

1 Introduction

When a model is called “higher order”, we usually associate it with being more accurate than a first order model. This is not always the case. Adding complexity to a model does not necessarily improve it, as is demonstrated in the class of higher order traffic models developed with the intention of improving the first order traffic model proposed by Lighthill and Whitham (1955) and Richards (1956). As Daganzo observes in his paper,

“A new theory (e.g. relativity) is deemed successful if it explains previously unexplained phenomena, plus everything else that was correctly explained with the theory it intends to replace (e.g. Newtonian physics). In the case of traffic flow, the new theories (high-order fluid models) fail to explain the behavior of traffic at the end of a queue (unlike the simpler, older LWR model; which explains it perfectly).”

In this paper we examine the second order traffic model developed by Payne (1971) and Whitham (1974) which was meant to improve how the LWR model explains traffic behavior near shocks. Their model takes its form from equations used to describe compressible fluid dynamics. Unfortunately, cars and fluid particles have some fundamental differences which make the model actually perform worse than the LWR model in certain cases. For example, by smoothing out discontinuities, the PW model predicts negative velocities, which is clearly a problem.

In addition to considering the PW model, we also take a look at a more successful model proposed by Aw and Rascle (2000). These authors challenge some of the assumptions of the PW model and suggest the use of a convective derivative to fix the problem of negative velocities. In order to verify that their model is valid, they test their new model against criteria they claim any reasonable model will satisfy.

2 LWR Model

We can start by considering a first order (one equation) model of traffic flow on a one-way highway without any exits, entrances, or passing. In this case, we can expect that the number of cars will be conserved, so we can use the equation for conservation of mass (with density ρ and velocity v):

- (a) Integral form of equation: $\frac{d}{dt} \int_{x_1}^{x_2} \rho dt = -[f(\rho)]_{x_1}^{x_2}$
- (b) Differential form of equation: $\rho_t + f(\rho)_x = 0$
 - i Light traffic: $\rho_t + (\rho v)_x = 0$
 - ii Congested traffic: $\rho_t + \left(\rho V(\rho)\right)_x = 0$ (LWR model)

The LWR behaves well macroscopically, but it does have some flaws. For example, it assumes cars change their velocity instantaneously as they travel through shocks. One way to eliminate shocks would be to add a diffusion term: $\rho_t + \left(\rho V(\rho)\right)_x = \mu \rho_{xx}$. This term is meant to account for the drivers awareness of the road ahead. However, this model can be shown to predict negative velocities in some instances, which is obviously wrong.

3 PW Model

3.1 Theory

Another approach to improving the LWR model would be to use a second order (two equation) model. Since cars can be thought of as a compressible gas, we can use equations for conservation of mass (above) and conservation of momentum, ρv , used to model compressible gas flow:

(a) Integral form of equation: $\frac{d}{dt} \int_{x_1}^{x_2} \rho v dt = - \left[f(\rho v) \right]_{x_1}^{x_2}$

(b) Differential form of equation: $(\rho v)_t + f(\rho v)_x = (\rho v)_t + \left(\rho v^2 + p \right)_x = 0$

We can rewrite the second equation in terms of velocity instead of momentum: $v_t + v v_x + \frac{p'(\rho)}{\rho} \rho_x = 0$.

The PW model is a modification of these equations for conservation of mass and conservation of momentum in gas dynamics, with added relaxation and diffusion terms:

$$\begin{cases} \rho_t + (\rho v)_x = 0 \\ v_t + v v_x + \frac{p'(\rho)}{\rho} \rho_x = \frac{V(\rho) - v}{\tau} + \mu v_{xx} \end{cases}$$

At first glance, this seems like a reasonable model. However, there are a couple of fundamental differences between gas particles and cars that could be problematic. For example, as pointed out by Daganzo, “a fluid particle responds to stimuli from the front and from behind, but a car is an anisotropic particle that mostly responds to frontal stimuli.” If we consider the eigenvalues of the Jacobian matrix of the linearized system, we see that one of the eigenvalues, $\lambda_2 = v + \sqrt{p'(\rho)}$, represents information traveling faster than the velocity of cars in the system. This implies that traffic conditions are partially determined by what is going on behind.

