

VREMENSKI ODZIV RC KRETA

1

• prvo gledao za $t=0^-$ i $t=0^+$

$$\tau = R \cdot C$$

• $0 \leq t \leq T$

$$u_c(t) = U_{co} + (U_0 - U_{co})(1 - \exp(-\frac{t}{\tau}))$$

↑
poč. vrijednost
napona na kond.
↑
razlika napona
koja nabija kond.

- za nabijanje kondenzatora je
potrebno vrijeme jednako iznosu
5 vremenskih konstanti (5 τ)

$$u_R(t) = u_{uc}(t) - u_c(t) = (U_0 - U_{co}) \exp(-\frac{t}{\tau}) \quad 0 < t < T$$

• u trenutku T^+ ulazni napon pada na 0V

• za $t \geq T$ $u_c(t) = u_c(T) \cdot \exp(-\frac{(t-T)}{\tau})$

• $u_R(t) = -u_c(t) \quad t > T$

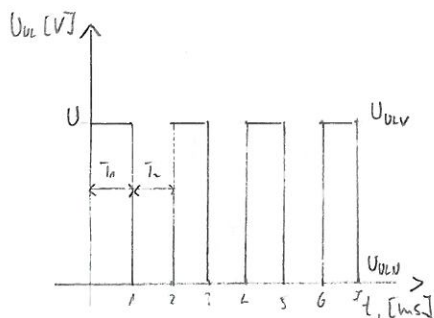
• CE mreža : $u_{iz}(t) = \frac{R}{R+R_g} (U_0 - U_{co}) \exp(-\frac{t}{\tau}) \quad 0 \leq t \leq T$

↑
unutarnji otpor (R_g) generatora

• u trenutku T^+ vrijedi: $u_{iz}(T^+) = -u_c(T^+) \cdot \frac{R}{R+R_g}$

• za $t > T$ $u_{iz}(t) = u_{iz}(T^+) \exp(-\frac{(t-T)}{\tau})$

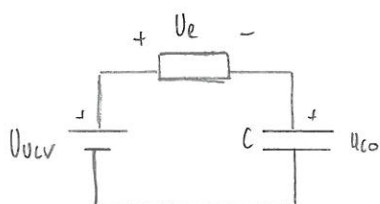
• analiza odziva na sinetričan pravokutni napon



• oznake:

visoka razina ulaznog napona - U_{HLV}
trajanje visoke razine ulaznog napona - T_H
niska razina ulaznog napona - U_{LLV}
trajanje niske razine ulaznog napona - T_L
početni napon na kondenzatoru - U_{co}

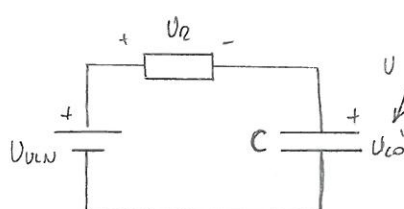
• visoka razina :



$$u_c(t) = U_{co} + (U_{HLV} - U_{co})(1 - \exp(-\frac{t}{\tau})) \quad 0 \leq t \leq T_H$$

$$u_R(t) = U_{HLV} - u_c(t) = (U_{HLV} - U_{co}) \exp(-\frac{t}{\tau}) \quad 0 < t < T_H$$

• niska razina :



vrijednost napona na kond.
u trenutku promjene napona sa
visoke na nisku razinu

$$u_c(t') = U_{co} + (U_{LLV} - U_{co})(1 - \exp(-\frac{t'}{\tau})) \quad 0 \leq t' \leq T_L$$

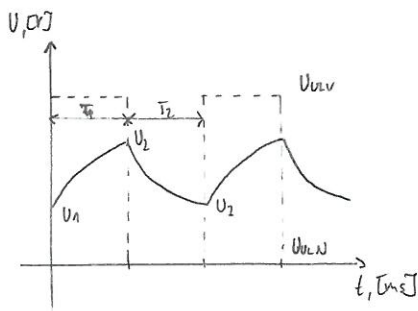
$$u_R(t') = U_{LLV} - u_c(t') = (U_{LLV} - U_{co}) \exp(-\frac{t'}{\tau}) \quad 0 < t' < T_L$$

$t' = 0 \Rightarrow$ trenutak promjene ulaznog napona sa visoke
na nisku

• slike nabijanja i nabijanja kond. nisu jednake: $|U_{HLV} - U_{co}| > |U_{LLV} - U_{co}|$

- u stacionarnom stanju napon na kond. varira oko srednje vrijednosti ulaznog napona. Srednja vrijednost napona na kond. jednaka je srednjoj vrijednosti ulaznog napona, dok srednja vrijednost napona na otporniku iznosi 0V.

• odziv na kondenzatoru



$$U_2 = U_1 + (U_{ULV} - U_1) \left(1 - \exp\left(-\frac{T_1}{\tau}\right)\right) = U_{ULV} - (U_{ULV} - U_1) \exp\left(-\frac{T_1}{\tau}\right)$$

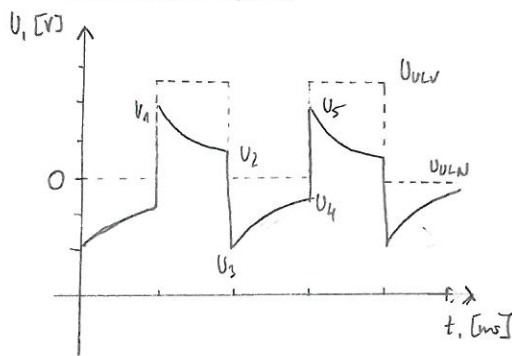
$$U_3 = U_2 + (U_{ULN} - U_2) \left(1 - \exp\left(-\frac{T_2}{\tau}\right)\right) = U_{ULN} - (U_{ULN} - U_2) \exp\left(-\frac{T_2}{\tau}\right)$$

$$U_3 = U_1$$

- za simetričan signal vrijedi: $U_{ULV} - U_2 = U_1 - U_{ULN}$

$$u_c(t) = u_{ULV}(t) - u_c(t)$$

• odziv na naponu



$$U_0 = U_{ULV} - U_{ULN}$$

$$U_2 = U_1 \cdot \exp\left(-\frac{T_1}{\tau}\right)$$

$$U_3 = U_2 - U_0$$

$$U_4 = U_3 \cdot \exp\left(-\frac{T_2}{\tau}\right)$$

$$U_5 = U_4 + U_0 = U_1$$

- za simetričan signal: $U_3 = -U_1$ i $U_4 = -U_2$

$$u_c(t) = u_{ULV}(t) - u_c(t)$$

OSNOVNA SVOJSTVA POLUVODIČA

$$n_i = C \cdot T^{3/2} \exp\left[-\frac{E_G(T)}{2 \cdot E_T}\right] = C_1 \cdot T^{3/2} \cdot \exp\left(-\frac{E_{G0}}{2 E_T}\right)$$

$$C = 7,07 \cdot 10^{15}$$

$$E_{G0} = 1,196$$

$$C_1 = 7,07 \cdot 10^{16}$$

$$E_T = k \cdot T = 8,62 \cdot 10^{-5} \cdot T$$

$$n_i^2 = n \cdot p$$

- ako je $n \gg n_i$ ili $p \gg n_i$ onda je vodič EKSTREMIZIRAN i možemo zaključiti:

$$n \approx N_D \quad \text{ili} \quad p \approx N_A$$

- ako ne vrijedi $N_D \gg n_i$ ili $N_A \gg n_i$ vodič je INTRINZICAN te koristimo:

$$n = \frac{1}{2} [N_D + \sqrt{N_D^2 + 4n_i^2}] \quad \text{ili} \quad p = \frac{1}{2} [N_A + \sqrt{N_A^2 + 4n_i^2}]$$

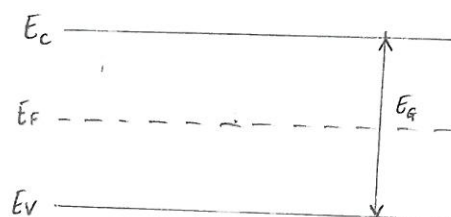
• Fermijeva energija

$$n_0 = N_C \exp\left(\frac{E_F - E_C}{E_T}\right) = n_i \exp\left(\frac{E_F - E_{Fi}}{E_T}\right)$$

$$p_0 = N_V \exp\left(\frac{E_V - E_F}{E_T}\right) = n_i \exp\left(\frac{E_{Fi} - E_F}{E_T}\right)$$

$$N_C = N_V = C T^{3/2}$$

$$E_{Fi} = \frac{E_V + E_C}{2}$$



E_C - vodljiv pojas

E_V - valentni pojas

• Vodljivost:

$$\sigma = q(\mu_n \cdot n + \mu_p \cdot p)$$

• otpor silicijske pločice: $R = \rho \cdot \frac{L}{S} = \frac{1}{\sigma} \cdot \frac{L}{S} \Rightarrow S = \frac{1}{\sigma} \Rightarrow$ specifični otpor

pn-DIODA

• kontaktni potencijal: $V_K = U_T \cdot \ln\left(\frac{n_{0n} \cdot p_{0p}}{n_i^2}\right)$

• širina osiromašenog područja: $d_B = \sqrt{\frac{2\epsilon_0 \cdot \epsilon_r}{q} \cdot \left(\frac{1}{N_A} + \frac{1}{N_D}\right) \cdot (U_K - U)}$

