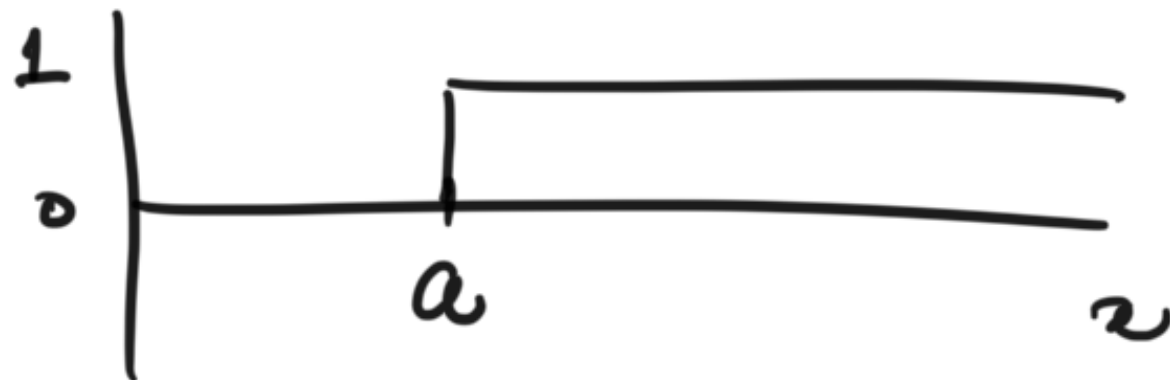


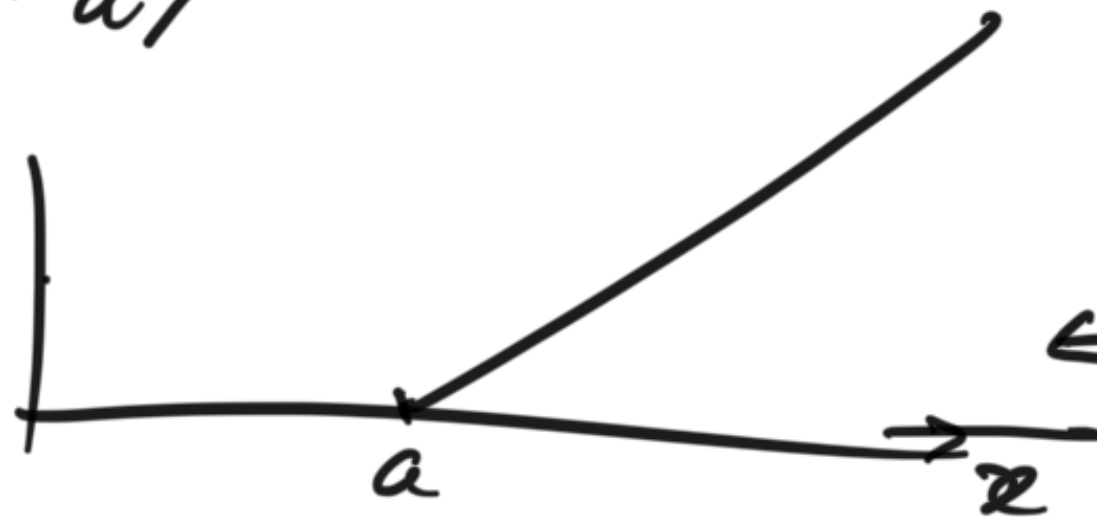
Singularity functions

unit step function
represented by $\langle x-a \rangle$

$f \langle \xi \rangle$ imply that if $\xi < 0$ we ignore or $f=0$
 $\xi \geq 0$ then the value is ξ .

