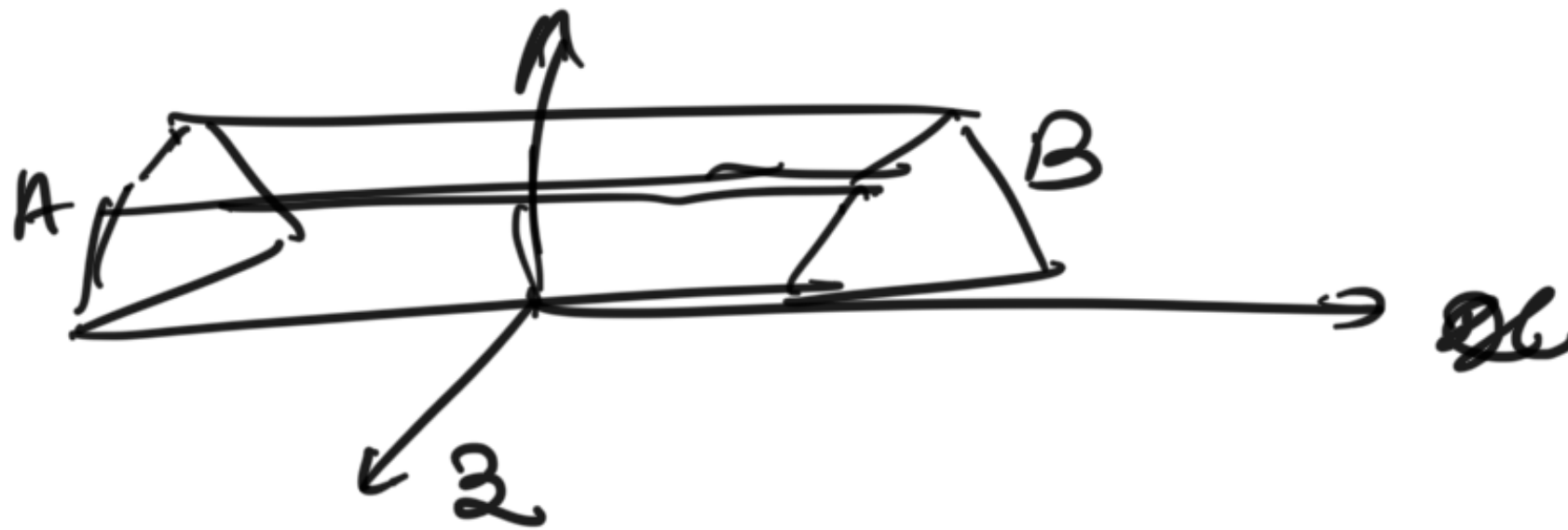


Bending

Bending of a slender prismatic member (bar)



slender \rightarrow x dimension $\gg y$ and z

Bending is caused by
in above configuration.
Torsion.

moments along z and y axis
Moment along x axis cause

M_z :

