

# Unveiling Cosmic Reionisation: Improvements in Understanding Interferometric Systematics

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NOVEMBER, 2024

A THESIS SUBMITTED IN COMPLETE FULFILMENT  
OF THE REQUIREMENTS FOR THE DEGREE OF

DOCTOR OF PHILOSOPHY  
PHYSICS  
THE UNIVERSITY OF MELBOURNE

*“The story so far:  
In the beginning the Universe was created.  
This has made a lot of people very angry and been widely regarded as a bad move.”*

— Douglas Adams, *The Restaurant at the End of the Universe*

## Abstract

The Epoch of Reionisation (EoR) spans a critical era in the Universe’s past, encompassing the ignition of the first luminous objects which triggered a final phase transition from neutral to its current completely ionised state. Largely unexplored and as of yet undetected, measurements of the EoR will encode a multitude of astrophysical and cosmological tracers, which promise to aid in the unravelling of mysteries surrounding the birth of the first stars and galaxies, their nature, and their influence on the evolution of the Universe. The 21-cm signal from neutral Hydrogen can be leveraged to tomographically map large cosmological volumes, tracing the ionisation morphology of the early Universe. Low-frequency radio interferometers, such as the Murchison Widefield Array (MWA), observe large cosmological volumes and possess the theoretical sensitivity to make a statistical detection of the 21-cm EoR signal. Astrophysical and terrestrial foregrounds dominate the EoR signal by factors exceeding five orders-of-magnitudes, and couple with complex instrumental systematics to impede a detection. Unprecedented precision is required at all levels to unveil the EoR signal; from instrumental understanding to astrophysical modelling. Current measured upper-limits are a couple of orders-of-magnitude higher than cutting-edge EoR models. A first EoR detection is on the horizon.

In this thesis we explore the impact of complex interferometric systematics, in particular primary beam models, on a future EoR detection. We design and implement an experiment to measure the all-sky dual-polarised beampatterns of 14 MWA receiving elements (tiles), using communication satellites. Unexpected inter-tile side-lobe variations were measured at a  $\sim 10\%$  level, attributed to a variety of environmental factors. We develop a physically motivated model of beam deformation, and explore their impact on an EoR power spectrum detection and MWA polarisation science. Our simulations indicate that including measured instrumental beams into calibration frameworks could reduce foreground coupling into EoR sensitive measurement modes by factors exceeding  $\sim 1000$ , potentially putting a first EoR detection within grasp. We outline the steps required to make our deformed beam calibration framework applicable to measured data, and discuss its impact on the next-generation SKA-Low observatory.

## **Declaration**

This page certifies that:

- This thesis contains only original work towards a Doctor of Philosophy, except where indicated in the preface
- Due acknowledgement has been made in the text to all other material used
- This thesis is fewer than 100 000 words in length, exclusive of tables, figures, bibliographies, and appendices

Aman Chokshi

## Preface

Here and henceforth, "the author" refers to Aman Chokshi, the author of this thesis. This thesis is an original work by the author reporting research done alone or in collaboration with other authors. This section provides a chapter-by-chapter summary of the author's contributions and the publication status of all material.

**Chapter 1** is an introduction to the history of the Universe, and the Epoch of Reionisation. It is an original work of the author, with editing from N. Barry and R. Webster, and has not and will not be submitted for publication.

**Chapter 2** is an introduction to low-frequency interferometry, and the Murchison Wide-field Array. It is an original work of the author, with editing from N. Barry and R. Webster, and has not and will not be submitted for publication.

**Chapter 3** is based on the published work *A. Chokshi, J. L. B. Line, N. Barry, D. Ung, D. Kenney, A. McPhail, A. Williams, R. L. Webster, Monthly Notices of the Royal Astronomical Society, Volume 502, Issue 2, April 2021, Pages 1990–2004*. It was written primarily by the author, with scientific input and editing from the co-authors. The author was responsible for data acquisition and data analyses. All figures and tables are the work of the author.

**Chapter 4** is based on the published work *A. Chokshi, N. Barry, J. L. B. Line, C. H. Jordan, B. Pindor, R. L. Webster, Monthly Notices of the Royal Astronomical Society, Volume 534, Issue 3, November 2024, Pages 2475–2484*. It was written primarily by the author, with scientific input and editing from the co-authors. The author was responsible for generating the simulations and data analyses. All figures and tables are the work of the author.

**Chapter 5** is based on a draft of work to be published *A. Chokshi, N. Barry, B. Pindor, J. L. B. Line, C. J. Riseley, X. Zhang, R. L. Webster, Publications of the Astronomical Society of Australia*. It was written primarily by the author, with scientific input and editing from the co-authors. The author was responsible for generating the simulations and data analyses. All figures and tables are the work of the author.

**Chapter 6** summarises the work in the previous chapters. It includes some exploratory future directions for the work in this thesis. It was written by the author, with editing from N. Barry and R. Webster.

The author also contributed to eleven other publications during their PhD candidature, which are not included for examination in this thesis but are listed here for completeness:

- *Prabhu, K., Raghunathan, S., Millea, M., ... Chokshi, A., ... et al. [SPT Collaboration], Testing the  $\Lambda$ CDM Cosmological Model with Forthcoming Measurements of the Cosmic Microwave Background with SPT-3G, The Astrophysical Journal, Volume 973, Number 1, September 2024.*
- *Gupta, A., Trott, C. M., ... Chokshi, A. [12 authors], MOSEL survey: Spatially offset Lyman-continuum emission in a new emitter at  $z=3.088$ , The Astrophysical Journal, Volume 973, Number 2, Septemer 2024.*
- *Coerver, A., Zebrowski, J. A., Takakura, S., ... Chokshi, A., ... et al. [SPT Collaboration], Measurement and Modeling of Polarized Atmosphere at the South Pole with SPT-3G, arXiv:2407.20579, July 2024*
- *C. J. Riseley, E. Bonnassieux, T. Vernstrom, T. J. Galvin, A. Chokshi, ... et al [24 authors], Radio fossils, relics, and haloes in Abell 3266: cluster archaeology with ASKAP-EMU and the ATCA, Monthly Notices of the Royal Astronomical Society, Volume 515, Issue 2, September 2022, Pages 1871–1896.*
- *N. Barry, A. Chokshi, The Role of the Instrumental Response in 21 cm Epoch of Reionization Power Spectrum Gridding Analyses, The Astrophysical Journal, Volume 929, Number 1, April 2022.*
- *M. Rahimi, B. Pindor, ... A. Chokshi, ... et al. [31 authors], Epoch of reionization power spectrum limits from Murchison Widefield Array data targeted at EoR1 field, Monthly Notices of the Royal Astronomical Society, Volume 508, Issue 4, December 2021, Pages 5954–5971.*
- *C. M. Trott, C. H. Jordan, ... A. Chokshi, ... et al. [32 authors], Constraining the 21 cm brightness temperature of the IGM at  $z = 6.6$  around LAEs with the murchison widefield array, Monthly Notices of the Royal Astronomical Society, Volume 507, Issue 1, October 2021, Pages 772–780.*
- *S. Yoshiura, B. Pindor, ... A. Chokshi, ... et al. [32 authors], A new MWA limit on the 21 cm power spectrum at redshifts 13–17, Monthly Notices of the Royal Astronomical Society, Volume 505, Issue 4, August 2021, Pages 4775–4790.*
- *A. Chokshi, J. L. B. Line, B. McKinley, EMBERS: Experimental Measurement of BEam Responses with Satellites, The Journal of Open Source Software, November 2020*
- *Z. Zheng, J. C. Pober, ... A. Chokshi, ... et al. [30 authors], The impact of tandem redundant/sky-based calibration in MWA Phase II data analysis, Publications of the Astronomical Society of Australia, November 2020*

- *C. M. Trott, C. H. Jordan, ... A. Chokshi, ... et al. [36 authors], Deep multiredshift limits on Epoch of Reionization 21 cm power spectra from four seasons of Murchison Widefield Array observations, Monthly Notices of the Royal Astronomical Society, Volume 493, Issue 4, April 2020, Pages 4711–4727.*

The author was supported by the Melbourne Research Scholarship from the University of Melbourne, which included a fee offset . This research was supported by the Australian Research Council Centre of Excellence for All Sky Astrophysics in 3 Dimensions (ASTRO 3D), through project number CE170100013. This work was supported by resources awarded under Astronomy Australia Ltd’s merit allocation scheme on the OzSTAR national facility at Swinburne University of Technology. OzSTAR is funded by Swinburne University of Technology and the National Collaborative Research Infrastructure Strategy (NCRIS). This work was supported by resources provided by the Pawsey Supercomputing Centre with funding from the Australian Government and the Government of Western Australia. This scientific work makes use of the Inyarrimanka Ilgari Bunda Murchison Radio-Astronomy Observatory, operated by CSIRO. We acknowledge the Wajarri Yamatji people as the traditional owners of the Observatory site.

## Acknowledgments

*I begin by acknowledging the Traditional Owners of the land which has been my home over the past 5 years, and where the majority of this work was performed; the Wurundjeri and Boon Wurrung people of the Kulin Nation, and pay my respects Elders past and present.*

The past five years have been a wonderful journey of both personal and scientific growth. It wouldn't have been possible without the support and encouragement of so many of you.

First, I must thank Rachel Webster for her unwavering support and encouragement. She introduced me to the frustrating yet endlessly fascinating field of interferometry, which I've grown to love. She has given me a massive and appreciated amount of freedom and space to grow.

A massive thank you to the most supportive group of postdocs ever – Nichole, Jack and Bart. I arrived clueless, and have learnt so incredibly much from all of you, none of this would have been possible without each one of you. Thank you for constantly indulging my questions, and being the best mentors and colleagues one could hope for.

I'm so grateful to have been a part of the MWA EoR collaboration. Thank you Ronniy, Ruby, Mike, Shintaro, Miguel, Cath and everyone else, for giving me the space to ask and re-ask silly questions till I understood, and never ever feel uncomfortable doing so.

To all the usual suspects on the astro floor: thank you for the curiosity, the friendships, and all the fun times together. Thank you Michele, Christian, Katie and Andrew for your mentoring, encouragement, and interesting chats.

Thank you Pete and Susanne, for welcoming me into your beautiful home.

Thank you, Bethan, for your friendship and the countless happy memories we've made during my time in Australia.

To my loving parents, thank you so much for nurturing curiosity and giving me and Avani so much freedom. For taking us adventuring and shooting-star watching. And thank you Avani, for being the best sister ever. I know you've all always been there for me, no matter what.

Finally, Erin – I'm so happy that we've found each other, and can't wait for our many future adventures together.

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1       *Universe shadowed;  
2        starry embers coalesce,  
3        spark curious dreams.*

4       Aman, 2020, Haiku

## CHAPTER 1

### Introduction

5       Across recorded time, humans have gazed up at the night sky and wondered about  
6       their place in the stars. Our curiosity has driven a massive evolution in our understand-  
7       ing of the Universe, teasing from physical observations insights spanning the structure  
8       of our Solar System to the very edges of the observable. This thesis represents my small  
9       contribution to this growing picture.

10      The finite nature of the speed of light provides an extraordinary opportunity to peer  
11     back into the past, enabling a study into the origin of our Universe. Early observations  
12     of galaxies outside the Milky Way revealed that the majority were receding away from  
13     us ([Hubble, 1929](#)). In fact, [Hubble \(1929\)](#) also showed that recessional velocities were  
14     directly proportional to their distance from us, inarguably establishing the fact that the  
15     Universe is expanding. Lemaître realised that the Universe must have been smaller at  
16     earlier times, which logically meant that there would exist a moment in the past where  
17     the entire Universe was compressed into a singularity ([Lemaître, 1927](#)) – an idea which  
18     marks the birth of Big Bang Cosmology.

19      This chapter presents a brief history of the Universe, laying the foundation and pre-  
20     senting context for my research. It explores how neutral Hydrogen, the most abundant  
21     element in the Universe, can be used as a cosmological tracer to illuminate a critical  
22     epoch of the Universe’s past which was predominantly dark. Within this darkness pri-  
23     mordial matter over-densities coalesced gravitationally, resulting in the ignition of the  
24     first luminous objects in our Universe. The resulting intense radiation triggered a uni-  
25     versal phase transition of matter from neutral to its current completely ionized state.  
26     The Epoch of Reionisation (EoR) spans this critical era, encoding within its light a mul-  
27     titude of astrophysical & cosmological tracers which promise to aid in the unravelling  
28     of mysteries surrounding the birth of the first stars and galaxies, their nature, and their  
29     influence on the evolution of the Universe.

30      Chapter 2 discusses low-frequency interferometry, a technique used to build flexible  
31     telescopes capable of precisely surveying large cosmological volumes. The rest of this  
32     thesis presents new experiments and analysis techniques which improve the prospects  
33     of a first detection of cosmological signals from the Epoch of Reionisation.

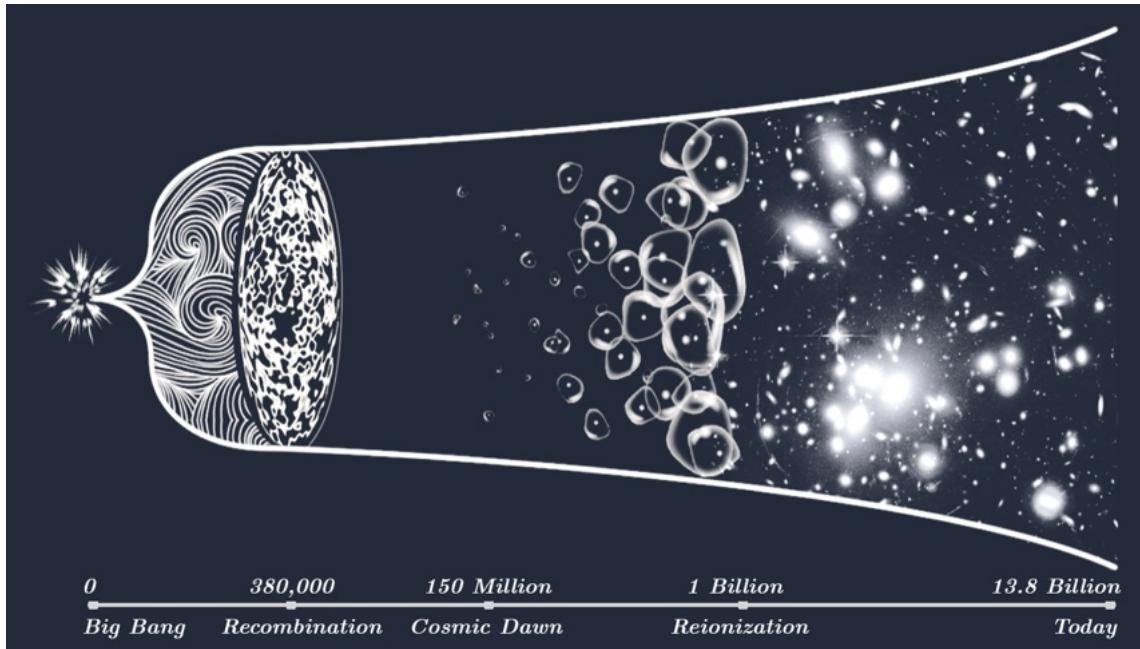


Figure 1.1: An illustration of the history of the Universe. Beginning with the Big Bang to the left, the Universe underwent a period of rapid expansion and cooling. Around  $\sim 0.38$  Myr later the Universe had cooled sufficiently for simple nuclei to combine with electrons, resulting in the first phase transition from an opaque ionised plasma to a transparent neutral state. The resulting free streaming photons preserve a snapshot of the Universe and is known as the Cosmic Microwave Background. Approximately  $\sim 150$  Myr later, at Cosmic Dawn, primordial over-densities have gravitationally coalesced to birth the first luminous sources in the Universe. Ionising radiation produced by these sources expand in bubbles, eventually overlapping to lead to a completely Reionised Universe, approximately  $\sim 1$  Gyr after the Big Bang. The period spanning from our Cosmic Dawn through to complete Reionisation is known as the Epoch of Reionisation. In this ionised Universe, through hierarchical mergers or early galaxies, we arrive at our local Universe, approximately  $\sim 13.787$  Gyr after the Big Bang.

<sup>34</sup> **1.1. A BRIEF HISTORY OF THE UNIVERSE**

<sup>35</sup> **1.1.1. *The Big Bang & the First Three Minutes***

<sup>36</sup> Our Universe was born in a Big Bang, with hot dense matter and light blooming into  
<sup>37</sup> existence (see Figure 1.1 for an illustration of key milestones of the Universe). Current  
<sup>38</sup> best estimates put the cataclysmic birth approximately  $13.787 \pm 0.002$  Gyr ago ([Planck](#)  
<sup>39</sup> [Collaboration et al., 2020](#)). Within the first fraction of a second it experiences an expon-  
<sup>40</sup> ential inflation, resulting in the Universe cooling adiabatically. A mere three minutes  
<sup>41</sup> later, Big Bang Nucleosynthesis ([Alpher et al., 1948](#)) has formed the primary building  
<sup>42</sup> blocks of the present Universe; the nuclei of Hydrogen, Helium and Lithium. At this  
<sup>43</sup> stage, the Universe consists of a hot dense soup of photons, protons, neutrons, and elec-  
<sup>44</sup> trons. Photons are strongly coupled with electrons via Thomson Scattering due to the  
<sup>45</sup> high density of the Universe, and the tiny cross-section of scattering. In this energetic  
<sup>46</sup> and opaque plasma ( $k_B T \gg 13.6\text{eV}$ ), any neutral atoms which form are almost imme-  
<sup>47</sup> diately dissociated by interactions with photons. The Universe continues expanding  
<sup>48</sup> and cooling adiabatically, with constantly decreasing photon-electron scattering (due to  
<sup>49</sup> reduced density and increased mean-free paths), also increasing the longevity of any  
<sup>50</sup> neutral atom formed.

<sup>51</sup> **1.1.2. *Recombination & the Cosmic Microwave Background***

<sup>52</sup> Approximately  $\approx 0.38$  Myr after the Big Bang, at redshift  $z \simeq 1100^*$ , a critical energy  
<sup>53</sup> density threshold is achieved ( $k_B T \leq 13.6\text{eV}$ ). Neutral Hydrogen atoms which form  
<sup>54</sup> now persist without being dissociated. This critical milestone in the Universe's past is  
<sup>55</sup> somewhat confusingly dubbed the "Epoch of Recombination"<sup>†</sup> (see Figure 1.1). With  
<sup>56</sup> the comprehensive capture of free electrons by atomic nuclei, the Universe undergoes  
<sup>57</sup> a rapid phase transition from completely ionised to neutral. This process also frees the  
<sup>58</sup> photons from their incessant Thomson scattering, enabling them to free stream through  
<sup>59</sup> the Universe. This relic radiation preserves a precious snapshot of the thermal state of  
<sup>60</sup> the Universe at the so called "surface of last scattering", when photons decoupled from  
<sup>61</sup> matter. These photons are redshifted through cosmological expansion and can now  
<sup>62</sup> be observed at microwave wavelengths as the Cosmic Microwave Background (CMB)  
<sup>63</sup> ([Kamionkowski & Kosowsky, 1999](#)). The existence of this isotropic blackbody radia-  
<sup>64</sup> tion is one of the pillars of the Big Bang model, as it implies that photons and baryonic  
<sup>65</sup> matter existed in a highly interacting thermal state earlier. First detected by [Penzias &](#)  
<sup>66</sup> [Wilson \(1965\)](#), it has now been characterised to have an extremely uniform temperature  
<sup>67</sup> across the sky  $T_{\text{CMB}} = 2.72548 \pm 0.00057$  K ([Fixsen, 2009](#)), with spatial temperature  
<sup>68</sup> anisotropies at the  $1/10^5$  level ([Planck Collaboration et al., 2016](#)). These minute fluctua-  
<sup>69</sup> tions in the nearly uniform CMB are a result of quantum fluctuations in the energy-  
<sup>70</sup> matter field of the early Universe. These primordial fluctuations are further distorted via

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\*Redshift ( $z$ ) serves as a measure of cosmological time.  $z$  indicates the factor by which emitted radia-  
tion's wavelength is *increased*, due to cosmological expansion. Higher values of  $z$  are further in the past,  
and thus experience larger redshifts. Radiation from the CMB ( $z = 1100$ ) is observed at wavelengths 1101  
times longer than those emitted.

<sup>†</sup>This epoch actually represents the first combination of these particles into stable atoms, in the stan-  
dard Big Bang model.

<sup>71</sup> interactions with matter along the way to the observer.

### <sup>72</sup> 1.1.3. *The Dark Age, Cosmic Dawn & Reionisation*

<sup>73</sup> Post recombination, the Universe enters a period of darkness and contains primarily Hydrogen, with traces of Helium and other heavier elements. At the start of this “Dark Age”  
<sup>74</sup> the matter distribution is almost homogeneous, exhibiting small fluctuations in density  
<sup>75</sup> correlated with observed CMB anisotropies. Over the next  $\sim 150$  Myr, regions of above-  
<sup>76</sup> average densities gravitationally attract matter from neighbouring under-dense regions.  
<sup>77</sup> This gravitational coalescence around primordial matter fluctuations led to the forma-  
<sup>78</sup> tion of web-like filamentary structures spanning the cosmos. Giant halos form at inter-  
<sup>79</sup> sections within this cosmic web, where gravitational forces can overcome cosmological  
<sup>80</sup> expansion to finally give birth to the first luminous sources in our Universe. These first  
<sup>81</sup> stars, black holes and galaxies emitted intense radiation, illuminating the dark ages and  
<sup>82</sup> heralding a cosmic dawn.

<sup>83</sup> Intense ultraviolet radiation from these first luminous sources propagated into the  
<sup>84</sup> intergalactic medium (IGM) resulting in bubbles of expanding ionisation. New sources  
<sup>85</sup> of ionisation came into being while old ionisation bubbles expanded into their neutral  
<sup>86</sup> surroundings. As first generation ionising sources reached the end of their lives, local  
<sup>87</sup> pockets of recombination occurred within ionised bubbles due to a lack of an active  
<sup>88</sup> ionising source. The interaction of old and new ionising sources resulted in a patchy  
<sup>89</sup> and non-trivial ionisation morphology as the Universe evolves. The eventual overlap  
<sup>90</sup> of expanding ionisation frontiers led to the inevitable transition of the Universe from  
<sup>91</sup> neutral to completely ionised. The Epoch of Reionisation (EoR) spans this critical period  
<sup>92</sup> ( $z \approx 20$  to  $z \approx 6$ ), ending almost a billion years after the Big Bang (see Figure 1.1).

<sup>93</sup> The local Universe we observe today consists of a variety of morphologically complex  
<sup>94</sup> galaxies, organised into large clusters and filaments, embedded in a ionised IGM. The  
<sup>95</sup> first sources which influenced the formation of this complex structured Universe are  
<sup>96</sup> suspected to be a combination of first generation stars, quasars and primordial black  
<sup>97</sup> holes (see e.g. [Aghanim et al., 1996](#); [Becker et al., 2015](#); [Mesinger et al., 2015](#); [Madau & Haardt, 2015](#); [Grazian et al., 2018](#)). Many questions surrounding these first sources  
<sup>98</sup> remain. When and how did they form? And how did they influence the process of  
<sup>99</sup> reionisation? Irrespective of their nature, their birth changed the nature of the Universe  
<sup>100</sup> fundamentally, bringing first light to the dark age. Observing the EoR has the scope  
<sup>101</sup> to revolutionise our understanding of our Universe, and represents one of last major  
<sup>102</sup> unanswered questions in observational cosmology. Theoretical models of the EoR are  
<sup>103</sup> advanced and well explored, but remain untested by observations (see [Furlanetto et al., 2006](#);  
<sup>104</sup> [Pritchard & Loeb, 2012](#), for theoretical EoR models). We also direct curious readers  
<sup>105</sup> to [Park et al. \(2019\)](#); [Mesinger \(2019\)](#), for reviews on the fundamental astrophysics and  
<sup>106</sup> cosmology which can be explored using the Epoch of Reionisation signal.

## <sup>109</sup> 1.2. NEUTRAL HYDROGEN AS A COSMOLOGICAL TRACER

<sup>110</sup> Observations of the CMB give us a snapshot of the state of the early Universe around  
<sup>111</sup> 0.38 Myr after the Big Bang ( $z \approx 1100$ ). The next furthest astronomical observation  
<sup>112</sup> (as of October, 2024) is of JADES-GS-z14-0, a Lyman-break galaxy at  $z \simeq 14.32$ , almost

113 290 Myr after the Big Bang (Robertson et al., 2024). Large surveys of galaxies extend  
114 out to  $z \leq 2$ , while systematic surveys of quasars can reach redshifts of  $z \leq 3$ . A dearth  
115 of observations between  $3 \leq z \leq 1100$  leave vast volumes of the Universe unexplored  
116 (see Figure 1.2).

117 Fortunately, the most abundant elemental species in the early Universe is neutral Hy-  
118 drogen (HI), which can be leveraged to map these unexplored cosmological volumes.  
119 Neutral Hydrogen emits radiation with a wavelength of 21-cm in the rest frame, which  
120 can be cosmologically redshifted to longer wavelengths. This wavelength is in fact one  
121 of the most precisely known quantities in astrophysics, measured by Goldenberg et al.  
122 1960 using a Hydrogen maser to 2 parts in  $10^{11}$ ! The forbidden spin-flip transition re-  
123 sponsible for this radiation arises from the relative spin alignment of the constituent  
124 electron and proton, which results in a higher energy triplet state and a lower energy  
125 singlet state (Feynman, 1965) (see Figure 1.3). The transition is considered forbidden as  
126 it has a mean lifetime of  $\sim 10^7$  years, which results in an extremely narrow emission  
127 line. Any appreciable concentration of 21-cm radiation implies the existence of massive  
128 amounts of neutral Hydrogen due to the almost 10 million year lifetime of the 21-cm  
129 spin-flip transition.

130 The precise correlation between observed wavelength and redshift enables the cre-  
131 ation of 3D 21-cm tomographic maps of the Universe. These maps trace the evolution of  
132 neutral Hydrogen across Cosmic Dawn and the Epoch of Reionisation (see Figure 1.2),  
133 revealing large-scale structure formation, and the growing voids surrounding the first  
134 sources of ionisation. This method is in contrast to traditional astronomy which focuses  
135 on observing light from stars, galaxies and other relatively small objects of interest. The  
136 long wavelength of 21-cm radiation also is not readily absorbed by intervening gas and  
137 dust, providing another advantage to 21-cm tomographic mapping as an ideal tool to  
138 observe vast volumes of the cosmos.

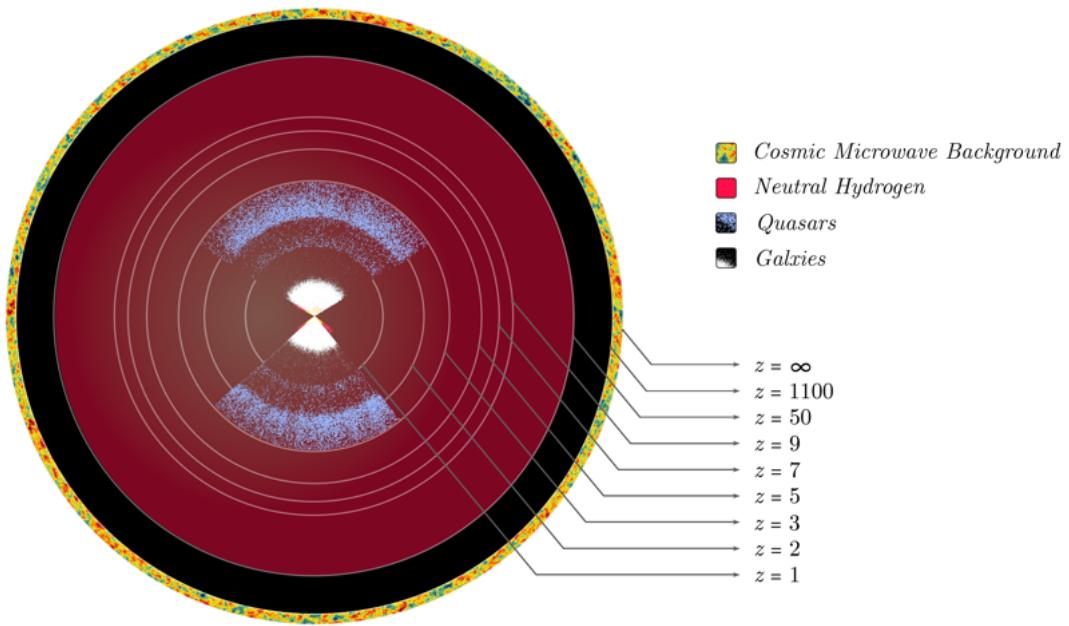


Figure 1.2: How much of the cosmos have we actually observed? This illustration of the Universe to scale shows galactic surveys in white cones near the centre, followed by observations of quasars in purple, and finally bounded by the CMB. Observations of the high-redshift Universe  $z \geq 3$  are extremely sparse. Observations of neutral Hydrogen can be leveraged to access orders-of-magnitude higher volumes of the Universe than ever before (see red section). An illustration inspired by [Mao et al. \(2008\)](#), an interpretation by [Adrian Liu](#), using an image of the BOSS survey by [Michael Blanton](#), and the Planck CMB map.

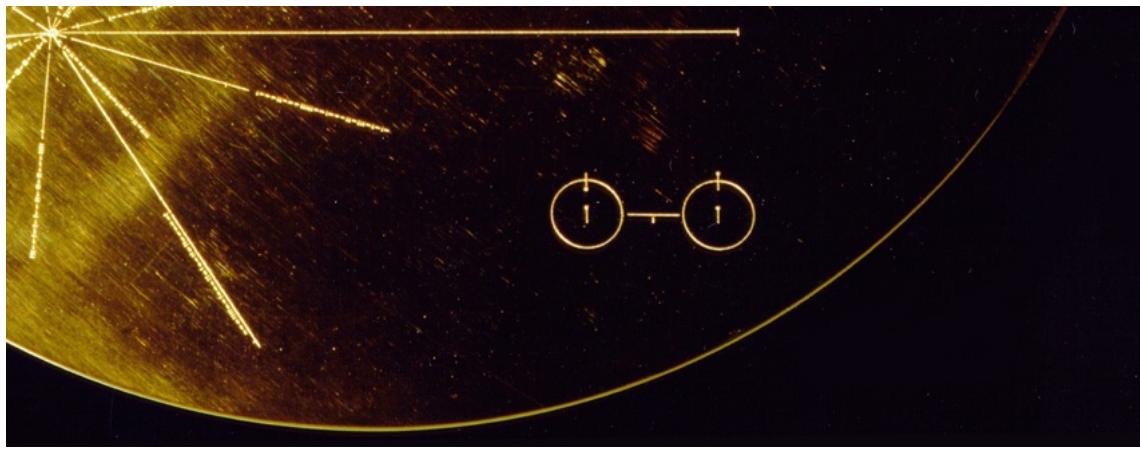


Figure 1.3: The hyperfine transition of neutral Hydrogen, considered so fundamental to the Universe that it was depicted on the Golden Record sent out on the Voyager space-crafts, and used as the key to decoding all other information from Earth to any intelligent extraterrestrial life form which may find it. This infrequent forbidden spin-flip of a neutral Hydrogen atom emits light with a 21 cm wavelength. Credit: NASA/JPL

### 139 1.3. EVOLUTION OF THE 21-CM SIGNAL

140 A range of physical properties and mechanisms can influence the 21-cm intensity (brightness  
 141 temperature), including density, velocity, ionisation state, gas temperatures and  
 142 spin temperatures (Furlanetto et al., 2006). At any redshift, the CMB provided a near  
 143 isotropic blackbody background for 21-cm radiation emitted from neutral Hydrogen.  
 144 The variation in brightness temperature due to neutral Hydrogen (HI) in contrast to  
 145 the background radiation can be quantified by the differential brightness temperature  
 146 (Morales & Wyithe, 2010) through:

$$\Delta T = 23.8 \left( \frac{1+z}{10} \right)^{\frac{1}{2}} [1 - \bar{x}_i(1 + \delta_x)] (1 + \delta)(1 - \delta_v) \left[ \frac{T_s - T_{CMB}}{T_s} \right] \text{ mK}, \quad (1.1)$$

147 where  $\bar{x}_i$  is the mean ionisation fraction ( $\bar{x}_i = 1 - \bar{x}_{HI}$ ),  $\delta$  is the dark matter density fluctuation,  
 148  $\delta_x$  is the ionisation fraction fluctuation,  $\delta_v = (1+z)H^{-1}\partial v_r/\partial r$  is the distortion  
 149 due to velocity ( $\partial v_r/\partial r$  being the radial velocity gradient, and Hubble parameter  $H$ ), and  
 150  $T_s$  and  $T_{CMB}$  are the spin temperatures of the HI and the temperature of the background  
 151 CMB radiation. The spin temperature  $T_s$  of HI quantifies the ratio of neutral HI atoms  
 152 in each of the two hyperfine levels of the ground state.

153 The balance between the process driving reionisation is non-trivial, but can be delineated  
 154 into important phases where different processes dominate. Figure 1.4 shows the  
 155 sky-averaged brightness temperature  $\Delta T$ , from Pritchard & Loeb (2012).

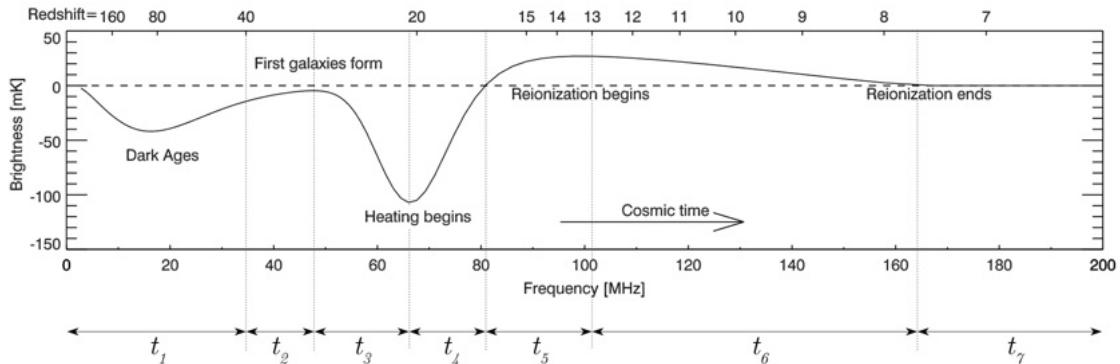


Figure 1.4: The expected evolution of sky-averaged 21-cm brightness temperature (taken from Pritchard & Loeb 2012, with modifications inspired by J. L. B. Line 2017) between the dark ages ( $z \approx 200$ ) to the end of reionisation ( $z \approx 6$ ). The solid curve indicates the signal, dashed line indicates  $\Delta T = 0$ , and the dotted lines demarcate important periods of the evolution of the 21-cm signal, labeled  $t$ :

- 156      $t_1$  Gas continues cooling adiabatically, resulting in collisional coupling  $T_s < T_{CMB}$ ,  
 157       leading to an absorption signal during the Dark Ages
- 158      $t_2$  Reduced efficiency of collisional coupling due to cosmological expansion, and ra-  
 159       diative cooling sets  $T_s = T_{CMB}$  with no detectable signal
- 160      $t_3$  Birth of first stars and galaxies leading to emission of both Lyman- $\alpha$  photons and  
 161       X-rays. X-rays heat the IGM, increasing gas temperature ( $T_k$ ), while Lyman- $\alpha$

162 couple to the gas. Spin temperature is coupled to cold gas such that  $T_s \sim T_k <$   
163  $T_{CMB}$ , resulting in an absorption signal

164  $t_4$  Lyman- $\alpha$  coupling saturates, and heating becomes significant. As  $T_k$  increases  
165 slowly so does  $T_s$  raising the 21-cm signal amplitude, till it eventually crosses over  
166 from absorption to emission

167  $t_5$   $T_k$  continues increasing due to Lyman- $\alpha$  coupling, until 21-cm signal saturation  
168 occurs when  $T_s \sim T_k \gg T_{CMB}$

169  $t_6$   $T_{CMB}$  no longer contributes to Equation 1.1. As reionisation progresses the signal  
170 is dominated by ionisation fraction, and reduces in amplitude

171  $t_7$  Reionisation is complete, most 21-cm signal comes from HI in galaxies

## 172 1.4. FOREGROUNDS

173 The cosmological 21-cm signal the Epoch of Reionisation between  $z \simeq 6 - 15$  can be ob-  
174 served between  $\sim 200 - 90$  MHz. The primary obstacle hindering a statistical detection  
175 of the 21-cm signal are a range of astrophysical and terrestrial foregrounds which can up  
176 to  $\sim 5$  orders of magnitude brighter than the cosmological signal (e.g. Oh & Mack, 2003;  
177 Santos et al., 2005; Jelić et al., 2008; Bowman et al., 2009; Pindor et al., 2011; Pober et al.,  
178 2013; Yatawatta et al., 2013). These foregrounds are dominated by Galactic diffuse syn-  
179 chrotron radiation, supernovae remnants, extragalactic radio-loud galaxies and Active  
180 Galactic Nuclei (AGNs). Time variable distortions induced by the ionosphere warp all  
181 celestial radiation. Terrestrial transmissions from radio, television, and satellite commu-  
182 nication all fall within or adjacent to this observing band. Galactic synchrotron radiation  
183 occupies  $\sim 70\%$  of the foreground flux budget at 150 MHz, while extragalactic sources  
184 contribute  $\sim 27\%$  (Shaver et al., 1999). Figure 1.5 depicts the various components of  
185 foregrounds ordered by proximity — from astrophysical to terrestrial and instrumental.

## 186 1.5. THESIS OUTLINE

187 The obstacles hindering the first EoR detection cannot be understated and require un-  
188 precedented precision at all levels — from the understanding of our instruments and  
189 foregrounds to the astrophysical inferences drawn from observations. This thesis presents  
190 advances in measuring and understanding the impact of interferometric instrumental  
191 systematics on an Epoch of Reionisation detection.

192 In Chapter 2, we provide a foundational introduction to low-frequency radio interfer-  
193 ometry, with a focus on the Murchison Widefield Array (MWA) telescope. In Chapter  
194 3, we develop and implement an experiment to use communication satellites to perform  
195 in-situ all-sky dual-polarised measurements of MWA beampatterns, revealing signifi-  
196 cant sidelobe distortions at the  $\sim 10\%$  level. In Chapter 4, we develop a framework  
197 to emulate measured beam deformations with cutting-edge beam models. This chapter  
198 also tests the impact of an imperfect instrumental representation, during calibration of  
199 astronomical data, can have on a future EoR detection. In Chapter 5, we explore how

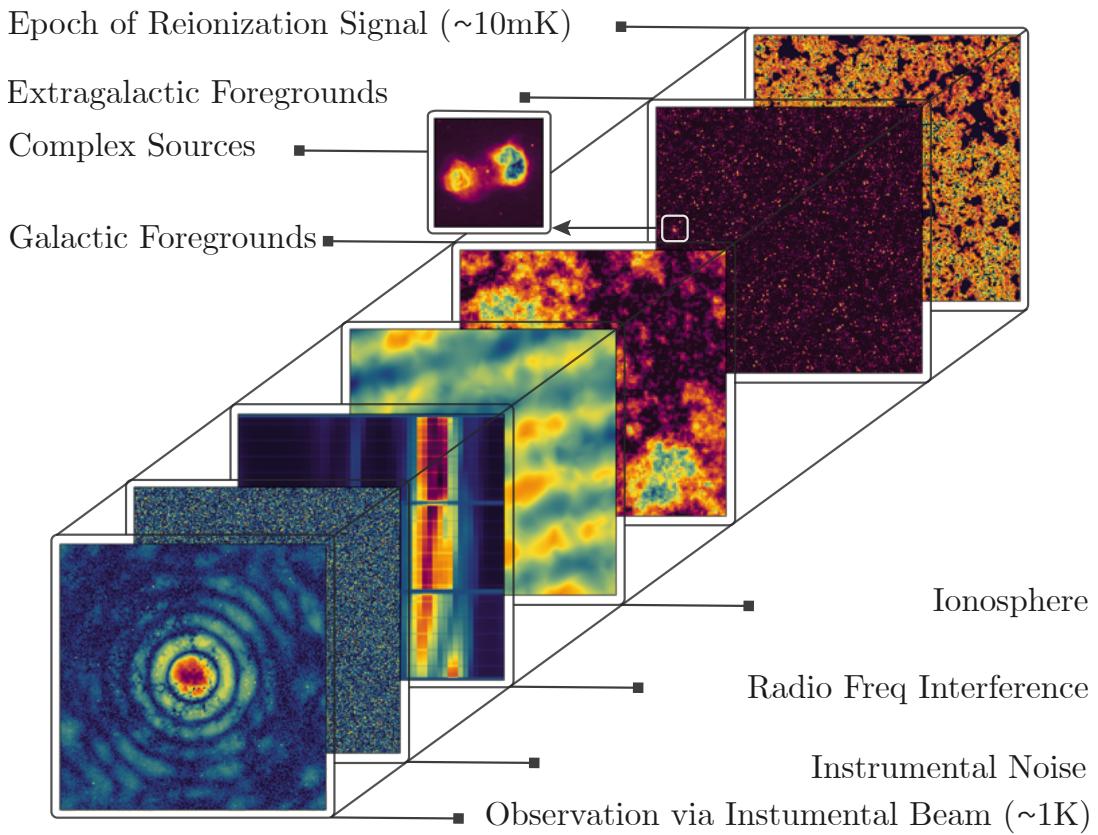


Figure 1.5: A breakdown of astrophysical and terrestrial foregrounds, ordered by proximity, which must be precisely peeled away or avoided to measure the EoR signal. An illustration inspired by [Jelić et al. \(2008\)](#), extended to include terrestrial and instrumental effects to depict the entire dynamic range that an EoR measurement must span.

200 deformed beams interact with the polarised radio sky, and the impact on studies of cosmic  
 201 magnetism. We finally conclude and discuss this thesis in Chapter 6, with a focus  
 202 of future directions of investigations towards a first detection of the cosmological signal  
 203 from the Epoch of Reionisation.

