

# STRUCTURAL ANALYSIS PORTFOLIO

**Draft by**

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**Abstract**

The presented document presents a selection of numerical models which I carefully validated by comparing the results either to experimental or analytically-derived ones.

**Reviews**

Rev.00 – July 2023

**Repository**

<https://github.com/amarchisella/STR.ANALYSIS>

# INTRODUCTION

## Preface

*Since a large number of mechanisms of resistance control the behaviour/strength of structural concrete, it is important to validate NLFEA (Note. Non-Linear-Finite-Element-Analysis) programs for the type of behaviour anticipated in the structure being designed or analyzed. This is best achieved by the development of a database of personally conducted and well-documented model calibration and validation efforts on a suite of NFLEA programs. Over time, the user will develop a measure of the strengths and limitations of each NLFEA program and develop appropriate global safety factors for each program.* (FIB. Bulletin 45 - Practitioners' Guide to Finite Element Modelling of Reinforced Concrete Structures. Vol 1. Lausanne, Lausanne, Switzerland; 2008. doi:10.1017/CBO9781107415324.004)

The presented document was mainly inspired by the previous statement which, although it refers specifically to non-linear-finite-element-analysis of reinforced-concrete structures, I believe applies generally to numerical structural analysis. In this regard, I briefly present a selection of numerical models which I carefully validated by comparing the results either to experimental or analytically-derived (as well as numerically-derived) ones.

Reinforced concrete (RC) structures are the ones which I addressed the most because they represented my core business during my PhD and Post-Doc period at Politecnico di Milano. Nevertheless, I tried increase my general confidence level in numerical models by addressing other structural problems when there was the chance, e.g. preparation of practices for MS courses at the University, freelance jobs, spare time.

Either global (load-to-displacement curves) or local (stress-to-strain) results were used in validating numerical models. Frequently experimental results are given only for the former. Further, because the lack of accuracy numerically-derived stresses (strains) with respect to displacements and reactions (see Payen DJ, Bathe KJ. The use of nodal point forces to improve element stresses. *Comput Struct.* 2011;89(5-6):485-495. doi:10.1016/j.compstruc.2010.12.002), the effort to validate a numerical model based on local response is generally large.

Of course, validation of a model is not an immediate outcome. Most of the presented results were obtained after several hours of trials-and-errors. Those hours, according to my opinion, increased my level of confidence in modelling much more than any perfect match obtained in comparing numerical results to experimental ones.

# INTRODUCTION

## Plan of the Document

The document has different sections mainly based on the type of element used such as frame, plane, shell, brick. Each model is presented in a single page form in which the both main characteristics and results are given along with some comments on the model's peculiarity. The terminology used throughout the document is summarized in the next page. Besides, pie-charts of the database are available subsequently.

For the sake of clarity, the Reader is invited to refer to the colour version of this document. Generally for plots, in comparing experimental results to numerical ones the red colour is used for the latter (unless specified differently).

## Acknowledgements

Most of the structural analysis were developed during my research work carried out at Politecnico di Milano where I took advantage of the availability of academic licenses for structural analysis software, such as SAP-2000, STRAUS-7, ATENA, R-FEM.

Additionally, for RC structures I used profoundly software developed by E. Bentz at University of Toronto (see <https://www.hadrianworks.com/>) which are freely distributed. Besides, I developed a FEM solver (using plate elements) for the column's base plate which is going to be embedded (at the date a testing version has been released) in calculation software for metal fasteners.

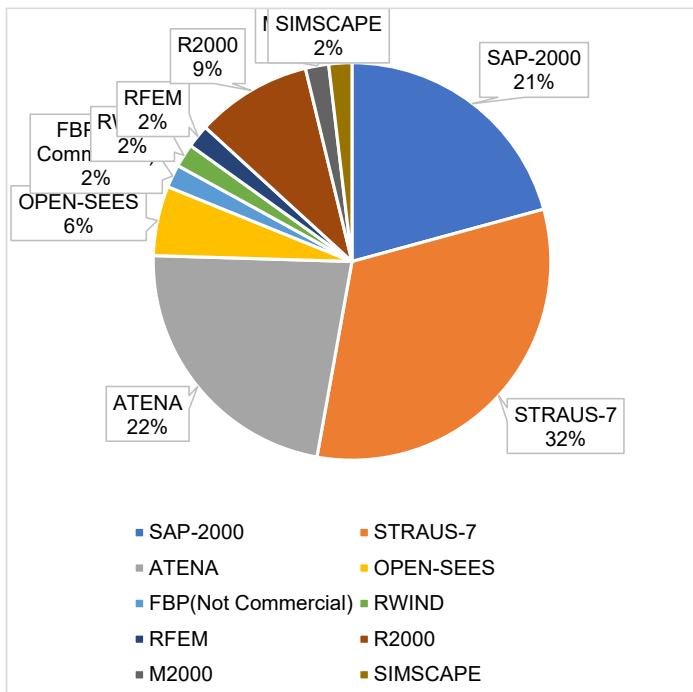
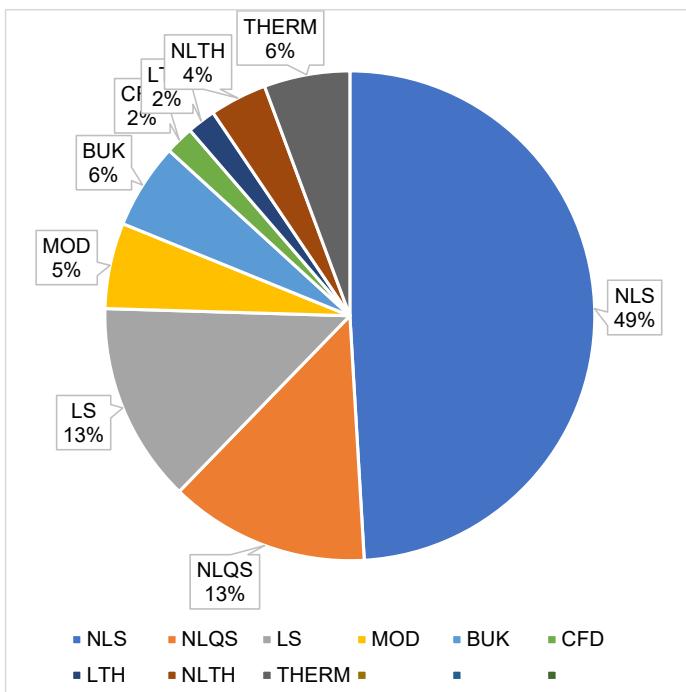
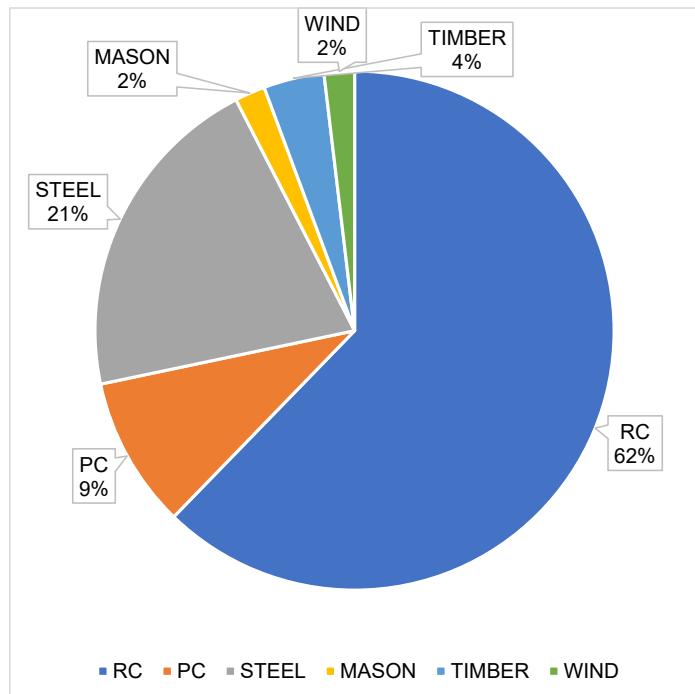
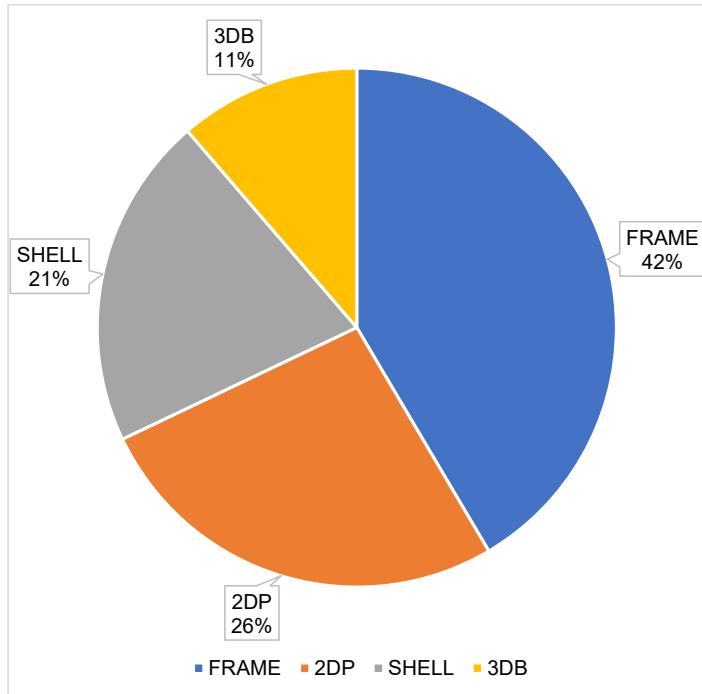
Finally, either experimental or numerical results used for comparison were retrieved from publications which I have surveyed. In many cases, results were digitally-re-derived by using GetDataDigitizer software.

# INTRODUCTION

## Pie charts

The following pie-charts represent the database (53 items) based on the following tags:

- Elements, i.e. frame, shells, two-dimensional plane stress (2DP), three-dimensional brick (3DB).
- Material, i.e. reinforced concrete (RC), prestressed concrete (PC), masonry, timber, steel.
- Material law, i.e. linear-elastic (LE), non-linear (NL).
- Type of analysis, i.e. linear-static (LS), non-linear static (NLS), non-linear quasi-static (NLQS), modal (MOD), buckling (BUCK), computational-fluid-dynamics (CFD), linear time-history (LTH), non-linear time-history (NLTH); thermal (THERM).



# FORM AND TERMINOLOGY

Source	
Elements	
Software	
Material	
Analysis	
Reference Model [Experimental]	
Reference Model [Numerical]	
Model	Results
Comments	

Reference is made to the available experimental results used for comparison with respect to the numerical model. NA, Not-Applicable.

Reference is made to the available numerical results used for comparison with respect to the numerical model. NA, Not-Applicable.

SECTION	TITLE
	<p>[Personal Archive]: The analysis was carried out either for research or professional job, results are not public.  [Published]: Results were published. Reference to the publication is given.</p>
	<p>[FRAME]: Linear element with 2 nodes and 12 dofs.  [2D PLANE STRESS]: Quadrilateral elements with 4 nodes and 8 dofs. Occassionally, refined to 8 nodes and 16 dofs.  [3D BRICK]: Hexagonal elements with 8 nodes and 16 dofs.  [PLATE]: Quadrilateral elements with 4 nodes and 12 dofs.  [SHELL]: Quadrilateral elements with 4 nodes and 20 dofs.</p>

<p>[SAP2000]: CSI. CSI Analysis Reference Manual. For SAP2000, ETABS, SAFE, CsiBridge [Version 2017]; 2017.  [ATENA]: Cervenka V, Jendele L, Cervenka J. ATENA Program Documentation Part 1 Theory. Atena. 2012:1-282.  [RFEM]: Dlubal. Rfem 5 - User Manual. 2016;(February):590.  [STRANZ 7]: Strand7. Using Strand7/Straus7. Introduction to the Strand/Straus7 Finite Element Analysis System. 2010. www.strand7.com.  [RESPONSE/MEMBRANE-2000]: 1. Bentz EC. Sectional analysis of reinforced concrete members. 2000. <a href="https://hdl.handle.net/1807/13811">https://hdl.handle.net/1807/13811</a>.  [FLEXIBLE BASE PLATE]: Developed by A. Marchisella as freelance. The software solves through FEM analysis, using PLATE elements, column's base plate attached to concrete foundation via fasteners. Technical documentation is available upon request.  [OPEN SEES]: McKenna F. OpenSees: A framework for earthquake engineering simulation. Comput Sci Eng. 2011;13(4):58-66.  doi:10.1109/MCSE.2011.66  [Stated otherwise].</p>
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<p>[Linear Elastic]: Characterized by Young's Modulus and Poisson Ratio.  [Non-Linear Concrete (MCFT)]: Cervenka V, Jendele L, Cervenka J. ATENA Program Documentation Part 1 Theory. Atena. 2012:1-282.  [Non-Linear Concrete (PLAS)]: Chen WF. Plasticity in Reinforced Concrete. J. Ross Publishing; 2007.  [Non-Linear Steel]: Unless otherwise stated, elasto-plastic + hardening is assumed.  [Non-Linear Spring]: Analytically-derived Force-to-Displacement constitutive law.</p>
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<p>[Linear Static]  [Non-Linear Static]{Max absolute residual error 10<sup>-2</sup>}  [Non-Linear Quasi-Static] {Max absolute residual error 10<sup>-2</sup>}  [Modal Response Spectrum]  [Linear Time-History]  [Non-Linear Time History] {Max absolute residual error 10<sup>-2</sup>}  [Buckling]  [Thermal]</p>
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# **FRAME and MULTI-SPRINGS**

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME(Truss)
<b>Software</b>	SAP2000
<b>Material</b>	Linear-Elastic
<b>Analysis</b>	Linear-Static
<b>Reference Model [Experimental]</b>	NA
<b>Reference Model [Analytic./Num.]</b>	Collins MP, Mitchell D. Prestressed Concrete Structures. Englewood Cliffs: Prentice-Hall International; 1991.

### Investigated Structure / Model

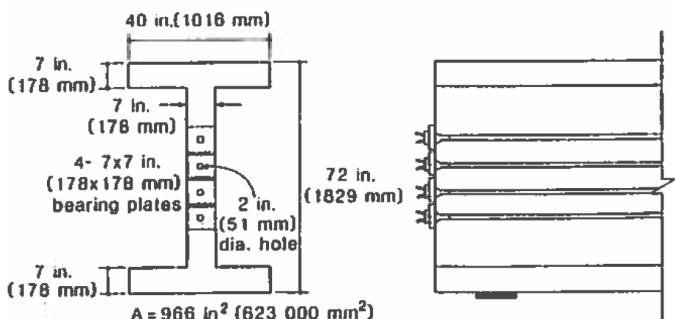
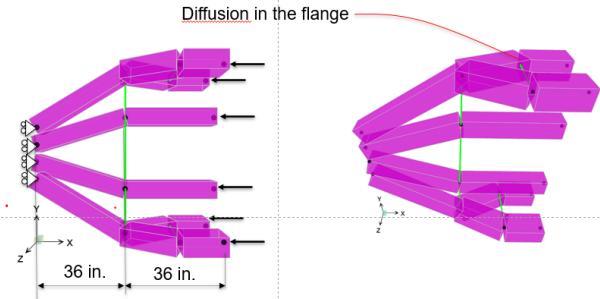


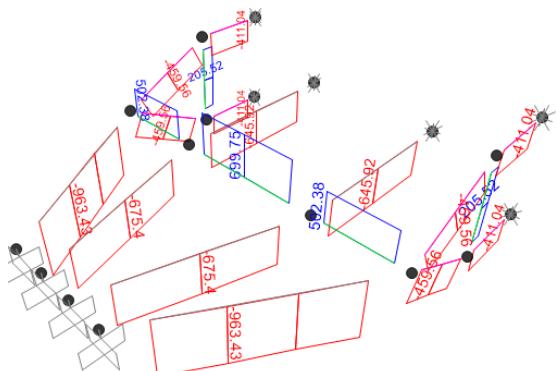
Figure 9-26 Details of anchorage region in post-tensioned I-beam.



### Results

#### Strut and Tie model (After Cracking)

Segm.	Pos.	Collins (kN)	AM (kN)	diff (-)
CD	web	564	502	-0.109
DE	web	774	700	-0.096
GH	flange	175	206	0.174



### Comments

The numerical investigation addressed anchorage zone of prestressed girder. Such diffusion zone (state of stress is not easy to derive) is analyzed using Strut-And-Tie approach. In this context concrete struts and reinforcement ties are introduced in an equivalent truss model. Axial forces derived from numerical model were compared with respect the values given in the reference.

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME / TENDONS
<b>Software</b>	SAP2000
<b>Material</b>	Linear-Elastic
<b>Analysis</b>	Linear-Static
<b>Reference Model [Experimental]</b>	NA
<b>Reference Model [Analytic./Num.]</b>	Collins MP, Mitchell D. Prestressed Concrete Structures. Englewood Cliffs: Prentice-Hall International; 1991.

### Investigated Structure / Model

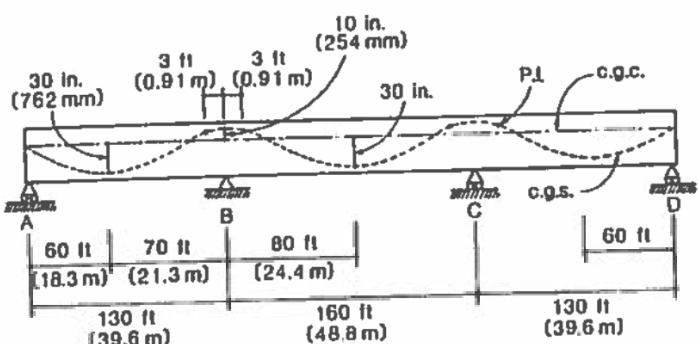


Figure 10-24 Three-span, post-tensioned bridge.

### Results

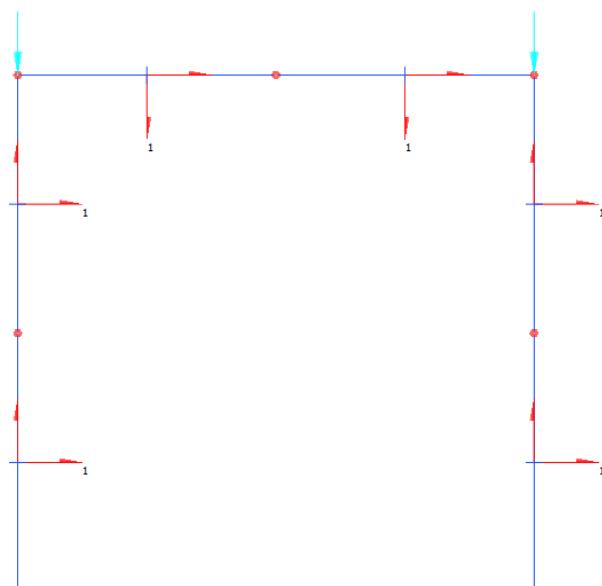
SPAN	Moment due to Redundancy		
	S2000 (kN·m)	Collins (kN·m)	Err. (-)
A-B	10707	10699	-0.001
B-C	10707	10699	-0.001

### Comments

The numerical investigation addressed redundant prestressed girder. Parabolic tendon element are used. Redundant bending moments in nodes B and C are compared with respect to values given in the reference.

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME
<b>Software</b>	STRAUS-7
<b>Material</b>	Linear-Elastic
<b>Analysis</b>	Buckling
<b>Reference Model [Experimental]</b>	NA
<b>Reference Model [Analytic./Num.]</b>	Bleich F. Buckling Strength of Metal Structures. New York: McGraw-Hill; 1952. / 1. Corradi Dell'Acqua L. Meccanica Delle Strutture (Vol. 3) - La Valutazione Della Capacità Portante. Milano: McGraw-Hill; 1994.

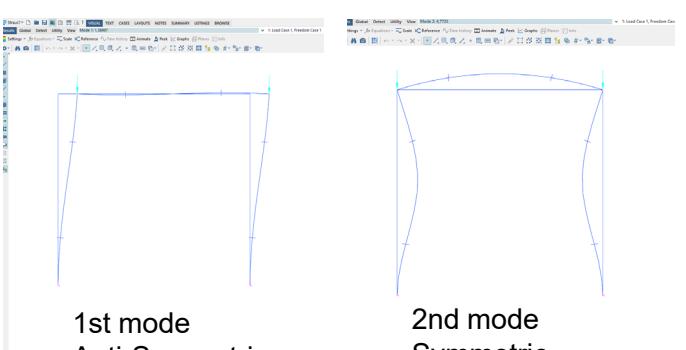
### Investigated Structure / Model



### Results

Esempio Corradi Paragrafo 17.3  
Portale Piano 3000x3000, sezione 100x100

Condition	LELE (mm)	pa			ps		
		Bleich	Corradi	FEM	Bleich	Corradi	FEM
HINGED	3000	1.826	1.837	1.825	12.890	12.689	16.870
HINGED	1500	1.826	1.837	1.821	12.890	12.689	13.014
HINGED	750	1.826	1.837	1.820	12.890	12.689	12.903
CLAMPED	3000	7.382	7.447	7.441	25.167	25.379	44.999
CLAMPED	1500	7.382	7.447	7.398	25.167	25.379	25.772
CLAMPED	750	7.382	7.447	7.377	25.167	25.379	25.247



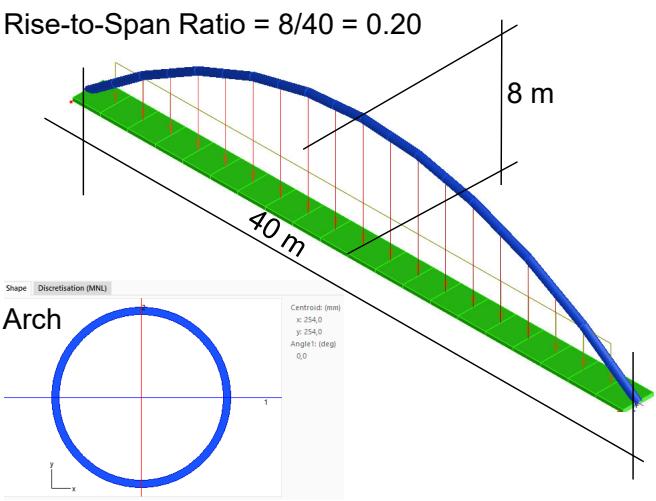
### Comments

The buckling multipliers numerically-obtained for the first and second buckling modes are compared with respect to analitically-derived ones. The effect of mesh refinement in the accuracy of the second buckling multiplier was evident.