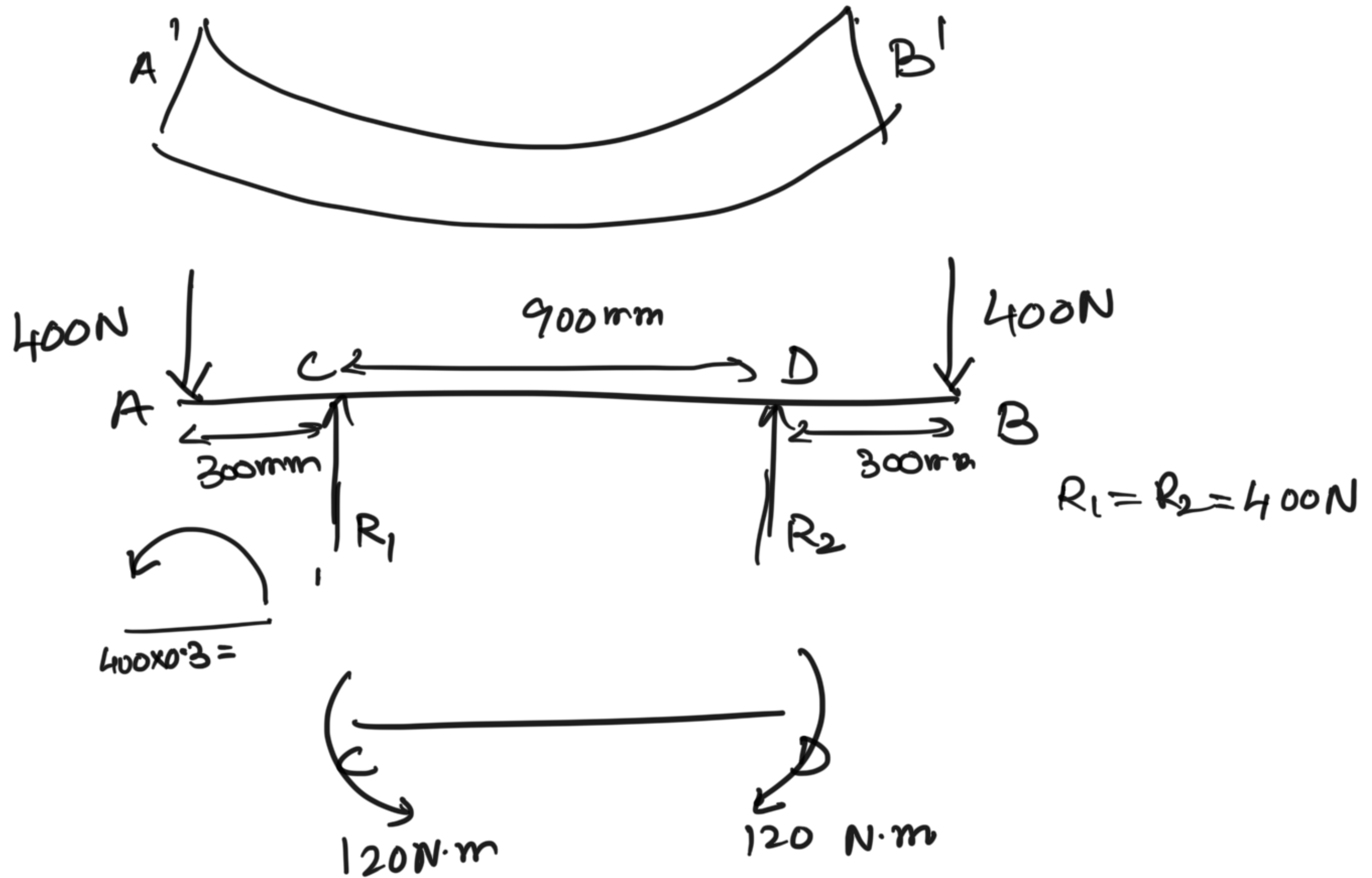
Bending moment M_z acts on a
prismatic member



Along the bar only couple (moment) M and M' act. No force.

