Dynamics, Simulation and Control of Quadcopters

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Outline

- Introduction
- Quadcopter Dynamics
- References



Introduction

- Quadcopter Dynamics
 - Definitions
 - Kinematics

Reference



- ▶ Copters are flying vehicles which use rapidly spinning rotors make themselves aloft.
- Conventional copters have two rotors
- ▶ There are two ways that rotors can be arranged:
 - As two coplanar rotors, spinning in opposite directions.
 - Description One main rotor providing thrust and a smaller side rotor oriented laterally
- The design of copters comes with a control and swashplate mechanism complication.
- The swashplate mechanism was needed to allow the copter to utilize more degrees of freedom.



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Definitions

Degrees of Freedom (DOF)

DOF of a mechanical system is the number of independent parameters that define its configuration.



- ▶ A quadcopter(quadrotor) is a copter which has four equally spaced rotors.
- With four independent rotors, the need for a swashplate mechanism is alleviated
- Quadcopters can obtain copters's degrees of freedom by having two more rotors instead of swashplate.
- Quadcopter control is a fundamentally difficult and interesting problem due to six DOF and only four independent inputs.
- ▶ In order to achieve six DOF, rotational and translational motion are coupled





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Introduction

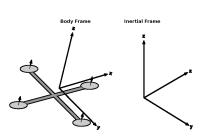
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The Body and Inertial Frame

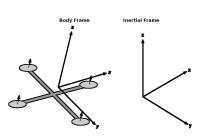
- ▶ The inertial frame is defined by the ground, with gravity pointing in the negative z direction.
- ▶ The body frame is defined by the orientation of the quadcopter, with the rotor axes pointing in the positive z direction and the arms pointing in the x and y directions.





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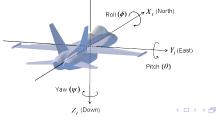
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Roll, Pitch and Yaw degrees

- ▶ The roll axis (or longitudinal axis) passes through the plane from nose to tail alongside of x axis.
- The pitch axis (also called lateral or transverse axis) passes through the plane from wingtip to wingtip alongside of y axis.
- ► The vertical **yaw axis** is defined to be perpendicular to the wings with its origin at the center of gravity and directed towards the bottom of the aircraft alongside of *z* axis.



- Position and velocity of the quadcopter in the inertial frame are defined as $p=(x,y,z)^T$ and $\dot{p}=(\dot{x},\dot{y},\dot{z})^T$, respectively.
- ▶ The roll, pitch, and yaw angles in the body frame are defined as $\theta = (\phi, \theta, \psi)^T$, with corresponding angular velocities equal to $\dot{\theta} = (\dot{\phi}, \dot{\theta}, \dot{\psi})^T$.



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In order to convert roll, pitch and yaw velocities into the angular velocity vector, we can use the following relation:

$$\omega = \begin{bmatrix} 1 & 0 & -s_{\theta} \\ 0 & c_{\phi} & s_{\theta}s_{\phi} \\ 0 & -s_{\phi} & c_{\theta}c_{\phi} \end{bmatrix} \dot{\theta} \tag{1}$$

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cont.

Rotation matrix R relates the body and inertial frame, which goes from the body frame to the inertial frame.

$$R = \begin{bmatrix} c_{\phi}c_{\psi} - c_{\theta}s_{\phi}s_{\psi} & -(c_{\psi}s_{\phi} + c_{\phi}c_{\theta}s_{\psi}) & s_{\theta}s_{\psi} \\ c_{\theta}c_{\psi}s_{\phi} + c_{\phi}s_{\psi} & c_{\phi}c_{\theta}c_{\psi} - s_{\phi}s_{\psi} & -c_{\psi}s_{\theta} \\ s_{\phi}s_{\theta} & c_{\phi}s_{\theta} & c_{\theta} \end{bmatrix}$$
(2)

- ▶ This matrix is derived by using the ZYZ Euler angle conventions
- For a given vector \vec{v} in the body frame, the corresponding vector is given by $R\vec{v}$ in the inertial frame.



