

# Computer Graphics I

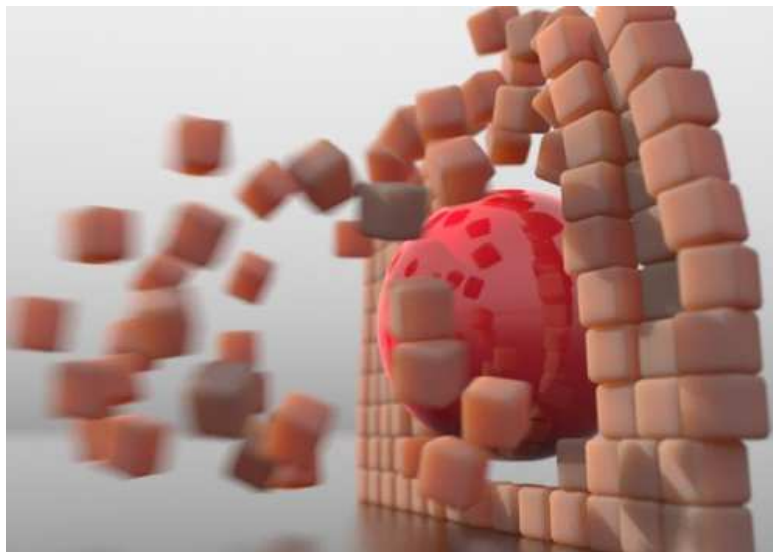
## Lecture 18: Computer animation 2

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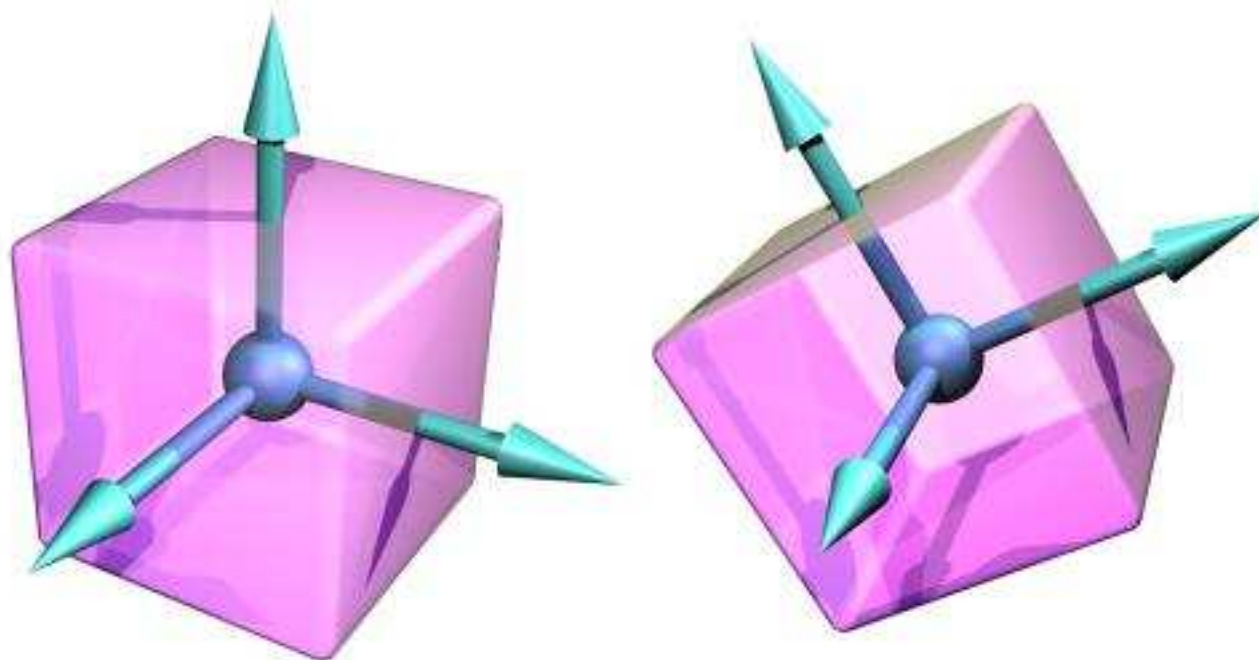
# Rigid body

- **What is a rigid body?**
  - The body never deforms nonlinearly (ideal)
  - The distance between any two given points of a rigid body remains constant in time regardless of any external forces



# Rigid body motion

- **Motion due to external forces**
  - Translation
  - Rotation



# **1. Rigid body**

# Particle system

- **Description of particle state**
  - Each particle is described by position and velocity

$$\mathbf{Y}(t) = \begin{pmatrix} x(t) \\ v(t) \end{pmatrix}$$

- For a particle system with n particles

$$\mathbf{Y}(t) = \begin{pmatrix} x_1(t) \\ v_1(t) \\ \vdots \\ x_n(t) \\ v_n(t) \end{pmatrix}$$

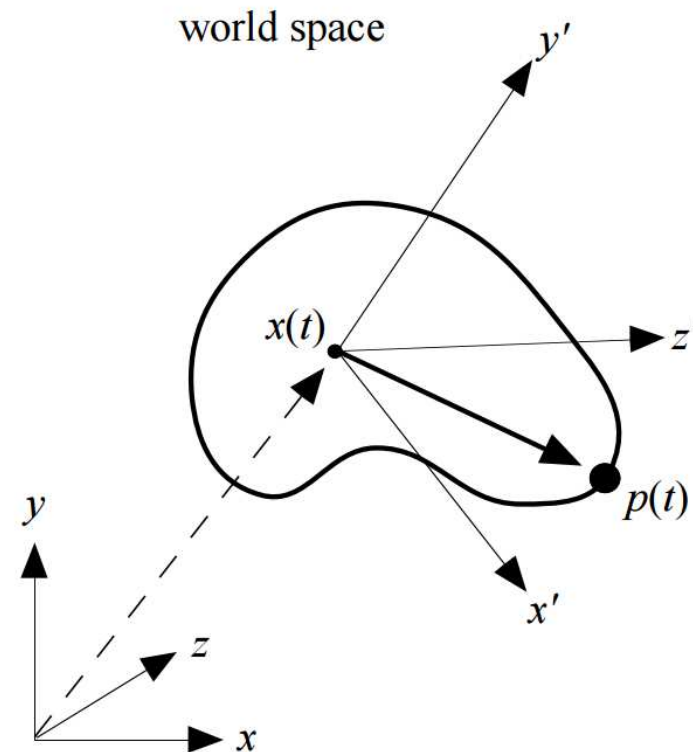
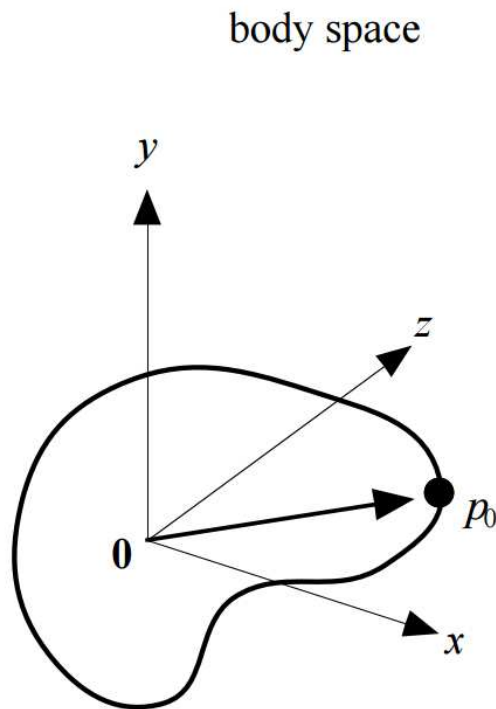
# Particle system

- **Dynamic system of particles**
  - For each particle
    - A force  $\mathbf{F}(t)$  acting on it
    - A mass  $m$  associated with it
  - Dynamic equation by ordinary differential equations

$$\frac{d}{dt}\mathbf{Y}(t) = \frac{d}{dt} \begin{pmatrix} x(t) \\ v(t) \end{pmatrix} = \begin{pmatrix} v(t) \\ F(t)/m \end{pmatrix}$$

# Position and orientation

- **World space and body space**
  - World space: a global space which does not change
  - Body space: a space relative to the body; the coordinate frame can be translated and rotated

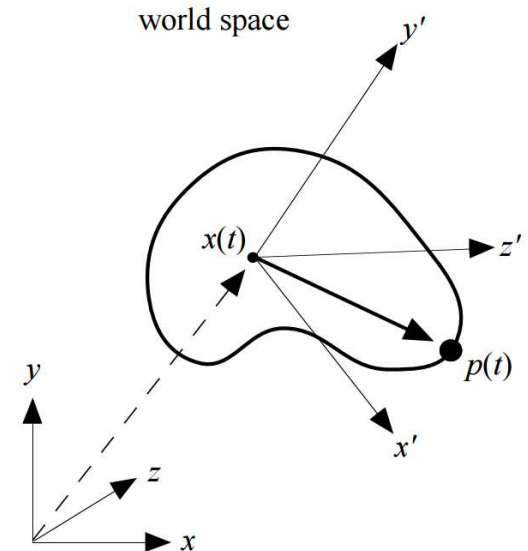
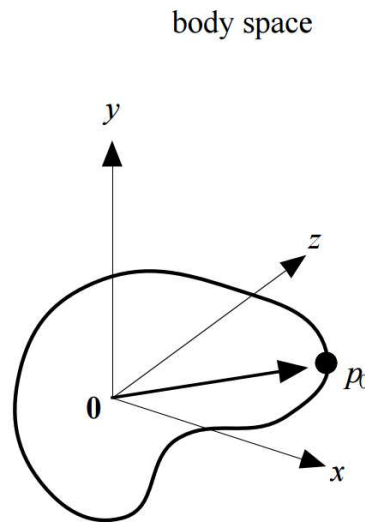


