Lab 8 Feedback Amplifier

Part 1: Feedback with Behavioral OTA

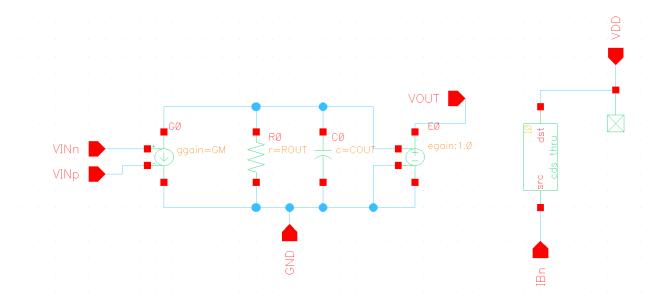


Figure 1 Behavioral Model Schematic

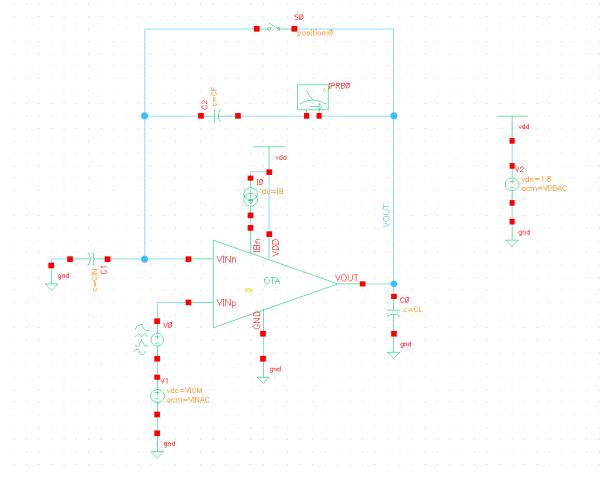


Figure 2 Testbench Schematic

1.1 Closed Loop Gain vs Frequency:

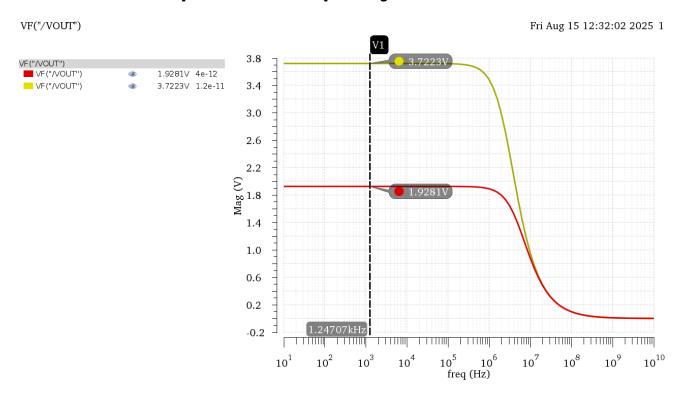


Figure 3 DC Gain in Mag

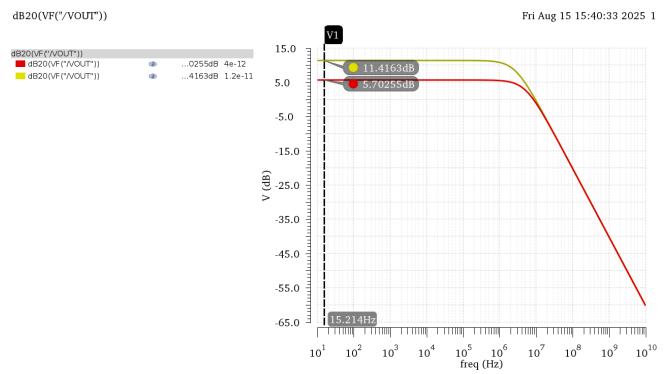


Figure 4 DC Gain in dB

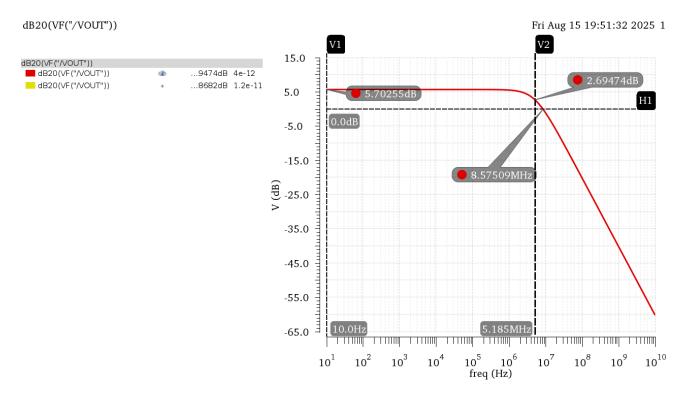


Figure 5 Gain Bode Plot Annotated CIN = 4pF

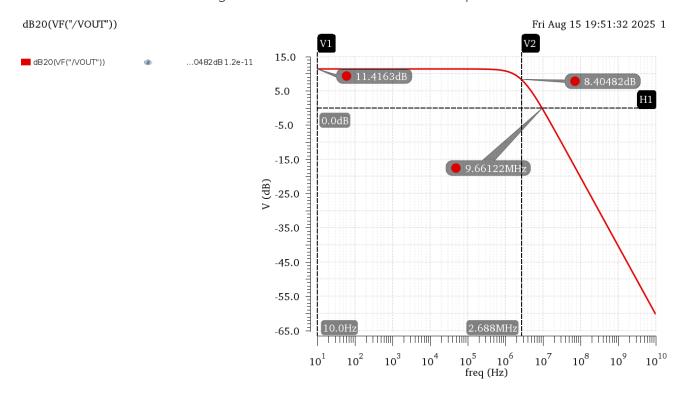


Figure 6 Gain Bode Plot Annotated CIN = 12pF

	CIN = 4pF	CIN = 12pF
DC Gain (dB)	5.703	11.42
DC Gain	1.928	3.722
BW	5.19E+06	2.69E+06
UGF	8.61E+06	9.69E+06
GBW	10E+06	10E+06

Table 1 Results from Simulation

Hand Analysis:

Open Loop Parameters from Last Lab:

$$\begin{split} A_{OL} &\approx 53, \quad BW_{OL} = 191 KHz, \quad GBW \approx 10.12 MHz \\ \beta &= \frac{Z_{in}}{Z_{in} + Z_f} = \frac{C_f}{C_f + C_{in}} = \frac{1}{2}, \ \frac{1}{4} \quad (For \ Both \ Values \ of \ C_{in}) \\ DC \ Gain &= A_{CL} = \frac{A_{OL}}{1 + \beta A_{OL}} = \textbf{1.927}, \ \textbf{3.72} \\ BW_{CL} &= (1 + \beta A_{OL}) BW_{OL} = \textbf{5.25} MHz, \ \textbf{2.721} MHz \\ GBW_{CL} &= \textbf{10.1167} MHz, \ \textbf{10.122} MHz \end{split}$$

	CIN = 4pF		CIN = 12pF	
	Simulation	Analytic	Simulation	Analytic
DC Gain (dB)	5.703	5.698	11.42	11.41
DC Gain	1.928	1.9272	3.722	3.72
BW	5.19E+06	5.25E+06	2.69E+06	2.72E+06
GBW	1.00E+07	1.01E+07	1.00E+07	1.01E+07

Analytic Results Agree with simulated ones in both cases of the input capacitor!