Source	Personal Archive
Elements	FRAME
Software	STRAUS-7
Material	Linear Elastic Steel
Analysis	Buckling
Reference Model [Experimental]	NA
Reference Model [Analytic./Num.]	Kollar L. <i>Structural Stability in Engineering Practice</i> . London: E & FN Spon; 1999. / Bergmeister K, Capsoni A, Corradi L, Menardo A. Lateral elastic stability of slender arches for bridges including deck slenderness. <i>Struct Eng Int J Assoc Bridg Struct Eng.</i> 2009;19(2):149-154. doi:10.2749/101686609788220259

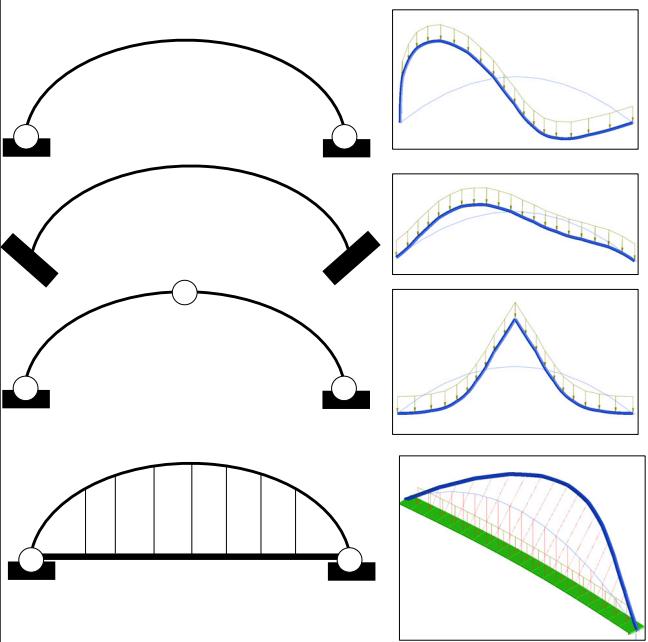
### Investigated Structure / Model

Rise-to-Span Ratio = 8/40 = 0.20



### Results

2-HINGE			CLAMPED			THREE-HINGED			HANGERS + DEF. DECK		
Th.	FEM	FEM/Th.	Th.	FEM	FEM/Th.	Th.	FEM	FEM/Th.	Th.	FEM	FEM/Th.
130	123	1.05	289	283	1.02	113	110	1.03	183	223	0.82

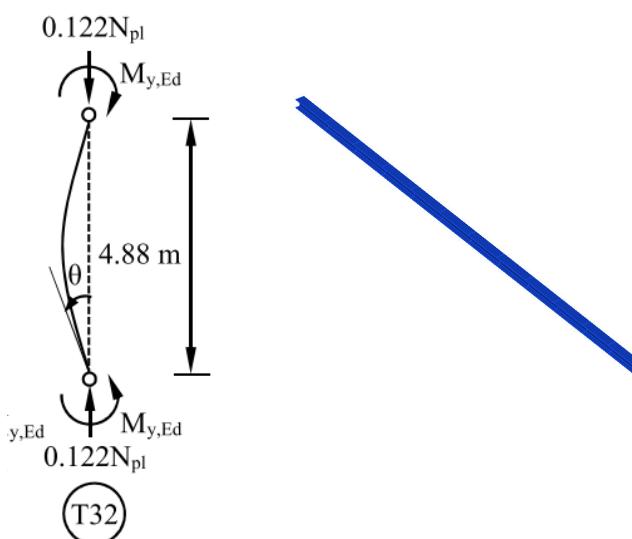


### Comments

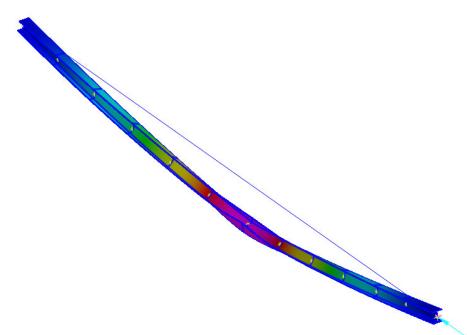
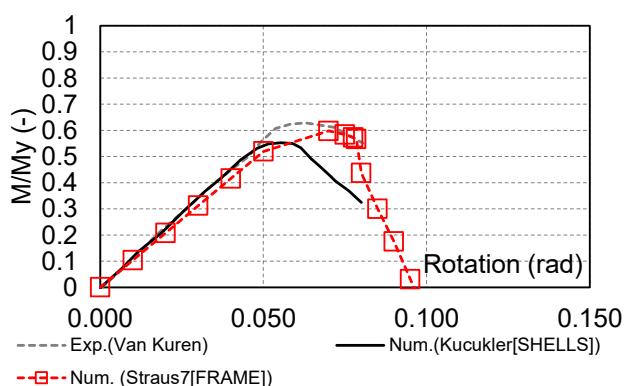
The numerical investigation addressed a steel arch (rise-to-span ration equal to 0.20) under gravity load-type. The investigation scope was to validate numerical buckling analysis results for different arch configurations, i.e. two-hinges, clamped, three-hinges, with a hangers and deformable deck. Results were compared with respect to analytical predictions showing good agreement. The case with hangers (lateral buckling) is particularly sensible to variation of bridge deck bending stiffness out-of-plane.

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME
<b>Software</b>	Straus-7
<b>Material</b>	Non-Linear (Elasto-Plastic [Von-Mises])
<b>Analysis</b>	Non-Linear (Material+Geometry)
<b>Reference Model [Experimental]</b>	Reported by Kucukler M, Gardner L, Macorini L. Flexural-torsional buckling assessment of steel beam-columns through a stiffness reduction method. <i>Eng Struct.</i> 2015;101:662-676. doi:10.1016/j.engstruct.2015.07.041
<b>Reference Model [Analytic./Num.]</b>	Kucukler M, Gardner L, Macorini L. Flexural-torsional buckling assessment of steel beam-columns through a stiffness reduction method. <i>Eng Struct.</i> 2015;101:662-676. doi:10.1016/j.engstruct.2015.07.041

### Investigated Structure / Model



### Results



### Comments

The numerical investigation addressed a steel beam under compression and uniform bending moment. Such condition was adopted experimentally to promote flexural-torsional buckling. Although selection of frame elements might be dubious in case of flexural-torsional buckling (compared to shells) a refinement was made by considering a dense subdivision of the cross-section to allow spread of both material and geometrical non-linearities. Agreement was found with respect to experimental results.

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME
<b>Software</b>	STRAUS-7
<b>Material</b>	Non-linear (Elasto-Plastic Steel)
<b>Analysis</b>	Non-linear(Material+Geometry)
<b>Reference Model [Experimental]</b>	Perotti, Federico, and G. Paolo Scarlassara. 1991. "Concentrically Braced Steel Frames under Seismic Actions: Non-linear Behaviour and Design Coefficients." <i>Earthquake Engineering &amp; Structural Dynamics</i> 20 (5): 409–27. <a href="https://doi.org/10.1002/eqe.4290200503">https://doi.org/10.1002/eqe.4290200503</a> .
<b>Reference Model [Analytic./Num.]</b>	Perotti, Federico, and G. Paolo Scarlassara. 1991. "Concentrically Braced Steel Frames under Seismic Actions: Non-linear Behaviour and Design Coefficients." <i>Earthquake Engineering &amp; Structural Dynamics</i> 20 (5): 409–27. <a href="https://doi.org/10.1002/eqe.4290200503">https://doi.org/10.1002/eqe.4290200503</a> .

### Investigated Structure / Model

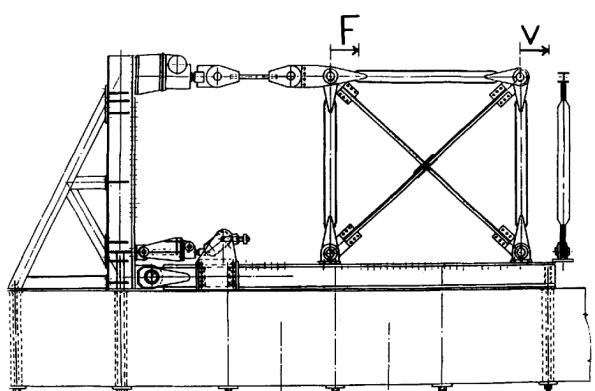
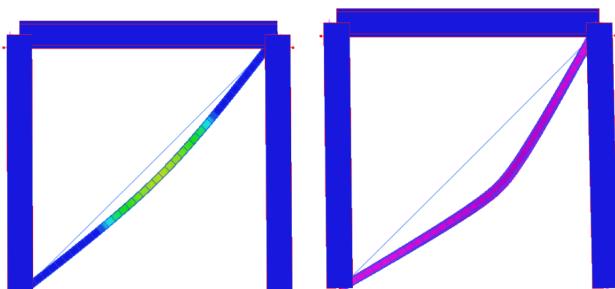
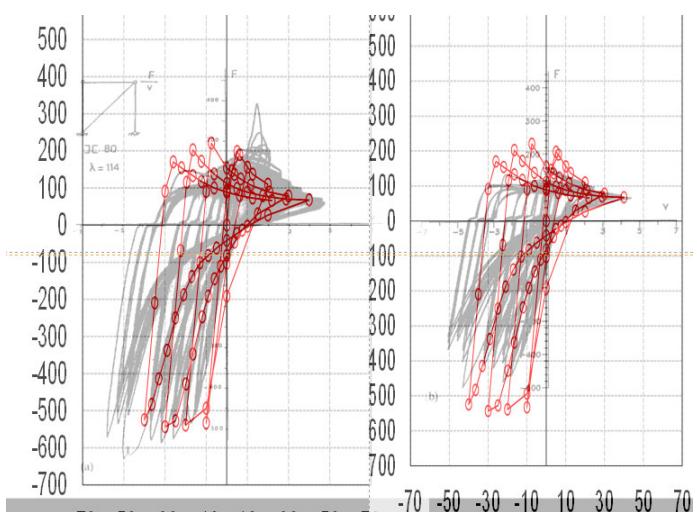


Figure 3. Experimental test on an X-braced pinned frame



### Results



Notes. Comparison between numerical (red) and experimental results (left) and numerically obtained by Perotti (right), both the reference curves are black. Load is given in (kN), displacements in (mm).

### Comments

The numerical investigation addressed a steel portal braced with a slender diagonal element. Such condition was adopted experimentally to promote buckling under reversal load condition (seismic). Numerical model uses frame elements. Initial imperfection to the diagonal element was equal to 1/1000 of its length according to the compared reference. Agreement was found with respect to experimental results.

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME
<b>Software</b>	RESPONSE2000
<b>Material</b>	Non-Linear Concrete(MCFT) / Non-Linear Steel (Rebar, Tendons)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	Oh BH, Kim KS. Shear Behavior of Full-Scale Post-Tensioned Prestressed Concrete Bridge Girders. ACI Struct J. 2004;101(2):176-182. doi:10.14359/13014
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model

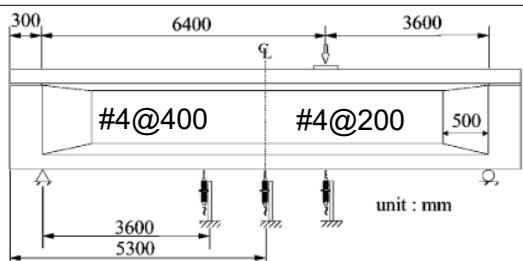
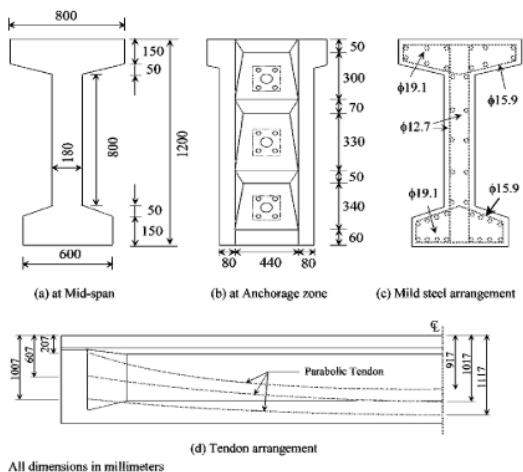


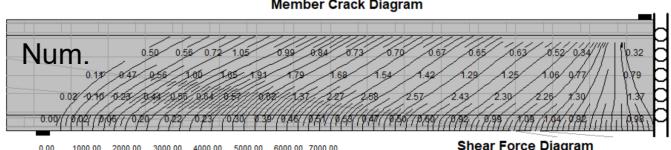
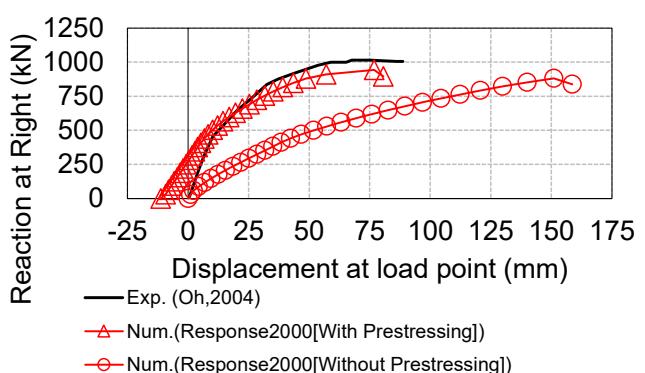
Fig. 1—Dimensions of test girder and loading arrangement.



### Comments

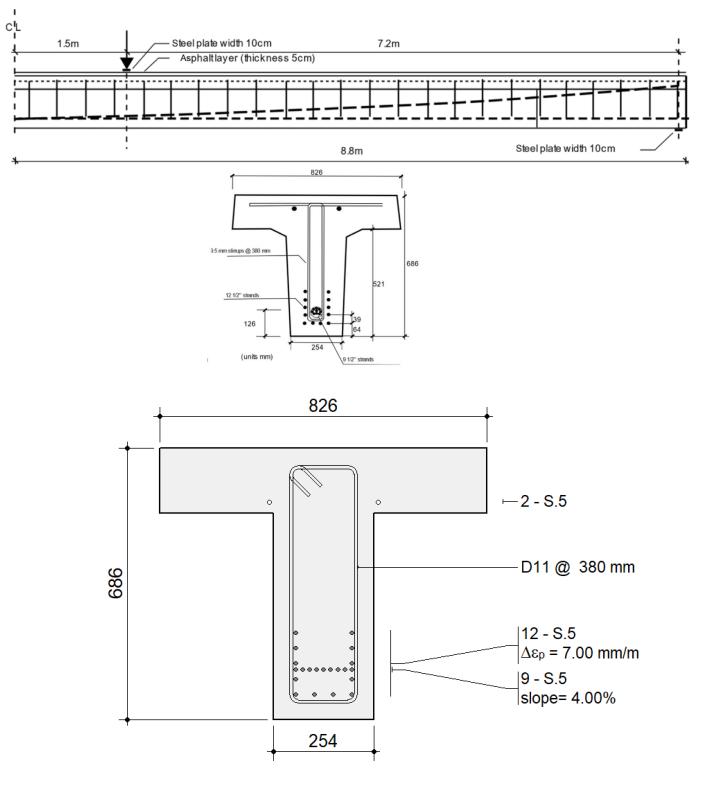
The numerical investigation addressed a prestressed beam under three-point bending test. The scope was to investigate the effect of prestressing in both load-carrying capacity and mode of failure. Results show that when prestressing is activated flexural failure is attained. Whereas shear failure is obtained without prestressing although comparable load-carrying capacities are numerically obtained. Finally agreement was found with respect to experimental results (with activated prestressing) apart from pre-camber effect at initial prestressing which was not measured during the experiments.

### Results

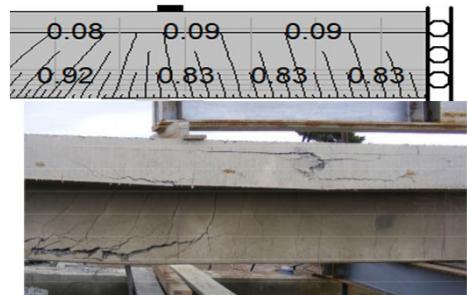
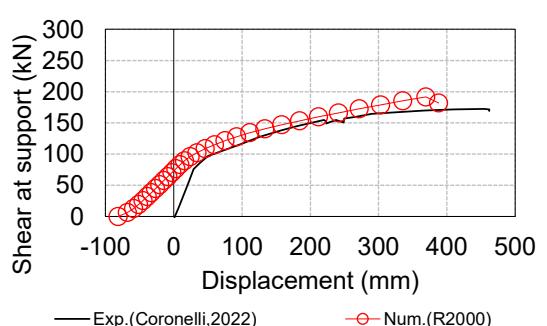


<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME
<b>Software</b>	RESPONSE 2000
<b>Material</b>	Non-linear concrete (MCFT)
<b>Analysis</b>	Non-linear static
<b>Reference Model [Experimental]</b>	Coronelli D, Mircea C, Rogers R, Rosati G, Consiglio AN. Structural assessment of prestressed beams with natural corrosion. Struct Concr. 2022;(June):1-15. doi:10.1002/suco.202200577
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



### Results

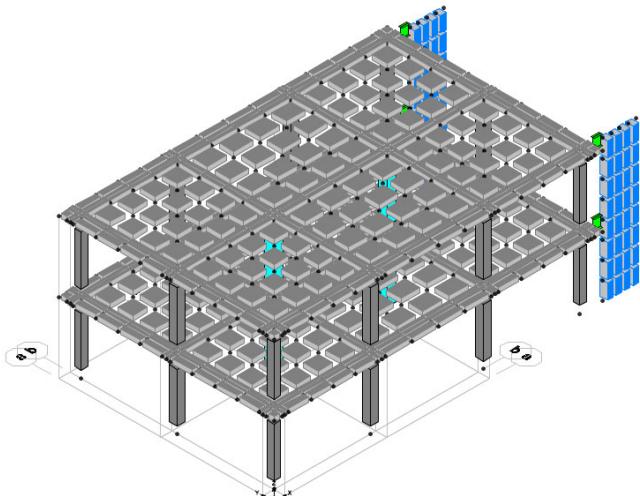


### Comments

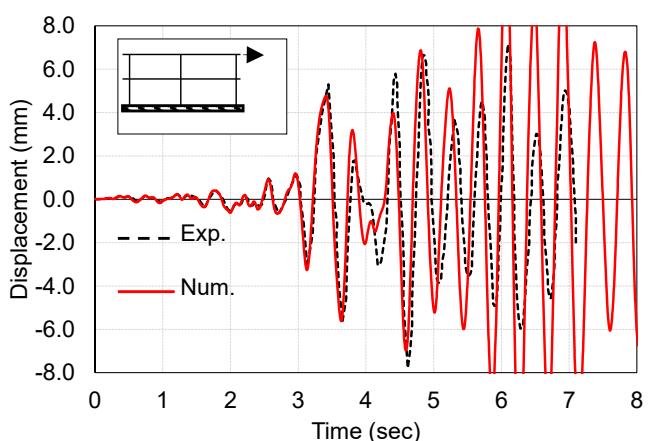
Similar discussion with respect to what was found for Oh's prestressed beams in a previous example.

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME/SHELLS
<b>Software</b>	SAP2000
<b>Material</b>	Linear Elastic
<b>Analysis</b>	Linear Time History
<b>Reference Model [Experimental]</b>	Coronelli D, Lamperti Tornaghi M, Martinelli L, et al. Testing of a full-scale flat slab building for gravity and lateral loads. Eng Struct. 2021;243(May):112551. doi:10.1016/j.engstruct.2021.112551
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



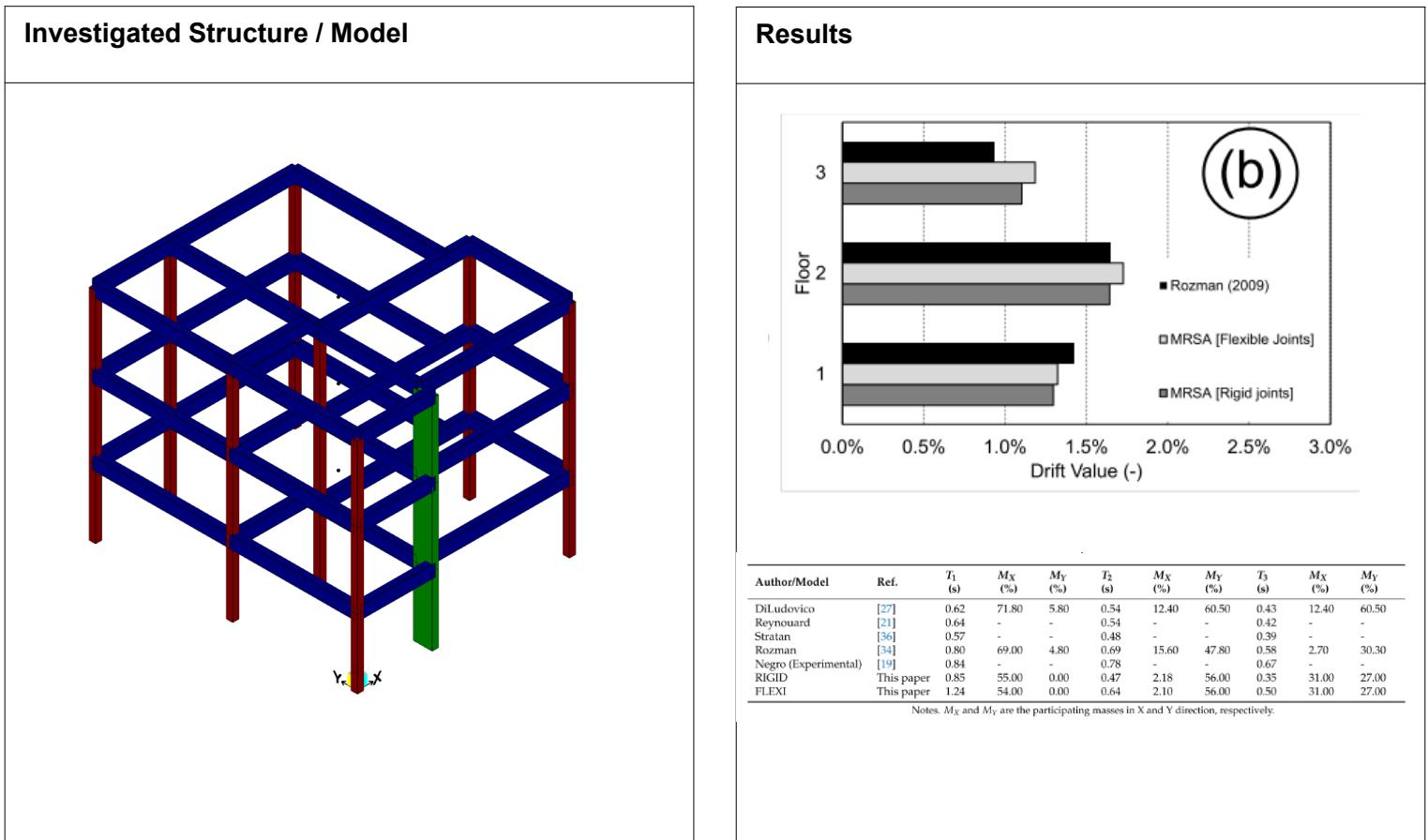
### Results



### Comments

The numerical investigation addressed a RC frame (flat slab type designed as secondary system) tested pseudo-dynamically. The test had the peculiarity of the adoption of two fictitious shear walls (numerically simulated during the test). Experimental behavior showed almost linear-elastic response without any evidence of damage under the application of a scaled earthquake time-history, thus linear-elastic material was assumed. The scope was to investigate the reliability of simple slab-to-column connections, i.e. only one node is shared. Although the dynamic period of the structure was comparable with respect to numerical results numerical displacements diverges most probably due to lack of accuracy on damping modeling.