# Position and orientation

- **Connection between body space and world space**
  - Body space origin is usually defined at the center of mass
  - Transformation between body space and world space:

$$p(t) = R(t)p_0 + x(t)$$

We call  $x(t)$  and  $R(t)$  the position and orientation of the body





# Linear & angular velocity

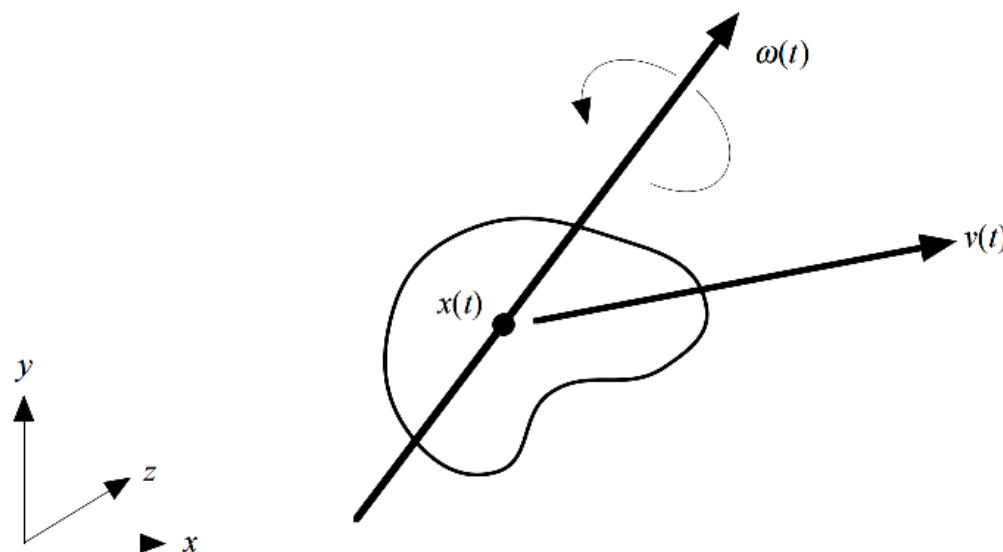
- **Definition of linear velocity**

- The linear velocity  $v(t)$

$$v(t) = \dot{x}(t)$$

- **Definition of an angular velocity**

- An axis the body rotates about
- The speed of the rotation



# Calculation of rotation

- **Given  $r(t)$  in world coordinates**

- Decomposition of  $r(t)$

$$r(t) = a + b$$

- Instant velocity

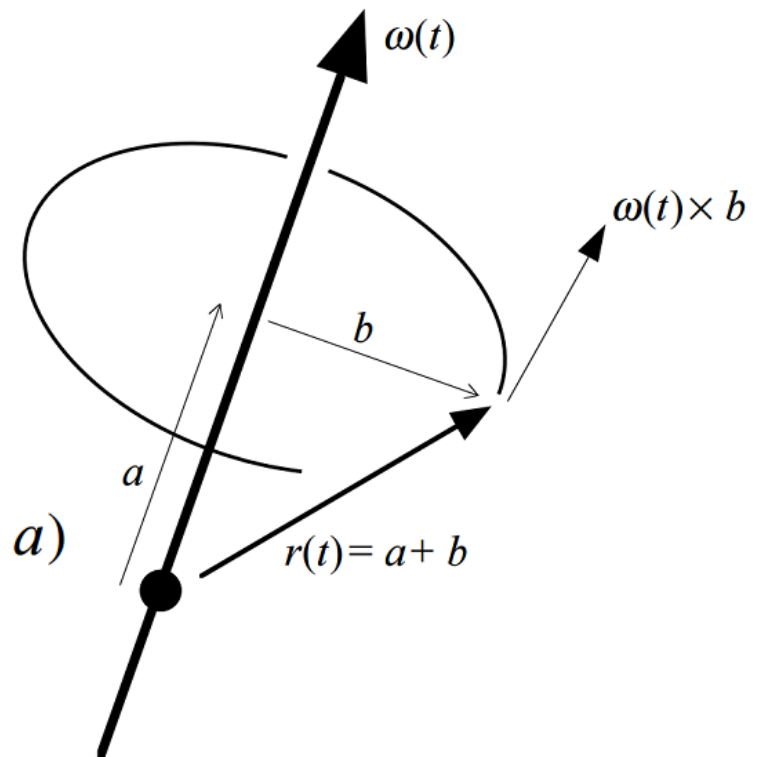
$$v(t) = \omega(t) \times b$$



$$\dot{r}(t) = \omega(t) \times b = \omega(t) \times b + \omega(t) \times a = \omega(t) \times (b + a)$$



$$\dot{r}(t) = \omega(t) \times r(t)$$

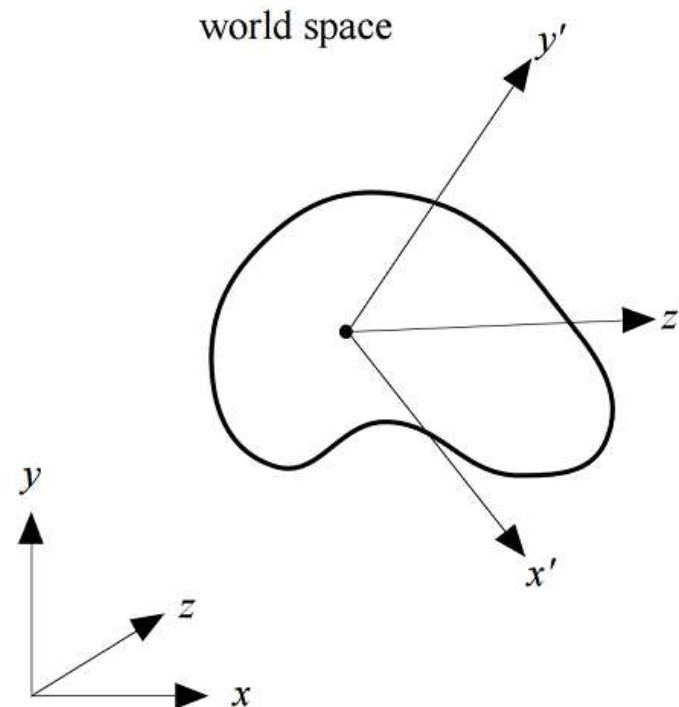


# Calculation of rotation

- Rotating a body coordinate frame

$$R(t) = \begin{pmatrix} r_{xx} & r_{yx} & r_{zx} \\ r_{xy} & r_{yy} & r_{zy} \\ r_{xz} & r_{yz} & r_{zz} \end{pmatrix} \rightarrow R(t) \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} r_{xx} \\ r_{xy} \\ r_{xz} \end{pmatrix}$$

$$R(t) = [x' \ y' \ z']$$



# Calculation of rotation

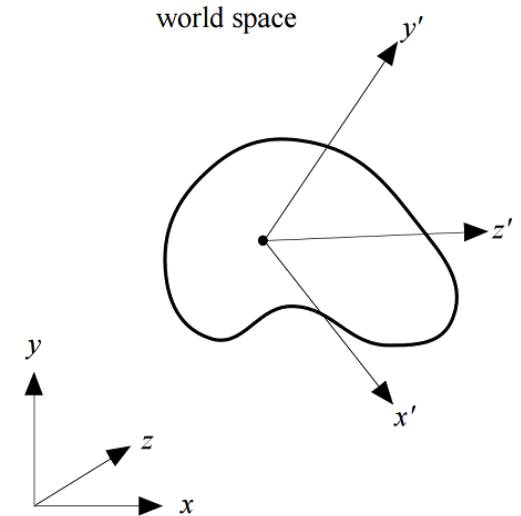
- Apply the angular velocity to the body frame after rotation

$$\dot{r}(t) = \omega(t) \times r(t)$$

$$\dot{R} = \left( \omega(t) \times \begin{pmatrix} r_{xx} \\ r_{xy} \\ r_{xz} \end{pmatrix} \quad \omega(t) \times \begin{pmatrix} r_{yx} \\ r_{yy} \\ r_{yz} \end{pmatrix} \quad \omega(t) \times \begin{pmatrix} r_{zx} \\ r_{zy} \\ r_{zz} \end{pmatrix} \right)$$

$$a^*b = \begin{pmatrix} 0 & -a_z & a_y \\ a_z & 0 & -a_x \\ -a_y & a_x & 0 \end{pmatrix} \begin{pmatrix} b_x \\ b_y \\ b_z \end{pmatrix} = \begin{pmatrix} a_y b_z - b_y a_z \\ -a_x b_z + b_x a_z \\ a_x b_y - b_x a_y \end{pmatrix} = a \times b$$

$$\dot{R}(t) = \omega(t)^* \left( \begin{pmatrix} r_{xx} \\ r_{xy} \\ r_{xz} \end{pmatrix} \quad \begin{pmatrix} r_{yx} \\ r_{yy} \\ r_{yz} \end{pmatrix} \quad \begin{pmatrix} r_{zx} \\ r_{zy} \\ r_{zz} \end{pmatrix} \right) \longrightarrow \dot{R}(t) = \omega(t)^* R(t)$$



# Mass of a body

- **Particle assumption**

- Imagine that a rigid body is made up of a large number of small particles
- The location of the  $i$ -th particle in world space at time  $t$ :

$$r_i(t) = R(t)r_{0i} + x(t)$$

- The total mass of the body,  $M$ , is the sum

$$M = \sum_{i=1}^N m_i$$

# Center of mass

- **The center of mass in a body**

- In world space (definition)

$$\frac{\sum m_i r_i(t)}{M}$$

- In body space

$$\frac{\sum m_i r_{0i}}{M} = \mathbf{0} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

# Center of mass

- **$x(t)$  as being the location of the center of mass?**
  - Yes

$$\frac{\sum m_i r_i(t)}{M} = \frac{\sum m_i (R(t)r_{0i} + x(t))}{M} = \frac{R(t) \sum m_i r_{0i} + \sum m_i x(t)}{M} = x(t) \frac{\sum m_i}{M} = x(t)$$

$$\sum m_i (r_i(t) - x(t)) = \sum m_i (R(t)r_{0i} + x(t) - x(t)) = R(t) \sum m_i r_{0i} = \mathbf{0}$$

# Velocity of a particle

- The velocity of the i-th particle

$$r_i(t) = R(t)r_{0i} + x(t)$$

$$\dot{R}(t) = \omega(t)^* R(t) \quad \xrightarrow{\text{differentiation}} \quad \dot{r}_i(t) = \omega^* R(t)r_{0i} + v(t)$$

$$v(t) = \dot{x}(t)$$

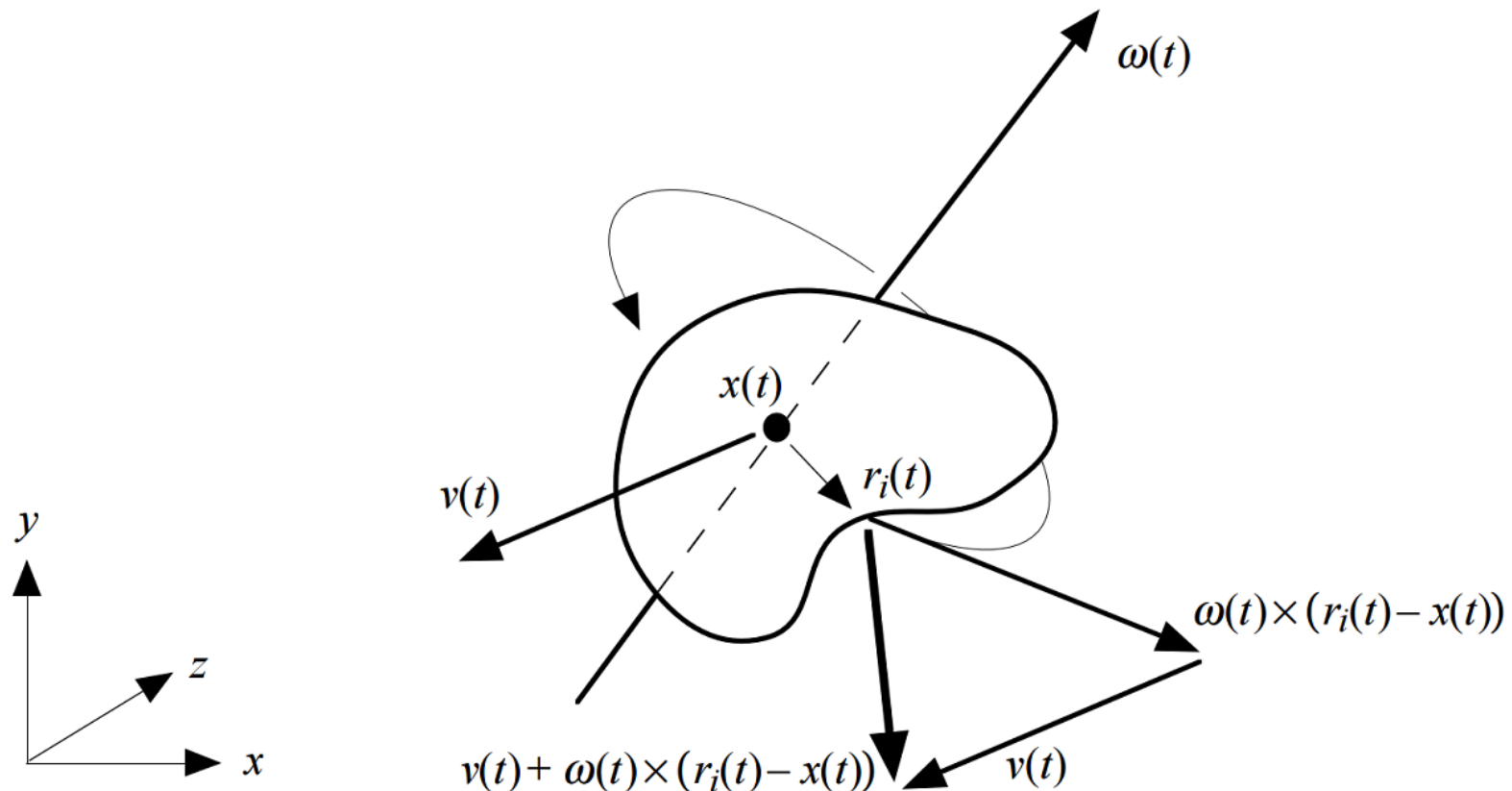
$$\begin{aligned} \dot{r}_i(t) &= \omega(t)^* R(t)r_{0i} + v(t) \\ &= \omega(t)^* (R(t)r_{0i} + x(t) - x(t)) + v(t) \\ &= \omega(t)^* (r_i(t) - x(t)) + v(t) \end{aligned}$$

$$\dot{r}_i(t) = \omega(t) \times (r_i(t) - x(t)) + v(t)$$



# Velocity of a particle

- **Illustration of particle velocity**
  - The velocity can be decomposed into a linear term and an angular