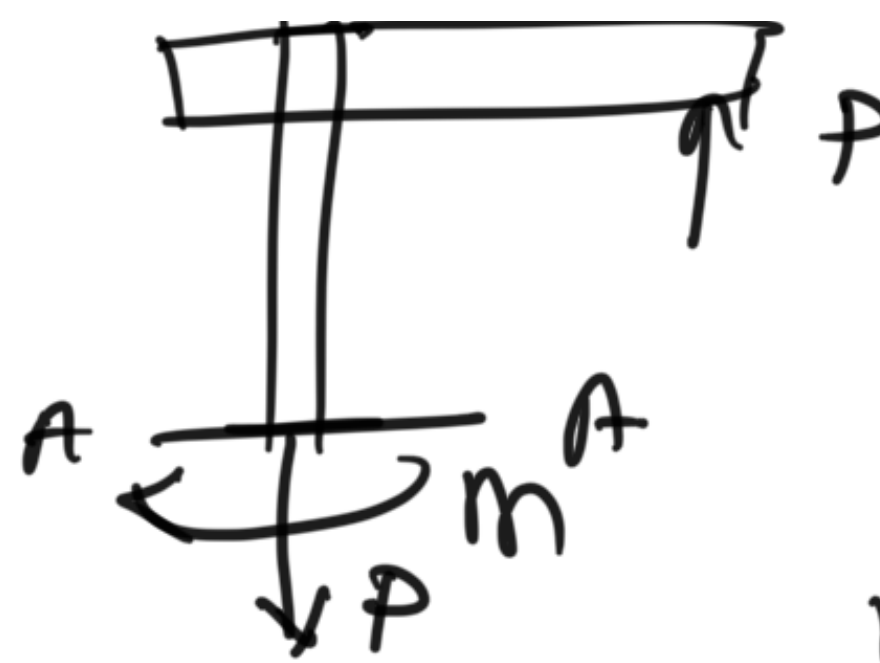
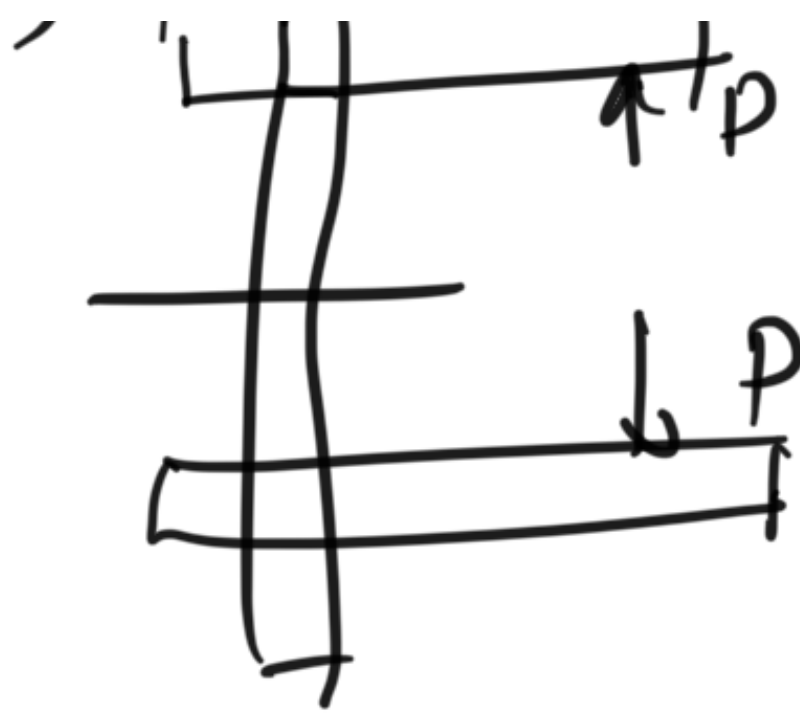
$m = m'$ (equilibrium)
Pure Bending





