the most commonly used acceleration type, the vibration condition is monitored by positioning it close to a bearing on the motor frame at high frequencies [36,41].

Vibration analysis is used in many studies on mechanical failures also occurring in induction motors. Imbalance, misalignment, looseness, and bearing failures are specific signs in the vibration spectrum [39]. A condition monitoring strategy can be established by correlating certain fault types with specific frequencies, or by trend analysis with acceleration data. Depending on the application and user requirements, with vibration condition monitoring, a cost-effective maintenance plan can diagnose and take action before the machine and its components fail or cause performance loss.

2.3.3 Motor current monitoring

Condition monitoring via supply current signals provide useful information on not only for motor itself but also the mechanical system that motor drive [42]. An important aspect of the maintenance strategy is the inclusion of a mechanical system that motor drive. Especially with VFD-fed systems, where current is already sensed to control motor operation, both electrical and mechanical faults can be diagnosed without additional sensor need [29,42–44].

In industrial applications where ambient conditions are not suitable for vibration signal measurement, current monitoring may be preferred due to its robustness to ambient conditions, especially when disturbances are high. Therefore, current-based condition monitoring, which proven in industrial applications, has benefits such as economical, versatile and reliable over other monitoring techniques.

Although many studies have been done to diagnose fault using current signals, studies on VFD-fed motors are limited. It should be noted that the PWM signals used in VFDs can mask the characteristics of a fault in the motor current signal, making diagnosis difficult [45]. In this study, electrical and mechanical fault detection is emphasized in

different load and frequency scenarios over the single-phase stator supply current of the VFD-fed three-phased induction motor.

3. EXPERIMENTAL SETUP AND METHODOLOGY

This chapter is devoted to explaining the experimental setup and the data obtained for the condition monitoring and diagnostics of the induction motor. Experiments were carried out in the General Purpose Industrial Motor Laboratory at WAT Motor Company facilities. During the studies, the faults related to the bearing, stator and rotor of the squirrel-cage induction motor were artificially created and their data were collected. The test system used in the study is shown in Figure 3.1.



Figure 3.1 : Experiment setup, courtesy of WAT Motor Co.

Table 3.1 : Equipments used in experimental-setup.

Equipment
Kistler 200 kW Dynamometer
Yokogawa Power Analyzer
Teledyne LeCroy Oscilloscope
WAT-11 kW Induction Motors
WAT-WF-80 General Purpose Variable Frequency Driver

In the experimental studies, the stability of the system was monitored by monitoring the three-phase current and voltage signals on the power analyzer. One phase of the stator supply current of the motor was recorded with a current probe at a sampling frequency of 5 kHz for 10 seconds. In addition, the load torque acting on the motor and the rotor rotation speed of the motor were measured via the dynamometer system.

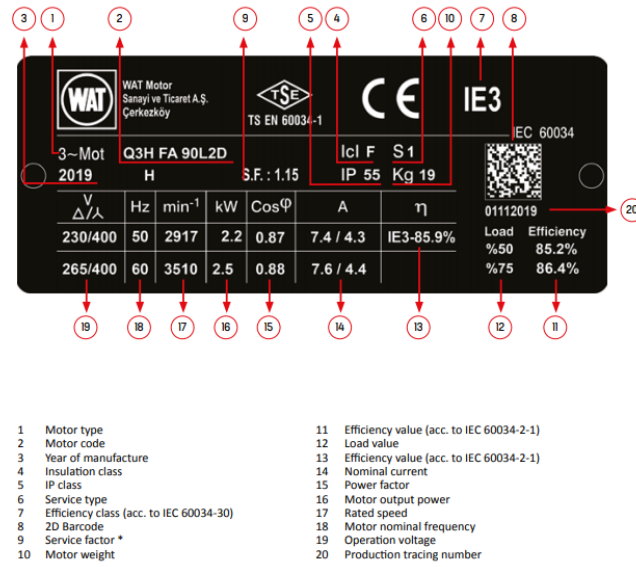


Figure 3.2 : Typical induction motor label, courtesy of WAT Motor Co.

Table 3.2 : Nominal Values of WAT Motor 3-phase Induction Motor.

Voltage (V)	Power		Speed (<i>rpm</i>)	Current (A)	Torque (<i>N · m</i>)
	(<i>kW</i>)	(<i>Hz</i>)			
400/690	11	50	1475	22.0/12.7	71.3

Experimental studies were carried out at a rated load of 72 Nm and a frequency of 30, 35, 40, 45 and 50 Hz at 54 Nm, which is 75% of the rated load, by applying the v/f control method over the VFD. Three motors produced in the same series on the same production line were taken and their data were collected in "healthy" condition under the mentioned conditions. For bearing failure, a fault was artificially created after hammering the drive-end bearing of one of the motors, while for stator failure, the insulation between the two turns in one phase of another motor was eroded. For the last motor, one of the bars in the rotor cage has been drilled for rotor failure. It should also be noted that studies conducted only for two cases in steady-state conditions for the motor as healthy and faulty.