• kapacitet osiromašenog područja: $C_B = \epsilon_0 \cdot \epsilon_r \cdot \frac{S}{d_B}$

• struja zasićenja za diodu:

$$I_s = q \cdot S \cdot \left(D_n \frac{n_{0p}}{L_n} + D_p \frac{p_{0n}}{L_p} \right) \quad \text{ili} \quad I_s = q \cdot S \cdot \left(D_n \frac{n_{0p}}{w_p} + D_p \frac{p_{0n}}{w_n} \right)$$

• ako je $L_p \gg w_n$ koristimo w_n umesto L_p , ako je $L_n \gg w_p$ koristimo w_p umesto L_n

• manjinski nosioci na p-strani:

$$n_{0p} = \frac{n_i^2}{N_A}$$

$$D_n = \mu_n \cdot U_T$$

$$L_n = \sqrt{D_n \cdot \tau_n}$$

• manjinski nosioci na n-strani:

$$p_{0n} = \frac{n_i^2}{N_D}$$

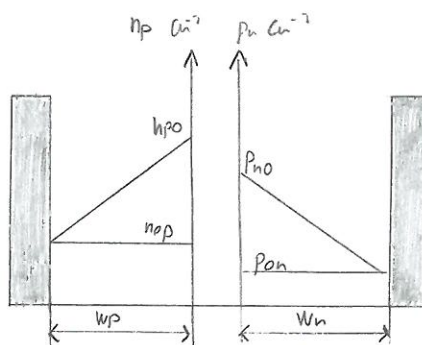
$$D_p = \mu_p \cdot U_T$$

$$L_p = \sqrt{D_p \cdot \tau_p}$$

• struja kroz diodu:

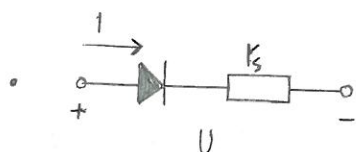
$$I = I_s \cdot \left[\exp\left(\frac{U}{m \cdot U_T}\right) - 1 \right]$$

• dinamički otpor: $r_d = \frac{U_T}{I + I_s}$



$$n_{p0} = n_{0p} \exp\left(\frac{U}{U_T}\right)$$

$$p_{n0} = p_{0n} \exp\left(\frac{U}{U_T}\right)$$



$$U = U_D + I \cdot R_s$$

$$U_D = U_T \cdot \ln\left(\frac{I}{I_s} + 1\right)$$

- ako je priključena izmjenična struja:

$$i_D = I + i_d \sin(\omega t)$$

$$U = U_D + I \cdot R_s$$

$$r_d = \frac{U_T}{I + I_s}$$

$$u_d = i_d (r_d + R_s)$$

$$\left. \begin{array}{l} U = U_D + I \cdot R_s \\ r_d = \frac{U_T}{I + I_s} \\ u_d = i_d (r_d + R_s) \end{array} \right\} u_D = U + u_d \cdot \sin \omega t$$

SKLOPOVI S DIODOM

- amplituda napora na sekundaru: $U_{sm} = \frac{\sqrt{2} \cdot U_{pct}}{n} = \frac{U_{pm}}{n} = U_{izm}$
→ omjer transformacije transformatora

$$\tau = R \cdot C$$

$$T = \frac{1}{f}$$

- amplituda napona valovitosti na trošilu je:

- polovalni: $U_{izvm} = U_{izm} \frac{T}{2\tau}$

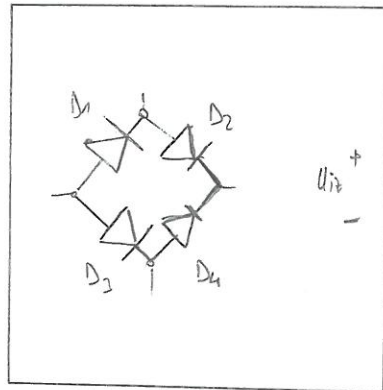
- ponovalni: $U_{izvm} = U_{izm} \frac{T}{4\tau}$

$$U_{iz} = U_{izm} - U_{izvm}$$

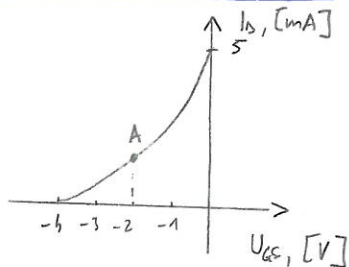
$$U_{izet} = \frac{U_{izvm}}{\sqrt{3}}$$

$$r = \frac{U_{izet}}{U_{iz}}$$

↑ faktor valovitosti



Unipolarni tranzistori - JFET



$$\Rightarrow U_p = -4V$$

$$I_{DSS} = 5mA$$

- ako je:

$U_p < 0 \rightarrow$ n-kanalni JFET $\leftarrow I_D$ opada kada U_{GS} postaje negativniji

$U_p > 0 \rightarrow$ p-kanalni JFET $\leftarrow I_D$ raste kada U_{GS} postaje negativniji

- u zasićenju vrijedi:

$$I_D = I_{DSS} \cdot \left(1 - \frac{U_{GS}}{U_p}\right)^2$$

$$g_m = \left. \frac{\partial I_D}{\partial U_{GS}} \right|_{U_{DS}} = \frac{2 \cdot I_{DSS}}{-U_p} \left(1 - \frac{U_{GS}}{U_p}\right)$$

$$I_D = I_{DSS} \left(1 - \frac{U_{GS}}{U_p}\right)^2 (1 + \lambda U_{DS})$$

$$g_d = \left. \frac{\partial I_D}{\partial U_{DS}} \right|_{U_{GS}} = 2 \cdot I_{DSS} \left(1 - \frac{U_{GS}}{U_p}\right)^2 \lambda = \frac{2 \cdot I_D}{(1 + \lambda U_{DS})}$$

$$r_d = \frac{1}{g_d}$$

$$\mu = g_m \cdot r_d$$

Unipolarni tranzistori - MOSFET

- kad U_{GS} postaje pozitivniji a I_D raste \rightarrow n-kanalni MOSFET
- kad U_{GS} postaje negativniji a I_D raste \rightarrow p-kanalni MOSFET
- kad za $U_{GS} = 0V$ kanal nije formiran ($I_D = 0$) \rightarrow OBOGAĆENI TIP (radi samo s jednim predznakom napona upravljačke elektrode)
- kad za $U_{GS} = 0V$ kanal je formiran ($I_D \neq 0$) \rightarrow OSIROMAŠEN TIP (radi s dva predznaka napona upravljačke elektrode)
- za konstantan napon faktor 2 nam nije potreban

• Ako je:

1) $|U_{DS}| < |U_{GS} - U_{GS0}| \rightarrow$ MOSFET je u TRIODNOM području

$$I_D = K \left[(U_{GS} - U_{GS0}) U_{DS} - \frac{U_{DS}^2}{2} \right]$$

• dinamički parametri:

$$g_m = \left. \frac{\partial I_D}{\partial U_{GS}} \right|_{U_{DS}} = K \cdot U_{DS}$$

$$g_d = \left. \frac{\partial I_D}{\partial U_{DS}} \right|_{U_{GS}} = K \cdot (U_{GS} - U_{GS0} - U_{DS}/2)$$

$$r_d = \frac{1}{g_d}$$

$$\mu = g_m \cdot r_d$$

2) $|U_{DS}| > |U_{GS} - U_{GS0}| \rightarrow$ MOSFET je u ZASIĆENOM području

$$I_D = \frac{K}{2} (U_{GS} - U_{GS0})^2 (1 + \lambda U_{DS})$$

• dinamički parametri:

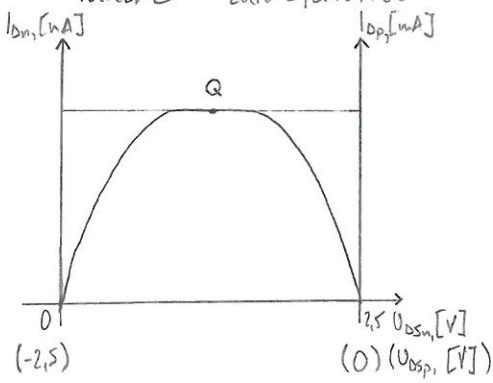
$$g_m = \left. \frac{\partial I_D}{\partial U_{GS}} \right|_{U_{DS}} = K (1 + \lambda U_{DS}) (U_{GS} - U_{GS0})$$

$$g_d = \left. \frac{\partial I_D}{\partial U_{DS}} \right|_{U_{GS}} = \frac{K \lambda}{2} (U_{GS} - U_{GS0})^2 = \frac{K \lambda}{2} (U_{GS} - U_{GS0})^2 \frac{1 + \lambda U_{DS}}{1 + \lambda U_{DS}} = \frac{I_D}{U_{DS} + \frac{1}{\lambda}}$$

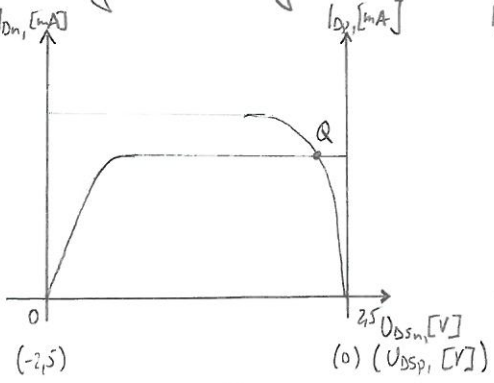
$$K = \mu_n \cdot \frac{\epsilon_{ox}}{t_{ox}} \cdot \frac{W}{L} \rightarrow \text{konstanta MOSFET-a}$$

$$C_G = \frac{\epsilon_{ox}}{t_{ox}} \cdot W \cdot L = \frac{\epsilon_{ox}}{t_{ox}} \cdot \frac{W}{L} \cdot L^2 = \frac{K}{\mu_n} \cdot L^2 \rightarrow \text{kapacitet upravljačke elektrode}$$