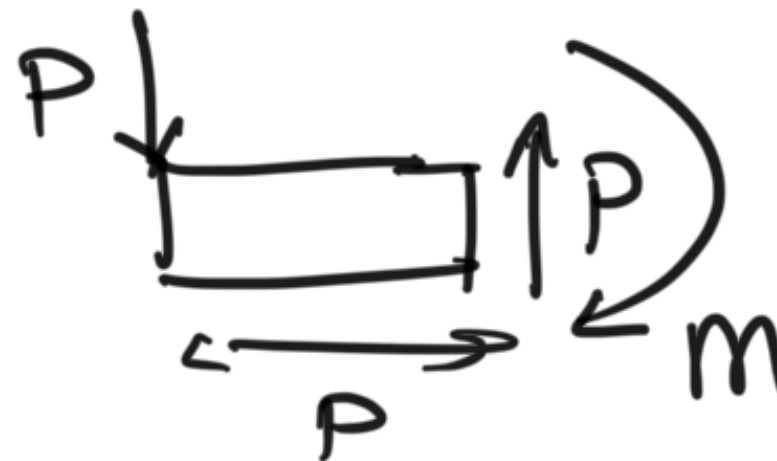
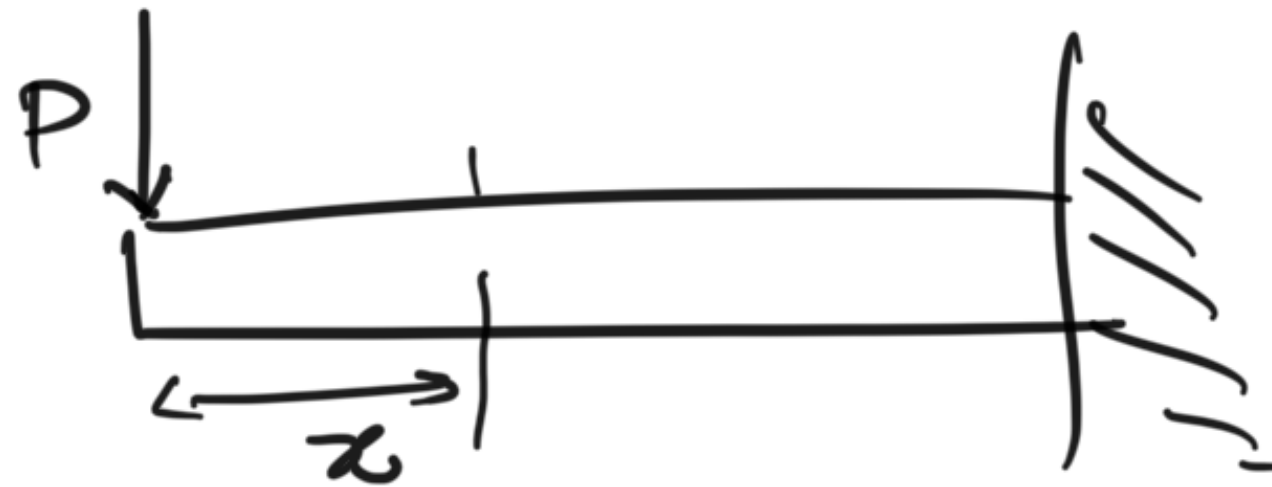
other modes of bending (not pure bending)