$$\langle x-a \rangle^n$$

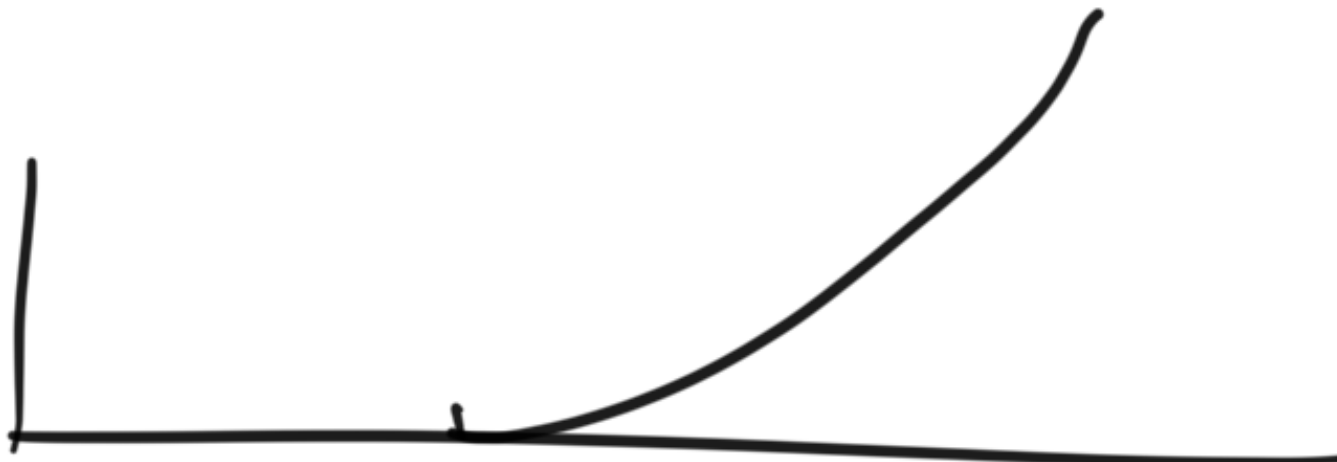
$n=1$



$(x-a)$ if $x \geq a$
 0 if $x < a$

$$\langle x-a \rangle^1$$


$n=2$

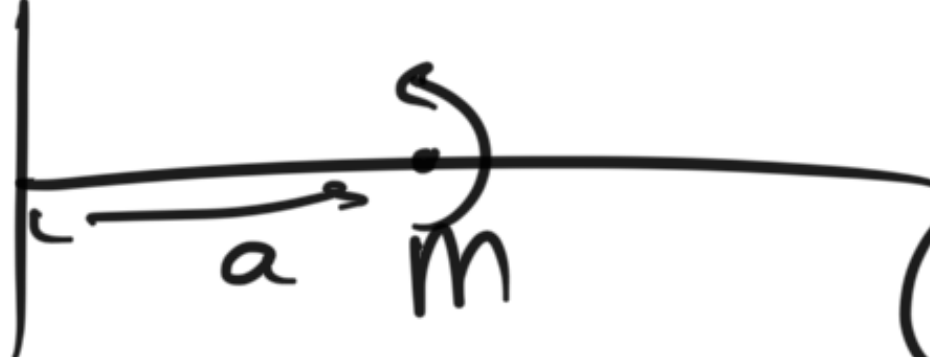


$$\langle x-a \rangle^2$$

$$\begin{aligned} \langle x-a \rangle^n &= (x-a)^n \quad \text{if } x \geq a \\ &= 0 \quad \text{if } x < a \end{aligned}$$

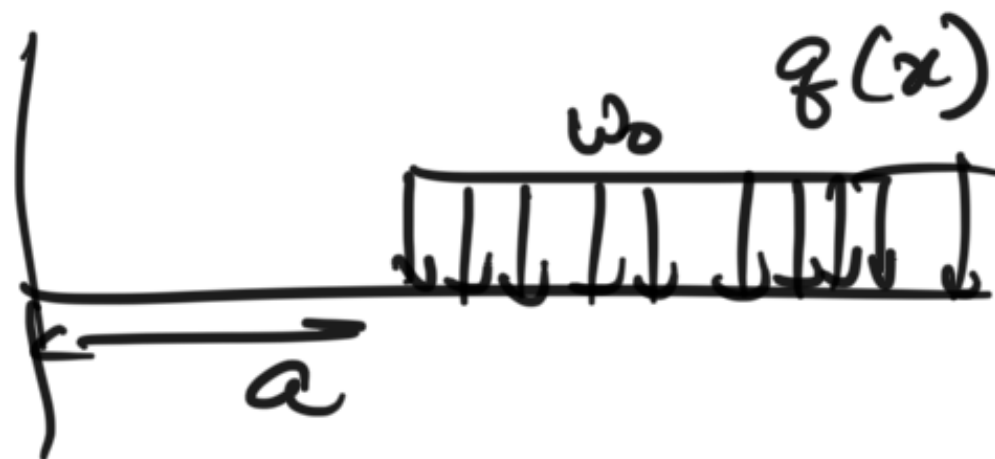
$$\int_{-\infty}^x \langle x-a \rangle^n dx = \frac{\langle x-a \rangle^{n+1}}{n+1}, \quad n \geq 0$$

$\langle x-a \rangle_{-1} =$  impulse function
 force P represented by $P \langle x-a \rangle_{-1}$ in loading $w(x)$ (unit force) \leftarrow loading

$\langle x-a \rangle_{-2} =$  (unit moment)

moment M represented by $M \langle x-a \rangle_{-2}$ in loading

eg.