Table 3.3 : Table with single row and centered columns.

Fault Type	Frequency (<i>Hz</i>)	Load (<i>N · m</i>)
Bering	30	≈ 72
Stator turn-turn	35	≈ 54
Broken Rotor Bar	40	
	45	
	50	

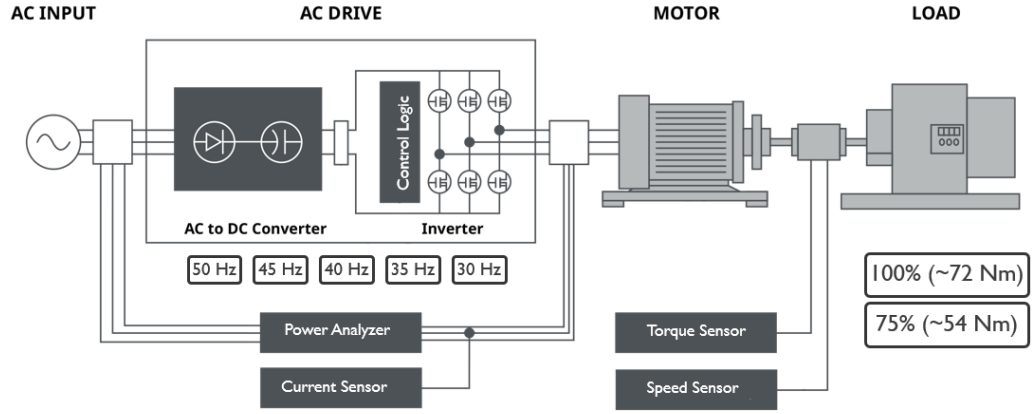


Figure 3.3 : Schematic of test system.

Another issue to be considered while collecting data is the amount of data required to see the effects of failure. In the experiments, the mechanical speed of the rotor varies between 857 and 1472 rpm according to the reference control command applied. According to the given in equation 3.1 [46], approximately 200 data points are taken per revolution of the rotor shaft with 5 kHz sampling frequency and sampling time of 10 seconds, a window width of 50,000 data points, fault impacts expected to be easily captured.

$$\text{Number of Data Points} = \frac{60 \cdot \text{Sampling Frequency (Hz)}}{\text{Rotor's Mechanical Speed}} \quad (3.1)$$

REFERENCES

- [1] **Faiz, J., Joksimović, G. and Ghorbanian, V.** (2017). *Fault diagnosis of induction motors*, Institution of Engineering & Technology.
- [2] **EN, B.** (2017). 13306:2017: Maintenance—Maintenance terminology, *BSI Standards Publication*.
- [3] **Tinga, T. and Loendersloot, R.,** (2019). Physical model-based prognostics and health monitoring to enable predictive maintenance, *Predictive Maintenance in Dynamic Systems*, Springer, pp.313–353.
- [4] **Karmakar, S., Chattopadhyay, S., Mitra, M. and Sengupta, S.** *Induction motor fault diagnosis*, volume 25, Springer.
- [5] **Waide, P. and Brunner, C.U.** (2011). Energy-efficiency policy opportunities for electric motor-driven systems.
- [6] **Kulterer, K., Werle, R., Lackner, P., Brunner, C. and Ellis, M.** (2014). Policy Guidelines for Electric Motor Systems–Part 2: Toolkit for Policy Makers, *4E Electric Motor Systems EMSA, 4E Energy Efficient Enduse Equipment, International Energy Agency*.
- [7] **Fleiter, T. and Eichhammer, W.** (2012). Energy efficiency in electric motor systems : Technology , saving potentials and policy options for developing countries.
- [8] **Mikami, H., Ide, K., Shimizu, Y., Senoo, M. and Seki, H.** (2011). Historical evolution of motor technology, *Hitachi Review*, 60(1), 39.
- [9] (2014). Improving Motor and Drive System Performance – A Sourcebook for Industry, <https://www.osti.gov/biblio/1220836>.
- [10] (1985). Report of Large Motor Reliability Survey of Industrial and Commercial Installations, Part I, *IEEE Transactions on Industry Applications*, IA-21(4), 853–864.
- [11] **Hovstadius, G. and Bolles, S.** (2016). Manual for Industrial Pump Systems Assessment and Optimization, **Technical Report**, United Nations Industrial Development Organization.
- [12] **Oliver, J.** (1992). Electric motor predictive and preventive maintenance guide, **Technical Report**, Electric Power Research Inst.
- [13] **Motors, W.E.** (2018). Induction motors fed by PWM frequency inverters, **Technical Report**, <https://www.weg.net/institutional/US/en/search/downloadcenter>.