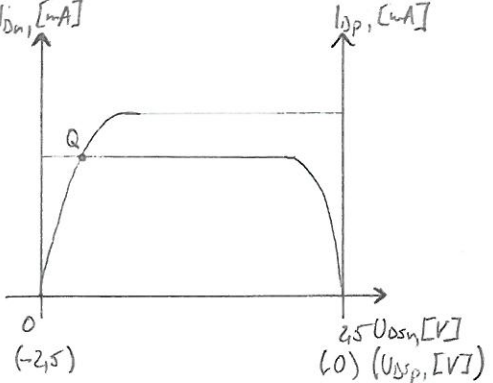
• Iznosne karakteristike za tri moguća slučaja:



NMOS i PMOS u zasićenju



NMOS u zasićenju
PMOS u triodnom



NMOS u triodnom
PMOS u zasićenju

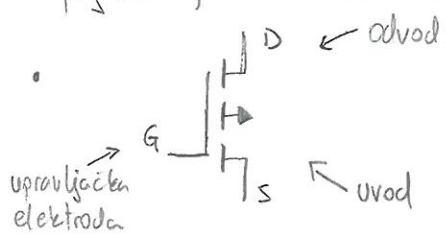


• $U_{gs} = U_g - U_s$

SKLOPOVI S MOSFET-om

- spojevi pojačala: → spoj zajedničkog ulaza
→ spoj zajedničke upravljačke elektrode
→ spoj zajedničkog odvoda

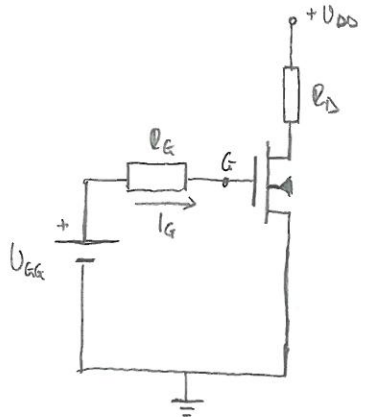
• da bi odredili koji spoj imamo pogledamo na što u spojeni ulaz i izlaz pojačala, što nam ostane to je zajedničko



• određivanje statičke radne točke:

- pri statičkoj analizi kondenzatori predstavljaju beskonačno velik otpor pa ih odspajamo
- tri slučaja:

1) bez otpora R_s u shemi



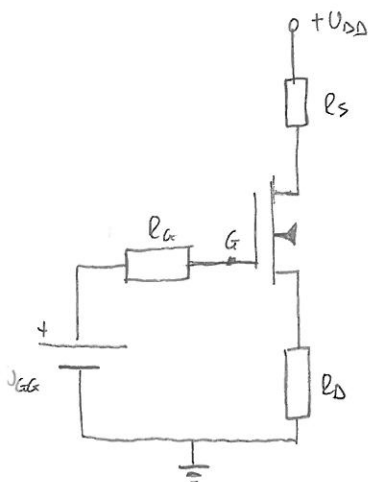
$$I_{DQ} = \frac{k}{2} (U_{GSQ} - U_{GS0})^2$$

$$U_{GSQ} = \frac{R_2}{R_1 + R_2} \cdot U_{DD}$$

$$R_G = R_1 || R_2$$

$$U_{DSQ} = U_{DD} - R_D \cdot I_{DQ}$$

2) Uz otpor R_S u shemi



$$R_G = R_1 \parallel R_2$$

$$V_{GG} = \frac{R_2}{R_1 + R_2} V_{DD}$$

$$I_{DQ} = \frac{K}{2} (V_{GSQ} - V_{th})^2 = \frac{V_{GG} - V_{th}}{R_S}$$

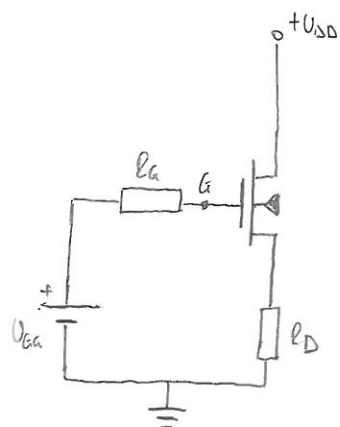
$$\Rightarrow V_{GSQ}^2 + 2 \left(\frac{1}{K \cdot R_S} - V_{th} \right) V_{GSQ} + V_{th}^2 - 2 \frac{V_{GG}}{K \cdot R_S} = 0$$

• NMOS $\Rightarrow V_{GSQ} > V_{th}$

• PMOS $\Rightarrow V_{GSQ} < V_{th}$

$$V_{DSQ} = V_{DD} - I_{DQ} (R_S + R_D)$$

3) bez otpora R_D u shemi



$$R_G = R_1 \parallel R_2$$

$$V_{GG} = \frac{R_2}{R_1 + R_2} V_{DD}$$

$$I_{DQ} = \frac{K}{2} (V_{GSQ} - V_{th})^2 = \frac{V_{GG} - V_{th}}{R_S}$$

$$\Rightarrow V_{GSQ}^2 + 2 \left(\frac{1}{K \cdot R_S} - V_{th} \right) V_{GSQ} + V_{th}^2 - 2 \frac{V_{GG}}{K \cdot R_S} = 0$$

• NMOS $\Rightarrow V_{GSQ} > V_{th}$

• PMOS $\Rightarrow V_{GSQ} < V_{th}$

$$V_{DSQ} = V_{DD} - I_{DQ} \cdot R_S$$

• određivanje dinamičkih parametara:

- kako tranzistor radi kao pojačalo samo kada je u zasićenju konstantna struja:

$$I_D = \frac{K}{2} (V_{GSQ} - V_{th})^2 \cdot (1 + \lambda V_{DS})$$

$$g_m = \left. \frac{\partial I_D}{\partial V_{GS}} \right|_Q = (1 + \lambda V_{DS}) K (V_{GSQ} - V_{th})$$

$$g_d = \left. \frac{\partial I_D}{\partial V_{DS}} \right|_Q = \lambda \frac{K}{2} (V_{GSQ} - V_{th})^2 = \lambda \cdot I_{DQ}$$

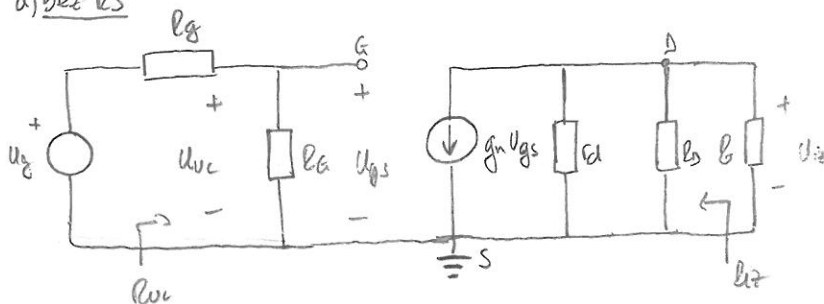
$$r_d = \frac{1}{g_d}$$

$$\mu = r_d \cdot g_m$$

• određivanje parametara tranzistora ($A_v, A_{v_g}, R_{in}, R_{iz}$)

1) Spoj zajedničkog uloda

a) bez R_s



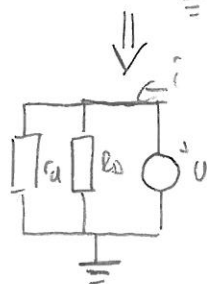
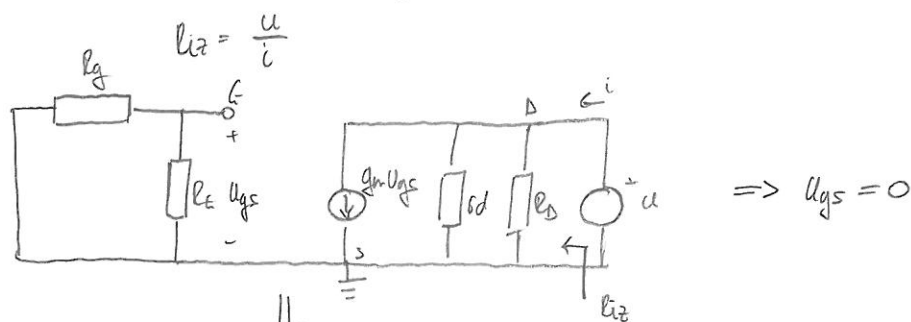
$$\left. \begin{aligned} u_{iz} &= -g_m \cdot u_{gs} \cdot r_d \parallel R_D \parallel R_L \\ u_{in} &= u_{gs} \end{aligned} \right\} A_v = \frac{u_{iz}}{u_{in}} = \frac{-g_m \cdot u_{gs} \cdot r_d \parallel R_D \parallel R_L}{u_{gs}} = -g_m \cdot r_d \parallel R_D \parallel R_L$$

$$u_{in} = \frac{R_g}{R_g + R_s} u_g$$

$$A_{v_g} = \frac{u_{iz}}{u_g} = \frac{u_{iz}}{u_{gs}} \cdot \frac{u_{gs}}{u_g} = A_v \cdot \frac{u_{gs}}{u_g} = A_v \cdot \frac{R_g}{R_g + R_s} = A_v \cdot \frac{R_g}{R_g + R_s}$$