3.2 Hugoniot Loci and Integral Curves

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4 AR Model

4.1 Theory

Another issue with the PW model, as Aw and Rascle point out in their paper, is that there is no conservation of momentum in car traffic. Instead, the term involving pressure is meant to represent an anticipation factor, or how a driver would react to a variation in the concentration of cars with respect to space. However, what we should really be concerned with is the perspective of the driver, which is relative to a moving timeframe. In this case, we should be using a convective derivative, $\partial_t + v \partial_x$, of the pressure. The new model becomes:

$$\begin{cases} \rho_t + (\rho v)_x = 0 \\ (v + p)_t + v(v + p)_x = 0 \end{cases}$$

The second equation can also be rewritten as an equation for velocity: $v_t + (v - \rho p'(\rho))v_x = 0$.

This updated model no longer conserves momentum. Instead, it conserves the quantity $y = v + p(\rho)$, which we can see if we rearrange the second equation to a conservation form: $(\rho(v + p(\rho)))_t + (\rho v(v + p(\rho)))_x = 0$. While the authors admit that there is no obvious physical interpretation of this quantity, they claim that it is the most natural pair of conservative variables.

The authors also claim that their improved model satisfies the following important conditions:

1. The system is hyperbolic.
2. When solving the Riemann problem with bounded nonnegative data (ρ, v) , the density and velocity must remain nonnegative and bounded from above.
3. When solving the Riemann problem, no waves connecting any state to its left (behind it) can have a propagation speed greater than the velocity v .
4. The solution to the Riemann problem must agree with qualitative properties that drivers actually experience: braking produces shock waves and acceleration produces rarefaction waves.
5. Near a vacuum, the solution to the Riemann problem must be sensitive to the data.

4.2 Hugoniot Loci and Integral Curves

The AR model starts from the system

$$\partial_t \rho + \partial_x(\rho v) = 0, \tag{1}$$

$$\partial_t (v + p(\rho)) + v \partial_x (v + p(\rho)) = 0 \tag{2}$$

with $p(\rho) = \rho^\gamma$.

To find the Hugoniot loci and the integral curves, [1] utilizes two different forms of this system. We will examine each of them in turn. What we will find is that the integral curves and the Hugoniot loci coincide, and furthermore that one of the waves is a contact discontinuity. Let us first consider the Hugoniot loci.

4.2.1 Hugoniot Loci

In order to consider the Hugoniot loci for this system we must first write the system in conservation form. To accomplish this, note that multiplying the first equation by $(v + p(\rho))$ and the second equation by ρ gives us the two equations

$$\begin{aligned} (v + p(\rho))\partial_t \rho + (v + p(\rho))\partial_x(\rho v) &= 0, \\ \rho \partial_t (v + p(\rho)) + \rho v \partial_x (v + p(\rho)) &= 0. \end{aligned}$$

Adding these two equations gives

$$\partial_t (\rho (v + p(\rho))) + \partial_x (\rho v (v + p(\rho))) = 0. \tag{3}$$

Then from (1) and (3) we have the system

$$\begin{aligned} \partial_t \rho + \partial_x(\rho v) &= 0, \\ \partial_t (\rho (v + p(\rho))) + \partial_x (\rho v (v + p(\rho))) &= 0. \end{aligned}$$

This can be rewritten as $q_t + f(q)_x = 0$ by defining

$$q = \begin{bmatrix} \rho \\ y \end{bmatrix}, \quad f(q) = \begin{bmatrix} v\rho \\ vy \end{bmatrix}.$$

where $y = \rho(v + p(\rho))$. The Rankine-Hugoniot condition tells us that

$$s(q_* - q) = f(q_*) - f(q).$$

Therefore, from this condition we get the two equations

$$s(\rho_* - \rho) = v_*\rho_* - v\rho, \quad (4)$$

$$s(y_* - y) = v_*y_* - vy. \quad (5)$$

With a little rearranging and by plugging in for y , these two equations can be rewritten as

$$\rho_*(s - v_*) = \rho(s - v), \quad (6)$$

$$\rho_*(s - v_*)(v_* + p(\rho_*)) = \rho(s - v)(v + p(\rho)). \quad (7)$$

From (6), we know that there are two cases:

(a) $\rho_*(s - v_*) = \rho(s - v) = 0$. In this case we have that

$$s - v_* = s - v$$

except if one of the two densities, ρ_* , ρ is zero. WHY DOES THIS NOT MATTER? Therefore, we can say that

$$v_* = v.$$

Since the velocity does not change, this is a contact discontinuity. Using the fact that $v = v_*$ in (5) gives

$$y_*(s - v) = y(s - v).$$

So, either $y = y_*$ or $s = v$. If $y = y_*$ we have a stationary point in the $Y = (\rho, y)$ plane, which does not describe a wave. Therefore, $s = v$. Note that we have no restrictions on y other than its definition. Therefore this loci in the Y plane is given by

$$y = \rho(v_* + p(\rho)).$$

(b) $\rho_*(s - v_*) = \rho(s - v) \neq 0$. In this case, plugging this into (7) gives

$$\rho_*(s - v_*)(v_* + p(\rho_*)) = \rho(s - v)(v + p(\rho))$$

$$\rho(s - v)(v_* + p(\rho_*)) = \rho(s - v)(v + p(\rho))$$

$$v_* + p(\rho_*) = v + p(\rho).$$

Therefore, the Hugoniot loci for this case in the Y plane are given by

$$y = v_* + p(\rho_*),$$

since $y = v + p(\rho)$ by definition. Note that solving (4) for s gives

$$s = \frac{\rho_*v_* - \rho v}{\rho_* - \rho}.$$

Using the fact that $v_* = v + p(\rho) - p(\rho_*)$, we get that

$$s = \frac{\rho_*(v + p(\rho) - p(\rho_*)) - \rho v}{\rho_* - \rho} = v - \rho_* \frac{p(\rho) - p(\rho_*)}{\rho - \rho_*} \approx v - \rho p'(\rho)$$

for $\rho_* \approx \rho$.

In the $U = (\rho, v)$ plane these loci become (a) $v = v_*$, ρ free, and (b) $v = v_* + p(\rho_*) - p(\rho)$. In the $M = (\rho, \rho v)$ plane these loci become (a) $\rho v = \rho_* v_*$, ρ free, and (b) $\rho v = \rho(v_* + p(\rho_*)) - \rho p(\rho)$. Figure 4.2.1 shows the Hugoniot loci in the different planes. TODO: ADD PARAMETERS USED FOR FIGURES? OR, WILL INCLUDING THE CODE MAKE THAT REDUNDANT? IF WE ADD PARAMETERS, MAYBE THE BEST PRESENTATION WOULD BE IN A TABLE?