*Beneath desert skies,  
Murchison listens for light,  
Echoes from the dawn.*

204

Aman, 2024, Haiku

205

## 206 Measurement Theory & the Murchison Widefield Array

207

208 Traditional telescopes achieve angular resolutions of  $\sim \lambda/D$ , where  $\lambda$  is the observing  
209 wavelength, and  $D$  is the aperture diameter. Exploring the Universe at longer radio  
210 wavelengths necessitated the development of larger and larger single-dish telescopes.  
211 Despite the mechanical marvel of the world's largest physically steerable telescope\*  
212 achieving an aperture of  $D = 100\text{ m}$ , pushing much beyond this is infeasible. The de-  
213 sire for higher resolutions at these longer wavelengths led to the development of ra-  
214 dio interferometry, where observations from multiple smaller telescopes are coherently  
215 synthesised to achieve angular resolutions determined by the separation between the  
216 telescopes rather than the diameter of each telescope. This concept revolutionised the  
217 field of radio astronomy.

218 This chapter discusses the fundamentals of radio interferometry, establishes a math-  
219 ematical framework in which Epoch of Reionisation measurements can be understood,  
220 and explores the elegance of the Murchison Widefield Array telescope.

### 221 2.1. INTRODUCTION TO INTERFEROMETRY

222 The fundamental measurement made by a radio interferometer is called a visibility, is  
223 the time-averaged cross-correlation between pairs of voltage signals observed by a pair  
224 of receiving elements. An interferometer composed of  $N$  receiving elements can be  
225 considered an ensemble of  $N(N - 1)/2$  two-element interferometers, each making a  
226 unique measurement. For a source in direction  $\hat{\mathbf{s}}$ , and a baseline vector  $\mathbf{b}$  separating a  
227 pair of antennas 1, 2, the plane wavefront arrives at one antenna before the other, with  
228 a geometric delay given by:

$$\tau_g = \vec{\mathbf{b}} \cdot \hat{\mathbf{s}} / c, \quad (2.1)$$

229 were  $c$  is the speed of light. Quasi-monochromatic signals measured by antennas 1, 2,  
230 centred at frequency  $\nu$  are  $V_1(t)$  and  $V_2(t)$  respectively. These voltages are multiplied  
231 and time-averaged by the correlator resulting in a visibility:

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\*A title currently held by the Green Bank Telescope

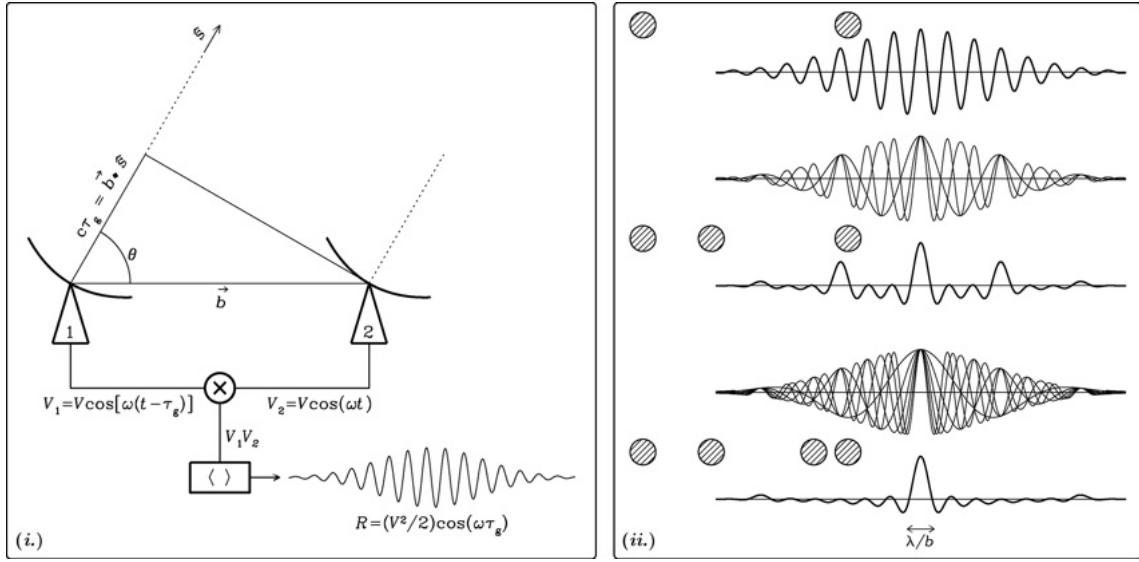


Figure 2.1: Illustrations of interferometry from Condon & Ransom (2016). The left panel (i.) represents a simple two-element interferometer. Plane waves incident on the pair, experience a geometric phase delay from an off-zenith source in direction  $\hat{s}$ . The time-averaged cross correlation of voltages measured by each pair of antennas represent a visibility, and exhibit a fringe pattern as the source transits the sky. The right panel illustrates how the combination of multiple pairs of two-element interferometers rapidly approaches a Gaussian response to the sky, known as the synthesised beam whose angular resolution approaches  $\theta \approx \lambda/b$ , the ratio of wavelength and maximum separation between receiving elements.

$$R = \langle V_1(t)V_2(t) \rangle = \left( \frac{V^2}{2} \right) \cos(\omega\tau_g), \quad (2.2)$$

whose amplitude is proportional to the flux density of the source at  $\hat{s}$ , and phase  $(\omega\tau_g)$  depends on geometric delay  $\tau_g$  and frequency  $\nu = \omega/2\pi$ . As the source transits the sky the geometric delay changes, resulting in an alternation between constructive and destructive combinations of signals from the two antennas. This is observed as a sinusoidal fluctuation in the measured visibility  $R$  known as a fringe, enveloped in a broad Gaussian envelope resulting from the primary beam response of the receiving elements (see panel (i.) of Figure 2.1). For interferometers constructed of identical receiving elements, the primary beam is the product of the power pattern of individual antennas (see Appendix B for a review of primary beam models). In the absence of antenna beams, the point source response of the interferometer would be a sinusoidal fringe spanning the sky – sampling a single Fourier mode of the sky brightness distribution with angular period  $\lambda/b \sin \theta$ .

Graduating from the pedagogic two element interferometer, we can gradually begin including more antennas. Every unique pair of antennas samples a different Fourier mode of the sky brightness distribution. The  $N(N - 1)/2$  visibilities measured by a  $N$  element interferometer can be coherently synthesised to rapidly approach a Gaussian response on the sky (see panel (ii.) of Figure 2.1). This is known as the instantaneous

249 synthesised beam, and has an angular resolution approaching  $\theta \approx \lambda/b$ , the ratio of wave-  
 250 length  $\lambda$  and maximum baseline  $b$ .

251 This framework can be further generalised by considering an extended sky brightness  
 252 distribution  $I(\hat{s})$  instead of a single point source. Additionally a fully complex correlator  
 253 must be utilised to describe an arbitrary source brightness distribution, using a sine and  
 254 cosine basis. The response of a two element interferometer to an extended source can be  
 255 formulated using Euler's formula to perform the complex correlation. We can generalise  
 256 Equation 2.2 to complex visibilities as:

$$\mathcal{V}_\nu = \int \mathcal{A}_\nu(\hat{s}) I_\nu(\hat{s}, \nu) \exp(-2\pi i \vec{b} \cdot \hat{s}/\lambda) d\Omega, \quad (2.3)$$

257 where  $\mathcal{A}_\nu(\hat{s})$  is the normalised beam response of the two antennas,  $I_\nu(\hat{s})$  is the intensity  
 258 of the source across the sky,  $\vec{b}$  is the baseline vector between antennas,  $\nu$  is frequency,  
 259 and  $d\Omega$  represents an integration across the sky.

260 In practice, the application of Equation 2.3 requires the introduction of a coordinate  
 261 system. A common notation is to use the Fourier dual of the spatial vector  $\hat{s}$  to describe  
 262 wavelength dependent baseline vectors  $\mathbf{u} = \mathbf{b}/\lambda = (u, v, w)$ . Note that,  $(u, v, w)$  are mea-  
 263 sured in terms of wavelengths, pointing East, North and towards the phase centre (a  
 264 direction of interest), respectively. Positions on the sky are conveniently described by  
 265 the directional cosines  $(l, m, n)$ , measured with respect to the  $(u, v, w)$  axes which obey  
 266  $l^2 + m^2 + n^2 = 1$ . In this coordinate system, Equation 2.3 become:

$$\mathcal{V}_\nu(u, v, w) = \int \int \frac{\mathcal{A}_\nu(l, m) I_\nu(l, m)}{(1 - l^2 - m^2)^{1/2}} \exp[-2\pi i(ul + vm + wn)] dl dm, \quad (2.4)$$

267 with the integrand evaluated where  $l^2 + m^2 < 1$ . This relation is reminiscent of a two-  
 268 dimensional Fourier transform, and can reduce to it under two sets of special conditions.  
 269 The first is by building East-West interferometers which have baselines confined to a  
 270 plane, under Earth Rotation. The baseline coordinates can then be defined with  $w$  point-  
 271 ing to a celestial pole. Setting  $w = 0$  in Equation 2.4 results in a Fourier relation which  
 272 can be readily inverted to form synthesised images. The second case occurs when  $|l|$  and  
 273  $|m|$  are small enough that:

$$(\sqrt{1 - l^2 - m^2} - 1)w \approx -\frac{1}{2}(l^2 + m^2)w = 0. \quad (2.5)$$

274 Equation 2.4 becomes:

$$\mathcal{V}_\nu(u, v) = \int \int \mathcal{A}_\nu(l, m) I_\nu(l, m) \exp[-2\pi i(ul + vm)] dl dm. \quad (2.6)$$

275 inverting this Fourier relation:

$$\mathcal{A}_\nu(l, m) I_\nu(l, m) = \int \int \mathcal{V}_\nu(u, v) \exp[2\pi i(ul + vm)] du dv, \quad (2.7)$$

276 in this narrow-field imaging regime, the dependence of visibilities on  $w$  is negligible.  
 277 We now posses the mathematical framework required to describe an arbitrary interfer-  
 278 ometre, and have explored how measured visibilities can be converted to a synthesised  
 279 image. In the following section we explore how the unique measurement spaces of in-

280 terferometers both facilitate and hinder the search for the EoR signal.

## 281 2.2. INTERFEROMETRIC MEASUREMENT SPACES

282 Measurements by interferometers are in a intermediate  $\{u, v, f\}$ -space comprised of sets  
283 of Fourier modes at the set of frequencies in the telescope's band. This space is neither  
284 convenient for imaging  $\{x, y, f\}$ , nor for power spectrum estimations  $\{u, v, \eta\}$ ; where I  
285  $x, y$  are spatial directions,  $u, v$  are Fourier modes defined by baseline vectors,  $f$  is fre-  
286 quency, and  $\eta$  is the Fourier dual of frequency (Morales & Hewitt, 2004). Transforma-  
287 tions between various spaces are depicted in Figure 2.2, and described below.

- 288 (i.) We observe galaxies scattered across a cosmological volumes, with the  $x, y$  Carte-  
289 sian axes aligned with the plane of the sky for an observer on Earth. The line-of-  
290 sight into the sky is aligned with the  $z$  axis, along which cosmological evolution  
291 can be observed (Figures 1.1, 1.4).
- 292 (ii.) As discussed in Section 1.3, the evolution of the Universe can be observed by mea-  
293 suring the intensity of the redshifted 21-cm line from neutral Hydrogen across  
294 cosmic time. In practice, this is achieved by observing the sky as a function of  
295 frequency  $f$ . Synchrotron emission follows a power law spectra, varying slowly  
296 with frequency. Thus in this intermediate spatial-frequency  $\{x, y, f\}$  space, extra-  
297 galactic sources span the frequency axis.
- 298 (iii.) Interferometers do not natively measure sky brightness intensity, rather each con-  
299 stituent baseline samples a Fourier mode on the sky for every frequency (see Sec-  
300 tion 2.1 and Equation 2.6). Thus the native measurement space of an interferom-  
301 eter is  $\{u, v, f\}$ , depicted in panel (iii.) of Figure 2.2.
- 302 (iv.) Interpreting native measurements in the  $\{u, v, f\}$  space is challenging. Perform-  
303 ing a spatial Fourier transform results in dirty images\* as a function of frequency  
304  $\{x^*, y^*, f\}$ , where  $x^*, y^*$  are indicative of dirty imaging.
- 305 (v.) An alternate method of understanding interferometric measurements is to em-  
306 brace their Fourier nature, and perform a one-dimensional Fourier transform along  
307 the frequency axis resulting in  $\{u, v, \eta\}$ -space. An additional coordinate transform  
308 results in a three-dimensional Fourier representation of the measurements in a  
309  $\{k_x, k_y, k_z\}$  space. Here the wavenumbers  $k_x, k_y$  lie along the plane of the sky, with  
310 modes along the line-of-sight being aligned with  $k_z$ . Interestingly, the majority of  
311 foreground flux described in Section 1.4 is slowly varying with frequency, result-  
312 ing in this power being contained within the first few  $k_z$  Fourier modes (see white  
313 dotted lines perpendicular to  $k_z$  in Figure 2.2). The utility of the Fourier space is  
314 already apparent!

---

\*Dirty images arise for the inherent incomplete sampling of the Fourier plane by interferometers. The inverse Fourier transform of visibilities results in an image containing *only* spatial scales sampled by the interferometer, thus missing some information and imperfectly recovering the true sky brightness distribution.

- 315 (vi.) Since there is nothing particularly unique about the rotation of the axes in the  
316 plane of the sky, performing a cylindrical average on the  $\{k_x, k_y, k_z\}$  space, along  
317  $k_z$  can separate modes of contamination and signal in deterministic ways. We de-  
318 fine two new wavenumber axes;  $k_{\parallel} = k_z$  (Fourier modes along the line-of-sight),  
319 and  $k_{\perp} = \sqrt{k_x^2 + k_y^2}$  in the plane of the sky. Slowly frequency varying foreground  
320 power is then contained within the lower  $k_{\parallel}$  modes (below horizontal white line  
321 in Figure 2.2). This two-dimensional power spectrum space is an elegant diagno-  
322 stic tool in which foreground, cosmological, and instrumental systematics become  
323 apparent. Of particular import is the wedge-like structure above the low- $k_{\parallel}$  fore-  
324 ground modes. This arises from the chromatic nature of interferometers, which  
325 inherently sample different  $u, v$  modes as a function of frequency, leading to mode-  
326 mixing of foreground power into higher  $k_{\parallel}$  modes. This characteristic of interfer-  
327 ometric measurements has long been studied (see Datta et al., 2010; Morales et al.,  
328 2012; Vedantham et al., 2012; Parsons et al., 2012; Trott et al., 2012; Hazelton et al.,  
329 2013; Thyagarajan et al., 2013; Pober et al., 2013; Liu et al., 2014a,b; Thyagarajan  
330 et al., 2015).
- 331 (vii.) Finally, spherically averaging Fourier  $\{k_x, k_y, k_z\}$  modes gives us the highest signal-  
332 to-noise. This one-dimensional representation of the power spectrum provides the  
333 optimal space in which to attempt making a statistical detection of the cosmolog-  
334 ical signal from redshifted Hydrogen.

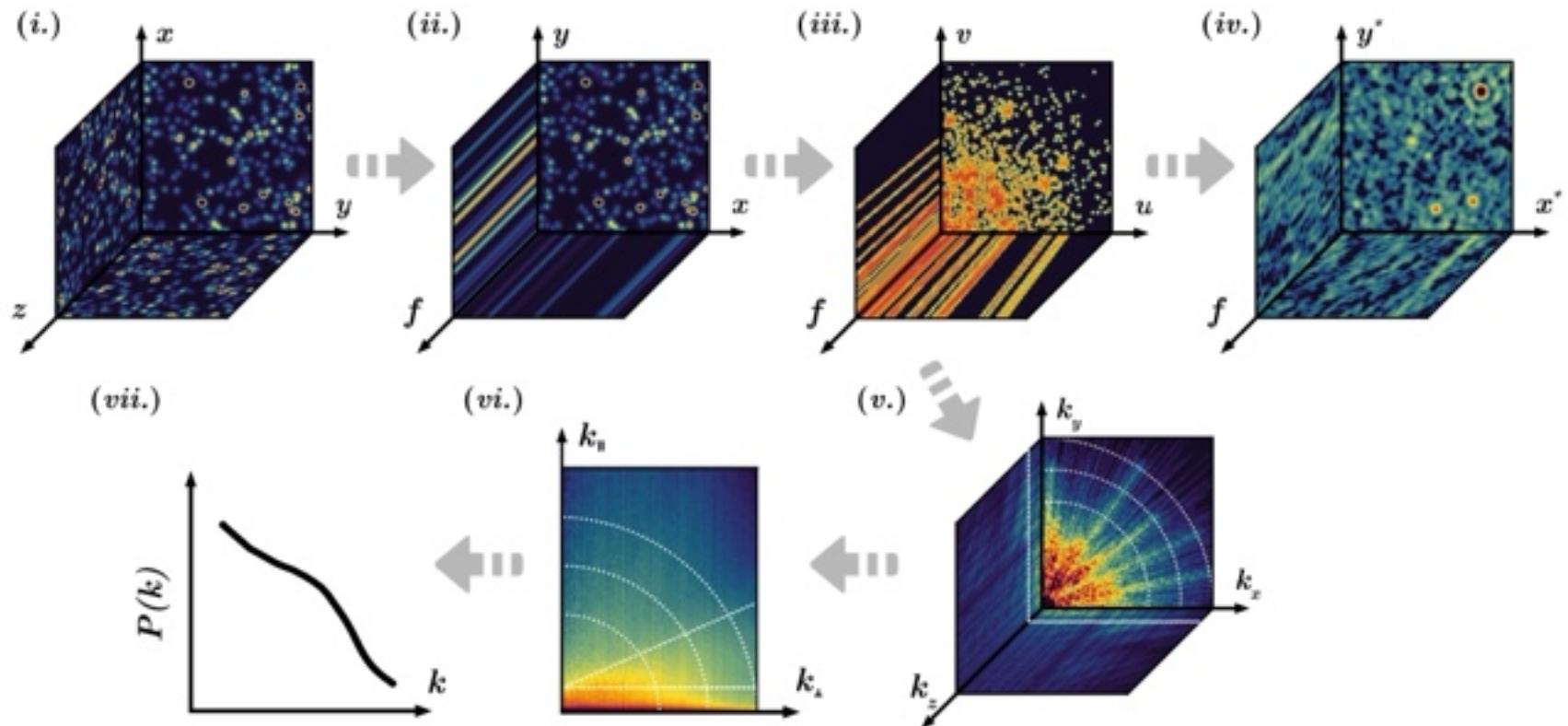


Figure 2.2: An illustration of the various mathematical spaces involved in interferometric measurements, from representations of Cartesian space in panel (i.), intermediate spatial-frequency space in (ii.), interferometric measurements in (iii.), interferometric imaging in iv., and power spectrum estimation panels (v.),(vi.),(vii.). Here  $(x, y, z)$  represent Cartesian coordinates with the first two aligned in the plane of the sky, with the third along the line of sight. Frequency is  $f$ , its Fourier dual is  $\eta$ ,  $(u, v)$  are Fourier spatial coordinates and  $(k_x, k_y, k_z)$  are wavenumber. The relation between various spaces are discussed in Section 2.2.

### 335 2.3. THE MURCHISON WIDEFIELD ARRAY

336 The Murchison Widefield Array\* (MWA) is the low-frequency radio interferometer lo-  
337 cated at *Inyarrimanha Ilgari Bundara*<sup>†</sup>, the CSIRO Murchison Radio-astronomy Obser-  
338 vatory (MRO), in the remote Western Australian outback. Designed with a primary goal  
339 of detecting the 21-cm EoR power spectrum, its science capabilities extend far beyond;  
340 including Galactic and extragalactic surveys, time variable astrophysics, solar and iono-  
341 spheric science and searches for exoplanets and fast radio bursts (see [Bowman et al.,](#)  
342 [2013; Beardsley et al., 2019a](#), for a description of key science goals).

343 Each antenna of the array is composed of a regular grid of  $4 \times 4$  dual-polarised bow-tie  
344 dipoles, on a  $5 \times 5$  m reflective metal mesh which acts as a groundsceen (see Figure 2.3).  
345 The orthogonal dipoles of each “tile” are aligned with the East-West and North-South  
346 cardinal directions, and are labeled X and Y respectively. The dipoles are sensitive to the  
347 entire visible sky in the  $80 - 300$  MHz band. The signals from each dipole are initially  
348 amplified by a low noise amplifier (LNA) in the central column of the dipole before being  
349 combined by an analogue beamformer (white box to the right of the tile in Figure 2.3).  
350 The analogue beamformer synthesises the signals from the 16 dipoles to construct a  
351 primary beam response on the sky with a full-width-half-max (FWHM) of roughly  $25^\circ$ ,  
352 and integrated collecting area of about  $15\text{m}^2$  at 150 MHz. By inserting analogue delays  
353 between the dipoles, the beamformer is capable of digitally pointing the primary beam  
354 response away from its neutral zenith sensitivity.

355 The initial construction of the Phase I stage of the MWA was composed of 128 tiles  
356 arranged in a pseudo-random configuration across  $\sim 3$  km of the desert ([Beardsley et al.,](#)  
357 [2012; Tingay et al., 2013](#)). In 2017, the telescope was upgraded with a Phase II expansion  
358 ([Wayth et al., 2018](#)) which increased the total number of tiles to 256, 128 of which could  
359 be correlated at any one time. The Phase II extension consisted of two possible con-  
360 figurations; an addition of two redundant hexagonal arrays to increase short baselines  
361 for EoR sensitivity, or a set of long baselines up to 5 km to improve angular resolution.  
362 The MWA is currently undergoing its Phase III upgrade (powered by the new MWAX  
363 correlator, see [Morrison et al., 2023](#)) which will enable it to correlate all 256 tiles at once,  
364 massively increasing sensitivity. The left panel of Figure 2.4 depicts the layout of Phase I  
365 tiles in green and Phase II tiles in orange. The right panel shows the density of baselines  
366 of the 128 Phase I tiles between 167 – 200 MHz.

367 Radio frequency signals from sets of 8 tiles are transmitted to digital receivers, which  
368 can process 30.72 MHz of bandwidth in real time. A polyphase filterbank first splits this  
369 bandwidth into  $24 \times 1.28$  MHz coarse bands, and then into 768 40 kHz fine channels.  
370 The correlator ([Ord et al., 2015; Morrison et al., 2023](#)) cross-multiplies data from every  
371 unique set of tiles, at a 0.5 s or 2 s resolution, to create visibilities (see Section 2.1, and  
372 Equation 2.4) - the fundamental measurements of interferometers.

373 Finally, the Murchison Widefield Array boasts a truly *wide* field-of-view. It is tough  
374 to understate how significant an impact this makes to the quality and scope of sci-  
375 ence it enables. The FWHM of the primary beam spans a staggering  $25^\circ \times 25^\circ$  field  
376 of view, enabling rapid sky surveys along with efficient measurements of large cosmo-

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\*<https://www.mwatelescope.org>

<sup>†</sup>The Wajarri Yamaji people, the traditional owners of the land, have named the site *Inyarrimanha Ilgari Bundara*, meaning *sharing sky and stars*.



Figure 2.3: Photos from the MWA site. In the top panel is one of 128 MWA tiles in the Western Australian desert, comprised of sixteen dual-polarisation bow-tie dipoles, signals from which are combined by an analogue beamformer to the right of the tile, before being passed to a digital receiver for processing. A goanna (not to scale), passes through the site during my visit in 2019. This beautiful specimen was roughly 1.5m in length. Goannas are notoriously stupid, and when startled are known to climb up humans with their sharp claws, mistaking them for trees. In the bottom left image, I am installing equipment into an MWA receiver for the satellite beam experiment described in Chapter 3 (Photo Credit: Jack Line). The final image is a reference antenna Nichole Barry, Jack Line and I built at the MRO, with me on top for scale (Credit: Nichole Barry).

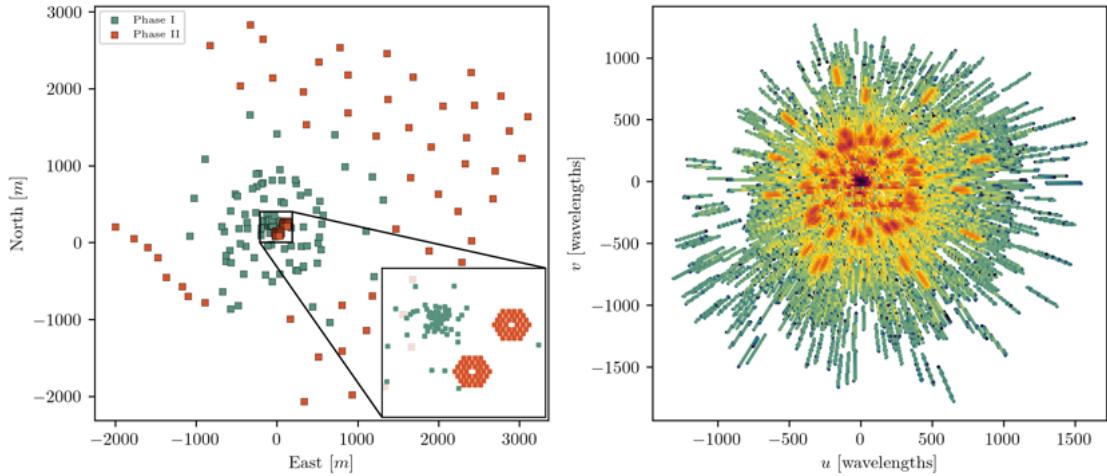


Figure 2.4: The left panel shows the location of the 256 MWA at the MRO, with the original Phase I tiles in green and the newer Phase II tiles in orange. The two Phase II redundant hexagonal arrays are showed in the inset. The right panel display the density of  $(u, v)$  baseline coverage of the 128 Phase I tiles, between 167 – 200 MHz.

logical volumes. What is less obvious is that the primary beam of each tile is actually sensitive to the *entire* sky - horizon to horizon. Figure 2.5 illustrates the extent of the primary beam pattern of the MWA at 182 MHz, with beam sensitivity contours at 90, 50, 30, 10, 1, 0.1% plotted over the Haslam map of the galaxy at 408 MHz (Haslam et al., 1981; Remazeilles et al., 2015). The figure is centred around the EoR 0 observing field ( $\alpha = 0, \delta = -27^\circ$ ), chosen to be one of the quietest parts of the sky, yet the beam sidelobes intersect with the rising Galactic plane. Even attenuated by a factor of a 1000, the apparent magnitude of the Galactic plane on the horizon can rival emission from the zenith of this quiet field.

Any uncertainties in the primary beam model can lead to the mis-estimation and mis-calibration of far-field sources. Much of this thesis focuses of developing and implementing experiments to measure the all-sky beam patterns of the MWA, and understand their non-trivial coupling to foreground power, with an emphasis of the implications of such effects on a future EoR detection.

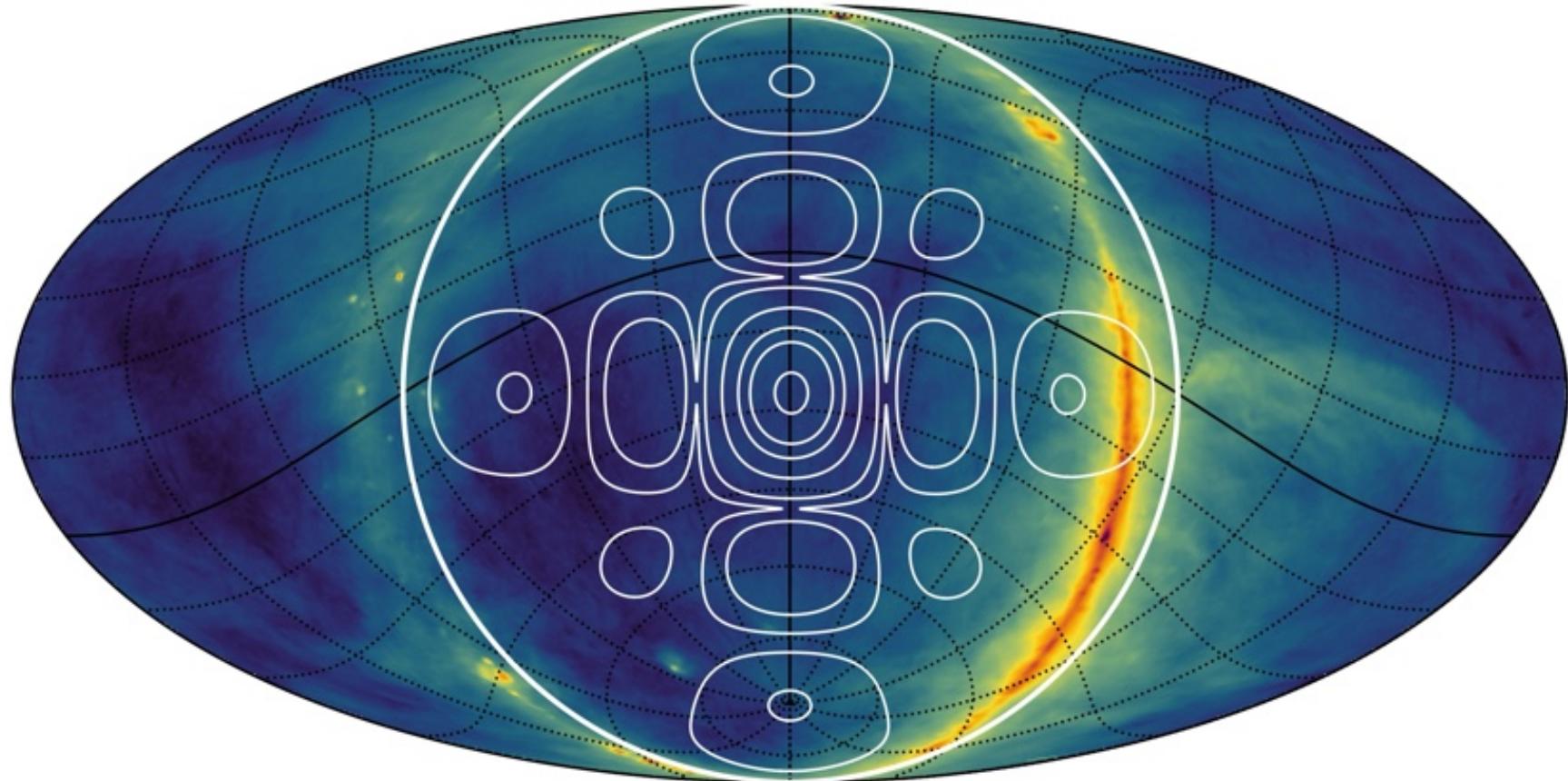


Figure 2.5: An illustration of the truly *wide* field-of-view of the Murchison Widefield Array. Plotted on top of the galactic Haslam map are all-sky sensitivity contours of the MWA primary beam at 182 MHz, with 90, 50, 30, 10, 1, 0.1% levels. This figure is centred around one of the quietest parts of the sky - the EoR 0 observing field ( $\alpha = 0, \delta = -27^\circ$ ), yet the beam is sensitive to the rising Galactic plane on the horizon.

# CHAPTER 3

391

## Dual Polarization Measurements of MWA Beampatterns at 137 MHz

392

393

394

395

### This chapter is based on

397 A. Chokshi, J. L. B. Line, N. Barry, D. Ung, D. Kenney, A. McPhail, A. Williams, R. L. Webster  
398 Monthly Notices of the Royal Astronomical Society, 502, 2, 2021, 1990

399 reformatted with the following changes only:

- 400 • The text is styled and restructured to match the rest of this thesis.  
401 • Where necessary, bibliographic records are updated.

### 402 3.1. ABSTRACT

403 The wide adoption of low-frequency radio interferometers as a tool for deeper and higher  
404 resolution astronomical observations has revolutionized radio astronomy. Despite their  
405 construction from static, relatively simple dipoles, the sheer number of distinct elements  
406 introduces new, complicated instrumental effects. Their necessary remote locations ex-  
407 acerbate failure rates, while electronic interactions between the many adjacent receiving  
408 elements can lead to non-trivial instrumental effects. The Murchison Widefield Array  
409 (MWA) employs phased array antenna elements (tiles), which improve collecting area at  
410 the expense of complex beam shapes. Advanced electromagnetic simulations have pro-  
411 duced the Fully Embedded Element (FEE) simulated beam model which has been highly  
412 successful in describing the ideal beam response of MWA antennas. This work focuses  
413 on the relatively unexplored aspect of various in-situ, environmental perturbations to  
414 beam models and represents the first large-scale, in-situ, all-sky measurement of MWA  
415 beam shapes at multiple polarizations and pointings. Our satellite-based beam measure-  
416 ment approach enables all-sky beam response measurements with a dynamic range of  
417 ~ 50 dB, at 137 MHz.

### 418 3.2. INTRODUCTION

419 The pursuit for deeper, higher resolution astronomical observations for new scientific  
420 programs has led to the adoption of low-frequency radio interferometer arrays. Large  
421 numbers of relatively simple dipoles, coherently synthesized together, have angular res-  
422 olutions capable of exceeding the largest traditional dish telescopes. Notably, some of  
423 the largest interferometers are now the size of the Earth and beyond. These instruments  
424 are ideal for investigations from the local to the early universe. Unfortunately, the spec-  
425 tral windows relevant to such observations are often contaminated by radio frequency  
426 interference (RFI) from FM radio, television, and other man-made sources, necessitat-  
427 ing that these sensitive instruments be located at some of the most remote and least  
428 populous regions of the world.

429 Electronic interactions between the large number of identical and adjacent elements  
430 in an interferometer can lead to complex instrumental responses, exacerbated by dispro-  
431 portionate dipole failure rates due to harsh environmental conditions. This underpins  
432 the importance of accurate instrumental beam models which will enable precise calibra-  
433 tion of data and increase the sensitivity of various science investigations.

434 The Murchison Widefield Array (MWA<sup>\*</sup>; Tingay et al., 2013; Wayth et al., 2018) is a pre-  
435 cursor to the Square Kilometer Array (SKA<sup>†</sup>), located at the Murchison Radio-astronomy  
436 Observatory, in the remote western Australian outback. Designed to observe the low-  
437 frequency radio sky between 80 and 300 MHz, one of the MWA’s key science goals is  
438 detection of redshifted 21 cm emission from the Epoch of Reionization (EoR) (Bowman  
439 et al., 2013; Beardsley et al., 2019b). In this work we will explore the in-situ measurement  
440 of MWA beam shapes, broadly in the context of EoR science.

441 The high dynamic range of EoR experiments, coupled with the intrinsic chromatic  
442 nature of radio interferometers can introduce spectral structure variations, leading to  
443 calibration errors which must be constrained to high levels of precision (e.g. Barry et al.,  
444 2016; Trott & Wayth, 2016; Patil et al., 2017). The Fully Embedded Element (FEE) beam  
445 model (Sutinjo et al., 2015; Sokolowski et al., 2017) is a cutting-edge electromagnetic  
446 simulation of the tile response using the FEKO<sup>‡</sup> simulation package which can be used  
447 in EoR pipelines such as the RTS and FHD (Mitchell et al., 2008; Sullivan et al., 2012; Barry  
448 et al., 2019a). While accurate simulations of the instrumental beam has been crucial in  
449 improving calibration, simulations reflect ideal conditions, which often do not perfectly  
450 represent the in-situ reality. This is especially true for the MWA, located in a remote  
451 harsh desert, where multiple environmental factors may perturb instrumental beams  
452 from their ideal behaviour.

453 A relatively unexplored aspect of the calibration of radio interferometric data is the  
454 instrumental beam. Errors in beam models can introduce flux calibration and polariza-  
455 tion errors which may significantly impede the detection of the EoR signal. Simulations  
456 by Joseph et al. (2019) show that beam deformations due to broken dipoles can introduce  
457 biases in the 2D power spectrum (PS) up to two orders of magnitude above the expected  
458 EoR signal. Laboratory measurements and simulations by Neben et al. (2016a) reveal  
459 that inter-tile beam variation due to beamformer errors make foreground subtraction

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\*<http://www.mwatelescope.org>

†<https://www.skatelescope.org>

‡<http://www.feko.info>

460 infeasible. This is not an insurmountable issue for scientific studies which plan on util-  
461 izing a foreground avoidance approach, as it is shown that beamformer errors do not  
462 contribute significant spectral structure into the theoretically foreground-free regions  
463 of the power spectrum.

464 Spectral features of  $\sim 10^{-5}$  in the antenna or receiver system can hinder the detection  
465 of the EoR signal (Barry et al., 2016). It is possible that spectral structure of this scale  
466 could be introduced via errors in beam calibrations. Local environmental effects can  
467 be large contributors to beam distortions and it is unclear in precisely what ways these  
468 distortions contribute spectral structure to the PS, emphasising the requirement for ex-  
469 ceptionally well characterised individual beam models for more sophisticated analysis  
470 of EoR data.

471 This paper is presented in the context of EoR science, but has broad implications and  
472 the scope to significantly inform a wide variety of science cases which utilise data from  
473 wide-field radio interferometers. For example, radio polarimetry studies using the MWA  
474 have found significant flux leakage from Stokes I into other Stokes parameters (Bernardi  
475 et al., 2013; Lenc et al., 2017, 2018). For a Zenith pointings (-27° declination) leakage  
476 was  $\sim 1\%$  and  $\sim 4\%$  at the edge of the primary beam, increasing to a range of 12-  
477 40% at off zenith pointings. The GaLactic and Extragalactic All-sky MWA (GLEAM)  
478 survey (Wayth et al., 2015; Hurley-Walker et al., 2014, 2017) found beam errors cause  
479 frequency and declination dependant errors in Stokes I. Surveys such as GLEAM form  
480 the basis for calibration of EoR observations, making a correct flux scale essential. The  
481 increasing unreliability of the beam model, away from zenith, causes surveys such as  
482 GLEAM to only use the central half-power portion of the primary beam. Accurate beam  
483 models would enable the use of a larger portion of the beam with confidence, presenting  
484 the opportunity for a significant increase in sensitivity and thus faster experiments and  
485 better utilisation of precious telescope time.

486 A traditional method of beam measurement, known as radio holography, utilises drift  
487 scans of celestial sources of known flux densities to probe cross-sectional slices of the  
488 primary beam (e.g. Nunhokee et al., 2020; Berger et al., 2016; Pober et al., 2012; Thyagarajan  
489 et al., 2011; Bowman et al., 2007). Pulsar holography has been proposed to improve  
490 polarised beam measurements (Newburgh et al., 2014). A significant impediment to such  
491 methods is the faint nature of celestial sources which often have insufficient flux to probe  
492 the depths of the beam sidelobes and nulls, especially since wide-field instruments such  
493 as the MWA are sensitive to the whole sky.

494 An alternate method being explored is the use of radio transmitters mounted on com-  
495 mercially available drones (e.g. Jacobs et al., 2017; Chang et al., 2015). This technique  
496 has been used as an in-situ validation of two SKA-Low prototype arrays (Paonessa et al.,  
497 2020) and LOFAR\* antennas (e.g. Ninni et al., 2020; Bolli et al., 2018; Virone et al., 2014). A  
498 distinct advantage of this approach is the control and repeatability of drone flight paths,  
499 at multiple frequencies, enabling broadband characterization of beam shapes. While  
500 promising, this method comes with a set of drawbacks. Drones have limited altitude  
501 ranges and thus operate in the near-field of the instrument as opposed to astronomical  
502 observations which occur in the far-field. This is particularly relevant to wide-field in-  
503 struments, where the projection of the drone mounted transmitter beam couples to the  
504 Antenna Under Test (AUT) beam, and is exacerbated as the drone moves further from

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\*<http://www.lofar.org>

505 zenith. Finally, the use of bright radio receivers at radio-quiet zones make such methods  
506 challenging for large interferometric arrays such as the MWA, LOFAR, HERA\* and the  
507 upcoming SKA-Low.

508 The final method used to measure beam shapes and the focus of this paper, utilises  
509 satellites as bright radio sources with known trajectories, to probe cross-sectional slices  
510 of the AUT. Advantages of this method include: bright satellites enabling high dynamic  
511 range observations of the beam and sidelobes; sources emitting in the far field; the preci-  
512 sion of orbital tracks creating new slices of the AUT beam with each orbit. This method  
513 was neatly demonstrated by [Neben et al. \(2015\)](#) using a test MWA tile and by [Neben](#)  
514 [et al. \(2016b\)](#) using a prototype HERA dish at the NRAO Green Bank Observatory†. The  
515 work of [Line et al. \(2018\)](#) represents the first in-situ demonstration of this method at the  
516 MWA site.

517 This paper represents the first large-scale, in-situ, all-sky measurement of MWA beam  
518 shapes at multiple polarizations and pointings, with the aim to quantify inter-tile vari-  
519 ations and measure environmental beam distortions at 137 MHz using communication  
520 satellites. Our methodology demonstrates a passive parallel monitoring system, which  
521 measures the beam shapes of MWA tiles in parallel to regular observations with no dis-  
522 ruption to the operation of the telescope. As this setup was built using cheap off-the-shelf  
523 components, and the analysis is carried out using our open-source python‡ package  
524 called EMBERS§ (Experimental Measurement of BEam Responses with Satellites) ([Chok-](#)  
525 [shi et al. 2020](#)), we present it as a prime candidate for a passive beam monitoring system  
526 for large interferometric arrays such as the MWA, HERA, LOFAR and SKA-Low. As Radio  
527 Frequency Interference (RFI) encroaches on the last remaining radio-quiet observatories,  
528 archival data becomes ever more valuable. The addition of measured beam shapes could  
529 be critical to the analysis of this data in the future, when more sophisticated analysis  
530 techniques are developed.

531 A description of the MWA Telescope, experimental setup and data acquisition sys-  
532 tem are explained in Section 3.3, following which Section 3.4 outlines our data analysis  
533 method. In Section 3.5 we present challenges encountered in our analysis, experimental  
534 biases and the results. Finally, in Section 3.6, we discuss implications of this work and  
535 possible future directions.