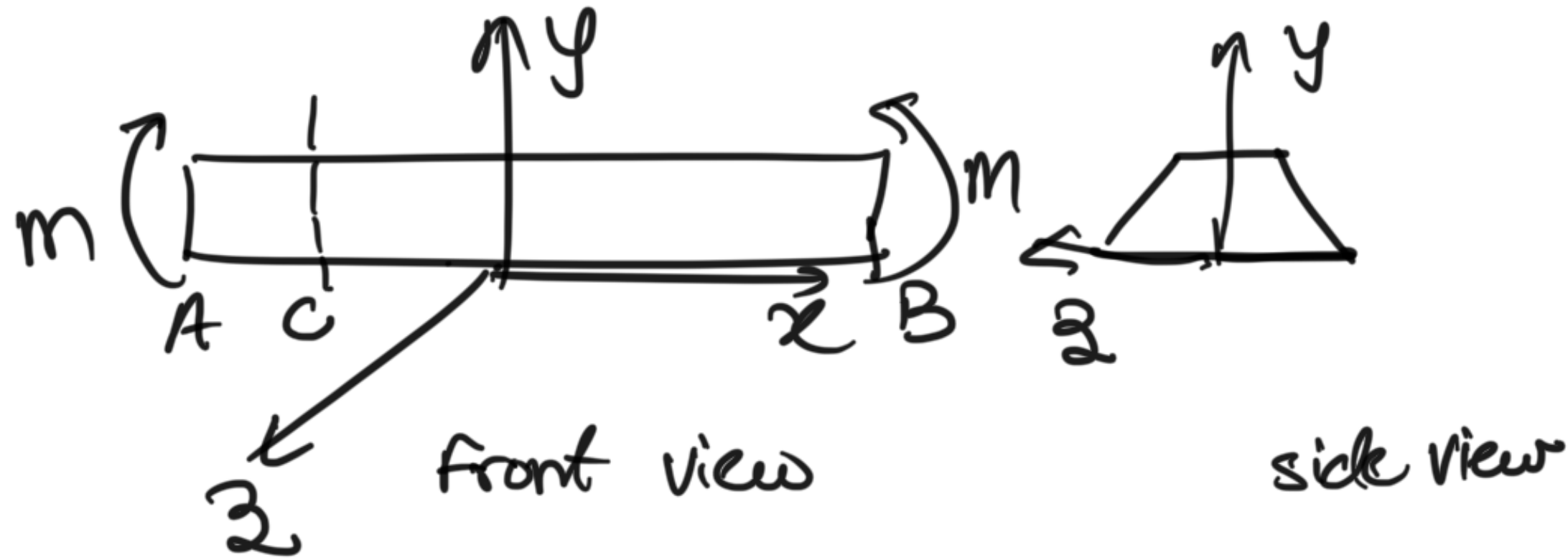
Force / moment
at AA
 $m = Pd$

b) Beam in transverse loading



$$m = Px$$

Symmetric members in pure bending



xy plane of symmetry.