# Force and torque

- **At each particle**

- A force  $F_i(t)$  may be exerted on it
- A torque may be generated due to  $F_i(t)$

$$\tau_i(t) = (r_i(t) - x(t)) \times F_i(t)$$

- **For the whole body**

- Total force

$$F(t) = \sum F_i(t)$$

- Total torque

$$\tau(t) = \sum \tau_i(t) = \sum (r_i(t) - x(t)) \times F_i(t)$$

# Linear momentum

- **The linear momentum  $p$  of a particle**

- Defined with mass  $m$  and velocity  $v$

$$p = mv$$

- **The total linear momentum  $P(t)$**

- The sum of the products of the mass and velocity of each particle

$$\dot{r}_i(t) = \omega(t) \times (r_i(t) - x(t)) + v(t)$$

$$P(t) = \sum m_i \dot{r}_i(t)$$

$$= \sum \left( m_i v(t) + m_i \omega(t) \times (r_i(t) - x(t)) \right) \quad \sum m_i (r_i(t) - x(t)) = 0$$

$$= \sum m_i v(t) + \omega(t) \times \sum m_i (r_i(t) - x(t))$$



$$P(t) = \sum m_i v(t) = \left( \sum m_i \right) v(t) = Mv(t)$$

# Linear momentum

- **Linear momentum is irrespective of rotation of the body**

- Linear acceleration

$$\dot{v}(t) = \frac{\dot{P}(t)}{M}$$

- Relation to total force

$$\dot{P}(t) = F(t) \quad \dot{v}(t) = \frac{F(t)}{M}$$

# Angular momentum

- **Why consider angular momentum?**

- Conserved unless there is external torque
- Let you write simpler equations

- **Analogous to linear momentum**

- Linear momentum

$$P(t) = Mv(t)$$

- Angular momentum

$$L(t) = I(t)\omega(t)$$

Inertia tensor: 3x3 matrix



- Relationship between angular momentum and the total torque

$$\dot{L}(t) = \tau(t)$$

Analogous to linear  
momentum relation:

$$\dot{P}(t) = F(t)$$

# Inertia tensor

- **Intrinsic property of a body**

- Determines the torque needed for a desired angular acceleration
- Depends on the body's mass distribution and the axis chosen

- **Definition by discrete particles**

- Let  $r'_i$  be the displacement of the  $i$ -th particle from  $x(t)$

$$I(t) = \sum \begin{pmatrix} m_i(r_{iy}'^2 + r_{iz}'^2) & -m_i r'_{ix} r'_{iy} & -m_i r'_{ix} r'_{iz} \\ -m_i r'_{iy} r'_{ix} & m_i(r_{ix}'^2 + r_{iz}'^2) & -m_i r'_{iy} r'_{iz} \\ -m_i r'_{iz} r'_{ix} & -m_i r'_{iz} r'_{iy} & m_i(r_{ix}'^2 + r_{iy}'^2) \end{pmatrix} \quad r'_i = r_i(t) - x(t)$$

Shall we re-compute when rotated?

- Continuous distribution: sum to integral, mass to density

# Inertia tensor

- Transformation of  $I(t)$

$$I(t) = \sum \begin{pmatrix} m_i(r'_{iy}{}^2 + r'_{iz}{}^2) & -m_i r'_{ix} r'_{iy} & -m_i r'_{ix} r'_{iz} \\ -m_i r'_{iy} r'_{ix} & m_i(r'_{ix}{}^2 + r'_{iz}{}^2) & -m_i r'_{iy} r'_{iz} \\ -m_i r'_{iz} r'_{ix} & -m_i r'_{iz} r'_{iy} & m_i(r'_{ix}{}^2 + r'_{iy}{}^2) \end{pmatrix} + \quad \textcolor{red}{+} \quad \cancel{r'_i}^T r'_i = r'_{ix}{}^2 + r'_{iy}{}^2 + r'_{iz}{}^2$$



$$I(t) = \sum m_i r_i'^T r'_i \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} - \begin{pmatrix} m_i r'_{ix}{}^2 & m_i r'_{ix} r'_{iy} & m_i r'_{ix} r'_{iz} \\ m_i r'_{iy} r'_{ix} & m_i r'_{iy}{}^2 & m_i r'_{iy} r'_{iz} \\ m_i r'_{iz} r'_{ix} & m_i r'_{iz} r'_{iy} & m_i r'_{iz}{}^2 \end{pmatrix} + \quad \textcolor{red}{+} \quad r'_i r_i'^T = \begin{pmatrix} r'_{ix}{}^2 & r'_{ix} r'_{iy} & r'_{ix} r'_{iz} \\ r'_{iy} r'_{ix} & r'_{iy}{}^2 & r'_{iy} r'_{iz} \\ r'_{iz} r'_{ix} & r'_{iz} r'_{iy} & r'_{iz}{}^2 \end{pmatrix}$$



$$I(t) = \sum m_i ((r_i'^T r'_i) \mathbf{1} - r'_i r_i'^T)$$

# Inertia tensor

- Transformation of  $I(t)$

$$I(t) = \sum m_i ((r_i'^T r_i') \mathbf{1} - r_i' r_i'^T) \quad + \quad \begin{array}{l} r_i(t) = R(t)r_{0i} + x(t) \quad r_i' = R(t)r_{0i} \\ R(t)R(t)^T = \mathbf{1} \end{array}$$



$$\begin{aligned} I(t) &= \sum m_i ((r_i'^T r_i') \mathbf{1} - r_i' r_i'^T) \\ &= \sum m_i ((R(t)r_{0i})^T (R(t)r_{0i}) \mathbf{1} - (R(t)r_{0i})(R(t)r_{0i})^T) \\ &= \sum m_i (r_{0i}^T R(t)^T R(t)r_{0i} \mathbf{1} - R(t)r_{0i}r_{0i}^T R(t)^T) \\ &= \sum m_i ((r_{0i}^T r_{0i}) \mathbf{1} - R(t)r_{0i}r_{0i}^T R(t)^T) \\ &= \sum m_i (R(t)(r_{0i}^T r_{0i})R(t)^T \mathbf{1} - R(t)r_{0i}r_{0i}^T R(t)^T) \\ &= R(t) \left( \sum m_i ((r_{0i}^T r_{0i}) \mathbf{1} - r_{0i}r_{0i}^T) \right) R(t)^T \end{aligned}$$

Constant, can be pre-computed!



# Inertia tensor

- **General computation**
  - Define body intrinsic inertia tensor

$$I(t) = R(t) \left( \sum m_i ((r_{0i}^T r_{0i}) \mathbf{1} - r_{0i} r_{0i}^T) \right) R(t)^T$$



$$I_{body} = \sum m_i ((r_{0i}^T r_{0i}) \mathbf{1} - r_{0i} r_{0i}^T)$$



$$I(t) = R(t) I_{body} R(t)^T$$

# Inertia tensor

- **General computation**
  - Inverse inertia tensor

$$R(t)^T = R(t)^{-1} \quad (R(t)^T)^T = R(t)$$



$$\begin{aligned} I^{-1}(t) &= (R(t)I_{body}R(t)^T)^{-1} \\ &= (R(t)^T)^{-1} I_{body}^{-1} R(t)^{-1} \\ &= R(t)I_{body}^{-1}R(t)^T \end{aligned}$$

## **2. Rigid body dynamics**

# Rigid body equations of motion

- **State variable**

- Position and orientation
- Linear and angular momentum

$$\mathbf{Y}(t) = \begin{pmatrix} x(t) \\ R(t) \\ P(t) \\ L(t) \end{pmatrix}$$

- **Auxiliary quantities**

$$v(t) = \frac{P(t)}{M}, \quad I(t) = R(t)I_{body}R(t)^T \quad \text{and} \quad \omega(t) = I(t)^{-1}L(t)$$

# Rigid body equations of motion

- Time rate change of the state variable

$$\frac{d}{dt}\mathbf{Y}(t) = \frac{d}{dt} \begin{pmatrix} x(t) \\ R(t) \\ P(t) \\ L(t) \end{pmatrix} = \begin{pmatrix} v(t) \\ \omega(t)^* R(t) \\ F(t) \\ \tau(t) \end{pmatrix}$$

- Computing order

$$F(t) \longrightarrow P(t)$$

$$\tau(t) \longrightarrow L(t)$$

$$P(t) \xrightarrow{P(t) = Mv(t)} v(t) \longrightarrow x(t)$$

$$L(t) \xrightarrow{L(t) = I(t)\omega(t)} \omega(t) \longrightarrow R(t)$$

# Quaternions vs. rotation matrices

- **Using rotation matrix is problematic**
  - Why?
    - Numerical error will accumulate on rotation matrix
    - Artificial skewing effects
    - Can be alleviated by representing rotations with unit quaternions
- **Quaternion**
  - The quaternion  $s + v_x\mathbf{i} + v_y\mathbf{j} + v_z\mathbf{k}$
  - Written as  $[s, v]$

# Quaternions vs. rotation matrices

- Quaternion multiplication

$$[s_1, v_1][s_2, v_2] = [s_1s_2 - v_1 \cdot v_2, s_1v_2 + s_2v_1 + v_1 \times v_2]$$

- From quaternion to rotation matrix

$$\begin{pmatrix} 1 - 2v_y^2 - 2v_z^2 & 2v_xv_y - 2sv_z & 2v_xv_z + 2sv_y \\ 2v_xv_y + 2sv_z & 1 - 2v_x^2 - 2v_z^2 & 2v_yv_z - 2sv_x \\ 2v_xv_z - 2sv_y & 2v_yv_z + 2sv_x & 1 - 2v_x^2 - 2v_y^2 \end{pmatrix}$$

# Quaternions vs. rotation matrices

- **Rotation of a rigid body**
  - Suppose the body to rotate with constant  $\omega(t)$  for a period of time  $\Delta t$  :

$$\left[ \cos \frac{|\omega(t)| \Delta t}{2}, \sin \frac{|\omega(t)| \Delta t}{2} \frac{\omega(t)}{|\omega(t)|} \right]$$