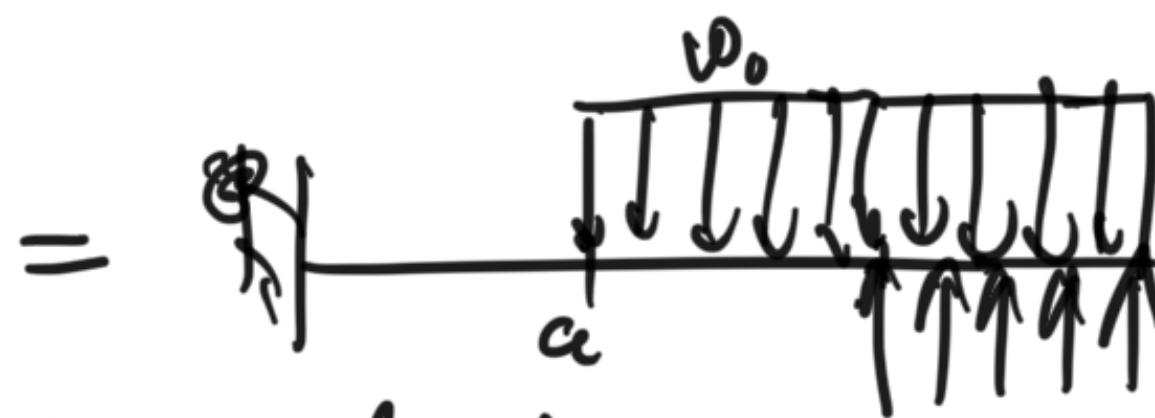
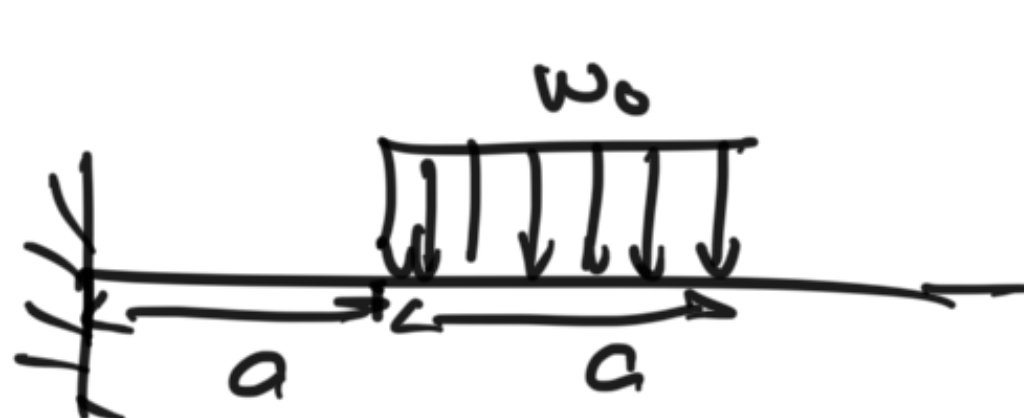


due to $f(x)$

$$w(x) = -f(x) \langle x-a \rangle^0$$

$$w(x) = -w_0 \langle x-a \rangle^0$$

$$\frac{dV}{dx} = -w, \quad \frac{dM}{dx} = V$$



$w(x)$ due to w_0

$$= -w_0 \langle x-a \rangle^0 + w_0 \langle x-2a \rangle^0$$

Use $\langle \rangle$ functions to write expression for $w(x)$, integrate twice to get $M(x)$.

Deflection of beams

- 1) Design specifications allow for a maximum value of deflection
- 2) Indeterminate beams can be solved for using theory of deflections
- 3) Method of superposition can be used to conveniently solve problems

When a beam undergoes a transverse load

$$\frac{1}{\rho} = \frac{m}{EI}$$

If $m = m(x)$, ρ is also a function of x .

$\delta \rightarrow$ curvature will help us to determine deflection of beam.

2, 12, 2 0 1 1 1 1 12, 1 1

$$s \equiv \frac{d^2 y}{dx^2}$$

s related to $\frac{d^2 y}{dx^2}$, $y =$ position of beam

$$\frac{d^3 y}{dx^3} = \frac{m(x)}{EI}$$



beam shape before load is applied



expected shape of beam after loading

$$y_A = 0$$

$$\frac{dy_A}{dx} = \text{slope of deflection} \equiv \theta_A = 0 \quad (\text{for fixed end - cantilever})$$