section passing through C



loading on AC
resultant

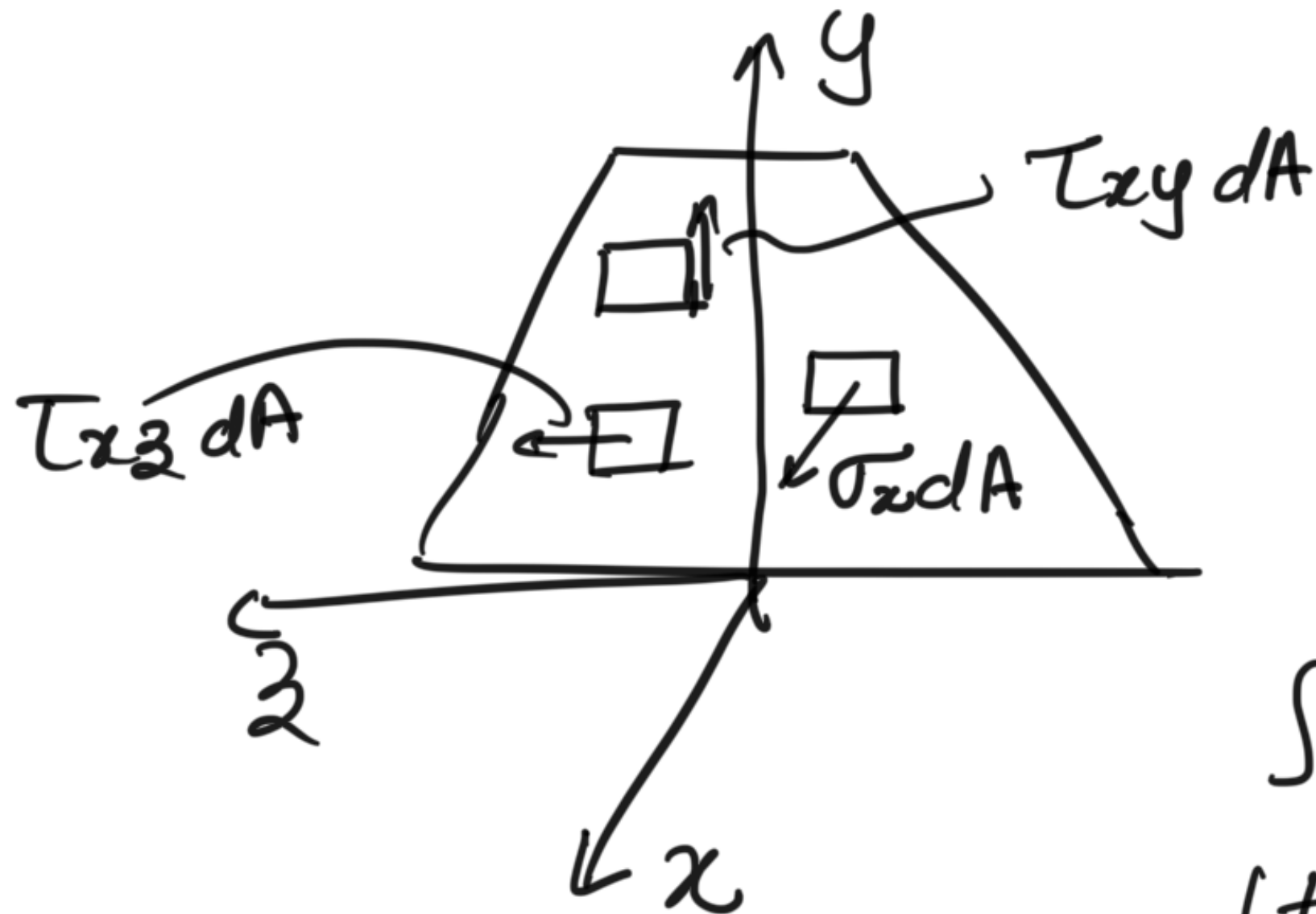
(internal force system at C
= M)



Bending is shown

m is true.
 (on a positive face
 m is CCW, then
 m is positive)