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Physics

- ▶ In order to properly model the dynamics of the system, we need an understanding of the physical properties that govern it.
- ▶ Topics which are going to discuss in this section are as follow:
 - Motors
 - Forces
 - Torques



▶ For electric motors, the torque produced is given by:

$$\tau = K_t(I - I_0) \tag{3}$$



Motors

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- Where:
 - $\, \, \triangleright \, \, \, \, \, au \,$ is the motor torque.
 - \triangleright I is the input current.
 - \triangleright I_0 is the current when there is no load on the motor.
 - $hd K_t$ is the torque proportionality constant.



▶ The voltage across the motor is:

$$V = IR_m + K_v \omega \tag{4}$$



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- ▶ Where:
 - $\, igrtap \, V$ is the voltage drop across the motor.
 - $ightharpoonup R_m$ is the motor resistance.
 - $ightharpoonup \omega$ is the angular velocity of the motor.
 - $ightharpoonup K_v$ is a proportionality constant.



Physics Motors – cont.

The motor's power consumption is:

$$P = IV = \frac{(\tau + K_t I_0)(K_t I_0 R_m + \tau R_m + K_t K_v \omega)}{K_t^2}$$
 (5)

- ▶ For the purposes of our simple model, we will assume
 - \triangleright A negligible motor resistance (i.e $R_m \approx 0$)
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▶ By conservation of energy, we know that:

$$P.dt = F.dx \tag{7}$$

Equivalently, the power is equal to the thrust times the air velocity

$$F = \frac{P}{v_h} \xrightarrow{\text{eq.6}} F = \frac{K_p \tau \omega}{v_h} \tag{8}$$

- ► We assume that
 - \triangleright Vehicle speeds are low, so v_h is the air velocity when hovering
 - \triangleright The free stream velocity, v_{∞} is zero
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► As torque is defined in The aerodynamic drag, we have:

$$\tau = \frac{1}{2}\rho A v_h^2 \tag{9}$$

- Where
 - $\triangleright \rho$ is the density of the surrounding air
 - \triangleright A is the area swept out by the rotor
- From equations 8 and 9, we can derive the following equation

$$F = \frac{K_p \tau \omega}{v_m}$$

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Physics Forces – cont.

▶ By eq.10 total thrust on the quadcopter(in the body frame) is given by:

$$T_B = \sum_{i=1}^{4} T_i = k \begin{bmatrix} 0 \\ 0 \\ \sum_{i=1}^{4} w_i \end{bmatrix}$$
 (11)

For modeling the friction, we will assume highly simplified version, which is

$$F_D = -k_d \begin{vmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{vmatrix} \tag{12}$$



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Each rotor contributes some torque about the body z axis.

$$F_D = \frac{1}{2}\rho C_D A v^2 \tag{13}$$



- ▶ Each rotor contributes some torque about the body z axis.
- ▶ The torque is required to keep the propeller spinning and providing thrust.
- It creates the instantaneous angular acceleration and overcomes the frictional drag forces.
- ▶ The drag equation from fluid dynamics gives us the frictional force:

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- ▶ Where
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Torques-cont.

▶ In general cases torque is cross product of distance vector and the applied force:

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► From eq.13 and eq.14 we have:

$$\tau_D = \frac{1}{2} R\rho C_D A v^2 \xrightarrow{\omega = \frac{v}{R}} \tau_D = \frac{1}{2} R\rho C_D A (R\omega)^2 = b\omega^2$$
 (15)

- ▶ Where:
 - $ightharpoonup \omega$ is the angular velocity of the propeller.
 - \triangleright R is the radius of the propeller.



Physics Torques – cont.

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Note:

We've assumed that all the force is applied at **the tip of the propeller**, which is certainly <u>inaccurate</u>.



Physics Torques - cont.

Torque about the z-axies for the *i*th motor is equal to:

$$\tau_i^z = \tau_{D_i} + I_M \dot{\omega}_i = b\omega_i^2 + I_M \dot{\omega}_i \tag{16}$$



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- Where:
 - I_M is the moment of inertia about the motor z-axis.
 - $\dot{\omega}$ is the angular acceleration of the propeller.
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- Inorder to neutralize the overall torque in quadcopter steady-state, two of the motors should spin clockwise, and the other two should spin counter-clockwise.