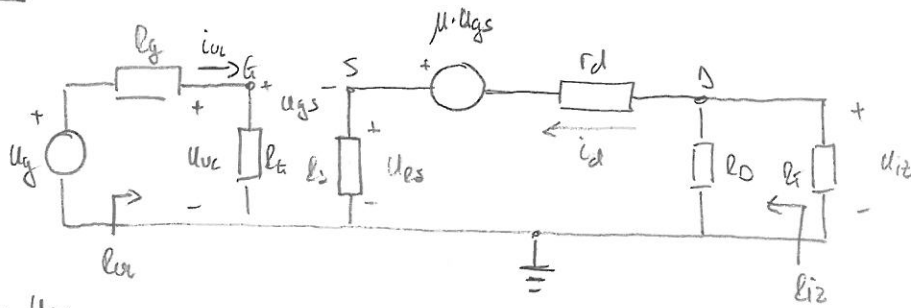
$$R_{in} = R_g$$

• Kod računanja izlaznog otpora sve nezavisne izvore ugasiš, tj. naponske izvore kratko spojiš, a strujne odspojiš. Zavisni izvori će postojati ako postoji napon ili struja o kojoj su ovisni. To isto zamijeniš naponskim izvorom u koji daje struju i . Izlazni otpor jednak je:



$$i = \frac{u}{r_d \parallel R_D} \Rightarrow R_{iz} = \frac{u}{i} = r_d \parallel R_D$$

b) Sa Rs



$$i_d = \frac{\mu \cdot u_{gs}}{r_d + r_s + r_{o1} || r_T}$$

$$u_{\mathcal{E}_S} = \text{id} \circ \mathcal{E}_S$$

$$u_{gs} = u_{uc} - u_{es} = u_{uc} - I_s r_{id} = u_{uc} - I_s \frac{\mu \cdot u_{gs}}{I_s + r_{id} + R_D || R_T}$$

$$\Rightarrow U_{ce} = U_{gs} + R_s \frac{\mu \cdot U_{gs}}{R_s + r_d + R_{o1} || R_f}$$

$$U_{12} = -i\omega \cdot L_{11} L_{22} = - \frac{L_{11} L_{22} \cdot \mu \cdot \omega_0}{L_1 + r_1 + L_{11} L_{22}}$$

$$A_v = \frac{a_{v0}}{a_{vc}} = - \frac{\mu \cdot R_D \parallel R_F}{R_S (1 + \mu) + r_d + R_D \parallel R_F}$$

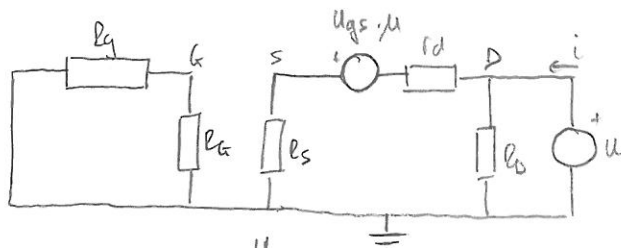
$$U_{02} = U_g \cdot \frac{R_A}{R_A + R_g}$$

$$A_{vg} = \frac{u_{12}}{u_g} = A_v \cdot \frac{u_{vc}}{u_g} = A_v \cdot \frac{R_c}{R_c + R_g}$$

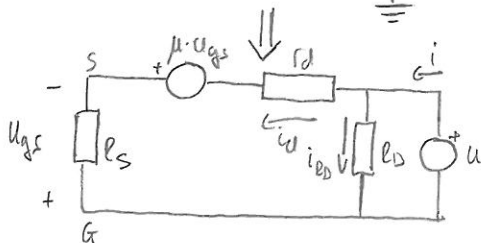
$$l_{WL} = l_G$$

- Kod računanja ključnog otpora odvojimo sve nezavisne izvore, a zavisići će postupak samo od postojećih napona ili struja o kojima su ovisni. Tražimo zamjenjivi naponski izvorom u koji daje struju i . Ključni otpor jednak je:

$$b_2 = \frac{u}{i}$$



→ G spojen na masu



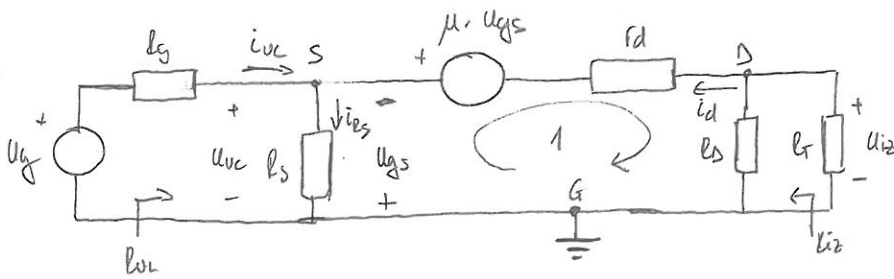
→ Ugs postojë

$$\vec{i} = i_d + i_{e_s} \quad , \quad i_d = \frac{u + \mu \cdot u_{gs}}{r_d + r_s} \quad , \quad u_{gs} = -i_d \cdot r_s$$

$$\Rightarrow i_d = \frac{u}{r_d + (1+\mu)r_s} \quad , \quad i_{E0} = \frac{U}{r_s} \Rightarrow i = u \left(\frac{1}{r_s} + \frac{1}{r_d + (1+\mu)r_s} \right)$$

$$R_T = \frac{u}{i} = \frac{u}{u \left(\frac{1}{R_S} + \frac{1}{R_D + (1+\mu)R_S} \right)} = R_S \parallel [R_D + (1+\mu)R_S]$$

2) Spoj zajedničke upravljačke elektrode



$$u_{ul} = -u_{gs}$$

• Iz petlje "1": $u_{gs} + \mu \cdot u_{gs} - i_d \cdot r_d - i_d \cdot l_r = 0$

$$(1 + \mu) u_{gs} = i_d (r_d + l_r \parallel l_r)$$

$$-(1 + \mu) u_{ul} = i_d (r_d + l_r \parallel l_r)$$

$$i_d = -\frac{(1 + \mu) \cdot u_{uc}}{r_d + l_r \parallel l_r}$$

$$u_{iz} = -i_d \cdot l_r \parallel l_r = \frac{(1 + \mu) \cdot u_{uc} \cdot l_r \parallel l_r}{r_d + l_r \parallel l_r}$$

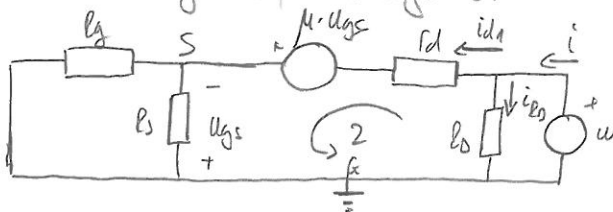
$$A_v = \frac{u_{iz}}{u_{uc}} = \frac{g_m \cdot r_d \cdot l_r \parallel l_r}{r_d + l_r \parallel l_r}$$

$$R_{ul} = \frac{u_{ul}}{i_{ul}}, \quad i_{ul} = i_{gs} - i_d, \quad i_{gs} = \frac{u_{uc}}{l_s}, \quad \Rightarrow i_{ul} = u_{uc} \left(\frac{1}{l_s} + \frac{1 + \mu}{r_d + l_r \parallel l_r} \right)$$

$$R_{ul} = \frac{1}{\frac{1}{l_s} + \frac{g_m \cdot r_d}{r_d + l_r \parallel l_r}} = l_s \parallel \frac{r_d + l_r \parallel l_r}{g_m \cdot r_d}$$

- Kod računanja izlaznog otpora sve nezavisne izvore pogasimo, a završni će postojati samo ako postoje naponi di stvara o kojoj su ovisni. Trebalo zamijeniti naponski izvor u koji daje struju i .

$$R_{iz} = \frac{u}{i}$$



→ dio struje i stvara pad napona na paraleli l_g i $l_s \rightarrow u_{gs} \neq 0$

$$i = i_{d1} + i_{ds}, \quad i_{ds} = \frac{u}{l_s}$$

• Iz petlje "2":

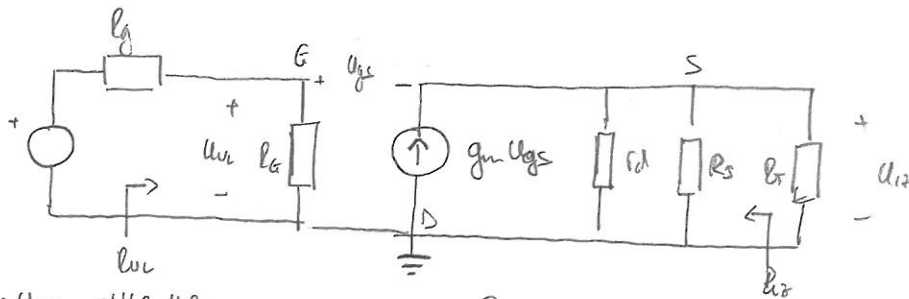
$$u = i_{d1} \cdot r_d - \mu \cdot u_{gs} + l_g \parallel l_s \cdot i_{d1} \Rightarrow i_{d1} = \frac{u}{r_d + (1 + \mu) l_s \parallel l_g}$$

$$u_{gs} = -i_{d1} \cdot l_g \parallel l_s$$

$$i = u \cdot \left(\frac{1}{l_s} + \frac{1}{r_d + (1 + \mu) l_s \parallel l_g} \right)$$

$$R_{iz} = \frac{u}{i} = \frac{1}{\frac{1}{l_s} + \frac{1}{r_d + (1 + \mu) l_s \parallel l_g}} = l_s \parallel [r_d + (1 + \mu) l_s \parallel l_g]$$