from Bends the bar concave upwards



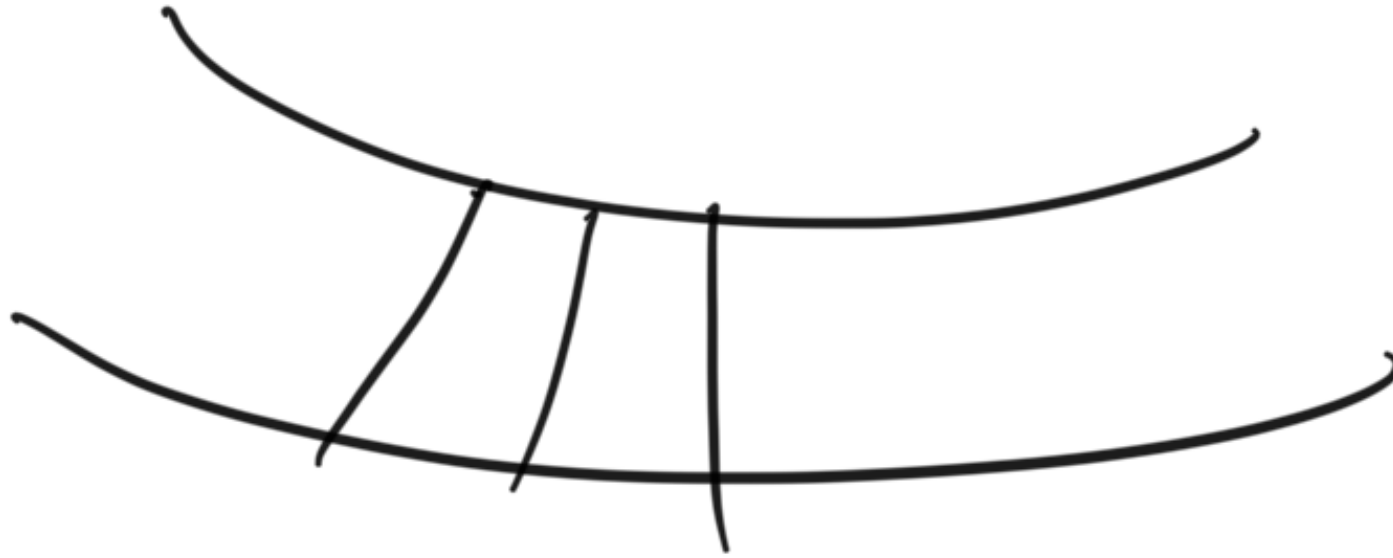
$$\int \sigma_x dA = F_x$$

(tensile σ_x)

$$\int y \sigma_x dA = -M$$

$$\int \tau_{xy} dA = F_y = 0$$

$$\int T x_2 dA = 0$$



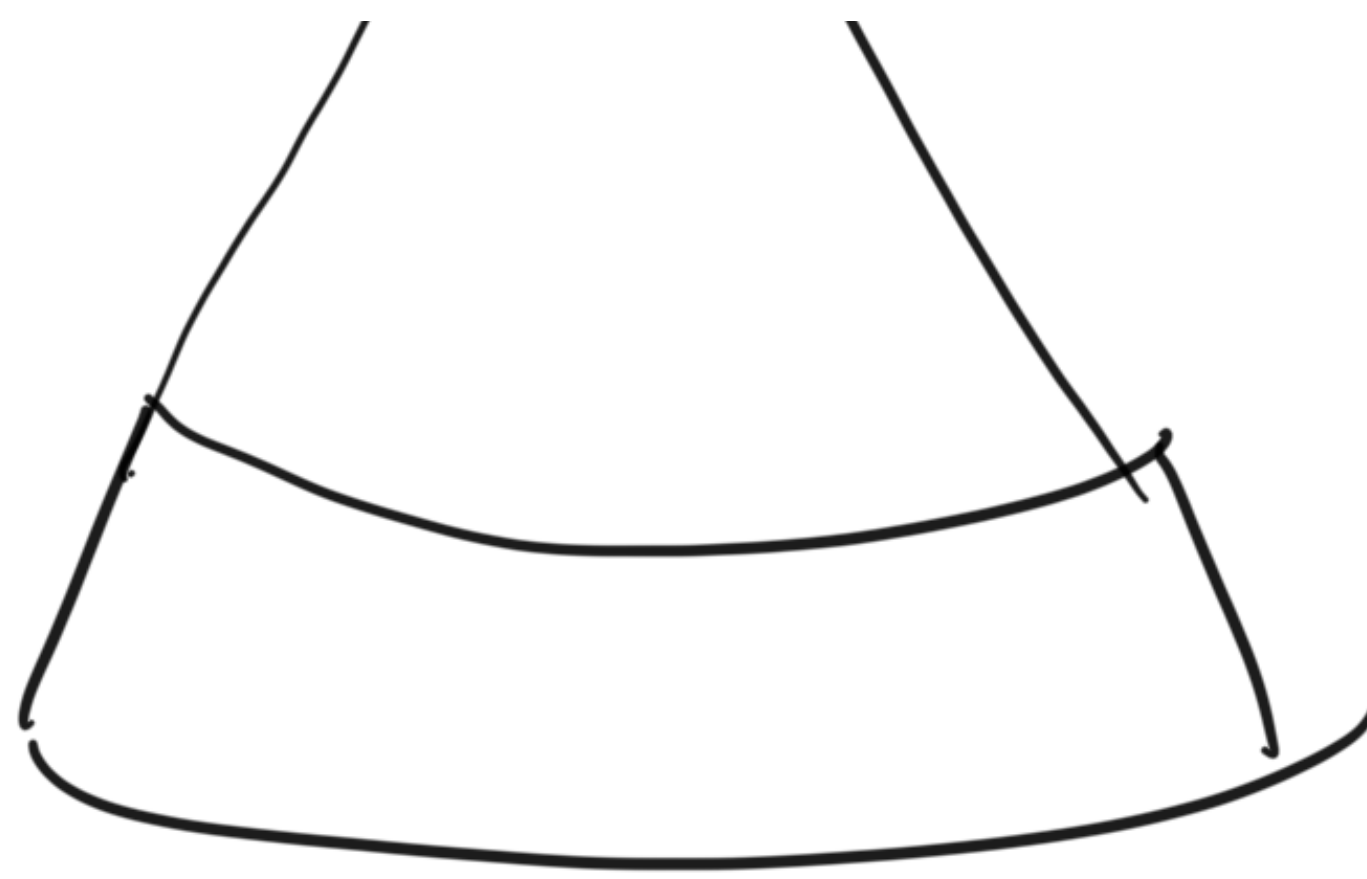
couple M acts on plane of symmetry.