### 536 3.3. EXPERIMENTAL METHOD

537 The approach taken in this experiment is an extension of investigations presented in  
538 [Line et al. \(2018\)](#) and [Neben et al. \(2015\)](#). The premise of this work is based around  
539 using radio satellites, with well known orbital trajectories, to probe the beam response  
540 of MWA tiles. The power received by the Antenna Under Test (AUT) is the product  
541 of the beam response  $B_{AUT}$  and the flux transmitted by the satellite  $F$ . A reference  
542 antenna with a simple, well known beam response  $B_{ref}$  is used to record the modulation  
543 of the transmitted flux, and can subsequently be used to compute the beam shape of the  
544 AUT. The power received by the AUT and reference antenna are  $P_{AUT} = B_{AUT}F$  and

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\*<https://reionization.org>

†<https://greenbankobservatory.org>

‡<https://www.python.org>

§<https://embers.readthedocs.io>

Table 3.1: Reference and MWA tiles used in the Experiment. Each tile is dual-polarised with both XX and YY dipoles. For example, the rf0 tile has rf0XX and rf0YY arrays.

rf0	rf1	S06	S07	S08	S09	S10	S12
S29	S30	S31	S32	S33	S34	S35	S36

545  $P_{\text{ref}} = B_{\text{ref}}F$  respectively. These expression can be reduced to give us the response of the  
 546 AUT, described by:

$$B_{\text{AUT}} = \frac{P_{\text{AUT}}}{P_{\text{ref}}} B_{\text{ref}}. \quad (3.1)$$

547 With each satellite pass, we measure a cross sectional slice of the AUT beam response.  
 548 With sufficient observation time, an all-sky beam response is built up.

### 549 3.3.1. *The Murchison Widefield Array*

550 The MWA is an aperture array telescope, with 128 receiving elements or tiles, each con-  
 551 structed from a grid of  $4 \times 4$  dual polarization bow-tie dipoles, mounted on a  $5 \times 5$  m  
 552 reflective metal mesh (Tingay et al., 2013). The two orthogonal linear polarizations of the  
 553 MWA tiles are labeled XX and YY, with dipoles aligned along the East-West and North-  
 554 South directions respectively. MWA tiles have a wide field of view, with a full-width  
 555 half-maximum  $\sim 25^\circ$  at 150 MHz, which can be steered using an analogue delay-line  
 556 beamformer. The beamformers have a set of quantised delays available, which results in  
 557 a set of 197 discrete pointings to which the beamformer can point the phase-center of  
 558 the MWA beam. The phased array design of MWA tiles improves the collecting area of  
 559 tiles, at the expense of additional complexity introduced to the beam shapes.

### 560 3.3.2. *Data acquisition*

561 The experimental setup used in this work is based on Line et al. (2018) and expanded to  
 562 accommodate our new science goals which differ from previous methods in a few key  
 563 ways.

564 We measure the all-sky beam response of 14 MWA tiles, over a 6 month period, at  
 565 both instrumental polarizations (XX, YY) and at multiple pointings using ORBCOMM\*  
 566 communication, METEOR† and NOAA‡ weather satellites. This work is the first demon-  
 567 stration of parallel, in-situ beam measurements without disruption to the telescope's  
 568 observational schedule. The 14 MWA tiles are a part of the inner core of the compact  
 569 configuration of the MWA array, located within the "Southern Hex" as shown in Figure  
 570 3.1. The names of the tiles can be found in Table 3.1. In addition to the Zenith pointing  
 571 of the telescope, measurements of the beam response are carried out at two off-zZenith  
 572 pointings (see Table 3.2).

573 Radio frequency (RF) signals are simultaneously recorded from 14 MWA tiles and two  
 574 reference antennas, in both XX and YY polarizations. The reference antennas are con-

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\*<https://www.orbcomm.com/en/networks/satellite>

†<http://www.russianspaceweb.com/meteor-m.html>

‡<https://www.noaa.gov/satellites>

Table 3.2: MWA beamformer pointings used in this work

MWA Pointing	Altitude	Azimuth	Integration [h]
0	90°	0°	~ 900
2	83°11'28.32"	90°	~ 350
4	83°11'28.32"	270°	~ 350

575    stuctured using a single dual polarization MWA dipole, centered on a  $5 \times 5$  m conductive  
 576    ground mesh. Custom-built RFI shielded circuits are used to power the Low Noise Am-  
 577    plifiers (LNAs) within the dipole, and retrieve data via coaxial cables. These field boxes  
 578    contain secondary LNAs, to further amplify RF signals, and Bias-Ts which facilitate data  
 579    and power transfer through coaxial cables. These field boxes are placed near the ref-  
 580    erence antennas and are connected with long coaxial cables, to RF Explorers\* located  
 581    within a RFI shielded hut approximately 50 m away. RF signals from the tiles are ac-  
 582    quired inside the MWA receivers (see Tingay et al., 2013), using beam splitters, after  
 583    amplification and filtering by the Analogue Signal Conditioning unit. These are passed  
 584    to RF Explorers installed within the receivers.

585    The RF Explorers are set to have a spectral resolution of 12.5 kHz, sampling 112 fre-  
 586    quency channels between 137.150 MHz and 138.550 MHz. This frequency window was  
 587    chosen to observe Meteor and NOAA weather satellites and the ORBCOMM constella-  
 588    tion of communication satellites, which provide excellent sky coverage. The signal is  
 589    acquired at a rate between 6 - 9 samples per second, limited by the hardware in the RF  
 590    Explorers. A set of five Raspberry Pi<sup>†</sup> single-board computers are used to control and  
 591    retrieve data from the 32 RF explorers connected to 14 MWA tiles and 2 reference an-  
 592    tennas. The positions of the antennas can be seen in Figure 3.1. USB hubs are used to  
 593    power and facilitate the control of multiple RF Explorers by a single Raspberri Pi. An  
 594    outline of our experimental setup can be found in Figure 3.2.

595    The Raspberri Pi's are connected to the MWA network via ethernet cables, enabling  
 596    remote control over the experiment. Network access allows the synchronisation of the  
 597    Raspberri Pi's by syncing them to the same NTP server. The Raspberri Pi's control the  
 598    RF Explorers using a custom python script and the pySerial<sup>‡</sup> module. Every 24 hours,  
 599    a scheduled cron job<sup>§</sup> transfers the recorded RF data to an external server and, using  
 600    the at<sup>¶</sup> command, schedules a day of 30 minute observations across all the RF Explorers.

601    The beam splitters allowed the experiment to run concurrently with normal MWA op-  
 602    erations, meaning the pointing of the telescope was dictated by the regular observational  
 603    schedule. A large amount of data was recorded using this setup, invariably including a  
 604    significant portion irrelevant to this project. Though the experiment was plagued by  
 605    technical failures of the RF Explorers, USB hubs and a rare lightning strike, between  
 606    12<sup>th</sup> September 2019 and 16<sup>th</sup> March 2020, over 4000 hours of raw data were collected.

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\*<http://rfexplorer.com>

<sup>†</sup><https://www.raspberrypi.org>

<sup>‡</sup><https://pythonhosted.org/pyserial>

<sup>§</sup><http://man7.org/linux/man-pages/man8/cron.8.html>

<sup>¶</sup><http://man7.org/linux/man-pages/man1/at.1p.html>

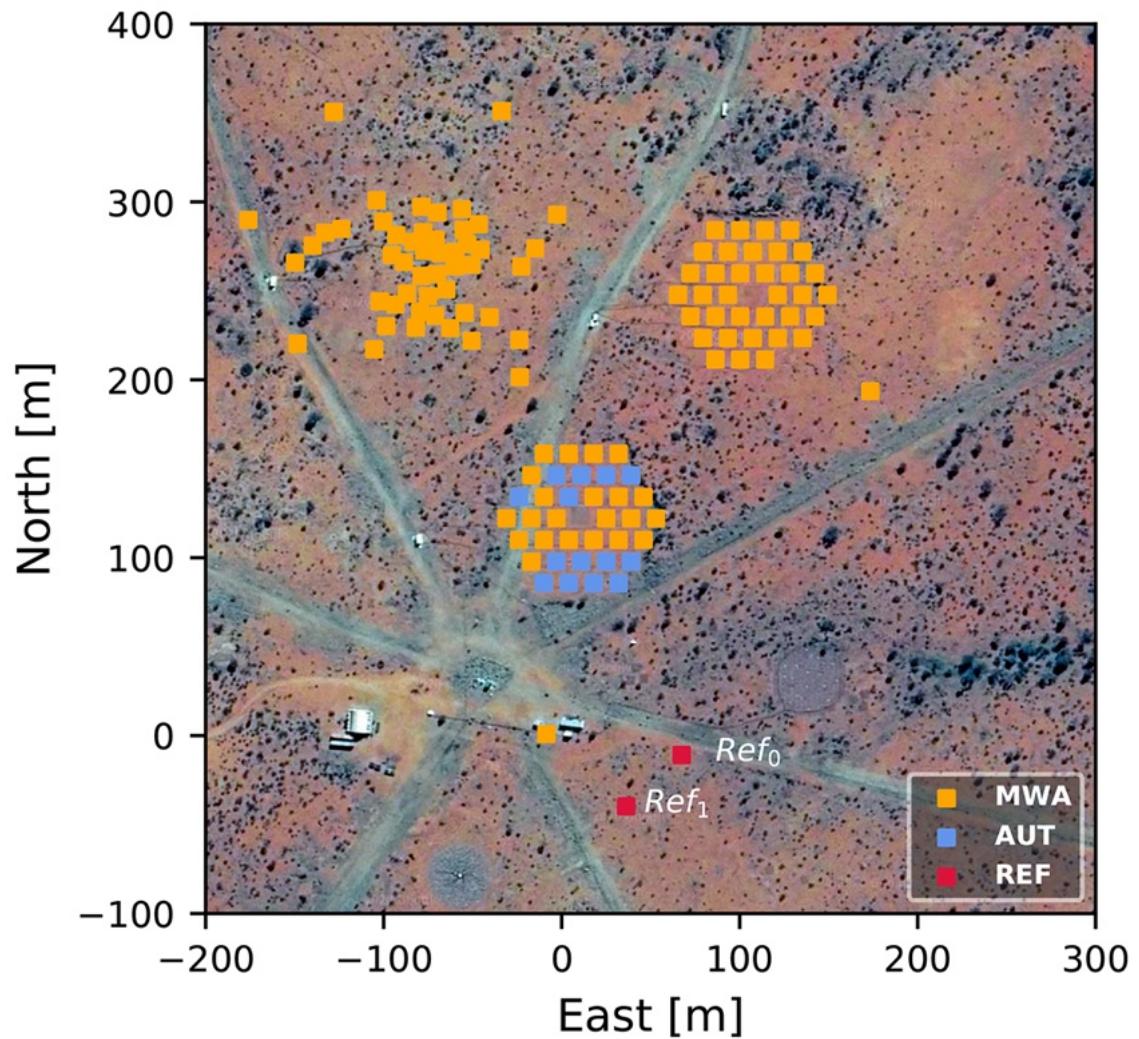


Figure 3.1: The positions of the AUTs (blue) and the Reference antennas (red). The ochre points represent the rest of the compact core of the MWA.

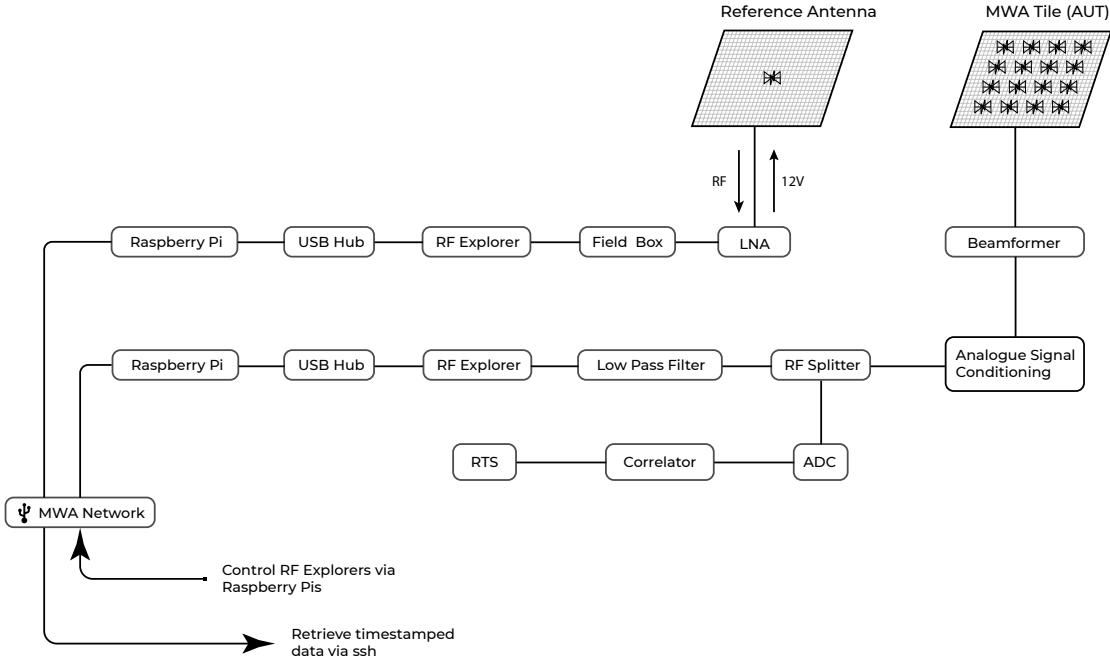


Figure 3.2: Flow chart of our experimental setup to measure MWA beam shapes. **Top:** The reference dipole receives satellite signals which is amplified by a Low Noise Amplifier (LNA). A Bias-T in the field box supplies the LNA with a 12V power supply and transmits the satellite signal from the dipole to the field box. Long coaxial cables carry the amplified signal to a RFI-shielded hut for analysis by a RF Explorer, the results of which are saved by a Raspberry Pi computer. **Bottom:** RF signals received by the Antenna Under Test (MWA Tile) are fed to an analogue beamformer, which introduces time delays to the signals from the 16 dipoles corresponding to the pointing of the telescope. The signals are combined and transmitted via long coaxial cables to an MWA receiver. Within the receiver, the Analogue Signal Conditioning unit performs amplification and filtering before passing it to a signal splitter. The splitter sends half the signal on its usual path to the correlator, while the other half passes through a low-pass filter before being analysed by a RF Explorer and saved by a Raspberry Pi. The USB hubs supply power to the RF Explorers and facilitates the transfer of data from multiple RF Explorers to the Raspberry Pi. The Raspberry Pis are connected to the MWA network, from which they can be remotely controlled and transfer data.

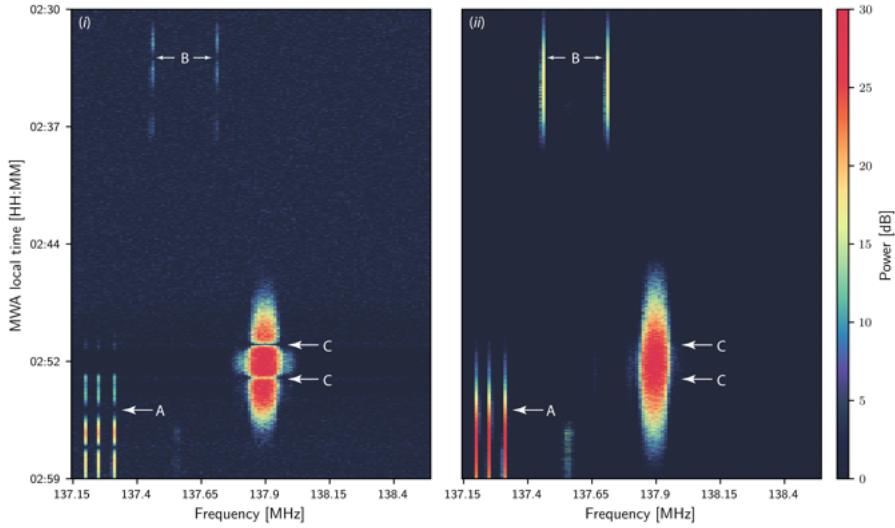


Figure 3.3: A sample set of raw data observed between 2:30AM and 3:00AM on 10/10/2019. The image on the left (i) is tile S10XX while the image on the right is data from reference ref0XX. Both sets of data have been scaled to have a median power of 0 with a dynamic range of 30dB. Interesting features have been annotated at the same positions in each plot with arrows indicating points of stark differences between the plots. The flux received by the MWA tile (i) drops to zero at the positions of the nulls at the edge of the MWA primary beam, which are absent in the reference antenna (ii). We find that ORBCOMM satellites generally have narrow band transmissions, occupying no more than 2 channels, as seen in A and B. Meteor weather satellites have significantly broader spectral footprints, occupying up to 10 channels, as seen in C.

### 607 3.4. DATA ANALYSIS

608 A sample of the raw data can be seen in Figure 3.3, in the form of a waterfall\* plot. OR-  
 609 BC COMM satellites were found to transmit in narrow frequency bands, occupying up to  
 610 two 12.5 kHz channels. In contrast, weather satellites exhibit a broader spectral signa-  
 611 ture, occupying up to 10 consecutive channels. In Neben et al. (2015), an ‘ORBCOMM  
 612 user interface box’ was used to match satellite ephemerides to transmission frequencies  
 613 of satellites above the horizon. As this technology is not commercially available, Line  
 614 et al. (2018) used satellite ephemerides, published by Space-Track.org†, to match satel-  
 615 lites above the horizon to observed RF signals seen in waterfall plots similar to Figure  
 616 3.3 and manually create a map of ORBCOMM transmission frequencies.

617 Multiple ORBCOMM satellites are often above the horizon simultaneously, and are  
 618 observed to periodically shift transmission frequencies to avoid inter-satellite interfer-  
 619 ence. With observations spanning more than 6 months, and the resulting large volume  
 620 of data it became infeasible to manually determine the transmission frequencies of every  
 621 satellite pass. This necessitated the development of an automated system of matching  
 622 satellite ephemerides and RF data, described in detail in Section 3.4.2.

\*time vs. frequency

†<https://www.space-track.org>

623    3.4.1. *Data conditioning*

624    Before the analysis of our data can proceed, it must be pre-processed to ensure that  
625    sensible comparisons can be drawn between the tiles and references. A complication  
626    we encountered was that different RF Explorers recorded the data at different temporal  
627    rates, ranging between 6 and 9 Hz. We attribute this issue to two distinct batches of RF  
628    Explorers used. The first batch of 8 were purchased in 2017, and recorded data at a rate  
629    between 6-7 samples per second, while the remaining 24 RF Explorers were purchased  
630    in 2019 and recorded data at a rate between 8-9 samples per second. Though the model  
631    numbers of the RF Explorers and their configuration settings were identical, we infer  
632    that there must have been hardware improvements in the more recently manufactured  
633    modules.

634    An optimal balance between the RF Explorers sampling rate, Signal-to-Noise and the  
635    sky coverage of our selected satellites, determines the N-side of our HEALPix ([Gorski et al., 2005](#)) maps. We use a N-side of 32, corresponding to an angular resolution of 110  
636    arcmins. An important consideration at this stage was that Satellites in Low Earth Orbit  
637    typically transit the visible sky in 5-15 minutes, depending on their orbital altitudes  
638    ([Cakaj et al., 2009](#)). Typical transit periods of satellites used in this experiment were  
639    observed to be in the 15 minute range, at which satellites took  $\sim$ 9 seconds to transit  
640    across one 110 arcmin HEALPix pixel.

642    The calculation above indicates that the raw data is highly oversampled, providing a  
643    certain leeway to get around the issue of varied temporal sampling. An iterative Sav-  
644    itzky–Golay (SavGol) filter is selected to smooth the raw noisy data, while preserving it's  
645    high dynamic range. Initially, a SavGol filter with a small window is used to preserve the  
646    depth of the null in the beam response, followed by a second SavGol filter with a larger  
647    window to smooth short time-scale noise present in the data. We then interpolate our  
648    data down to a 1 Hz frequency, while retaining multiple data points per HEALPix pixel.  
649    This enables us to compare our tile and reference data accurately. Figure 3.4 shows the  
650    concurrence between the raw data and the SavGol smoothed, interpolated data.

651    A noise threshold is defined at this stage, allowing further analysis to be limited to  
652    RF satellite signals above the noise floor. In a 30 minute observation, typically 3-7 of  
653    the 112 frequency channels contain satellite signals. These channels are identified to  
654    first order by having peak signals above a single standard deviation ( $\sigma_{\text{raw}}$ ) of the data.  
655    Excluding these occupied channels, the Median Absolute Deviation (MAD\*)  $\sigma_{\text{noise}}$  and  
656    the median  $\mu_{\text{noise}}$  of the remaining noisy channels are used to define a noise threshold  
657    shown in Equation 3.2. The noise threshold for both  $P_{\text{AUT}}$  and  $P_{\text{ref}}$  is computed for every  
658    time-step with

$$P_{\text{noise}} = \mu_{\text{noise}} + \sigma_{\text{noise}}. \quad (3.2)$$

659    If  $P < P_{\text{noise}}$  for either the AUT or reference data, the time-step data is flagged as “noisy”.

660    As observations were carried out in parallel to the regular observational schedule  
661    of the MWA, satellite RF data is recorded at all pointings the telescope visited over the  
662    course of the experiment, accumulating over 4000 hours of raw data. The total integrated  
663    data at most pointings fell far short of the  $\sim$  400 hours required to make maps with a  
664    N-side of 32. The Zenith and two EoR 2, 4 pointings met this criteria, resulting in  $\sim$  1600

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\*MAD - robust statistic more resilient to outliers than standard deviation

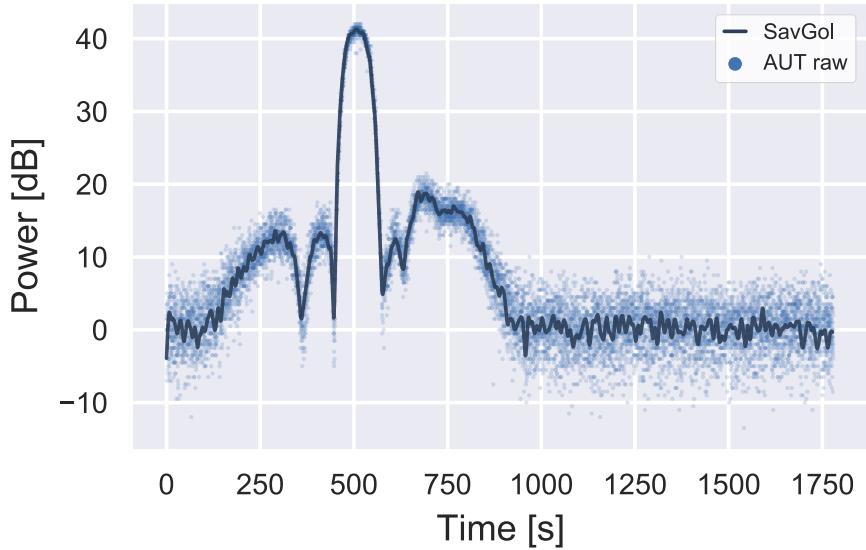


Figure 3.4: A single channel of raw data with a bright satellite pass. The solid curve is the SavGol smoothed data, interpolated down to 1 Hz.

665 hours of usable data. The data is sorted based on pointing, and separate maps are created  
 666 for each. See Table 3.2 for details about the pointings and the amount of usable data  
 667 collected at each.

### 668 3.4.2. *Satellite ephemerides*

669 Satellites transmit data to Earth on their allocated “downlink” frequency, the exact lo-  
 670 cation of which are often proprietary. Reliable sources of data regarding spectrum al-  
 671 locations in the 137-138 MHz band are scarce and often outdated. Our initial estimate  
 672 of  $\sim 70$  active satellites within our window was optimistic, with a total of 18 satellites  
 673 being regularly observed in our data. Some of our initial satellite candidates were no  
 674 longer actively transmitting, while others presumably transmitting marginally outside  
 675 our frequency window. Table 3.3 contains information on the satellites we used. The  
 676 orbital parameters (ephemeris) of most satellites are recorded multiple times a day by  
 677 USSPACECOM and are published by Space-Track.org. The ephemerides of our satellites  
 678 are downloaded in the form of Two Line Elements\* (TLEs). A custom python script  
 679 reads these TLEs and accurately (within  $\sim 10$  arcsec at epoch) computes when the satel-  
 680 lites are above the horizon and their trajectories in the sky, at the MWA telescope . The  
 681 Skyfield<sup>†</sup>(Rhodes, 2019) software package was instrumental to these calculations.

### 682 3.4.3. *Frequency mapping*

683 The sheer quantity of data made it infeasible to manually determine transmission fre-  
 684 quencies of our satellites. Instead, we developed a method to automatically cross match  
 685 satellite ephemerides and raw RF data, identifying the transmission frequency of every

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\*<http://www.satobs.org/element.html>

<sup>†</sup><https://rhodesmill.org/skyfield>

Table 3.3: Satellite constellations and frequency bands.

Constellation	Spectral band [MHz]	Satellites observed
ORBCOMM	137.2 -137.800	15
NOAA	137.1 -137.975	2
METEOR	137.1 -137.975	1

satellite in each 30 minute observation. Using the ephemerides of each satellite, a temporal window within the RF data is identified, within which transmissions are expected to be found. We define a set of criteria to identify the correct frequency channel.

**Window Occupancy:**  $W_{RF}$  is the percentage of RF signal above the noise threshold  $P_{noise}$  (Eq. 3.2), within the temporal window. Identified satellites were required to have an occupancy in the range  $80\% \leq W_{RF} < 100\%$ . The lower limit accounts for satellite passes close to the horizon, where long noise-like tails are observed on either end of the satellite data.

**Power Threshold:**  $P_{peak}$  is introduced to set a minimum peak satellite power. It was observed that channels adjacent to a bright satellite pass were often observed to be contaminated with lower power, noise-like, RF signals. This probably occurs due to transmission bandwidth marginally exceeding the 12.5 kHz channel width of the RF Explorers, leading to spectral leakage. Such channels typically have peak power in the range of 10-15 dB, compared to the 20-40 dB peak powers. To eliminate these contaminated channels, we require identified channels to have  $P_{peak} \geq 15\text{dB}$ .

**Triplets:** It is common to observe pairs or triplets of almost identical signal, as seen in labels A, B of Figure 3.3, which often pass both filters described above. In such cases, the channel with the higher window occupancy is selected, indicative of a superior match between RF data and satellite ephemerides.

While this method has been highly effective, it is not foolproof. At later stages in the analysis, described in Section 3.5.3, obvious errors in this method are eliminated by implementing a goodness of fit test between measured beam profile and the FEE simulated model.

#### 3.4.4. Map making

FEKO simulations were run to create simulated beam models of the reference antennas  $B_{ref}$ , using on-site measurements of the ground screen and dipole positions, identical to those used to generate the FEE models of the MWA beam. These models are used to make maps of the tile responses by computing  $P_{AUT}/P_{ref} \times B_{ref}$  (Eq. 3.1) for each satellite pass, for every pair of AUT and Reference. The different amplifications that the RF signals undergo along the two distinct signal paths – through the field box for the reference data, and via the beamformer and the Analogue Signal Conditioning unit for the AUTs – have not been considered (see Figure 3.2). Since we are interested in the profile of the signal, rather than the absolute power, a least-squares method is used to assign each satellite pass, a single multiplicative gain factor  $G_{FEE}$ , effectively fitting it to power level of a corresponding slice of the FEE model.

This slice of the beam response is now projected onto a HEALPix map with a N-side of 32, using the satellite ephemerides, resulting in a map with an angular resolution of 110 arcmins, a good balance between integration per pixel and resolution. Each pixel of the map now contains a distribution of values from multiple satellite passes, the median of which gives us a good estimate of the beam response, without being influenced by outliers.

## 3.5. RESULTS

### 3.5.1. Null tests

Two reference antennas  $\text{ref}_0$  and  $\text{ref}_1$ , seen in Figure 3.5, were used in this experiment. This provides the ability to perform a null test to characterize the differences between the beam patterns of the references, and their FEKO simulated models. The ratio of the beam powers, for a set of perfect reference antennas, should ideally be unity and  $P_{\text{ref}0}/P_{\text{ref}1} = 1$  should hold true for all satellite passes. Deviations from this expression are indicative of systematics such as alignment errors and imperfections in the ground screen, soil, dipole or the surrounding environment.

The results of the null test are shown in Figure 3.6. The first row (subplots (i)-(iv)) shows slices of the  $\text{ref}_0$  HEALPix map along both East-West (EW) and North-South (NS) directions for XX and YY polarizations, respectively. The median of the distribution of values in each pixel is power  $P_{\text{ref}0}$ , while an estimate of the errors is determined from the Median Absolute Deviation  $\sigma_{\text{MAD}}$  of the distribution. These are compared to corresponding slices of the reference FEKO model  $B_{\text{ref}}$ , and the residuals  $\Delta_{\text{ref}0} = P_{\text{ref}0} - B_{\text{ref}}$  are fit with a third order polynomial. The second row (subplots (v)-(viii)) is an identical analysis carried out for the  $\text{ref}_1$  HEALPix map. The null test is performed in the third row (subplots (ix)-(xii)), where corresponding slices of  $\text{ref}_0$  and  $\text{ref}_1$  HEALPix maps are compared. The green data represents a pixel to pixel comparison between  $\text{ref}_0$  and  $\text{ref}_1$ , with error bars propagated in quadrature from the  $\sigma_{\text{MAD}}$  of each references. We also compare the fits to the residual power  $\Delta_{\text{ref}}$  (orange curve), seen in the lower panels of the first two rows of Figure 3.6.

An interesting pattern emerges in the residuals between the map slices and FEKO model  $\Delta_{\text{ref}}$  (Figure 3.6 (i)-(viii) lower panels). For zenith angles between  $30^\circ - 60^\circ$ , a systematic deficit of power is observed with residual power structure observed with deviations up to  $\pm 2$  dB from the FEKO reference models. This feature is investigated by summing the residuals of all four reference HEALPix maps and averaging the results in  $2^\circ$  radial bins. By classifying the data according to the progenitor satellite type, an illuminating pattern emerges, shown in Figure 3.7. We achieve a good fit of the radial residuals using a 8<sup>th</sup> order polynomial. Each satellite has a distinct and well defined residual structure. These residuals represent a profile measurement of the beam shapes of satellite transmitting antennas. This can be understood by considering that satellites primarily focus on transmitting data downwards, normal to the surface of Earth. As satellites rise above the horizon, the reference antennas observe RF transmitted power convolved with the sidelobes of the satellite beam shapes, which is attenuated away from its primary beam (pointed to the surface).

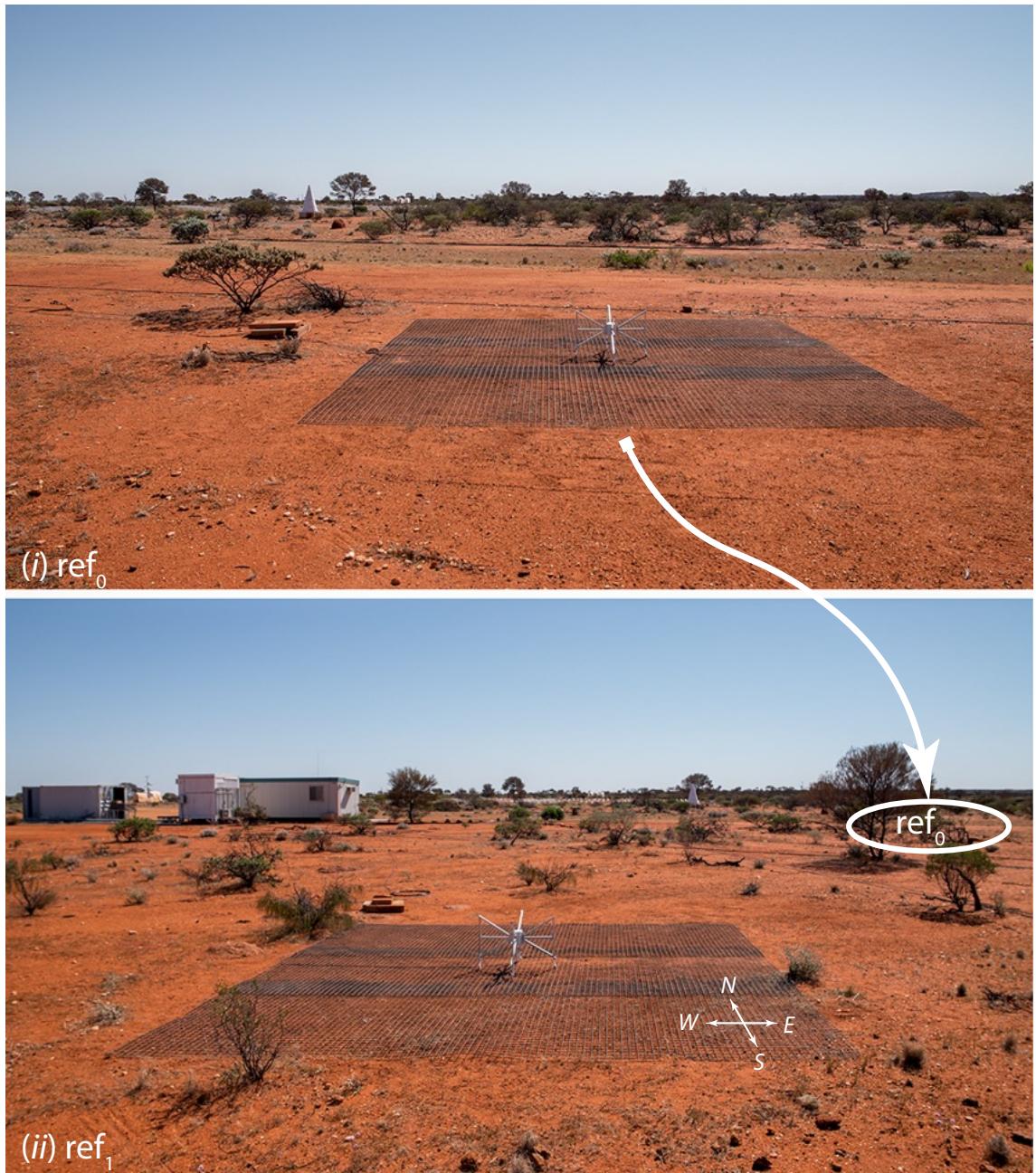
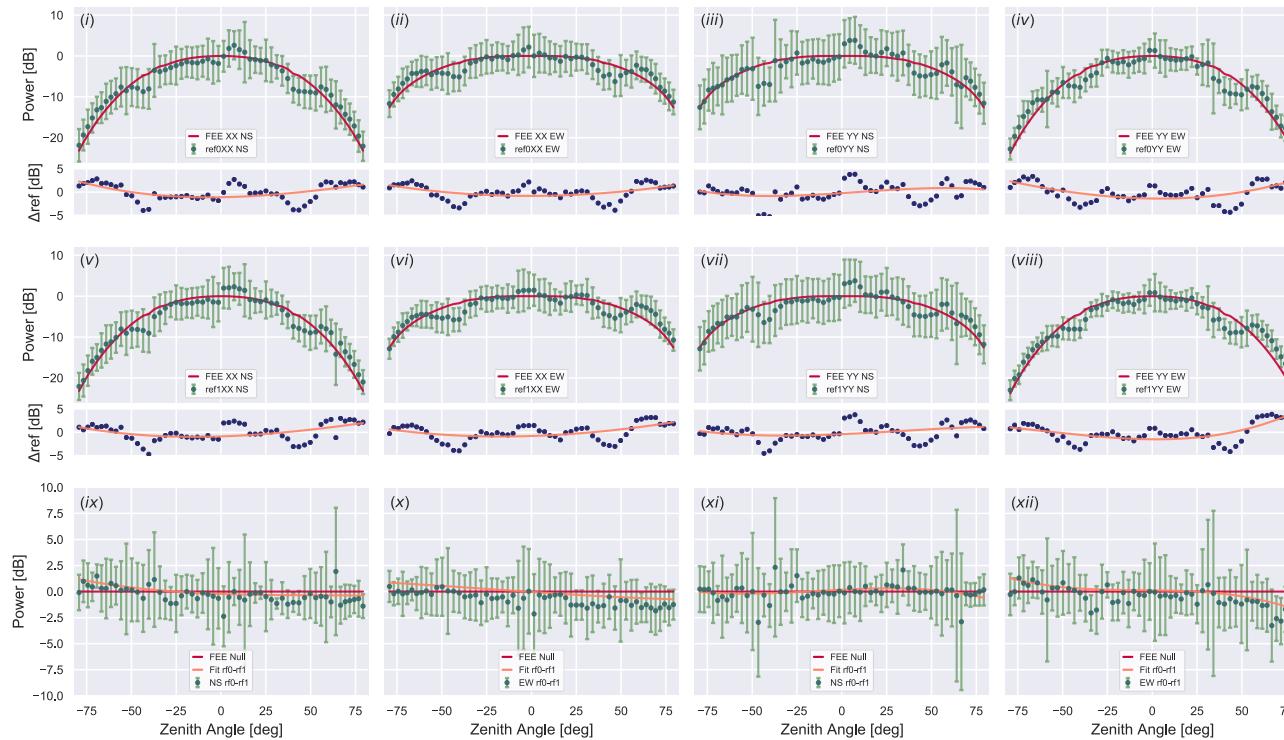


Figure 3.5: The reference antennas (i):  $\text{ref}_0$  and (ii):  $\text{ref}_1$  on site. In the bottom panel, the RFI shielded huts can be seen, as well as the position of  $\text{ref}_1$  in the distance behind a bush.



**Figure 3.6: Null Test Results:** The first row (i)-(iv) represent slices of HEALPix maps generated from RF data of  $\text{ref}_0$ . (i) and (ii) are North-South (NS) and East-West (EW) slices of the XX polarization of  $\text{ref}_0$  while (iii) and (iv) are matching NS, EW slices of the YY polarization of  $\text{ref}_0$ . The green data-points indicate the median value of each HEALPix pixel, with the median absolute deviation as the error bars. The crimson curves represent corresponding slices of the FEKO reference model (Section 3.4.4). The difference between the data and model  $\Delta\text{ref}$  are plotted in the lower panel as blue points. The orange curve is a third order polynomial fit to the residuals. The second row (v)-(viii) show an identical analysis performed on  $\text{ref}_1$ . The bottom row (ix)-(xii) are the null tests, each computed from the two preceding plots. In (ix), the crimson line represent the the ideal null test while the green data represents the difference between  $\text{ref}_0$  from (i) and  $\text{ref}_1$  from (v). The error bars are computed by propagating errors from (i) and (v) while the orange curve shows a third order fit to the null test. (x)-(xii) are similar to (ix), each being calculated from the two plots above it.

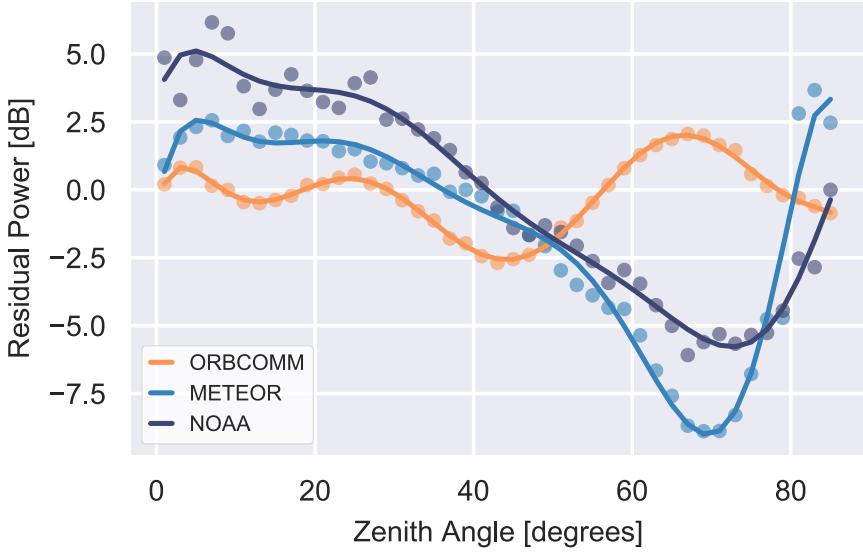


Figure 3.7: Radially averaged reference residual power, displaying unique beam profiles for each of the three types of satellites used in the analysis, validating our methodology and null tests.

The amplitude and structure of these residuals may appear significant to our analysis, but are in-fact accounted for by our primary Equation 3.1. This can be illustrated by considering the concurrent measurement of satellite data by both MWA and reference tiles. Any modulation encoded in the data transmitted by the satellites will be identically recorded by all antennas, convolved with individual tile beam shapes. The ratio of observed powers in Eq. 3.1 ( $P_{\text{AUT}}/P_{\text{ref}}$ ) will neatly divide out any satellite beam structure or modulation encoded within the incoming RF data.

We note the slightly exaggerated slope in the null test of the EW slice of the YY reference maps, as seen in the last column of Figure. 3.6 (subplots (iv), (viii), (xii)). On further inspection of subplot (viii), we note that the East edge of the  $\text{ref}_1$  receives  $\sim 2$  dB less, and the West edge receives  $\sim 2$  dB more power than the corresponding slice of  $\text{ref}_0$ . We suggest that this discrepancy probably results from a slight EW gradient in ground screen or the dipoles of the tile, which points the bore-sight of the dipole marginally off-zenith.

The agreement between the fits to the residuals (orange curve in subplots (ix)-(xii) of Figure. 3.6) and the expected null (red lines) represent a good validation of our experimental procedure described in section 3.3. We observe less than a  $\sim 0.5$  dB error in the central  $25^\circ$  of the reference model, corresponding to the primary lobe of the MWA beam at 137 MHz. These errors do increase as we move towards the horizon, reaching a maximum of  $\sim 2$  dB, in our most inaccurate reference. This validates the efficacy of our null test, in characterising systematic effects from the references, which propagate into the beam maps created in the following sections (see grey errorbars in Figure 3.12).

The null tests display a marginally better performance of reference tile 0 ( $\text{ref}_0$ ). Despite this, we have chosen to use reference tile 1 ( $\text{ref}_1$ ) in proceeding sections as hardware failures on  $\text{ref}_0$  resulted in more data and better sky coverage for  $\text{ref}_1$ .

788    3.5.2. *RF explorer gain calibration*

789    During the last stages of the experiment, we noticed that the very brightest satellite  
790    signals exceeded the maximum recommended power of the RF explorers, resulting in  
791    the internal amplifiers entering a non-linear regime. Unfortunately, the limited dynamic  
792    range of the RF Explorers coupled with the high dynamic range of satellite observations  
793    resulted in almost no leeway for errors in this regard. This effect was only present in  
794    RF Explorers recording data from MWA tiles, via the MWA receivers and is apparent in  
795    Figure 3.8, where the light blue raw tile data is  $\sim 6$  dB lower than a corresponding slice  
796    of the FEE model (yellow curve). This deficit of measured power in the primary lobe  
797    was unexpected as the primary lobe has been well characterized (Line et al., 2018) and  
798    validated by scientific studies which primarily use the primary lobe (e.g. Hurley-Walker  
799    et al., 2017) . The effort to recover the “missing” power led to the creation of a global  
800    gain calibration scheme.