<b>Source</b>	Marchisella A, Muciaccia G. Comparative Assessment of Shear Demand for RC Beam-Column Joints under Earthquake Loading. Appl Sci. 2022;(12). doi:10.3390/ app12147153
<b>Elements</b>	FRAME
<b>Software</b>	SAP2000
<b>Material</b>	Lumped Plasticity
<b>Analysis</b>	Modal Response Spectrum
<b>Reference Model [Experimental]</b>	Negro P, Mola E, Molina FJ, Magonette GE. Full-scale PsD testing of a torsionally unbalanced three-storey non-seismic RC frame. In: 13th World Conference on Earthquake Engineering. Vancouver; 2004.
<b>Reference Model [Analytic./Num.]</b>	Rozman M, Fajfar P. Seismic response of a RC frame building designed according to old and modern practices. Bull Earthq Eng. 2009;7(3):779-799. doi:10.1007/s10518-009-9119-4

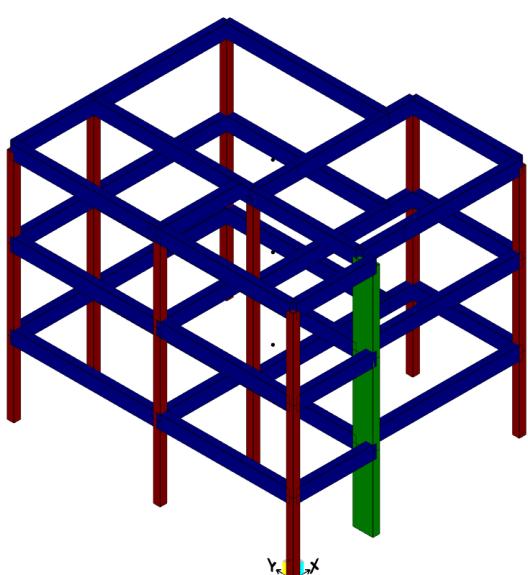


**Comments**

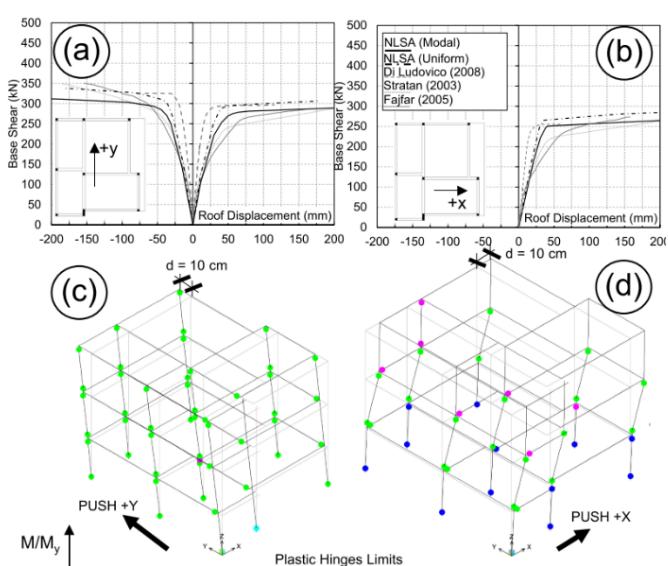
See Marchisella A, Muciaccia G. Comparative Assessment of Shear Demand for RC Beam-Column Joints under Earthquake Loading. Appl Sci. 2022;(12). doi:10.3390/ app12147153.

<b>Source</b>	Marchisella A, Muciaccia G. Comparative Assessment of Shear Demand for RC Beam-Column Joints under Earthquake Loading. Appl Sci. 2022;(12). doi:10.3390/ app12147153
<b>Elements</b>	FRAME
<b>Software</b>	SAP2000
<b>Material</b>	Lumped Plasticity
<b>Analysis</b>	Non-linear Static
<b>Reference Model [Experimental]</b>	NA
<b>Reference Model [Analytic./Num.]</b>	Stratan A, Fajfar P. Influence of Modelling Assumptions and Analysis Procedure on the Seismic Evaluation of Reinforced Concrete GLD Frames. Lubjana; 2002.

### Investigated Structure / Model



### Results

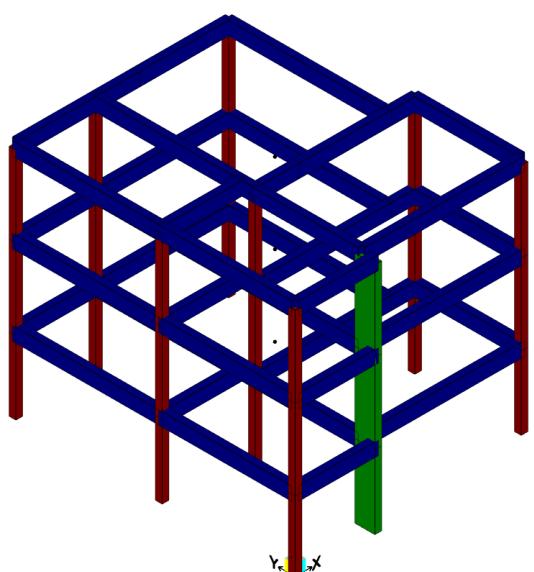


### Comments

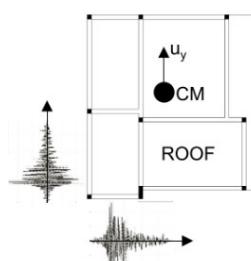
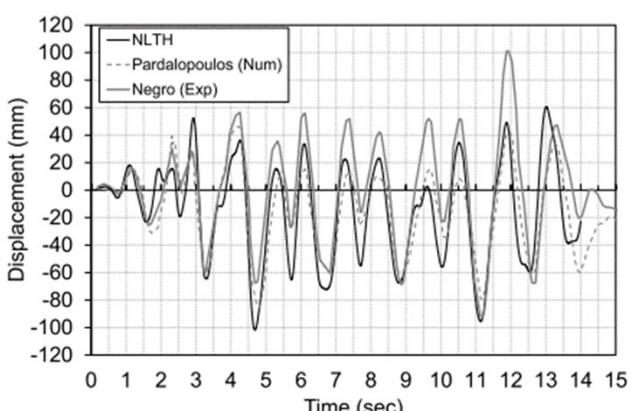
See Marchisella A, Muciaccia G. Comparative Assessment of Shear Demand for RC Beam-Column Joints under Earthquake Loading. Appl Sci. 2022;(12). doi:10.3390/ app12147153

<b>Source</b>	Marchisella A, Muciaccia G. Comparative Assessment of Shear Demand for RC Beam-Column Joints under Earthquake Loading. Appl Sci. 2022;(12). doi:10.3390/ app12147153
<b>Elements</b>	FRAME
<b>Software</b>	SAP2000
<b>Material</b>	Lumped Plasticity
<b>Analysis</b>	Non-linear Time History
<b>Reference Model [Experimental]</b>	Negro P, Mola E, Molina FJ, Magonette GE. Full-scale PsD testing of a torsionally unbalanced three-storey non-seismic RC frame. In: 13th World Conference on Earthquake Engineering. Vancouver; 2004.
<b>Reference Model [Analytic./Num.]</b>	Pardalopoulos SI, Pantazopoulou S, Manolis GD. On the Modeling and Analysis of Brittle Failure in Existing RC Structures Due to Seismic Loads. Appl Sci. 2022.

### Investigated Structure / Model



### Results

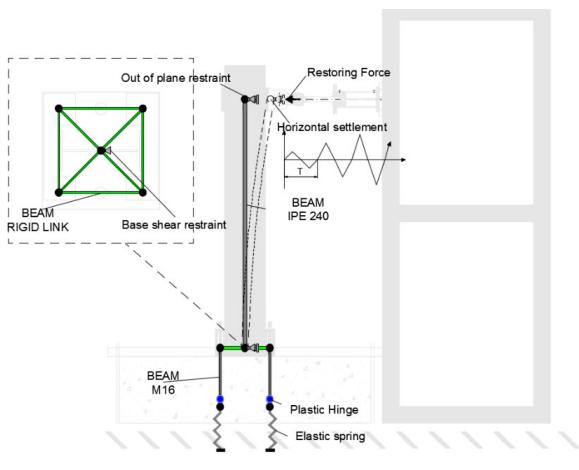


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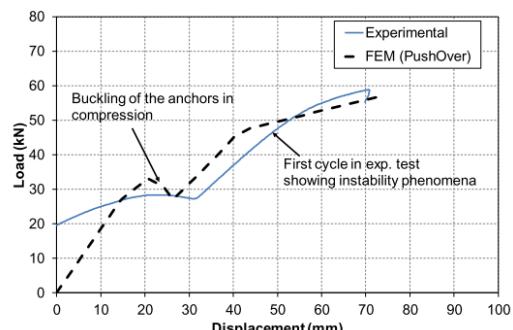
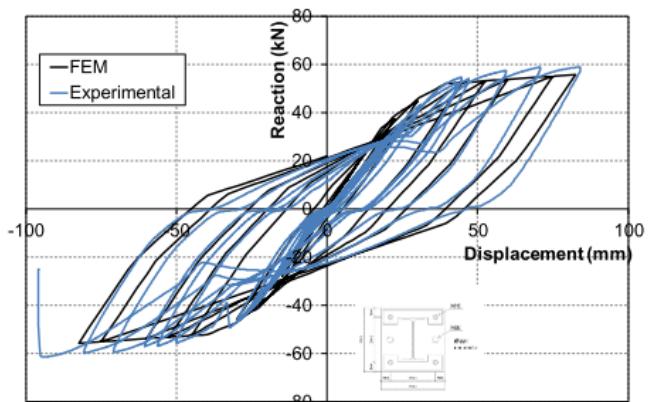
See Marchisella A, Muciaccia G. Comparative Assessment of Shear Demand for RC Beam-Column Joints under Earthquake Loading. Appl Sci. 2022;(12). doi:10.3390/ app12147153.

<b>Source</b>	Marchisella A, Muciaccia G. Numerical Investigation of Dissipative Behavior of Connection Using Post-Installed Anchors. In: <i>16th European Conference on Earthquake Engineering</i> ; 2018:1-12.
<b>Elements</b>	FRAME / SPRINGS
<b>Software</b>	SAP2000
<b>Material</b>	Linear-Elastic steel for beam/ Non-Linear springs for anchors
<b>Analysis</b>	Non-Linear Quasi-Static
<b>Reference Model [Experimental]</b>	Muciaccia G. Behavior of post-installed fastening under seismic action. ACI J. 2017;February:1-34.
<b>Reference Model [Analytic./Num.]</b>	

### Investigated Structure / Model



### Results

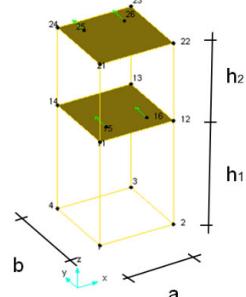
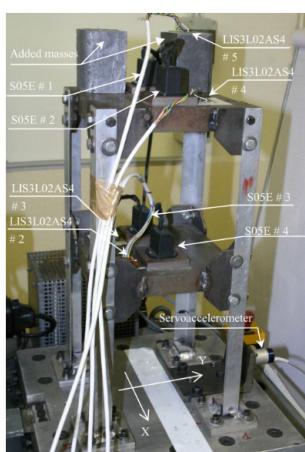


### Comments

The numerical investigation addressed a steel-to-concrete connection (column-to-foundation). The peculiarity of the connection is the adoption of stretch length for anchor to promote ductile mechanical response under uni-axial bending. Lumped plasticity was used to model the anchors. Agreement between numerical and experimental results was found with respect to hysteretic behavior however a thorough understanding of buckling phenomena occurred during experiments was possible by means of additional pushover analysis.

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME
<b>Software</b>	SAP2000
<b>Material</b>	Linear-Elastic
<b>Analysis</b>	Modal
<b>Reference Model [Experimental]</b>	Martinelli L, Gentile C. System identification and monitoring by using low-cost MEMS sensors. In: PAPI 15. ; 2015:123-132.
<b>Reference Model [Analytic./Num.]</b>	Martinelli L, Gentile C. System identification and monitoring by using low-cost MEMS sensors. In: PAPI 15. ; 2015:123-132.

### Investigated Structure / Model



### Results

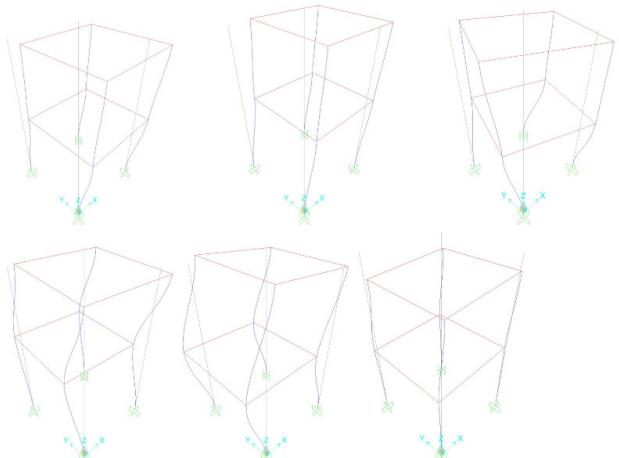
MODE	SAP2000 (Hz) <sup>a</sup>	Direction <sup>b</sup>	FDD - Sweep (Hz) <sup>c</sup>	FDD - Impulse <sup>d</sup>
I	28.30	yy	26.37	26.85
II	39.96	xx	39.06	39.55
III	73.40	zz	75.19	76.17
IV	102.98	yy	104.49	105.957
V	140.21	xx	-	-
VI	211.59	z + zz	-	211.26

<sup>a</sup> Natural frequencies obtained via modal analysis (SAP2000)

<sup>b</sup> Direction of the modal shapes obtained via modal analysis (SAP2000)

<sup>c</sup> Peak-picking via FDD method in case of sweep loading

<sup>d</sup> Peak-picking via FDD method in case of impulse loading

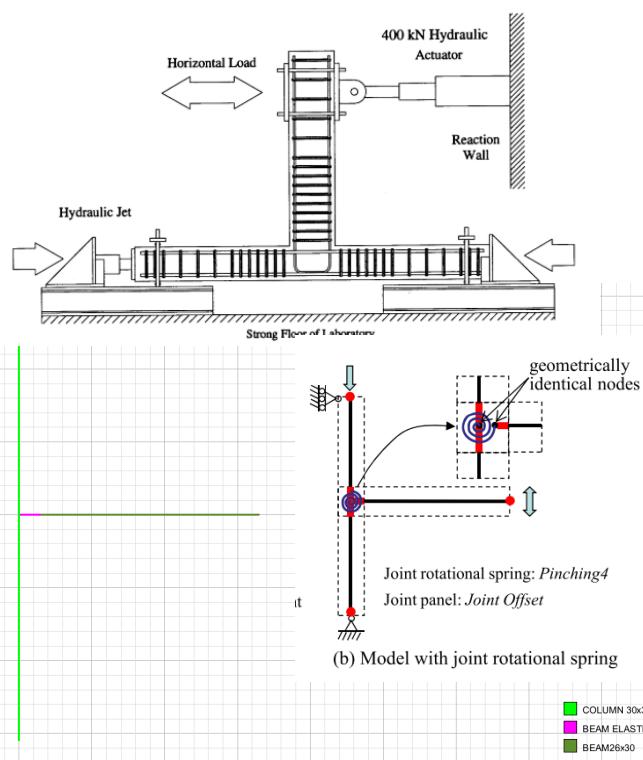


### Comments

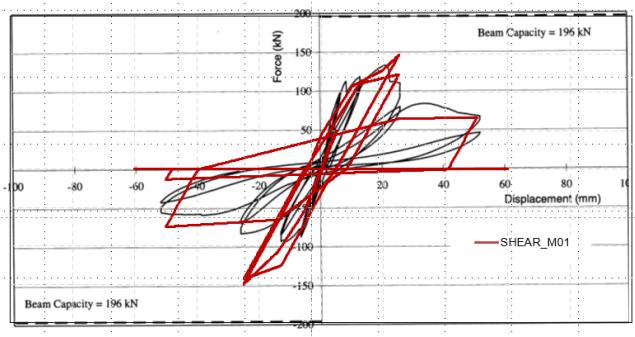
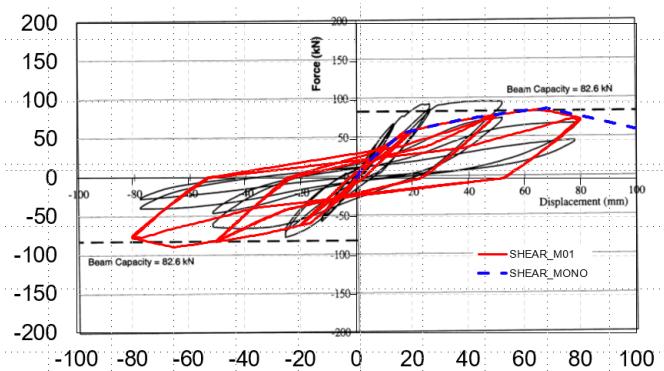
The numerical investigation addressed a scaled frame (two-storeys, 1 bay) tested under sweep and impulse excitation. Experimental time signals recorded via accelerometers (courtesy of L. Martinelli) were analyzed using Frequency Domain Decomposition (FDD, implemented in MatLab). Natural frequencies and modal shapes were numerically-derived from numerical model and finally compared to experimentally-derived ones.

Source	Personal Archive
Elements	FRAME / SPRINGS
Software	OPEN SEES
Material	Non-linear equivalent spring for joint / Fiber sections for beam
Analysis	Non-Linear
Reference Model [Experimental]	Wong HF. Shear Strength And Seismic Performance of Non-Seismically Designed Reinforced Concrete Beam-Column Joint. 2005. doi:10.14711/thesis-b914043
Reference Model [Analytic./Num.]	NA

### Investigated Structure / Model



### Results

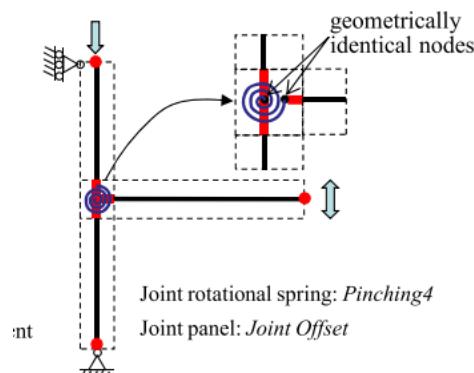
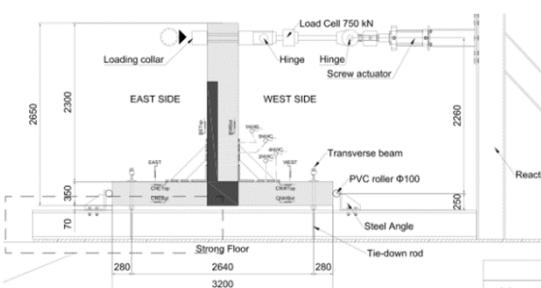


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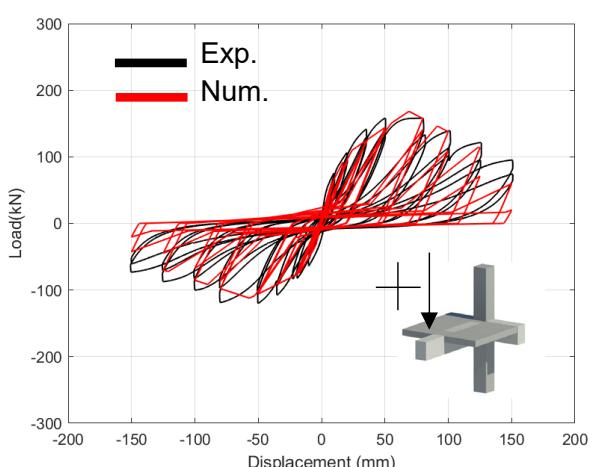
The numerical investigation addressed a shear critical beam-column joint. The non-linear backbone assigned to the joint panel was analytically-derived from Park S, Mosalam KM. Simulation of reinforced concrete frames with nonductile beam-column joints. *Earthq Spectra*. 2013;29(1):233-257. doi:10.1193/1.4000100. Hysteresis model according to «Pinching-4» (see [https://opensees.berkeley.edu/wiki/index.php/Pinchng4\\_Material](https://opensees.berkeley.edu/wiki/index.php/Pinchng4_Material)) was able to reproduce the intermediate un-loading path quite well.

