

**Kuwait University**  
College of Engineering and Petroleum



جامعة الكويت  
KUWAIT UNIVERSITY

# **ME417 CONTROL OF MECHANICAL SYSTEMS**

PART II: CONTROLLER DESIGN VIA STATE-SPACE

LECTURE 3: STATE-SPACE CONTROLLER REPRESENTATION AND DESIGN

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- Objectives:
  - Introduce the state-space feedback control form
  - Introduce the controller design by matching coefficients
  - Introduce the concept of controllability
- Reading:
  - *Nise: 12.1-12.3*
- Practice Problems Included

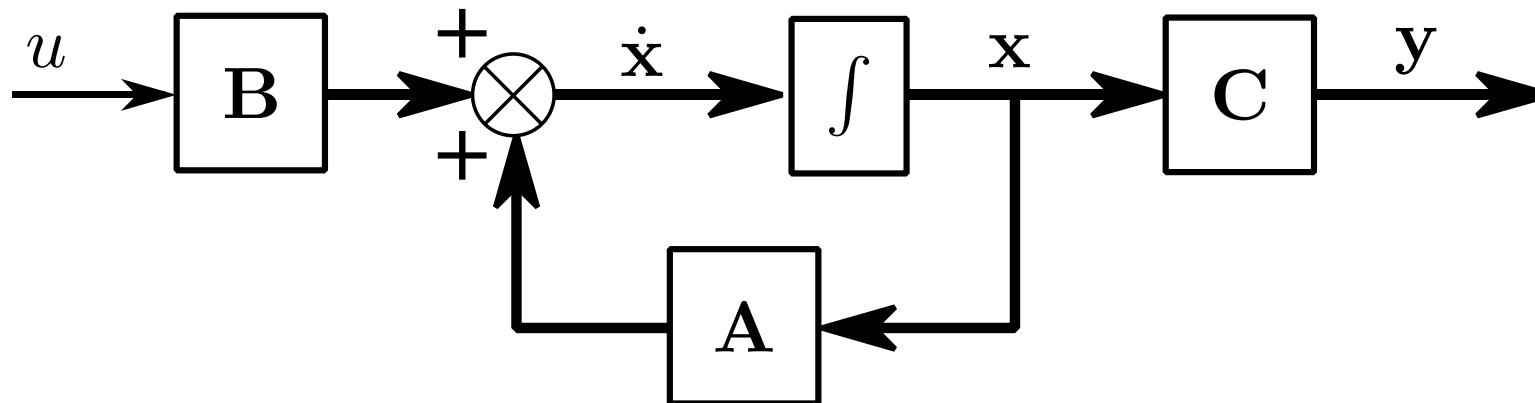


## State-Space Block Diagram Form – Open-Loop

- The open-loop LTI system represented in state-space

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u, u \in \mathcal{R}^1$$
$$\mathbf{y} = \mathbf{C}\mathbf{x}$$

- Can be represented in block diagram form
  - This is not a feedback loop, just a block diagram representation of the state-space equation



- There is no standard feedback form for systems in state-space. The form depends on the control method.
- A common feedback form for analyzing systems in state-space is the full state variable feedback control.
- With full-state feedback, it is assumed that all the system states  $\mathbf{x}$  are available, the input becomes  $u = r - \mathbf{K}\mathbf{x}$ ,  $\mathbf{K} \in \mathcal{R}^{1 \times n}$ ,  $\mathbf{x} \in \mathcal{R}^{n \times 1}$