- Equation for  $\dot{q}(t)$

$$\dot{q}(t) = \frac{1}{2} \omega(t) q(t)$$



# Solving ordinary differential equations

- **The rigid body dynamics results in**
  - Ordinary set of differential equation of the form:

$$y' = f(x, y)$$

- Seldom have closed-form solution
- Usually with initial condition

$$y(x_0) = y_0$$

- Initial value problem

$$\mathbf{y}' = \mathbf{f}(x, \mathbf{y}) , \quad \mathbf{y}(x_0) = \mathbf{y}_0$$

# Solving ordinary differential equations

- **Numerical solution**

- Euler's method

- We divide this interval by the mesh-points

$$x_n = x_0 + nh, \quad n = 0, \dots, N$$

- Integrating the differential equation

$$y' = f(x, y)$$



$$y(x_{n+1}) = y(x_n) + \int_{x_n}^{x_{n+1}} f(x, y(x)) \, dx$$



$$\int_{x_n}^{x_{n+1}} g(x) \, dx \approx hg(x_n)$$

$$y(x_{n+1}) \approx y(x_n) + hf(x_n, y(x_n))$$

# Solving ordinary differential equations

- **Runge–Kutta methods**

- Achieve higher accuracy
- Re-evaluate  $f(\cdot, \cdot)$  at points intermediate between  $(x_n, y(x_n))$  and  $(x_{n+1}, y(x_{n+1}))$

Now pick a step-size  $h > 0$  and define

$$y_{n+1} = y_n + \frac{1}{6} (k_1 + 2k_2 + 2k_3 + k_4),$$

$$t_{n+1} = t_n + h$$

for  $n = 0, 1, 2, 3, \dots$ , using

$$k_1 = h f(t_n, y_n),$$

$$k_2 = h f\left(t_n + \frac{h}{2}, y_n + \frac{k_1}{2}\right),$$

$$k_3 = h f\left(t_n + \frac{h}{2}, y_n + \frac{k_2}{2}\right),$$

$$k_4 = h f(t_n + h, y_n + k_3).$$

### **3. Non-penetration constraints**

# Problems of non-penetration constraints

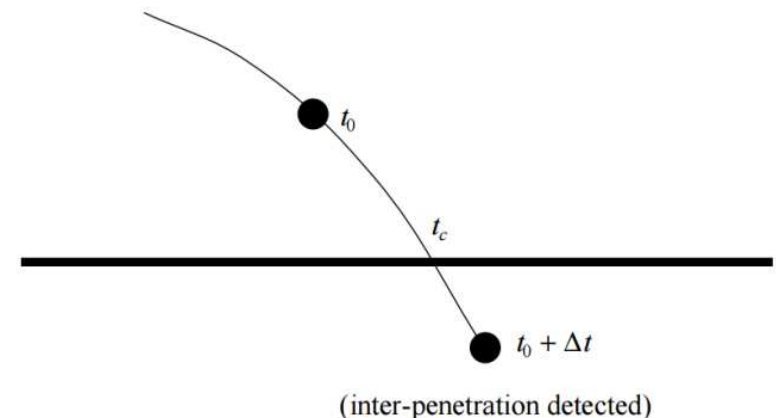
- **Two types of contacts**

- Colliding contact

- Two bodies are in contact at some point  $p$
    - They have a velocity towards each other
    - $Y(t)$  has discontinuity
      - E.g., instantaneous change of velocity

- How to solve?

- Stop ODE solver at the contact
    - Compute how  $Y(t)$  changes
    - Restart ODE solver



# Problems of non-penetration constraints

- **Two types of contacts**

- Resting contact

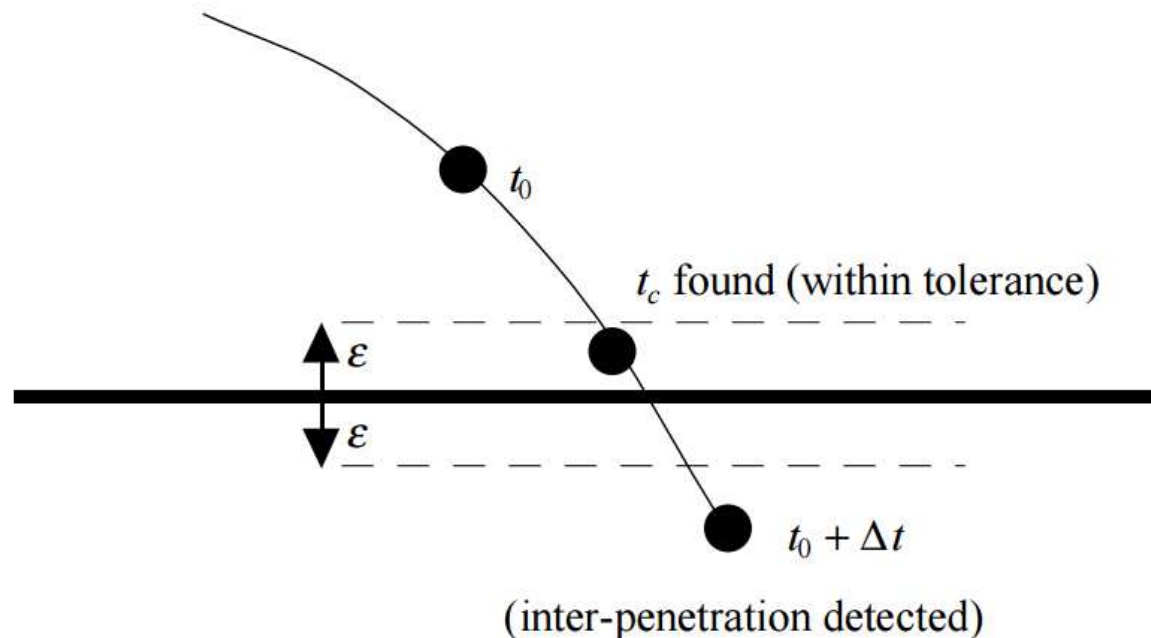
- Whenever bodies are resting on one another at some point  $p$
    - We compute a force that prevents the particle from accelerating
    - Contact force
      - A force that acts at the point of contact between two objects

- **Two problems to solve**

- Compute velocity changes for colliding contact
  - Compute the contact forces that prevent inter-penetration

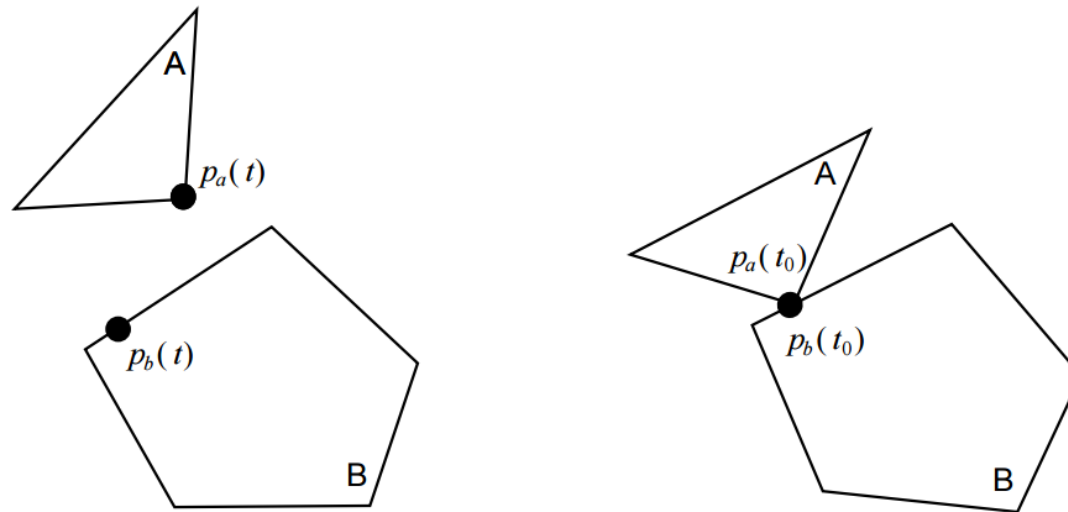
# Bisection

- **When inter-penetration is detected**
  - We inform the ODE solver that we wish to restart back at time  $t$
  - Simulate forward to time  $t_0 + \Delta t/2$ , and repeat until some tolerance is met



# Colliding contact

- Description of a colliding contact
  - Illustration



- Formula

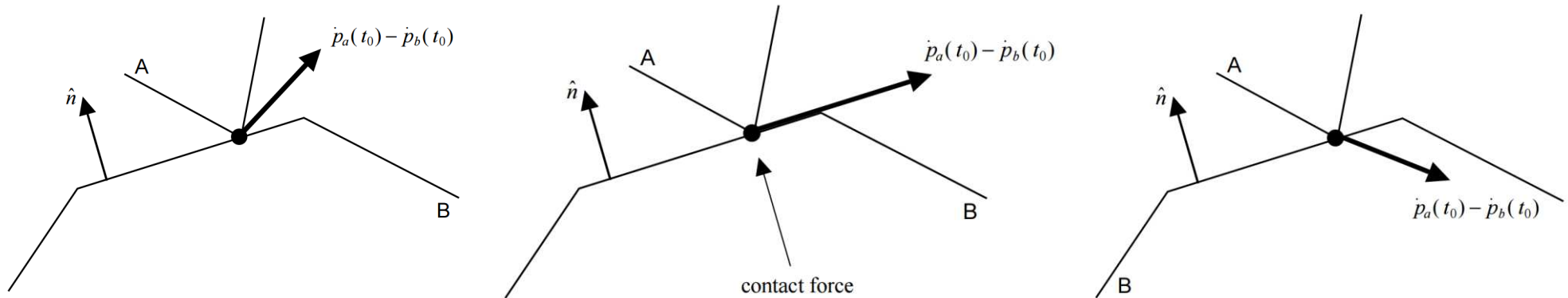
$$\dot{p}_a(t_0) = v_a(t_0) + \omega_a(t_0) \times (p_a(t_0) - x_a(t_0))$$

$$\dot{p}_b(t_0) = v_b(t_0) + \omega_b(t_0) \times (p_b(t_0) - x_b(t_0))$$



# Colliding contact

- Examine the relative velocity



$$v_{rel} = \hat{n}(t_0) \cdot (\dot{p}_a(t_0) - \dot{p}_b(t_0))$$

- $v_{rel} > 0$ : two bodies leaving apart, not interested
- $v_{rel} = 0$ : resting contact
- $v_{rel} < 0$ : a colliding contact
  - How do we compute the change in velocity?