| P



$$y_A = y_B = 0$$

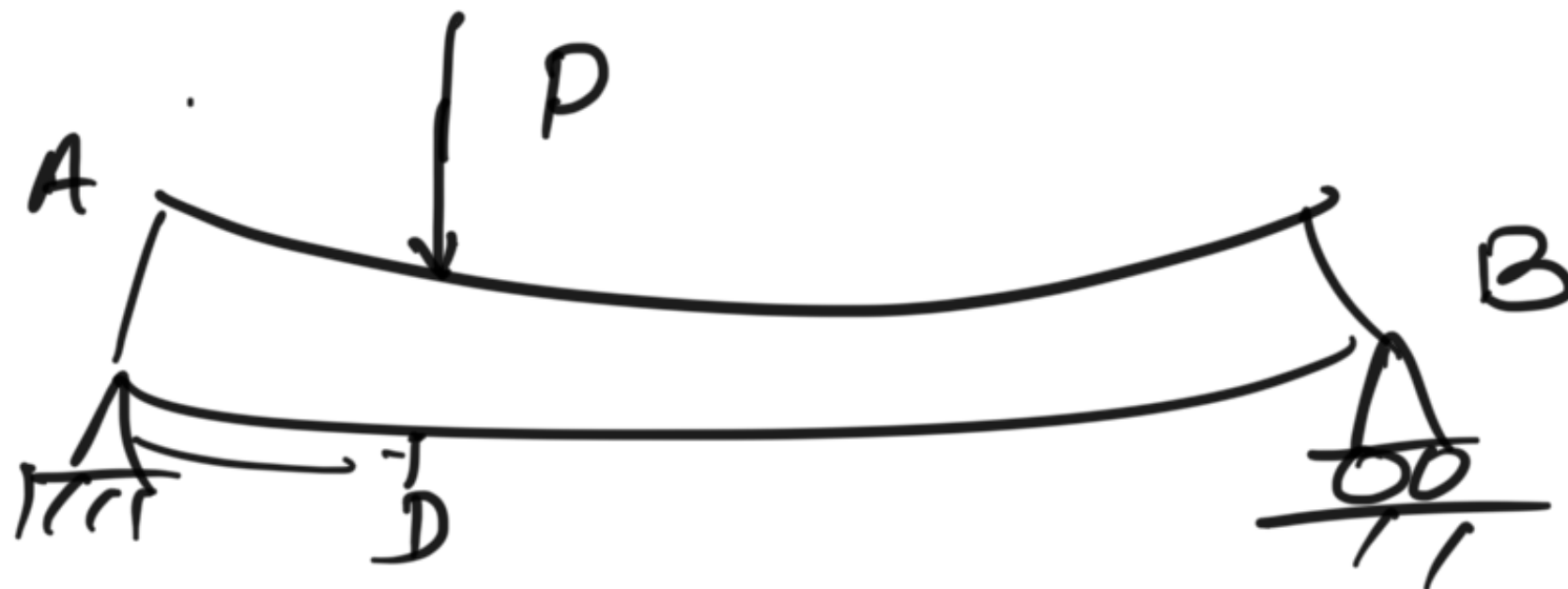
(even after deflection)

shape after deflection

$$\frac{d^2 y}{dx^2} = \frac{M(x)}{EI}$$

2nd order ODE

integrate twice.



y obtained after successive integrations.

deflected beam due to load P

$y_1(x)$ be deflection from A to D. ← based on $M(x)$ from A to D

$y_2(x)$ be deflection from D to B ← based on $M(x)$ from D to B

integrate 2nd order ODE for ~~refm~~ ^{refm} AD \rightarrow 2 constants
^{over} $m(x)$ from D to B
 refm DB \rightarrow 2 constants.