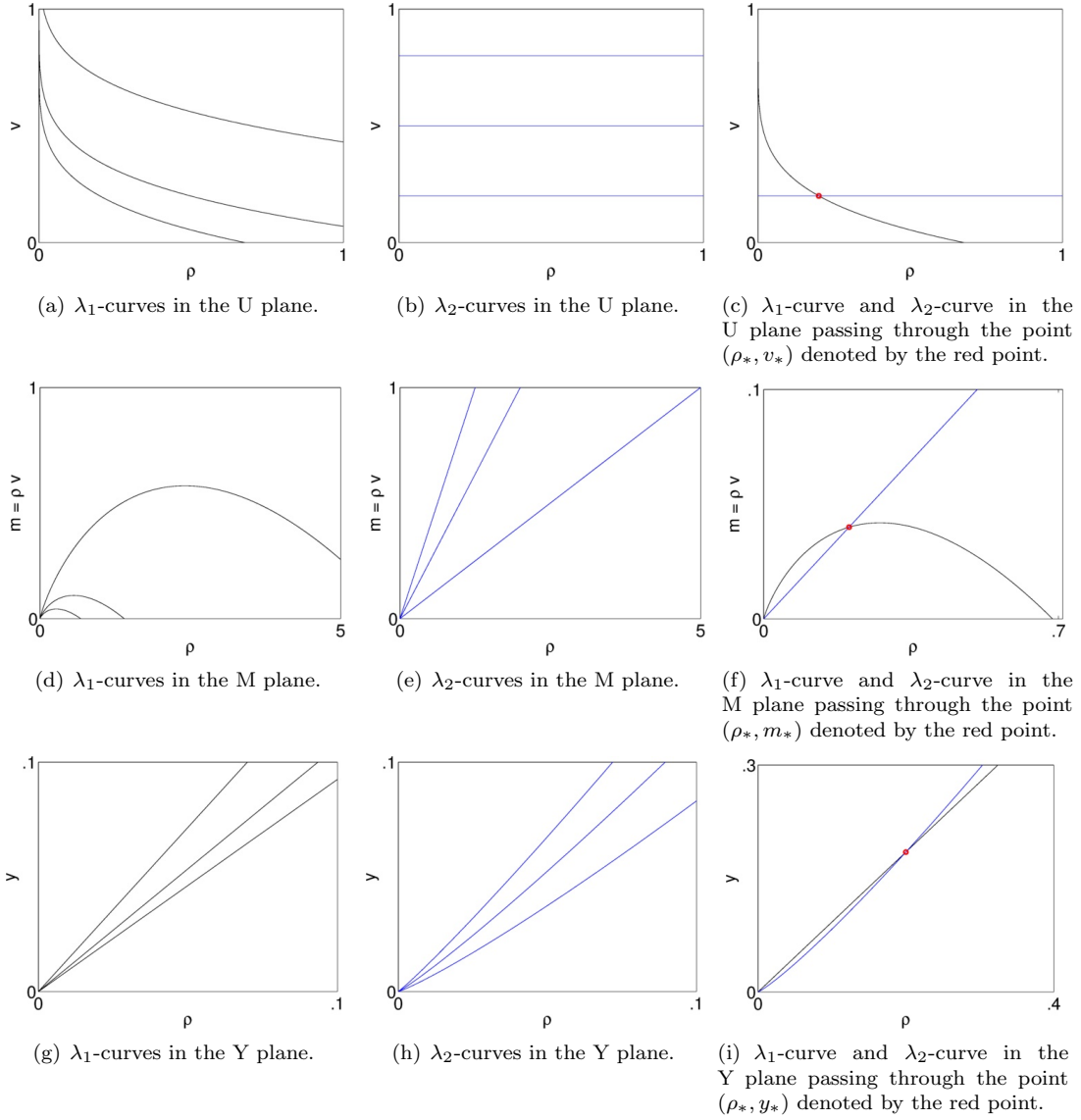


Figure 1: Figures of the Hugonio loci and integral curves for λ_1 and λ_2 in each of the different planes. Since the loci and integral curves coincide, they are both simply called the “curves” in the captions of the above figures. Figures (c), (f), (i) show both curves for a given point in each plane.

4.2.2 Integral Curves

In order to consider the integral curves for this system [1] works from the system

$$\begin{aligned}\partial_t \rho + \partial_x(\rho v) &= 0 \\ \partial_t v + (v - p'(\rho)\rho) \partial_x v &= 0,\end{aligned}$$

where the second equation is found by multiplying (1) by $p'(\rho)$ and subtracting it from (2). This can be rewritten as $q_t + Aq_t = 0$ by defining

$$q = \begin{bmatrix} \rho \\ v \end{bmatrix}, \quad A = \begin{bmatrix} v & \rho \\ 0 & v - p'(\rho)\rho \end{bmatrix}.$$

The eigenvalues of A are $\lambda_1 = v - p'(\rho)\rho$ and $\lambda_2 = v$. Note that since $p(\rho) = \rho^\gamma$ and $\rho \geq 0$, $\lambda_1 < \lambda_2$ so long as $\rho \neq 0$. Also note that if $\rho = 0$ then A is no longer hyperbolic. The eigenvectors of A are

$$r_1 = \begin{bmatrix} 1 \\ -p'(\rho) \end{bmatrix}, \quad r_2 = \begin{bmatrix} 1 \\ 0 \end{bmatrix}.$$

Using equation (13.24) from [2] with $\alpha = 1$ tells us that the integral curves can be found by considering $q'(\xi) = r_p$. For $p = 1$ this gives us the two equations

$$\begin{aligned} \rho'(\xi) &= 1 \\ v'(\xi) &= -p'(\rho), \end{aligned}$$

which can be solved to find that we have parameterized our curve by ρ , and $v = -p'(\rho) + c_1$ while ρ is free, where c_1 is a constant. Since for a given point (ρ_*, v_*) when $\rho = \rho_*$ we want $v = v_*$, we get that $c_1 = v_* + p'(\rho_*)$. Thus, the integral curve is given by

$$v = v_* + p'(\rho_*) - p'(\rho).$$

This coincides with the Hugoniot loci from case (b). For $p = 2$, we get the two equations

$$\begin{aligned} \rho'(\xi) &= 1 \\ v'(\xi) &= 0, \end{aligned}$$

which can be solved to find that we have parameterized our curve by ρ , and that v is a constant. Therefore, $v = v_*$ and ρ is free. This coincides with the Hugoniot loci from case (a).