# Colliding contact

- **Definition of an impulse**

- Force exerted over a time period

$$F\Delta t = J$$

- Apply an impulse  $J$  to a rigid body with mass  $M$

$$\Delta v = \frac{J}{M} \quad \Delta P = J$$

- Impulsive torque

$$\tau_{impulse} = (p - x(t)) \times J$$

- Change in angular momentum

$$\Delta L = \tau_{impulse}$$

- Change in angular velocity

$$I^{-1}(t_0)\tau_{impulse}$$


# Colliding contact

- **How to compute the impulse?**

- Force  $F$  is unknown
- For frictionless bodies, the direction of the impulse will be in the normal direction

$$J = j\hat{n}(t_0)$$

- How to compute  $j$ ?
  - We compute  $j$  by using an empirical law for collisions
- Some definitions

$\dot{p}_a^-(t_0)$   velocity of the contact vertex of A prior to the impulse being applied

$\dot{p}_a^+(t_0)$   velocity after we apply the impulse  $J$

# Colliding contact

- **Definition of relative velocities**

- Initial relative velocity in the normal direction

$$v_{rel}^- = \hat{n}(t_0) \cdot (\dot{p}_a^-(t_0) - \dot{p}_b^-(t_0))$$

- After the application of the impulse

$$v_{rel}^+ = \hat{n}(t_0) \cdot (\dot{p}_a^+(t_0) - \dot{p}_b^+(t_0))$$

- Empirical law for frictionless collisions

$$v_{rel}^+ = -\epsilon v_{rel}^- \quad 0 \leq \epsilon \leq 1$$

↖  
Coefficient of restitution

# Colliding contact

- **Physical meaning for coefficient of restitution**

- Perfect bouncing

- No kinetic energy is lost

$$\epsilon = 1 \qquad v_{rel}^+ = -v_{rel}^-$$

- Perfect dissipative

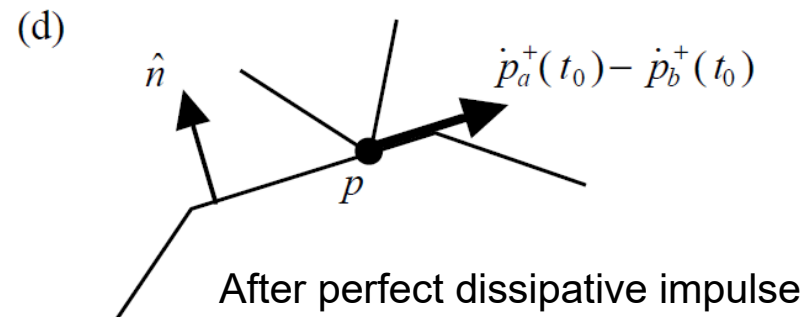
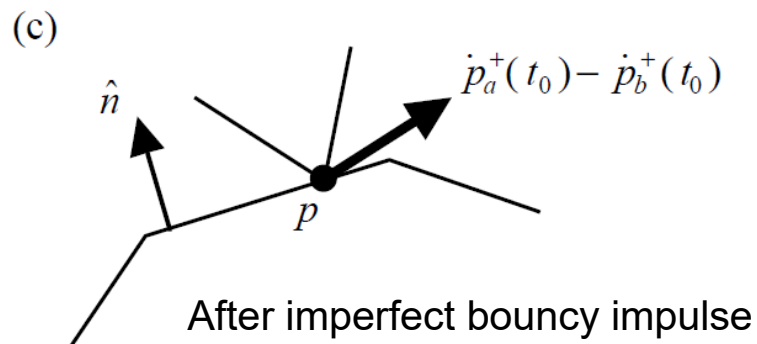
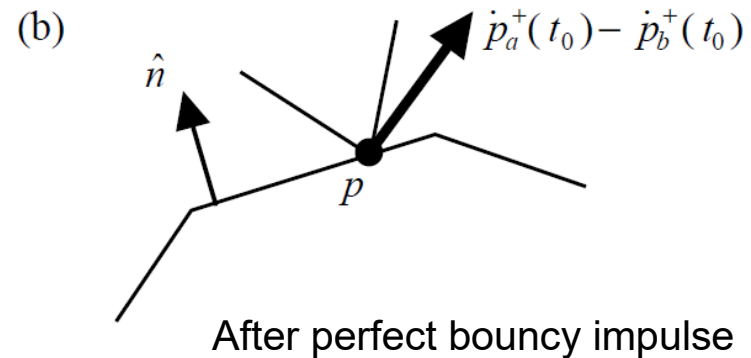
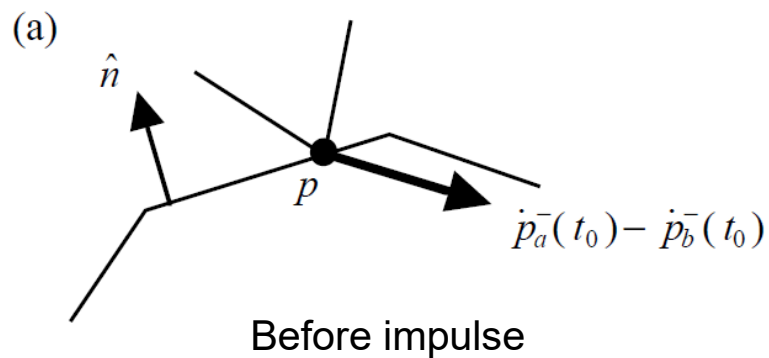
- A maximum of kinetic energy is lost

$$\epsilon = 0 \qquad v_{rel}^+ = 0$$

- After this collision, the two bodies will be in rest contact

# Colliding contact

- Physical meaning for coefficient of restitution
  - Illustration



# Colliding contact

- Derivation

$$\dot{p}_a^+(t_0) = v_a^+(t_0) + \omega_a^+(t_0) \times r_a \quad v_a^+(t_0) = v_a^-(t_0) + \frac{j\hat{n}(t_0)}{M_a} \quad \omega_a^+(t_0) = \omega_a^-(t_0) + I_a^{-1}(t_0) (r_a \times j\hat{n}(t_0))$$



$$\begin{aligned} \dot{p}_a^+(t_0) &= \left( v_a^-(t_0) + \frac{j\hat{n}(t_0)}{M_a} \right) + \left( \omega_a^-(t_0) + I_a^{-1}(t_0) (r_a \times j\hat{n}(t_0)) \right) \times r_a \\ &= v_a^-(t_0) + \omega_a^-(t_0) \times r_a + \left( \frac{j\hat{n}(t_0)}{M_a} \right) + \left( I_a^{-1}(t_0) (r_a \times j\hat{n}(t_0)) \right) \times r_a \\ &= \dot{p}_a^- + j \left( \frac{\hat{n}(t_0)}{M_a} + I_a^{-1}(t_0) (r_a \times \hat{n}(t_0)) \right) \times r_a \end{aligned}$$



$$\dot{p}_b^+(t_0) = \dot{p}_b^- - j \left( \frac{\hat{n}(t_0)}{M_b} + I_b^{-1}(t_0) (r_b \times \hat{n}(t_0)) \right) \times r_b$$

# Colliding contact

- This yields

$$\dot{p}_a^+(t_0) - \dot{p}_b^+ = (\dot{p}_a^-(t_0) - \dot{p}_b^-) + j \left( \frac{\hat{n}(t_0)}{M_a} + \frac{\hat{n}(t_0)}{M_b} + \right. \\ \left. (I_a^{-1}(t_0) (r_a \times \hat{n}(t_0))) \times r_a + (I_b^{-1}(t_0) (r_b \times \hat{n}(t_0))) \times r_b \right)$$



$$v_{rel}^+ = \hat{n}(t_0) \cdot (\dot{p}_a^+(t_0) - \dot{p}_b^+) \\ = \hat{n}(t_0) \cdot (\dot{p}_a^-(t_0) - \dot{p}_b^-) + j \left( \frac{1}{M_a} + \frac{1}{M_b} + \right. \\ \left. \hat{n}(t_0) \cdot (I_a^{-1}(t_0) (r_a \times \hat{n}(t_0))) \times r_a + \hat{n}(t_0) \cdot (I_b^{-1}(t_0) (r_b \times \hat{n}(t_0))) \times r_b \right) \\ = v_{rel}^- + j \left( \frac{1}{M_a} + \frac{1}{M_b} + \right. \\ \left. \hat{n}(t_0) \cdot (I_a^{-1}(t_0) (r_a \times \hat{n}(t_0))) \times r_a + \hat{n}(t_0) \cdot (I_b^{-1}(t_0) (r_b \times \hat{n}(t_0))) \times r_b \right)$$



# Colliding contact

- This yields
  - Empirical law for frictionless collision

$$v_{rel}^+ = -\epsilon v_{rel}^- \quad 0 \leq \epsilon \leq 1$$



$$v_{rel}^- + j \left( \frac{1}{M_a} + \frac{1}{M_b} + \hat{n}(t_0) \cdot \left( I_a^{-1}(t_0) (r_a \times \hat{n}(t_0)) \right) \times r_a + \right. \\ \left. \hat{n}(t_0) \cdot \left( I_b^{-1}(t_0) (r_b \times \hat{n}(t_0)) \right) \times r_b \right) = -\epsilon v_{rel}^-$$



$$j = \frac{-(1 + \epsilon)v_{rel}^-}{\frac{1}{M_a} + \frac{1}{M_b} + \hat{n}(t_0) \cdot \left( I_a^{-1}(t_0) (r_a \times \hat{n}(t_0)) \right) \times r_a + \hat{n}(t_0) \cdot \left( I_b^{-1}(t_0) (r_b \times \hat{n}(t_0)) \right) \times r_b}$$

# Colliding contact

- **Handling fixed bodies**

- Some bodies cannot be moved
  - Floors, walls, etc.
- Look at the formulation again

$$j = \frac{-(1 + \epsilon)v_{rel}^-}{\frac{1}{M_a} + \frac{1}{M_b} + \hat{n}(t_0) \cdot \left( I_a^{-1}(t_0) (r_a \times \hat{n}(t_0)) \right) \times r_a + \hat{n}(t_0) \cdot \left( I_b^{-1}(t_0) (r_b \times \hat{n}(t_0)) \right) \times r_b}$$

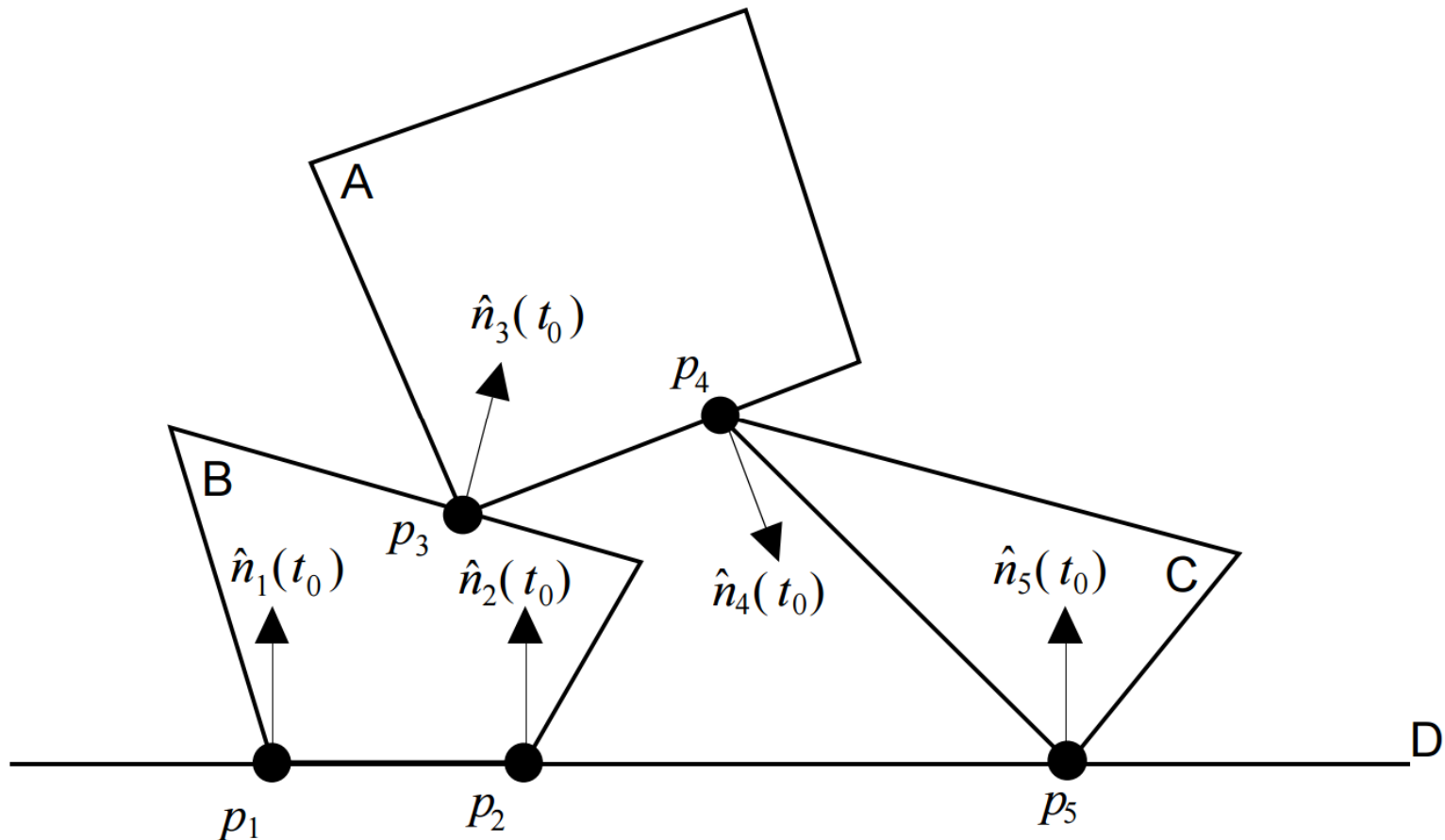
- What we need
  - Inverse of mass and inertia tensor
- Tricks
  - Set inverse mass to be zero
  - Set inverse inertia tensor to be zero matrix