$$y_A = 0$$

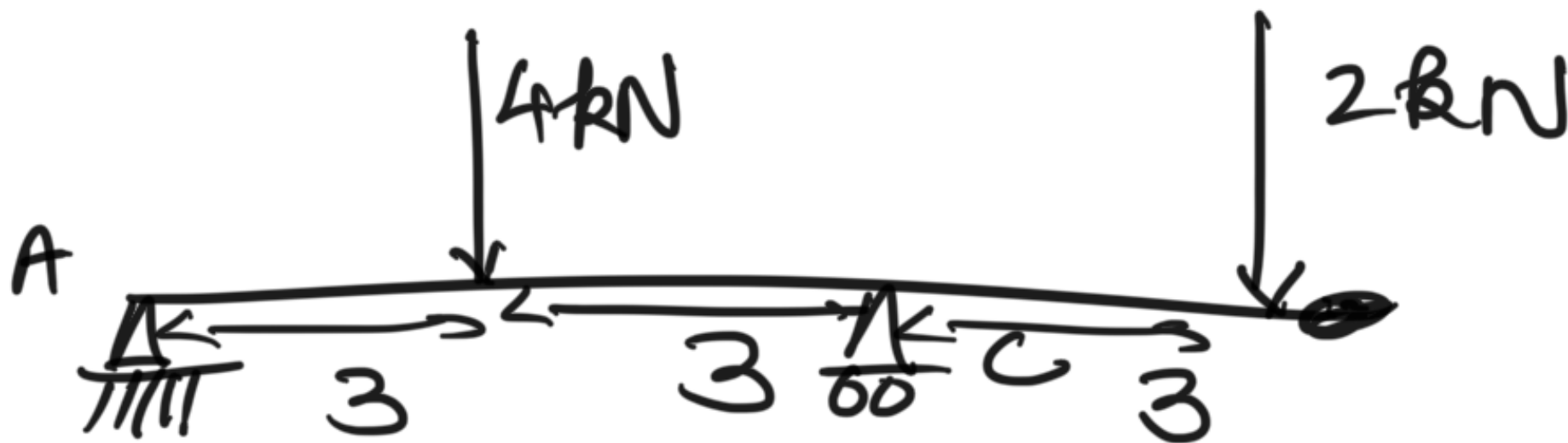
$$y_B = 0$$

At D, deflection & slopes are equal

$$y_1(D) = y_2(D)$$

$$\theta_1(D) = \theta_2(D) \quad \text{where } \theta = \frac{dy}{dx}$$

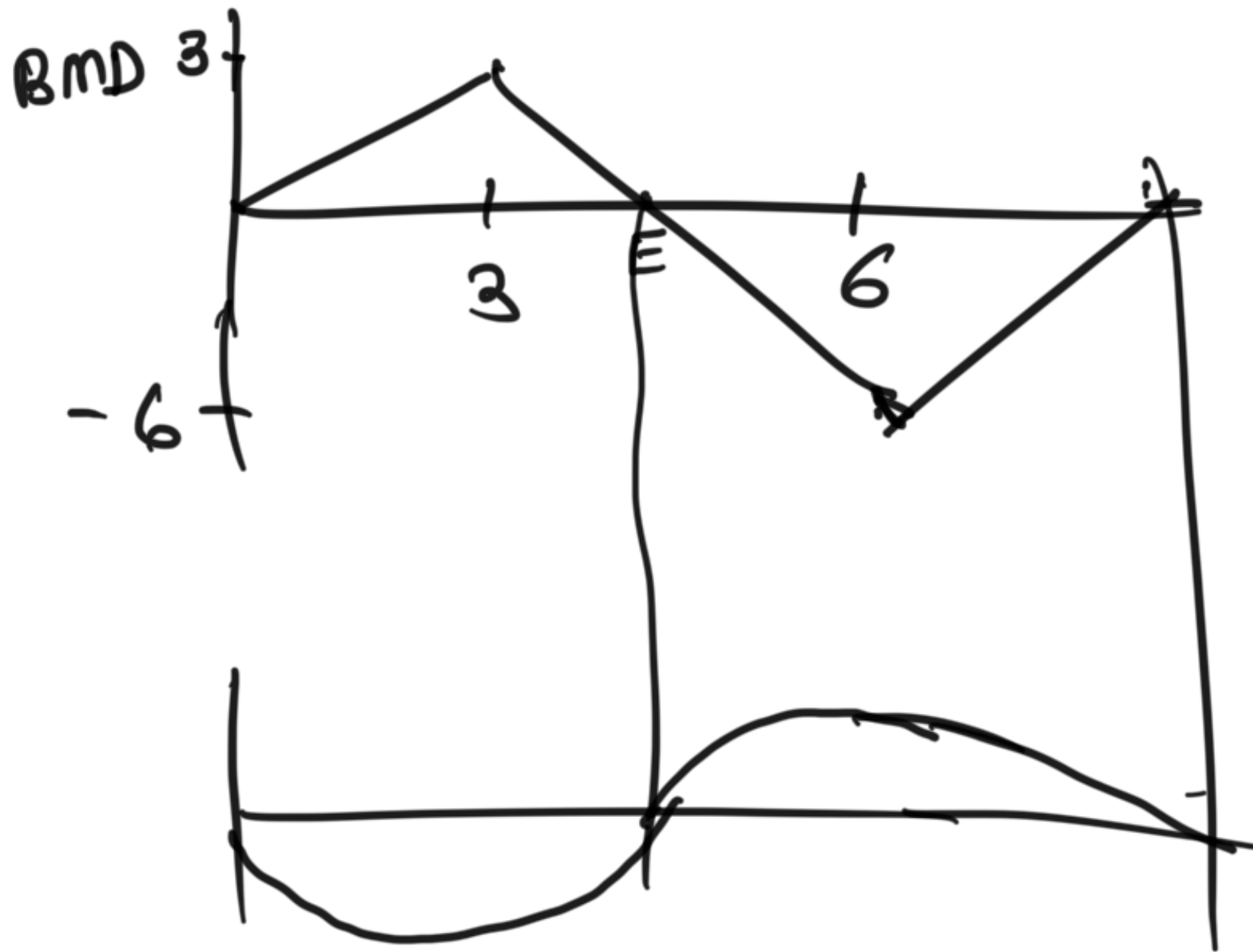
Fig.