3) Spoj zajedničkog odzvala

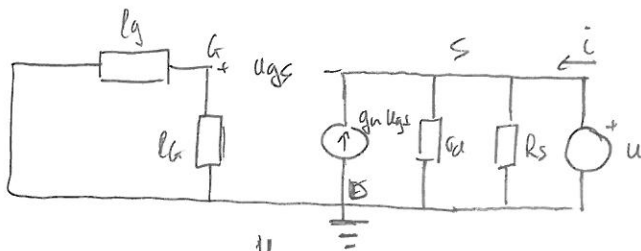


$$U_{iz} = g_m \cdot U_{gs} \cdot r_d \parallel R_s \parallel R_L$$

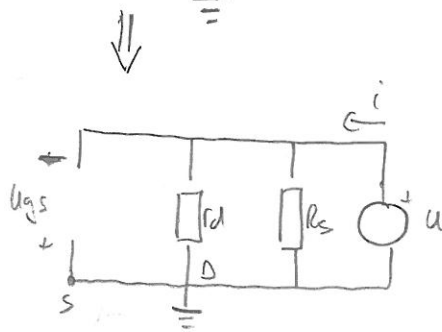
$$U_{ul} = U_{gs} + U_{iz} = U_{gs} (1 + g_m \cdot r_d \parallel R_s \parallel R_L) \quad \left. \vphantom{U_{ul}} \right\} A_v = \frac{U_{ul}}{U_{iz}} = \frac{g_m \cdot r_d \parallel R_s \parallel R_L}{1 + g_m \cdot r_d \parallel R_s \parallel R_L}$$

$$R_{ul} = \frac{U_{ul}}{i_{ul}} = R_g$$

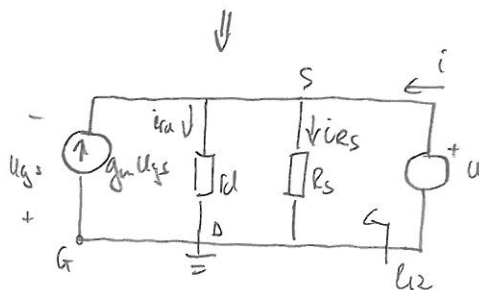
- Kod računanja relativnog otpora sve nezavisne izvore treba ugasiti; zavisni izvori će postojati ako postoji napon ili struja od koje zavise. Tražimo zamjenjivni naponski izvorom u koji daje struju i . $R_{iz} = \frac{u}{i}$



- prvo odspojimo izvor i pogledamo da li postoji napon U_{gs}



- U_{gs} postoji



$$i + g_m U_{gs} = i_{rd} + i_{es}$$

$$\Rightarrow i = i_{rd} + i_{es} - g_m U_{gs} = i_{rd} + i_{es} + g_m u$$

$$i = \frac{u}{r_d} + \frac{u}{R_s} + g_m u$$

$$R_{iz} = \frac{u}{i} = \frac{1}{\frac{1}{r_d} + \frac{1}{R_s} + g_m} = r_d \parallel R_s \parallel \frac{1}{g_m}$$

BIPOLARNI TRANZISTOR

12

• NPN tranzistor

$$-I_E < 0 \quad I_C, I_B > 0$$

$$I_E + I_C + I_B = 0$$

$$-I_E = I_{nE} + I_{pE}$$

$$I_C = I_{nC} + I_{CBO} = \underbrace{-\gamma \beta^* I_{nE}}_{\alpha} + I_{CBO}$$

$$I_B = I_{pE} + I_{R} - I_{CBO}$$

$$I_E = I_{nE} - I_{nC}$$

- faktor injekcije / efikasnost emitera : $\gamma = \frac{I_{nE}}{I_{nE} + I_{pE}} = \frac{I_{nE}}{-I_E} = \frac{1}{1 + \frac{I_{pE}}{I_{nE}}}$

- transportni faktor : $\beta^* = \frac{I_{nC}}{I_{nE}} = 1 - \frac{I_{nR}}{I_{nE}} = 1 - \frac{1}{2} \left(\frac{W_R}{L_{nB}} \right)^2$

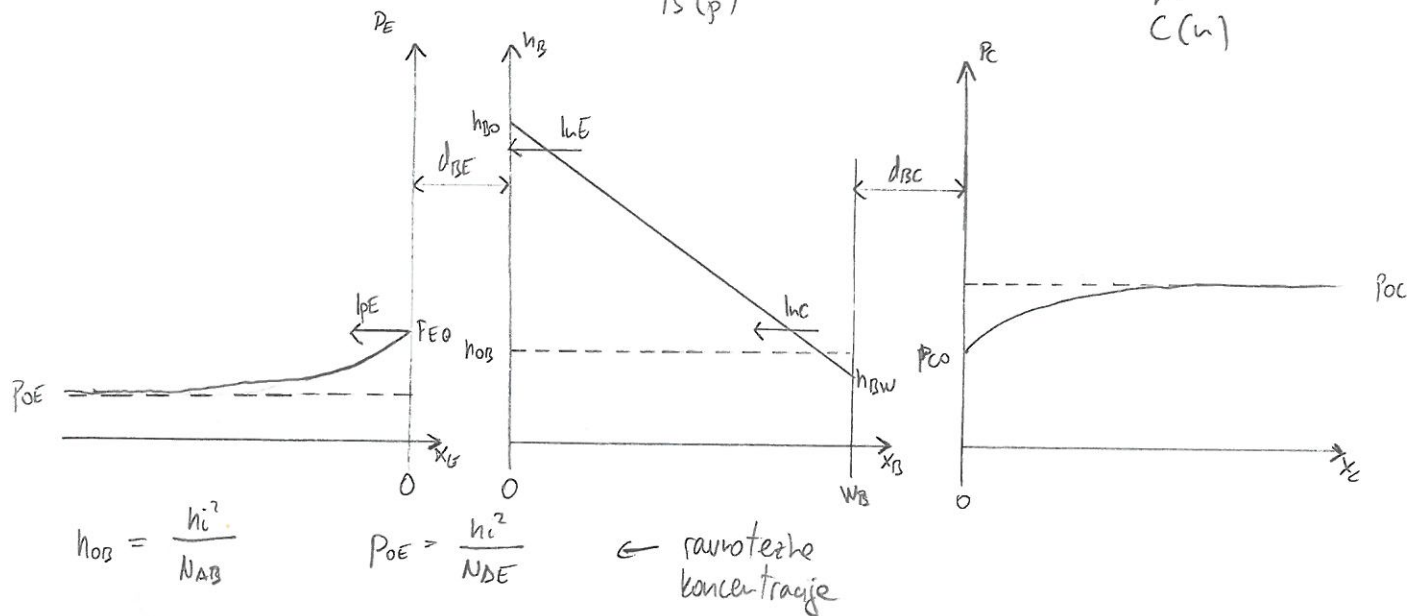
- faktor sinjlnog pojačanja : $Z_B \rightarrow \alpha = \frac{I_C}{-I_E} = \frac{I_{nC}}{I_{nE} + I_{pE}} = \frac{\beta^* I_{nE}}{I_{nE} + I_{pE}} = \beta^* \cdot \gamma$

$$Z_E \rightarrow \beta = \frac{I_C}{I_B} = \frac{\alpha}{1 - \alpha} = \frac{\gamma \cdot \beta^*}{1 - \gamma \beta^*}$$

$E(n)$

$B(p)$

$C(n)$



• rubne koncentracije :

$$n_{BO} = n_{0B} \cdot \exp\left(\frac{U_{BE}}{U_T}\right)$$

$$p_{EO} = p_{0E} \cdot \exp\left(\frac{U_{BE}}{U_T}\right)$$

$$n_{BW} = n_{0B} \exp\left(\frac{U_{BC}}{U_T}\right)$$

$$p_{CO} = p_{0C} \exp\left(\frac{U_{BC}}{U_T}\right)$$

• komponente struja:

$$I_{nE} = q S D_{nB} \cdot \frac{n_{B0}}{W_B} = \frac{Q_{nE}}{t_r}$$

$$I_{pE} = q S D_{pE} \cdot \frac{p_{E0}}{W_E}$$

$$\gamma = \frac{1}{1 + \frac{D_{pE} W_B N_{AB}}{D_{nE} W_E N_{DE}}}$$

• nakrani naboj:

$$Q_{nB} \approx q S \frac{n_{B0} W_B}{2}$$

$$\frac{Q_{nB}}{I_{nE}} = t_{tr} = \frac{W_B^2}{2 D_{nB}} \Rightarrow \text{vrijeme proleta manjinskih nosilaca kroz bazu}$$

$$I_E = q S D_{nB} \frac{n_{B0}}{W_B} \frac{W_B^2}{2 L n_B} = q S \frac{n_{B0} \cdot W_B}{2 \tau_{nB}}$$

$$\tau_{nB} = \frac{Q_{nB}}{I_E} \rightarrow \text{vrijeme života manjinskih elektrona u bazi}$$