▶ Eq.16 can be written as following for each propellor:

$$\tau_i^z = (-1)^{i+1} b\omega_i^2 \tag{17}$$

- ▶ Which the $(-1)^{i+1}$ term is positive for the ith propeller if the propeller is spinning clockwise and negative if it is spinning counterclockwise.
- The total torque about the axises can be derived from standard mechanics

$$\tau_{\psi} = b \sum_{i=1}^{4} (-1)^{i+1} \omega_i^2 \tag{18}$$

$$\tau_{\theta} = \sum_{i \in \{2,4\}} \vec{r} \times T = Lk(\omega_2^2 - \omega_4^2)$$
 (19)

$$\tau_{\phi} = \sum_{i \in \{1.3\}} \vec{r} \times T = Lk(\omega_1^2 - \omega_3^2)$$
 (20)

 \triangleright Where the L is the distance from the center of the quadcopter to any of the propellers.



Torques - cont.

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Torques - cont.

▶ From equations 18...20 we can calculate the torque matrix in body frame:

$$\tau_{B} = \begin{bmatrix} Lk(\omega_{1}^{2} - \omega_{3}^{2}) \\ Lk(\omega_{2}^{2} - \omega_{4}^{2}) \\ b \sum_{i=1}^{4} (-1)^{i+1} \omega_{i}^{2} \end{bmatrix}$$
 (21)

- ► Rotational drag forces(our rotational velocities are relatively low).
- Blade flapping(deformation of propeller blades due to high velocities and flexible materials).
- Surrounding fluid velocities(wind).
- ▶ The noise distribution model of our motors' speed
- ▶ etc



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Equations of Motion

Acceleration

- ▶ In the inertial frame, the acceleration of the quadcopter is due to thrust, gravity and linear friction.
- ightharpoonup We can obtain the thrust vector in the inertial frame by using the rotation matrix R to map the thrust vector from the body frame to the inertial frame:

$$F = m\ddot{x} \tag{22}$$

$$F = m\vec{G} + RT_B + F_D \tag{23}$$

$$\ddot{x} = \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix} + \frac{RT_B + F_D}{m} \tag{24}$$

- Where:
 - \triangleright \vec{x} is the position of the quadcopter.
 - g is the acceleration due to gravity.
 - \triangleright F_D is the drag force.
 - \triangleright T_B is the thrust vector in the body frame.



Equations of Motion

Rotational Speed - cont.

Rotational equations can be drived from Euler's equations for rigid body dynamics, Expressed in vector form:

$$I\dot{\omega} + \omega \times (I\omega) = \tau \tag{25}$$

- Where:
 - \triangleright ω is the angular velocity vector.
 - I is the inertia matrix.
 - \triangleright τ is a vector of external torques.
 - T_B is the thrust vector in the body frame.
- ▶ The eq.25 can rewrite this as:

$$\dot{\omega} = \begin{bmatrix} \dot{\omega}_x \\ \dot{\omega}_y \\ \dot{\omega}_z \end{bmatrix} = I^{-1}(\tau - \omega \times (I\omega)) \tag{26}$$



Equations of Motion

Rotational Speed - cont.

For simplification if we assume that the quadcopter as two thin uniform rods crossed at the origin with a point mass (motor) at the end of each; The inertia matrix would come in form of a diagonal matrix.

$$I = \begin{bmatrix} I_{xx} & 0 & 0 \\ 0 & I_{yy} & 0 \\ 0 & 0 & I_{zz} \end{bmatrix}$$
 (27)

Therefore, we obtain our final result for the body frame rotational equations of motion:

$$\dot{\omega} = \begin{bmatrix} \tau_{\phi} I_{xx}^{-1} \\ \tau_{\theta} I_{yy}^{-1} \\ \tau_{\psi} I_{zz}^{-1} \end{bmatrix} - \begin{bmatrix} \frac{I_{yy} - I_{zz}}{I_{xx}} \omega_{y} \omega_{z} \\ \frac{I_{zz} - I_{xx}}{I_{yy}} \omega_{x} \omega_{z} \\ \frac{I_{xx} - I_{yy}}{I_{zx}} \omega_{x} \omega_{y} \end{bmatrix}$$
(28)



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