<b>Source</b>	Personal Archive
<b>Elements</b>	FRAME / SPRINGS
<b>Software</b>	OPEN SEES
<b>Material</b>	Non-linear equivalent spring for joint / Fiber sections for beam
<b>Analysis</b>	Non-Linear Quasi Static
<b>Reference Model [Experimental]</b>	Marchisella A, Muciaccia G, Sharma A, Eligehausen R. Experimental investigation of 3d RC exterior joint retrofitted with FFHR. Eng Struct. 2021;239(July):112206. doi:10.1016/j.engstruct.2021.112206
<b>Reference Model [Analytic./Num.]</b>	Tonidis M, Sharma A. Numerical investigations on the influence of transverse beams and slab on the seismic behavior of substandard beam-column joints. Eng Struct. 2021;247(September):113123. doi:10.1016/j.engstruct.2021.113123

### Investigated Structure / Model



### Results

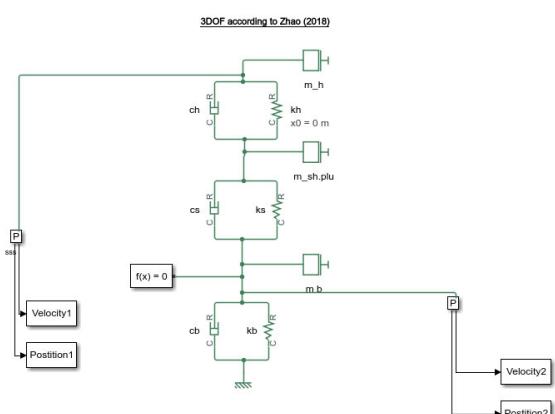
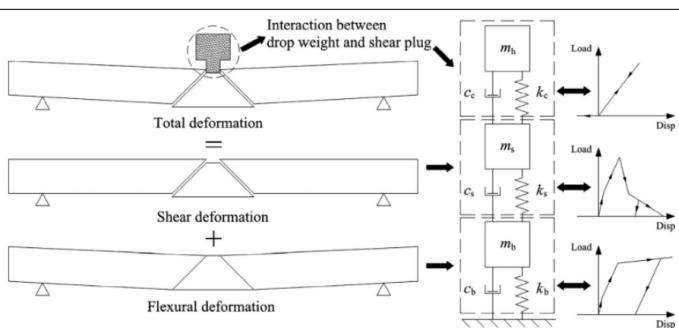


### Comments

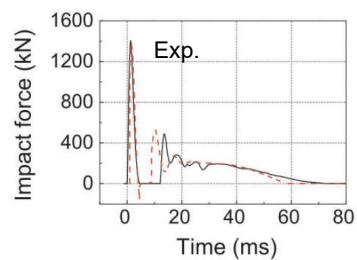
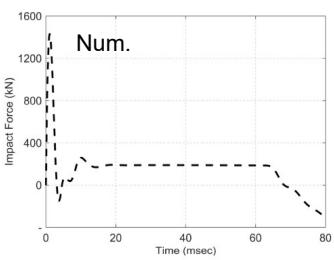
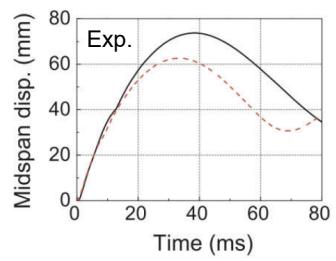
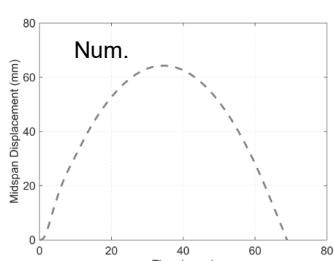
The numerical investigation addressed a shear critical beam-column joint with slab and transverse beam. The non-linear backbone assigned to the joint panel was analytically-derived from Park S, Mosalam KM. Simulation of reinforced concrete frames with nonductile beam-column joints. *Earthq Spectra*. 2013;29(1):233-257. doi:10.1193/1.4000100. Hysteresis model according to «Pinching-4» (see [https://opensees.berkeley.edu/wiki/index.php/Pinchng4\\_Material](https://opensees.berkeley.edu/wiki/index.php/Pinchng4_Material)) was able to reproduce the intermediate unloading path quite well.

Source	Personal Archive
Elements	SPRINGS
Software	SIMSCAPE (see Matworks. Simscape User Guide. 2018. )
Material	Non-linear equivalent spring for beam under impact
Analysis	Non-Linear Time History
Reference Model [Experimental]	Zhao D-B, Kunnath SK. Simplified Approach for Assessing Shear Resistance of Reinforced Concrete Beams under Impact Loads. ACI Struct J. 2016;113(4). doi:10.14359/51688617
Reference Model [Analytic./Num.]	NA

### Investigated Structure / Model



### Results

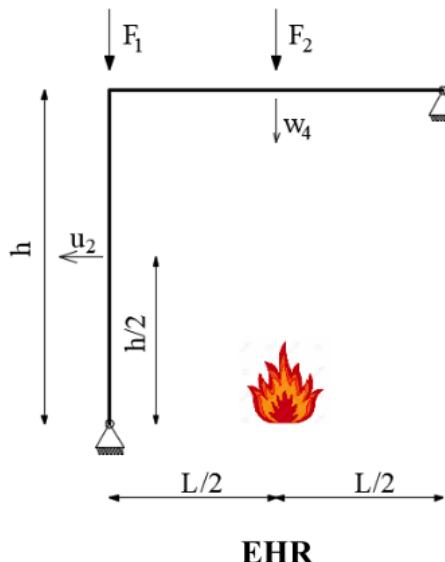


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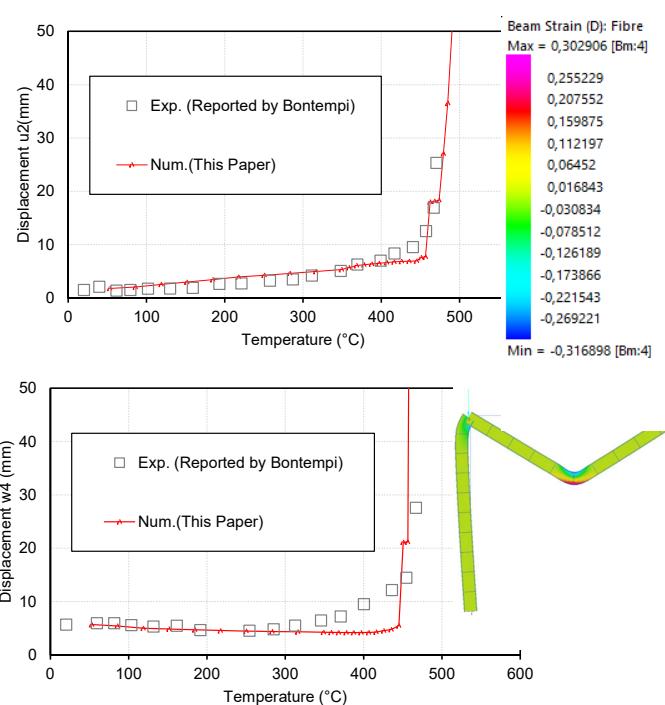
The numerical investigation addressed RC beam under impact (drop-weight test). An analytical model, retrieved from technical literature, composed by a series of springs, dashpots and lumped masses was implemented in Simscape. Agreement was found for the comparison of both deflection and impact force.

<b>Source</b>	Personal archive
<b>Elements</b>	FRAME
<b>Software</b>	Straus-7
<b>Material</b>	Steel (elastic-plastic + thermal degradation)
<b>Analysis</b>	Non-linear coupled thermo-mechanical
<b>Reference Model [Experimental]</b>	F. Bontempi, "Structural analysis in case of fire (In Italian)," <i>Ingenio</i> , 2019.
<b>Reference Model [Analytic./Num.]</b>	F. Bontempi, "Structural analysis in case of fire (In Italian)," <i>Ingenio</i> , 2019.

### Investigated Structure / Model



### Results

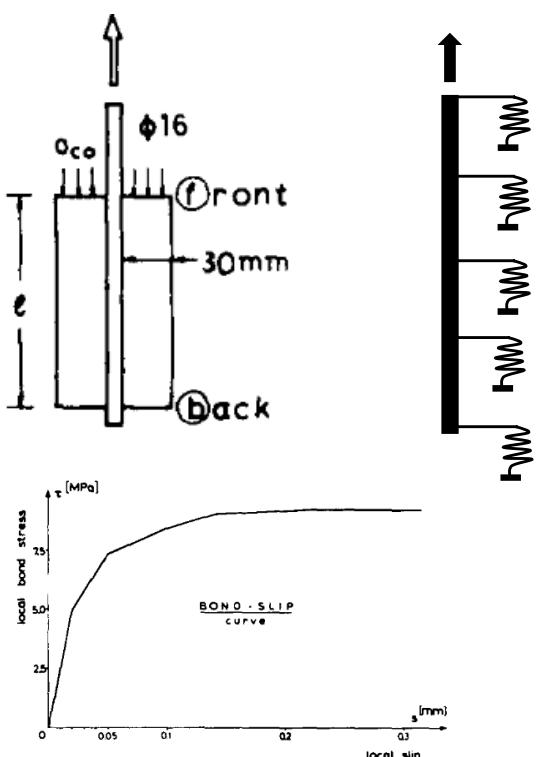


### Comments

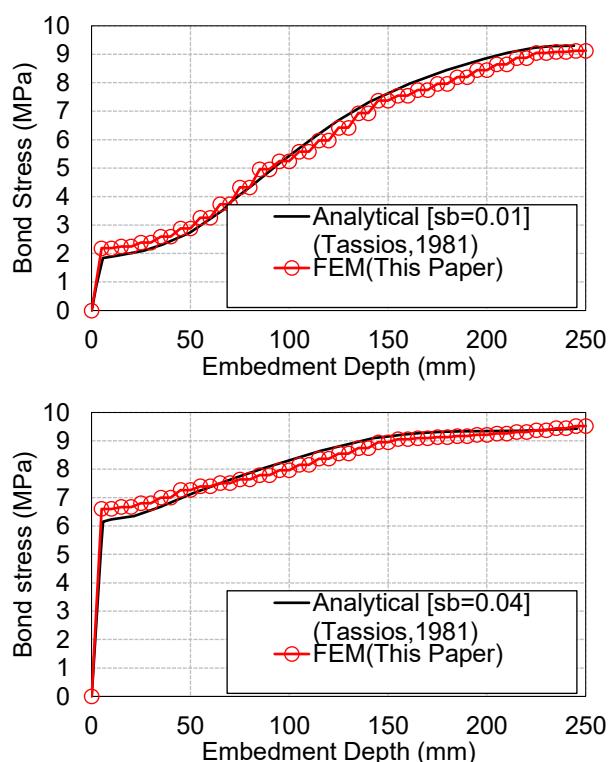
The numerical investigation addressed a steel frame under ISO-384 fire (all sides exposed). Numerical model solved the coupled thermo-mechanical problem, viz. considering transient heat simultaneous to thermal degradation of steel (stiffness, strength). Agreement was found, up to 500  $^{\circ}\text{C}$  when relevant displacements were compared to experimental results.

Source	Personal archive
Elements	FRAME
Software	Straus-7
Material	Steel (elastic-plastic) + Spring simulating bond stress-slip
Analysis	Non-linear
Reference Model [Experimental]	Not applicable
Reference Model [Analytic./Num.]	T. P. Tassios and P. J. Yannopoulos, "Analytical Studies on Reinforced Concrete Members Under Cyclic Loading Based on Bond Stress-Slip Relationships," ACI J., no. 78, pp. 206–216, 1981.

### Investigated Structure / Model



### Results



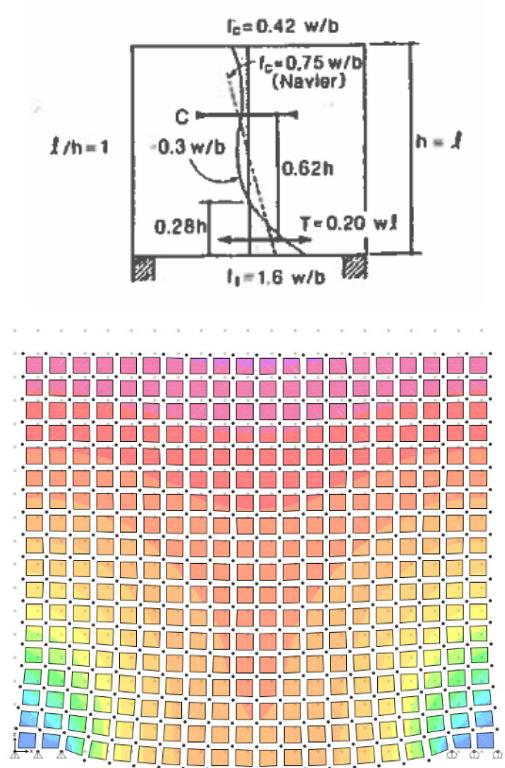
### Comments

The numerical investigation addressed a single bar embedded in concrete subjected to pullout test. The bar is modelled as uniaxial element with a curtain of springs aiming at simulating the local bond-slip behaviour. Numerically-derived bond stresses distributions (at different level of the imposed slip at the back section (sb)) agreed with analytically-derived results retrieved from the due reference.

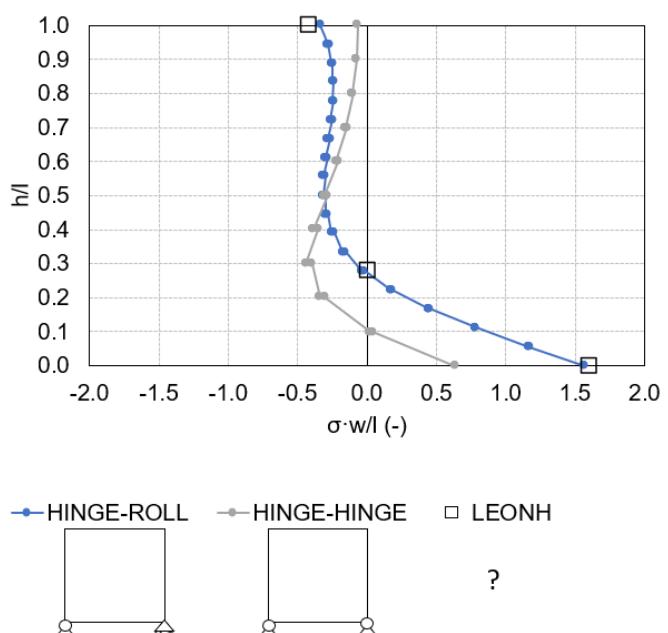
## **2D PLANE**

<b>Source</b>	Personal Archive
<b>Elements</b>	2D plane stress
<b>Software</b>	SAP 2000
<b>Material</b>	Linear Elastic
<b>Analysis</b>	Linear Static
<b>Reference Model [Experimental]</b>	NA
<b>Reference Model [Analytic./Num.]</b>	Collins MP, Mitchell D. Prestressed Concrete Structures. Englewood Cliffs: Prentice-Hall International; 1991.

### Investigated Structure / Model



### Results

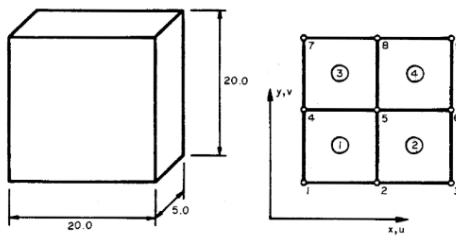


### Comments

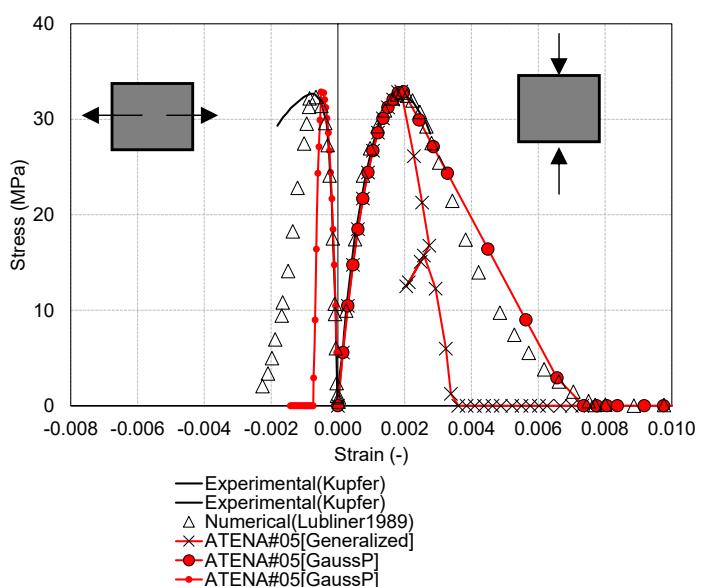
The numerical investigation addressed the problem of a deep beam having the height of the cross-section equal to the span. Scopes of the numerical investigations were two: (i) define the restraint conditions (which were not clearly stated in the reference document) and (ii) evaluate the accuracy of numerically-derived stresses. For the latter, comparison was given with respect to analytically-derived stresses.

<b>Source</b>	Personal Archive
<b>Elements</b>	2D plane stress
<b>Software</b>	ATENA
<b>Material</b>	Non-Linear Concrete (MCFT)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	Kupfer H, Hilsdorf H. Behavior of Concrete Under Biaxial Stresses. ACI J Proc. 1969;(66):656-666.
<b>Reference Model [Analytic./Num.]</b>	Lubliner J, Oliver J, Oller S, Oñate E. A plastic-damage model for concrete. Int J Solids Struct. 1989;25(3):299-326. doi:10.1016/0020-7683(89)90050-4

### Investigated Structure / Model



### Results

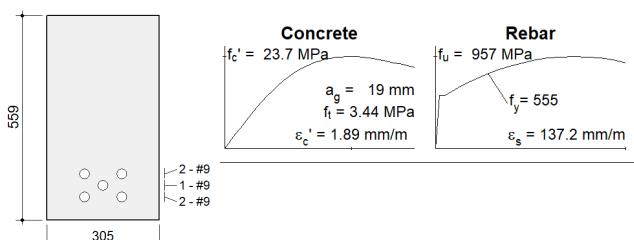
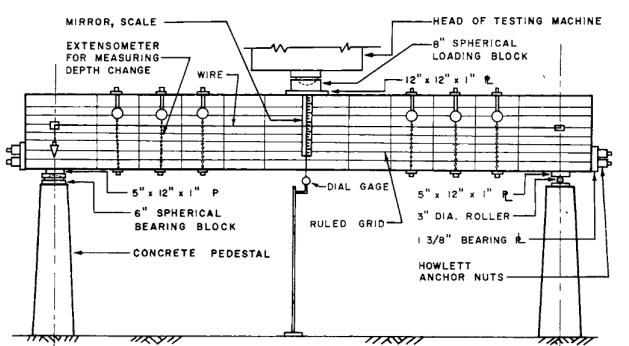


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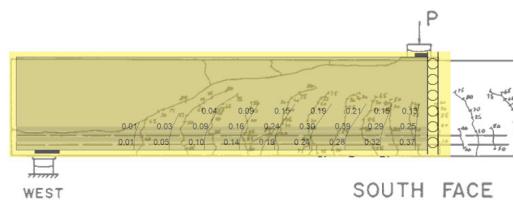
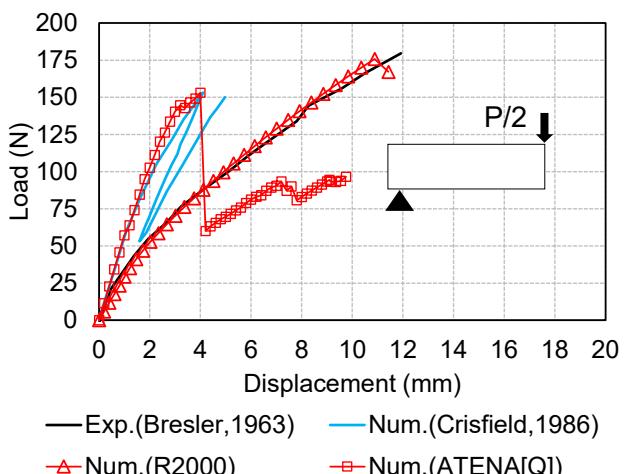
The numerical investigation addressed square block of plain concrete under pure compression. The scope of the investigation was to evaluate the performance of non-linear model of concrete implemented in ATENA software. Agreement was found with respect to experimental and numerically-derived independent results. Differences in numerically-derived stresses between gauss points and nodes (after average) were recognized.

<b>Source</b>	Personal Archive
<b>Elements</b>	2D Plane stress
<b>Software</b>	ATENA / RESPONSE 2000
<b>Material</b>	Non-Linear concrete (MCFT)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	Bresler B, Scordelis AC. Shear strength of large reinforced concrete beams. Am Concr Institute, ACI Spec Publ. 1963;SP-118(60):259-279.
<b>Reference Model [Analytic./Num.]</b>	Crisfield MA. Snap-through and snap-back response in concrete structures and the dangers of under-integration. <i>Int J Numer Methods Eng.</i> 1986;22(3):751-767. doi:10.1002/nme.1620220314

### Investigated Structure / Model



### Results

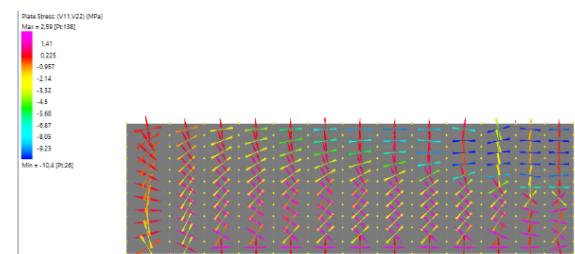
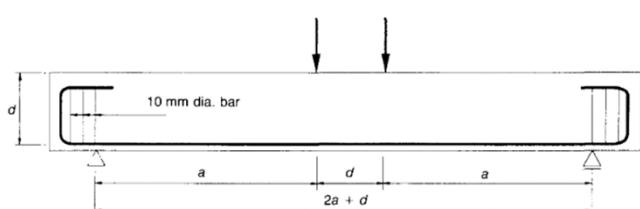


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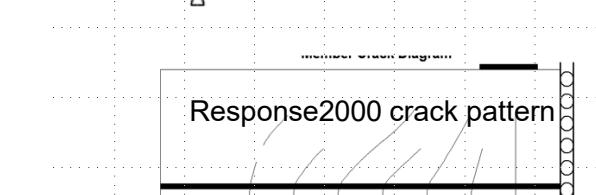
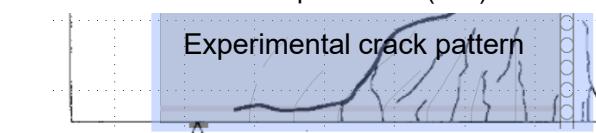
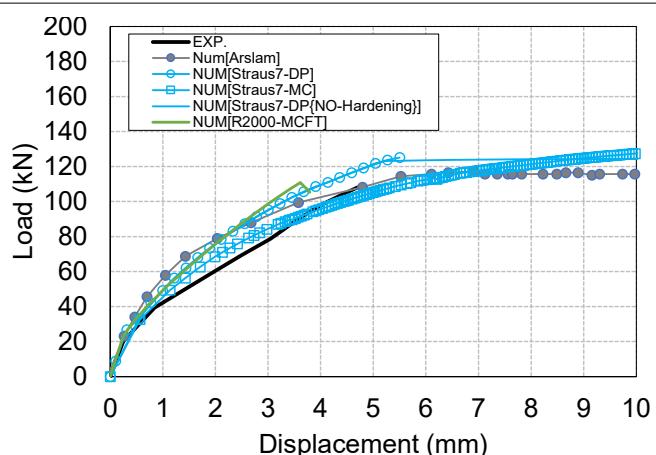
The numerical investigation addressed shear critical beam tested by Bresler. The scope was to replicate instable numerical solution found by Crisfield (Crisfield, 1986) using plane stress approach. Besides, satisfactory comparison was found with respect to experimental results by using Response 2000 (using non-linear frame elements).