• PNP tranzistor

$$\bullet I_E > 0 \quad I_C, I_B < 0$$

$$I_E = I_{pE} + I_{nE}$$

$$I_C = -I_{pC} + I_{CBO} = -\alpha I_E + I_{CBO}$$

$$I_R = I_{pE} - I_{pC}$$

$$I_B = -I_{nE} - I_R - I_{CBO}$$

- Faktor injekcije: $\gamma = \frac{I_{pE}}{I_{pE} + I_{nE}} = \frac{I_{pE}}{I_E} = \frac{1}{1 + \frac{D_{nE} W_B N_{AB}}{D_{pE} L n_E N_{AE}}}$

- transportni faktor: $\beta^* = \frac{I_{pC}}{I_{pE}} = 1 - \frac{I_R}{I_E} = 1 - \frac{1}{2} \left(\frac{W_B}{L_{pB}} \right)^2$

- naboj: $Q_{pB} = q S \frac{p_{B0} \cdot W_B}{2}$

$$I_{pE} = q S D_{pE} \frac{p_{E0}}{W_E}$$

$$I_R = q S \frac{p_{B0} W_B}{2 \tau_{pB}}$$

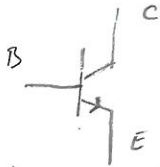
$$\frac{Q_{pB}}{I_{pE}} = \frac{W_B^2}{2 D_{pB}} = t_{tr}$$

$$\frac{Q_{pB}}{I_R} = \tau_{pB}$$

SKLOPOVI S BIPOLARNIM TRANZISTORIMA

(14)

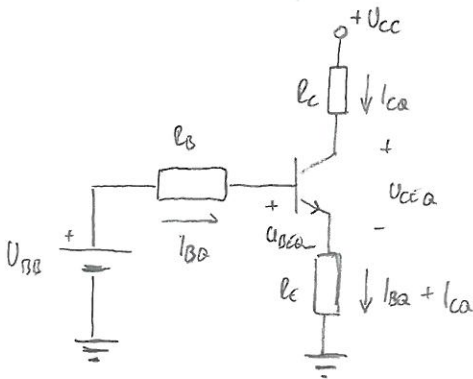
- spojevi pojačala: → spoj zajedničkog emitera
→ spoj zajedničke baze
→ spoj zajedničkog kolektora
- da bi odredili koji spoj imamo pogledano na što su nam spojeni ulaz i izlaz pojačala, što nam ostane to je zajedničko



- NPN → strelica prema van
- PNP → strelica prema unutra

- određivanje statičke radne točke:
- dva slučaja:

1) sa otporom R_c u shemi



$$R_B = R_1 \parallel R_2$$

$$U_{BB} = \frac{R_2}{R_1 + R_2} U_{CC}$$

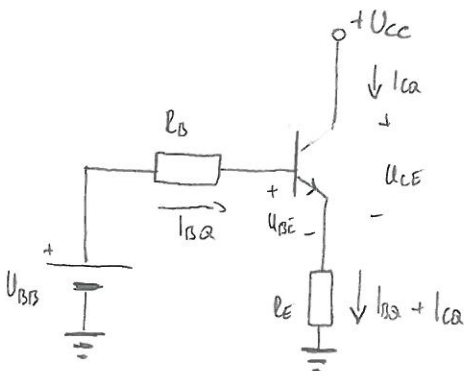
$$U_{BEQ} = U_T$$

$$I_{BQ} = \frac{U_{BB} - U_{BEQ}}{R_B + (1 + \beta) R_E}$$

$$I_{CQ} = \beta \cdot I_{BQ}$$

$$U_{CEQ} = U_{CC} - R_c \cdot I_{CQ} - R_E (I_{BQ} + I_{CQ})$$

2) bez otpora R_c u shemi



$$R_B = R_1 \parallel R_2$$

$$U_{BB} = \frac{R_2}{R_1 + R_2} U_{CC}$$

$$U_{BEQ} = U_T$$

$$I_{BQ} = \frac{U_{BB} - U_{BEQ}}{R_B + (1 + \beta) R_E}$$

$$I_{CQ} = \beta \cdot I_{BQ}$$

$$U_{CEQ} = U_{CC} - R_E (I_{BQ} + I_{CQ})$$

- određivanje dinamičkih parametara:

$$h_{fe} \approx \beta$$

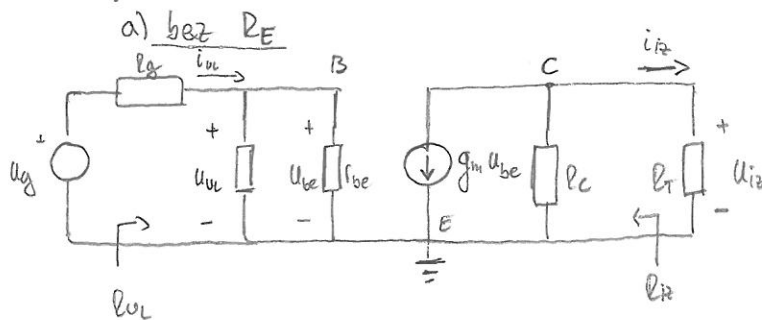
$$r_{be} = \frac{U_T}{I_{CQ}}$$

$$r_{ce} = \frac{U_{CEQ} + U_A}{I_{CQ}}$$

$$g_m = \frac{h_{fe}}{r_{be}}$$

• određivanje parametara tranzistora:

1) zajednički emiter



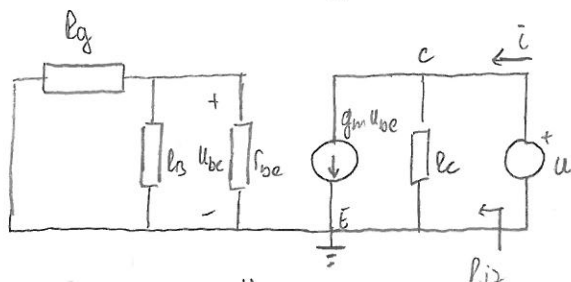
$$\left. \begin{aligned} u_{iz} &= -g_m \cdot u_{be} \cdot R_C || R_L \\ u_{ul} &= u_{be} \end{aligned} \right\} A_v = \frac{u_{iz}}{u_{ul}} = -g_m \cdot R_C || R_L$$

$$\left. \begin{aligned} i_{iz} &= \frac{u_{iz}}{R_L} \\ i_{ul} &= \frac{u_{ul}}{R_B || R_E} \end{aligned} \right\} A_i = \frac{i_{iz}}{i_{ul}} = \frac{\frac{u_{iz}}{R_L}}{\frac{u_{ul}}{R_B || R_E}} = A_v \cdot \frac{R_B || R_E}{R_L}$$

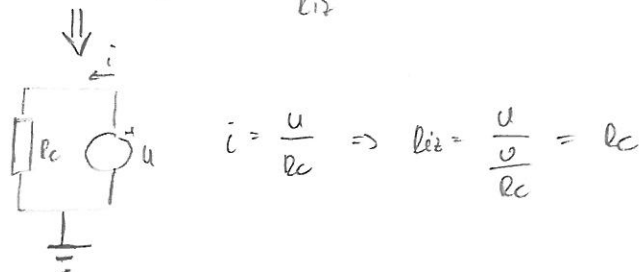
$$u_{ul} = u_g \cdot \frac{R_B || R_E}{R_B || R_E + R_g} \Rightarrow A_{vg} = \frac{u_{iz}}{u_g} = \frac{u_{iz}}{u_{ul}} \cdot \frac{u_{ul}}{u_g} = A_v \cdot \frac{u_{ul}}{u_g} = A_v \cdot \frac{R_B || R_E}{R_B || R_E + R_g}$$

$$R_{ul} = R_B || R_E$$

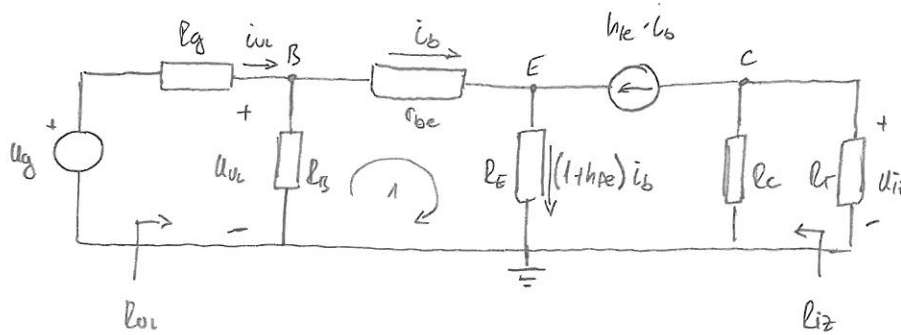
• za računanje izlaznog otpora sve nezavisne izvore ugasio, a zavisni će postojati samo ako postoje naponi ili struje o kojima su ovisni. Trebalo bi zatvoriti naponskim izvorom u koji daje struju i : $i_{iz} = \frac{u}{R_C}$



• iz slike vidimo da je $u_{be} = 0$



b) sa R_E



$$\left. \begin{aligned} U_{iz} &= -h_{fe} \cdot i_b \cdot R_c \parallel R_L \\ \text{iz putuje "1":} \\ U_{be} &= i_{be} \cdot r_{be} + i_b (1+h_{fe}) R_E \end{aligned} \right\} A_v = \frac{U_{iz}}{U_{be}} = - \frac{h_{fe} \cdot R_c \parallel R_L}{r_{be} + (1+h_{fe}) R_E}$$