801    It was observed that RF Explorers begin to leave their linear amplification zone at  
802    around -45 dBm\* and were definitely non-linear by -35dBm, where slices of the FEE  
803    model had visibly diverged from raw tile data (see Fig. 3.8). We begin by considering  
804    deformed AUT power  $P_{def}$ , non deformed reference power  $P_{ref}$  and slices of the FEKO  
805    reference  $B_{ref}$  and FEE MWA beam  $B_{FEE}$  models for a satellite pass. Once Equation 3.1  
806    is computed, information regarding absolute power recorded by the RF explorers is lost  
807    in favour of a normalized beam profile (see Section 3.4.4). Thus, gain calibration of the  
808    RF explorers must take place at the tile power level, before scaling or normalization  
809    processes distort the original power levels. A mask  $M_{def}$  is created using the region  
810    where the deformed tile power  $P_{def}$  exceeds -35dBm. This mask prevents the distorted  
811    sections of the measured primary beam from biasing the results of the multiple least-  
812    squares gain fits described below.

813    Equation 3.1 is used to compute the deformed beam slice  $B_{def}$  using  $P_{def}$ ,  $P_{ref}$  and  
814     $B_{ref}$ . To maintain the initial power level, we mask the deformed section of  $B_{def}$  using  
815    the mask  $M_{def}$  and use a least-squared method to determine a single multiplicative gain  
816    factor which will scale  $B_{def}$  down to the initial power level of  $P_{def}$ . A similar method is  
817    used to scale the slice of the FEE beam  $B_{FEE}$  down to the initial power level of  $P_{def}$ . The  
818    result of the scaling can be seen in Figure 3.8 where  $B_{FEE}$  (yellow) and  $B_{def}$  (light blue)  
819    have been successfully scaled to match at low powers while clearly displaying a deficit  
820    of power at the peak of the primary beam.

821    We can now empirically determine a gain calibration solution by looking at the resid-  
822    ual power ( $B_{FEE} - B_{def}$ ) of all satellite passes. The 2D histogram of all residual power  
823    is shown in Figure 3.9, with the horizontal axis representing power observed by the  
824    AUT RF explorers, and the vertical axis representing residual power. The figure dis-  
825    plays a bridged bimodal distribution, which can be explained by considering the profile  
826    shape of cross sectional slices of the MWA beam models. The nodes at the edges of the  
827    primary beam are sharply peaked and extremely narrow, leading to a dearth of obser-  
828    vational data points in such regions as satellites pass over them relatively quickly. The  
829    cluster of points at lower observed power is the result of satellites passing over the rel-  
830    atively broad secondary lobes of the MWA beam while the cluster at higher observed  
831    power comes from satellite passes transiting through the primary beam. For linear gain

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\* dBm - physical units of power, measured with respect to 1 milliwatt

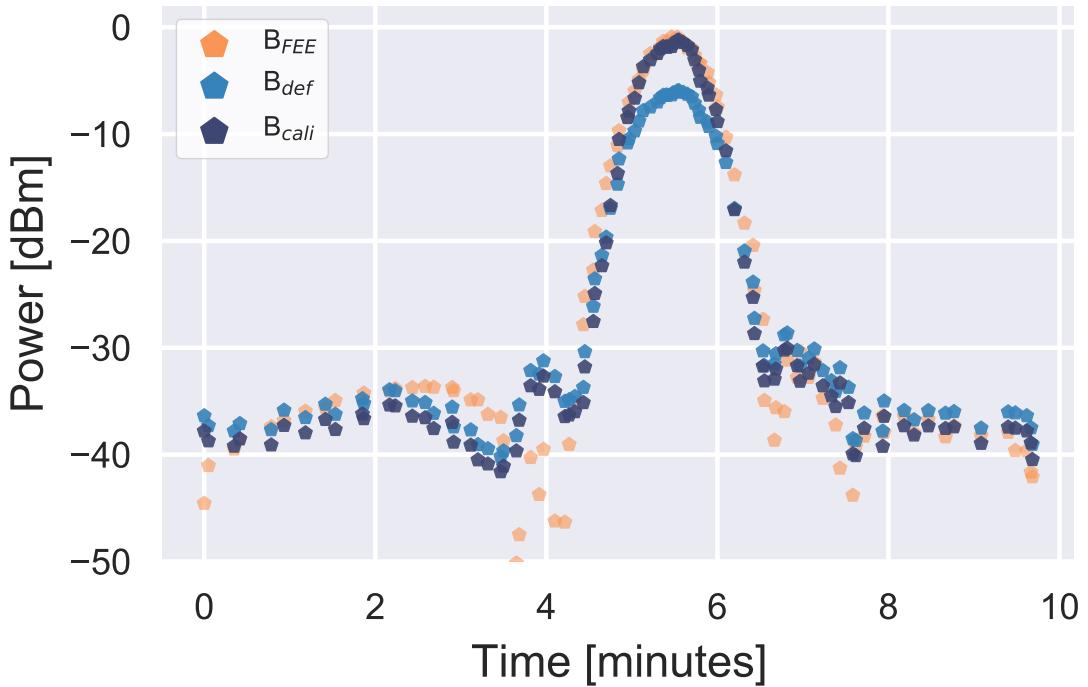


Figure 3.8: A bright satellite pass recorded by the non-linear gain of the AUT RF explorer, which results in a deformed beam model  $B_{def}$  compared to a corresponding slice of the FEE model  $B_{FEE}$ . The power of  $B_{def}$  is significantly lower than  $B_{FEE}$ , in the primary beam. The efficacy of the RF explorer gain calibration method is demonstrated by the dark blue data points  $B_{cali}$  which result from applying the gain calibration solution to the distorted beam model (light blue). The nulls of the FEE model extend beyond the depth of the recorded data due to the -50dB sensitivity of the experiment. A significant mismatch between  $B_{FEE}$  and  $B_{cali}$  is observed around the 4 minute timestamp. This error can probably be attributed to a combination of a gradient in the ground screen and a slight rotation of the tile, which lead to significant deviations around the edges of the steep nulls as explored in Section 3.6.

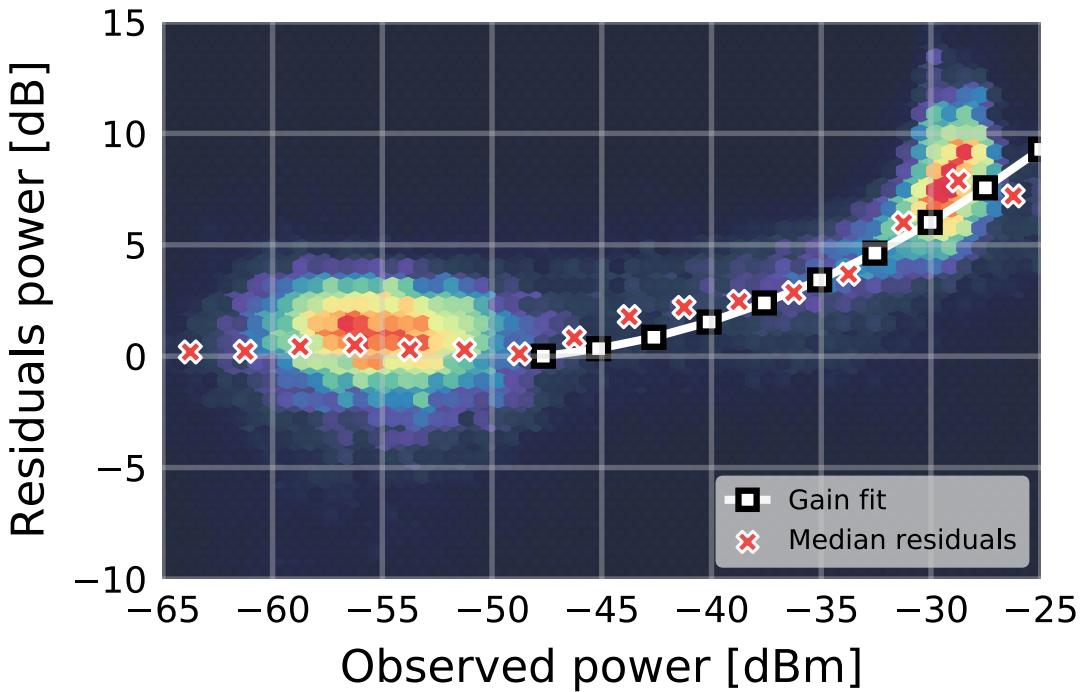


Figure 3.9: The 2D histogram distribution of high power distortions to RF signals. Ideally the residuals should have a value of 0 at all observed powers, indicating that the RF explorers reproduce input signals faithfully. The white curve is a 3<sup>rd</sup> order polynomial fit to the median values (black squares) of the data binned in  $\sim 4\text{dBm}$  intervals.

internal to the RF Explorer, one would expect the residuals to be  $\sim$  zero, while positive residuals result from non-linear gains. The white curve and associated black squares are a 3<sup>rd</sup> order polynomial fit to the median values (red crosses) of the data binned in  $\sim 4\text{dBm}$  intervals. This clearly demonstrates that the RF explorers gradually enter the non-linear regime at  $\sim -40\text{dBm}$  and exhibit residuals of  $\sim 6\text{dB}$  at observed powers of  $-30\text{ dBm}$ .

The result of applying the calibration solution developed above to a single satellite pass are seen in Figure 3.8 where  $B_{\text{def}}$  (light blue) is scaled up to  $B_{\text{cali}}$  (navy blue) and represents a much better fit to a slice of the fee model  $B_{\text{FEE}}$  (yellow).

The RF Explorer gain calibration technique presented in this section has been shown to be necessary but comes with a minor drawbacks. Primarily, the global nature of our method could result in the loss of potentially interesting structure present at the center of the primary lobe. The accuracy of the primary lobe has been validated by multiple studies (e.g. [Line et al., 2018](#); [Hurley-Walker et al., 2017](#)) and deviations are not expected. The gain correction was essential as the absolute scale of fluctuations in the more uncertain side-lobes, were determined by fitting satellite signals to the well characterized primary lobe. These corrections also enable us to regenerate all-sky beam maps which may be utilized in further studies. Future iterations of this experiment, which could be scaled to passively monitor the full MWA array or SKA-Low, will have to extensively characterize off-the-shelf components such as RF Explorers. Our characterization of the gain profile revealed that the accuracy of factory specification may not be sufficient for

853 experiments of such sensitivity and scale.

### 854 3.5.3. Tile maps

855 We now create MWA beam maps using the method described in Section 3.4 with the  
856 caveat that the RF explorers gain calibration solution described in Section 3.5.2 are ap-  
857 plied to all data from the AUT RF explorers. A single multiplicative gain factor, de-  
858 termined by least-squares minimization, is used to scale measurements to the level of  
859 the zenith-normalized FEE beam model. Before  $B_{AUT}$  can be projected onto a HEALPix  
860 map, it must pass a final goodness-of-fit test. The frequency mapping method described  
861 in Section 3.4.3 has been highly successful at dealing with the massive volume of data  
862 produced over the course of this experiment, but does exhibit an  $\sim 2\%$  failure rate, where  
863 the transmission frequency of satellites is misidentified. To catch these final outliers, a  
864 chi-squared p-value goodness-of-fit test between the scaled measured beam  $B_{AUT}$  and  
865 the FEE model  $B_{FEE}$  is implemented, with a threshold tuned to ensure that only the beam  
866 profiles with obviously wrong null positions are rejected. Successful satellite passes are  
867 projected onto a HEALPix map representative of an accurate all-sky MWA beam re-  
868 sponse.

869 A set of tile maps at multiple pointings and polarisations are shown in Figure 3.10,  
870 created with data from tile S08 and Ref<sub>1</sub>. The residual maps shown in the second and  
871 fourth row of Figure 3.10 display large gradients in power at the Southern and Eastern  
872 edges of their primary lobes. This effect is attributed to gradients in the ground screen  
873 of the MWA tiles. Such gradient can lead to systematic angular offsets from the intended  
874 pointing of the MWA tiles specified by the beamformers. This effect is most pronounced  
875 at the steep nulls surrounding the primary lobe where systematic displacements in null  
876 positions occur. The mismatch in the measured position of the nulls as compared to the  
877 FEE model manifest as the gradients observed in the residual maps of Figure 3.10.

878 We further investigate this effect to determine the gradient of the ground screens of  
879 our MWA tiles. This is achieved by displacing our measured beam maps and minimizing  
880 the residual power at the edge of the primary lobe. The gradient in the ground screens  
881 were determined to  $\sim 15$  arcmin resolution by interpolating our HEALPix maps to a  
882 higher resolution with NSIDE=256. Figure 3.11 shows the measured angular offset of  
883 our 14 tiles from the zenith pointing. Local surveys of the tiles in the Southern Hex  
884 have identified a gradual half degree gradient in the soil, from the North-West to the  
885 South-East which would result in all beams being offset by  $\sim 0.5^\circ$  towards the South-  
886 East, displayed as the black cross in Figure 3.11. This analysis shows a significant scatter  
887 in angular beam offsets, indicative of tile gradients ranging up to  $1.4^\circ$ , and vertical dis-  
888 placements exceeding 10 cm over a 5 m ground screen.

889 In Figure 3.12, NS and EW slices of the tile maps are compared to the corresponding  
890 FEE models. The first row (subplots (i)-(iii)) represent NS slices of the XX beam map of  
891 tile S08. The lower panels of these subplots explore residual power between measure-  
892 ments and the FEE model. The orange curve represents a 3<sup>rd</sup> order polynomial fit to  
893 the residual power, while the cyan shaded regions account for errors which can be at-  
894 tributed to the reference tiles, as seen from the null tests (See Section 3.5.1 and Fig. 3.6).  
895 The second row (subplots (iv)-(vi)) represents an identical analysis for the EW slice of  
896 the beam maps. The last two rows (subplots (vii)-(xii)) complete the analysis described

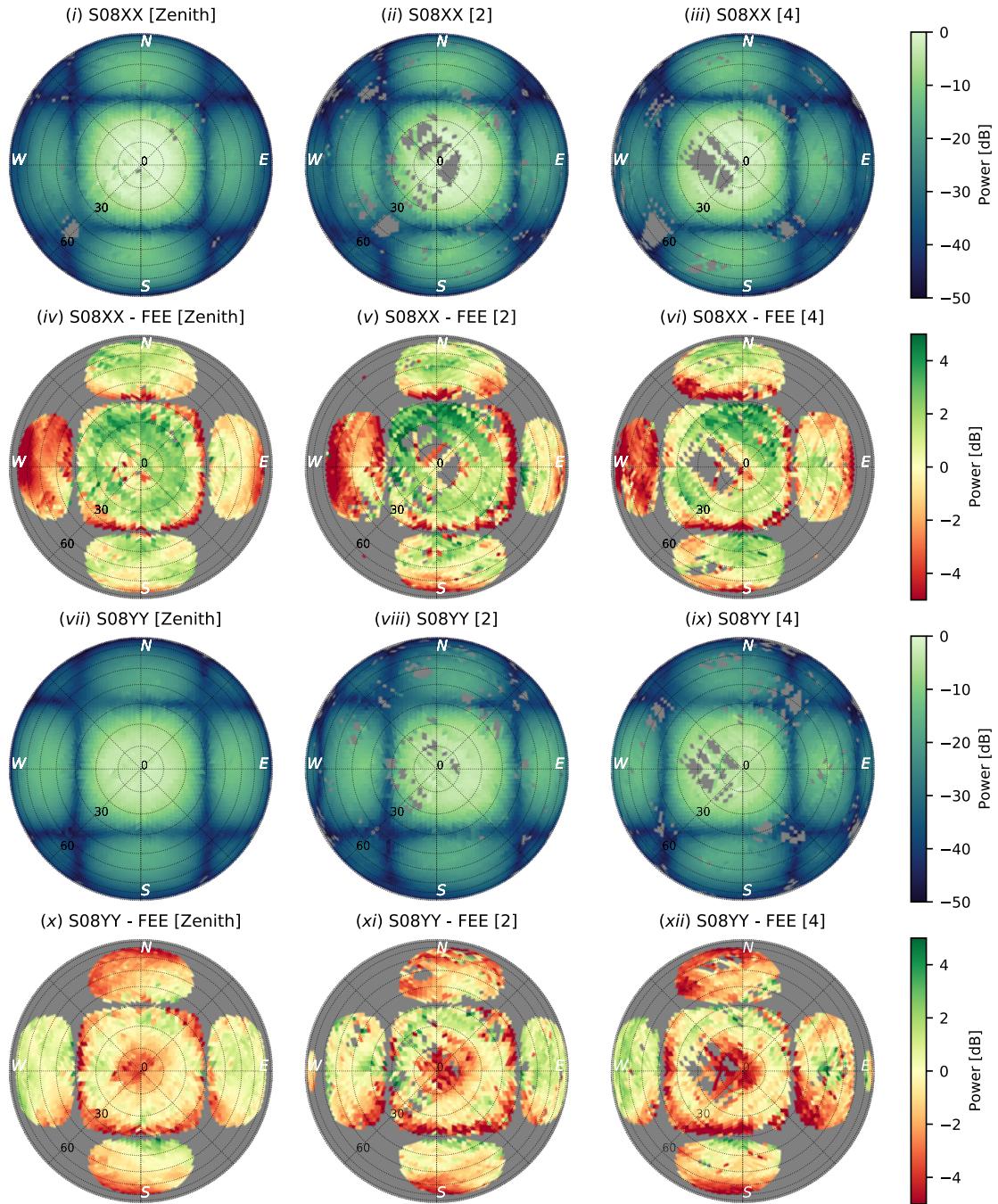


Figure 3.10: A set of beam maps measured for tile S08. The first row (i)-(iii) are maps of the XX polarization of tile S08, while the second row (iv)-(vi) represent the ratios between the beam maps and the corresponding FEE models. The three columns represent maps at the zenith, 2 and 4 pointing of the MWA. The last two rows (vii)-(xii) are an identical analysis for the YY polarization of tile S08.

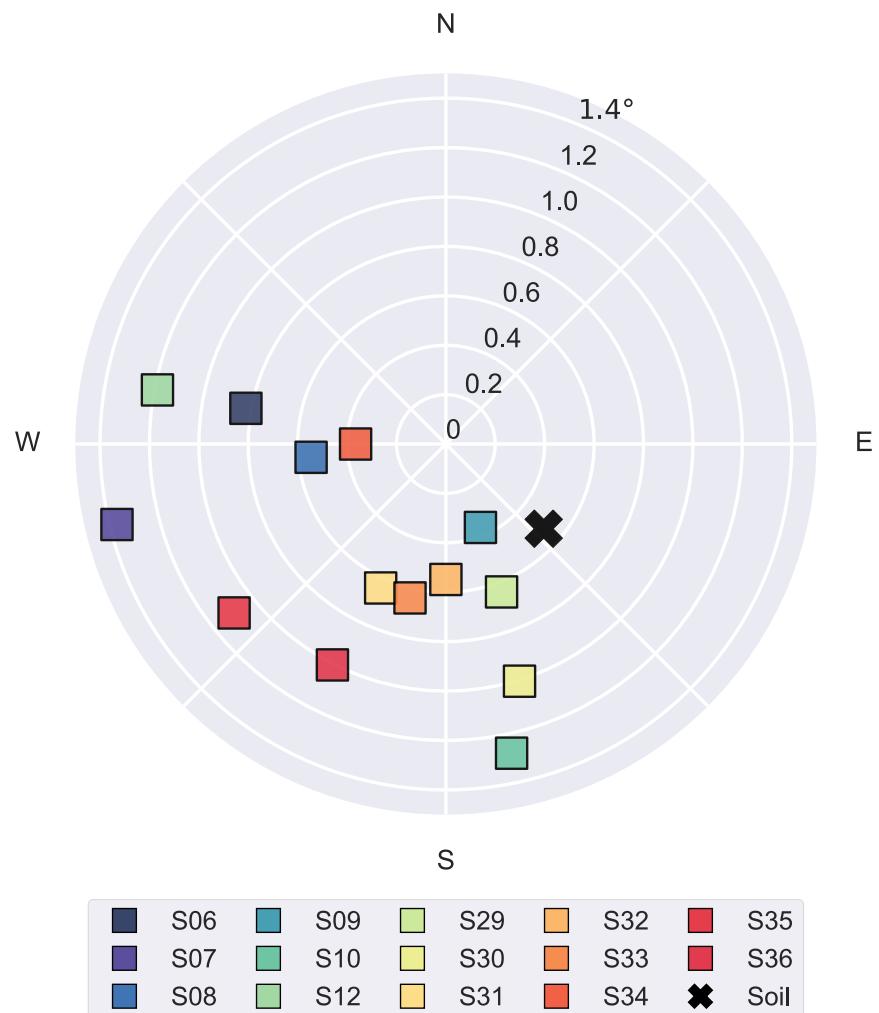


Figure 3.11: Measured angular offsets of zenith beam maps. The black cross represents a pervasive  $\sim 0.5^\circ$  gradient of the soil in the Southern Hex towards the South-East.

897 above, for the YY beam maps. The three columns represent the zenith and the 2 and 4  
898 off-zenith pointings.

899 The distribution of beam shapes of our 14 tiles can be seen in Figure 3.13, displayed  
900 as cross-sections of the beam maps along the cardinal axes. The marginally larger scatter  
901 observed of data points around the primary lobes can be attributed to the global RF Explorer  
902 gain calibration described in 3.5.2.

903 A subtle but interesting pattern emerges from Figures 3.12 and 3.13. Consider the  
904 first row of subplots, representing NS slices of XX beams. There is a slight excess of  
905 measured power ( $\sim 2$ dB) at the outer edge of the secondary lobes. XX dipoles are EW  
906 oriented and are most sensitive perpendicular to their physical orientation. Thus our  
907 measurements indicate a greater than expected sensitivity along the most sensitive axis  
908 of the XX dipole. Similarly, the YY beam oriented along the NS, measures an excess  
909 of power along its most sensitive axis (EW) as seen in the fourth rows of Figures 3.12  
910 and 3.13. Conversely, the power measured by the dipoles along their least sensitive axis,  
911 parallel to their physical orientation, is less than expected. This is seen in the second  
912 and third rows of Figures 3.12 and 3.13.

913 This effect was investigated by computing median residual power for all 14 tiles along  
914 EW and NS slices. The results shown in Figure 3.14 (i) have been fit with a 2<sup>nd</sup> order  
915 polynomial which shows systematic, radially dependent offsets. This residual structure  
916 could potentially be attributed to a rotation of the reference antenna. This scenario was  
917 explored using the simulated FEKO models of the reference, as shown in Figure 3.14 (ii).  
918 The solid lines represent the residual power which would be measured along a NS slice  
919 of the XX MWA beam if the reference tile was rotated by a range of angles, while the  
920 dashed lines represent the EW slices. As observed in Figures 3.12 and 3.13, the excess  
921 measured power along the most sensitive axis of the dipole and the deficit of power  
922 along the least sensitive axis of the dipoles seem to have similar shapes to the simulated  
923 residuals of reference antenna rotations. Unfortunately, the degeneracy inherent to the  
924 symmetric reference FEKO models prevents the identification of the direction of this  
925 rotation.

926 The measurements of the western sidelobe of tile S08 show a significant deficit in  
927 power of order  $\sim 4$  dB, seen in the second row of Figure 3.10. Pictures of the in-situ  
928 condition of the tile reveal potential environmental factors which could potentially be  
929 responsible. In Figure 3.15, we observe a number of large rocks on the ground screen  
930 of the tile. Additionally, the harsh weather conditions on site seem to have swept some  
931 loose soil onto the ground screen, partially obscuring the metal mesh. Both these effects  
932 are most prominent along the western edge of the tile and could plausibly explain the  
933 measured deficit of power.

### 934 3.6. CONCLUSIONS

935 We have measured the all-sky beam response of 14 onsite MWA tiles, at both instru-  
936 mental polarizations and at three pointings. As the first dual polarization MWA beam  
937 measurement experiment, both our XX and YY beam maps display good agreement with  
938 the cutting-edge FEE beam models (Sokolowski et al., 2017) to first order. Further inves-  
939 tigations reveal a range of environmental perturbations from the FEE models, which  
940 may present the scope for improved calibration for EoR and other science cases.

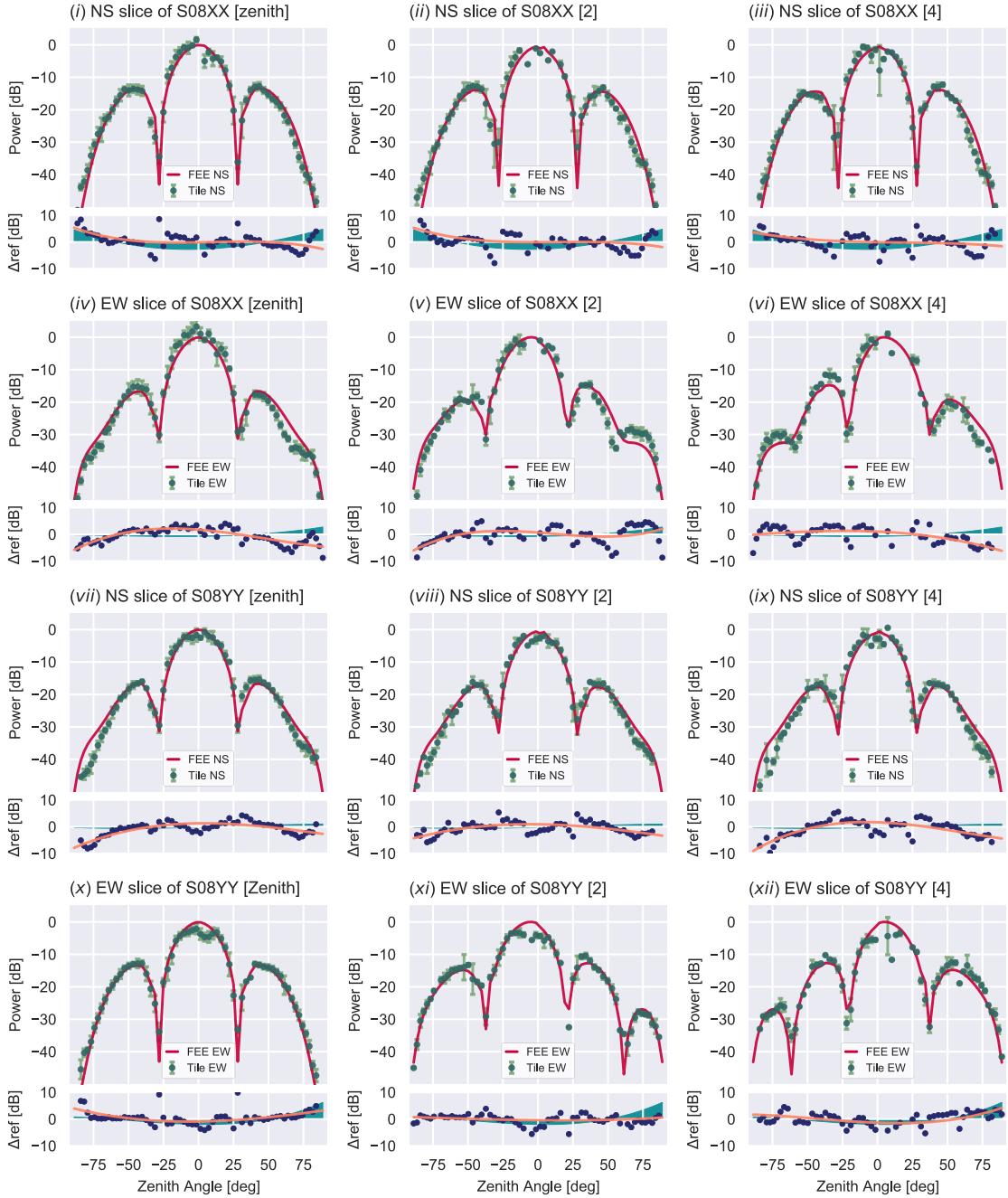


Figure 3.12: North-South(NS) and East-West(EW) slices of beam maps (S08) presented in Figure. 3.10. The first row (i)-(iii) displays NS slices of tile S08 compared to corresponding slices of the FEE model, in the XX polarization and at three pointings. The lower panels show the residuals between the measured tile maps and the FEE models, with the cyan shaded regions representing errors which can be attributed to the reference antennas. The second row (iv)-(vi) display EW slices of S08XX. The bottom two rows (vii)-(xii) represent an identical analysis for the YY polarization of tile S08.

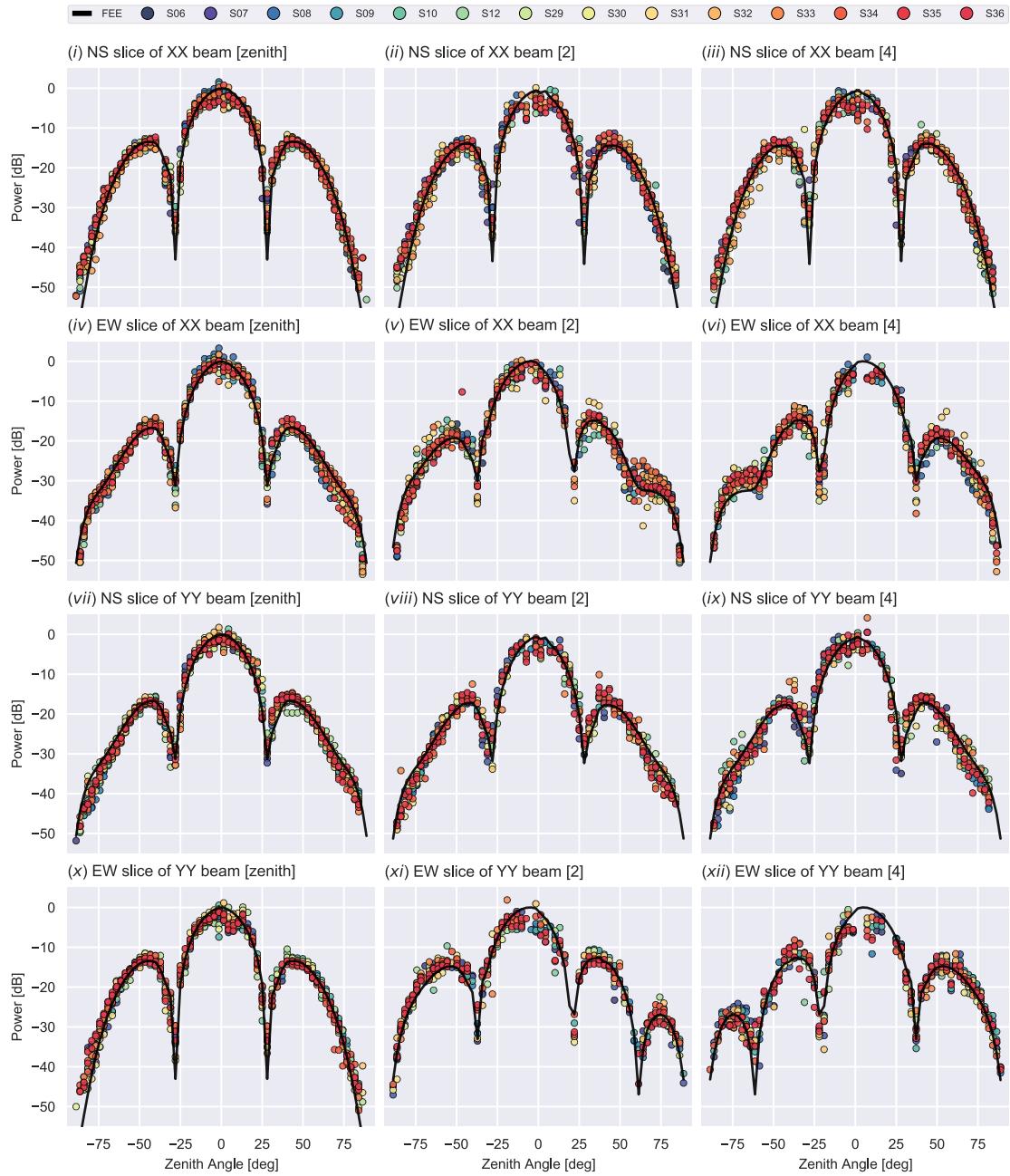


Figure 3.13: Distribution of all beam maps compared to corresponding slices of the FEE beam. The three vertical columns represent the Zenith, 2, 4 MWA pointings, while the horizontal rows represent cardinal (NS, EW) slices of beam maps at both polarizations (XX, YY).

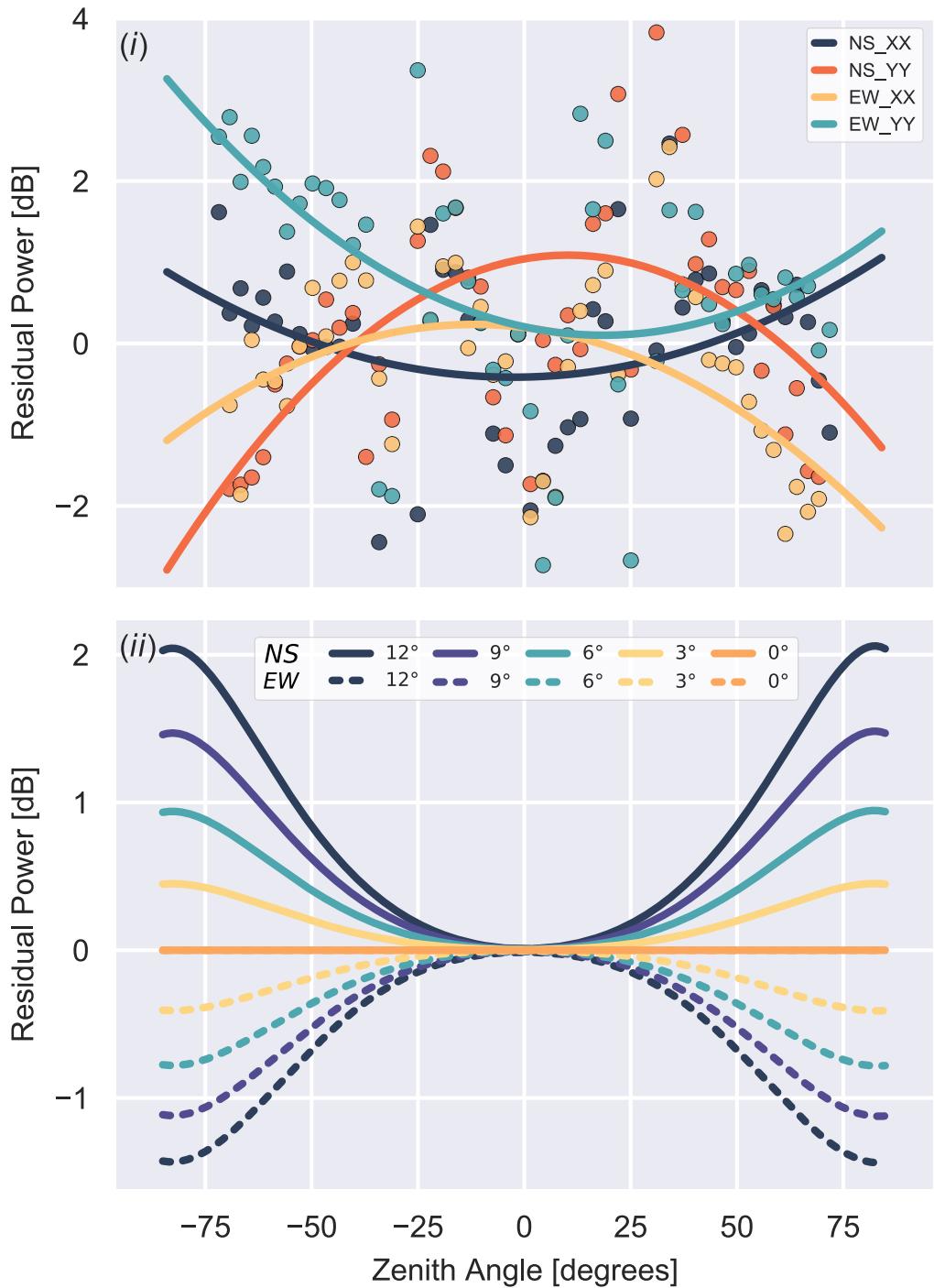


Figure 3.14: (i) Global residual power averaged over all 14 tiles. Each point represents the median power at various zenith angles, along cross-sectional slices of residual power between measured MWA tile maps and the FEE model. Second order polynomials fit to this data reveal systematic offsets attributed to rotations in the reference tiles. (ii) Simulated effect of anticlockwise rotation in the XX reference tile on measurements of MWA tile power. The solid and dashed lines represent North-South and East-West cross-sectional slices of the beam model.

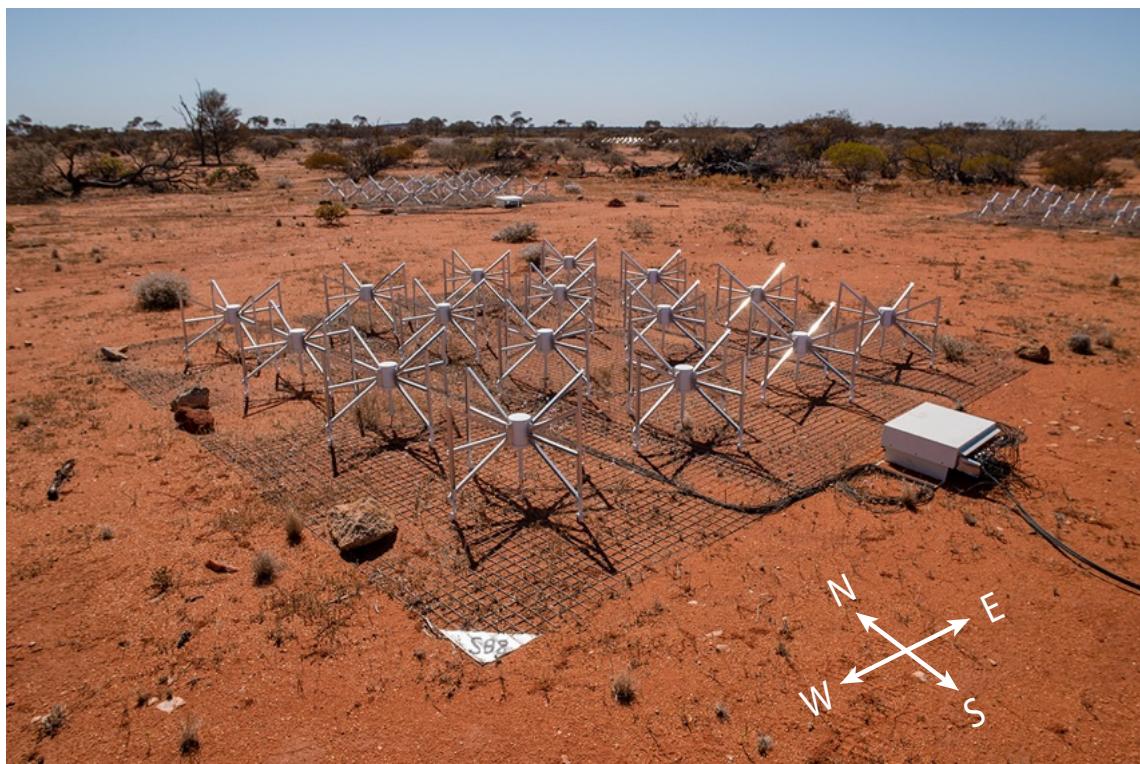


Figure 3.15: A current image of the condition of tile S08 reveals several large rocks on the western edge of the ground screen as well as a significant amount of loose soil which has covered portions of the metal mesh of the ground screen.

941 The most significant distortions to the MWA beams are found to be asymmetric and  
942 in one or more of the sidelobes. These distortions have been observed to occur due to  
943 environmental effects such as the obscuration of the metal mesh of the ground screen  
944 by loose soil, and other large objects such rocks (see Figure 3.15). Further, local foliage  
945 surrounding the tile may also contribute to beam deformations in an unpredictable, non-  
946 static manner as they grow and wither over the course of a year. These effects have been  
947 seen to deform the sidelobes with up to a  $\sim$  5dB deficit in measured power. Such effects  
948 are at the level of  $\sim$  10% zenith power and could have a serious effect on multiple science  
949 cases.

950 Further, investigations into the mismatch of positions of the primary nulls have re-  
951 vealed the effects of gradients in soil and ground screens. The Southern Hex is known  
952 to have a  $0.5^\circ$  gradient in the soil from the NW to the SE. Our investigation revealed the  
953 existence of local soil gradients, beyond the gradual background gradient, up to  $\sim 1.5^\circ$ ,  
954 scattered around the local gradient (see Figure 3.11). This effect results in the bore-sight  
955 of the MWA beam pointing slightly away from its expected position, and is analogous to  
956 pointing errors in traditional telescopes. While these effects do not significantly effect  
957 the central portion of the primary lobe, the steep edges of the beam surrounding the  
958 nulls are susceptible to large power offsets, approaching  $\sim$  8dB, with pointing offsets  
959 as low as  $\sim 1.5^\circ$ . This may be of particular import to observations conducted during  
960 the day, where clever observation techniques are used to place the sun in one of the  
961 primary beam nulls and achieve maximum attenuation (Morgan et al., 2019). Positional  
962 offsets of the nulls could potentially introduce significant erroneous solar flux to such  
963 observations.

964 Finally, unexpected deviations from measured power, along and perpendicular to dipole  
965 axis have revealed rotations in our reference tiles. Degeneracies resulting from symme-  
966 tries in the reference antenna beam models have prevented the exact identification of  
967 the direction of this rotation. While the rotation of the reference tile does not affect  
968 MWA science cases, it does present an interesting proxy to study effects rotations in  
969 MWA tiles may have. MWA tiles are aligned to within  $0.5\text{--}1.0^\circ$  of the NS meridian. We  
970 estimate that such uncertainties in rotation may introduce error less than  $\sim 1$ dB close to  
971 the horizon. Such effects do not significantly effect the primary lobe but increase radi-  
972 ally outwards. Interferometric arrays such as the MWA are prone to flux leakage, which  
973 may be exacerbated by rotational errors which will increase the coupling between the  
974 orthogonal, independent dipoles. With better calibration of reference antennas, future  
975 versions of this satellite experiments will be able to measure rotations of MWA beams,  
976 enabling studies of the effects of tile rotations and place upper limits on the acceptable  
977 leeway in beam rotations. More comprehensive simulations of such effects have been  
978 reserved for future work.