<b>Source</b>	Personal Archive
<b>Elements</b>	2D Plane Stress
<b>Software</b>	STRAUS-7 / RESPONSE 2000
<b>Material</b>	Non-Linear Concrete (PLAST) / Non-Linear Steel reinforcement (perfect bond)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	Kim J-K, Park Y-D. Shear strength of reinforced high strength concrete beams without web reinforcement. Mag Concr Res. 1994;46(166):7-16. doi:10.1680/macr.1994.46.166.7
<b>Reference Model [Analytic./Num.]</b>	Arslan G. Sensitivity study of the Drucker-Prager modeling parameters in the prediction of the nonlinear response of reinforced concrete structures. Mater Des. 2007;28(10):2596-2603. doi:10.1016/j.matdes.2006.10.021

### Investigated Structure / Model



### Results

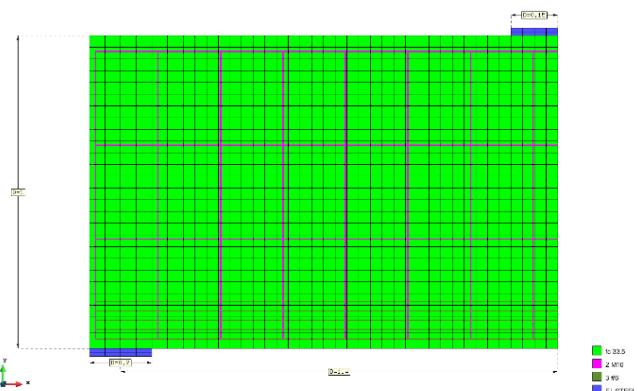
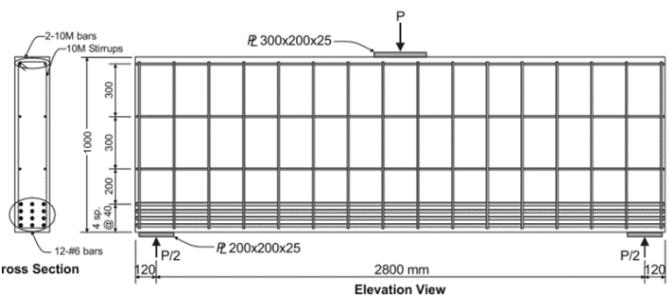


### Comments

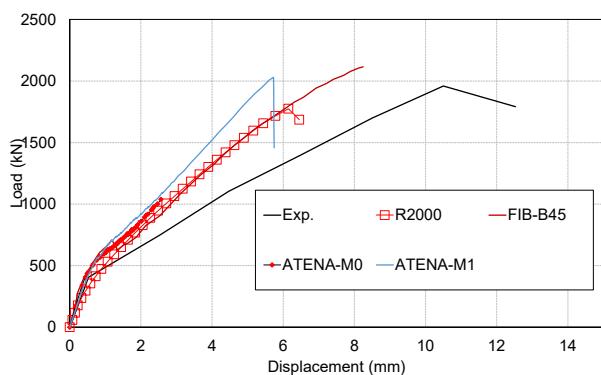
The scope of the investigation was to evaluate the performance non-linear model of concrete implemented in STRAUS-7 software, based on plasticity theory (e.g. Mhor-Coulomb type). The selected benchmark was a shear-critical RC beam. Numerically-derived load-carrying capacity was in agreement with respect to both experimental results and numerically-derived ones using Response-2000. Displacement field cannot be compared conclusively because lack of kinematic description intrinsic to plasticity models.

<b>Source</b>	Personal Archive
<b>Elements</b>	2D Plane stress
<b>Software</b>	ATENA / RESPONSE 2000
<b>Material</b>	Non-Linear concrete (MCFT) / Non-Linear steel reinforcement (perfect bond)
<b>Analysis</b>	Non-Linear static
<b>Reference Model [Experimental]</b>	FIB. Bulletin 45 - Practitioners' Guide to Finite Element Modelling of Reinforced Concrete Structures. Vol 1. Lausanne, Lausanne, Switzerland; 2008. doi:10.1017/CBO9781107415324.004
<b>Reference Model [Analytic./Num.]</b>	FIB. Bulletin 45 - Practitioners' Guide to Finite Element Modelling of Reinforced Concrete Structures. Vol 1. Lausanne, Lausanne, Switzerland; 2008. doi:10.1017/CBO9781107415324.004

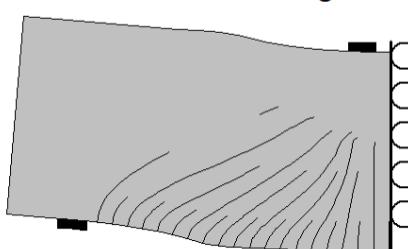
### Investigated Structure / Model



### Results



### Member Crack Diagram

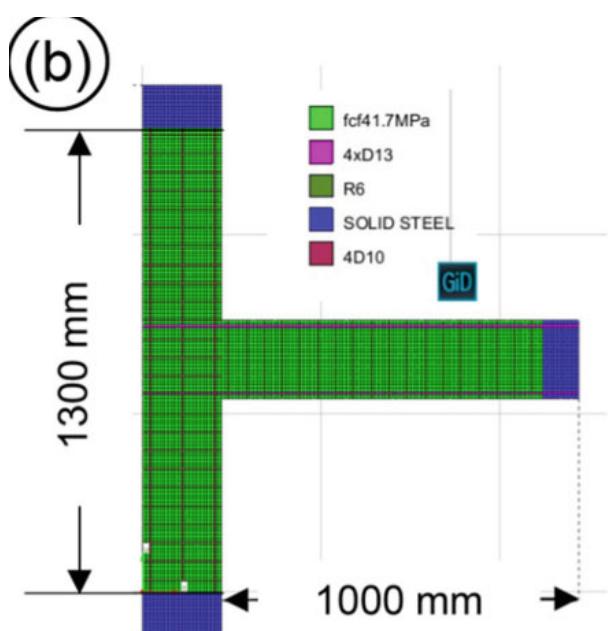


### Comments

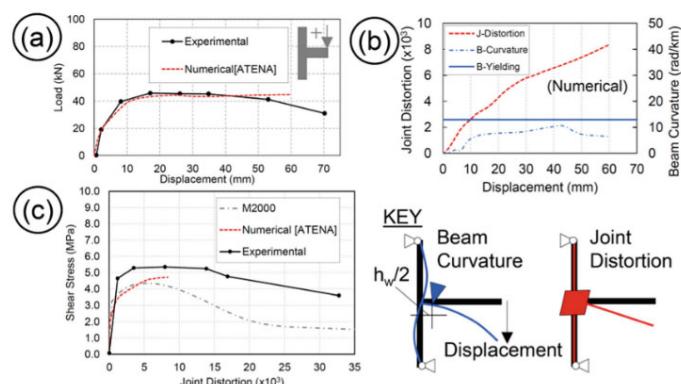
The scope of the investigation was to evaluate the performance non-linear model of concrete implemented in ATENA software, based on MCFT. The selected benchmark was a shear-critical RC beam. Numerically-derived load-carrying capacity was in agreement with respect to both experimental results and numerically-derived ones using Response-2000. Besides, comparison is made to numerical results included in the reference document, i.e. FIB-B45 curves in the figure. Displacement field cannot be compared conclusively.

<b>Source</b>	Marchisella A, Muciaccia G. RC Beam-Column Joints as Membrane Elements: An Application of MCFT. In: Fib SYMPOSIUM: International Symposium of the International Federation for Structural Concrete. Springer Nature Switzerland; 2023:509–519. doi:10.1007/978-3-031-32511-3_54
<b>Elements</b>	2D plane stress
<b>Software</b>	ATENA / MEMBRANE 2000
<b>Material</b>	Non-linear concrete (smeared crack) / Non-Linear steel reinforcement (perfect bond)
<b>Analysis</b>	Non-linear Static
<b>Reference Model [Experimental]</b>	Kaku T, Asakusa H. Bond and anchorage of bars in reinforced concrete beam-column joints. ACI Spec Publ. 1991;123:401-424.
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



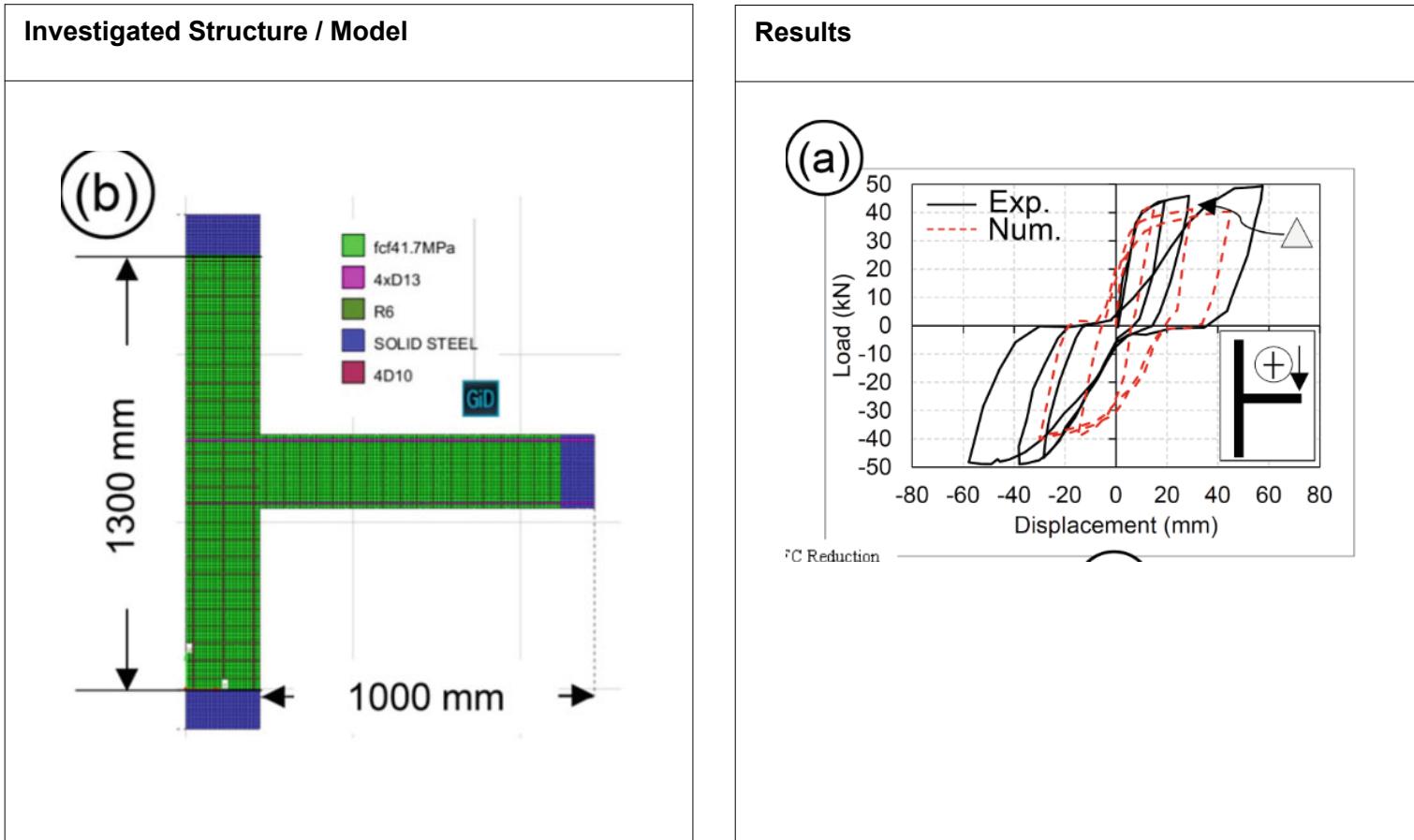
### Results



### Comments

See Marchisella A, Muciaccia G. RC Beam-Column Joints as Membrane Elements: An Application of MCFT. In: Fib SYMPOSIUM: International Symposium of the International Federation for Structural Concrete. Springer Nature Switzerland; 2023:509–519. doi:10.1007/978-3-031-32511-3\_54.

<b>Source</b>	Marchisella A, Muciaccia G. RC Beam-Column Joints as Membrane Elements: An Application of MCFT. In: Fib SYMPOSIUM: International Symposium of the International Federation for Structural Concrete. Springer Nature Switzerland; 2023:509–519. doi:10.1007/978-3-031-32511-3_54
<b>Elements</b>	2D plane stress
<b>Software</b>	ATENA / MEMBRANE 2000
<b>Material</b>	Non-linear concrete (smeared crack) / Non-Linear steel reinforcement (Bond-Slip with memory)
<b>Analysis</b>	Non-linear Quasi-Static
<b>Reference Model [Experimental]</b>	Kaku T, Asakusa H. Bond and anchorage of bars in reinforced concrete beam-column joints. ACI Spec Publ. 1991;123:401-424.
<b>Reference Model [Analytic./Num.]</b>	NA

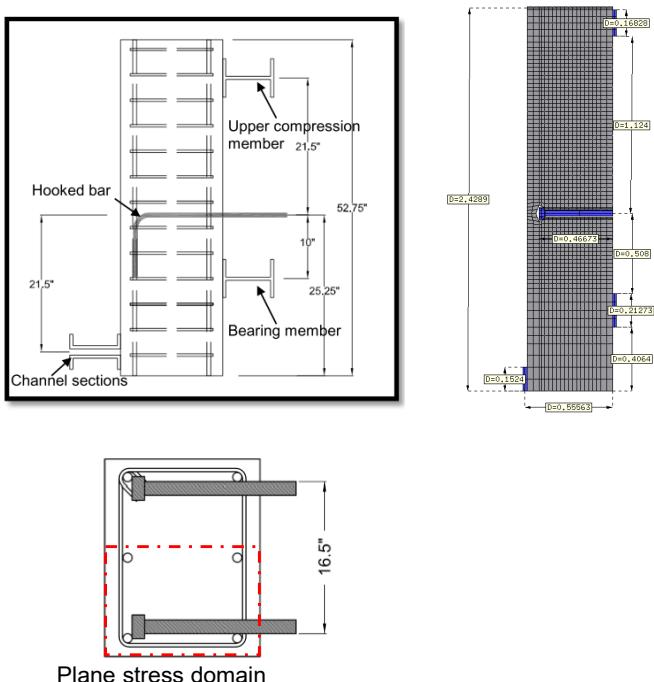


**Comments**

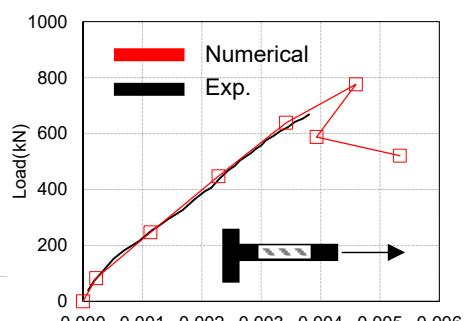
See Marchisella A, Muciaccia G. RC Beam-Column Joints as Membrane Elements: An Application of MCFT. In: Fib SYMPOSIUM: International Symposium of the International Federation for Structural Concrete. Springer Nature Switzerland; 2023:509–519. doi:10.1007/978-3-031-32511-3\_54.

<b>Source</b>	Personal Archive
<b>Elements</b>	2D plane stress
<b>Software</b>	ATENA
<b>Material</b>	Non-linear concrete (MCFT)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	Shao Y, Darwin D, O'Reilly M, Lequesne R, Ghimire K, Hano M. Anchorage of Conventional and High-Strength Headed Reinforcing Bars [SM Report No.117].; 2016.
<b>Reference Model [Analytic./Num.]</b>	

### Investigated Structure / Model



### Results



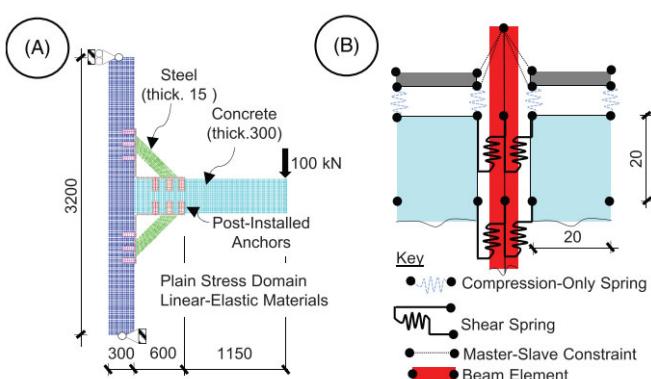
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### Comments

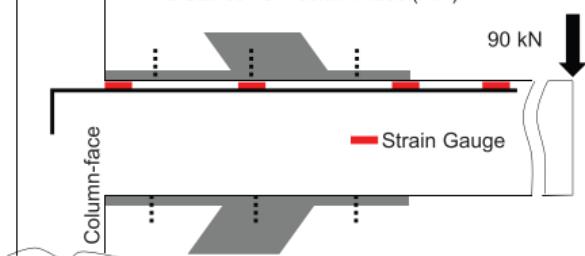
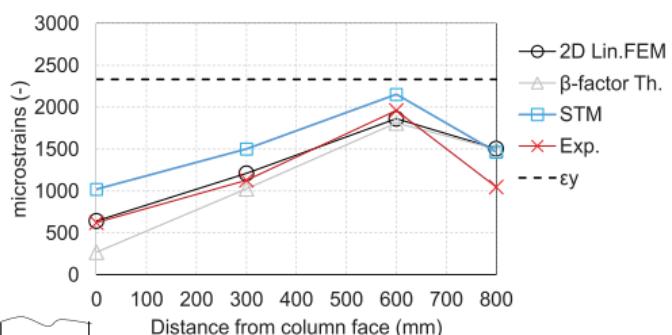
The numerical investigation addressed anchorage test using column-type specimen which, according to researchers who performed experimental tests, represent a static equivalent condition of RC beam-column joint. The scope of the investigation was to determine the stress field of the specimen. Validation was based on load and strains measured at the bar. Moreover comparison of the crack pattern obtained at the end of both experimental test and numerical simulation was made.

<b>Source</b>	Marchisella A, Muciaccia G. Haunch retrofit of RC beam – column joints : Linear stress field analysis and Strut-and-Tie method application. 2023;(May):1-25. doi:10.1002/eqe.3921
<b>Elements</b>	2D Plane stress
<b>Software</b>	SAP2000
<b>Material</b>	Linear-Elastic Concrete / Compression-only grout / Linear-Elastic Steel plates / Linear-Elastic steel rod (bond-slip law)
<b>Analysis</b>	Linear Static
<b>Reference Model [Experimental]</b>	Genesio G. Seismic Assessment of RC Exterior Beam- Column Joints and Retrofit with Haunches Using Post-Installed Anchors. 2012.
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



### Results

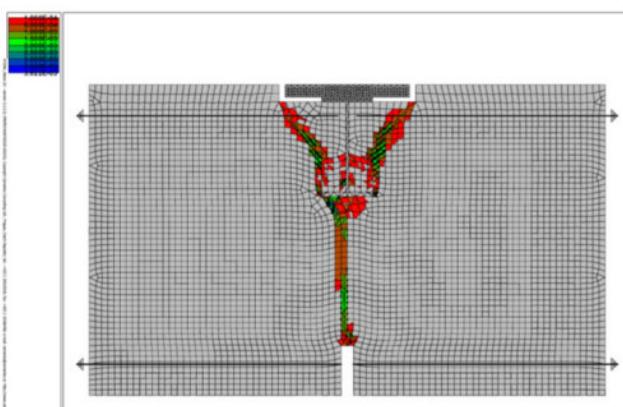


### Comments

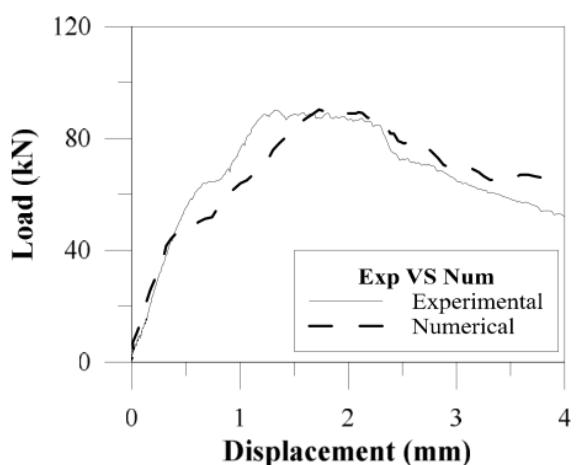
See Marchisella A, Muciaccia G. Haunch retrofit of RC beam – column joints : Linear stress field analysis and Strut-and-Tie method application. 2023;(May):1-25. doi:10.1002/eqe.3921.