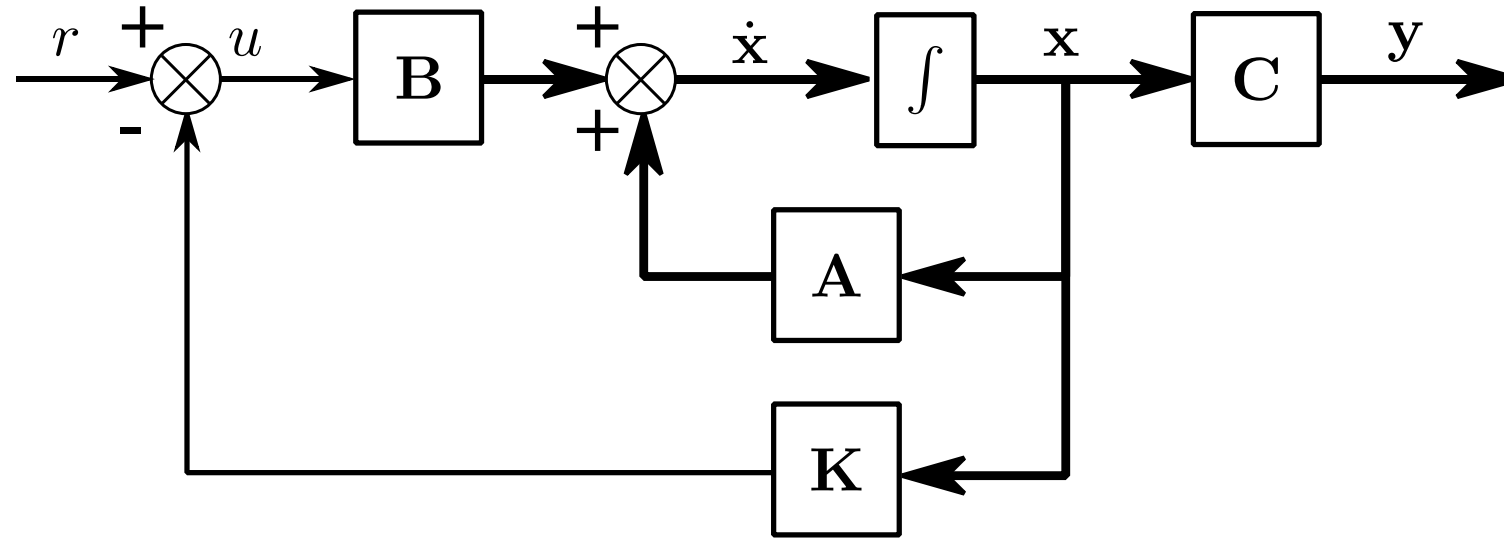
$$u = r - [K_1 \quad K_2 \quad \dots \quad K_n] \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix} = r - (K_1 x_1 + K_2 x_2 + \dots + K_n x_n)$$

- The gains in  $\mathbf{K}$  are the controller gains in this architecture.
  - All the system states are *weighted* in computing the control action  $u$



# State-Space Block Diagram Form – Full State Variable Feedback

- The full state feedback, can be represented in block diagram as



$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}(r - \mathbf{K}\mathbf{x}) = (\mathbf{A} - \mathbf{B}\mathbf{K})\mathbf{x} + \mathbf{B}r = \tilde{\mathbf{A}}\mathbf{x} + \mathbf{B}r$$
$$\mathbf{y} = \mathbf{C}\mathbf{x}$$

- The eigenvalues of the new matrix  $\tilde{\mathbf{A}}$  give the **closed-loop poles** of the feedback system:  $\det(s\mathbf{I} - \tilde{\mathbf{A}}) = \det(s\mathbf{I} - (\mathbf{A} - \mathbf{B}\mathbf{K})) = 0$

- The output  $y$  and the output matrix  $\mathbf{C}$  are normally set to reflect the sensors outputs.
- For example, if we have a motor model with  $\mathbf{x} = \begin{bmatrix} \theta_m \\ \dot{\theta}_m \end{bmatrix}$  and a tachometer (rotational speed sensor) is the only sensor installed on the system.
- Then we only have one **output**, and the output  $y = \dot{\theta}_m = \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} \theta_m \\ \dot{\theta}_m \end{bmatrix} = \mathbf{C}\mathbf{x}$



- With full state variable feedback, the design of the controller is done through pole placement (coefficient matching).
- Take the characteristic equation (the transfer function denominator) of the closed-loop system and equate it to a desired equivalent polynomial

$$\det(s\mathbf{I} - \tilde{\mathbf{A}}) = \det(s\mathbf{I} - \mathbf{A} + \mathbf{BK}) = a_n s^n + a_{n-1} s^{n-1} + \cdots + a_1 s + a_0$$

Where the constants  $a_n, \dots, a_0$  are **chosen** to result in a specific/desired closed loop pole locations, then the gains in  $\mathbf{K}$  are computed by coefficient matching.

Design a full state feedback controller to achieve a settling time of  $T_s = 1\text{s}$  and damping ratio of  $\zeta = 0.25$ , for the following system

$$\dot{\mathbf{x}} = \begin{bmatrix} 1 & 2 \\ -2 & -1 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$
$$\mathbf{y} = \begin{bmatrix} 1 & 0 \end{bmatrix} \mathbf{x}$$





Design a full state feedback controller to achieve a settling time of  $T_s = 1s$  and peak time of  $T_p = 0.25s$ , for the following system

$$G(s) = \frac{1}{s^2 + 4s + 8}$$



- Full state variable feedback is often unrealistic in real-world applications, and an observer is implemented instead.
  - Full state measurement means that we have sensors available to measure all the system states
  - An observer is a dynamic system, whose purpose is to **estimate** the states from the output  $y$ .
  - Observers are also called **state estimators** (e.g. Luenberger Observer, Recursive Least Squares Estimator, Kalman Filter)
  - Estimation Theory is a big subset of the world systems and control theory
    - It is also extremely beneficial in modern real-world applications
    - Artificial Intelligence has roots in Estimation Theory.