979 These measurements provide useful insight to various beam deformations, but are  
980 limited to an extremely narrow frequency band. This is an apparent shortcoming of  
981 satellite based beam measurement techniques and presents a significant impediment to  
982 the adoption of satellite based beam maps by the radio astronomy community. So far,  
983 the utility of such methods has been limited to the validation of advanced electromag-  
984 netic simulations. Future work based on our measured beam maps will investigate the  
985 fitting of 32 complex-valued gain parameters of the FEE model (Sokolowski et al., 2017)  
986 to create perturbed FEE models representative of measurements at 137 MHz. Future

987 investigations will explore the efficacy of extrapolating these gain values to cover the  
988 MWA's frequency band, potentially opening an avenue for broadband, pseudo-realistic  
989 beam models. Finally, a study combining our measured beam maps and data from the  
990 regular short dipole tests, used to find dead dipoles, may enable the creation of more  
991 realistic beam models for use with archival MWA data.

992 The implications of more accurate beam models are far-reaching. The detection of  
993 the EoR and studies of the cosmic dawn are key science cases of the MWA and upcom-  
994 ing telescopes such as the SKA-Low. The extreme dynamic range of such experiments  
995 necessitate uncompromising precision, which may be impeded by imperfect beam mod-  
996 els. Particularly, imperfect beam models with radially increasing uncertainty can result  
997 in flux calibration errors of bright sources such as Fornax A, and the diffuse galactic  
998 plane, close to the horizon. The intrinsic chromatic nature of radio interferometers can  
999 be exacerbated by in-situ beam distortions. Such effects could lead to the introduction  
1000 of bright, unphysical spectral structure, impeding the detection of the EoR signal (e.g.  
1001 [Byrne et al., 2019](#); [Orosz et al., 2019](#)).

1002 Large precise surveys such as GLEAM ([Hurley-Walker et al., 2017](#)), along with planned  
1003 surveys such as GLEAM-X and LoBES, use the half-power portion of the central lobe.  
1004 This has primarily been necessary due to beam modelling errors, and results in a loss  
1005 of sensitivity and survey efficiency. Instruments such as the MWA are sensitive to large  
1006 portions of the sky, and approach all-sky sensitivity at low frequencies. Increased confi-  
1007 dence in beam models would enable larger swatches of the sky to be observed at a time.  
1008 Additionally, unresolved sources in the sidelobes contribute to confusion-noise, place  
1009 lower limits on sensitivity to faint sources.

1010 This experiment has demonstrated the feasibility of a passive parallel monitoring sys-  
1011 tem, built from off-the-shelf and relatively inexpensive components, which could easily  
1012 be scaled up to monitor the beam shapes of the entire MWA array, providing invaluable  
1013 information to many science cases and improving calibration across the board. Using  
1014 individual tile models for calibration of MWA data is possible using pipelines such as  
1015 the RTS and FHD, but presents a significant increase in computational effort. The level  
1016 of measured beam distortions and their complex nature reinforces our conjecture that  
1017 more realistic beam shapes could significantly improve the accuracy and sensitivity of  
1018 science possible using the MWA. Further investigation and detailed simulations will be  
1019 necessary to understand how realistic beam models will effect calibration and improve  
1020 results. If successful in improving calibration, a similar passive parallel monitoring sys-  
1021 tem may be an essential tool for upcoming telescopes. This is particularly applicable to  
1022 SKA-Low stations constructed of 512 dipoles, with multiple degrees of freedom available  
1023 for complex beam perturbations.

1024 This experiment has led to the development of an open-source python package called  
1025 EMBERS\* – Experimental Measurement of BEam Responses with Satellites. EMBERS  
1026 is almost completely parallelized and is capable of being scaled to much larger arrays,  
1027 enabling an end-to-end analysis of satellite beam measurement data. EMBERS can be  
1028 used and modified by anyone, with the aim of enabling the measurement of beam shapes  
1029 of radio telescopes all over the world with ease.

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\*<https://embers.readthedocs.io>

# CHAPTER 4

1030

1031

## 1032 The Necessity of Individually Validated Beam Models for an 1033 Interferometric Epoch of Reionization Detection

1034

### 1035 This chapter is based on

1036 A. Chokshi, N. Barry, J. L. B. Line, C. H. Jordan, B. Pindor, R. L. Webster  
1037 Monthly Notices of the Royal Astronomical Society, 534, 3, 2024, 2475

### 1038 reformatted with the following changes only:

- 1039 • The text is styled and restructured to match the rest of this thesis.
- 1040 • Where necessary, bibliographic records are updated.

### 1041 4.1. ABSTRACT

1042 A first statistical detection of the 21-cm Epoch of Reionization (EoR) is on the horizon,  
1043 as cosmological volumes of the Universe become accessible via the adoption of low-  
1044 frequency interferometers. We explore the impact which non-identical instrumental  
1045 beam responses can have on the calibrated power spectrum and a future EoR detec-  
1046 tion. All-sky satellite measurements of Murchison Widefield Array (MWA) beams have  
1047 revealed significant sidelobe deviations from cutting-edge electromagnetic simulations  
1048 at the  $\sim 10\%$  zenith power level. By generating physically motivated deformed beam  
1049 models, we emulate real measurements of the MWA which inherently encode the im-  
1050 prints of varied beams. We explore two calibration strategies: using a single beam model  
1051 across the array, or using a full set of deformed beams. Our simulations demonstrate  
1052 beam-induced leakage of foreground power into theoretically uncontaminated modes,  
1053 at levels which exceed the expected cosmological signal by factors of over  $\sim 1000$  be-  
1054 tween the modes  $k=0.1-1 \text{ hMpc}^{-1}$ . We also show that this foreground leakage can be  
1055 mitigated by including measured models of varied beams into calibration frameworks,  
1056 reducing the foreground leakage to a sub-dominant effect and potentially unveiling the

1057 EoR. Finally, we outline the future steps necessary to make this approach applicable to  
1058 real measurements by radio interferometers.

## 1059 4.2. INTRODUCTION

1060 The past decade has seen the adoption of relatively simple, large interferometric arrays  
1061 as powerful tools for the investigation of the low-frequency radio sky. These aperture  
1062 arrays are generally constructed from sets of simple metal dipoles, coherently synthe-  
1063 sised to achieve high angular resolution imaging over unprecedented wide fields-of-  
1064 view. Such telescopes are often designed to have a large number of receiving elements  
1065 (tiles or stations), each constructed from a number of identical dipoles, with theoretically  
1066 identical sensitivities across the sky.

1067 Low-frequency radio interferometers with large collecting areas can sample many  
1068 modes on the sky, allowing them to search for faint, cosmic signals. The Murchison  
1069 Widefield Array (MWA, [Tingay et al. 2013](#); [Wayth et al. 2018](#)), the Hydrogen Epoch of  
1070 Reionization Array (HERA, [DeBoer et al. 2017](#)), the New Extension in Nançay Upgrading  
1071 LOFAR (Nenufar, [Zarka et al. 2020](#); [Munshi et al. 2024](#)), the Low Frequency Array (LO-  
1072 FAR, [van Haarlem et al. 2013](#)), and the Long Wavelength Array (LWA, [Eastwood et al.](#)  
1073 [2019](#)) are all searching for cosmic signals below 200 MHz.

1074 Understanding the telescope's varied sensitivity across the sky, or primary beam re-  
1075 sponse, is a crucial part of the inherent calibration process. Beam sensitivity measure-  
1076 ments show that this often differs from the instrumental simulations, especially in at-  
1077 tenuated parts of the beam. Sensitivity measurements have been made with the MWA  
1078 ([Bowman et al., 2007](#); [Neben et al., 2015](#); [Line et al., 2018](#); [Chokshi et al., 2021](#)), with  
1079 LOFAR ([Ninni et al., 2020](#)), and with HERA ([Neben et al., 2016b](#); [Nunhokee et al., 2020](#)).

1080 Ideally, the beam shape of each interferometric station or tile is identical, enabling  
1081 massive computational simplifications during beam calibration. However, the realities  
1082 of dipole failure and other environmental perturbations breaks this assumption (e.g. as  
1083 measured by [Line et al. 2018](#); [Chokshi et al. 2021](#)) and requires more complicated cali-  
1084 bration schemes to be considered in the pursuit of high fidelity science. This may prove  
1085 costly for extremely large arrays, especially future telescopes like the Square Kilometre  
1086 Array (SKA-Low, [Mellema et al. 2013](#); [Koopmans et al. 2015](#)).

1087 The precision of calibration is particularly crucial for power spectrum measurements  
1088 of the 21-cm Epoch of Reionisation (EoR) signal. This cosmological, redshifted signal is  
1089 expected to be up to five orders of magnitude fainter than the various foregrounds (see  
1090 Figure 4.1) (e.g. [Oh & Mack, 2003](#); [Santos et al., 2005](#); [Pober et al., 2013](#); [Yatawatta et al.,](#)  
1091 [2013](#)), but will naturally separate in Fourier space due to its varying spectral structure.  
1092 However, calibration can impart varying structure on otherwise spectrally smooth fore-  
1093 grounds, clouding the EoR measurement (e.g. [Barry et al. 2016](#); [Patil et al. 2016](#); [Byrne](#)  
1094 [et al. 2019](#)).

1095 Calibration errors in the context of beam variations have been explored within simu-  
1096 lation. Redundant calibration, where tile parameters are reduced from multiple measure-  
1097 ments of the same mode, is particularly susceptible to variations in antennas and their  
1098 placement ([Joseph et al., 2018](#); [Orosz et al., 2019](#); [Choudhuri et al., 2021](#); [Kim et al., 2022](#)).  
1099 Sky calibration, where tile parameters are reduced from comparisons between measure-  
1100 ments and full-sky models, is also affected by unaccounted broken dipoles within tiles

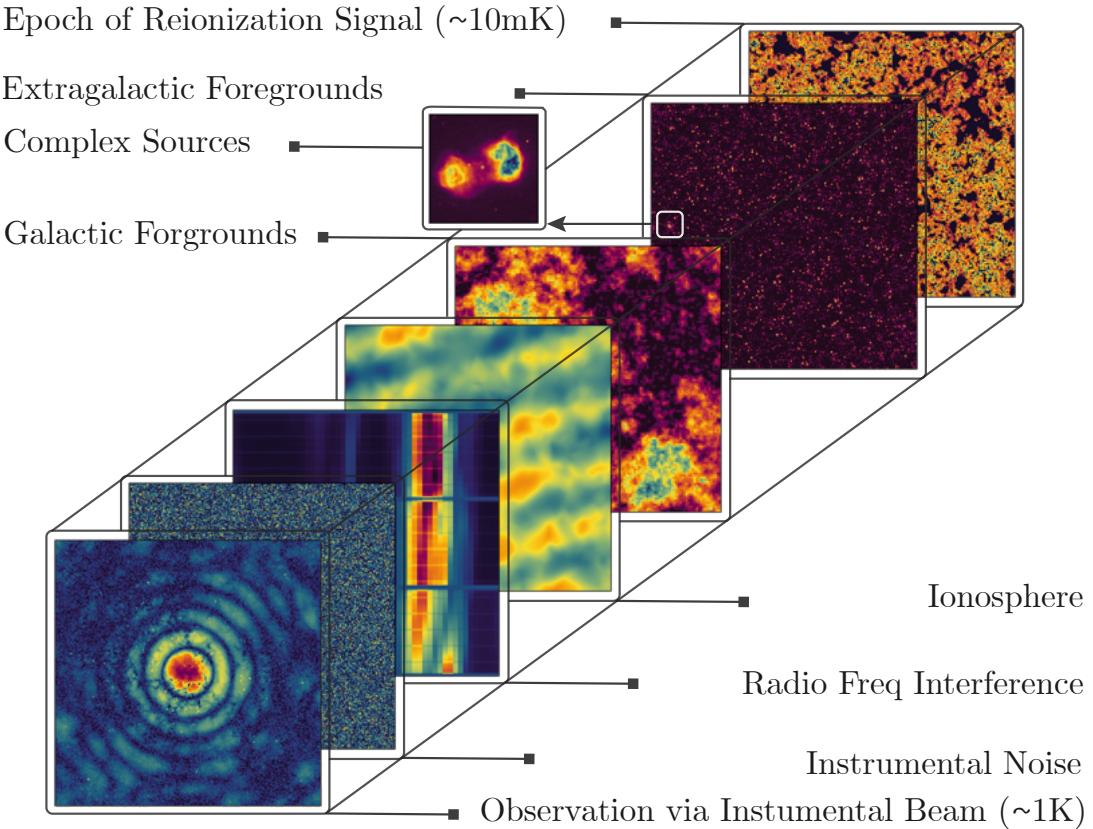


Figure 4.1: A schematic representation of the primary contributing components captured in a standard EoR observation (inspired by figures in Jelić et al. 2008), spanning five orders of magnitudes from the faint cosmological signal, to foreground, terrestrial and instrumental effects.

or stations (Joseph et al., 2019). Given the computational complexity of unique beams in analyses, these studies explore discrete variations.

We show a more complete picture of the effects of beam variation within sky calibration of MWA Phase II, using actual beam measurements to inform our simulations. We have 14 dual polarisation measurements of true beam variation from Chokshi et al. (2021), and we produce simulations which use these measurements to modify the dipole gains within a tile on a floating-point level to match. While our simulations are still encoding discrete variation representative of 14 measurements, it adds to work that was previously binary in nature (Joseph et al., 2019). This gives a more realistic portrayal of expected errors from an instrument that has been in the field for over a decade. Given our evidence-based beam variations and our analysis framework, deformed beams may be the cause of current limiting systematics in recent MWA limits (Trott et al., 2020; Rahimi et al., 2021).

In Section 4.3, we describe how we build optimal beam maps via satellite measurements from Chokshi et al. (2021) for 14 tiles. In Section 4.4, we take these optimal maps and forward model them through a simulation and calibration framework which is representative of real data analysis. We summarise our power spectrum metric in Section 4.5 and investigate the effects of performing calibration with and without knowledge of the

1119 deformed beams in Section 4.6 and compare the results in power spectrum space. We  
1120 summarise our conclusions in Section 4.7.

### 1121 4.3. OPTIMAL SATELLITE BEAM MAPS

1122 The Fully Embedded Element (FEE) beam model (Sutinjo et al., 2015; Sokolowski et al.,  
1123 2017) is a cutting-edge numerical electro-magnetic simulation of the MWA tile response  
1124 using FEKO\*. The FEE beam model incorporates a number of significant improvements  
1125 over the previous analytic representations of the beam, including mutual coupling be-  
1126 tween the multiple dipoles in the tile and a model of the electromagnetic effects of the  
1127 soil below the tile.

1128 The FEE simulations represent a tile under ideal conditions. Unfortunately, the arid  
1129 conditions at the MWA site, and its remote location lead to a range of environmental fac-  
1130 tors which perturb beam models away from the FEE standard. In-situ, all-sky measure-  
1131 ments of MWA beam shapes using communication and weather satellites have shown  
1132 that the measured beam shapes differ from the FEE model, particularly away from zenith  
1133 and within the sidelobes of the beams, at a  $\sim$ 10% level (see, Line et al., 2018; Chokshi  
1134 et al., 2021). The dual polarised beam shapes of 14 MWA tiles were measured by Chokshi  
1135 et al. (2021), creating all-sky HEALPix (Gorski et al., 2005) maps with a angular resolu-  
1136 tion of 110 arcminutes at 137 MHz. These maps were created by an open-source Python  
1137 package called EMBERS (Chokshi et al., 2020), and are available online. The direct incor-  
1138 poration of these measured beam maps into standard calibration software is hindered  
1139 by their low resolution and narrow frequency bandwidth.

1140 The FEE beam model has 16 variable dipole amplitude parameters per polarisation,  
1141 which can each be tuned to weight the contribution of dipoles to the MWA tile. Typically,  
1142 all dipole amplitudes are set to one, representing a perfect tile, with the occasional tile  
1143 having a single dipole set to zero indicating the presence of a malfunctioning or flagged  
1144 dipole (occurring in  $\sim$ 20–40% of all tiles at any given time, see Joseph et al. 2019). This  
1145 predominantly occurs due to the failure of the primary low noise amplifier (LNA) within  
1146 the central column of the MWA dipoles as they gradually degrade upon contact with the  
1147 slightly acidic local soil.

1148 Our proposed method of incorporating more complex and perturbed beam models is  
1149 to use the measured satellite beam maps to determine the optimal set of 16 dipole am-  
1150 plitudes, which best reproduce the measurements. This does not address the issue of  
1151 extrapolating the narrow bandwidth satellite measurements at 137 MHz, as most Epoch  
1152 of Reionization searches are conducted across the 167–198 MHz band where Galactic &  
1153 extragalactic foregrounds and ionospheric effects are least dominant. Given the response  
1154 of the MWA FEE beam, to first order, the scaling of these dipole amplitudes across fre-  
1155 quency is considered to be linear. A study of the frequency scaling of these dipole param-  
1156 eters is beyond the scope of this work as it would likely involve drone measurements of  
1157 the MWA beam patterns across the entire frequency band. In this work, we assume that  
1158 it is valid to linearly extrapolate the dipole parameters recovered from 137 MHz satellite  
1159 beam maps across the 167–198 MHz band where EoR observations are conducted.

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\*<http://www.feko.info>

1160 The beam maps from Chokshi et al. (2021) are available\* in the form of HEALPix maps  
 1161 of two types. The first represents a median satellite map, with pixel values averaged over  
 1162 all satellite passes, while the second are error maps with pixel values representing the  
 1163 median absolute deviation (MAD) of all satellite passes.

1164 We define a likelihood function  $\mathcal{L}$  which quantifies how similar the FEE model with  
 1165 16 dipole amplitudes ( $d_0 : d_{15}$ ) is to the measured beam maps. The set of dipole param-  
 1166 eters which correspond to the maximum likelihood estimator  $\mathcal{L}_{\max}$  leads an optimised  
 1167 FEE model.

$$\mathcal{L} = -1 \cdot \ln \left\{ \sum_{i=1}^N \frac{\left| \mathbb{S}_i - \mathbb{F}_i |_{d_0:d_{15}} \right|^2}{\mu_{\mathbb{S}i}} \right\}, \quad (4.1)$$

1168 where  $\mathbb{F}$  is the FEE beam model evaluated on a HEALPix grid, with a set of 16 dipole  
 1169 amplitudes, using the GPU accelerated hyperbeam† package.  $\mathbb{S}$  is the satellite beam  
 1170 map with  $\mu_{\mathbb{S}i}$  being the MAD error map and  $i$  the pixel indices. Pixels with FEE power  
 1171 lower than  $-30$ dB from zenith are masked out due to low signal to noise, along with the  
 1172 central  $20^\circ$  where bright satellites saturated the amplifiers used in Chokshi et al. (2021),  
 1173 leading to a low confidence central region.

1174 We use the Bayesian Information Criteria (BIC) as the metric for our optimal model  
 1175 selection, as it accounts for the number of free parameters and amount of data used in  
 1176 the model evaluation, where BIC is defined as:

$$\text{BIC} = k \cdot \ln(n) - 2 \cdot \mathcal{L}_{\max}, \quad (4.2)$$

1177 where  $k$  is the number of free parameters in the model (16 in the case of the FEE beam  
 1178 model),  $n$  is the number of data points used (number of unmasked HEALPix pixels in  
 1179 satellite beam maps) and  $\mathcal{L}_{\max}$  being the maximum likelihood estimator. The model  
 1180 with the lowest BIC value corresponds to a set of 16 dipole amplitude parameters which  
 1181 best optimise the FEE model to the given satellite beam map.

1182 Figure 4.2 shows the best BIC values obtained via the maximum likelihood estimator  
 1183 of Eqn. 4.2 of an optimised FEE model (FEE Min - purple line), compared to the BIC  
 1184 value corresponding to a perfect FEE model (blue line), with all 16 dipole amplitudes set  
 1185 to 1. Figure 4.2 shows that the optimised FEE model is consistently preferred over the  
 1186 nominal FEE model, with improvements in BIC values of  $\sim 2$  across the board. In Figure  
 1187 4.3, the 16 optimal dipole amplitudes for MWA tile “S06” in the North-South polarisation  
 1188 (henceforth “S06YY”), recovered via the beam minimisation described above, are applied  
 1189 to the FEE model to quantify how well this process can reproduce measured MWA beam  
 1190 shapes. The top row ( $i, ii, iii$ ) shows the perfect FEE beam model, the measured satellite  
 1191 beam model for tile “S06YY” and an optimised FEE model perturbed to best match the  
 1192 satellite map. Notice how the optimised FEE model ( $iii$ ) has primary beam nulls which  
 1193 are less deep and distinct than the corresponding perfect FEE model, closely matching  
 1194 the satellite map ( $ii$ ). The bottom row ( $iv, v$ ) depicts residuals between the FEE or opti-  
 1195 mised FEE model and the satellite beam map respectively, with regions of the FEE model  
 1196 lower than 30dB below zenith power being masked out due to low signal to noise. The

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\*<https://github.com/amanchokshi/MWA-Satellite-Beam-Maps>

†[https://github.com/MWATelescope/mwa\\_hyperbeam](https://github.com/MWATelescope/mwa_hyperbeam)

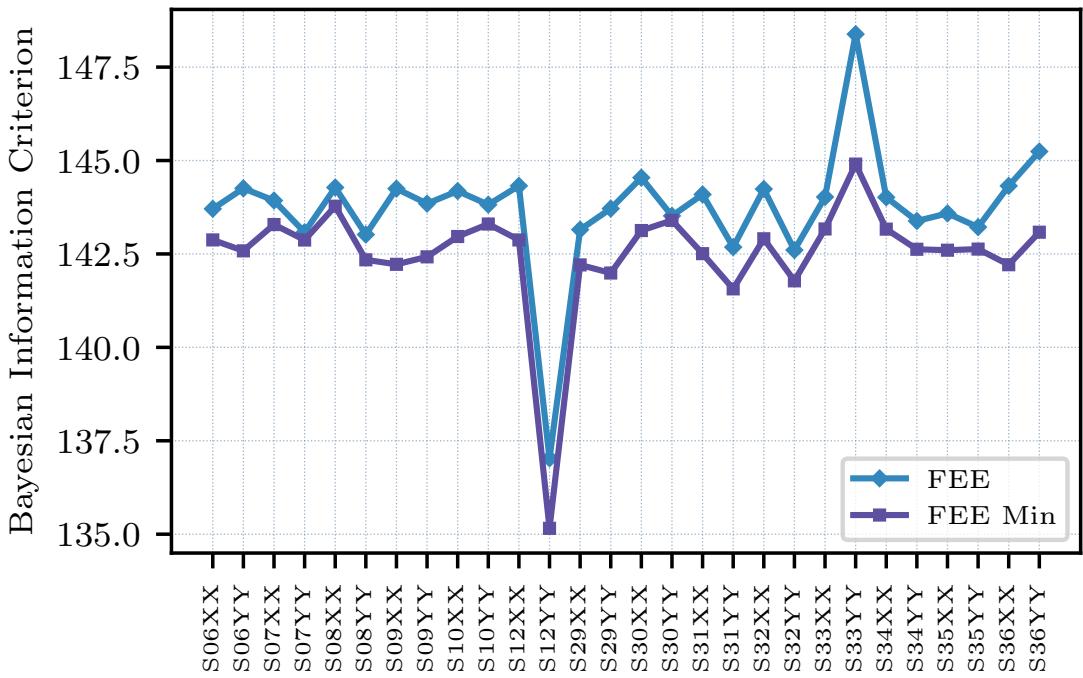


Figure 4.2: The best (lowest) BIC values obtained by the optimisation of the 16 dipole amplitude parameters in Eqn. 4.2, for the 14 dual polarised (XX, YY) MWA satellite beam maps available. The blue line (FEE), show the BIC value of the satellite map compared to the full FEE model, while the purple line (FEE Min) shows the BIC values for the optimised set of dipole amplitudes. Tile “S12YY” has lower BIC values due to sparse satellite coverage which led to a lower  $n$  in Eqn. 4.2.

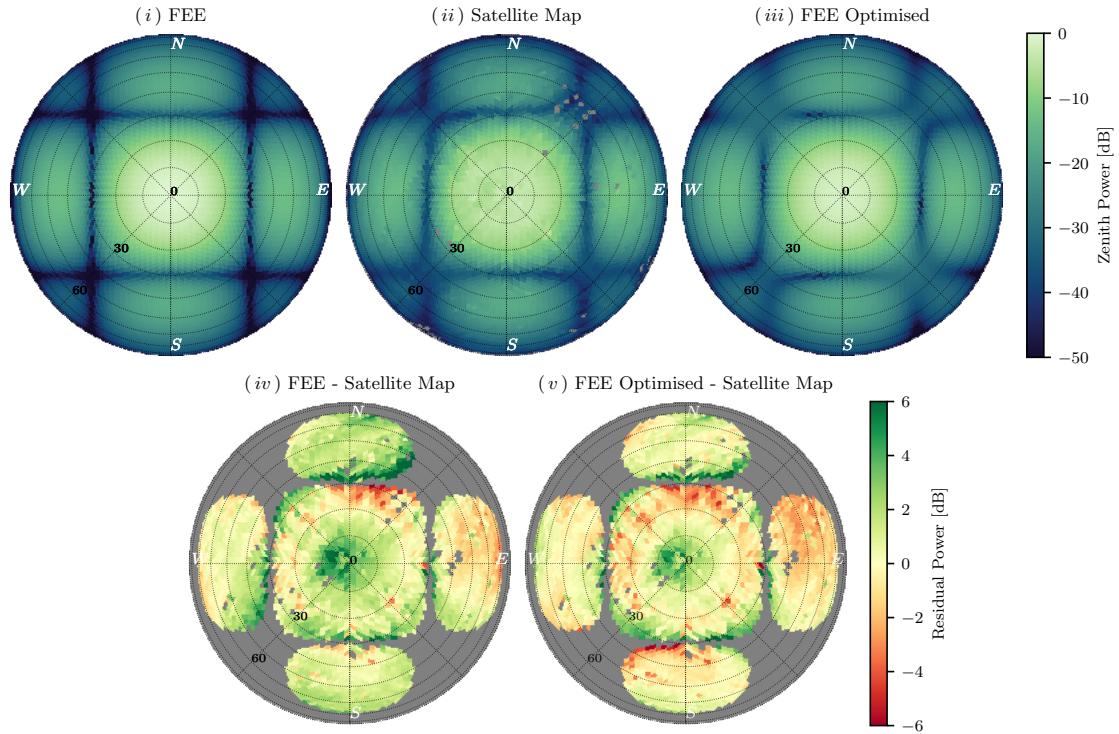


Figure 4.3: A study of the efficacy of the beam minimization procedure described in Section 4.3, tested on MWA tile “S06YY”. The top row (*i*, *ii*, *iii*) represent the perfect FEE model, the measured satellite model, and the optimised FEE model using dipole amplitude parameters recovered by minimisation. The second row (*iv*, *v*) depicts the residual power between the FEE, optimised FEE models and the satellite beam map. Panels (*iii*, *v*) show that the optimised FEE model better matches the satellite beam maps (*ii*), accurately capturing first-order beam deformations present in the satellite data.

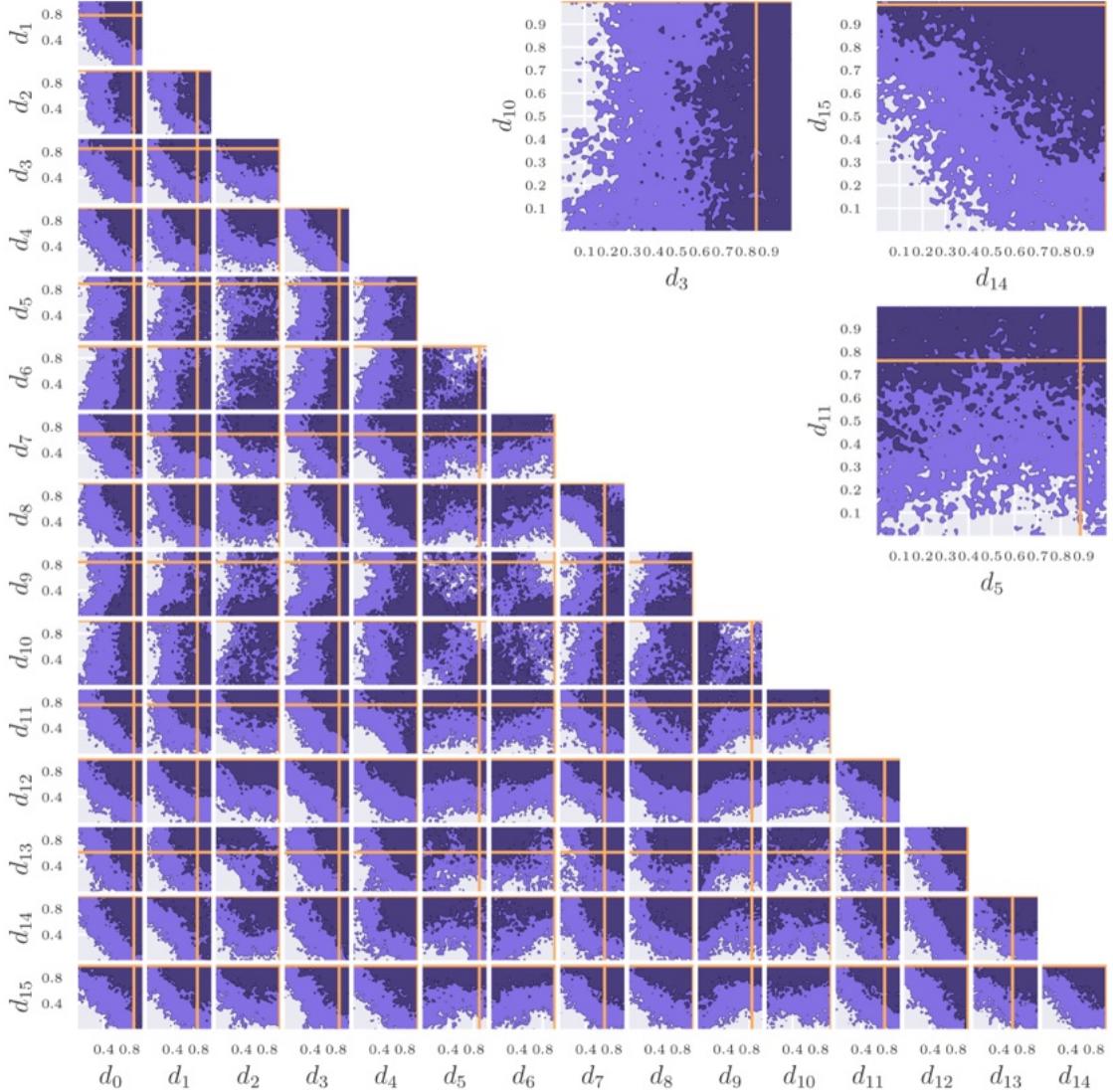


Figure 4.4: A MCMC analysis of MWA tile “S06YY” where purple contours represent 86% and 39% confidence levels respectively. The orange lines depict the results of beam minimisation from Section 4.3. The insets on the top right focus on three sets of dipole pairs which display varying levels of degeneracy between parameter constraints.

1197 residuals with the optimised FEE model ( $v$ ) have visibly reduced gradients across the  
 1198 beam sidelobes, and better match the satellite map at the zenith.

1199 An in-depth investigation into the distribution of optimal parameters in the 16-dimensional  
 1200 dipole amplitude space was performed for MWA tile “S06YY”, using a Markov chain  
 1201 Monte Carlo (MCMC) method, with the likelihood defined in Eqn. 4.1 and uniform, un-  
 1202 informative priors. The MCMC analysis was performed using a Python package called  
 1203 EMCEE (Foreman-Mackey et al., 2013), with corner plots made using ChainConsumer  
 1204 (Hinton, 2016). Figure 4.4 shows the result of the MCMC analysis, marginalised over  
 1205 pairs of parameters, with the purple contours representing 86% (dark purple) and 39%  
 1206 (light purple) confidence levels respectively. The orange lines represent the results of the  
 1207 beam minimisation described above, and shown in Fig. 4.3. While the results of the beam  
 1208 minimisation do concur with the central confidence contours in Fig. 4.4, large degenera-  
 1209 cies are observed in certain pairs of parameters, representing a lack of tight constraints  
 1210 on some dipole amplitudes. The insets in the top right corner of Fig. 4.3 show that  
 1211 for dipoles  $d_3$  &  $d_{10}$ , any possible value of  $d_{10}$  is as valid. Similarly, for the dipole pair  
 1212  $d_5$  &  $d_{11}$ , any value of  $d_{11}$  is equally valid. In essence, this indicates that dipole  $d_3$  &  $d_5$   
 1213 place almost no constraints on dipoles  $d_{10}$  &  $d_{11}$ , respectively. In contrast, the dipoles  
 1214  $d_{14}$  &  $d_{15}$  constrain each other well, leading to much lower degeneracy between these  
 1215 parameters.

1216 We observe that the pairs of dipole parameters which are often least well constrained  
 1217 include one of the four central dipoles. The FEE beam is used in a “zenith normalised”  
 1218 form, where zenith power is scaled to 1, with everything else being correspondingly  
 1219 scaled. We posit that the observed degeneracy in dipole amplitudes which arises from  
 1220 the central dipoles can be explained by the fact that variation in the central dipole am-  
 1221 plitudes tend to scale the overall power without significant deviations in beam shape.  
 1222 The effect is mostly eliminated by the zenith normalization of the beam. In contrast,  
 1223 the 12 dipoles on the edge of a MWA tile have a more significant effect on beam shapes,  
 1224 leading to significant distortions in the beam sidelobes. The  $\chi^2$  metric used in the beam  
 1225 minimisation and the MCMC analysis is only sensitive to global changes in the shape of  
 1226 the beam. The above procedure thus preferentially places most constraints on dipoles  
 1227 which affect the beam shape adversely.

## 1228 4.4. SIMULATION & CALIBRATION FRAMEWORK

### 1229 4.4.1. Calibration & Beams

1230 Each unique pair of antennas in an interferometer, separated by baseline  $\mathbf{u}$ , samples the  
 1231 sky brightness distribution  $I(\mathbf{l}, \nu)$  by measuring of the complex visibility

$$1232 V(\mathbf{u}, \nu) = \int g_p g_q^* b_p(\mathbf{l}, \nu) b_q^*(\mathbf{l}, \nu) I(\mathbf{l}, \nu) e^{-2\pi i \mathbf{u} \cdot \mathbf{l}} d^2 \mathbf{l}, \quad (4.3)$$

1233 where  $\mathbf{l}$  is the sky coordinate vector,  $\nu$  is the observing frequency,  $g_p$  and  $b_p$  are the  
 1234 complex-valued gain and voltage beam pattern of antenna  $p$ , respectively. Calibration  
 1235 of measured visibilities enables the accurate reconstruction of the true sky brightness  
 1236 distribution  $I(\mathbf{l}, \nu)$ . Equation 4.3 demonstrates how each measured visibility  $V(\mathbf{u}, \nu)$   
 1237 contains the fundamental imprint of the constituent pair of receiving element beams.

1237 Traditional sky-based calibration (e.g., [Mitchell et al. 2008](#); [Salvini & Wijnholds, 2014](#))  
 1238 minimises the squared differences between a measured visibility  $V_{pq}^{\text{data}}$  and a model  
 1239 visibility  $V_{pq}^{\text{model}}$  simulated from sky and beam models, to solve for unknown antenna  
 1240 complex-valued gains  $g_p$  and  $g_q$

$$\chi^2 = \sum_{pq} |V_{pq}^{\text{data}} - g_p g_q^* V_{pq}^{\text{model}}|^2. \quad (4.4)$$

1241 This work investigates the effects of an imperfect representation of the instrumental  
 1242 beams during this critical calibration stage.

#### 1243 4.4.2. *Fiducial Simulation*

1244 To simulate a MWA array of 128 deformed tiles, 16 gain values are required per tile and  
 1245 polarization. [Chokshi et al. \(2021\)](#) measured all-sky dual-polarised beam maps of 14 fully  
 1246 polarized MWA tiles, and in Section 4.3 we determined the optimal gain parameters for  
 1247 each of their dipoles. For each dipole in a simulated deformed tile we make a random  
 1248 selection from the relevant 14 available gain parameters. This ensures that each of the  
 1249 128 tiles has a physically motivated distortion model. This simulation framework can  
 1250 be used to emulate measurements made an interferometric array composed of deformed  
 1251 beams.

1252 `hyperdrive`\* (Jordan et al., in prep) is a cutting-edge sky-based calibration and simu-  
 1253 lation tool designed for the MWA, developed to be the successor to the Real Time System  
 1254 (RTS; [Mitchell et al. 2008](#)). `hyperdrive` is used to create a noiseless simulation of the  
 1255 30,000 brightest foreground sources (see Figure 4.5) from the LoBES survey ([Lynch et al.,](#)  
 1256 [2021](#)), centered around the EoR0 field (R.A.  $0^h$ , Dec  $-27^\circ$ ), with the set of 128 deformed  
 1257 MWA beams described above. This simulation is performed at a 80kHz frequency reso-  
 1258 lution, over the 167-198 MHz band, and represents a fiducial “measurement” made by a  
 1259 realistically deformed and complex array.

#### 1260 4.4.3. *Perfect & Imperfect Calibration*

1261 The fiducial simulation created in Section 4.4.2 can be used to explore the effects of cali-  
 1262 bration errors introduced by the imperfect knowledge of beam models. We discriminate  
 1263 between two calibration scenarios below:

1264 **Perfect Calibration [ $\mathbb{C}_P$ ]:** In this case, a perfect understanding of our instrument is  
 1265 assumed, which is perfectly accounted for during calibration, along with a complete sky  
 1266 model. In particular, the set of deformed beam models used to generate the fiducial sim-  
 1267 ulation in Section 4.4.2 are used to generate the model visibilities for calibration ( $V^{\text{model}}$   
 1268 from Eqn. 4.4). This results in a perfect match between the fiducial simulation and the  
 1269 model visibilities used for calibration, leading to perfect calibration solutions.

1270

1271 **Imperfect Calibration [ $\mathbb{C}_I$ ]:** In this case, an incomplete understanding of our instru-  
 1272 ment is emulated by using a single, perfect (FEE) beam model to generate the the model

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\*[https://github.com/MWATelescope/mwa\\_hyperdrive](https://github.com/MWATelescope/mwa_hyperdrive)

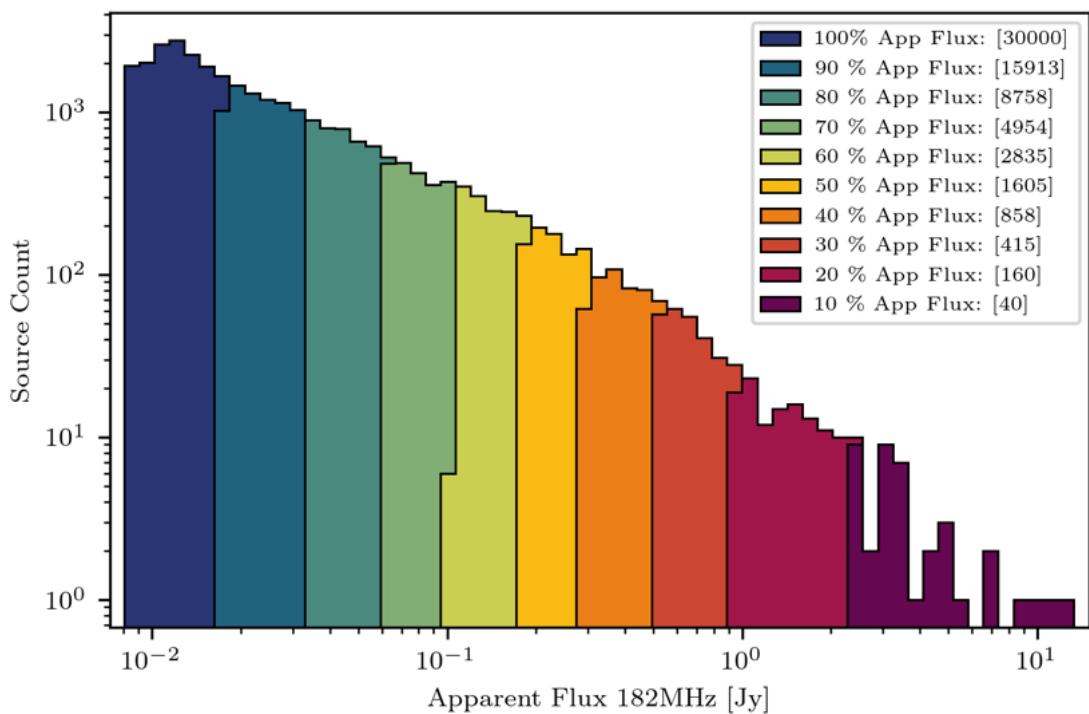


Figure 4.5: A histogram of apparent brightness of all 30,000 sources included in this work, at 182MHz. Each coloured section represent 10% of the integrated flux, from brightest on the right, to faintest on the left.

1273 visibilities for calibration. This scenario was chosen to mimic current interferometric  
 1274 calibration pipelines where varied or deformed beams are not considered. This case also  
 1275 uses a complete sky model, ensuring that any calibration errors arise purely from beam  
 1276 errors.

1277 Following the application of these two calibration scenarios to our fiducial simulated  
 1278 data, a 2D (cylindrical) and 1D (spherical) power spectrum analysis is performed to quan-  
 1279 tify the effects of mismatches in instrumental and calibration beams on an EoR detection  
 1280 pipeline, described below.

## 1281 4.5. POWER SPECTRUM

1282 The spatial power spectrum is designed to quantify spatial correlations in a cosmological  
 1283 field, and measures signal power as a function of spatial scale,  $k$  ( $h\text{Mpc}^{-1}$ ). It can be  
 1284 defined as the Fourier transform of the two-point spatial correlation function:

$$P(|\vec{k}|) = \int_V \xi(\vec{r}) e^{-2\pi i \vec{k} \cdot \vec{r}} d\vec{r}, \quad (4.5)$$

1285 where  $\xi(\vec{r})$  is the two-point spatial correlation function. The power spectrum can be  
 1286 estimated from the volume normalised Fourier transformed brightness temperature field,  
 1287 given an observing volume  $\Omega$ :

$$P(|\vec{k}|) \equiv \frac{1}{\Omega} \langle \tilde{T}(k)^\dagger \tilde{T}(k) \rangle. \quad (4.6)$$

1288 It's relevant to note that in an interferometer, the observing volume  $\Omega$  is determined  
 1289 by the primary beam of each receiving element or tile. Given the nature of the satel-  
 1290 lite beam measurements made in Chokshi et al. 2021, we only consider changes to the  
 1291 shape of beam responses across the array in this work, and make no assertions regarding  
 1292 changing observing volumes. This is in contrast to the case of flagged or dead dipoles,  
 1293 which change both the beam shape as well as observed cosmological volumes (see e.g.  
 1294 Joseph et al., 2018).