# Resting contact

- **Condition of resting contact**
  - Relative velocity  $v_{\text{rel}}$  is zero (within numerical threshold)
  - Contact force  $f_i \hat{n}_i(t_0)$ 
    - At each contact point, there is a contact force where  $f_i$  is an unknown scalar
    - Our goal
      - Determine each  $f_i$  at the same time
      - To maintain contact between bodies

# Resting contact

- Condition of resting contact
  - Computing contact forces



# Resting contact

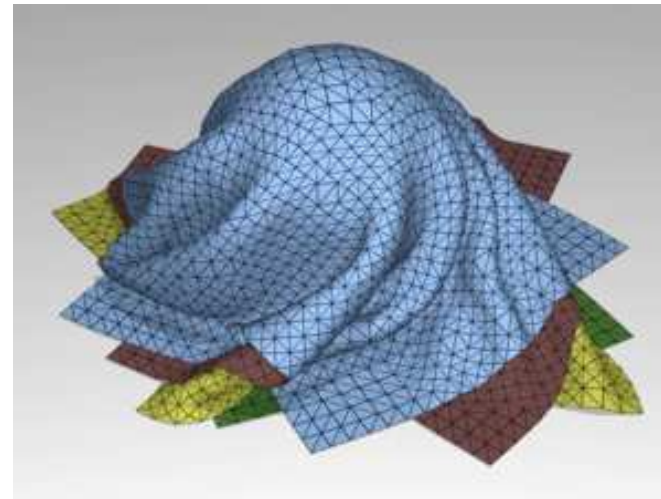
- **Derivation**
  - Contact force subject to three conditions
    - 1. Must prevent inter-penetration
    - 2. Must be repulsive
      - Never act like a “glue” and hold bodies together
    - 3. Be zero if the bodies begin to separate

## **4. Collision detection**

# Collision Detection Problem

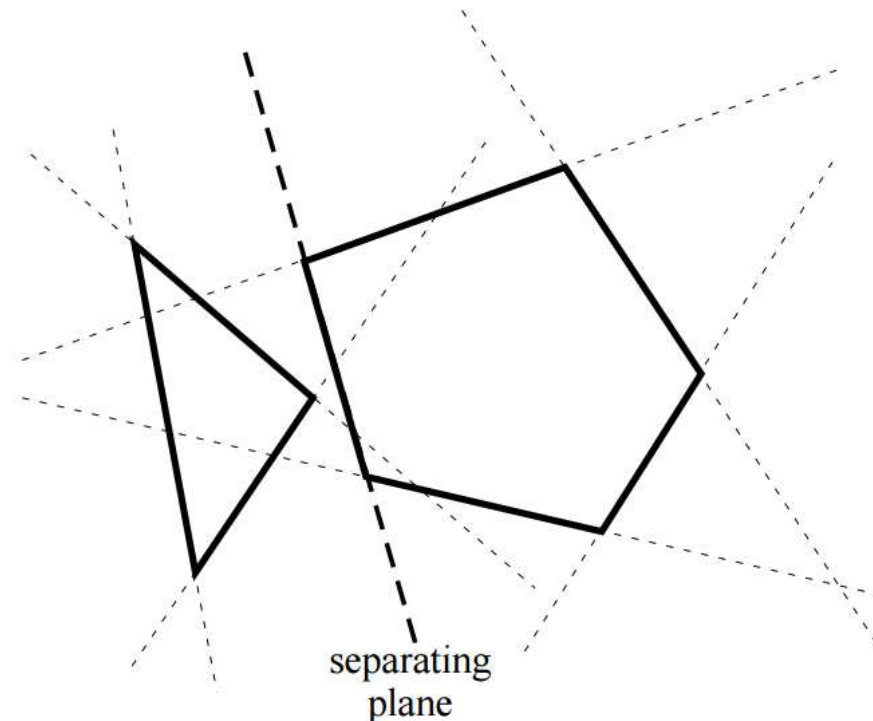
- **Problem formulation**

- The computational problem of detecting the intersection of two or more objects



# Collision detection

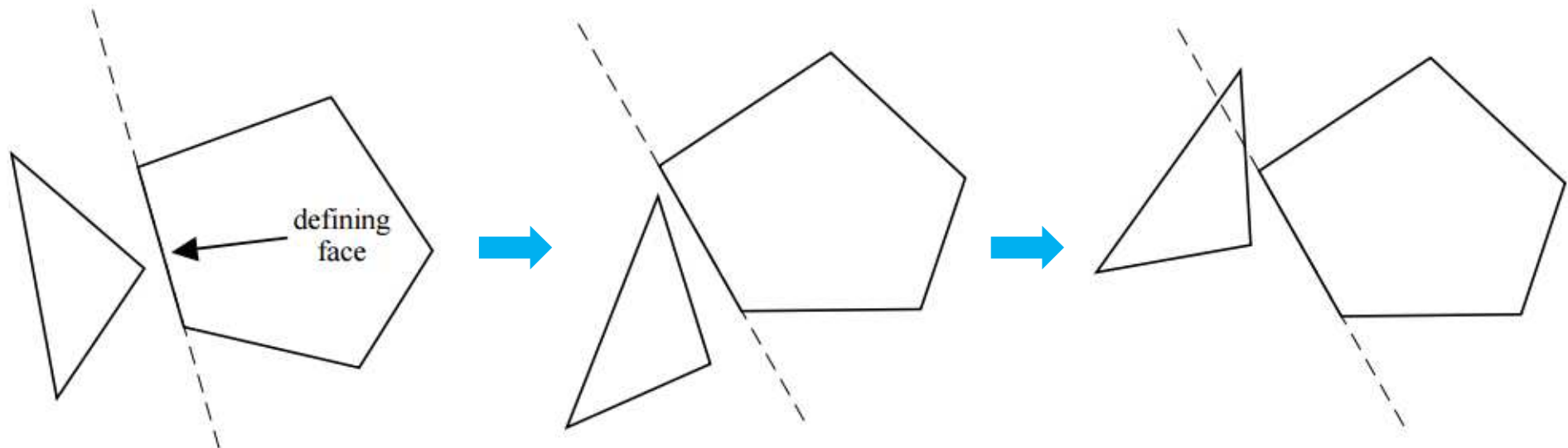
- **How to detect inter-penetration?**
  - Convex polyhedron
    - Two polyhedra do not inter-penetrate if and only if a separating plane between them exists
    - Finding the separating plane





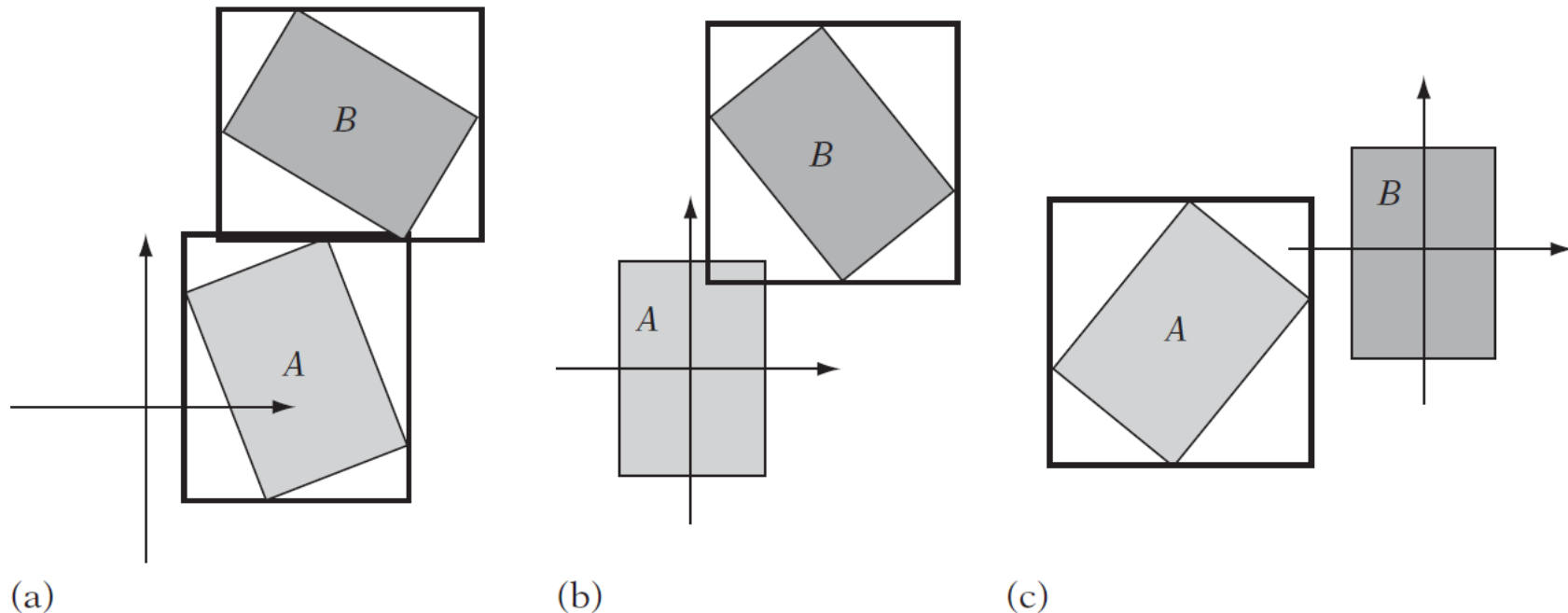
# Collision detection

- **How to detect inter-penetration?**
  - Convex polyhedra
    - Progress with defining face



# Bounding volumes

- **Axis-aligned bounding boxes (AABBs)**
  - AABBs in terms of different coordinate system



(a) AABBs in world space (b) AABBs in the local space of A (c) AABBs in the local space of B