<b>Source</b>	Di Nunzio G, Marchisella A, Muciaccia G. Influence of head-size on concrete cone capacity: a comparison for two cast-in solutions. In: 12th Fib International PhD Symposium in Civil Engineering. Prague; 2018:187-194.
<b>Elements</b>	2D Plane stress
<b>Software</b>	ATENA
<b>Material</b>	Non-Linear concrete (MCFT) / Linear-Elastic steel reinforcement (perfect bond)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	Di Nunzio G, Marchisella A, Muciaccia G. Influence of head-size on concrete cone capacity: a comparison for two cast-in solutions. In: 12th Fib International PhD Symposium in Civil Engineering. Prague; 2018:187-194
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



### Results

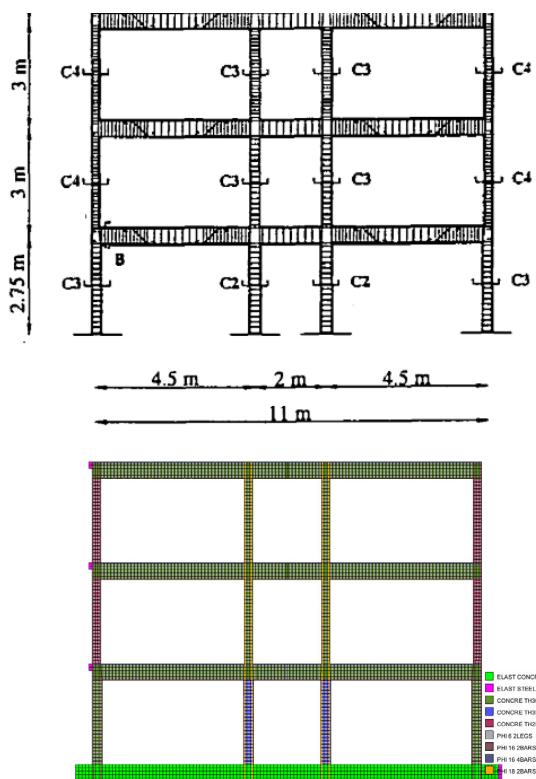


### Comments

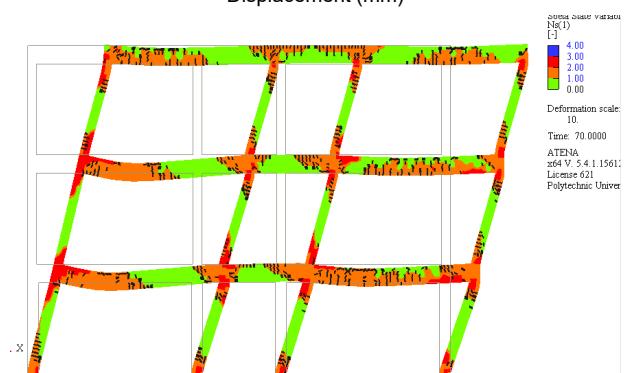
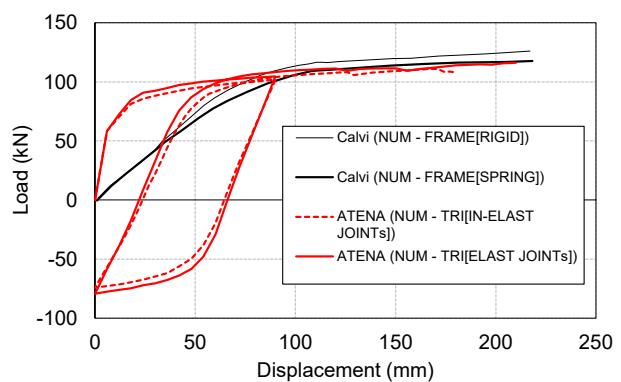
See Di Nunzio G, Marchisella A, Muciaccia G. Influence of head-size on concrete cone capacity: a comparison for two cast-in solutions. In: 12th Fib International PhD Symposium in Civil Engineering. Prague; 2018:187-194.

<b>Source</b>	Personal Archive
<b>Elements</b>	2D Plane stress
<b>Software</b>	ATENA
<b>Material</b>	Non-Linear concrete (MCFT) / Linear-Elastic steel reinforcement (perfect bond)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	NA
<b>Reference Model [Analytic./Num.]</b>	Calvi, Gian Michele, Guido Magenes, and Stefano Pampanin. 2002. "Relevance of Beam-Column Joint Damage and Collapse in Rc Frame Assessment." Journal of Earthquake Engineering 6 (November): 75–100. <a href="https://doi.org/10.1080/13632460209350433">https://doi.org/10.1080/13632460209350433</a> .

### Investigated Structure / Model



### Results



### Comments

The numerical investigation addressed a RC frame characterized by seismic deficiencies such as strong beam and weak columns, no stirrups inside beam-column joint. Numerical model was made using two-dimensional plane stress elements. To compare numerically derived load-displacement curve with respect to Calvi's results which uses frame element with reduced stiffness with respect to elastic one, push-over analysis was to-steps. Indeed, a first load and un-load path was imposed to the structure to decrease the stiffness (with respect to un-cracked condition) then a re-load path followed. For the latter agreement with respect to experimental results was found.

<b>Source</b>	Personal Archive
<b>Elements</b>	2D Plane Stress
<b>Software</b>	ATENA
<b>Material</b>	Non-Linear concrete (MCFT) / Linear-Elastic steel reinforcement (perfect bond)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	A. Sharma, R. Elieghausen, and J. Asmus, "Experimental investigation of concrete edge failure of multiple-row anchorages with supplementary reinforcement," Struct. Concr., vol. 18, no. 1, pp. 153–163, 2017.
<b>Reference Model [Analytic./Num.]</b>	Not Applicable

### Investigated Structure / Model

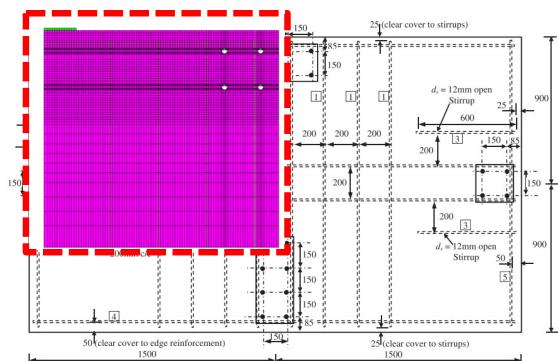
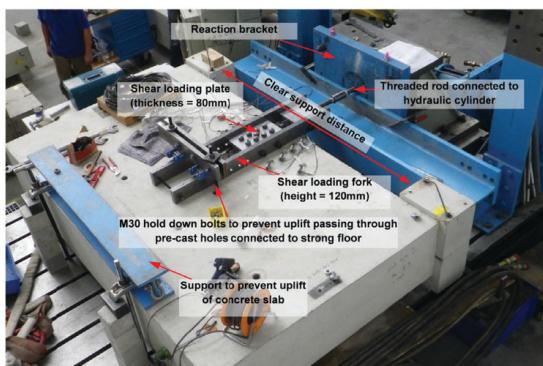
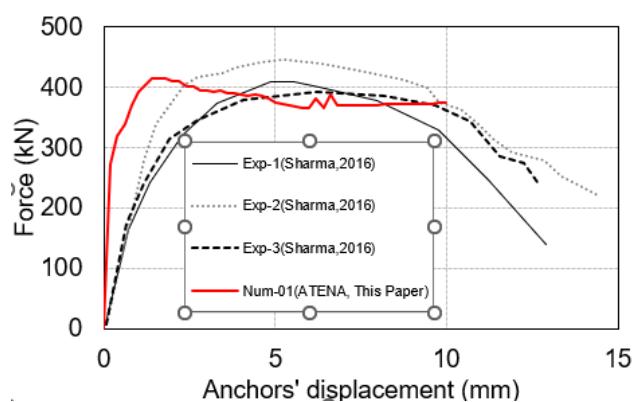


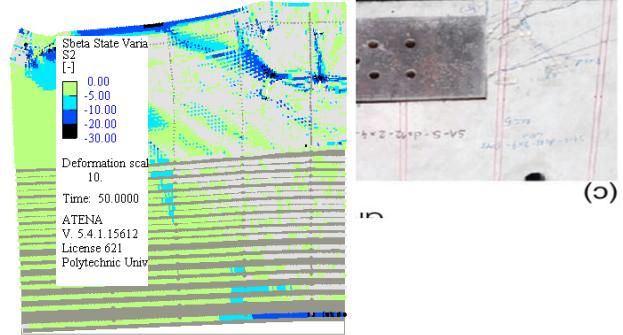
FIGURE 5 Typical design of the reinforced concrete slab used for the tests (All dimensions in mm).



### Results



Compression field (Stress in MPa)



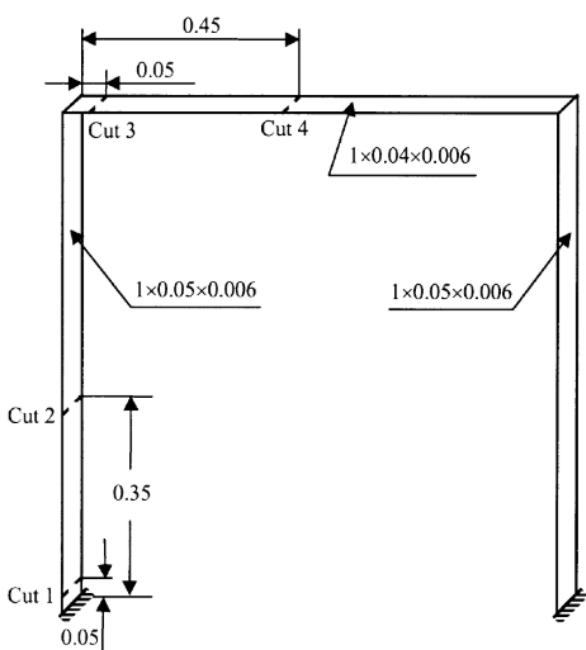
### Comments

The numerical investigation addressed anchors' group (cast-in headed stud) loaded in shear toward an edge. Concrete specimens were designed with supplementary reinforcement to confine concrete edge breakout. The structure is modelled as 2D plane stress with quite refined mesh (size 15 mm) to accurately reproduce geometry of the studs' shank. Agreement is found between experimental and numerically-derived load-carrying capacities. There is difference in initial stiffness most probable due to different displacements considered, i.e. the anchors' shank displacement is assumed for numerical curve while, in all likelihood, experimental curve are referred to the actuator's displacement.

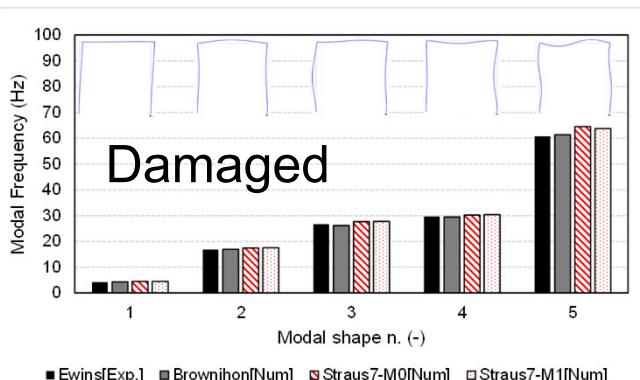
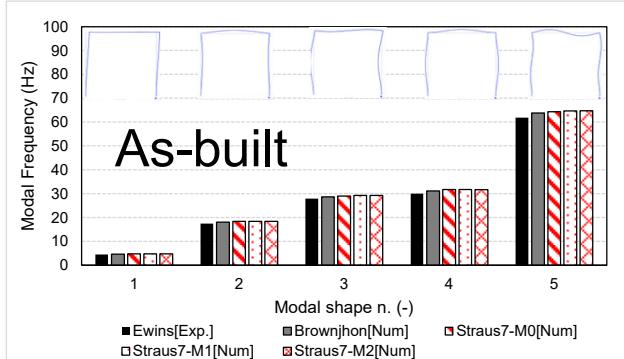
## **PLATES and SHELLS**

<b>Source</b>	Personal Archive
<b>Elements</b>	SHELL
<b>Software</b>	Straus-7
<b>Material</b>	Linear-Elastic
<b>Analysis</b>	Modal
<b>Reference Model [Experimental]</b>	Brownjohn JMW, Xia PQ, Hao H, Xia Y. Civil structure condition assessment by FE model updating: Methodology and case studies. <i>Finite Elem Anal Des.</i> 2001;37(10):761-775. doi:10.1016/S0168-874X(00)00071-8
<b>Reference Model [Analytic./Num.]</b>	Brownjohn JMW, Xia PQ, Hao H, Xia Y. Civil structure condition assessment by FE model updating: Methodology and case studies. <i>Finite Elem Anal Des.</i> 2001;37(10):761-775. doi:10.1016/S0168-874X(00)00071-8

### Investigated Structure / Model



### Results

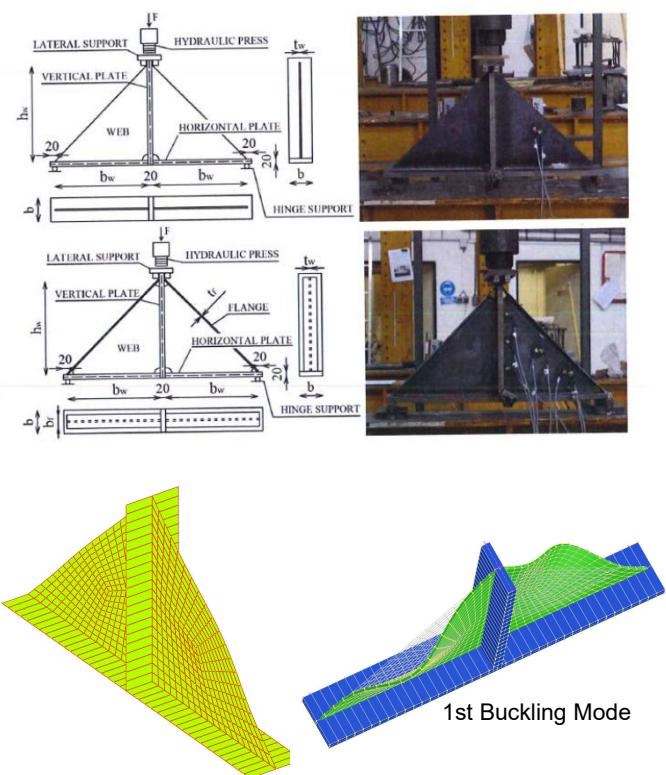


### Comments

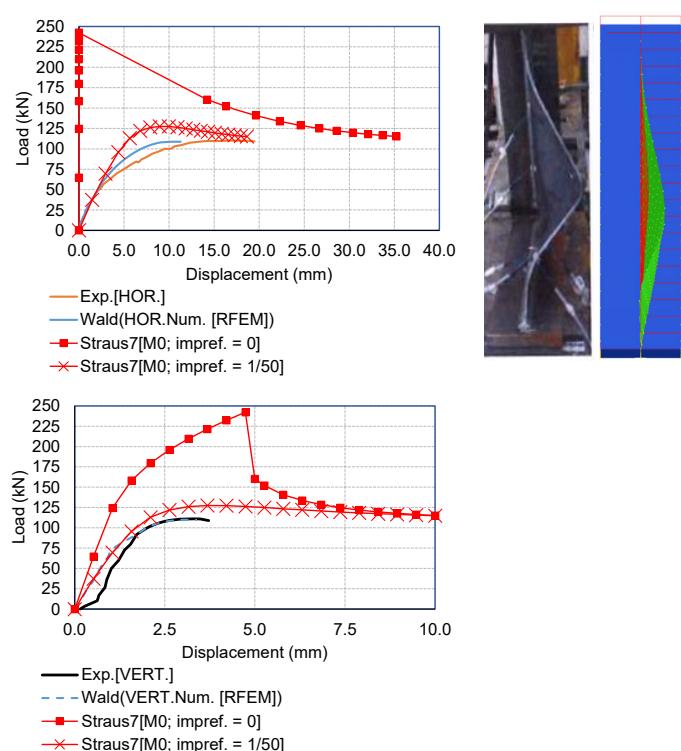
The numerical investigation addressed steel portal frame (steel strips) tested under impulse excitation to get modal information of the structure. The experimental modal analysis was performed on the frame before and after cutting the steel strips at four points. Agreement was found, for modal shape and frequency values, both considering experimental and numerical independent results.

Source	Personal Archive
Elements	SHELL
Software	Straus-7
Material	Elasto-Plastic
Analysis	Non-Linear Static (Material+Geometry)
Reference Model [Experimental]	Wald F. <i>Benchmark Cases For Advances Design of Structural Steel Connections</i> . Ceska technika - nakladatelstvi CVUT; 2016.
Reference Model [Analytic./Num.]	Wald F. <i>Benchmark Cases For Advances Design of Structural Steel Connections</i> . Ceska technika - nakladatelstvi CVUT; 2016.

### Investigated Structure / Model



### Results

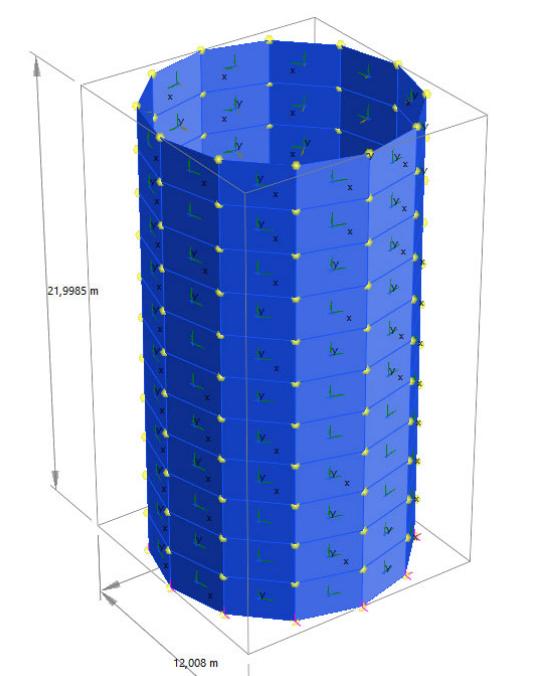


### Comments

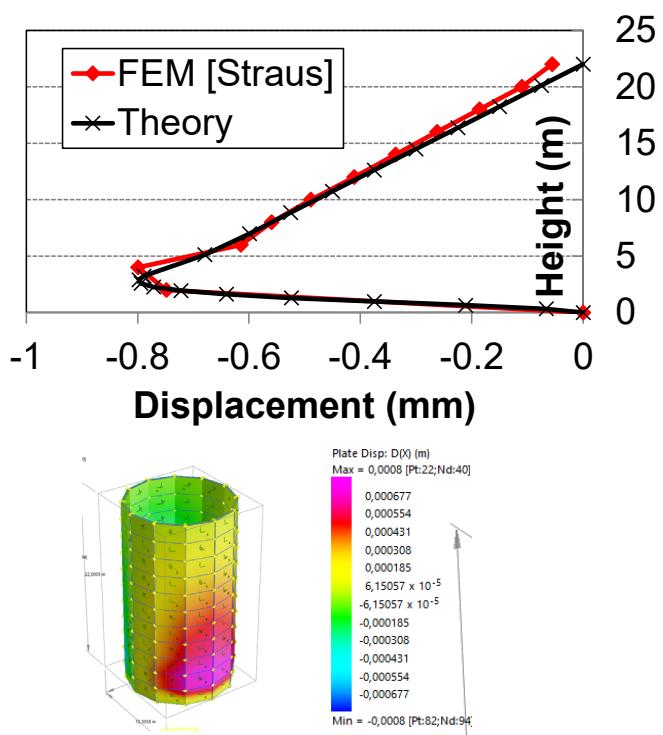
The numerical investigation addressed steel haunch, i.e. triangular stiffeners used at beam-to-column connection. Test condition was such that buckling failure of the haunch was promoted. The scope of numerical investigation was to validate non-linear analysis (non-linearity was both expected to occur from material and geometry) considering, also, initial imperfection which assumed (i) first buckling mode and (ii) 1/50 of the diagonal dimension as magnitude of the initial deformation, according to Annex C of EN1993-1-5:2006. Agreement with respect to both experimental and independent numerical results was found.

Source	Personal Archive
Elements	SHELL
Software	Straus-7
Material	Linear-Elastic
Analysis	Linear-Static
Reference Model [Experimental]	NA
Reference Model [Analytic./Num.]	Timoshenko S. <i>Plate and Shells</i> . McGraw-Hill; 1959.

### Investigated Structure / Model



### Results

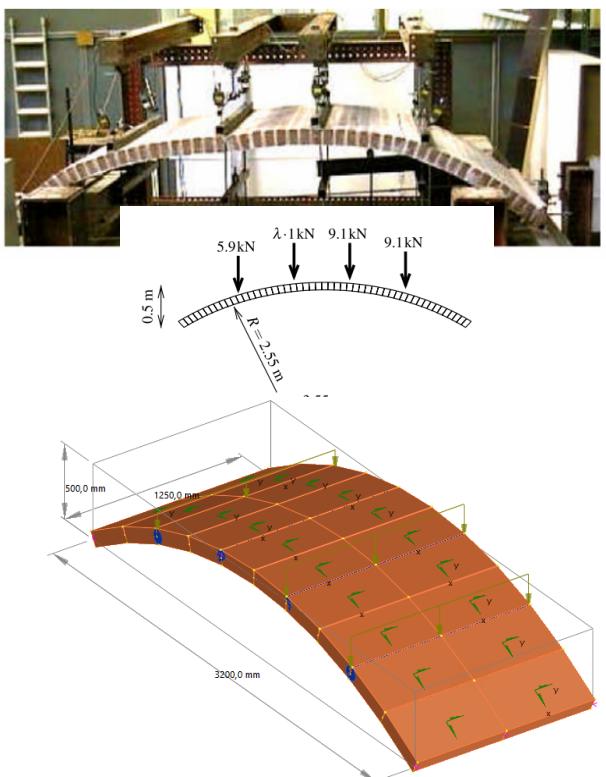


### Comments

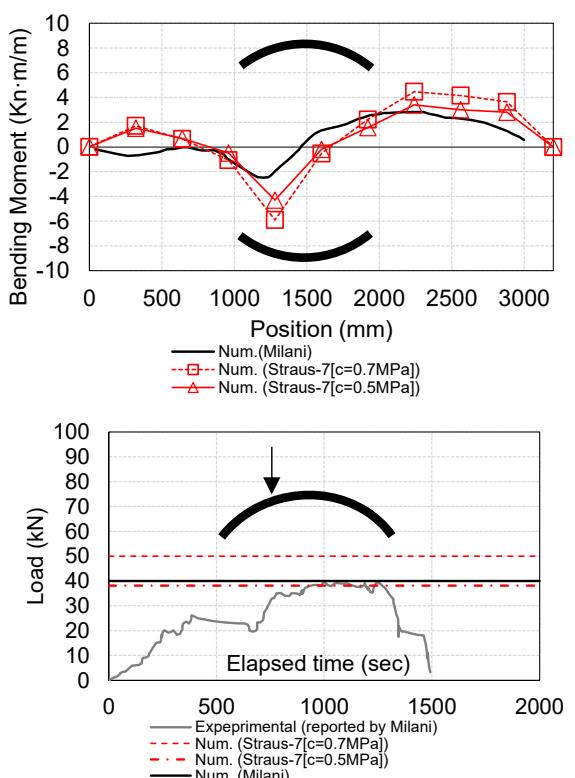
The scope of the numerical investigation was to verify the ability of shell elements, implemented in STRAUS-7, in reproducing the displacement field of the cylindrical shell under water-type pressure distribution (internal). Agreement with respect to analytically-derived results was found.