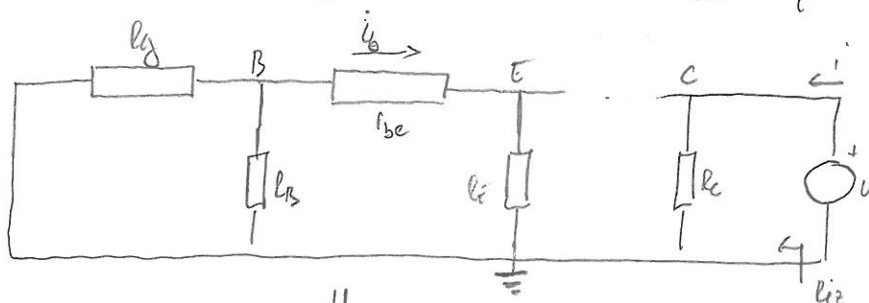
$$R_{be} = \frac{U_{be}}{i_{be}}, \quad i_{be} = i_B + i_{RB}, \quad i_{RB} = \frac{U_{be}}{R_B}, \quad i_B = \frac{U_{be}}{r_{be} + (1+h_{fe}) R_E}$$

$$R_{be} = \frac{U_{be}}{i_{be} \left(\frac{1}{R_B} + \frac{1}{r_{be} + (1+h_{fe}) R_E} \right)} = R_B \parallel \underbrace{\left[r_{be} + (1+h_{fe}) R_E \right]}_{R'_{be}}$$

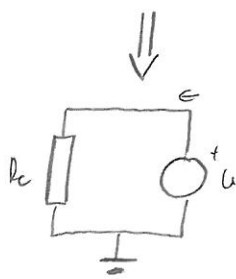
$$\left. \begin{aligned} i_{iz} &= \frac{U_{iz}}{R_L} \\ a_v &= \frac{U_{be}}{R_{be}} \end{aligned} \right\} A_i = \frac{i_{iz}}{i_{be}} = \frac{\frac{U_{iz}}{R_L}}{\frac{U_{be}}{R_{be}}} = A_v \cdot \frac{R_{be}}{R_L}$$

$$U_{be} = U_g \cdot \frac{R_{be}}{R_{be} + R_g} \Rightarrow A_{vg} = \frac{U_{iz}}{U_g} = \frac{U_{iz}}{U_g} \cdot \frac{U_{be}}{U_{be}} = A_v \cdot \frac{U_{be}}{U_g} = A_v \cdot \frac{R_{be}}{R_{be} + R_g}$$

- Za računanje izlaznog otpora odspojimo sve nezavisne izvore, a zavisni će postojati samo ako postoje izvori struje o kojoj su ovisni. Trećio zavisjenih naponskim izvorom o koji daje struju i : $R_{iz} = \frac{U}{i}$



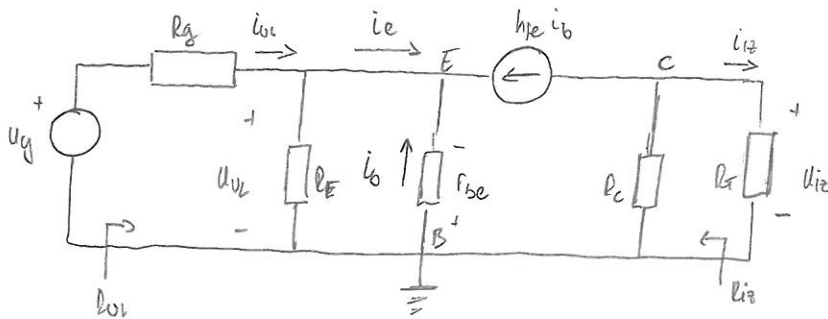
• vidno da je $i_b = 0$



$$i = \frac{U}{R_c} \Rightarrow R_{iz} = \frac{U}{\frac{U}{R_c}} = R_c$$

2) Zajednička baza

(14)



$$\left. \begin{aligned} u_{i2} &= -h_{fe} \cdot i_b \cdot R_C \parallel R_L \\ u_{u1} &= -i_b \cdot R_E \end{aligned} \right\} A_v = \frac{u_{i2}}{u_{u1}} = h_{fe} \cdot \frac{R_C \parallel R_L}{R_E}$$

$$R_{u1} = \frac{u_{u1}}{i_{u1}} \quad , \quad i_{u1} = i_e + i_{bE} \quad , \quad i_{bE} = \frac{u_{u1}}{R_E} \quad , \quad i_b = -\frac{u_{u1}}{R_E}$$

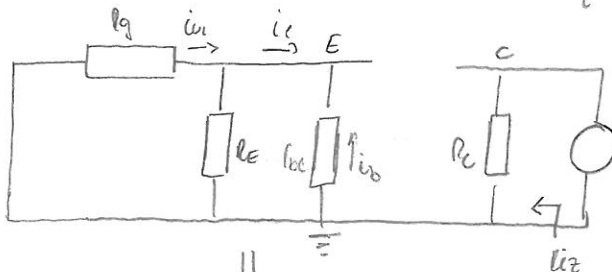
$$i_e + i_b + i_b h_{fe} = 0 \Rightarrow i_e = -i_b (1 + h_{fe}) = \frac{u_{u1}}{R_E} (1 + h_{fe})$$

$$R_{u1} = R_E \left[\frac{1}{R_E} + \frac{1}{\frac{R_E}{1 + h_{fe}}} \right] \Rightarrow R_{u1} = \frac{1}{\frac{1}{R_E} + \frac{1}{\frac{R_E}{1 + h_{fe}}}} = R_E \parallel \frac{R_E}{1 + h_{fe}}$$

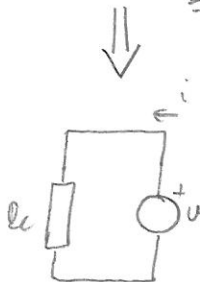
$$\left. \begin{aligned} i_{i2} &= \frac{u_{i2}}{R_L} \\ i_{u1} &= \frac{u_{u1}}{R_{u1}} \end{aligned} \right\} A_i = \frac{i_{i2}}{i_{u1}} = \frac{u_{i2} \cdot R_{u1}}{u_{u1} \cdot R_L} = A_v \cdot \frac{R_{u1}}{R_L}$$

$$u_{u1} = u_g \cdot \frac{R_{u1}}{R_{u1} + R_g} \Rightarrow A_{vg} = \frac{u_{i2}}{u_g} = \frac{u_{i2}}{u_{u1}} \cdot \frac{u_{u1}}{u_g} = A_v \cdot \frac{R_{u1}}{R_{u1} + R_g}$$

• Za računanje naponskog otpora sve nezavisne izvore odspjimo, a zavisni će su ovisni. Treba zamjeniti naponskim izvorom u koji daje struju i : $i_{i2} = \frac{u}{R_L}$



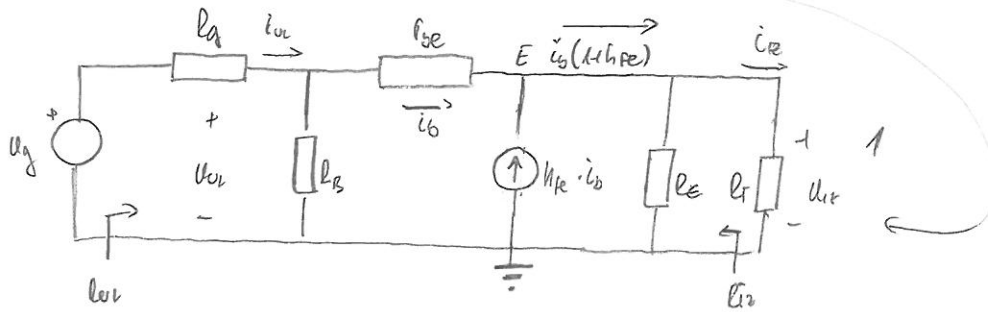
• vidimo da je $i_b = 0$



$$i = \frac{u}{R_L} \Rightarrow R_{i2} = \frac{u}{i} - R_L$$

3) zajednički kolektor

18



$$u_{L2} = i_b (1 + h_{FE}) \cdot R_E \parallel R_L$$

• iz pethie "1":

$$u_{L1} = i_b [r_{be} + (1 + h_{FE}) R_E \parallel R_L]$$

$$A_V = \frac{u_{L2}}{u_{L1}} = \frac{(1 + h_{FE}) R_E \parallel R_L}{r_{be} + (1 + h_{FE}) R_E \parallel R_L}$$