- [14] **Drives, D.** (2019). Facts Worth Knowing about AC Drives, **Technical Report**, <https://danfoss.ipapercms.dk/Drives/DD/Global/SalesPromotion/FWK>.
- [15] **Bose, B.** (2002). *Modern Power Electronics and AC Drives*, Eastern Economy Edition, Prentice Hall PTR.
- [16] **Lughofer, E. and Sayed-Mouchaweh, M.**, (2019). Prologue: Predictive maintenance in dynamic systems, *Predictive Maintenance in Dynamic Systems*, Springer, pp.1–23.
- [17] **Ruiz-Sarmiento, J.R., Monroy, J., Moreno, F.A., Galindo, C., Bonelo, J.M. and Gonzalez-Jimenez, J.** (2020). A predictive model for the maintenance of industrial machinery in the context of industry 4.0, *Engineering Applications of Artificial Intelligence*, 87, 103289.
- [18] **Ahmad, R. and Kamaruddin, S.** (2012). An overview of time-based and condition-based maintenance in industrial application, *Computers & Industrial Engineering*, 63(1), 135–149.
- [19] **Bonnett, A.H.** (2010). Root cause failure analysis for AC Induction Motors in the petroleum and chemical industry, *2010 Record of Conference Papers Industry Applications Society 57th Annual Petroleum and Chemical Industry Conference (PCIC)*, pp.1–13.
- [20] **Albrecht, P., Appiarius, J., McCoy, R., Owen, E. and Sharma, D.** (1986). Assessment of the reliability of motors in utility applications-Updated, *IEEE Transactions on Energy conversion*, (1), 39–46.
- [21] **Albrecht, P., Appiarius, J., Cornell, E., Houghtaling, D., McCoy, R., Owen, E. and Sharma, D.** (1987). Assessment of the reliability of motors in utility applications, *IEEE transactions on energy conversion*, (3), 396–406.
- [22] **Thorsen, O.V. and Dalva, M.** (1995). A survey of faults on induction motors in offshore oil industry, petrochemical industry, gas terminals, and oil refineries, *IEEE transactions on industry applications*, 31(5), 1186–1196.
- [23] **Bonnett, A.H. and Yung, C.** (2008). Increased efficiency versus increased reliability, *IEEE Industry Applications Magazine*, 14(1), 29–36.
- [24] **Trigeassou, J.C.** (2013). *Electrical machines diagnosis*, John Wiley & Sons.
- [25] **Zhang, P., Du, Y., Habetler, T.G. and Lu, B.** (2010). A survey of condition monitoring and protection methods for medium-voltage induction motors, *IEEE Transactions on Industry Applications*, 47(1), 34–46.
- [26] **Bonnet, A.H.** (2012). The Cause and Analysis of Bearing and Shaft Failures in Electric Motors, **Technical Manual 27**, EASA Technology & Education Consultant.

- [27] (2017). Bearing damage and failure analysis, **Technical Manual PUB BU/I3 14219/2 EN**, SKF Group.
- [28] **Schoen, R.R., Habetler, T.G., Kamran, F. and Bartfield, R.** (1995). Motor bearing damage detection using stator current monitoring, *IEEE transactions on industry applications*, 31(6), 1274–1279.
- [29] **EN, B.** (2013). 20958:2013: Condition monitoring and diagnostics of machine systems — Electrical signature analysis of three-phase induction motors, *BSI Standards Publication*.
- [30] **Siddique, A., Yadava, G. and Singh, B.** (2005). A review of stator fault monitoring techniques of induction motors, *IEEE Transactions on Energy Conversion*, 20(1), 106–114.
- [31] **Lipo, T.A.** (2017). *Introduction to AC Machine Design*, John Wiley & Sons, Ltd.
- [32] **Bonnett, A.H.** (1999). Root cause AC motor failure analysis, *Industry Applications Society 46th Annual Petroleum and Chemical Technical Conference (Cat. No. 99CH37000)*, IEEE, pp.85–97.
- [33] **Penman, J., Sedding, H., Lloyd, B. and Fink, W.** (1994). Detection and location of interturn short circuits in the stator windings of operating motors, *IEEE Transactions on Energy Conversion*, 9(4), 652–658.
- [34] **İmeryüz, M.** (2009). Asenkron Makinede Kafes Kırılmasının İncelenmesi, *Ph.D. Dissertation*, Fen Bilimleri Enstitüsü.
- [35] **Filippetti, F., Bellini, A. and Capolino, G.A.** (2013). Condition monitoring and diagnosis of rotor faults in induction machines: State of art and future perspectives, *2013 IEEE Workshop on Electrical Machines Design, Control and Diagnosis (WEMDCD)*, IEEE, pp.196–209.
- [36] **Mistry, R., Finley, W.R., Hashish, E. and Kreitzer, S.** (2016). Rotating machines—Pros and cons of monitoring devices, *2016 Petroleum and Chemical Industry Technical Conference (PCIC)*, IEEE, pp.1–12.
- [37] **Society, I.P.E.** (2017). IEEE standard test procedure for polyphase induction motors and generators, *ANSI, IEEE Standard 112*.
- [38] **Kumar, S., Mukherjee, D., Guchhait, P.K., Banerjee, R., Srivastava, A.K., Vishwakarma, D. and Saket, R.** (2019). A comprehensive review of condition based prognostic maintenance (CBPM) for induction motor, *Ieee Access*, 7, 90690–90704.
- [39] **Thorsen, O. and Dalva, M.** (1998). Methods of condition monitoring and fault diagnosis for induction motors, *European transactions on electrical power*, 8(5), 383–395.
- [40] **Randall, R.B.** (2021). *Vibration-based condition monitoring: industrial, automotive and aerospace applications*, John Wiley & Sons.