<b>Source</b>	Personal Archive
<b>Elements</b>	SHELL
<b>Software</b>	Straus-7
<b>Material</b>	Non-Linear Brick (Mohr-Coulomb)
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	NA (Reported by Milani, 2008)
<b>Reference Model [Analytic./Num.]</b>	Milani E, Milani G, Tralli A. Limit analysis of masonry vaults by means of curved shell finite elements and homogenization. <i>Int J Solids Struct.</i> 2008;45(20):5258-5288. doi:10.1016/j.ijsolstr.2008.05.019

### Investigated Structure / Model



### Results

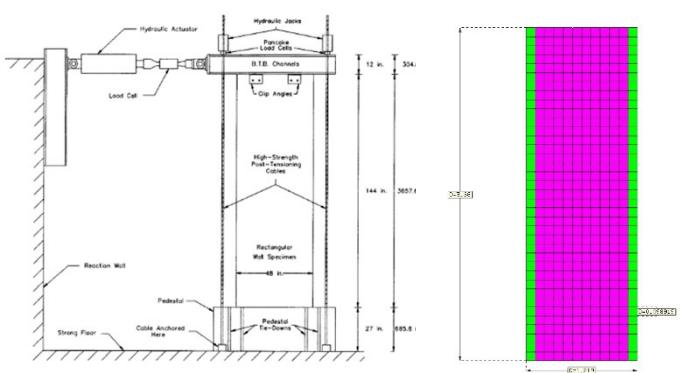


### Comments

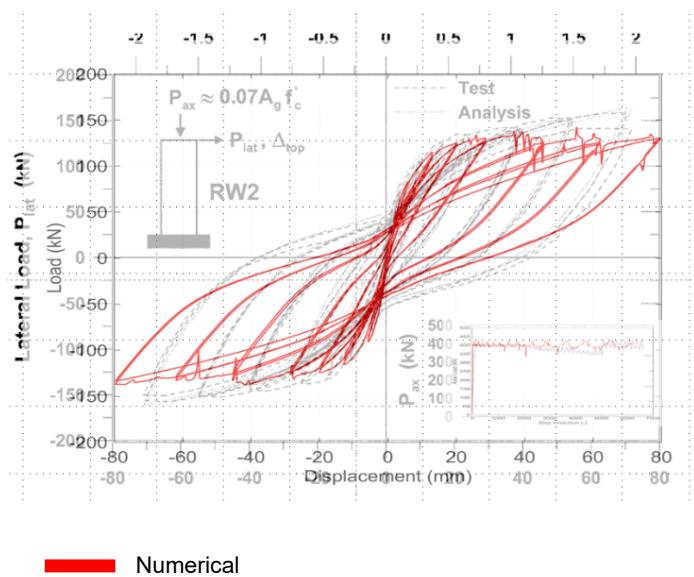
The numerical investigation addressed masonry arch tested up to collapse. Scope of the investigation was to show how simple Mohr-Coulomb (MC) criterion combined with rectangular finite elements (arch was discretized by 10 segments) can be useful tool in predicting the load-carrying capacity. Joints were not modeled. Calibration of the MC's cohesion parameter was needed whereas friction angle was kept equal to 45°. Agreement with respect to both experimental and independent numerical (Milani, 2008 using curved shell element) results was found.

<b>Source</b>	Personal Archive
<b>Elements</b>	SHELL (MultiLayer)
<b>Software</b>	OPEN SEES
<b>Material</b>	Non-Linear Concrete
<b>Analysis</b>	Non-Linear Quasi-Static
<b>Reference Model [Experimental]</b>	Thomsen J, Wallace JW. Displacement-Based Design of Slender Reinforced Concrete Structural Walls - Experimental Verification. <i>J Struct Eng (United States)</i> . 2015;9445(April 2004):1562-1569. doi:10.1061/(ASCE)0733-9445(2004)130
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



### Results

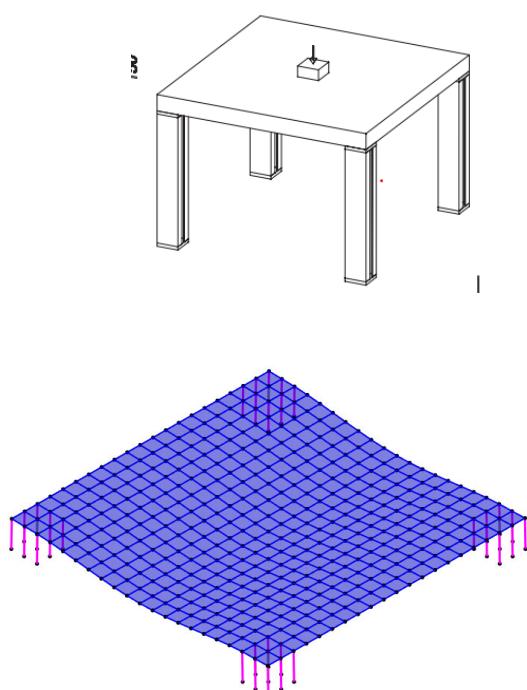


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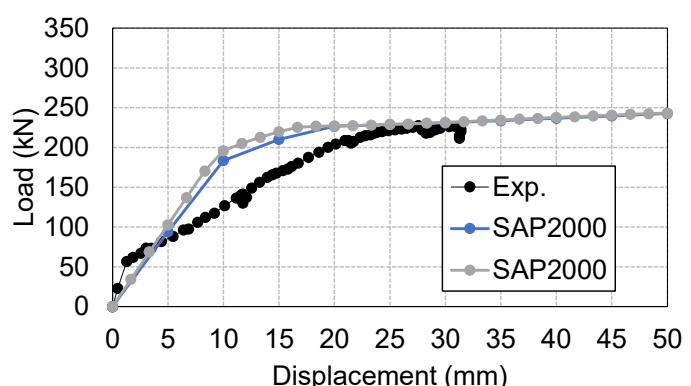
The numerical investigation addressed an RC shear wall (flexural critical) tested cyclically. The wall was modeled using multi-layer shell element, viz. concrete layer coupled with reinforcement layers. Agreement with respect to experimental result was found both for backbone and hysteresis characteristic of the load-to-displacement curve.

<b>Source</b>	Personal Archive
<b>Elements</b>	SHELL(Multi-Layer)
<b>Software</b>	SAP2000
<b>Material</b>	Non-Linear Concrete / Non-Linear Steel
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	di Prisco M, Colombo M, Pourzarabi A. Biaxial bending of SFRC slabs: Is conventional reinforcement necessary? Mater Struct Constr. 2019;52(1):1-15. doi:10.1617/s11527-018-1302-0
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



### Results

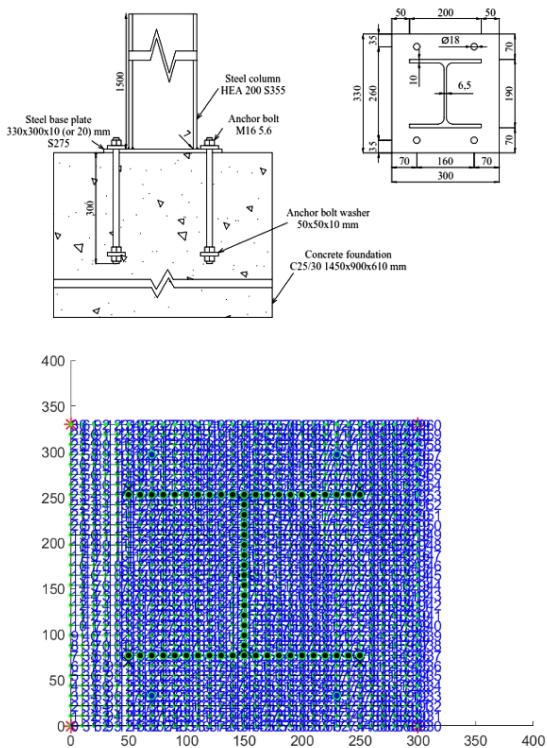


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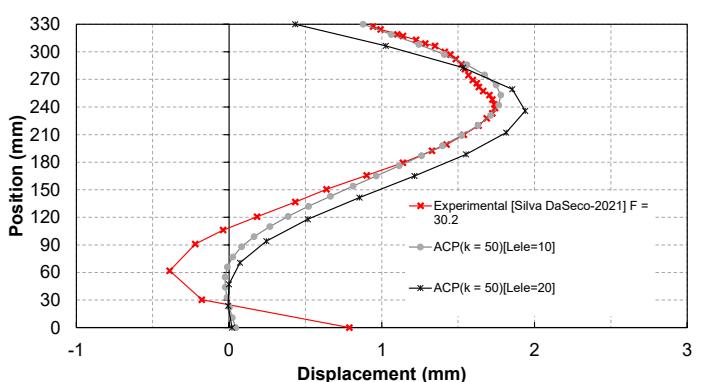
The numerical investigation addressed an RC slab (flexural critical). The slab was modeled using multi-layer shell element, viz. concrete layer coupled with reinforcement layers. Agreement was found with respect to the predicted load-carrying capacity. Difference in stiffness are recognizable, most probably due to lack of modeling correspondence of restraints conditions.

Source	Personal Archive
Elements	PLATE
Software	Flexible Base Plate (Developed by A. Marchisella)
Material	Linear Elastic steel / Compression-only concrete
Analysis	Non-Linear Static
Reference Model [Experimental]	Da Silva Seco L, Couicha M, Hjiaj M, Neves LC, Column base-plates under biaxial bending moment. Eng Struct. 2021;231(January). doi:10.1016/j.engstruct.2020.111386
Reference Model [Analytic./Num.]	NA

### Investigated Structure / Model



### Results

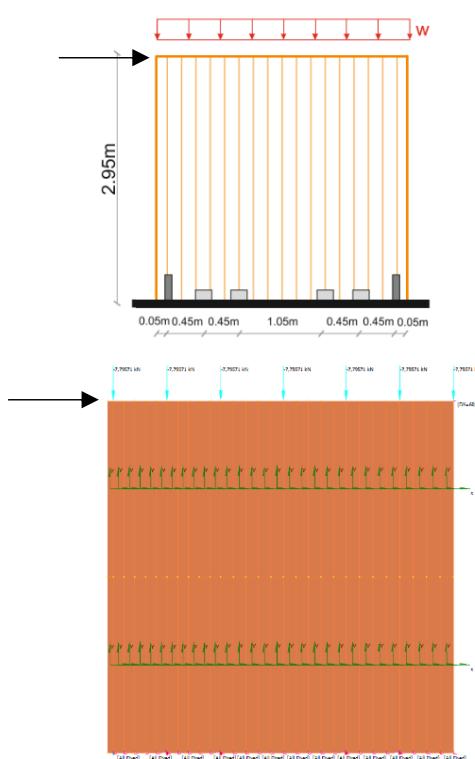


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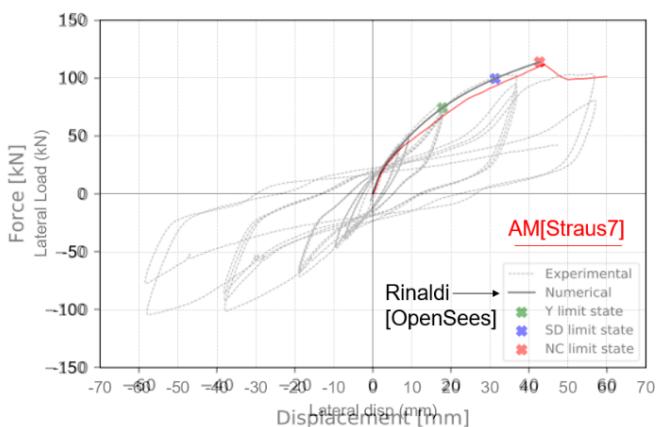
The numerical investigation addressed column base-plate tested under uni-axial bending. Steel plate was modeled using shell elements. Anchors were modeled using springs. Concrete pad was modeled using compression-springs. Attached element was not explicitly modeled but a kinematic constraint was given to all the nodes belonging to the profile's footprint. Agreement was found with respect to experimental displacements (measured via digital-image-correlation). Results slightly depended on the adopted mesh size.

<b>Source</b>	Personal Archive
<b>Elements</b>	SHELL / SPRINGS
<b>Software</b>	STRAUS 7
<b>Material</b>	Linear Elastic (Ortho) / Non-Linear Spring
<b>Analysis</b>	Non-Linear Static
<b>Reference Model [Experimental]</b>	Gavric I. Seismic Behavior of Cross-Laminated Timber Buildings. 2011.
<b>Reference Model [Analytic./Num.]</b>	Rinaldi V. The Seismic Behavior of CLT Timber Buildings: Evaluation of the Behavior Factor for the Revision of Eurocode 8. 2021.

### Investigated Structure / Model



### Results

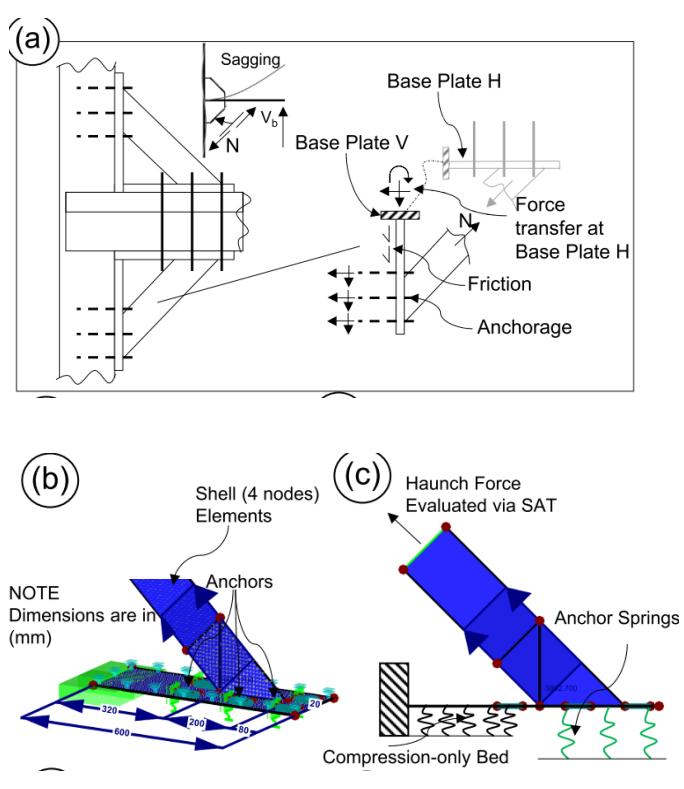


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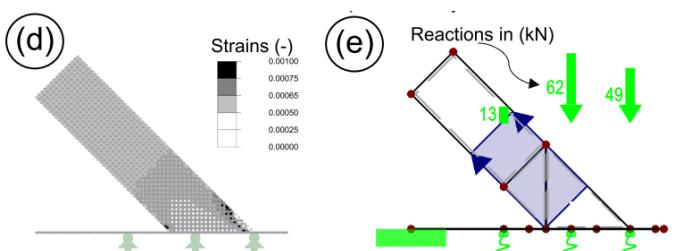
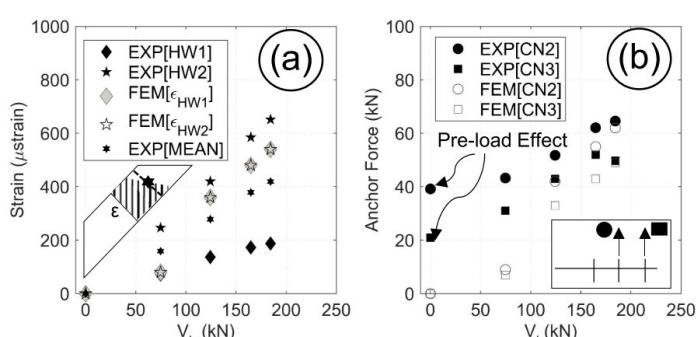
The scope of the numerical investigation was to verify the reliability of modeling metal devices (hold-down and angle brackets) used to connect the timber panel to concrete foundation as uni-axial springs. Constitutive laws, given to the springs, were non-linear. Agreement with respect to both experimental and independent numerical results was found.

<b>Source</b>	Marchisella A. Seismic Assessment of Existing 3D RC Beam-Column Joints and Retrofit with Fully Fastened Haunch. 2022. <a href="http://hdl.handle.net/10589/187062">http://hdl.handle.net/10589/187062</a> .
<b>Elements</b>	SHELL / SPRINGS
<b>Software</b>	RFEM
<b>Material</b>	Linear-Elastic steel / Non-Linear Spring
<b>Analysis</b>	Linear-Static
<b>Reference Model [Experimental]</b>	Marchisella A. Seismic Assessment of Existing 3D RC Beam-Column Joints and Retrofit with Fully Fastened Haunch. 2022. <a href="http://hdl.handle.net/10589/187062">http://hdl.handle.net/10589/187062</a> .
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



### Results

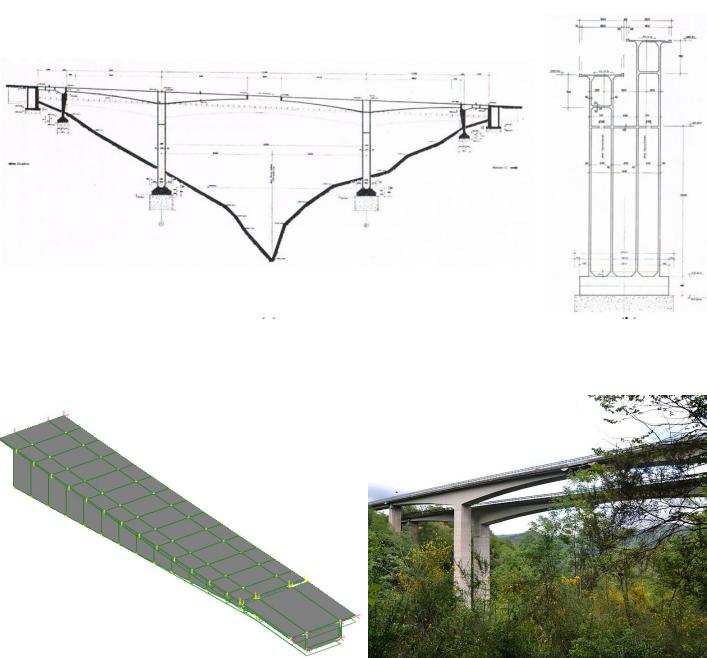


### Comments

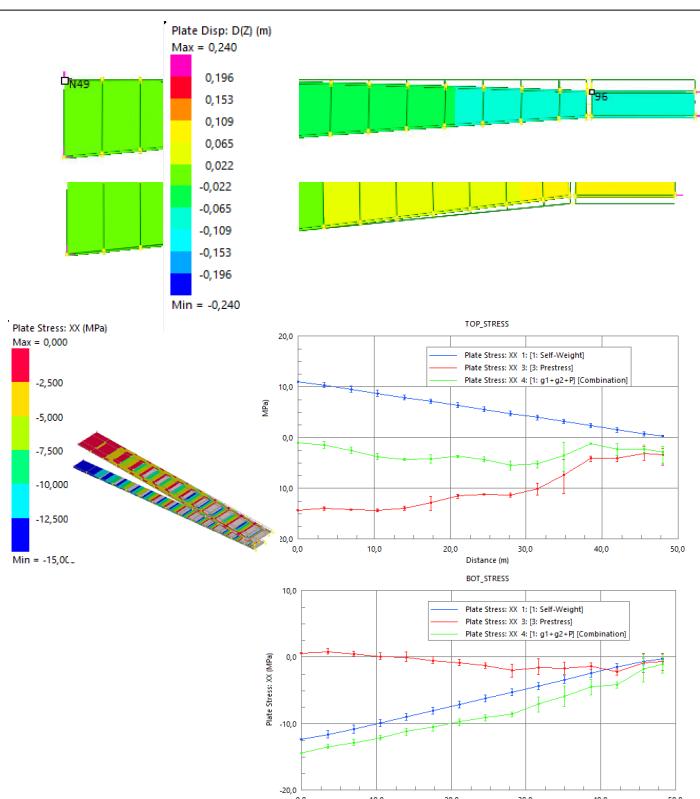
The numerical investigation addressed haunch element used to retrofit RC beam-column joint. Sub-modeling technique was employed, in only the a convenient static equivalent portion of the sub-assemblage was analyzed. Comparison of both strains and anchors' forces was possible showing a good agreement only for the latter.

<b>Source</b>	Personal Archive
<b>Elements</b>	Shell
<b>Software</b>	Straus 7
<b>Material</b>	Concrete (Linear-Elastic)
<b>Analysis</b>	Linear Static
<b>Reference Model [Experimental]</b>	C. Cestelli-Guidi, "Viadotto Grottalunga," in <i>Prestressed Concrete (In Italian)</i> , Hoepli, 1987.
<b>Reference Model [Analytic./Num.]</b>	C. Cestelli-Guidi, "Viadotto Grottalunga," in <i>Prestressed Concrete (In Italian)</i> , Hoepli, 1987.