1295 Radio interferometers fundamentally sample Fourier modes across the spatial (angular)  
 1296 extent of the sky, captured by the measured interferometric visibilities (see Eq. 4.3):  
 1297  $\mathbf{u} \equiv (u, v) \mapsto k_\perp$ . For a resonant line signal, such as the 21-cm line, line-of-sight Fourier  
 1298 modes can be mapped with the spectral channels:  $\mathbf{f}(f) = \eta \mapsto k_\parallel$ . This mapping from  
 1299 measured interferometric visibility space  $(u, v, f)$  to Fourier space  $(u, v, \eta)$  leads to read-  
 1300 ily applicable expression for the power spectrum:

$$P(|\vec{k}|) \equiv \frac{1}{\Omega} \langle \tilde{V}(k)^\dagger \tilde{V}(k) \rangle. \quad (4.7)$$

1301 In practice, multiple sets of measured visibilities are integrated coherently by gridding  
 1302 to a discretised  $uv$ -plane, following a Fourier transform along the spectral axis which  
 1303 results in an  $u, v, \eta$  data cube. This can now be squared to arrive at an unnormalised  
 1304 estimate of the cosmological power spectrum. Typically this orthogonal  $k$ -space is com-  
 1305 pressed to a 2D (cylindrically-averaged) and 1D (spherically-averaged) power spectra,  
 1306 where the former is used to isolate and diagnose foreground leakage and instrumental

1307 systematics, and the latter for cosmological measurements. The MWA EoR collaboration  
 1308 typically uses CHIPS - the Cosmological HI Power Spectrum estimator (Trott et al.,  
 1309 2016) and eppsi - Error Propagated Power Spectrum with Interleaved Observed Noise  
 1310 (Barry et al., 2019a) for power spectrum estimation. In this work we use CHIPS to per-  
 1311 form our power spectrum analysis.

#### 1312 4.5.1. *Foreground Contamination and Subtraction*

1313 Galactic and extragalactic foregrounds dominate the faint cosmological EoR signal by up  
 1314 to five orders of magnitude (see Figure 4.1). To have any hope of detecting the EoR, ex-  
 1315 tensive and accurate models of these foregrounds are necessary, including extended and  
 1316 bright sources such at Fornax A (Line et al., 2020), diffuse emission (Byrne et al., 2022),  
 1317 the Galactic plane (Barry et al., 2024), and the ubiquitous faint point-like extragalactic  
 1318 sources (Barry et al., 2016). A powerful discriminator between foreground flux and the  
 1319 background cosmological signal are their disparate spectral characteristics. The emis-  
 1320 sion mechanisms of foreground sources are expected to be spectrally smooth (Di Matteo  
 1321 et al., 2002; Oh & Mack, 2003), while the 21-cm signal is anticipated to be uncorrelated  
 1322 on frequency scales larger than a MHz due to the topography of bubble formation and  
 1323 evolution as probed along the line-of-sight.

1324 The cylindrically-averaged 2D power spectrum is formed by collapsing the cartesian  
 1325 3D  $k$ -space along the spatial extent  $k_{\perp} = \sqrt{k_x^2 + k_y^2}$ , and the spectral or line-of-sight  
 1326 direction  $k_{\parallel}$ . In this space, spectrally smooth foreground components will dominate  
 1327 the low line-of-sight modes ( $k_{\parallel}$ ) at all spatial modes perpendicular to the line-of-sight  
 1328 ( $k_{\perp}$ ). We would thus expect a large region of this 2D  $k$ -space, above the low  $k_{\parallel}$  modes,  
 1329 to be free of power from the intrinsic foreground components. Unfortunately, radio  
 1330 interferometers are chromatic - they exhibit frequency dependant responses in both their  
 1331 primary beams and their synthesized beam or Point Spread Function (PSF). This results  
 1332 in the well-documented “foreground wedge” caused by the mode-mixing of power from  
 1333 low  $k_{\parallel}$  into larger  $k_{\parallel}$  values (Datta et al., 2010; Morales et al., 2012; Vedantham et al., 2012;  
 1334 Parsons et al., 2012; Trott et al., 2012; Hazelton et al., 2013; Thyagarajan et al., 2013; Pober  
 1335 et al., 2013; Liu et al., 2014a,b; Thyagarajan et al., 2015). This effect can also be considered  
 1336 to be the result of spectral structure being introduced to the otherwise spectrally smooth  
 1337 foregrounds by a chromatic instrumental response. The characteristic “wedge” shape of  
 1338 foreground mode-mixing arises from the fact that longer baselines (higher  $k_{\perp}$ ) change  
 1339 more rapidly with frequency, resulting in faster spectral fluctuation which manifest as  
 1340 power at higher  $k_{\parallel}$  modes.

1341 The area above the wedge is known as the “EoR window” and is expected to be con-  
 1342 tamitant free. The cosmological signal peaks at large scales, or small  $k = \sqrt{k_{\perp}^2 + k_{\parallel}^2}$ ,  
 1343 leading to an area of higher sensitivity in the lower left corner of the EoR window. This  
 1344 also means that  $k$ -modes within the wedge can have significantly more 21-cm power  
 1345 than those in the EoR window. The accurate subtraction of foreground flux from 21-  
 1346 cm data sets can enable the recovery of highly sensitive  $k$ -modes at the wedge-window  
 1347 boundary, boosting the significance of power spectrum measurements (Pober et al., 2014,  
 1348 2016; Beardsley et al., 2016; Cook et al., 2022; Barry et al., 2024), and can theoretically  
 1349 put a statistical detection of the cosmological signal within reach of current generation

1350 experiments.

## 1351 4.6. RESULTS

1352 Following the two calibration scenarios described in Section 4.4.3, a systematic subtraction  
1353 of foreground flux is performed to enable the recovery of  $k$ -modes around the edge  
1354 of the EoR window. Of the 30,000 sources included in the fiducial simulation from Section  
1355 4.4.2, we generate model visibilities (using the relevant set of calibration beam models)  
1356 with integrated apparent flux in 10% intervals (see Figure 4.5), between the brightest  
1357 10% to brightest 90% to subtract from the two calibrated data sets. CHIPS is then used  
1358 to calculate the 2D cylindrical-averaged power spectrum, and a 1D spherically-averaged  
1359 power spectrum within the EoR window.

### 1360 4.6.1. 2D Power Spectrum

1361 The 2D or cylindrically-averaged power spectrum is the compressed parameter space  
1362 where line-of-sight modes ( $k_{\parallel}$ ) and those in the orthogonal plane of the sky ( $k_{\perp}$ ) are  
1363 separated, making it an ideal space to observe and understand the complex effects of  
1364 foreground-instrumental coupling (Pober et al., 2016). Figure 4.6 displays the 2D power  
1365 spectra of the two calibration scenarios described in Section 4.4.3 before and after the  
1366 majority of foreground flux has been subtracted. The dashed lines in Figure 4.6 represent  
1367 the full-width half-max of the MWA primary beam response, while the black contours  
1368 in the upper left corner of each panel represent the EoR window above the horizon.

1369 The first two panels (*i*, *ii*) of Figure 4.6 contain flux from all 30,000 sources included in  
1370 the simulation, with key differences occurring in the EoR window in the top left. The EoR  
1371 window of the perfect calibration case ( $\mathbb{C}_P$ : panel (*i*)) has much less foreground power  
1372 than the imperfect calibration case ( $\mathbb{C}_I$ : panel (*ii*)), by a factor of approximately 100.  
1373 This excess foreground power present in the EoR window can be completely attributed  
1374 to the mismatch between the set of measurement beam models (used to create the fiducial  
1375 simulations in Section 4.4.2) and the single perfect beam model used during calibration.

1376 We subsequently subtract a sky-model, generated with the relevant set of beams, con-  
1377 taining 90% of the brightest apparent flux (see Figure 4.5) from each calibrated data set  
1378 results. This results in an anticipated reduction of power within the foreground-wedge  
1379 (lower sections of panels *iii*, *iv*), but unexpected behaviour within the EoR window.  
1380 In the perfect calibration case ( $\mathbb{C}_P - \mathbb{M}_{0.9}$ : panel (*iii*)), the EoR window has signifi-  
1381 cantly reduced power, while in the imperfect calibration case ( $\mathbb{C}_I - \mathbb{M}_{0.9}$ : panel (*iv*)),  
1382 the EoR window power has remained essentially the same. The difference in EoR win-  
1383 dow power after foreground subtraction has now widened to be greater than a factor  
1384 of 10,000, reaching levels significantly below the expected EoR in the perfect calibration  
1385 case (panel (*iv*)).

1386 This implies that spectral structure introduced into the calibration solutions by the  
1387 mismatch between the set of instrumental and single calibration beam leads to mode  
1388 mixing from low  $k_{\parallel}$  modes to high  $k_{\parallel}$  well beyond the expected foreground wedge. It  
1389 also demonstrates that this excess beam-based chromaticity introduces power to the  
1390 EoR window which cannot be mitigated by simply subtracting partial models of the  
1391 foregrounds.

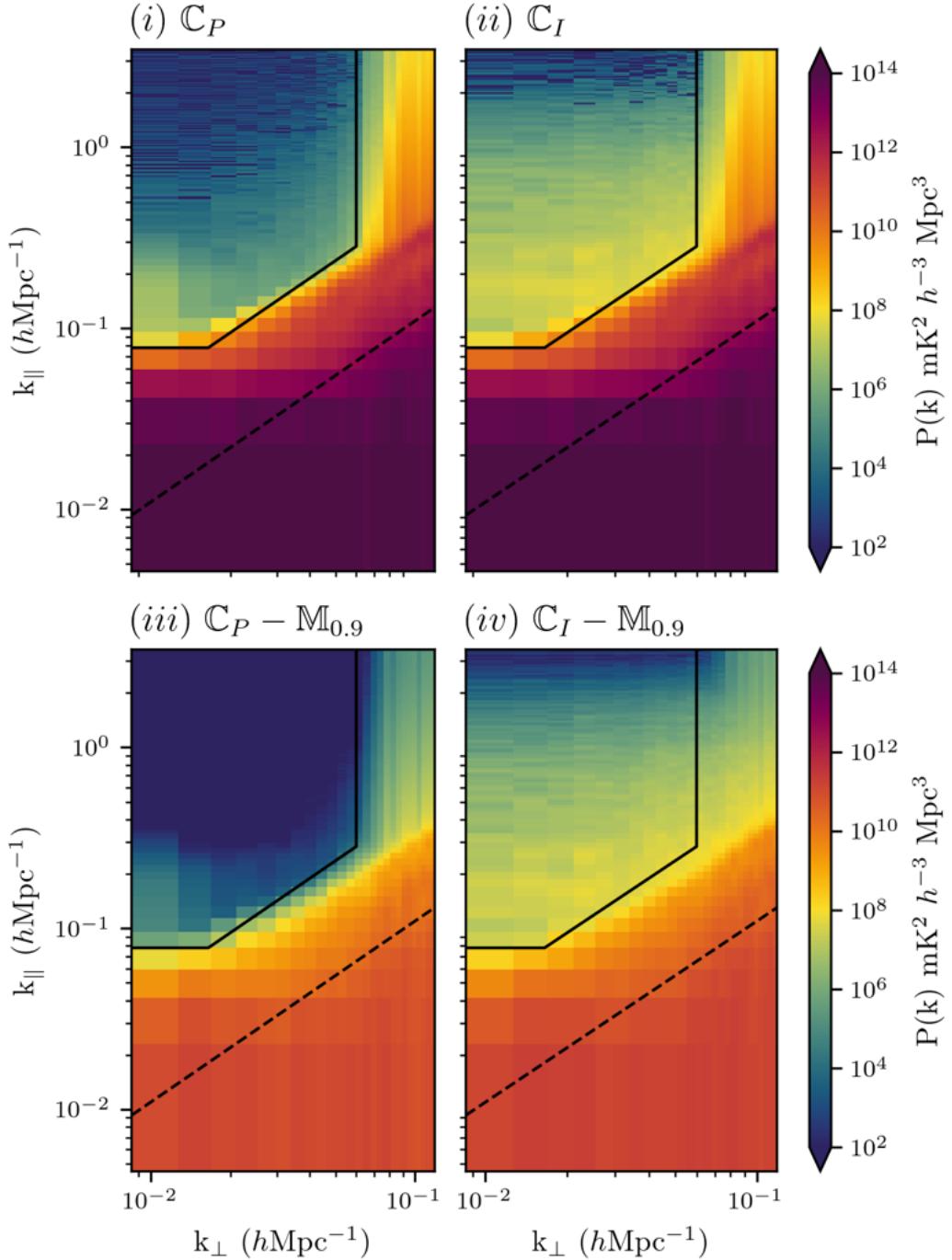


Figure 4.6: Cylindrical-averaged power spectra of the two calibration scenarios described in Section 4.4.3. The left column (panels *i*, *iii*) represents perfect calibration where the varied beam models are accounted for during calibration. The right column (panels *ii*, *iv*) represent imperfect calibration when a simple and incomplete instrumental model is used for calibration. The bottom row (panels *iii*, *iv*) are identical to the top row (panels *i*, *ii*) except that a 90% of the brightest foreground flux have been subtracted. The top left region of each panel is the EoR window where a search for the cosmological signal can be performed.

1392    4.6.2. 1D Power Spectrum

1393    Spherically averaging the  $k$ -modes within the EoR window leads to a 1D power spec-  
1394    trum typically assumed to be free of foreground power which can then be used to make  
1395    cosmological measurements. In this work, we use the 1D power spectrum to quantify  
1396    the extent of foreground spectral leakage into the EoR window caused by the differing  
1397    instrumental and calibration beams.

1398    In Figure 4.7 the grey dotted line and shaded regions denote the power level of an  
1399    EoR model and its 95% confidence limits (Barry et al., 2019b; Greig et al., 2022) - which  
1400    are used as a reference to compare levels of beam-based spectral leakage. Only when  
1401    foreground leakage into the EoR window is below the EoR level and thus a sub-dominant  
1402    systematic, is there any hope of a direct measurement of the cosmological signal. The  
1403    different colours in Figure 4.7 denote varied levels of foreground subtraction from the  
1404    brightest 10% in apparent flux to a complete 100% of all sources in 10% integrated flux  
1405    bins (see Figure 4.5). The solid and dashed lines represent the perfect and imperfect  
1406    calibration cases respectively.

1407    In the imperfect calibration case (dashed lines in Figure 4.7) when an incomplete model  
1408    of the telescope (i.e. a single beam model) is assumed during calibration, the resultant  
1409    spectral structure introduced into the calibration solutions leads to foreground spectral  
1410    leakage over a 1000 times our fiducial EoR model between  $k=0.1$  and  $k=1 \text{ hMpc}^{-1}$ . This  
1411    foreground leakage into the EoR window is not appreciably reduced by subtracting mod-  
1412    els of foreground sources (dashed lines in Figure 4.7 lie practically on top of one another),  
1413    demonstrating that the excess chromaticity introduced by beam-based calibration errors  
1414    results in mode mixing beyond the well characterised foreground-wedge effect caused  
1415    by instrumental chromaticity.

1416    If an accurate instrumental model is used during calibration, as demonstrated by the  
1417    perfect calibration scenario (solid lines in Figure 4.7), systematically subtracting models  
1418    of the brightest apparent flux reduces spectral leakage into the EoR window till it is a sub-  
1419    dominant effect. In fact, the solid navy blue line which represents a complete subtraction  
1420    of foreground flux ( $\mathbb{C}_P - \mathbb{M}_{1.0}$ ) during perfect calibration lies at the  $\sim 10^{-20} \text{ mK}^2$  level  
1421    far below the bottom of the y-axis in Figure. 4.7, and is numerically insignificant. This  
1422    demonstrates that in the perfect calibration scenario, all foreground flux which is known  
1423    can be subtracted from the EoR window, in contrast to the imperfect calibration scenario  
1424    where a fundamental spectral leakage imprint remains in the EoR window despite the  
1425    subtraction of sky-model flux.

1426    A pertinent question to consider is why there is any power in the perfect calibration  
1427    case prior to any flux subtraction ( $\mathbb{C}_P$ : black solid line in Figure 4.7), since all the fore-  
1428    ground flux is expected to be contained in the foreground-wedge. We primarily attribute  
1429    this to excess chromaticity from the implementation of the FEE beam model, but can also  
1430    arise from the bandpass, decoherence due to frequency smearing, and other unidentified  
1431    analysis or instrumental systematics. Any excess chromaticity leads to mode mixing of  
1432    power from the foreground-wedge into the EoR window, which is then measured in the  
1433    spherically-averaged power spectrum.

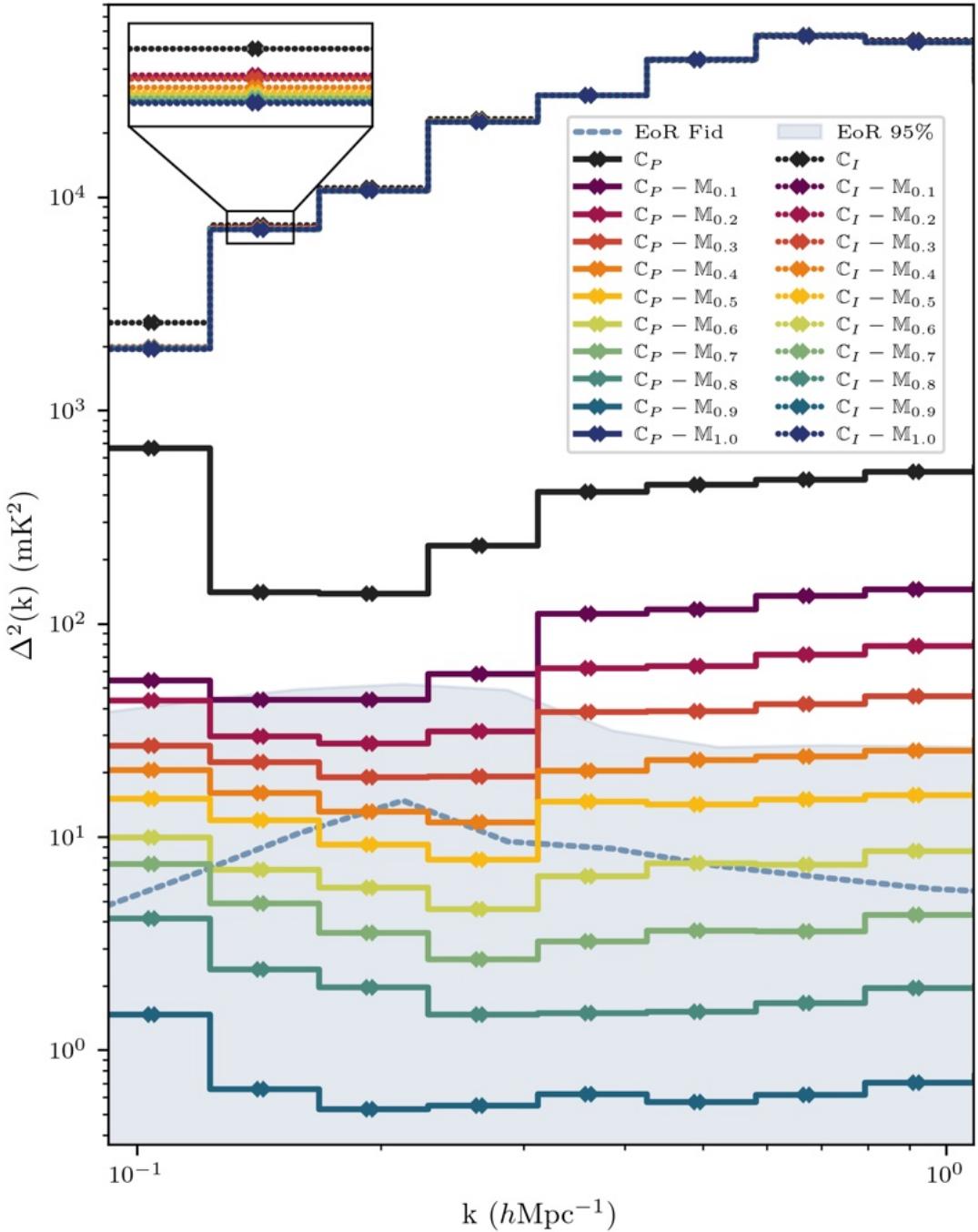


Figure 4.7: Spherically-averaged power spectra within the EoR window. The dashed lines represent the imperfect calibration ( $\mathbb{C}_I$ ) scenario, while the solid lines represent the perfect calibration ( $\mathbb{C}_P$ ) case. The coloured lines represent a systematic subtraction of apparent foreground flux, in intervals between 10% to 100%. The grey dotted line is the fiducial EoR level while the shaded region represents the 95% confidence limits. Note that all the dashed lines from the imperfect calibration scenario lie practically on top of one another, and do not change significantly after subtracting foreground flux models.

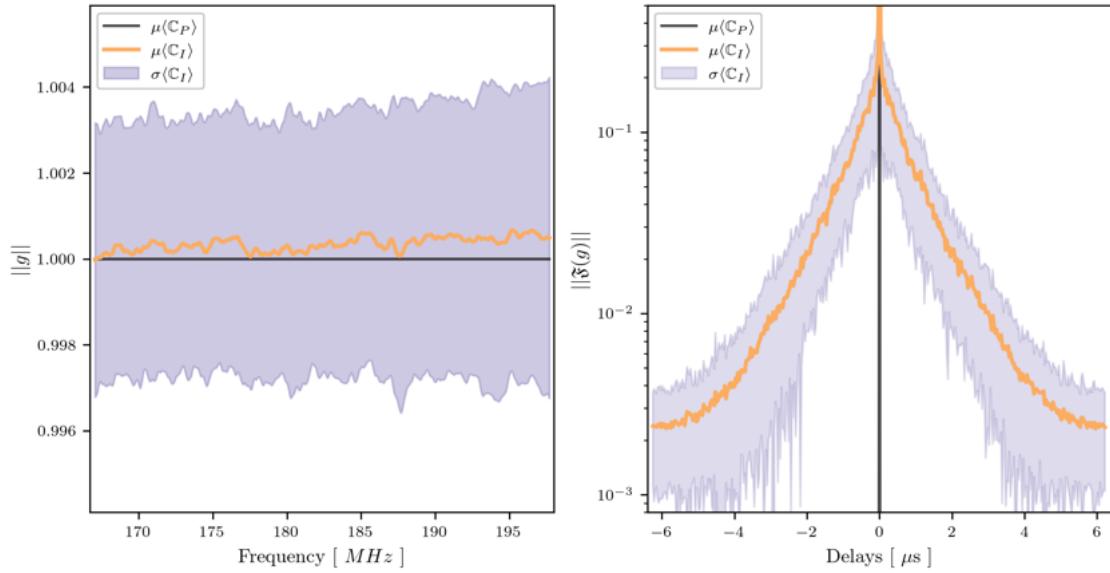


Figure 4.8: Gain amplitudes of calibration solutions are shown in the left panel, with the black line representing perfect calibration averaged over tiles ( $\mu(\mathbb{C}_P)$ ), while the yellow line is the antenna averaged gain amplitudes in the imperfect calibration scenario ( $\mu(\mathbb{C}_I)$ ) with the purple region enclosing 68% of values ( $\sigma(\mathbb{C}_I)$ ). The right panel is the Fourier transform along frequency of gain amplitudes, and plot the results as a function of delay. The black line is perfect calibration, while the yellow line represent the antenna averaged quantity and purple region encloses 68% of values from the imperfect calibration scenario.

1434    4.6.3. *Spectral Structure in Calibration Solutions*

1435    The 2D and 1D power spectra clearly demonstrate the effects of beam-based calibration  
1436    errors, yet it is instructive to explore the raw calibration solutions obtained in Section  
1437    4.4.3, where beam-based spectral leakage initially originates.

1438    The fiducial simulation from Section 4.4.2 was noiseless, and used a sky catalogue of  
1439    30,000 sources to generate visibilities which emulated a measurement by the MWA with  
1440    a set of deformed beam models ( $V^{\text{data}}$ ). While thermal noise can be a significant system-  
1441    atic in single observations, for a temporally stable instrument such as the MWA, noise  
1442    in calibration solutions has been shown to incoherently average (Barry et al., 2019a). In  
1443    the perfect calibration scenario, an identical set of deformed beams and sky catalogue  
1444    are used to generate model visibilities ( $V^{\text{model}}$ ) for the calibration minimisation process  
1445    (see Equation 4.4). In the absence of noise, the fact that the data and model visibilities  
1446    are identical leads to gain solutions which are unity within double precision across the  
1447    frequency band (black line in the left panel of Figure 4.8). Adding thermal noise to the  
1448    simulations would introduce uncertainty in the calibration solutions leading to a devi-  
1449    ation for unity described above. This has the potential to introduce spectral leakage  
1450    into the EoR window, even in simulations using a single perfect beam model. Further  
1451    investigations along this line are left for future works.

1452    In the imperfect calibration scenario, a single perfect beam model is used to generate  
1453    the model visibilities ( $V^{\text{model}}$ ) with the original sky catalogue. During the calibration  
1454    process, the mismatch between the data and model visibilities lead to non-unity gain  
1455    solutions as a function of frequency. This frequency structure is the root cause of fore-  
1456    ground leakage from the EoR wedge into the EoR window observed in the power spectra,  
1457    and can be solely attributed to an incomplete representation of the instrument (single  
1458    beam model instead of set of deformed beam models) during the calibration process. The  
1459    yellow solid line in the left panel of Figure 4.8 represent the antenna-averaged calibra-  
1460    tion gain amplitudes to visualise any common spectral structure, while the purple region  
1461    encloses 68% of values.

1462    To gauge the spectral structure within calibration solutions, we perform a Fourier  
1463    transform across frequency, which decomposes calibration error amplitudes as a func-  
1464    tion of delay modes. In the perfect calibration scenario, this results in a delta function  
1465    at a delay of zero, and any deviation from this would lead to excess calibration chro-  
1466    maticity, resulting in mode mixing from the foreground-wedge into the EoR window.  
1467    The right panel of the Figure displays the Fourier transform of the calibration gain am-  
1468    plitudes, with the green line being the antenna-averaged quantity, while the blue region  
1469    again encloses 68% of values.

1470    4.7. CONCLUSIONS & NEXT STEPS

1471    This work explores the impact that imperfect and varied beams across a radio inter-  
1472    ferometer could have on EoR power spectrum measurements. We demonstrate how  
1473    incomplete representations of varied and complex beams during calibration can lead to  
1474    the leakage of foreground power into modes sensitive to the cosmological signal. This  
1475    leads to contamination beyond the well-known foreground wedge into the EoR window,  
1476    which is typically assumed to be free of foreground contaminants, at levels which ex-

1477 exceed the expected EoR level by factors greater than  $\sim 1000$  between  $k=0.1\text{--}1 \text{ hMpc}^{-1}$ .  
1478 We also demonstrate how this effect is not improved by subtracting models and fore-  
1479 ground sources, and necessitates the inclusion of validated and measured beam models  
1480 in calibration frameworks.

1481 Appreciable differences have been measured between cutting-edge electromagnetic  
1482 Fully Embedded Element (FEE) MWA beam model (Sutinjo et al., 2015) and in-situ mea-  
1483 surements using satellites (Line et al., 2018; Chokshi et al., 2021). These effects are pre-  
1484 dominantly measured as deformations in beam sidelobes, and are attributed to a variety  
1485 of environmental factors. In Section 4.3, we develop a method of leveraging the 16 dipole  
1486 gain parameters, natively used to weight the contribution of each dipole to the summed  
1487 MWA tile response, to deform the FEE beam model to best match satellite beam maps  
1488 from Chokshi et al. (2021).

1489 In Section 4.4, we develop a physically motivated model to simulate a full 128-tile  
1490 MWA array composed of realistically deformed beams based on the 14 dual polarization  
1491 maps available from Chokshi et al. (2021). Using 30,000 complex sources from the  
1492 LoBES catalog (Lynch et al., 2021), we create a noiseless fiducial simulation using the set  
1493 of deformed beams, which emulates a real measurement with the MWA. We now cali-  
1494 brate our fiducial simulation using two strategies; perfect calibration where a complete  
1495 understanding of the instrument is assumed by using the set of deformed beams during  
1496 calibration, or imperfect calibration where a single FEE beam model is used to emu-  
1497 late currently accepted calibration strategies which do not account for beam variations  
1498 across the radio interferometer. Using the spatial power spectrum described in Section  
1499 4.5, we investigate the effects of beam-induced calibration errors on the prospects of  
1500 recovering an EoR signal in Section 4.6 (see Figures 4.6 & 4.7).

1501 Our work demonstrates that **including physically motivated beam models dur-**  
1502 **ing calibration has the potential to reduce foreground spectral leakage into the**  
1503 **EoR window by factors greater than 1000, which could potentially put a statis-**  
1504 **tical detection of the cosmological signal within grasp.** We outline the necessary  
1505 step required to make this technique applicable to real data below:

- 1506 • Satellite beam maps of each station in the radio interferometer will be a crucial first  
1507 step. The satellite backend developed in Line et al. (2018); Chokshi et al. (2021) and the  
1508 EMBERS analysis pipeline (Chokshi et al., 2020) have provided excellent all-sky maps at  
1509 137MHz at a very reasonable expense.
- 1510 • A key question which has not been addressed by this work is the fact that the satellite  
1511 maps by Chokshi et al. (2021) span a 1.4 MHz bandwidth, and are relatively narrowband  
1512 in comparison to the observing bandwidth of  $\sim 30$  MHz. Thus the beam deformation  
1513 model described in Section 4.3 is generated from narrowband data and applied across the  
1514 broader observing band. The validity of this approach must be validated and augmented  
1515 using a drone-based beam measurement system (Chang et al., 2015; Jacobs et al., 2017;  
1516 Bolli et al., 2018; Ninni et al., 2020; Paonessa et al., 2020; Herman et al., 2024).
- 1517 • The 16 parameter beam deformation model developed in this work was physically  
1518 motivated by the aperture array design of MWA tiles, and could be modified to be ap-  
1519 plicable to telescopes such as LOFAR, NenuFAR, or the future SKA-Low. Unfortunately,  
1520 telescopes such as HERA which employ parabolic dishes as their interreferometric ele-

1521 ments will require new innovative models such as those developed by Wilensky et al.  
1522 (2024).

1523 We have demonstrated how a mismatch between the complex set of instrumental  
1524 beams and the beam assumed during calibration can lead to the introduction of arti-  
1525 ficial spectral structure into calibration solutions which results in foreground leakages  
1526 beyond the foreground wedge and into the EoR window. While we have shown that this  
1527 beam-based calibration leakage can be mitigated by the inclusion of more accurate repre-  
1528 sentations of instrumental beam models into calibration frameworks, it is not necessarily  
1529 the only solution. While beyond the scope of this work, we leave the investigation of  
1530 direction-dependant calibration, delay filtering, and regularised calibration solutions for  
1531 future works.

1532

## CHAPTER 5

1533

### 1534 Effects of Deformed Interferometric Beams: Depolarization 1535 & Rotation Measure

1536

1537 **This chapter is based on a draft of**

1538 *A. Chokshi, N. Barry, B. Pindor, J. L. B. Line, C. J. Riseley, X. Zhang, R. L. Webster*  
1539 to be submitted to the Publications of the Astronomical Society of Australia,

1540 **reformatted with the following changes only:**

- 1541 • **The text is styled and restructured to match the rest of this thesis.**  
1542 • **Where necessary, bibliographic records are updated.**

#### 1543 5.1. ABSTRACT

1544 The origins of cosmic magnetism can be unveiled by observing grids of polarised sources  
1545 across large cosmological volumes, recently enabled by the adoption of wide-field inter-  
1546 ferometers. This work explores the impact which non-identical beam responses can have  
1547 on instrumental depolarisation, which can result in biased populations within polarised  
1548 surveys. All-sky satellite measurements of Murchison Widefield Array (MWA) beams  
1549 have revealed significant sidelobe deviations from cutting-edge electromagnetic simula-  
1550 tions at the  $\sim 10\%$  zenith power level. This work builds an all-sky simulations framework  
1551 of the MWA composed of physically motivated deformed beams, as a test-bed to explore  
1552 the impacts of deformed beams on polarisation science. We observe  $\sim 1\%$  fractional  
1553 leakages at the beam centre rising to  $\sim 5\%$  at the full width half maximum ( $\sim 22^\circ$  at  
1554 180MHz), which is similar to the baseline leakage observed in cutting-edge MWA beam  
1555 models, but with significantly altered leakage morphology. The depolarisation observed  
1556 with the set of deformed beams is  $\geq 10\%$  worse than that observed with a single beam,  
1557 and exhibits large gradients and non-uniform patches. We demonstrate how this altered  
1558 leakage morphology is not improved by traditional direction independent calibration,

1559 and outline avenues of investigations to improve the polarised behaviour of large im-  
1560 perfect interferometric arrays.

## 1561 5.2. INTRODUCTION

1562 Extended interferometric arrays have been adopted as the tool of choice for the efficient  
1563 mapping of large cosmological volumes for multiple reasons. Constructed from hosts  
1564 of identical and cheap dipoles, these aperture arrays can be coherently synthesised to  
1565 achieve high angular resolutions over unprecedented large field-of-views. The search for  
1566 distant and faint cosmic signals, coupled with the paradigm of simple software-driven  
1567 telescopes, necessitates a precise and prior understanding of the instrument when push-  
1568 ing the upper bounds of sensitivity. A crucial part of the calibration process involves an  
1569 understanding of the telescope's varied sensitivity across the sky, or its primary beam  
1570 response. The construction of such arrays in remote and harsh radio-quiet sites can  
1571 have a detrimental impact on the longevity of instruments, leading to an increased rate  
1572 of dipole failure and other environmental perturbations to the beam models requiring  
1573 more complicated calibration schemes to be considered in the pursuit of high fidelity  
1574 science.

1575 The Murchison Widefield Array (MWA<sup>\*</sup>; Tingay et al., 2013; Wayth et al., 2018) is a  
1576 low frequency radio interferometer, located in remote Western Australia at the Inyarrima-  
1577 manha Ilgari Bundara Murchison Radio-astronomy Observatory, and is a precursor to  
1578 the Square Kilometer Array (SKA<sup>†</sup>). The MWA is an aperture array telescope, with 128  
1579 receiving tiles, each constructed from a grid of  $4 \times 4$  dual polarization bow-tie dipoles.  
1580 The MWA is a fully polarised instrument capable of imaging the sky in all Stokes pa-  
1581 rameters using orthogonal linear dipoles in the MWA tiles, aligned along the East-West  
1582 and North-South directions respectively.

1583 Large surveys of polarised radio sources and the exploration of cosmic magnetism are  
1584 among the key science goals of low frequency radio telescopes such as the MWA (see,  
1585 Wayth et al., 2015; Hurley-Walker et al., 2014, 2017; Riseley et al., 2018, 2020). Radio  
1586 polarimetry at low frequencies is plagued by a host of challenges which include Faraday  
1587 depolarisation (where polarised sources depolarise with increasing wavelength; Burn  
1588 1966), synthesised beam depolarization (here a mix of polarisation angles within the  
1589 PSF can lead to an apparent reduction in observed polarisation fraction), and primary  
1590 beam depolarisation (errors in beam models can lead to the loss of polarised signal).  
1591 Significant flux leakage from Stokes I into other Stokes parameters have been observed  
1592 in MWA polarimetric observations (see, Bernardi et al., 2013; Lenc et al., 2017, 2018).  
1593 In zenith observations, leakage of  $\sim 1\%$  at the beam centre and  $\sim 4\%$  at the edge (full  
1594 width half max  $\sim 25^\circ$  at 150MHz) of the primary beam have been measured, increasing  
1595 to a range of 12-40% at off-zenith pointings.

1596 The statistical detection of 21-cm Epoch of Reionisation (EoR) signal is another key  
1597 priority of low-frequency arrays such as the MWA (Bowman et al., 2013; Beardsley et al.,  
1598 2019b). Obscured by various foregrounds up to five orders of magnitude brighter than  
1599 the redshifted cosmological signal (Oh & Mack, 2003; Santos et al., 2005; Pober et al.,

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\*<http://www.mwatelescope.org>

†<https://www.skatelescope.org>

1600 2013; Yatawatta et al., 2013) a detection has yet to be made. Complex gain errors dur-  
 1601 ing calibration and primary beam model errors can lead to the leakage of polarised flux  
 1602 into the Stokes  $I$  maps hindering an EoR detection (Geil et al., 2011; Asad et al., 2015,  
 1603 2016, 2018; Kohn et al., 2016, 2019). Faraday rotation measure techniques and direc-  
 1604 tion dependant calibration can be used to decontaminate leakage from various polarised  
 1605 foregrounds (Geil et al., 2011; Asad et al., 2016).

1606 Large computational simplifications in interferometric imaging are achieved by as-  
 1607 suming that receiving elements across an array are identical. The reality of environ-  
 1608 mental interactions across large arrays leads to frequent failure of dipoles and more  
 1609 nuanced deformations in beam models, breaking the assumption of identical receiving  
 1610 elements. This is expected to be exacerbated and costly for extremely large arrays, such  
 1611 as the future SKA-Low telescope (Mellema et al., 2013; Koopmans et al., 2015). In-situ  
 1612 satellite measurements of MWA tiles revealed variations in sidelobe sensitivity at the  
 1613  $\sim 10\%$  level (Line et al., 2018; Chokshi et al., 2021). The impact of assuming a single  
 1614 beam model during calibration of measurements which encode non-identical beams has  
 1615 been investigated by Chokshi et al. 2024. They revealed leakage of non-polarised fore-  
 1616 grounds into theoretically uncontaminated modes at levels over 1000 times brighter than  
 1617 the expected EoR, highlighting the importance of a precise understanding of instrumen-  
 1618 tal complexities.

1619 This work explores the importance of individually validated beam models across in-  
 1620 terferometric arrays for the accurate and unbiased recovery of polarised flux. It validates  
 1621 all-sky primary beam based polarisation leakage for the current cutting-edge MWA beam  
 1622 model, and compares them to the results simulated via an array of realistically deformed  
 1623 beam models. This work also highlights the importance of diverse beam sidelobes to  
 1624 polarisation science as we enter the SKA era.

1625 A summary of the rotation measure synthesis technique is presented in Section 5.3,  
 1626 following which we develop a Jones matrix based framework of beam depolarization in  
 1627 Section 5.4. A simulation pipeline is developed in Section 5.5 to evaluate all-sky beam  
 1628 depolarisation induced by interferometric arrays composed of uniquely deformed beams.  
 1629 Results are presented in Section 5.6 with concluding statements in Section 5.7.

### 1630 5.3. ROTATION MEASURE SYNTHESIS

1631 Faraday Rotation Measure Synthesis is a novel technique developed and formulated by  
 1632 Burn (1966); Brentjens & de Bruyn (2005); Heald (2009). It leverages the Fourier rela-  
 1633 tionship between observed complex narrowband linear polarisation and the function  
 1634 describing intrinsic polarisation, to disentangle multiple polarisation components along  
 1635 a line-of-sight.

1636 Magnetised plasma in the intergalactic and interstellar medium acts as a birefringent  
 1637 medium, rotating the polarised plane of radiation as a function of frequency. This effect  
 1638 is known as Faraday rotation, and rotates the polarisation angle by:

$$\chi(\lambda) = \chi_0 + \text{RM} \cdot \lambda^2, \quad (5.1)$$

1639 where  $\chi_0$  is the intrinsic polarisation angle and  $\chi(\lambda)$  is the polarization angle at wave-  
 1640 length  $\lambda$ . RM is the Faraday rotation measure, which characterises the amount of rota-

1641 tion and is given by:

$$\text{RM} = 0.81 \int_{\ell}^0 n_e \vec{B} \cdot d\vec{\ell}, \quad (5.2)$$

1642 where  $\ell$  is the distance to the source in parsecs,  $n_e$  is the free electron density expressed  
1643 in units of  $\text{cm}^{-3}$  and  $\vec{B}$  is the magnetic field strength in  $\mu\text{G}$ . It is often useful to express  
1644 these quantities in terms of measured Stokes parameters  $I, Q, U$  and  $V$ . Polarisation angle  
1645  $\chi$  can be expressed as:

$$\chi = \frac{1}{2} \tan^{-1} \frac{U}{Q}, \quad (5.3)$$

1646 with the complex narrowband linear polarisation  $P$  being expressed in terms of Stokes  
1647 parameters and fractional polarisation ( $\Pi$ ), as:

$$P = Q + iU = \Pi I e^{2i\chi}. \quad (5.4)$$

1648 Traditionally, rotation measure was defined as the slope of the polarization angle  $\chi$   
1649 versus  $\lambda^2$ :

$$\text{RM} = \frac{d\chi(\lambda^2)}{d\lambda^2}.$$

1650 This approach is good in theory, but is often limited in its application. The linear fit de-  
1651 scribed above breaks down when there are multiple sources of polarised emission along  
1652 the line of sight. Faint sources with high RM often have low signal to noise in individual  
1653 channels. Integrating channels can lead to the decoherence of rapidly oscillating stokes  
1654  $Q$  and  $U$  fluxes resulting in a reduced perceived polarisation fraction, an effect dubbed  
1655 bandwidth depolarisation. Further, there is an  $n\pi$  radian ambiguity in the determination  
1656 of polarisation angle which can lead to multiple degenerate RM fits (see [Rand & Lyne, 1994](#)). Rotation measure synthesis can be used to overcome these issues while also being  
1657 capable of simultaneously disentangling multiple components of magnetic fields along  
1658 the line of sight.