# Basic primitive tests

- **Testing primitives**

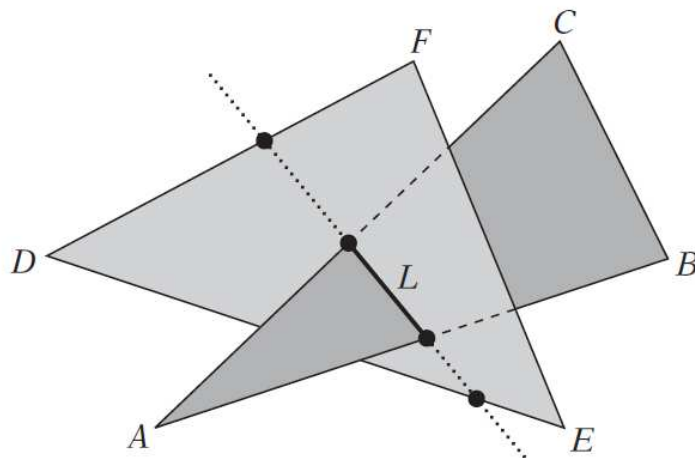
- Testing triangle against triangle

- Detecting the intersection of two triangles ABC and DEF

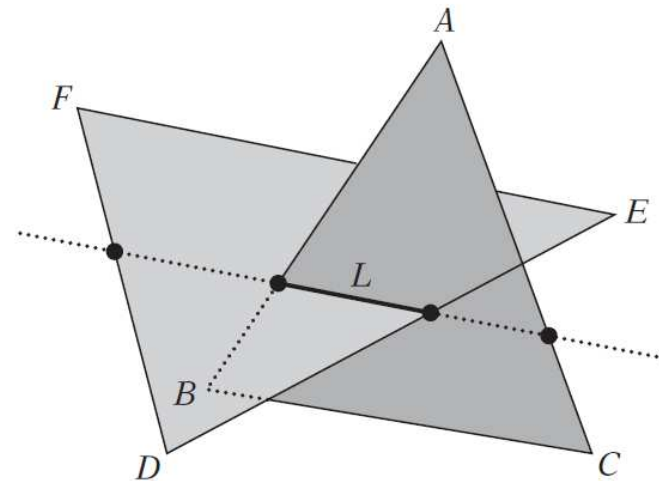
- When two triangles intersect

- Two edges of one triangle pierce the interior of the other

- One edge from each triangle pierces the interior of the other



(a)

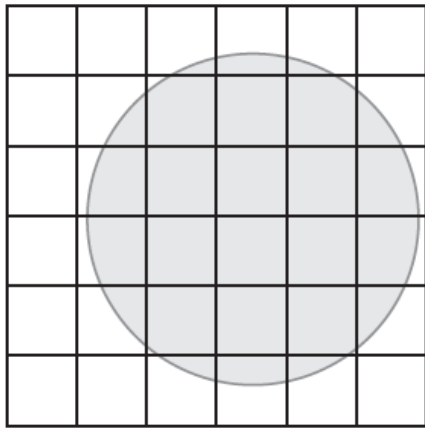


(b)

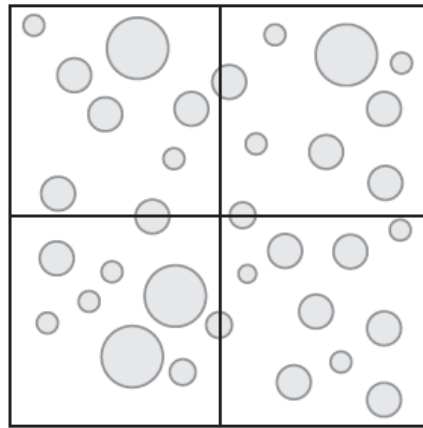
# Spatial partitioning

- **Uniform grids**

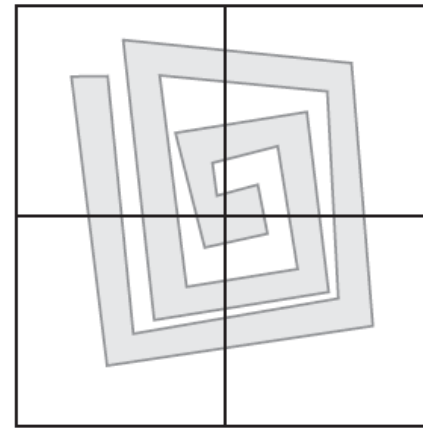
- In-depth tests are only performed against those found sharing cells



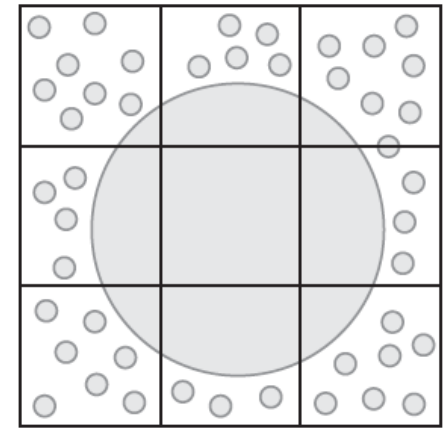
(a)



(b)



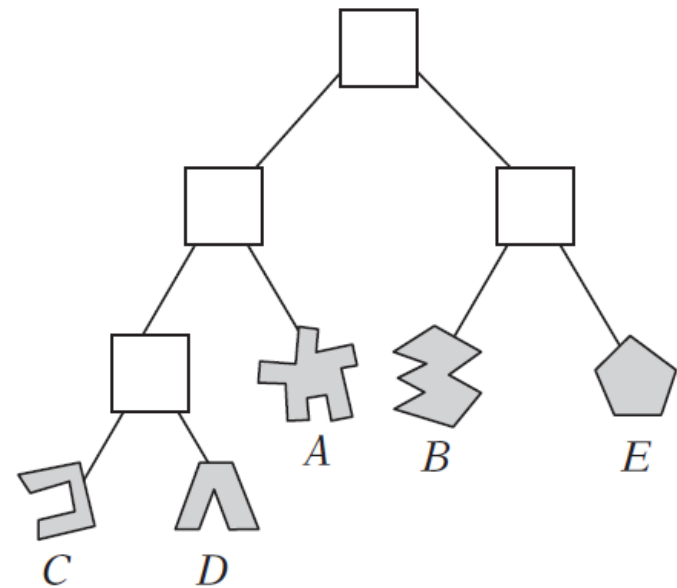
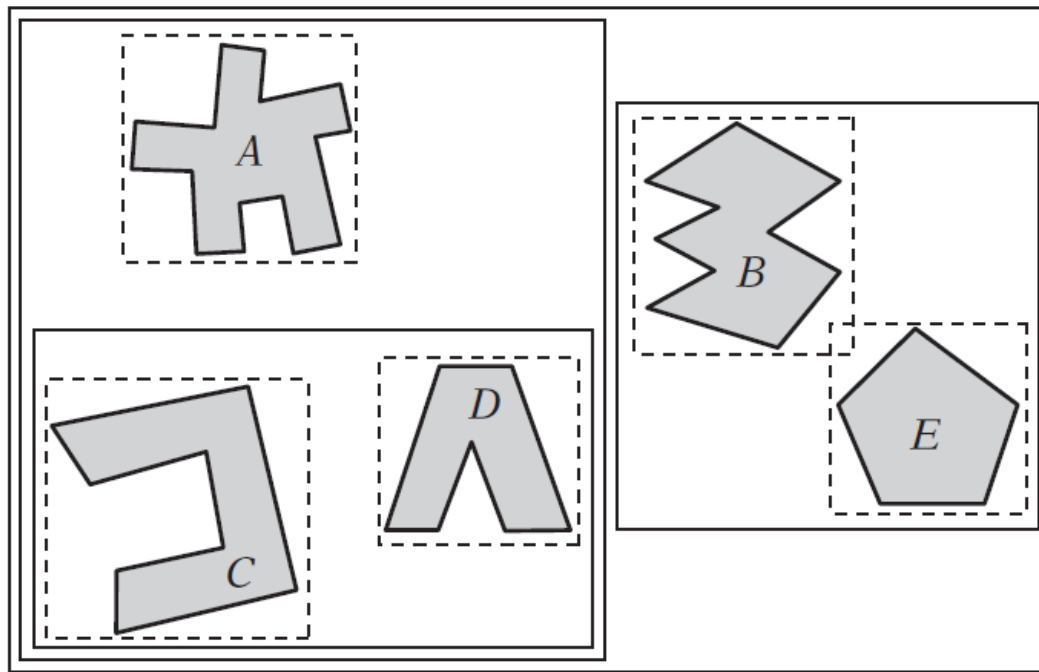
(c)



(d)

# Bounding volume hierarchies

- **Bounding volume hierarchy (BVH)**
  - Time complexity can be reduced to logarithmic in the number of tests performed

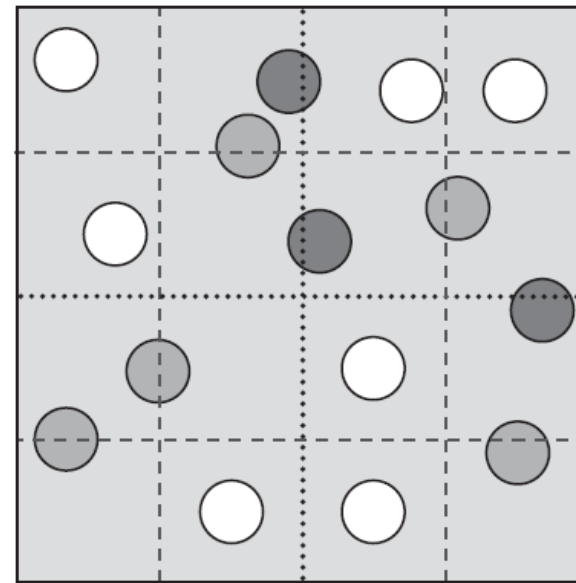
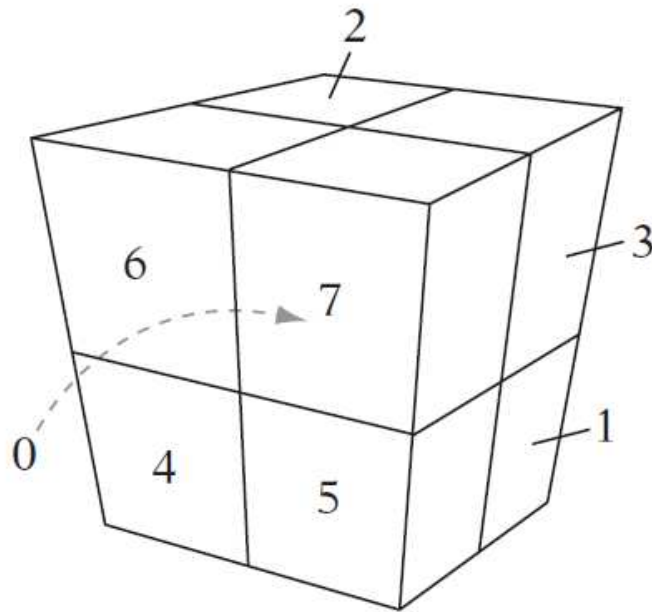


# Spatial partitioning

- **Trees**

- Octree (quadtree for 2D)

