# **Kuwait University**College of Engineering and Petroleum





#### **ME417 CONTROL OF MECHANICAL SYSTEMS**

PART II: CONTROLLER DESIGN USING ROOT-LOCUS

LECTURE 1: INTRODUCTION TO ROOT-LOCUS

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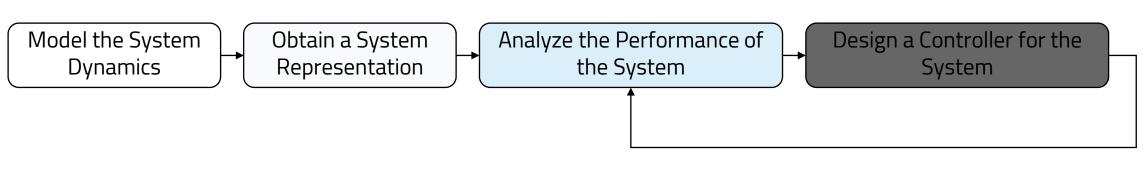
#### Lecture Plan

- Objectives:
  - Review the anatomy of a control system block diagram
  - Introduction to the concept of root-locus diagrams
  - Overview the properties of the root-locus
- Reading:
  - Nise: 8.1-8.3
- Practice problems are more applicable after the subsequent lectures.



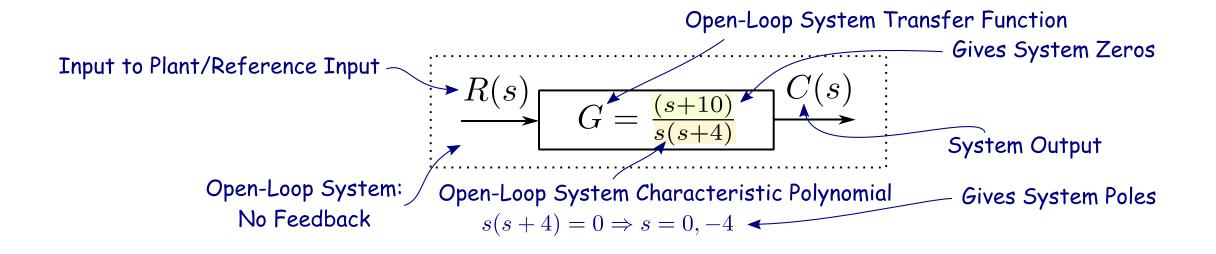
#### Where we are

- We will now begin to introduce the first main technique of designing a controller.
- The design technique we will learn in this part is a graphical technique, it offers an alternative and qualitative method to understand the behavior of a dynamic system.
- It is also considered a way to represent the system and a method to analyze the performance (inherent to the design intent).