1660 The elegance of the rotation measure (RM) synthesis technique comes from the ability  
1661 to invert the complex polarisation vector via a Fourier transform. Equation. 5.4, denotes  
1662 the observed complex polarisation vector, in which we can substitute  $\chi$  from Equation.  
1663 5.1, replacing RM with a more generalised quantity known as Faraday depth, ( $\phi$ ). As all  
1664 possible values of  $\phi$  can contribute to the observed polarisation vector,

$$P(\lambda^2) = \int_{-\infty}^{+\infty} \Pi I e^{2i[\chi_0 + \phi\lambda^2]} d\phi.$$

1665 This can be re-written as:

$$P(\lambda^2) = \int_{-\infty}^{+\infty} F(\phi) e^{2i\phi} d\phi,$$

1666 where  $F(\phi)$  is the Faraday dispersion function, describing the polarised flux as a function  
1667 of Faraday depth. This equation is in the form of a Fourier transform and can be inverted  
1668 to obtain the Faraday dispersion function  $F(\phi)$  in terms of observable quantities:

$$F(\phi) = \int_{-\infty}^{+\infty} P(\lambda^2) e^{-2i\phi\lambda^2} d\lambda^2. \quad (5.5)$$

1669 While this is an elegant result, a few caveats must be noted. Having a negative value  
 1670 of  $\lambda^2$  is non-physical, and in fact any real telescope will have a finite bandwidth and  
 1671 will not observe up to  $\lambda^2 = \infty$ . This problem is solved by introducing a quantity known  
 1672 as the rotation measure spread function (RMSF), which is convolved (\*) with the true  
 1673 Faraday dispersion function to produce an observed Faraday dispersion function given  
 1674 by:

$$\tilde{F}(\phi) = F(\phi) * R(\phi).$$

1675 This is analogous to the point spread function (PSF) of optical telescopes, which arise  
 1676 from the finite aperture of telescopes. In the case of the RMSF, the finite bandwidth  
 1677 of a radio telescope leads to the spread of the Faraday dispersion function ( $\phi$ ), from a  
 1678 compact delta function into a structure with sidelobes reminiscent of a sinc function. For  
 1679 a more rigorous introduction to RM synthesis, see [Burn \(1966\)](#); [Brentjens & de Bruyn \(2005\)](#);  
 1680 [Heald \(2009\)](#).

## 1681 5.4. BEAM DEPOLARIZATION

1682 Beam depolarisation is one of the effects that can arise from imperfect beam models.  
 1683 A polarised source which undergoes Faraday rotation via a magnetised plasma, is ob-  
 1684 served to have a sinusoidally oscillating flux in frequency, in both  $Q$  &  $U$  Stokes param-  
 1685 eters. Typical synchrotron radio sources have Stokes  $I$  fluxes which follow power-law  
 1686 behaviour with the flux density  $S \propto \nu^\alpha$ , where the typical spectral index is  $\alpha = -0.7$ .  
 1687 Beam errors can lead to complex couplings between the Stokes parameters, leading to  
 1688 ripples in the  $I$  &  $V$  fluxes, while decreasing the amplitudes of  $Q$  &  $U$  fluxes, which is ob-  
 1689 served as a loss of polarisation. In this section we will build a mathematical framework  
 1690 to understand these effects, based on the Jones matrix formalism described by [Hamaker et al. \(1996\)](#).

1692 We begin by defining a feed Jones matrix for antenna A:

$$\mathbf{J}_A = \begin{bmatrix} G_{Ax} & l_{Ax} \\ -l_{Ay} & G_{Ay} \end{bmatrix}, \quad (5.6)$$

1693 with the diagonal terms  $G_{Ax}$ ,  $G_{Ay}$  representing the complex gains and the off-diagonal  
 1694 terms  $l_{Ax}$ ,  $l_{Ay}$  the leakage terms of the X & Y dipoles respectively. The gain terms ac-  
 1695 count for sensitivity variations, while the leakage terms account for erroneous mixing of  
 1696 signals between the orthogonal X & Y dipoles. For a perfect feed, the complex gains are  
 1697 unity while the leakage terms are zero, reducing the feed Jones matrix to the Identity.

1698 The complex vector amplitudes of a quasi-monochromatic signal propagating through  
 1699 space, evaluated at antenna A, can be represented as:

$$\mathbf{e}_A = \begin{bmatrix} e_{Ax} \\ e_{Ay} \end{bmatrix}.$$

1700 .

1701 The effect of a feed Jones matrix on incoming signals  $e_A^{in}$  can be represented as:

$$\mathbf{e}_{A,out} = \mathbf{J}_A \mathbf{e}_{A,in}$$

1702 Consider two antennas A, B, with corresponding feed Jones matrices  $\mathbf{J}_A, \mathbf{J}_B$ . The visi-  
1703 bility matrix for a baseline defined by antennas A and B is the cross-correlation or the  
1704 outer product of electric field vectors  $\mathbf{e}_A$  and  $\mathbf{e}_B$  is given by:

$$\mathbf{e} = \mathbf{e}_A \otimes \mathbf{e}_B^* = \begin{bmatrix} e_{Ax} e_{Bx}^* \\ e_{Ax} e_{By}^* \\ e_{Ay} e_{Bx}^* \\ e_{Ay} e_{By}^* \end{bmatrix}.$$

1705 The column vector above represents the complete set of polarised quantities measured  
1706 by an interferometer such as the MWA, made in the instrumental frame of reference; i.e.,  
1707 aligned with the local EW, NS coordinate system on the ground. We can now observe  
1708 the effect the two feed Jones matrices have on measurements:

$$\begin{aligned} \mathbf{e}_{out} &= \mathbf{e}_{A,out} \otimes \mathbf{e}_{B,out}^* = \mathbf{J}_A \mathbf{e}_{A,in} \otimes \mathbf{J}_B^* \mathbf{e}_{B,in}^* \\ &= (\mathbf{J}_A \otimes \mathbf{J}_B^*) (\mathbf{e}_{A,in} \otimes \mathbf{e}_{B,in}^*) = \mathbf{J} \mathbf{e}_{in}. \end{aligned} \quad (5.7)$$

1709 These measurements are in a local instrumental Altitude and Zenith angle coordinate  
1710 frame. Stokes parameters are basis dependant, and while valid in any orthogonal basis  
1711 they are typically presented in a coordinate system aligned with Right Ascension and  
1712 Declination. Due to the bow-tie nature of MWA dipoles, and projection effects, the local  
1713 Altitude and Zenith angle coordinate frame is only orthogonal at the zenith. To calculate  
1714 stokes parameters in any arbitrary direction, we can perform a rotation over parallactic  
1715 angle to be aligned with the celestial Right Ascension and Declination frame. Measured  
1716 instrumental visibilities, in the celestial frame, can be related to Stokes visibilities via a  
1717 linear transformation given by:

$$\begin{bmatrix} XX \\ XY \\ YX \\ YY \end{bmatrix} = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 0 & 1 & i \\ 0 & 0 & 1 & -i \\ 1 & -1 & 0 & 0 \end{bmatrix} \begin{bmatrix} I \\ Q \\ U \\ V \end{bmatrix} \quad (5.8)$$

1718 Substituting Eqn. 5.8 in Eqn. 5.7, we obtain a set of equations which can be solved to  
1719 express the observed Stokes parameters  $I', Q', U' & V'$  in terms of feed Jones matrices  
1720 and real Stokes parameters  $I, Q, U & V$ . The relevant equations can be found in the  
1721 Appendix A.

1722 Figure 5.1 demonstrates the efficacy of the developed framework at reproducing beam  
1723 depolarisation on a toy two element interferometer. We simulate a radio source with a  
1724 reference Stokes  $I$  flux of 7 Jy at 200 MHz, with a spectral index of  $\alpha = -0.7$ . Stoke  $V$   
1725 fluxes of real radio sources are often observed to be atypical - in this work we assume  
1726 a power law to demonstrate how the artificial coupling of  $I$  and  $V$  fluxes can occur via  
1727 beam errors. The source has a simulated rotation measure of  $+20 \text{ rad/m}^2$  and a fractional  
1728 polarisation of 30 %. The black lines in all panels of Fig. 5.1 depict the RM spectra, and the

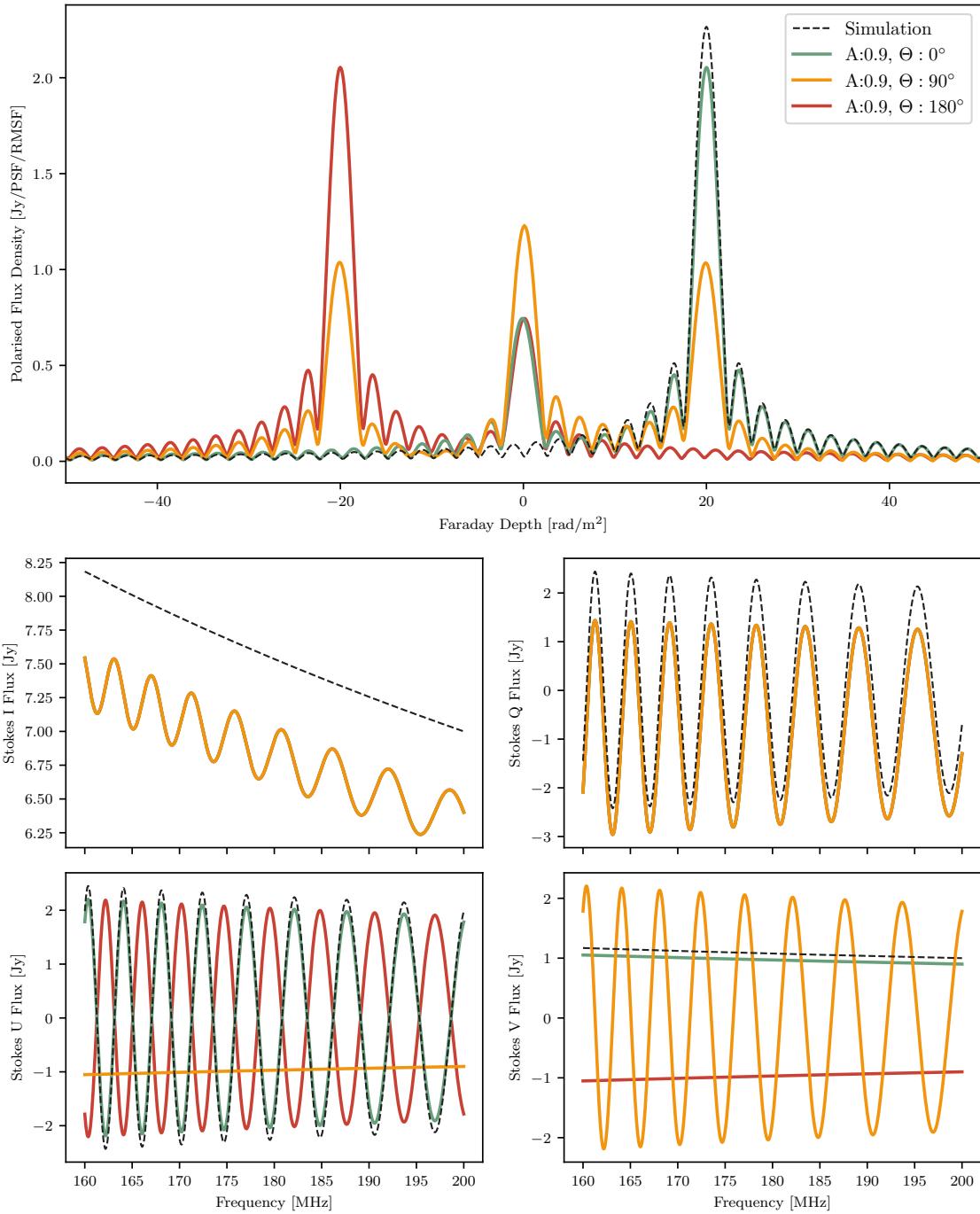


Figure 5.1: Theoretical models of beam depolarisation from a toy two element interferometer based on the Jones matrix formalism described in Section 5.4. The top panel shows the RM spectra of a simulated radio source of  $\text{RM} = +20 \text{ rad/m}^2$  (Black), with the coloured lines depicting various beam errors. In this model, the X dipole of both tiles are reduced to 90%, with the aqua, ochre, orange lines corresponding to phase errors of  $\Theta = 0^\circ, 90^\circ, 180^\circ$  respectively. The lower four panels show the effects of the above beam errors on the four Stokes parameters.

I, Q, U, V Stokes fluxes of the simulated source over a 160 to 200 MHz frequency range, where the MWA is most sensitive to large Faraday depths. The coloured lines show various effects that can be produced using the above Jones matrix formalism. Here, the amplitude of the X dipoles in both tiles A & B were reduced to 90%, in addition to a range of phase errors, indicated by  $\Theta$  in the top panel of Fig. 5.1. The top panel shows that it is possible to almost completely depolarise the signal, or in extreme cases “mirror” the RM spectra peak, with a RM of  $-20 \text{ rad/m}^2$  measured instead of the true  $+20 \text{ rad/m}^2$ . This would falsely be interpreted as a reversal in the direction of the line of sight magnetic field, purely due to beam errors. The bottom four panels of Fig. 5.1 represent the Stokes I, Q, U & V fluxes as a function of frequency. Note the various frequency-dependant effects that are introduced due to beam errors, manifested in the form of ripples or phase errors in the observed  $I'$ ,  $Q'$ ,  $U'$  &  $V'$  fluxes (see Appendix A).

## 5.5. SIMULATION FRAMEWORK

The primary purpose of this work is to investigate the effects non-uniform and deformed beams across an interferometric array can have on Faraday Rotation Measure Synthesis and the apparent depolarisation of polarised sources via beam errors. Chokshi et al. (2021) measured significant sidelobe distortions in 14 MWA tiles at a 10% level. A framework to model and physically emulate the effect of deformed beams across a 128 tile MWA array was developed and tested in the context of Epoch of Reionisation science in Chokshi et al. (2024). Leveraging the 16 available dipole gain parameters in the MWA FEE beam model (Sokolowski et al., 2017; Sutinjo et al., 2015), Chokshi et al. (2024) used a Bayesian MCMC framework to optimally emulate beam deformations measured by Chokshi et al. (2021) by creating a dipole based weighting scheme. Drawing from this sample of optimal dipole gain parameters, 128 physically motivated deformed (DEF) MWA beams were generated to populate a realistically deformed MWA array. For a more in-depth review of this methodology refer to Chokshi et al. (2024).

hyperdrive\* (Jordan et al., in prep) is a cutting-edge sky based calibration tool designed for the MWA, developed to be the successor to the RTS or the Real Time System (Mitchell et al., 2008). We perform hyperdrive simulation with either a perfect FEE beam model, or a unique set of deformed (DEF) beams described above. For each beam type (FEE or DEF), 40 simulations are performed using a calibration source list and a grid of polarised sources with one of 40 possible RM values to determine the all-sky effect of deformed beams on RM Synthesis and depolarisation.

The 20,000 brightest sources from the LoBES survey (Lynch et al., 2021), centered around the EoR0 field (R.A.  $0h$ , Dec  $-27^\circ$ ), represent the set of fiducial stokes  $I$  calibration sources. These are combined with a set of 6144 simulated polarised sources placed on a HEALPi x (Gorski et al., 2005) grid with (NSIDE=32, spacing  $\sim 110$  arcseconds) across the sky (see Figure 5.2). Each polarised source is identical to the one used in Section 5.4 (See black line in Fig. 5.1) – reference Stokes  $I$  flux of 7 Jy at 200 MHz, with a spectral index of  $\alpha = -0.7$ , and a fractional polarisation of 30 %. For each set of simulations, the RM value of all the polarised sources is selected from values spanning  $-70$  to  $+70 \text{ rad/m}^2$  at intervals of  $3.5 \text{ rad/m}^2$ , with models of each distinct RM being shown in Figure 5.3.

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\*[https://github.com/MWATelescope/mwa\\_hyperdrive](https://github.com/MWATelescope/mwa_hyperdrive)

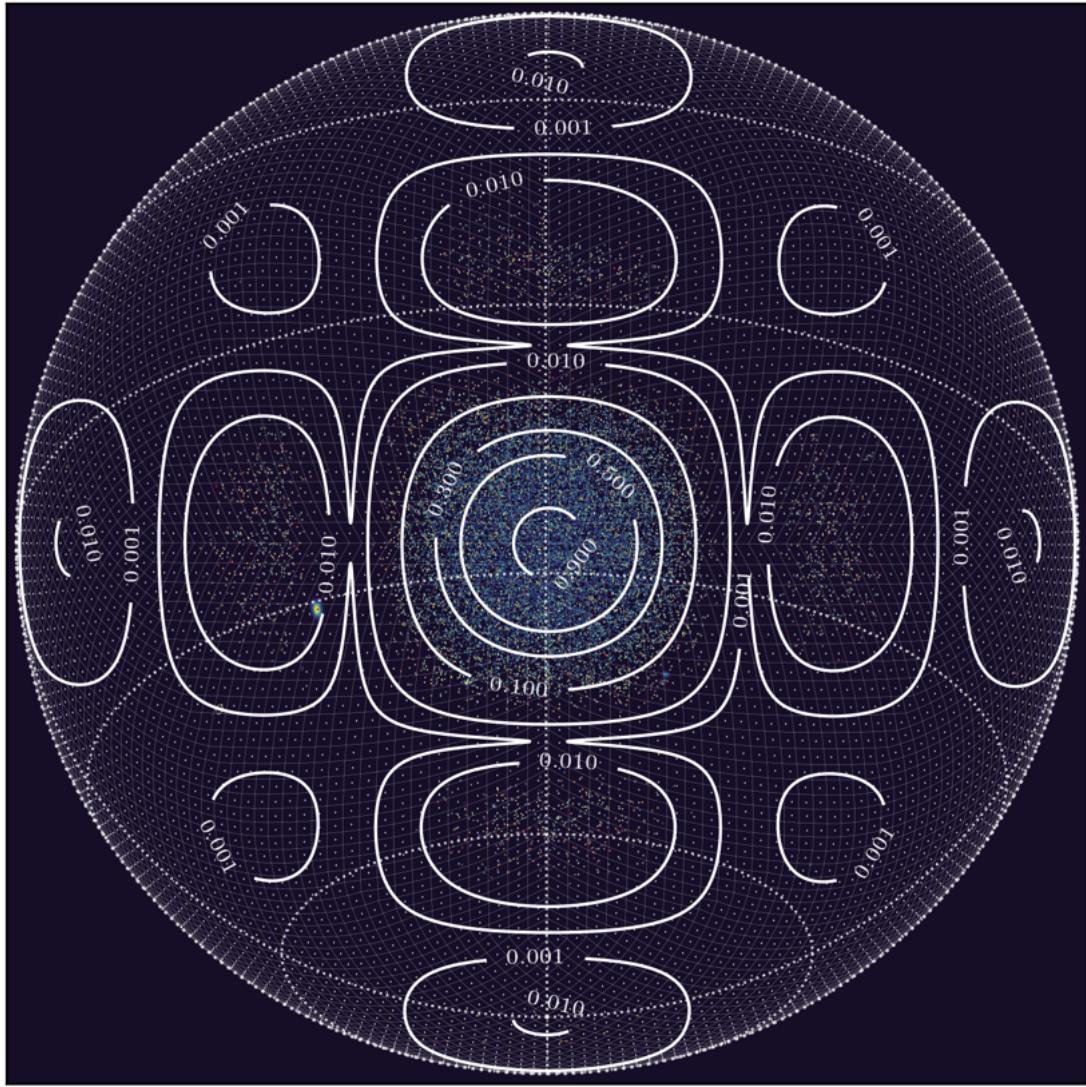


Figure 5.2: A simulated all-sky field-of-view with 20,000 calibration sources distributed across the sky, seen in the coloured background. Each HEALPix pixel with a white dot at its center represents the 6144 polarised sources. The white contours denote levels of zenith normalised MWA beam power.

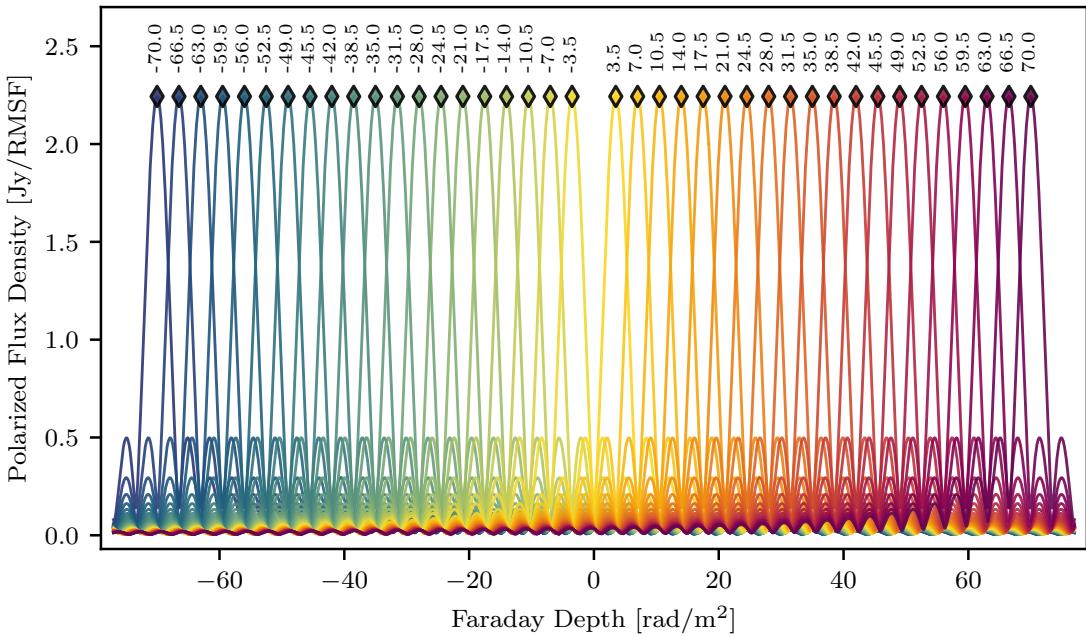


Figure 5.3: Models of the 40 possible RM values which each polarised source in Figure 5.2 can be. Each source displays significant sidelobe flux which is a result of the finite bandwidth and spectral resolution of the instrument, leading to input delta functions being convolved with the RMSF.

1771 The simulations are performed at a 320kHz frequency resolution, over the 169-200kHz  
 1772 band optimised for RM sensitivity as well as computational feasibility.

1773 These simulations contain a combination of flux from real stokes  $I$  calibration sources  
 1774 along with a grid of bright polarised sources. Any real observation of the sky would  
 1775 never contain this much polarised flux, yet the grid of polarised sources serves as a tool  
 1776 to probe all-sky polarisation leakage. The addition of a significant amount of artificial  
 1777 polarised flux has the scope to impact and bias any sky based calibration strategy. We  
 1778 mitigate any potential calibration bias introduced by the excess polarised flux by per-  
 1779 forming simulations using the FEE & DEF beams, with only the 20,000 stokes  $I$  calibra-  
 1780 tion sources. These simulations can then be calibrated with the input simulation source  
 1781 list using either the FEE or DEF set of beams. The resulting spectral structure in the cali-  
 1782 bration solutions purely encode the effect of the varied simulation or calibration beams.  
 1783 These calibration solutions can be directly applied to the earlier simulations containing  
 1784 the polarised grid of sources, avoiding the issue of calibration biased excess polarised  
 1785 flux. The three calibration strategies explored are described below:

1786 **SIM:FEE|CAL:FEE** – Each interferometric element in the simulation and calibration is  
 1787 identical to the FEE beam model. This case will reveal baseline beam depolarisation  
 1788 purely from the FEE beam model.

1789 **SIM:DEF|CAL:FEE** – The simulation is performed with a set of deformed beams, while the  
 1790 calibration assumes a single FEE beam model. This case probes how an incomplete un-  
 1791 derstanding of nuanced beam variations across the array can effect beam depolarisation  
 1792 after calibration.

1793 **SIM:DEF|CAL:DEF** – Both the simulation and calibration stage encode the set of deformed  
 1794 beams, implying a perfect understanding of a complex interferometric array. This case  
 1795 will reveal baseline beam depolarisation due to a varied range of beam models across  
 1796 the array.

1797 **WSClean** (Offringa et al., 2014; Offringa & Smirnov, 2017) is used to image the cali-  
 1798 brated Hyperdrive data at the simulation 320kHz frequency resolution. Primary beam  
 1799 corrected dirty images of the entire sky in stokes Q and U channels were generated  
 1800 with **WSClean** using Briggs weighting (Briggs, 1995), with `robust = -1.0` to minimize  
 1801 sidelobe confusion. Primary beam correction during the imaging stage is required to  
 1802 recover correct flux levels across the sky, and to ensure that the parallactic angle correc-  
 1803 tion mentioned in Section 5.4 is applied, ensuring stokes parameters aligned with Right  
 1804 Ascension and Declination. **WSClean** currently only uses the FEE beam model during  
 1805 primary beam correction, which can result in errors when the simulations being imaged  
 1806 were created with a set of deformed beams. Developing imaging frameworks capable of  
 1807 utilising varied beam models is currently beyond the scope of this work, but is left for  
 1808 future work.

1809 The rotation measure synthesis describes in Section 5.3 is performed with a GPU ac-  
 1810 celerated software package called CuFFS\*(Sridhar et al., 2018), resulting in 3D RM cubes  
 1811 with Faraday dispersion functions for line-of-sight across the entire sky.

## 1812 5.6. RESULTS

1813 Following the simulations described in Section 5.5, we measure the recovered polarised  
 1814 flux at the expected input RM depth and the leakage flux at the  $\phi = 0$  mode to charac-  
 1815 terise a fractional beam leakage across the sky. Each set of simulations has a HEALPix  
 1816 grid of RM sources peaking at one of 40 possible values ranging from  $-70$  to  $+70$  rad/m<sup>2</sup>,  
 1817 at intervals of 3.5 rad/m<sup>2</sup> (see Figure 5.3). RM spectra are extracted from each 3D RM  
 1818 cube at the input HEALPix grid centers, from which a fractional leakage  $\mathbb{F}$  metric can  
 1819 be calculated for each pixel:

$$1820 \mathbb{F} = \frac{1}{40} \sum_{RM:(-70:70)} \frac{\Delta \mathbb{L}_{RM=0}}{\mathbb{P}_{RM} + \Delta \mathbb{L}_{RM=0}}, \quad (5.9)$$

1820 where  $\Delta \mathbb{L}_{RM=0}$  is the flux at the  $\phi = 0$  mode in excess of a model RMSF sidelobe seen  
 1821 in Figure 5.3, and  $\mathbb{P}_{RM}$  is the peak flux at the expected input Faraday depth from the  
 1822 simulation. The 1/40 factor arises from averaging over the 40 simulations to arrive at a  
 1823 mean fractional leakage surface over a large range of RMs.

1824 Figure 5.4 displays various components of polarisation leakage of simulations de-  
 1825 scribed in Section 5.5. The first column (panels *i*, *iv*, *vii*) of Figure 5.4 displays peak  
 1826 polarised flux  $\mathbb{P}_{RM:(-70:70)}$  from various simulations. The second column (panels *ii*, *v*,  
 1827 *viii*) displays leakage flux  $\Delta \mathbb{L}_{RM=0}$ , while the final column (panels *iii*, *vi*, *ix*) shows frac-  
 1828 tional leakage  $\mathbb{F}$  calculated from Equation 5.9. Areas of the sky where the beam sensi-  
 1829 tivity drops below 0.1% have been masked due to low sensitivity resulting in numerical  
 1830 noise dominated outputs. In the absence of any errors in the beam models, calibration

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\*<https://github.com/sarrvesh/cuFFS>

and in the stokes imaging phase, we would expect the peak polarised flux our simulations to be 2.243 Jy/RMSF across the sky, given the reference flux, spectral index and fractional polarisation of the simulations. We would also ideally expect no leakage flux, resulting in a zero fractional leakage across the sky. This project aims to quantify the effect of various instrumental beams and calibration on the level and morphology of the fractional leakage plane, across the sky.

The first row (panels *i*, *ii*, *iii*) of Figure 5.4 represent the results of a set of simulations performed with the perfect FEE beam model, and calibrated with the same beam model. Given that the calibration is performed with *all* the flux in the simulation, and that the simulations were noiseless, the calibration solutions were identically one. This set of results quantifies the extent and morphology of polarisation leakage in the best case scenario, where every interferometric element is identically perfect and also perfectly represented during calibration. We observe a  $\sim 1\%$  leakage error at beam center, rising to  $\sim 5\%$  at the full width half maximum (FWHM) of the primary beam ( $\sim 22^\circ$  at 180MHz). Leakage increases to between  $\sim 5 - 30\%$  when extending outwards into regions of the primary beam sensitivity  $\geq 10\%$ . The leakage levels in the first sidelobes in regions with  $\geq 1\%$  beam sensitivity range between  $\sim 8 - 50\%$ . Any area below a 1% beam sensitivity is considered effectively depolarised with leakages exceeding  $\geq 50\%$ .

The second row (panels *iv*, *v*, *vi*) of Figure 5.4 represent the results of a set of simulations performed with the set of deformed (DEF) beam models described in Section 5.5, and calibrated with the same set of beam models. Due to identical sets of beams being utilised in both simulation and calibration, calibration solutions are identically one. Similar to the case above, this set of results quantifies the extent and morphology of polarisation leakage, in the presence of a set of perfectly characterised but unique deformed beams across an array. While the level of polarisation leakage is not drastically different to the case in the first row, the morphology of the leakage surface is significantly altered. This is most apparent by looking at the third row (panels *vii*, *viii*, *ix*) of Figure 5.4, which represent the difference between the first and second rows. In the residual leakage plot (panel *ix*), it is clear that the two cases can differ by  $\pm 3\%$  in the primary lobe. It is interesting to note that depolarisation in the simulation with the deformed beams are consistently worse by beyond  $\geq 10\%$  in first sidelobes. This intuitively makes sense since the central lobe of the primary beam is extremely well constrained, while environmental factors have been shown to preferentially effect beam sidelobes (see [Line et al., 2018](#); [Chokshi et al., 2021](#)), to varied extents and in non symmetric manners.

The results investigated in Figure 5.4 characterise polarisation leakage of either the single FEE beam, or a set of uniquely deformed (DEF) beams. It does not touch upon the effect of calibrating data with beams different than those which produced the simulations. Satellite measurements of MWA beams have revealed sidelobe variation from the FEE beam model at the  $\sim 10\%$  level ([Chokshi et al., 2021](#)). Any observation made by an interferometric array inherently encoded *all* primary beams of the array. This implies that observations by the MWA must contain imprints of the range of deformed beams which constitute the array. All current MWA calibration strategies assume a single identical beam model across the array which can lead to the introduction of spurious spectral structure into calibrated data. [Chokshi et al. \(2024\)](#) demonstrated how such a simplistic representation of the instrument during calibration can negatively effect the prospect of an Epoch of Reionisation detection. We now aim to gauge the effects of

1877 calibrating data which encodes a set of deformed (DEF) beams with a single FEE beam  
1878 model. Simulations created with the set of deformed (DEF) beams are calibrated with  
1879 either the same set of deformed beams, or a single perfect FEE beam model. Fraction  
1880 leakages surfaces are calculated for both using Equation 5.9, as in Figure 5.4, and the  
1881 difference between the two scenarios is displayed in Figure 5.5. We observe noise-like  
1882 residuals in fractional leakage between the two scenarios, yet no significant spatial struc-  
1883 ture across the sky. Least variations are observed in closer to the beam center, increasing  
1884 in regions of lower beam sensitivity. Figure 5.6 show a histogram of the residual frac-  
1885 tional leakage which shows a distinctly peaked symmetric structure centred about zero.  
1886 The histogram is well described by a Laplacian distribution with mean  $\mu = 0$  and scale  
1887 parameter  $b = 0.0027$ . This implies that calibrating data which inherently encoded a  
1888 range of deformed beams, with a single perfect beam model, can result in a noise-like  
1889 change in the fraction leakage plane at a  $\pm 0.3\%$  level. We do not observe any significant  
1890 variation of the morphology of the leakage plane, which appears to be dictated by the  
1891 various deformed beam models across the array.

## 1892 5.7. CONCLUSION

1893 This work explores the impact that imperfect and varied beams across a radio inter-  
1894 ferometer could have on low frequency polarisation science. We demonstrate how de-  
1895 formed beams across interferometric arrays can introduce complex variations to the ex-  
1896 tent and morphology of depolarisation across the sky.

1897 In-situ satellite measurements of all-sky MWA beams ([Line et al., 2018](#); [Chokshi et al.,](#)  
1898 [2021](#)) have shown significant sidelobe distortions at the  $\sim 10\%$  level. Chokshi et al.,  
1899 2024a developed a Bayesian MCMC framework to utilise satellite measurements to opti-  
1900 mally emulate measured beam deformations in the cutting-edge MWA FEE beam model  
1901 ([Sutinjo et al., 2015](#); [Sokolowski et al., 2017](#)). This enables the creation of physically mo-  
1902 tivated simulated MWA arrays with realistically deformed beam models. Adopting this  
1903 methodology, this work develops a Jones matrix based mathematical framework to ex-  
1904 plore depolarisation arising from varied beams across an interferometer in Section 5.4.  
1905 In Section 5.5 we outline our simulation methodology, which includes using subset of  
1906 the 20,000 brightest sources from the LoBES ([Lynch et al., 2021](#)) catalog in addition to a  
1907 array of 6144 synthetic polarised sources arraying in a HEALPix grid to simulate all-sky  
1908 depolarisation effects.

1909 Within the FWHM of the MWA beam ( $\sim 22^\circ$  at 180 MHz), the level of depolarisation  
1910 caused by a set of deformed beams is similar to the inherent depolarisation with the  
1911 cutting-edge FEE beam model at  $\sim 1\%$  at beam center and rising to  $\sim 5\%$  at the FWHM,  
1912 but demonstrating a different morphology. Beyond the FWHM, significant quantitative  
1913 and structural changes are observed in the depolarisation plane. Within regions of the  
1914 sidelobe with sensitivity  $\geq 1\%$ , simulations with deformed beams demonstrate  $\geq 10\%$   
1915 increases in fractional depolarisation compared to the perfect FEE beam, observed in  
1916 non-uniform patches and gradients. Our simulations also indicate that in areas of the  
1917 beam with sensitivity  $\leq 1\%$ , irrespective of beam type, polarised signal are effectively  
1918 depolarised with fractional depolarisation exceeding  $\geq 50\%$ .

1919 Any observation by an interferometer inherently encodes imprints of *all* primary beams  
1920 across the array. Given the  $\sim 10\%$  sidelobe distortions in MWA beams measured by [Chok-](#)

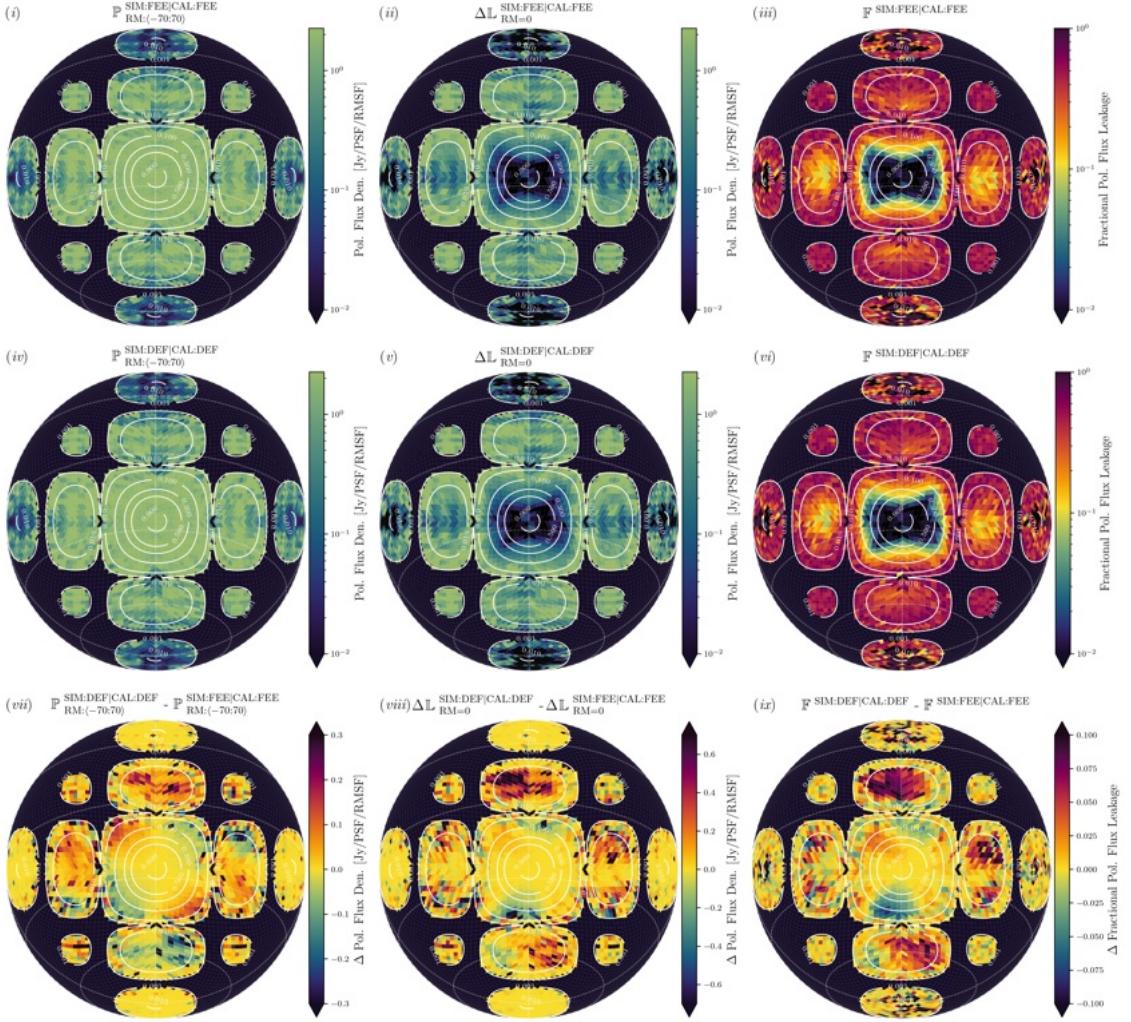


Figure 5.4: All sky maps of various components of polarisation leakage simulations described in Section 5.5. The top row (panels *i*, *ii*, *iii*) represents simulations of a HEALPix grid of polarised & calibration sources with a single perfect FEE beam, and calibrated with the same beam model. The second row (panels *iv*, *v*, *vi*) are simulations using a set of 128 unique deformed (DEF) beams, and calibrated with the same set of deformed beam models. The final row (panels *vii*, *viii*, *ix*) represents the residuals between the two corresponding panels above. The left column (panels *i*, *iv*, *vii*) represents polarised flux  $\mathbb{P}_{RM:(-70:70)}$  at the expected RM value, averaged over the set of 40 simulations. The central column (panels *ii*, *v*, *viii*) represents leakage flux  $\Delta L_{RM=0}$  at the  $\phi = 0$  Faraday depth, in excess of modeled RMSF sidelobes. The final column (panels *iii*, *vi*, *ix*) represent the fractional polarisation leakage  $F$  given by Equation 5.9, calculated from the two corresponding panels to the left. Areas of the sky where the beam sensitivity drops below 0.1% have been masked due to low sensitivity resulting in numerical noise dominated outputs and are shown in black. The white contours in each panel represent levels of zenith normalised MWA beam power.

$$\mathbb{F} \text{ SIM:DEF|CAL:DEF} - \mathbb{F} \text{ SIM:DEF|CAL:FEE}$$

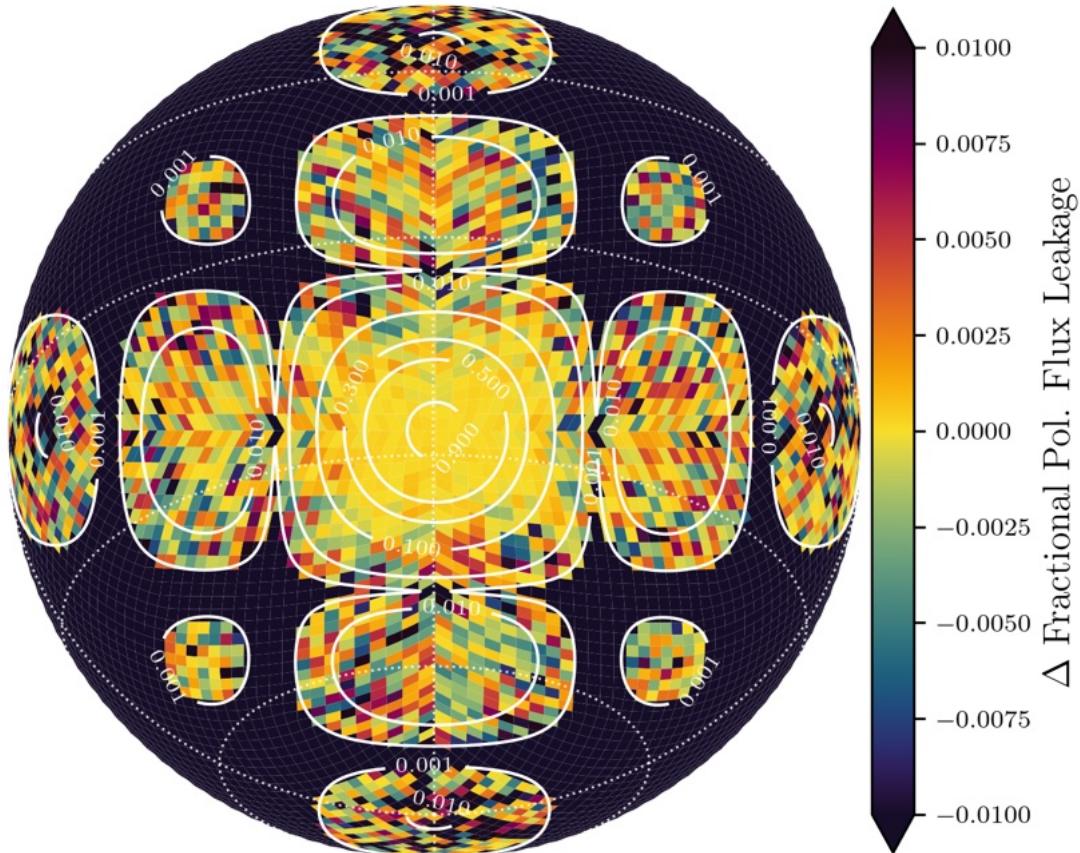


Figure 5.5: The difference between fractional polarisation leakage surfaces for two calibration scenarios. Simulations of a HEALPix grid of polarised sources a performed using a set of uniquely deformed (DEF) beams. The simulations are calibrated using either the input set of DEF beams, or a single perfect FEE beam model. Fraction polarisation leakage is calculated using Equation 5.9, and the difference between the two scenarios is plotted.