statically determinate

H_y C_y

$$A_y = 1 \text{ kN}, \quad C_y = 5 \text{ kN}$$



expected shape of beam
based on BMD

$$\left(\begin{aligned} \sum F_y &= 0 \\ \sum M_{A \text{ or } C} &= 0 \end{aligned} \right)$$

$$0 < x < 3$$

$$m = 1.2$$

$$3 < x < 6$$

$$\begin{aligned} m &= x - 4(x-3) \\ &= x - 4x + 12 \\ &= 12 - 3x \end{aligned}$$

expected shape
of deflected
Beam

$m > 0$ +ve curvature
concave upwards

Calculus: $\frac{1}{\rho} = \frac{\frac{d^2 y}{dx^2}}{\left[1 + \left(\frac{dy}{dx}\right)^2\right]^{3/2}}$

$y(x)$ for beam \rightarrow Elastic curve of beam

$\frac{dy}{dx} \ll 1 \Rightarrow$ denominator can be written as

$$\left[1 + \left(\frac{dy}{dx}\right)^2\right]^{3/2} \approx 1$$

$$\frac{1}{\rho} = \frac{d^2 y}{dx^2} = \frac{m(x)}{EI} \approx$$

$$EI \frac{d^2 y}{dx^2} = m(x)$$

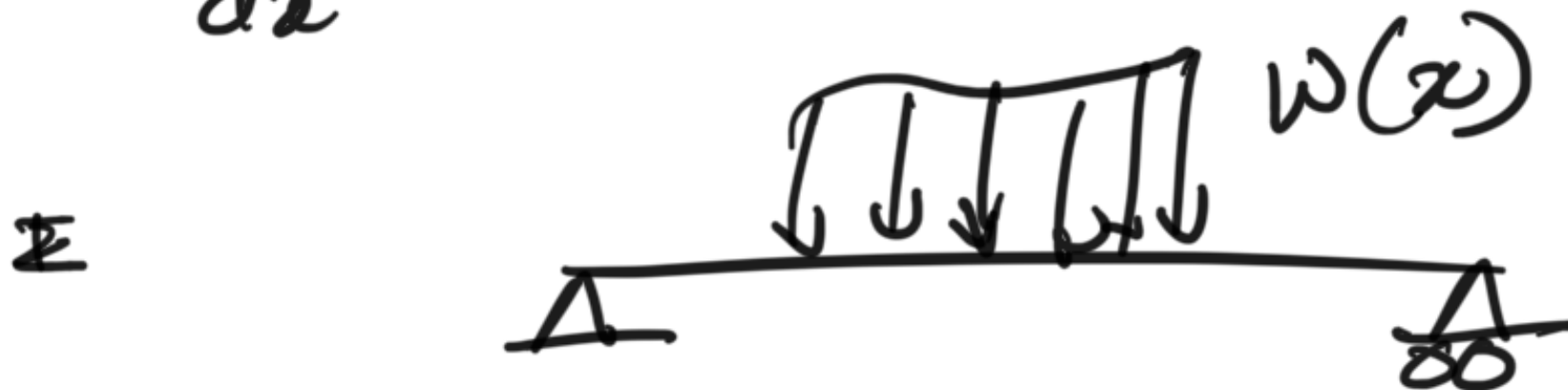
$$EI \frac{dy}{dx} = \int_0^x m(x) dx + C_1$$

$$EI y(x) = \left[\int_0^x \left\{ \int_0^x m(x) dx + C_1 \right\} dx \right]$$

$$\frac{dy}{dx} = \theta(x) \rightarrow \text{slope (radians)}$$

tangent to the elastic curve

$$\frac{dy}{dx} = \tan \theta \approx \theta \text{ (if } \theta \text{ is small.)}$$