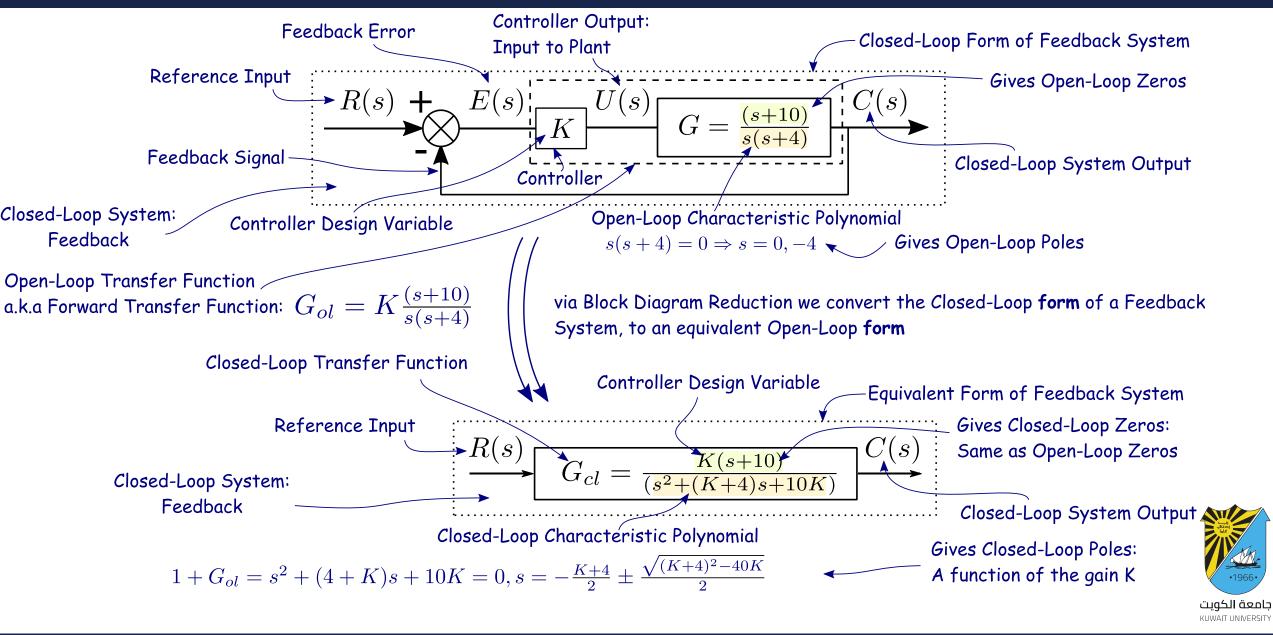


# Review of Control System Block Diagram Anatomy: Open-Loop System





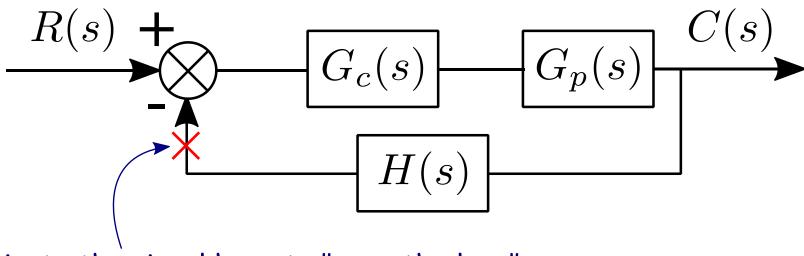
# Review of Control System Block Diagram Anatomy: Unity Closed-Loop System



# Open-Loop Transfer Function of a Non-Unity Feedback System

- The open-loop transfer function of a **any** feedback system is obtained by terminating the feedback signal at just before the summation block. And multiplying all the blocks in series up to the termination point.
- For a Non-Unity Feedback System, the open-loop transfer function is:

$$G_{ol} = G_C(s)G_P(s)H(s)$$



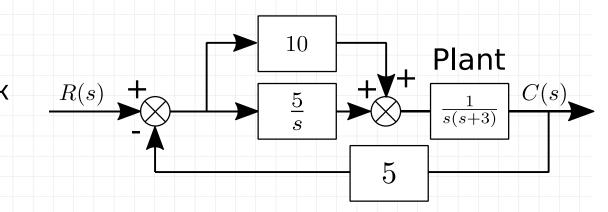
Terminate the signal here to "open the loop"



For the following unity feedback system. Derive the following:

Example

- a. The plant transfer function
- b. The controller transfer function
- c. The open-loop transfer function without feedback
  - (The open-loop <u>system</u> T.F.)
- d. The open-loop transfer function with feedback
- e. The forward transfer function
- f. The closed-loop transfer function
- g. The closed-loop characteristic polynomial
- h. The input to the plant in terms of the reference.
- i. The controller design variables

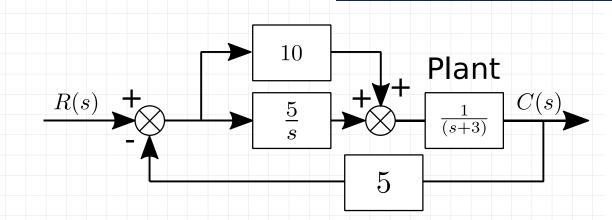




For the following unity feedback system, place the:

Example

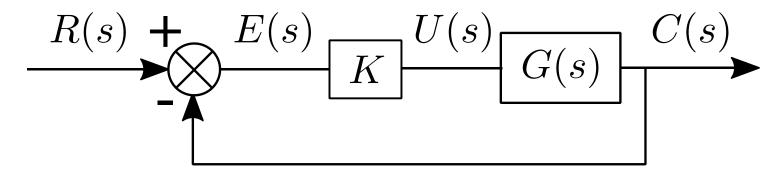
- a. Plant poles and zeros
- b. Open-loop poles and zeros
- c. Closed-loop poles and zeros





#### What is a Root-Locus

Given a feedback control system of the form

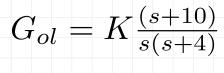


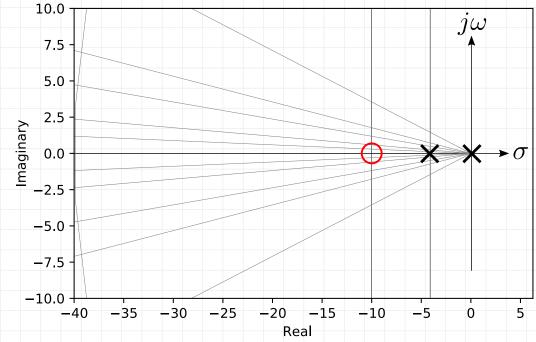
• With the equivalent open-loop **form**:

$$R(s) \longrightarrow G_{cl}(s) = \frac{KG(s)}{1+KG(s)} \longrightarrow C(s)$$

• The root-locus is the locus of the roots of the characteristic polynomial of the closed-loop transfer function:  $1+KG_{ol}=0$ , on the s-plane, as K goes from 0 to  $\infty$ 

#### Closed-Loop System Representation on the S-Plane

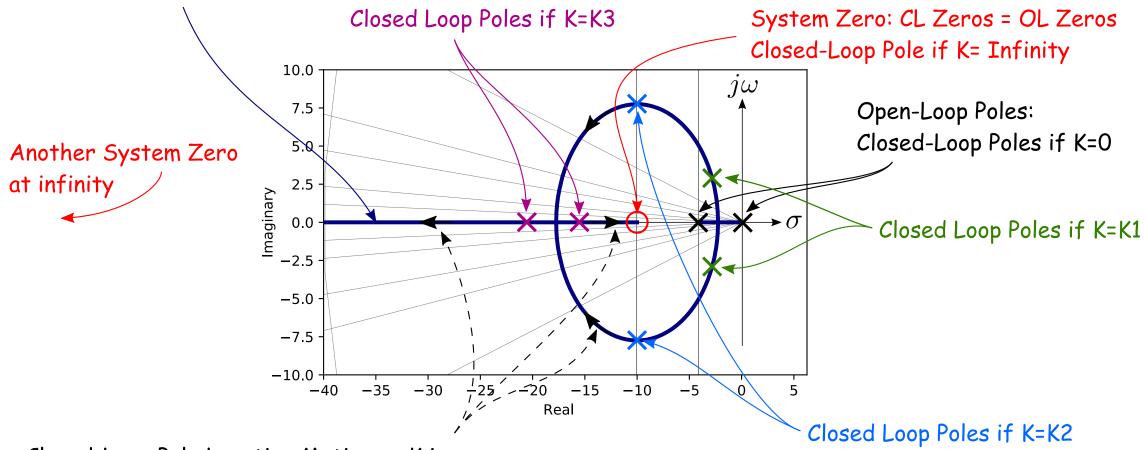






#### Closed-Loop System Representation on the S-Plane

The Locus of the Closed-Loop Poles as K goes from 0 to infinity (Root-Locus)



Closed-Loop Pole Location Motion as K increases:

As K increases, CL Poles move away from OL poles and toward system zeros:

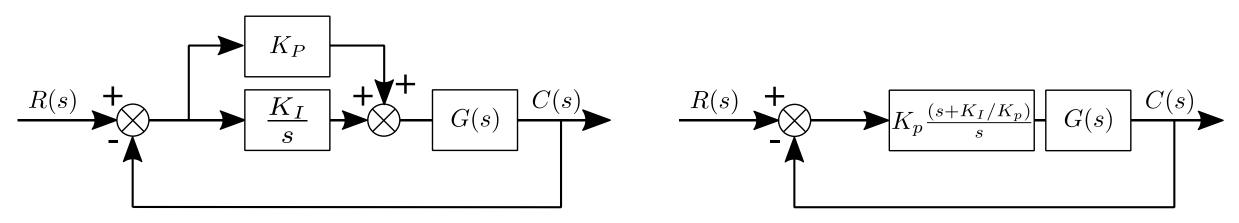
Here: K1<K2<K3

$$G_{ol} = K \frac{(s+10)}{s(s+4)}$$
  $G_{cl} = \frac{K(s+10)}{(s^2 + (K+4)s + 10K)}$ 



# What if we have more than just one gain?

- The root locus is drawn for a single variable *K*, what if there is more than one gain in the feedback loop, as is the case when applying a PID controller?
- Take the **PI** Controller:



- We can factor out the proportional gain  $K_p$  as the root locus variable and fix the ratio  $K_I/K_p$ . The ratio  $K_I/K_p=z_1$ , determines the location of the added zero by the PI controller. The root-locus will become a variable of  $K_p$
- Char. Poly.:  $1 + K_p \frac{(s+z_1)G(s)}{s} = 0$

We wish to apply a PI feedback controller on a dc motor to control its speed. Find the values of the gain  $K_I$ , if  $K_p=1$ , to achieve a settling time of 0.25s, when a step input of  $10 \, \text{rad/s}$  is applied.

#### Example



Given the following unity feedback system, determine the location of the open-loop poles, then compute the characteristic polynomial for the closed-loop system. How would you find the poles of the closed-loop sys? R(s) +

Example

 $\begin{array}{c|c} \hline (s+5) \\ \hline s \\ \hline \end{array} \begin{array}{c|c} \hline 1 \\ \hline (s^2+9) \\ \hline \end{array} \begin{array}{c|c} C(s) \\ \hline \end{array}$ 

The open-loop transfer function is: 
$$G_{ol} = G_c G_p = \frac{(s+5)}{s(s^2+9)}$$

The poles of the open loop transfer function are the roots of the open-loop characteristic polynomial:

$$s(s^2 + 9) = 0 \Rightarrow s = 0, \pm 3j$$

The closed-loop transfer function is:  $G_{cl} = \frac{G_c G_p}{1 + G_c G_p}$ 

The characteristic polynomial of the closed-loop system:  $1+G_cG_p=0$ 

The poles of the closed-loop system are the roots of the closed-loop characteristic polynomial:

$$1 + \frac{(s+5)}{s(s^2+9)} = s^3 + 10s + 5 = 0$$

In order to find the poles of the closed loop system we need to factor a 3<sup>rd</sup> degree polynomial. This becomes hard, but fortunately, we can use the root-locus technique to treat such case.



## Why design via Root-Locus

- What if we want to:
- 1. Observe the effect of changing gain parameters on the system response
  - Where would the poles of the closed-loop system be as we change the gain K
- 2. Observe the effect of adding dynamic compensation to the closed loop system
  - What happens when we use a controller that adds poles and zeros to the closed-loop system?