- For comparison, observe how a proportional feedback controller is represented in state-space
- For the following LTI system

$$\begin{aligned}\dot{\mathbf{x}} &= \mathbf{A}\mathbf{x} + \mathbf{B}u, \quad u \in \mathcal{R}^1 \\ \mathbf{y} \in \mathcal{R}^1 &= \mathbf{C}\mathbf{x}\end{aligned}$$

- The proportional controller is defined as

$$u = K_p e = K_p(r - y) = K_p(r - \mathbf{C}\mathbf{x})$$

- Substituting in the state-space form,

$$\begin{aligned}\dot{\mathbf{x}} &= (\mathbf{A} - \mathbf{B}K_p\mathbf{C})\mathbf{x} + \mathbf{B}K_p r \\ \mathbf{y} \in \mathcal{R}^1 &= \mathbf{C}\mathbf{x}\end{aligned}$$

- Comparing full state feedback to a proportional controller
  - Full State Feedback:  $u = r - \mathbf{K}\mathbf{x} = r - (K_1x_1 + \dots + K_nx_n)$
  - Proportional Controller for  $y = x_1$ :  $u = K_p(r - x_1)$

- What if you required the behavior of a second order system, but the system is higher than 2<sup>nd</sup> order, or if there is zero or more in the system?
- Several Options
  - Place the third, and higher poles, further into the LHP
  - If there is a **zero near the dominant poles**, place the third pole **on the zero** to cancel its effect.
- Remember that, with Full-State Feedback pole placement, if the system is **controllable**, you literally can place the poles where you desire.



Design a full state feedback controller to achieve a settling time of  $T_s = 1s$  and damping ratio  $\zeta = 0.5$

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -2 & -3 & -2 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$$
$$\mathbf{y} = [1 \quad 0 \quad 0] \mathbf{x}$$



- Can we always apply full state feedback?
- Can we always control all the states of the system?
- Can we always place the  $n$  poles of the closed-loop system where we want?
- The answer to the above questions is, no, we can not always achieve those outcomes.
- For the above outcomes to be met, the system must be **Controllable**

*"If an input to a system can be found that takes every state variable from a desired initial state to a desired final state, the system is said to be **controllable**; otherwise, it is **uncontrollable**"*



- Consider the following system

$$\dot{\mathbf{x}} = \begin{bmatrix} -5 & 0 & 0 \\ 0 & -2 & 0 \\ 0 & 0 & -1 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 2 \\ 1 \end{bmatrix} u$$

- Or

$$\begin{aligned}\dot{x}_1 &= -5x_1 \\ \dot{x}_2 &= -2x_2 + 2u \\ \dot{x}_3 &= -x_3 + u\end{aligned}$$

- Note that the states are decoupled, since one does not influence the other.
- The controller  $u$  only affects  $x_2$  and  $x_3$
- So, neither  $u$  affects  $x_1$  nor the other states affect  $x_1$  by proxy
- Thus, state  $x_1$  is **uncontrollable**: The system is **uncontrollable**

- Consider the following system

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -5 & -3 & -1 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$$

- Or

$$\begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= x_3 \\ \dot{x}_3 &= -5x_1 - 3x_2 - x_3 + u \end{aligned}$$

- Note that the states are coupled in  $\dot{x}_3$
- The controller  $u$  affects  $\dot{x}_3$
- And  $\dot{x}_3$  is coupled with all states, so  $u$  affects all states by proxy.
- Thus, all states are **controllable**: The system is **controllable**





- The solution is generalized by considering the rank of the controllability matrix  $\mathbf{C}_M$
- For a given dynamic system  $\dot{\mathbf{x}} \in \mathcal{R}^n = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{u}$ , the system is controllable if the rank of the controllability matrix  $\mathbf{C}_M$  is  $n$ : The number of states of the system
- The controllability matrix for a system with  $n$  states is defined as

$$\mathbf{C}_M \in \mathcal{R}^{n \times n} = [\mathbf{B} \quad \mathbf{AB} \quad \mathbf{A}^2\mathbf{B} \quad \dots \quad \mathbf{A}^{n-1}\mathbf{B}]$$

- A sufficient condition for  $\text{rank}(\mathbf{C}_M) = n$  is that
$$\det(\mathbf{C}_M) \neq 0$$
- In other words, if  $\det(\mathbf{C}_M) \neq 0$ , the system is **controllable**; otherwise, it is **uncontrollable**



Can full state feedback be applied to the following system?

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & -5 \\ 0 & -1 \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$
$$\mathbf{y} = \begin{bmatrix} 1 & 0 \end{bmatrix} \mathbf{x}$$



Nise 6<sup>th</sup> Global Edition:  
12-4, 12-6, 12-7, 12-18