Member will bend but stay symmetric w.r.t. xy plane. So the member bends uniformly.

Any cross section \perp axis remains planar and the plane passes through C , Centric of curvature.



straight member



straight member
AB
bends to the
shape of a
circular arc
under
pure bending.

On surface of member, $\sigma_y, \sigma_z, \tau_{yz} = 0$

only non zero element of stress = σ_x
all other stresses for a symmetric beam in pure
bending are equal to zero ($\sigma_y = \sigma_z = \tau_{xy} = \tau_{yz}$
 $= \tau_{xz} = 0$)



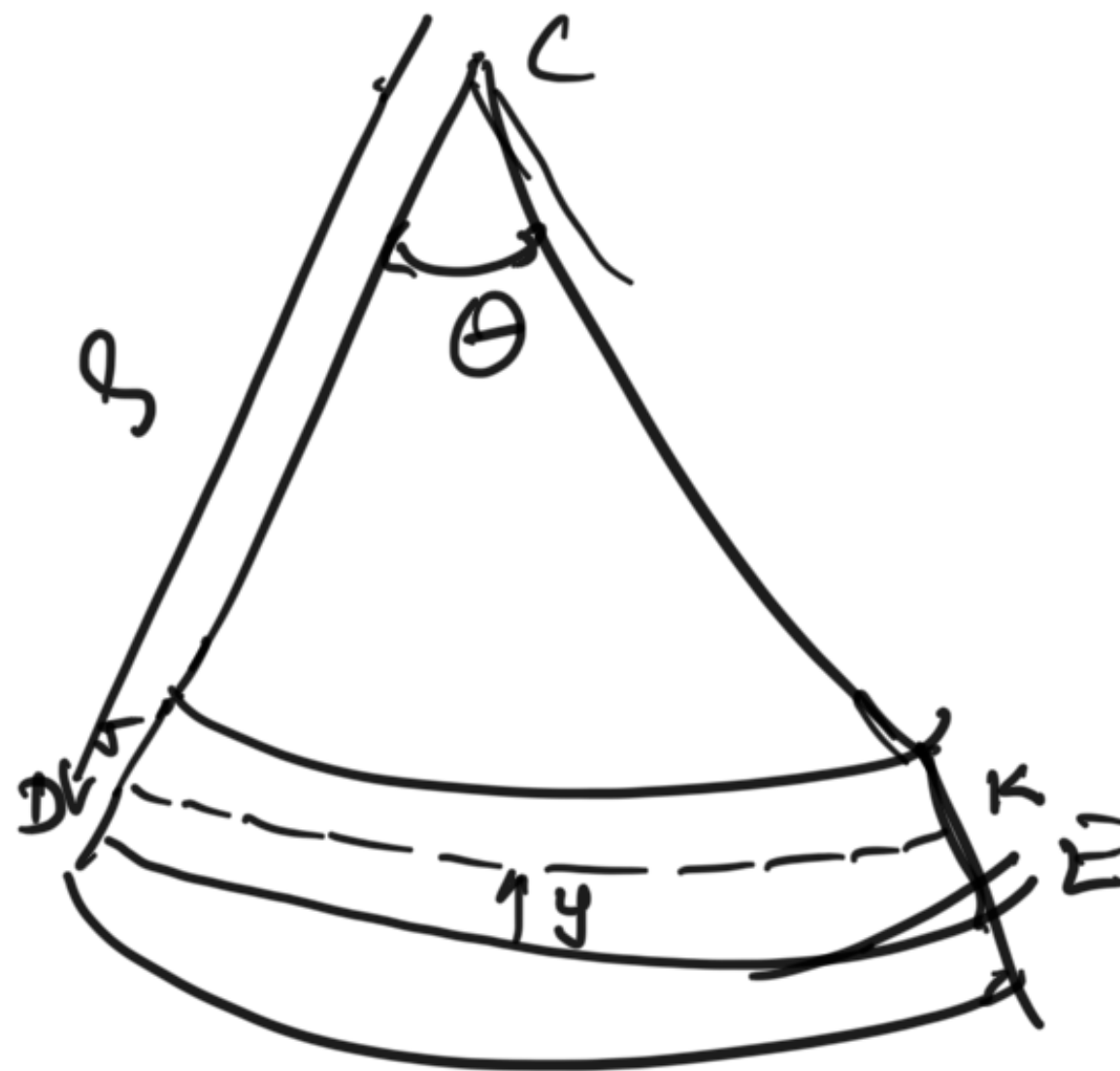
$$\epsilon_x > 0$$

$$\Rightarrow \sigma_x > 0$$

state of uniaxial stress (but not uniform)

There must be a surface \parallel x axis where $\epsilon_x = 0$

NEUTRAL SURFACE ($\sigma_x = 0$)



← neutral surface

Arc DE intersects a transverse section along a straight line \parallel z axis \rightarrow neutral axis.

C in centre of curvature. $\rho \rightarrow$ distance from C to D.

Arc Length $DE = \rho \theta = L$

arc JK located y above neutral axis,

$$JK = (\rho - y) \theta = L'$$

$$\delta = L' - L = (\rho - y) \theta - \rho \theta = -y \theta$$

$$\epsilon_x = -\frac{y \theta}{L} = -\frac{y \theta}{\rho \theta} = -\frac{y}{\rho}$$

-ve sign because bending moment is +ve & beam concave upwards.

ϵ_x varies linearly with y .

$|\epsilon_x|$ maximum when y is largest.

Denote largest y as c

$$\epsilon_m = \frac{C}{\rho} \Rightarrow \frac{1}{\rho} = \frac{\epsilon_m}{C}$$

$$\epsilon_x = -\frac{y}{\rho} \Rightarrow \epsilon_x = -\frac{y}{C} \epsilon_m$$

Elastic range $\sigma_x = E \epsilon_x$

$$E \epsilon_x = -\frac{y}{C} (E \epsilon_m)$$

$$\sigma_x = -\frac{y}{C} \sigma_m$$

σ_m = absolute maximum value of stress.

stress varies linearly with distance from neutral axis.

$$\int \sigma_x dA = 0 \Rightarrow \int -\frac{y}{C} \sigma_m dA = 0$$

$$\Rightarrow -\frac{\sigma_m}{c} \underbrace{\int y dA}_{=0} = 0$$

Neutral axis passes through centroid of cross section for
 a) elastic range
 b) pure bending

$$\int -y \sigma_x dA = M$$

if z axis coincides with neutral axis

$$\int -y \left(-\frac{y}{c} \right) \sigma_m dA = M$$

$$\frac{\sigma_m}{c} \int y^2 dA = M$$

$\int y^2 dA \rightarrow$ second moment of inertia

$$\sigma_m = \pm \frac{Mc}{I}$$

$$\sigma_x = - \frac{My}{I}$$

Elastic flexural
formulae

σ_x compressive above
Neutral axis

σ_x tensile below
Neutral axis

$$\frac{I}{c} = S \text{ (section modulus)}$$