$$\frac{d^2 y}{dx^2} = \frac{m(x)}{EI}$$

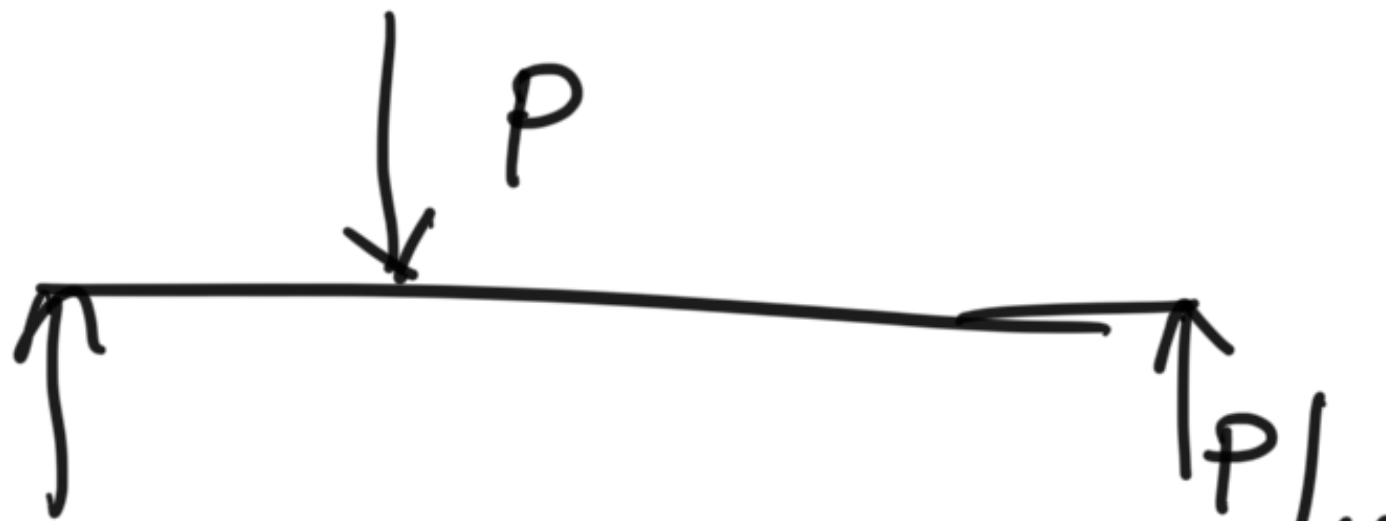
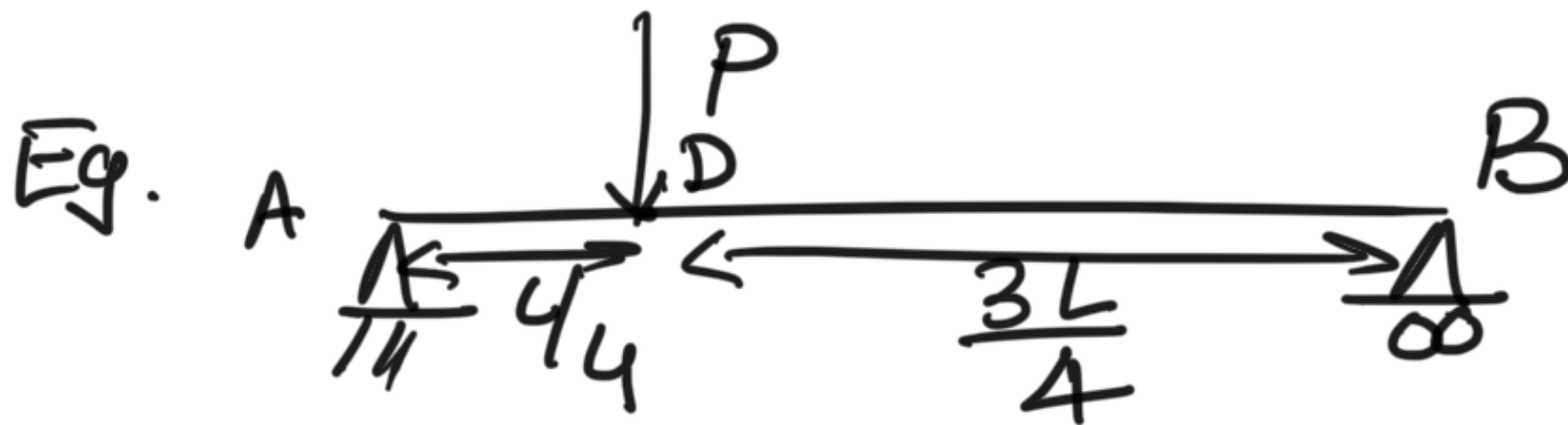
$$\frac{dM}{dx} = V \Rightarrow \frac{d^3 y}{dx^3} = \frac{V(x)}{EI}$$

$$\frac{dV}{dx} = -w \Rightarrow \frac{d^4 y}{dx^4} = -\frac{w(x)}{EI}$$

At free end, $V = 0$

$$M = 0$$

On simply supported end $M = 0$



Eqbm.