- [41] **EN, I.** (2002). 13373-1:2002: Condition monitoring and diagnostics of machines — Vibration condition monitoring — Part 1: General procedures, *International Organization for Standardization*.
- [42] **Thomson, W.T. and Fenger, M.** (2001). Current signature analysis to detect induction motor faults, *IEEE Industry Applications Magazine*, 7(4), 26–34.
- [43] **Gritli, Y., Bellini, A., Rossi, C., Casadei, D., Filippetti, F. and Capolino, G.** (2017). Condition monitoring of mechanical faults in induction machines from electrical signatures: Review of different techniques, *2017 IEEE 11th international symposium on diagnostics for electrical machines, power electronics and drives (SDEMPED)*, IEEE, pp.77–84.
- [44] **Corne, B., Knockaert, J. and Desmet, J.** (2017). Misalignment and unbalance fault severity estimation using stator current measurements, *2017 IEEE 11th International Symposium on Diagnostics for Electrical Machines, Power Electronics and Drives (SDEMPED)*, IEEE, pp.247–253.
- [45] **Shaeboub, A.** (2018). The Monitoring of Induction Machines Using Electrical Signals from the Variable Speed Drive, *Ph.D. Dissertation*, University of Huddersfield.
- [46] **Shenfield, A. and Howarth, M.** (2020). A novel deep learning model for the detection and identification of rolling element-bearing faults, *Sensors*, 20(18), 5112.

APPENDICES

CURRICULUM VITAE

PHOTO

Name Surname :

Place and Date of Birth :

E-Mail :

EDUCATION :

- **B.Sc.** : Graduation year, Istanbul Technical University, Faculty of Electrical and Electronics, Department of Electrical Engineering
- **M.Sc. (If exists)** : Graduation year, Istanbul Technical University, Faculty of Electrical and Electronics, Department of Electrical Engineering

PROFESSIONAL EXPERIENCE AND REWARDS:

- 1950-1956 Istanbul Technical University at the Central Laboratory of Theoretical Physics.
- 1953 Nobel Prize for Physics
- 1956 Completed Doctorate at Istanbul Technical University

PUBLICATIONS, PRESENTATIONS AND PATENTS ON THE THESIS:

- **Ganapuram S., Hamidov A., Demirel, M. C., Bozkurt E., Kindap U., Newton A.** 2007. Erasmus Mundus Scholar's Perspective On Water And Coastal Management Education In Europe. *International Congress - River Basin Management*, March 22–24, 2007 Antalya, Turkey. (Presentation Instance)
- **Satoğlu, Ş.I., Durmuşoğlu, M. B., Ertay, T. A.** 2010. A Mathematical Model And A Heuristic Approach For Design Of The Hybrid Manufacturing Systems To Facilitate One-Piece Flow, *International Journal of Production Research*, 48(17), 5195–5220. (Article Instance)

- **Chen, Z.** 2013. Intelligent Digital Teaching And Learning All-In-One Machine, Has Projection Mechanism Whose Front End Is Connected With Supporting Arm, And Base Shell Provided With Panoramic Camera That Is Connected With Projector. Patent numarası: CN203102627-U. (Patent Instance)

OTHER PUBLICATIONS, PRESENTATIONS AND PATENTS:

F. M. SURNAME	CONDITION MONITORING AND FAULT DIAGNOSIS OF VFD-FED INDUCTION MOTORS	2020
---------------	--	------