### Investigated Structure / Model



### Results



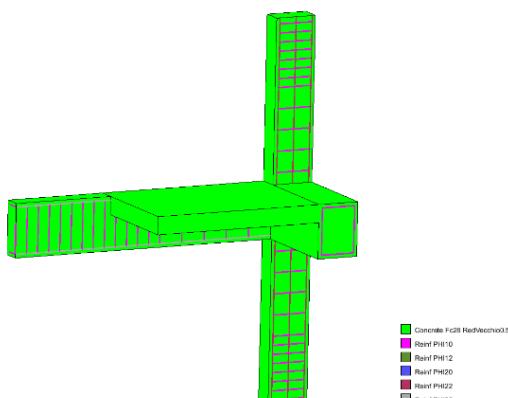
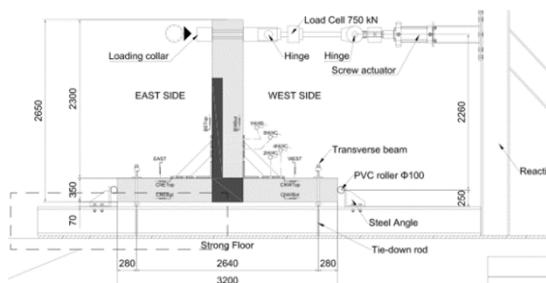
### Comments

The numerical investigation addressed prestressed concrete cantilever viaduct. Shell elements were used to investigate possible occurrence of shear-lag effect. Prestressing was introduced with equivalent tendons considering the actual eccentricity with respect to the box-girder cross section. Comparison was possible only for compressive stress of concrete (under service condition) which was reported, in reference document, not larger than 15 MPa. Numerically-derived strains agreed with such reference value.

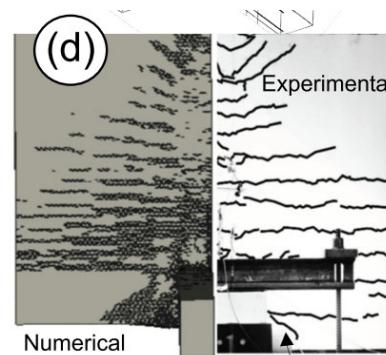
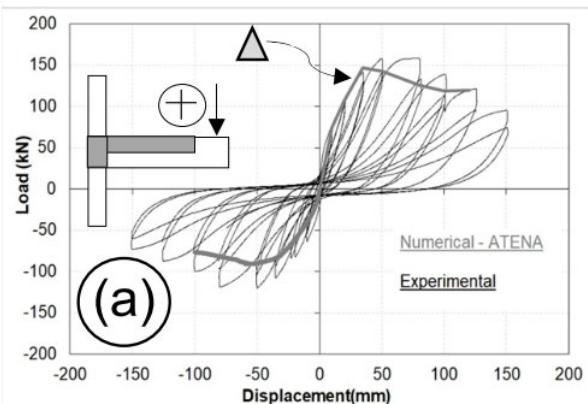
## **3D – BRICK / AXISYMMETRIC**

<b>Source</b>	Marchisella A. Seismic Assessment of Existing 3D RC Beam-Column Joints and Retrofit with Fully Fastened Haunch. 2022. <a href="http://hdl.handle.net/10589/187062">http://hdl.handle.net/10589/187062</a> .
<b>Elements</b>	3D brick
<b>Software</b>	ATENA
<b>Material</b>	Non-linear concrete (smeared crack) / Non-Linear steel reinforcement (perfect bond)
<b>Analysis</b>	Non-linear
<b>Reference Model [Experimental]</b>	Marchisella A, Muciaccia G, Sharma A, Eligehausen R. Experimental investigation of 3d RC exterior joint retrofitted with FFHR. Eng Struct. 2021;239(July):112206. doi:10.1016/j.engstruct.2021.112206
<b>Reference Model [Analytic./Num.]</b>	NA

### Investigated Structure / Model



### Results

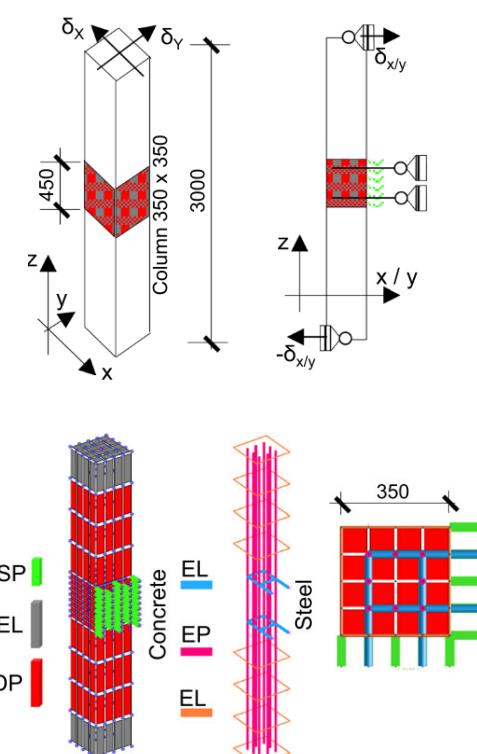


### Comments

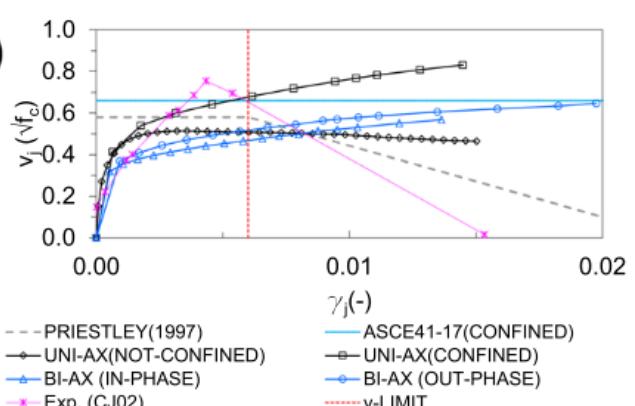
The numerical investigation addressed an exterior RC beam-column joint with slab of transverse beam. Three-dimensional model was employed to investigate the torsional behavior of the transverse beam. Agreement with respect to experimental result was found both for load-carrying capacity and non-symmetric load-to-displacement response.

<b>Source</b>	A. Marchisella and G. Muciaccia, "Bi-axially loaded RC beam-column joints and haunch retrofit," Bull. Earthq. Eng., doi:10.1007/s10518-024-01881-5, 2024.
<b>Elements</b>	3D bricks
<b>Software</b>	STRAUS-7
<b>Material</b>	Drucker–Prager
<b>Analysis</b>	Non-Linear
<b>Reference Model [Experimental]</b>	A. Marchisella and G. Muciaccia, "Bi-axially loaded RC beam-column joints and haunch retrofit," Bull. Earthq. Eng., doi:10.1007/s10518-024-01881-5, 2024.
<b>Reference Model [Analytic./Num.]</b>	A. Marchisella and G. Muciaccia, "Bi-axially loaded RC beam-column joints and haunch retrofit," Bull. Earthq. Eng., doi:10.1007/s10518-024-01881-5, 2024.

### Investigated Structure / Model



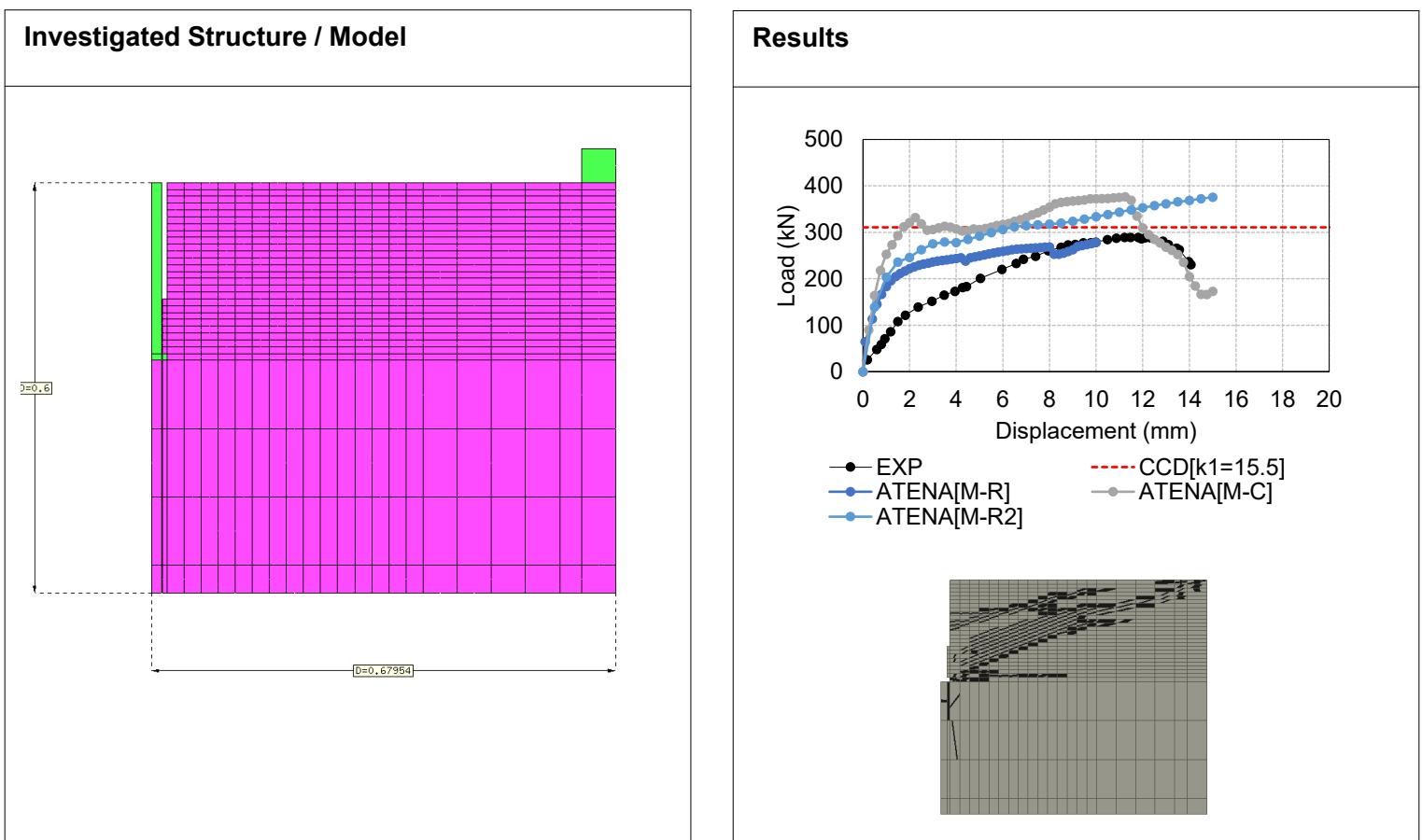
### Results



### Comments

See A. Marchisella and G. Muciaccia, "Bi-axially loaded RC beam-column joints and haunch retrofit," Bull. Earthq. Eng., doi:10.1007/s10518-024-01881-5, 2024.

<b>Source</b>	Personal Archive
<b>Elements</b>	Axisymmetric
<b>Software</b>	ATENA
<b>Material</b>	Non-Linear concrete
<b>Analysis</b>	Non-Linear
<b>Reference Model [Experimental]</b>	Eligehausen R, Sawade G. A fracture mechanics based description of the pull-out behavior of headed studs embedded in concrete. <i>Fract Mech Concr Struct.</i> 1989;281-299. doi:10.18419/opus-7930
<b>Reference Model [Analytic./Num.]</b>	



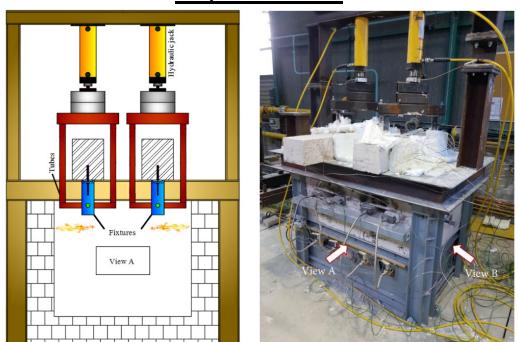
**Comments**

The numerical investigation addressed a single anchor (headed stud) tested under tensile load. Axisymmetric model was employed. Agreement with respect to experimental result was found for load-carrying capacity. Lack of accuracy in stiffness prediction was most probably due to inability of reproducing large compressive strain at the head zone. Differences associated to meshes were recognized.

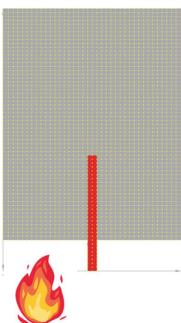
<b>Source</b>	Personal Archive
<b>Elements</b>	3D bricks, 2D planes
<b>Software</b>	STRAUS-7
<b>Material</b>	Concrete and Steel temperature dependent conductivity and specific heat
<b>Analysis</b>	Thermal - Transient
<b>Reference Model [Experimental]</b>	O. Al-Mansouri <i>et al.</i> , "Numerical investigation of parameters influencing fire evaluation tests of chemically bonded anchors in uncracked concrete," <i>Eng. Struct.</i> , vol. 209, no. January, p. 110297, 2020.
<b>Reference Model [Analytic./Num.]</b>	O. Al-Mansouri <i>et al.</i> , "Numerical investigation of parameters influencing fire evaluation tests of chemically bonded anchors in uncracked concrete," <i>Eng. Struct.</i> , vol. 209, no. January, p. 110297, 2020.

### Investigated Structure / Model

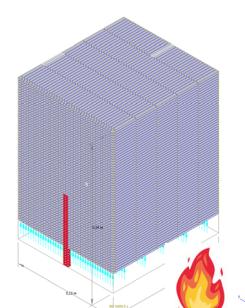
#### Experimental



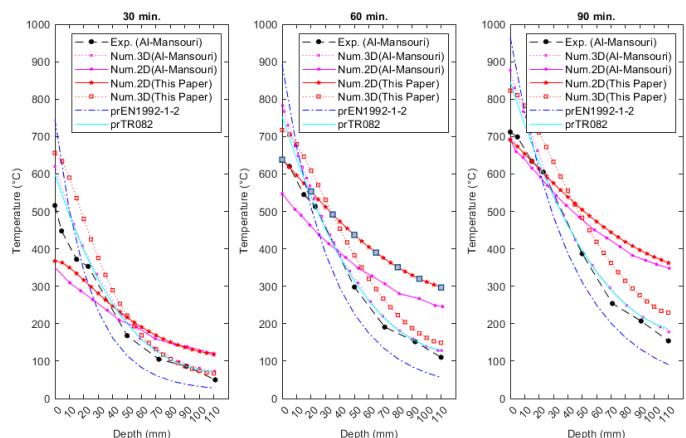
#### 2D Plane



#### 3D



### Results

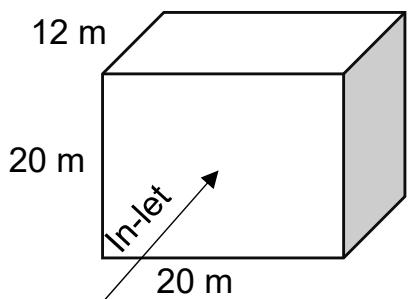
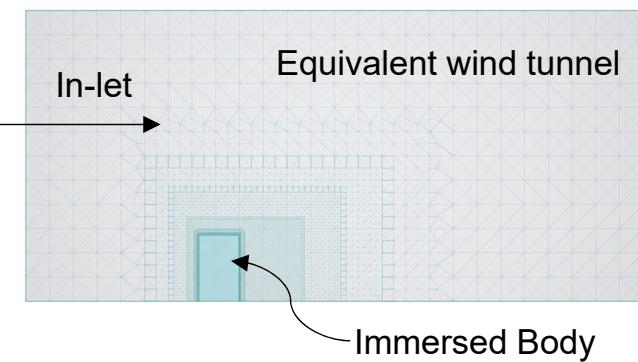


### Comments

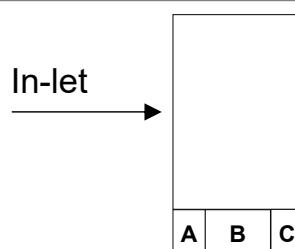
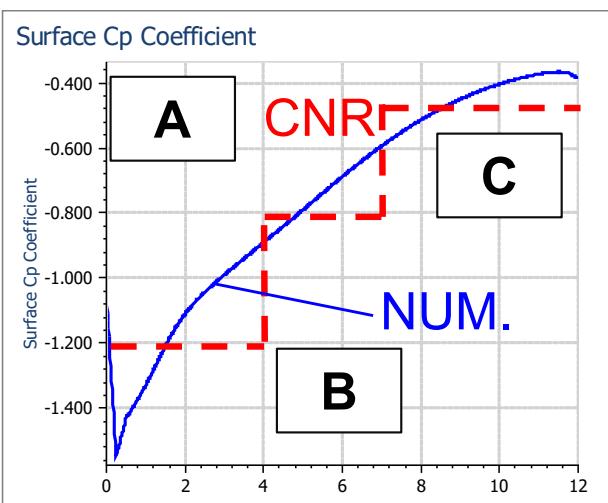
The numerical investigation addressed thermal profiles for concrete member where an anchor (bonded) is embedded. Both 2D plane elements and 3D bricks were employed. The bottom surface of the concrete member is exposed to ISO-384 fire. Transient heat analysis is performed. Agreement with respect to experimental result was found for temperature profile. 3D analysis give more accurate temperature if compared to experiments. 2D overestimates temperature due to absence of heat flow in the out-of-plane direction.

<b>Source</b>	Personal Archive
<b>Elements</b>	3D Brick
<b>Software</b>	RRWIND (see Dlubal. RWIND Generation of Wind-Induced Loads on General Models. 2012)
<b>Material</b>	Incompressible turbulent flow – Static Body (without aeroelastic effect)
<b>Analysis</b>	Computational Fluid Dynamics (CFD)
<b>Reference Model [Experimental]</b>	NA
<b>Reference Model [Analytic./Num.]</b>	CNR. CNR-DT 207/2008 Istruzioni per la valutazione delle azioni e degli effetti del vento sulle costruzioni. 2008.

### Investigated Structure / Model



### Results

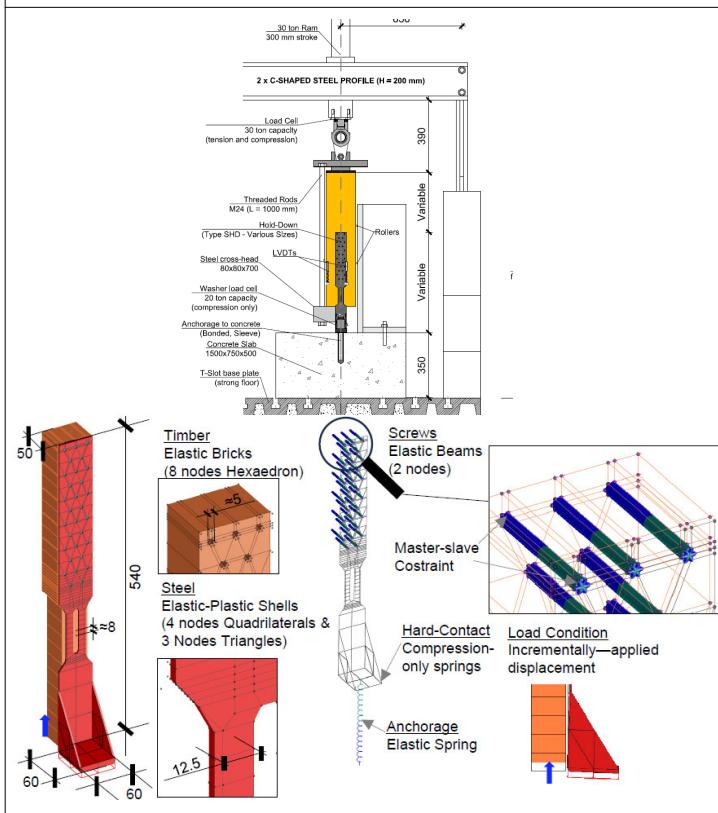


### Comments

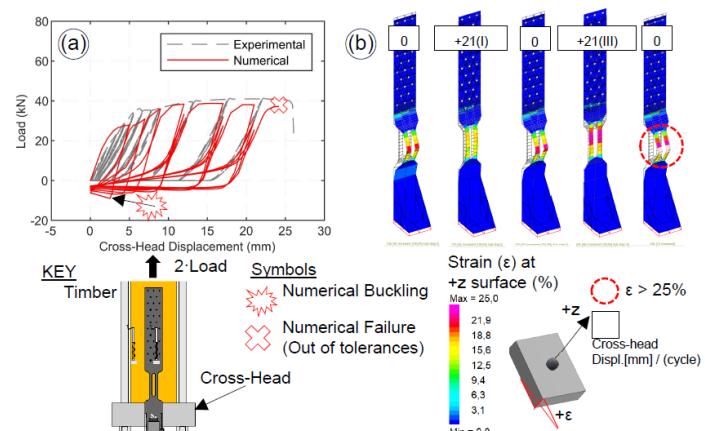
The numerical investigation addressed the problem of a building under wind load condition. A fluid-mechanics simulation of the flow around objects in an equivalent wind tunnel was applied. Comparison of pressure coefficients was made with respect to provisions provided by an Italian technical document addressing wind effect on structures.

<b>Source</b>	Personal Archive
<b>Elements</b>	3D bricks; SHELLS
<b>Software</b>	STRAUS-7
<b>Material</b>	Elastic-Plastic Steel; Linear-Elastic Timber; Mohr-Coulomb Friction pad; Linear-Elastic Beams (Connectors)
<b>Analysis</b>	Non-Linear (material and geometry) quasi static
<b>Reference Model [Experimental]</b>	A. Marchisella, M. Cervio, and G. Muciaccia, "Seismic Design and Experimental Investigation of a New Timber Hold-Down Connection," in 17th World Conference on Earthquake Engineering, 17WCEE, 2020, pp. 1–12.
<b>Reference Model [Analytic./Num.]</b>	Not Applicable

### Investigated Structure / Model



### Results



### Comments

The numerical investigation addressed uniaxial behavior of hold-down connection designed for seismic applications in cross-laminated-timber buildings. Test conditions were cyclic. Agreement is found between experimental results and numerically-derived ones although buckling of the flange during up-lift displacement recovering has been observed only numerically.