$$3P/4$$

14

$$A \text{ to } D: x < \frac{L}{4} \Rightarrow m = \frac{3P}{4}x$$

$$EI \frac{d^2 y_1}{dx^2} = \frac{3P}{4}x$$

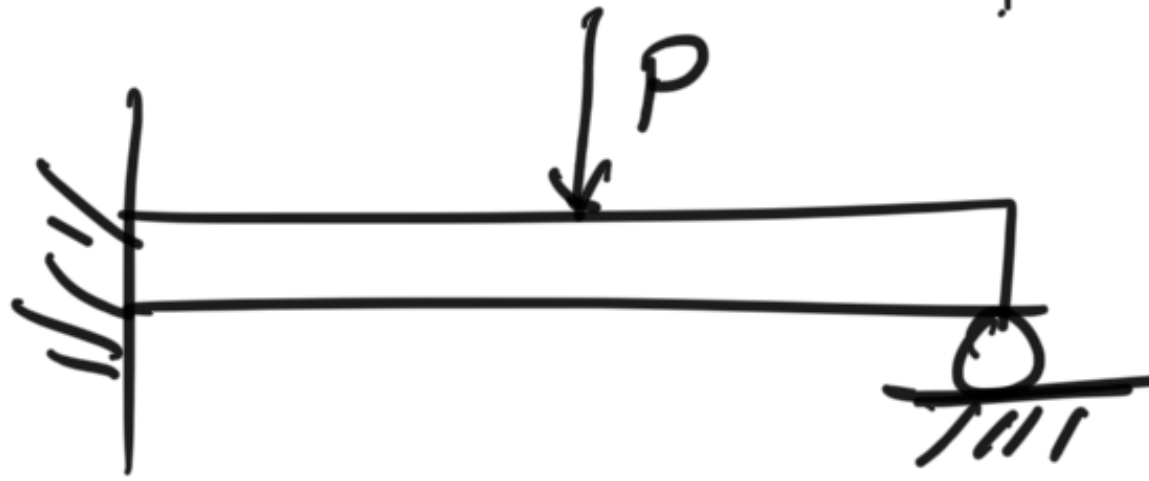
$$EI y_1 = \frac{Px^3}{8} + C_1 x + C_2$$

from D to B:

$$\begin{aligned} m(x) &= \frac{3Px}{4} - P\left(x - \frac{L}{4}\right) \\ &= \frac{P}{4}(L - x) = EI \frac{d^2 y_2}{dx^2} \end{aligned}$$

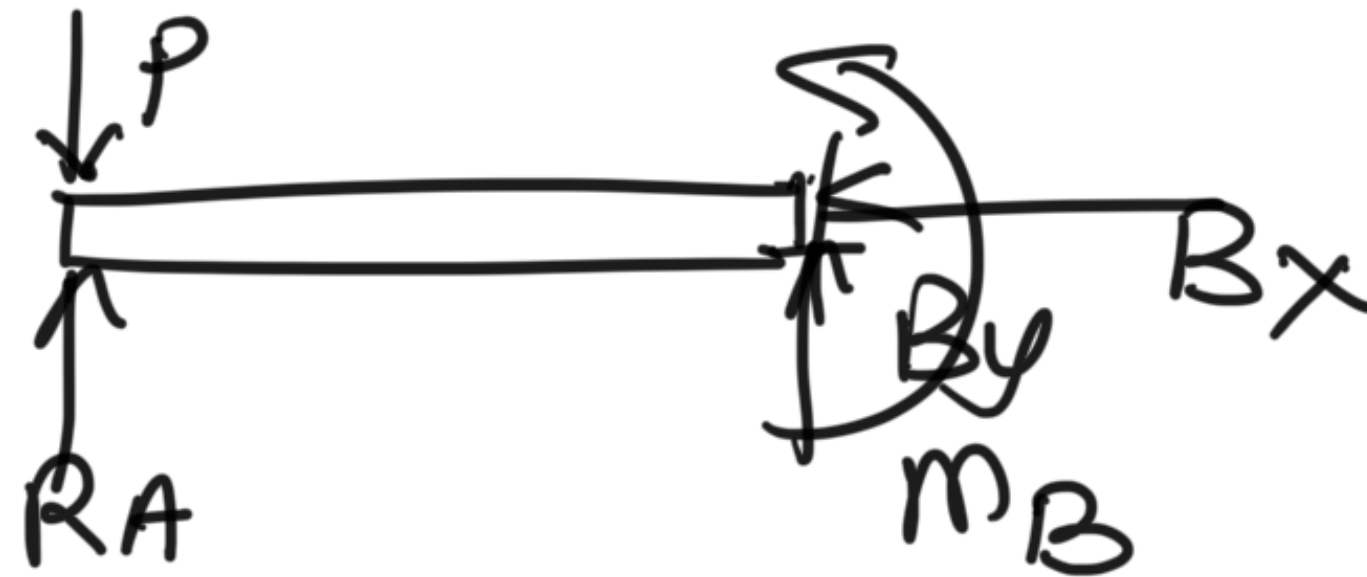
$$y_2 = -\frac{Px^3}{24} + \frac{PL}{8}x^2 + C_3 x + C_4$$

statically indeterminate problem



eg. of statically
indeterminate
problem.

eg. 2



$$m = (R_A - P) x.$$

$$EI \frac{d^2 y}{dx^2} = (R_A - P) x$$

$$EI y = (R_A - P) \frac{x^3}{6} + C_1 x + C_2$$

$$\left. \begin{array}{l} y(0) = 0, \\ y(L) = 0 \\ \theta(L) = 0 \end{array} \right\} \begin{array}{l} \text{get } R_A \\ C_1, C_2 \end{array}$$