- An axis-aligned hierarchical partitioning of a volume of 3D world space

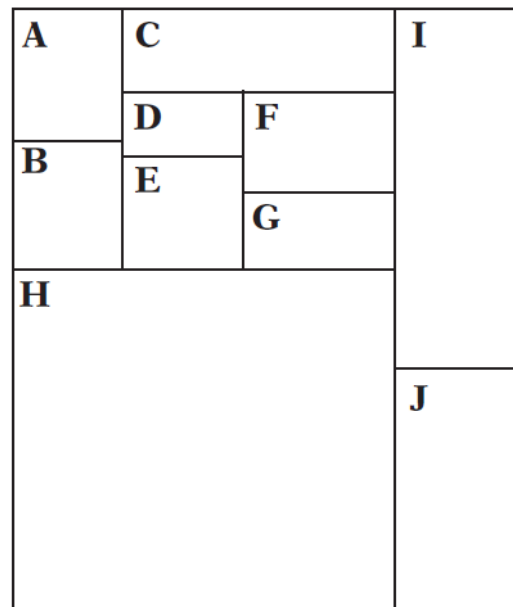


# Spatial partitioning

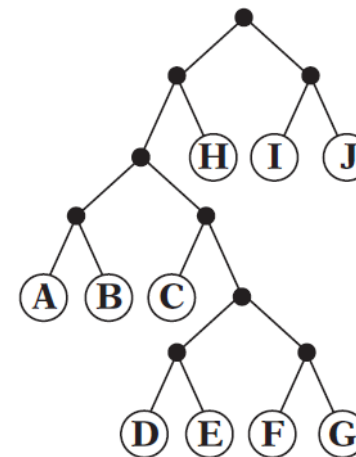
- **Trees**

- k-d trees

- A generalization of octrees and quadtrees
    - The k-d tree divides space along one dimension at a time



(a)



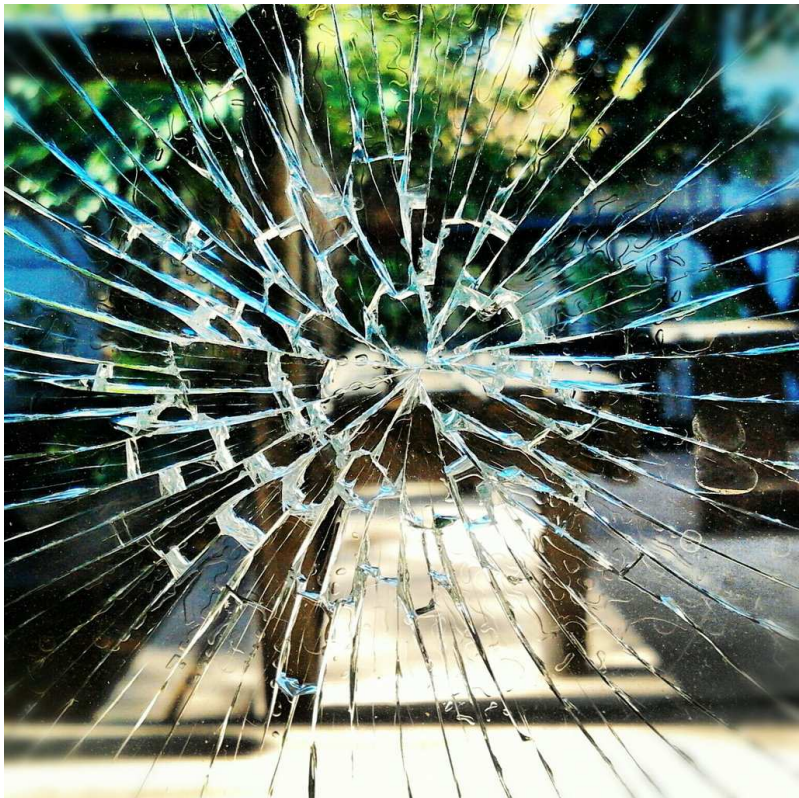
(b)

## **5. Rigid body fracture**



# What is a fracture?

- **A fracture**
  - The separation of an object or material into two or more pieces under the action of stress



# How to model fracture?

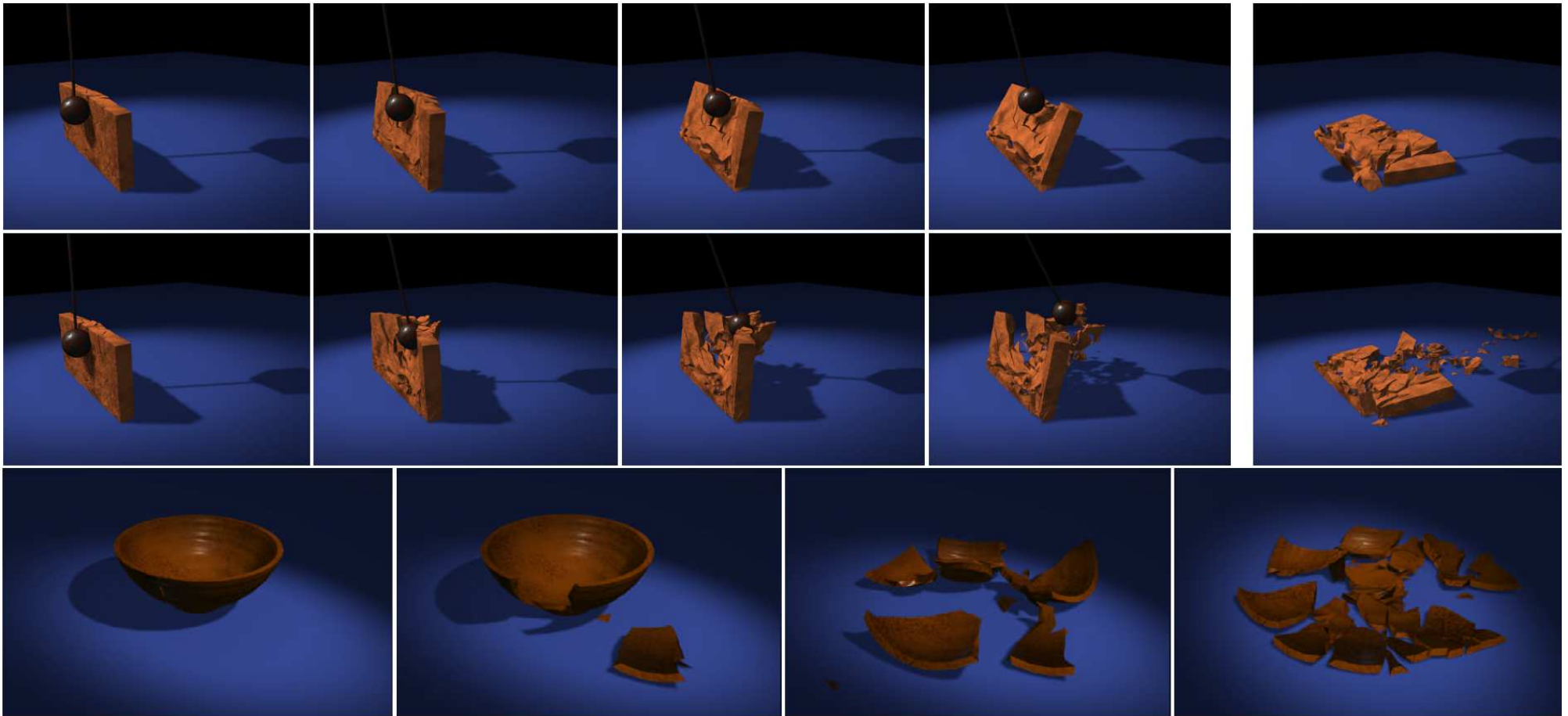
- **Consider material deformations**
  - Even rigid body objects have small deformations
  - Deformation causes change of internal stress
  - Fracture arises when internal stress exceed the material toughness (strength)
- **Modeling**
  - Computation of internal stress distribution
  - Determine the fracture point and fracture geometry

# Continuum mechanics

- **A branch of mechanics**
  - Modeled as a continuous mass rather than as discrete particles
  - The matter in the body is continuously distributed
  - A continuum is a body that can be continually sub-divided into infinitesimal elements
    - Derivatives are available to compute
  - Deal with deformable bodies
    - As opposed to ideal rigid bodies
    - Analyzing internal force of rigid bodies should consider deformation (very small)

# Simulation results

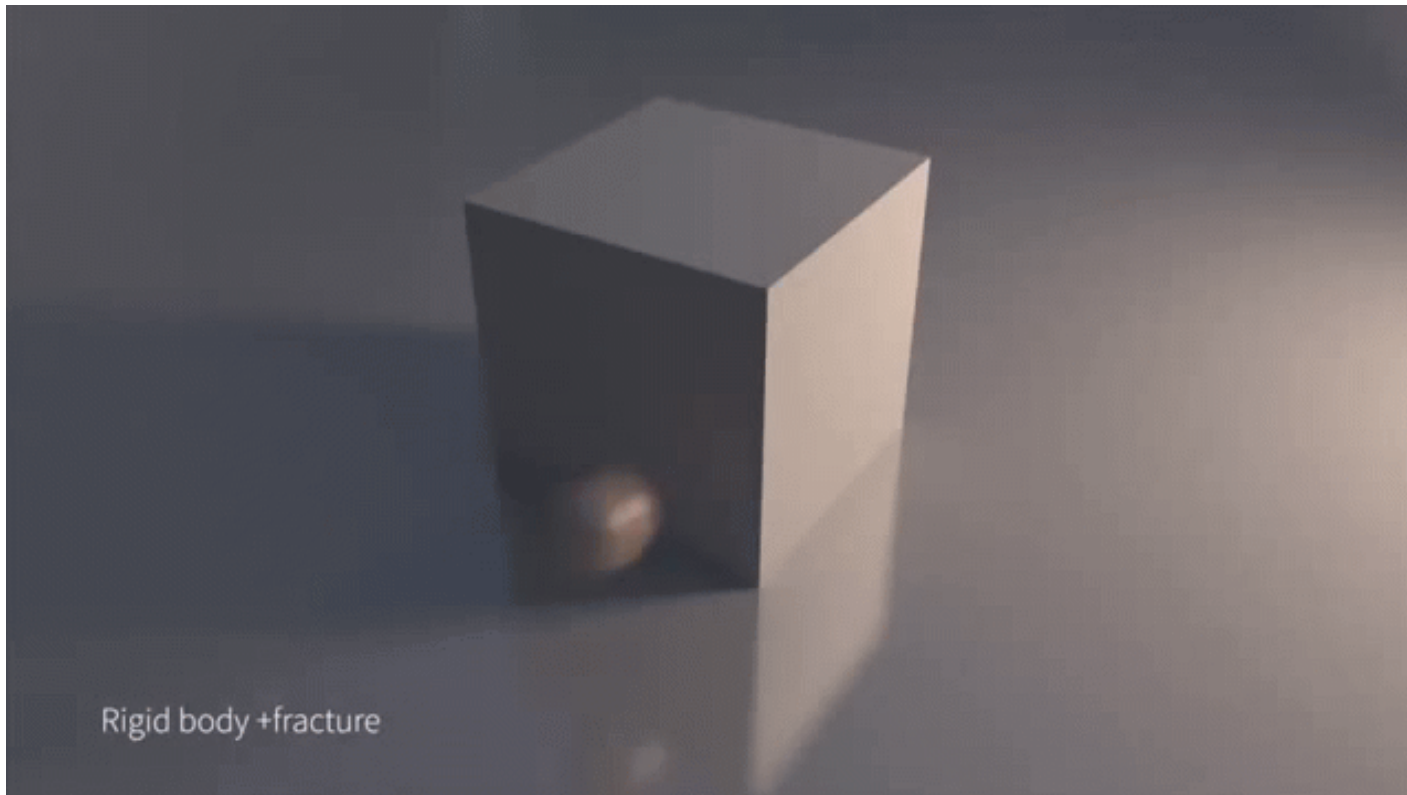
- Fracture-based rigid body simulation





# What you will get finally?

- An example of a system of rigid body motion



**Next lecture: Computer animation 3**