4.2.3 Regions of Validity

Restrictions on the way that λ must vary across a wave allow us to identify the regions of the Hugoniot loci and integral curves that are valid for any given point. When traveling across a shock from a left state, q_l , to a right state q_r , λ must decrease. When traveling across a rarefaction wave from a left state, q_l , to a right state q_r , λ must increase.

Therefore, it is important to take into account the contour lines of λ when looking at the loci and integral curves. Figures 4.2.3(a) and 4.2.3(d) show the λ_1 -curves in the U and M planes, with the contour lines of λ_1 shown in magenta. This information is used to determine which areas of the λ_1 curves are valid shock waves and which are valid rarefaction waves. The rest of the subfigures show the regions of validity for specific points q_* , depending on whether $q_* = q_l$ or $q_* = q_r$. For these plots, $q_* = (\rho_*, v_*) = (0.2, 0.2)$. Note that the contact discontinuity is valid anywhere in the plane.

5 Examples

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References

- [1] A. Aw and M. Rascle. Resurrection of “second order” models of traffic flow. *SIAM Journal of Applied Math*, 60(3):916938, 2000.
- [2] Randall J. LeVeque. *Finite Volume Methods for Hyperbolic Problems*. Cambridge University Press, 2002.

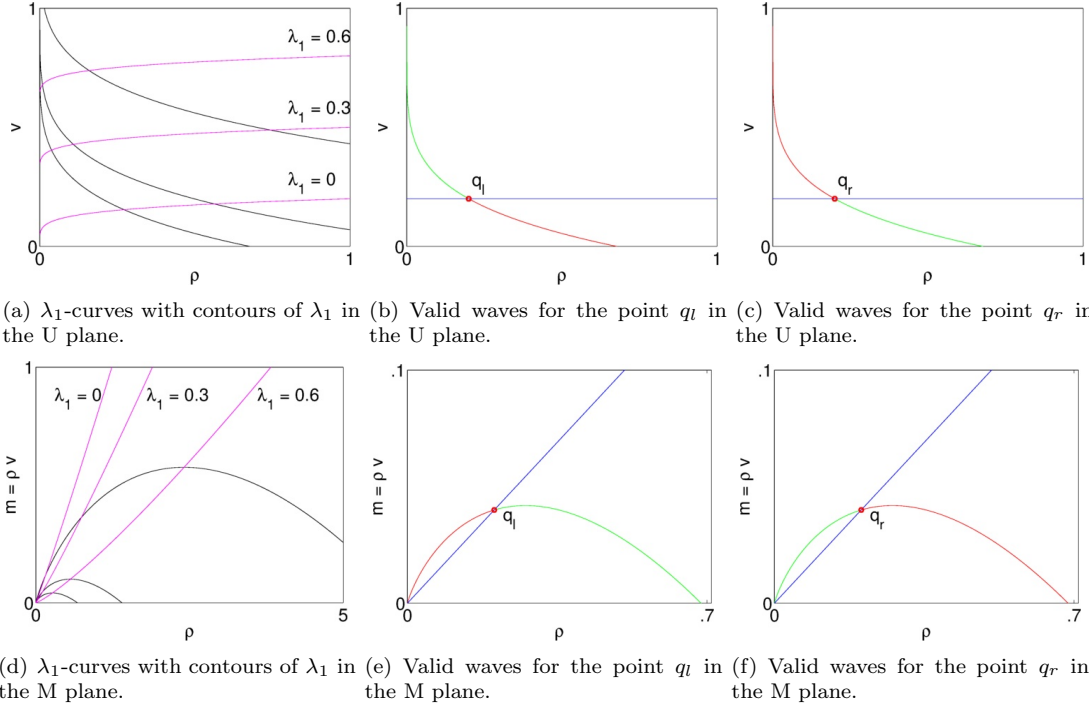


Figure 2: Figures showing the calculation of the valid waves for a given point. Figures (a) and (d) show the λ_1 curves in black with the λ_1 contours in magenta. The other figures show valid shocks in red and valid rarefaction waves in green. The contact discontinuity is shown in blue.