Example: PI Controller, 
$$G_c = K_P \frac{s + K_I/K_p}{s}$$
, adds a zero and a pole

- 3. Examine the sensitivity and stability of a closed loop system
  - How close are the closed-loop poles to stability?
- 4. Design controllers for higher order systems
  - It is hard to factor roots for polynomials of 3rd and higher order.
- A graphical controller design **technique**, such as the root-locus, can help us



## Complex Numbers and Vector Representation

- The Laplace Function F(s), is a function of the complex variable s, but how do we evaluate the function at any s?
- If we have the function in factored form

$$F(s) = \frac{\prod_{i=1}^{m} (s+z_i)}{\prod_{j=1}^{n} (s+p_j)} = \frac{(s+z_1)(s+z_2) \dots (s+z_m)}{(s+p_1)(s+p_2) \dots (s+p_n)}$$

Where  $\prod$  denotes product, m the number of zeros, n the number of poles

• The solution:  $F(s) = M \angle \theta$ 

$$M = \frac{\prod(\text{zero vector lengths})}{\prod(\text{pole vector lengths})}$$

$$\theta = \sum \text{zero angles} - \sum \text{pole angles} = \sum_{i=1}^{m} \angle(s + z_i) - \sum_{j=1}^{n} \angle(s + z_j)$$



# Evaluate, vectorially, the function $F(s) = \frac{(s+1)}{s(s+2)}$ at s = -3 + j4

Example - Solved

To solve for this vectorially, we find the lengths and angles of all poles and zeros then add them

Zero: Length = 
$$\sqrt{(-3-(-1))^2+(4-0)^2} = \sqrt{20}$$
, angle =  $\tan^{-1}\left(\frac{4-0}{-3+1}\right) = 116^\circ$ 

Pole at 0: Length = 
$$\sqrt{(-3-(0))^2+(4-0)^2} = \sqrt{25} = 5$$
, angle =  $\tan^{-1}\left(\frac{4-0}{-3-0}\right) = 127^\circ$ 

Pole at -2: Length = 
$$\sqrt{(-3 - (-2))^2 + (4 - 0)^2} = \sqrt{17}$$
, angle =  $\tan^{-1} \left( \frac{4 - 0}{-3 + 2} \right) = 104^\circ$ 

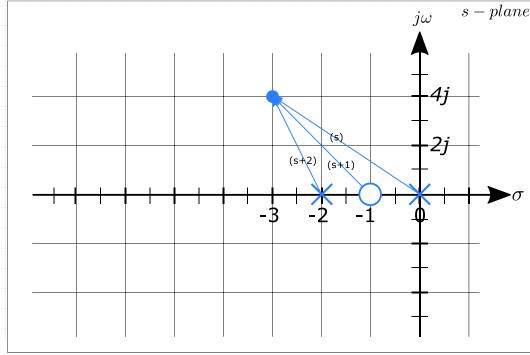
$$F(s = -3 + j4) = M \angle \theta = \frac{\prod(\text{zero vector lengths})}{\prod(\text{pole vector lengths})} \angle \sum \text{zero angles} - \sum \text{pole angles}$$

$$F(s = -3 + j4) = \left(\frac{\sqrt{20}}{5\sqrt{17}}\right) \angle 116^o - 127^o - 104^o = -114^o$$

$$F(s = -3 + j4) = 0.217 \angle -114^{\circ}$$

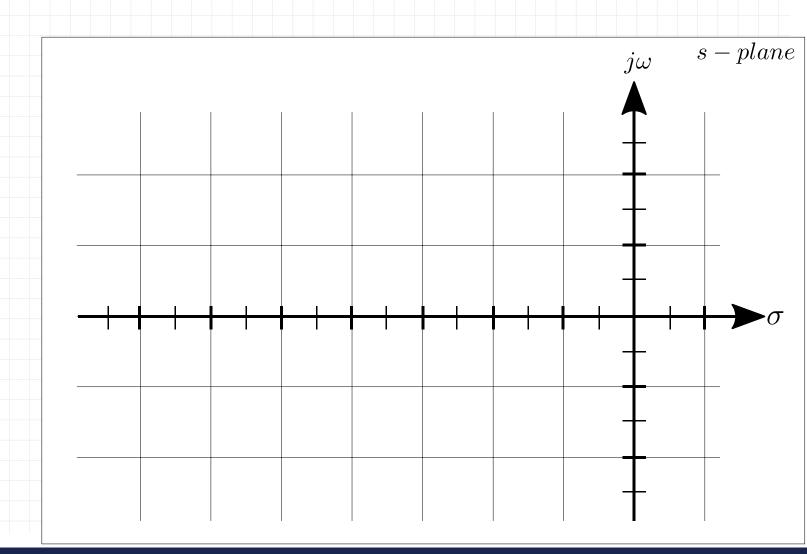
Verify in MATLAB using evalfr()

$$F = -0.089 - .197j$$



Evaluate, vectorially, the function 
$$F(s) = \frac{(s+3)(s+1)}{s(s+2)}$$
 at  $s = -2 + j$ 