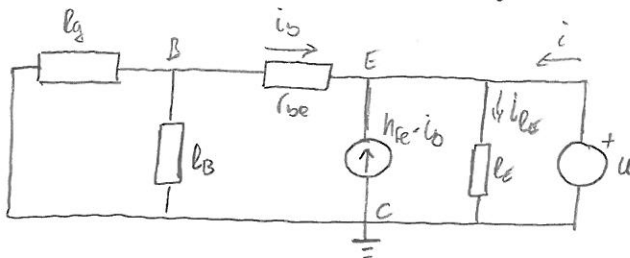
$$R_{L1} = \frac{u_{L1}}{i_{L1}}, \quad i_{L1} = i_b + i_{eB}, \quad i_{eB} = \frac{u_{L1}}{R_E}, \quad i_b = \frac{u_{L1}}{r_{be} + (1 + h_{FE}) R_E \parallel R_L}$$

$$R_{L1} = \frac{u_{L1}}{i_{L1} \left[\frac{1}{R_E} + \frac{1}{r_{be} + (1 + h_{FE}) R_E \parallel R_L} \right]} = R_E \parallel [r_{be} + (1 + h_{FE}) R_E \parallel R_L]$$

$$\left. \begin{aligned} i_{L2} &= \frac{u_{L2}}{R_L} \\ i_{L1} &= \frac{u_{L1}}{R_{L1}} \end{aligned} \right\} A_1 = \frac{i_{L2}}{i_{L1}} = \frac{u_{L2} \cdot R_{L1}}{u_{L1} \cdot R_L} = A_V \cdot \frac{R_{L1}}{R_L}$$

$$u_{L1} = u_g - \frac{R_{L1}}{R_g + R_{L1}} \Rightarrow A_{Vg} = \frac{u_{L2}}{u_g} = \frac{u_{L2}}{u_{L1}} \cdot \frac{u_{L1}}{u_g} = A_V \cdot \frac{R_{L1}}{R_g + R_{L1}}$$

• Za računanje faktora otpora odspjina sve nezavisne izvore, a zavisi ce postupak ako postoje struja i_b napr o kopa su ovisni. Trebalo zamijeniti naponskim izvorom u koji daje struju i: $R_{L1} = \frac{u}{i}$



• vidno da je $i_b \neq 0$

$$\left. \begin{aligned} i_c &= i_{eE} - i_b - i_{b h_{FE}} = i_{eE} - i_b (1 + h_{FE}), \quad i_{eE} = \frac{u}{R_E} \\ u &= -i_b (r_{be} + R_g \parallel R_B) \Rightarrow i_b = -\frac{u}{r_{be} + R_g \parallel R_B} \end{aligned} \right\} i = u \left(\frac{1}{R_E} + \frac{1 + h_{FE}}{r_{be} + R_g \parallel R_B} \right)$$

$$R_{L2} = \frac{u}{i} = \frac{1}{\frac{1}{R_E} + \frac{1 + h_{FE}}{r_{be} + R_g \parallel R_B}} = R_E \parallel \frac{r_{be} + R_g \parallel R_B}{1 + h_{FE}}$$

• dodatno:

- kod spoja zajedničkog emitera oba su pojačanja, naponsko i strujno, negativna, a kod preostala dva spoja pozitivna
- po iznosu naponska pojačanja spoja ZE i ZB su velika i međusobno su jednaka
- naponsko pojačanje spoja ZC samo je malo manje od 1
- od sva tri spoja jedino pojačalo u spoju ZE ima oba pojačanja po iznosu veća od 1 (red iznosa tih pojačanja je tipično 100)
- pojačalo u spoju ZB ima strujno pojačanje manje od 1, a pojačalo u spoju ZE naponsko pojačanje manje od 1
- ulazni otpori u spoju ZB tipični su oko 10Ω , u spoju ZE oko $1k\Omega$, a u spoju ZC oko $100k\Omega$
- u pojačalima u spoju ZE i ZB izlazni otpor je R_C (veličine kilooma), u pojačalu ZC izlazni otpor je mali (oko 10Ω)

DIFERENCIJSKO POJAČALO

- zajednički signal: $u_z = \frac{u_{g1} + u_{g2}}{2}$ (istofazni signal)
 - diferencijalni signal: $u_d = u_{g2} - u_{g1}$ (protufazni signal)
- $$\left. \begin{array}{l} u_{g1} = u_z - \frac{u_d}{2} \\ u_{g2} = u_z + \frac{u_d}{2} \end{array} \right\}$$

- za dobro pojačalo: $A_{vd} \gg A_{vz} \propto \frac{1}{R_E}$

$$A_{vz1} = \frac{u_{z1}}{u_z} = \frac{-h_{ie} \cdot R_{C1}}{R_{g1} + r_{be1} + 2R_E(1+h_{ie})} \quad (-)$$

$$A_{vz2} = \frac{u_{z2}}{u_z} = \frac{-h_{ie} \cdot R_{C2}}{R_{g2} + r_{be2} + 2R_E(1+h_{ie})} \quad (-)$$

$$A_{vd1} = \frac{u_{d1}}{u_d} = \frac{+h_{ie} R_{C1}}{2(R_{g1} + r_{be1})} \quad (-)$$

$$A_{vd2} = \frac{u_{d2}}{u_d} = \frac{-h_{ie} \cdot R_{C2}}{2(R_{g2} + r_{be2})} \quad (+)$$

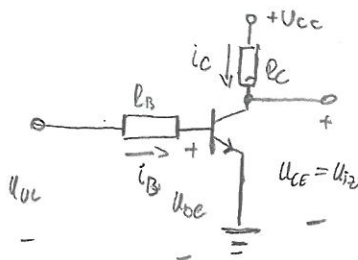
$$A_{vz} = A_{vz2} - A_{vz1}$$

$$A_{vd} = A_{vd2} - A_{vd1}$$

BIPOLARNI TRANZISTOR KAO SKLOPKA

20

- konstrui se spoj zajedničkog emitera



$$I_B = \frac{U_{in} - U_{BE}}{R_B}$$

$$U_{out} = U_{CE} = U_{CC} - R_C \cdot I_C$$

- kada je U_{in} negativniji od 0,5V radi se zanemarljivo malim strujama, tada je zanemarljiv i pad napona na R_C i izlazni napon $U_{out} = U_{CE} = U_{CC}$ (zapriranje)

\Rightarrow ISKLJUČENA SKLOPKA

- porastom napona U_{in} iznad 0,5V tranzistor počne voditi i ulazi u NAP; uz veće ulazne napone U_{in} napon $U_{BE} \approx 0,7V$; porastom napona U_{in} raste struja I_B , s njom raste i struja I_C a njenim porastom pada $U_{CE} = U_{out}$
- U_{out} se može smanjiti do $U_{CE_{zas}}$, kolektorska struja tada postigne maksimalnu vrijednost:

$$I_{C_{zas}} = \frac{U_{CC} - U_{CE_{zas}}}{R_C}$$

- $U_{CE_{zas}}$ je tipično između 0,1 i 0,3 V, u području zasićenja struja baze mora biti:

$$I_{B_{zas}} \geq \frac{I_{C_{zas}}}{\beta}$$

pa ćemo struju baze $I_{B_{zas}}$ i dalje određuje ulazni krug sklopa

$$I_{B_{zas}} = \frac{U_{in} - U_{BE_{zas}}}{R_B}$$

$$\Rightarrow U_{BE_{zas}} \approx \text{od } 0,7 \text{ do } 0,8 V$$

\Rightarrow UKLJUČENA SKLOPKA

• IDEALNO pojačalo:

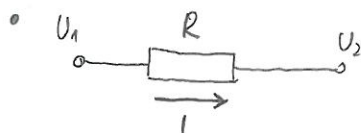
$$1) R_{OL} = \infty \Rightarrow I_{OP} = 0$$

$$2) A_{VOL} = \infty \Rightarrow U_{IZ} = A_{VOL} (U_+ - U_-) \Rightarrow U_+ - U_- = \frac{U_{IZ}}{A_{VOL}}$$

$$\boxed{U_- = U_+} \rightarrow \text{prividni kratak spoj}$$

$$3) I_{IZ} = 0$$

NE PIŠEMO JEDNAČICE ZA IZLAZNI ČVOR.

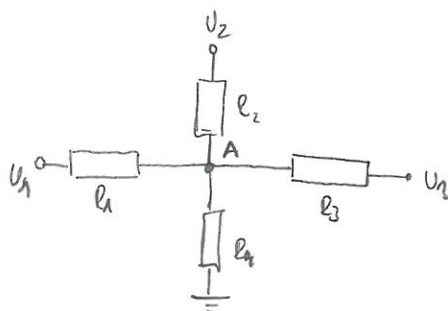


$$I = \frac{U_1 - U_2}{R}$$

• potencijal čvorova:

- napon čvora puta zbroj svih vodljivosti koje ulaze u taj čvor minus naponi susjednih čvorova puta vodljivost ravnodužno ta dva čvora:

(Pr)



$$U_A \left(\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} + \frac{1}{R_4} \right) - \frac{U_1}{R_1} - \frac{U_2}{R_2} - \frac{U_3}{R_3} - \frac{0}{R_4} = 0$$

DODATAK:

- crtanje statičkog i dinamičkog radnog pravca:

- x os $\rightarrow U_{CE}$

- y os $\rightarrow I_C$

- statički radni pravac određen je jednačinom:

$$U_{CE} = U_{CC} - (R_C + R_E) I_C$$

\rightarrow za $I_C = 0$ i $U_{CE} = 0$ dobijemo presjecište sa osima

\rightarrow na njemu označimo statičku radnu tačku $Q(U_{CEQ}, I_{CQ})$

- dinamički radni pravac nacrtano tako da nadamo udaljenost njegovih presjecista od koordinata tačke Q , te udaljenosti su ΔU_{CE} i ΔI_C koje smo odredili iz nadonjesne sheme

- maksimal. hod napona je manji od dva raspona po kojima radna tačka može šetati po DEP-u. Ti rasponi su U_{CEQ} i ΔU_{CE} , što je i za struju