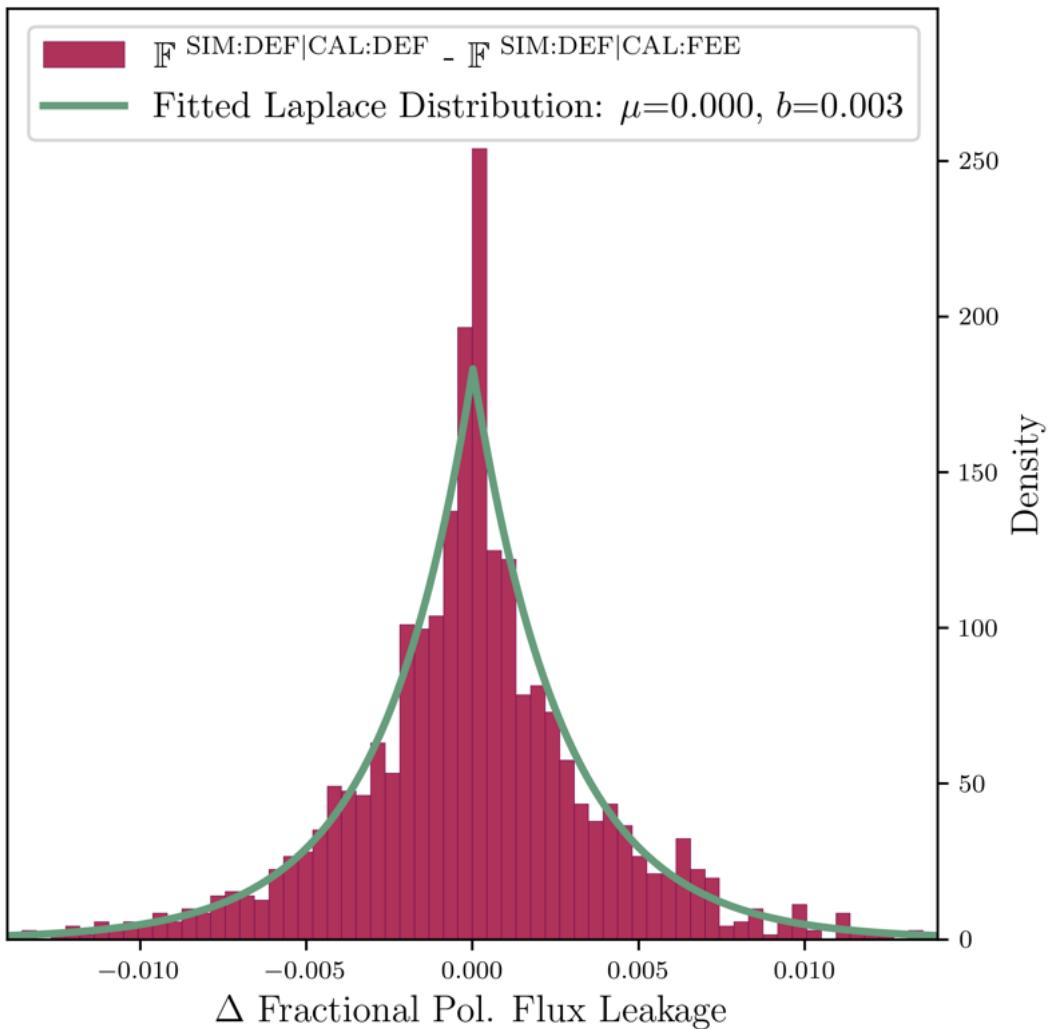


Figure 5.6: A histogram of the noise-like residuals between a set of simulations performed with a set of deformed (DEF) beams, calibrated with either the input set of DEF beams, or a single perfect FEE beam model (Figure 5.5). The histogram is well described by a Laplacian distribution with mean  $\mu = 0$ , and scale parameter  $b = 0.003$ .

shi et al. (2021), all MWA data must encode characteristics of varied beams. To recover true and unbiased sky intensities, calibration processes much account for nuanced instrumental systematics. Unfortunately *all* current MWA calibration strategies only use a single beam model which is assumed to perfectly represent every interferometric element across the array. Chokshi et al. (2024) demonstrated that this mismatch between imperfect instrumental beams, and single assumed calibration beams can lead to spurious calibration artefacts dominating an Epoch of Reionisation power spectrum detection by factors exceeding 1000. In contrast, we find that in the context of polarisation leakage, calibrating with a single beam introduces noise to the all-sky fractional depolarisation as seen in Figures 5.5 & 5.6, but does not appreciable change the extent or morphology of the depolarisation structure introduced by a set of deformed beams. This lack of change in fractional leakage morphology after calibration could potentially arise from the fact that during the imaging stage of the simulation pipeline, WSClean performs the crucial primary beam correction using a single perfect FEE beam model. This could lead to calibration effects being sub-dominant, only resulting in the excess noise observed in Figures 5.5 and 5.6.

For widefield instruments with relatively simple primary beam patterns such as the MWA, this work suggest that beam depolarisation resulting from a set of deformed beams is not an insurmountable factor within the FWHM of the primary lobe. Asymmetric variations in the fractional leakage surface show in Figure 5.4 have the potential to introduce biases to populations of observed polarised sources, where dimmer polarised sources could be sufficiently depolarised to disappear within the noise floor. More advanced survey and mosaicing strategies utilising overlapping FWHM sized patches could potentially mitigate or reduce this bias. Quantifying this bias and exploring mitigation strategies are left for future works.

As the astronomical community prepares for the commissioning of the SKA-Low observatory, we must be aware and prepared for increased instrumental complexities. With 256 dipole per station, the potential for station beams to deviate from ideal models, due to environmental factors is significantly exacerbated in comparison to a simple 16 dipole MWA tile. With the plan for multiple pseudo-random dipole layouts for SKA-Low stations, and with each being uniquely susceptible to environmental beam deformations, we expect extremely complex sidelobe structure. This will inevitably lead to high levels of sidelobe depolarisation. With the SKA-Low's narrower  $4 \times 4^\circ$  primary FoV, sensitive surveys of cosmic magnetism will be extremely slow and susceptible to population biased due to the expected complex depolarisation morphology. Simulation of the SKA-Low beam deformations are beyond the scope of this work.

We have demonstrated that deformed beams across interferometric arrays can lead to complex and unexpected depolarisation morphology across the sky. We note that direction dependant polarised calibration strategies could be particularly effective in the context of deformed interferometric beams - investigations along this line are left for future work.

*Computer spinning,  
The segfault tells me nothing,  
Goddam GPU.*

1962

Jack Line, 2024, Haiku

## CHAPTER 6

1963

1964

## Conclusions & Discussions

1965

1966     The Epoch of Reionisation represents one of the last frontiers of modern cosmology.  
1967     A crucial transformative period in our Universe's history, the EoR spans the birth of  
1968     the first luminous sources via the gravitational coalescence of primordial over-densities.  
1969     Bubbles of ionising radiation expanded into the Universe, centred around these first lu-  
1970     minous objects, heralding a phase transition of matter from neutral to the completely  
1971     ionised state we observe today. This epoch also encompassed the formation of the mor-  
1972     phologically complex and structured galaxies we observe around us today. Observing  
1973     the EoR promises to aid in the unravelling of mysteries surrounding the birth of the first  
1974     stars and galaxies, their nature, and their influence on the evolution of the Universe.  
1975     Prior to the completion of reionisation, the spin-flip 21-cm line of neutral Hydrogen acts  
1976     as a powerful tool to probe the early Universe. Tracing the morphology of reionisation,  
1977     it can be leveraged to observe large cosmological volumes (see Figure 1.2). Unfortu-  
1978     nately, a range of astrophysical and terrestrial foregrounds obscure signals from the  
1979     EoR by factors exceeding  $\sim 100,000$  (see Figure 1.5). Chapter 1 outlines the history of  
1980     the Universe, highlights the importance of the EoR and explores challenges to its de-  
1981     tection. Low-frequency radio interferometers are powerful modern telescopes designed  
1982     to achieve unprecedented angular resolution over wide fields-of-view. In Chapter 2 we  
1983     develop the mathematical tools required to understand interferometry, and discuss its  
1984     applicability to EoR searches; both in the context of a statistical detection, and for future  
1985     tomographic imaging efforts.

1986     The journey to a first validated detection of the EoR signal will necessitate a precise  
1987     understanding of our telescopes. The dominant obscuring foreground flux couples with  
1988     complex instrumental characteristics in a non-trivial manner. Precisely understanding  
1989     this coupling will be required to disentangle foreground flux from the cosmological sig-  
1990     nal five orders-of-magnitude fainter. Current measured upper-limits of the EoR 21-cm  
1991     power spectrum are still a couple of orders-of-magnitude higher than EoR models.

1992     The focus of this thesis was to explore the possibility of interferometric primary beam  
1993     models contributing to analysis systematics, and whether understanding them could im-  
1994     prove the prospects of a future EoR detection (see Appendix B for a discussion of often  
1995     overlooked nuances of primary beam models). The assumption of identical beam models  
1996     across interferometric arrays is ubiquitous as it enables massive computational simplifi-

cations via the convolution theorem. Is this a valid assumption, and if not, at what level are we introducing beam-based analysis systematics into our science? As a first step, we developed and deployed an experiment to measure the all-sky dual-polarised primary beam patterns of 14 MWA beams using communication satellites. This work was described in Chapter 3, and revealed unexpected and significant sidelobe variation at the  $\sim 10\%$  level, along with sub-degree rotations in the tiles. These inter-tile variations were primarily attributed to environmental factors; erosion of the soil under the reflective ground screens leading to their deformation, local foliage growth and infrequent animal interactions.

Our measurements showed that interferometric beams deviate from cutting-edge electromagnetic models at a significant level. An obvious next step was to explore the level at which deformed beams across interferometric arrays effect various science cases. In Chapter 4, we develop a physically motivated model of beam deformation capable of emulating beam measurements performed in Chapter 3. Using this framework, we explored the impact of deformed beams on a potential EoR power spectrum detection. We showed that assuming a single perfect beam model during calibration of data which encoded a set of deformed beams introduced foreground spectral leakage greater than the expected EoR level by factors exceeding  $\sim 1000$  between  $k = 0.1 - 1 \text{ hMpc}^{-1}$ . This spectral leakage was not appreciably reduced by the subtraction of large fractions of sky-flux models. On the other hand, including knowledge of deformed beams into calibration frameworks reduced this foreground spectral leakage to a sub-dominant effect. This could potentially put an EoR detection within grasp if we can measure instrumental beams across an entire interferometric array and include them into calibration frameworks.

Low-frequency interferometric arrays are fully polarised instruments, making measurements in all Stokes  $\{I, Q, U, V\}$  parameters. In Chapter 5, we explore the impact of deformed beams on polarisation science. The ISM and IGM plasma acts as a birefringent medium, rotating the plane of polarisation of radiation in the presence of magnetic fields. Fourier Rotation Measure (RM) synthesis is a novel technique which enables the recovery of multiple magnetic fields along lines-of-sight to polarised sources, providing a powerful probe of cosmic magnetism. Errors in the primary beam model can unfortunately introduce an effect known as “beam leakage”, where polarised signals appear depolarised. In this work, we demonstrate that the presence of deformed beams across interferometric arrays can lead to a change of this beam leakage morphology, particularly significant in beam sidelobes where leakage can be exacerbated by factors  $\geq 10\%$ . This has the potential to completely depolarise faint polarised sources, as well as bias the population of polarised surveys. This could be of particular import for the future SKA-Low observatory whose sidelobes are expected to be notoriously hard to characterise.

In the rest of this conclusion, we discuss an exploratory investigation as a motivation for future studies, followed by a outline of future investigations of interest.

## 6.1. AT WHAT LEVEL DO DEFORMED BEAMS MATTER?

In Chapter 4, we demonstrated the impact that deformed beams can have on a power spectrum EoR detection. Not including knowledge of deformed beams during calibration resulted in spectral leakage of foreground power into cosmologically sensitive modes,

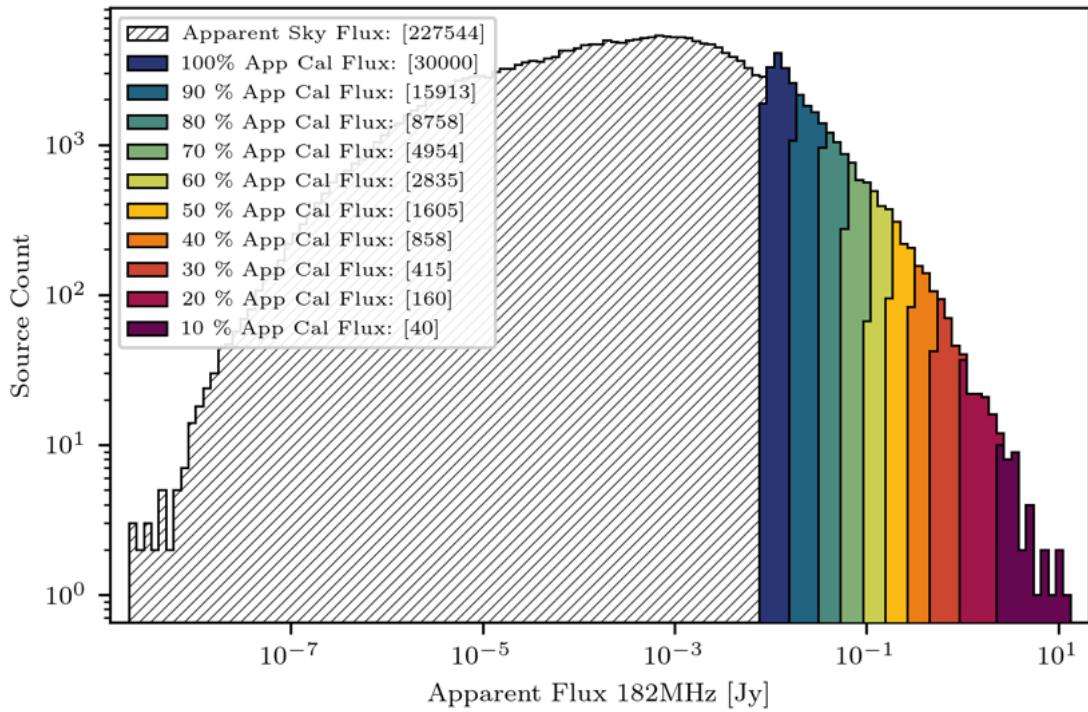


Figure 6.1: A histogram of all almost 300,000 beam-weighted foreground sources in the LoBES catalogue, with the brightest 30,000 used in Chapter 4, Figure 4.5 highlighted to the right.

at levels exceeding  $\sim 1000$  times greater than the expected EoR level. While the work in Chapter 4 demonstrated the critical need to include validated beams during calibration, it only represents a first step into such investigations due to a set of simplifying assumptions:

- The simulations were performed with the set of 30,000 brightest LoBES sources shown in Figure 4.5. Figure 6.1 shows that the selected sources represent a biased sample from the  $\sim 300,000$  available LoBES sources, which have a significant number of fainter sources.
- Calibration was performed using *all* the flux in simulations (all 30,000 sources), which clearly isolated the effects of deformed beams during calibration.
- The study was noiseless. There is no evidence that instrumental noise introduces spectral structure into calibration solutions, and thus an analysis using noise was omitted.

In reality, it is impossible to include *all* foreground flux during calibration. The hope is that by including large fractions of foreground flux during calibration, we can accurately characterise the instrumental transfer function, and undo it to reveal the true sky. To explore this we perform a set of WODEN\* simulations, mirroring those in Chapter 4, using all

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\*<https://github.com/JLBLline/WODEN>

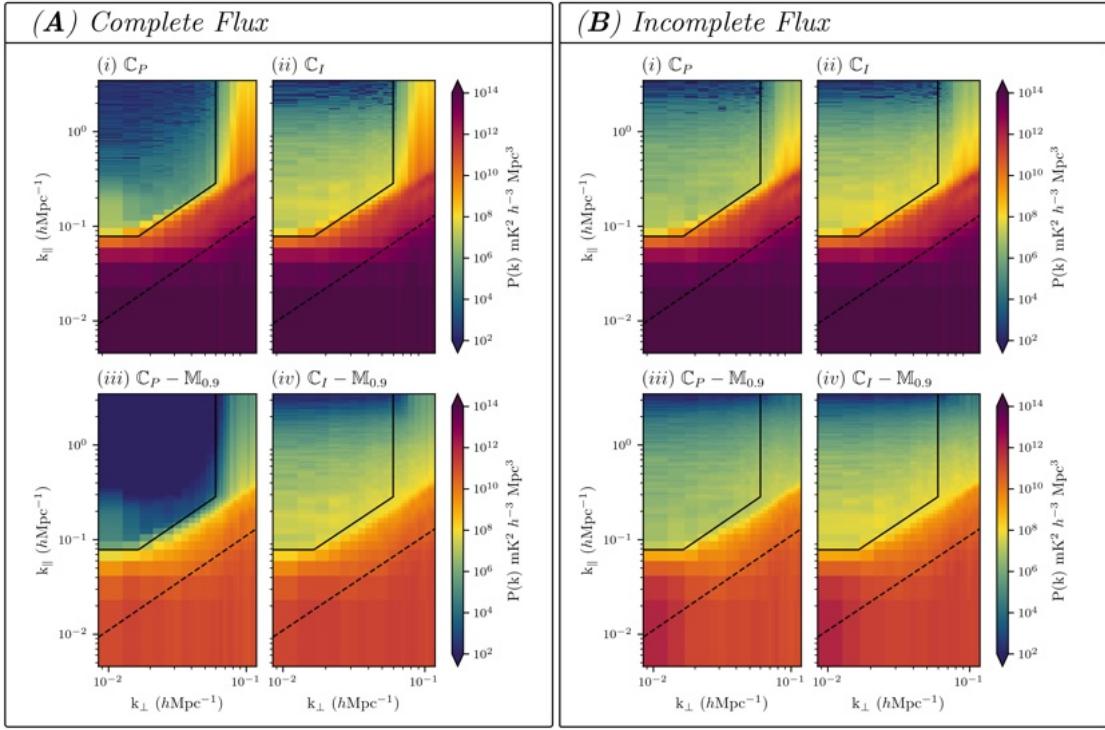


Figure 6.2: Panel (A) represents an investigation into beam models when all sky flux is included during calibration, mirroring the results of Chapter 4. Panel (B) repeats the previous exercise, with all 300,000 LoBES sources included in the sky simulation, while only the brightest 30,000 were included during calibration.

2058 300,000 LoBES foreground sources, with and without the deformed beams. Calibration  
 2059 is performed using `hyperdrive` and only the brightest 30,000 LoBES sources. Results  
 2060 are depicted in Figure 6.2, with panel (A) reproducing the case from Chapter 4 where  
 2061 all sky flux is included in calibration, and panel (B) showing when only the brightest  
 2062 30,000 sources are used during calibration of a simulation containing all 300,000 LoBES  
 2063 sources (see Figure 6.1). The striking difference is that when only a fraction of the sky  
 2064 flux is used during calibration, substantially higher leakage occurs from the foreground  
 2065 wedge to the EoR window. In this case, the calibration process is imperfect for two rea-  
 2066 sons; both the partial flux model used during calibration and the deformed beams leads  
 2067 to calibration errors.

2068 This simple test shows that foreground-flux-based errors occur at a higher level than  
 2069 beam based errors. Like Figure 1.5, where a variety of celestial and terrestrial fore-  
 2070 grounds obscure the EoR, there may be layers of calibration and instrumental errors  
 2071 which become apparent as higher-order effects are addressed. Once sky-flux-based cal-  
 2072 ibration errors are solved, deformed-beam-based errors will become a dominating con-  
 2073 tamitant, and need to be solved before an EoR detection can be made.

2074    **6.2. FUTURE DIRECTIONS**

2075    In the following section I outline ideas which will extend the work presented in this  
2076    thesis.

2077    **6.2.1. Calibrating real data with measured MWA beam models**

2078    In Chapter 4, we demonstrated that including measured models of MWA beams into  
2079    calibration frameworks has the potential to improve foreground spectral leakage into  
2080    the EoR window by factors greater than  $\sim 1000$  using simulations. The obvious pressing  
2081    question is how we apply this to data, and whether the results will be as significant as  
2082    the simulations predicted. Below are steps which could make this a reality.

2083    *All-sky satellite beam measurements across the MWA*

2084    We currently only possess measurements of 14 MWA beam models, measured in 2020 by  
2085    Chokshi et al. (2021). At minimum we require measurements of the 128 compact Phase II  
2086    MWA tiles (sensitive to the EoR), and hopefully all 256 Phase III tiles. Scaling the original  
2087    satellite beam measurement (Chokshi et al., 2021) experiment from 14 to 256 will not be  
2088    feasible without at minimum a redesign of the hardware used.

2089    It is impractical to have a pair of RF Explorer Spectrum Analysers<sup>\*</sup> per polarised MWA  
2090    tile, with many Raspberry Pis<sup>†</sup> running the capture software. One path forward would  
2091    be to engineer a set of receiver boards which could channelise raw MWA tile power, all  
2092    of which could be controlled by a single board computer installed into MWA receiver  
2093    boxes. This system is non-ideal since it is extremely invasive to the telescope, requiring  
2094    the installation of new hardware into the signal chain of each MWA tile. Any failure in  
2095    this hardware could lead to the degradation or the complete loss of MWA data.

2096    An alternate avenue would be to emulate a passive observing strategy developed by  
2097    Sokolowski et al. (2024), leveraging the new MWAX correlator (Morrison et al., 2023).  
2098    By re-channelising current MWA observations using the commensal MWAX observa-  
2099    tion mode, we may be able to capture raw voltages from tiles to generate satellite beam  
2100    models of *all* tiles, without the necessity of signal-chain interruptions. The drawback  
2101    of this method is that we could only observe at the frequencies of the original MWA  
2102    observation schedule, which would reduce the time spent in the 138 MHz band where  
2103    bright communication satellites are active. This would result in a reduced beam mapping  
2104    efficiency.

2105    *Hybrid drone-satellite framework*

2106    The nature of satellite beam mapping experiments is that they are inherently narrow-  
2107    band, in comparison to the MWA's 30.72 MHz instantaneous bandwidth. The beam  
2108    deformation model developed in Chapter 4 assumed that the 16 beam deformation pa-  
2109    rameters did not change with frequency. Using a test MWA tile, it may be possible  
2110    to investigate the chromatic scaling of these deformation parameters across the MWA

---

\*<http://rfexplorer.com>

†<https://www.raspberrypi.org>

band, using a drone mounted broadband transmitter. If an empirical scaling relation can be developed, it could be applied to measured narrow-band satellite maps.

#### 2113 *Temporal evolution of beam deformation*

2114 Finally, the beam deformations measured in Chapter 4 were primarily attributed to environmental factors — erosion of soil below the ground screen, foliage growth around and in the tile, and interaction with animals on site. These are not static, and could potentially change slowly between observing seasons. Long term beam monitoring experiments will be needed to understand the temporal variation and scale of beam deformation. It may be challenging or impossible to apply current measured deformed beams to archival data. In the worst case scenario, we may need to re-observe EoR data and calibrate it with a set of matched beam measurements.

#### 2122 *6.2.2. A rising Galactic plane and deformed beams*

2123 The MWA beam is sensitive to the entire visible sky (horizon-to-horizon) as seen in Figure 2.5. Measurements of MWA beams have revealed that the largest variations from cutting-edge beam models occur away from the zenith, and are worst along the horizon. The MWA EoR observing fields are chosen to be centred around the quietest patches of the sky with least foreground emission. Unfortunately, even with this careful selection of observing fields, the Galactic plane is unavoidably rising on the horizon (see Figure 2.5). [Barry et al. \(2024\)](#) demonstrated that the presence of the Galactic plane on the horizon could introduce foreground contamination at a level  $\sim 20$  times higher than the EoR power, when the MWA beams were identically perfect.

2132 It would be pertinent to explore how the extremely bright Galactic plane on the horizon couples with a simulated MWA array composed of a set of deformed beams (like those developed in Chapter 4). We could also explore calibration strategies which could mitigate these effects.

#### 2136 *6.2.3. Dead dipoles and the SKA-Low*

2137 In its Phase I or II configuration, the MWA is composed of 2048 ( $128 \text{ tiles} \times 16 \text{ dipoles}$  per tile) identical dual-polarisation dipoles. Dipoles occasionally experience failures in their LNAs, or in the connections to the analogue beamformer. These are primarily due to environmental factors such as the slightly acidic soil at the MRO degrading the LNAs and lightning strikes. Figure 6.3 shows the percentage of MWA tiles with either one or two flagged dipoles, between 2013 and 2019. At any time between  $\sim 15 - 35\%$  of MWA tiles have at least one non-functional dipole. [Joseph et al. \(2019\)](#) demonstrated that the unaccounted presence of these non-functional dipoles resulted in calibration-based power spectrum errors at the  $\sim 10^3 \text{mk}^2 \text{h}^{-3} \text{Mpc}^3$  level.

2146 The current design of the SKA-Low telescope has a total of 131,072 dipoles ( $512 \text{ stations} \times 256 \text{ dipoles per station}$ ). This represents a staggering increase in the number of dipoles, and a proportional increase in their potential for failure. It would be interesting to quantify the effect of various levels of dipole failure on the SKA-Low's potential for making an EoR detection. This is likely to be a real problem that the SKA-Low obser-

2151 vatory will struggle with — the sheer human resources required to keep it in perfect  
2152 operating condition could be infeasible.

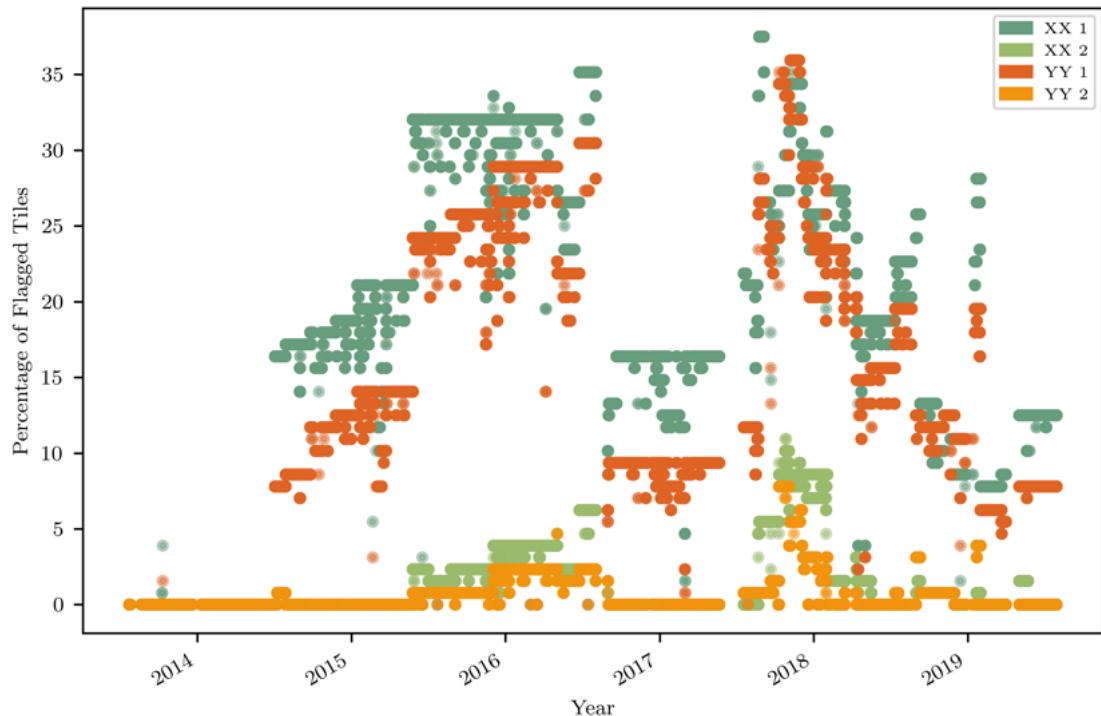


Figure 6.3: The percentage of MWA tiles with either one or two dead dipoles, for each polarisation, between 2013 and 2019. The dark green and dark orange are the percentage of tiles with one XX (East-West) and YY (North-South) dipole flagged respectively. The lighter green and orange represent the fraction of tiles with two dipoles flagged.

### 2153 6.3. FINAL THOUGHTS

2154 The field of 21-cm cosmology is poised to be revolutionised with the arrival of the SKA-  
2155 Low observatory, which promises to deliver tomographic images of the Epoch of Reion-  
2156 isation. The first stations are currently being constructed at *Inyarrimanka Ilgari Bundara*,  
2157 our Murchison Radio-astronomy Observatory, with an expected completion within the  
2158 next 5 years. It is my hope that some of the lessons learnt over the course of this thesis,  
2159 particularly regarding the complexity of modeling beams, will be valuable in enabling  
2160 the best science with next-generation telescopes.

## APPENDIX A

2161

2162

### Beam Depolarisation & Stokes Parameters

2163

2164 This sections build upon the mathematical theory presented in Section 5.4. We pick up  
2165 by substituting Eqn. 5.8 in Eqn. 5.7, and writing the full form of  $\mathbf{J} = \mathbf{J}_A \otimes \mathbf{J}_B^*$ :

$$\begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 0 & 1 & i \\ 0 & 0 & 1 & -i \\ 1 & -1 & 0 & 0 \end{bmatrix} \begin{bmatrix} I' \\ Q' \\ U' \\ V' \end{bmatrix} = \begin{bmatrix} G_{Ax}G_{Bx}^* & G_{Ax}l_{Bx}^* & l_{Ax}G_{Bx}^* & l_{Ax}l_{Bx}^* \\ -G_{Ax}l_{By}^* & G_{Ax}G_{By}^* & -l_{Ax}l_{By}^* & l_{Ax}G_{By}^* \\ -l_{Ay}G_{Bx}^* & -l_{Ay}l_{Bx}^* & G_{Ay}G_{Bx}^* & G_{Ay}l_{Bx}^* \\ l_{Ay}l_{By}^* & -l_{Ay}G_{By}^* & -G_{Ay}l_{By}^* & G_{Ay}G_{By}^* \end{bmatrix} \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 0 & 1 & i \\ 0 & 0 & 1 & -i \\ 1 & -1 & 0 & 0 \end{bmatrix} \begin{bmatrix} I \\ Q \\ U \\ V \end{bmatrix}.$$

2166 Expanding and rearranging, we obtain expressions for the observed Stokes fluxes  $I'$ ,  $Q'$ ,  
2167  $U'$  &  $V'$ , given antennas with feed Jones matrices  $\mathbf{J}_A$  &  $\mathbf{J}_B$  and source Stokes fluxes  $I$ ,  $Q$ ,  
2168  $U$  &  $V$ .

$$I' = \frac{1}{2}[(G_{Ax}G_{Bx}^* + l_{Ax}l_{Bx}^* + l_{Ay}l_{By}^* + G_{Ay}G_{By}^*)I + (G_{Ax}G_{Bx}^* - l_{Ax}l_{Bx}^* + l_{Ay}l_{By}^* - G_{Ay}G_{By}^*)Q + (G_{Ax}l_{Bx}^* + l_{Ax}G_{Bx}^* - l_{Ay}G_{By}^* - G_{Ay}l_{By}^*)U + (iG_{Ax}l_{Bx}^* - il_{Ax}G_{Bx}^* - il_{Ay}G_{By}^* + iG_{Ay}l_{By}^*)V] \quad (A.1)$$

$$Q' = \frac{1}{2}[(G_{Ax}G_{Bx}^* + l_{Ax}l_{Bx}^* - l_{Ay}l_{By}^* - G_{Ay}G_{By}^*)I + (G_{Ax}G_{Bx}^* - l_{Ax}l_{Bx}^* - l_{Ay}l_{By}^* + G_{Ay}G_{By}^*)Q + (G_{Ax}l_{Bx}^* + l_{Ax}G_{Bx}^* + l_{Ay}G_{By}^* + G_{Ay}l_{By}^*)U + (iG_{Ax}l_{Bx}^* - il_{Ax}G_{Bx}^* + il_{Ay}G_{By}^* - iG_{Ay}l_{By}^*)V] \quad (A.2)$$

$$U' = \frac{1}{2}[(-G_{Ax}l_{By}^* + l_{Ax}G_{By}^* - l_{Ay}G_{Bx}^* + G_{Ay}l_{Bx}^*)I + (-G_{Ax}l_{By}^* - l_{Ax}G_{By}^* - l_{Ay}G_{Bx}^* - G_{Ay}l_{Bx}^*)Q + (G_{Ax}G_{By}^* - l_{Ax}l_{By}^* - l_{Ay}l_{Bx}^* + G_{Ay}G_{Bx}^*)U + (iG_{Ax}G_{By}^* + il_{Ax}l_{By}^* - il_{Ay}l_{Bx}^* - iG_{Ay}G_{Bx}^*)V] \quad (A.3)$$

$$V' = \frac{-i}{2}[(-G_{Ax}l_{By}^* + l_{Ax}G_{By}^* + l_{Ay}G_{Bx}^* - G_{Ay}l_{Bx}^*)I + (-G_{Ax}l_{By}^* - l_{Ax}G_{By}^* + l_{Ay}G_{Bx}^* + G_{Ay}l_{Bx}^*)Q + (G_{Ax}G_{By}^* - l_{Ax}l_{By}^* + l_{Ay}l_{Bx}^* - G_{Ay}G_{Bx}^*)U + (iG_{Ax}G_{By}^* + il_{Ax}l_{By}^* + il_{Ay}l_{Bx}^* + iG_{Ay}G_{Bx}^*)V] \quad (A.4)$$

2170

## APPENDIX B

2171

2172

2173

### Musings on beam models

2174

2175 In a perfect world, a beam model of any receiving element perfectly reproduces the  
 2176 variation of sensitivity across the sky at all frequencies of interest. The phased-array  
 2177 receiving elements of the MWA are constructed from a set of simple dipoles which are  
 2178 coherently summed. This can be described by an array factor, AF,

$$AF = \sum_{n=1}^N w_n \exp[i(k_x x_n + k_y y_n)], \quad (B.1)$$

2179 where  $w_n$  is a complex weight applied to each dipole,  $x_n, y_n$  are Cartesian coordinates  
 2180 of dipole  $n$  from the centre of the tile, otherwise known as the the instrument frame.  
 2181 Directional cosines  $k_x, k_y$  are defined in spherical coordinates as:

$$\begin{aligned} k_x &= \frac{2\pi}{\lambda} \sin \theta \sin \phi, \\ k_y &= \frac{2\pi}{\lambda} \sin \theta \cos \phi, \end{aligned} \quad (B.2)$$

2182 where  $\theta, \phi$  are zenith angle and azimuth respectively. Multiplying the Array Factor by  
 2183 the response of a single dipole on a ground screen results in an analytic representation  
 2184 of the full MWA tile (described by [Balanis, 2016](#)):

$$B_{\text{MWA}} = AF \times B_{\text{dipole}}, \quad (B.3)$$

2185 where  $B_{\text{MWA}}$  is the beam response of the phased-array MWA tile,  $AF$  is the array factor,  
 2186 and the beam response of a single, simple dipole on a ground screen  $B_{\text{dipole}}$  is typically  
 2187 well characterised, and varies smoothly with frequency. For a regular array of dipoles,  
 2188 such as in the MWA, the array factor can have a strong frequency dependence, leading  
 2189 to a highly chromatic beam model.

2190 The physical reality of a closely packed array of dipoles is that they interact with  
 2191 each other in a non-trivial manner, leading to a deviation from the simple analytic beam  
 2192 model described in Equation B.3. Signals reflected off one dipole can be absorbed by a  
 2193 neighbouring one, and potentially even fractionally re-transmitted - an effect known as  
 2194 mutual coupling. Further, signals reflected off one dipole, can be received by orthogo-

nally polarised dipole, leading to polarisation leakage. Mutual coupling can also introduce frequency dependent effects when resonances in couplings between dipoles occur at particular frequencies.

The cutting-edge Fully-Embedded-Element (FEE) MWA beam model was generated with numerical electromagnetic simulations (Sokolowski et al., 2017; Sutinjo et al., 2015). These simulations are computationally expensive and were only performed at a 1.28 MHz frequency resolution over the MWA band. Any line-of-sight on the sky thus experiences a step-response as a function of frequency. Figure B.1 shows the response of once cross-sectional slice (azimuth=0, zenith angle={0 : 90°}) of the FEE beam model, across the MWA high-band (167 – 197 MHz). In the upper left panel we observe the simulation frequency discontinuity as a noticeable vertical banding. To gauge the spectral structure encoded by the beam model, we perform a Fourier transform across frequency. This decomposes the beam power as a function of delay modes and is shown in the upper right panel of Figure B.1, with the sharp vertical aliasing arising from the 1.28 MHz frequency resolution. Daniel Ung\* has developed a frequency interpolated MWA beam model, which has a much smoother chromatic response. The bottom panels of Figure B.1 repeat the analysis in the upper panels, using the frequency interpolated FEE beam model. The vertical banding and delay aliasing has now been suppressed by the smoother frequency response.

The impact of the non-continuous frequency response of the original FEE beam model is best observed in 2D power spectrum space. We perform a hyperdrive (Jordan et al., submitted) simulation of 30,000 foreground sources from the LoBES catalogue (Lynch et al., 2021) with both the the FEE and the interpolated FEE beam model, with power spectrum estimation performed using CHIPS(Trott et al., 2016). The results of the simulations are shown in Figure B.2, with clear coarse-band harmonics appearing horizontally in the simulations of the FEE model (panel (i)), which are absent in the simulations using the interpolated FEE model (panel (ii)). These simulations demonstrate the necessity of instrumental primary beams with smooth frequency variation, and crucially, instrumental beam models of high fidelity, which capture all actual frequency characteristics.

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\*<https://www.researchgate.net/profile/Daniel-Ung-2>

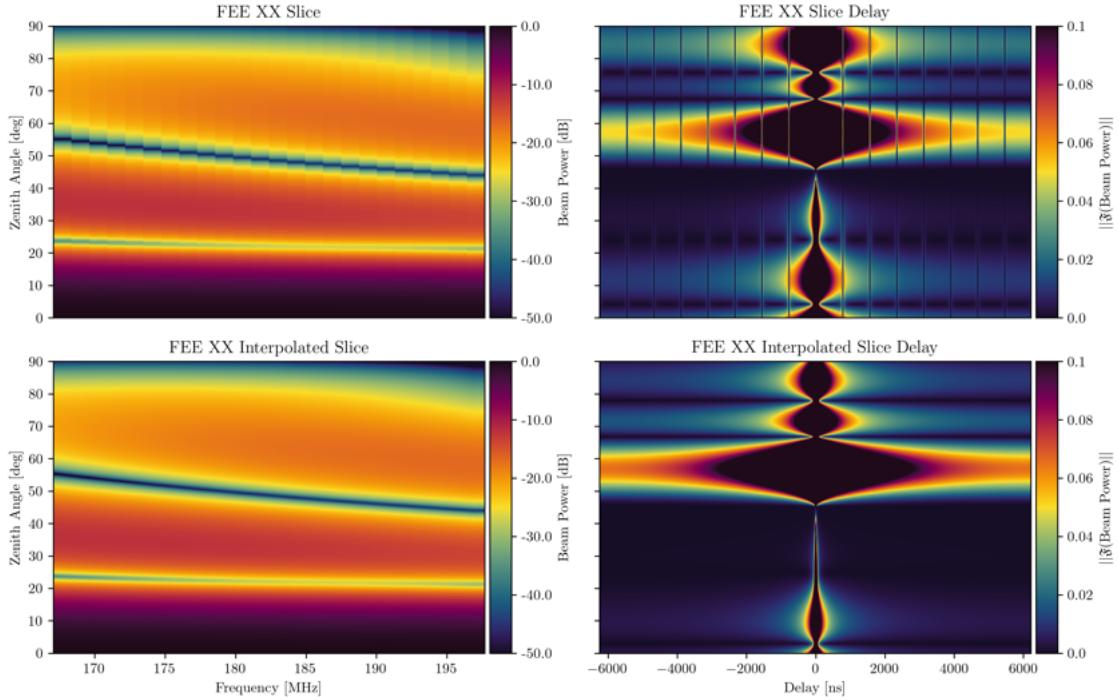


Figure B.1: An investigation into the frequency structure in the FEE beam model. A slice (along azimuth=0, zenith angle={0 : 90°}) of the X (East-West) polarisation of the FEE beam response in the MWA high band (167 – 197 MHz). The upper left panel shows beam power of the FEE model as a function of frequency, displaying marked vertical banding from the 1.28 MHz resolution. The upper right panel shows the delay transformation of beam power, with sharp vertical aliasing arising from the frequency resolution. The two lower panels repeat the analysis of the upper panels with a frequency interpolated FEE beam model, displaying a much smoother frequency structure.

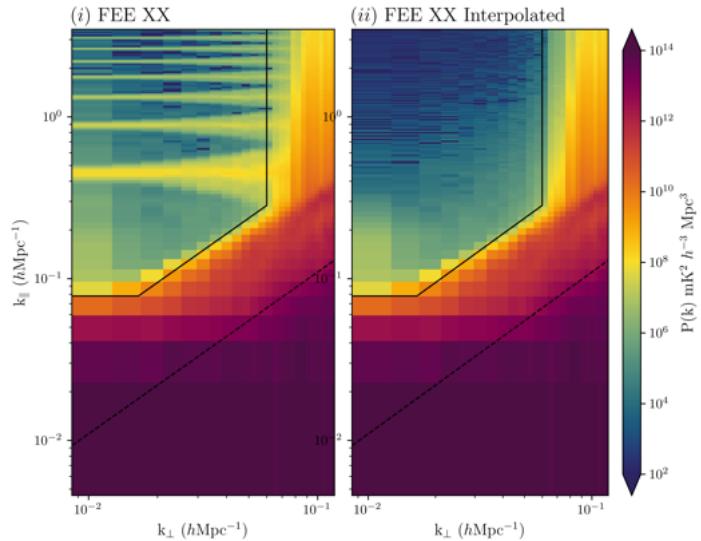


Figure B.2: A power spectrum analysis of 30000 LoBES sources using the FEE model (panel (i)), and the interpolated FEE model (panel (ii)), where XX represents East-West oriented dipoles. Clear coarse-band harmonics are visible in the simulation with the FEE beam model due to the 1.28 MHz frequency resolution.

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