Algebraically: F = 0.4 - 0.8j



#### Properties of the Root-Locus

- Given the closed-loop transfer function
  - $G_{cl} = \frac{KG(s)}{1+KG(s)H(s)}$ : non-unity feedback
- A pole, *s*, exists when the characteristic polynomial becomes zero:

$$1 + KG(s)H(s) = 0,$$
  
 $KG(s)H(s) = -1 = 1 \angle (2k + 1)180^{o}, k = 0, \pm 1, \pm 2, \pm 3, ...$ 

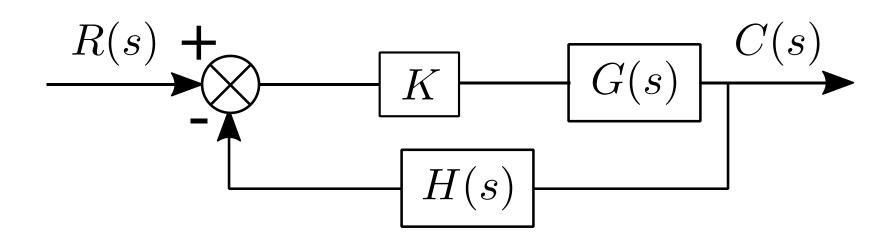
Where -1 is represented in polar form as:  $1 \angle (2k + 1)180^o$ 

- Also, the magnitude: |KG(s)H(s)| = 1
  - And if we assume  $K \ge 0$  strictly. Then  $K = \frac{1}{|G(s)||H(s)|}$  (eq. 1)
- And angle:  $\angle KG(s)H(s) = (2k+1)180^o$  (eq. 2)
- In other words: for s to be a pole of the CL system it has to satisfy eq. 1 and eq. 2



#### Properties of the Root-Locus

- The root locus is the locus of pole locations in the s-plane for varying values of gain  $K \ge 0$ , in the closed loop transfer function  $G_{cl} = \frac{KG(s)}{1+KG(s)H(s)}$ , that satisfy the following two conditions:
  - 1. Magnitude Condition:  $K = \frac{1}{|G(s)||H(s)|}$
  - 2. Angle Condition:  $\angle KG(s)H(s) = (2k+1)180^o$

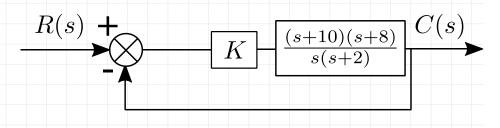




# For the feedback system shown, show that the point s = -5 + 3.87j, is on the root-locus and find the value of the gain K at this point

Example - Solved

To find if a point lies on the root-locus, given a feedback system open-loop (forward) transfer function. We check to see if the Angle Condition is met:



Angle Condition:  $\angle \Sigma$  zero angles  $-\angle \Sigma$  pole angles  $=\angle |KG(s)| = \angle (2k+1)180^{\circ}$ 

$$\angle |KG(s)| = \theta_3 + \theta_4 - \theta_1 - \theta_2$$
  
=  $atan(3.87/3) + atan(3.87/5) - (180 - atan(3.87/5))$   
-  $(180 - atan(3.87/3)) \approx 180 - 180 - 180 \approx -180^{\circ}$ 

The point is thus on the root locus, as it meets the angle condition.

To find the value of the gain, we check the magnitude condition

$$K = \frac{1}{|G(s)|} = \frac{\text{Pole Lengths}}{\text{Zero Lengths}} = \frac{L_1 L_2}{L_3 L_4} = 1$$