1.2 Loop Gain vs Frequency:

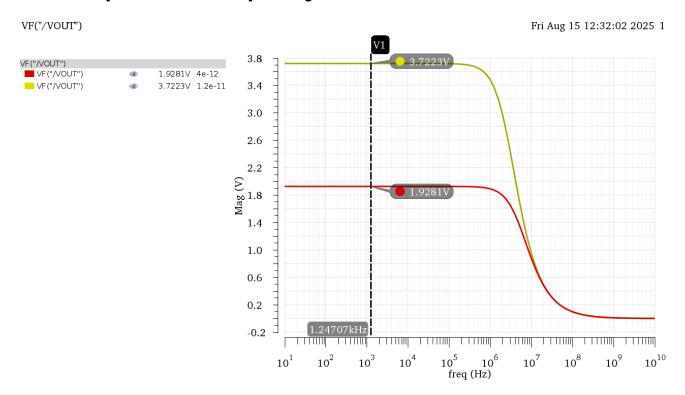


Figure 7 LG Overlaid in Mag

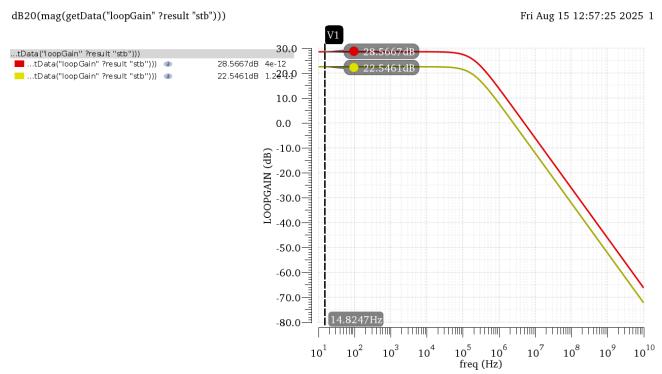


Figure 8 LG Overlaid in dB

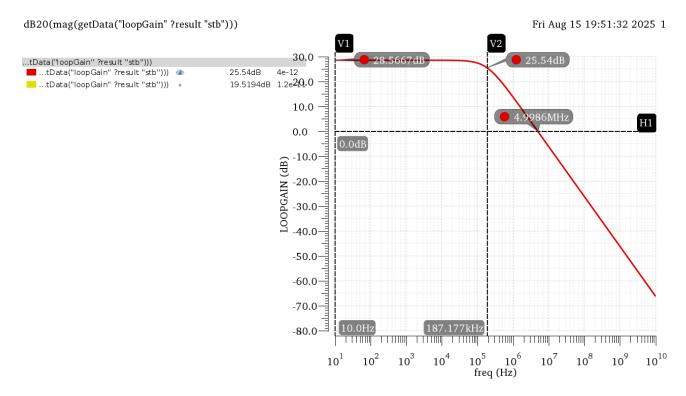


Figure 9 LG Bode Plot Annotated CIN = 4pF

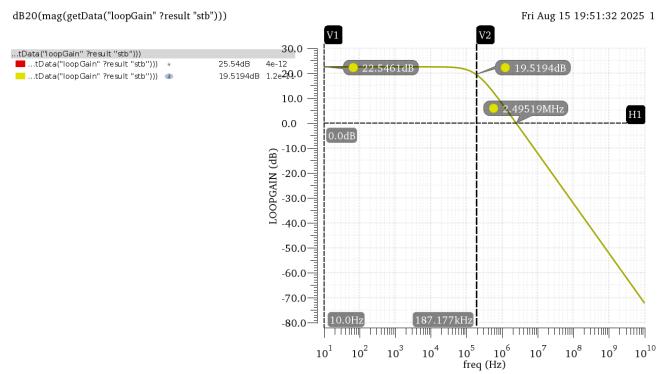


Figure 10 LG Bode Plot Annotated CIN = 12pF

	CIN = 4pF	CIN = 12pF
DC LG (dB)	28.57	22.55
DC LG	26.81	13.41
BW	187.17 KHz	187.17 KHz
UGF	5 MHz	2.5 MHz

Table 2 Results from Simulation

Hand Analysis:

Open Loop Parameters from Last Lab:

$$A_{OL} \approx 53$$
, $BW_{OL} = 191KHz$, $GBW \approx 10.12MHz$
 $\beta = \frac{Z_{in}}{Z_{in} + Z_f} = \frac{C_f}{C_f + C_{in}} = \frac{1}{2}$, $\frac{1}{4}$ (For Both Values of C_{in})
 $DC \ LG = LG = \beta A_{OL} = 26.5$, $13.25 \rightarrow 28.465dB$, $22.444dB$
 $BW_{LG} = BW_{OL} = 191KHz$
 $\omega_u = GBW_{LG} = 5.0615MHz$, $2.53MHz$

	CIN = 4pF		CIN = 12pF	
	Simulation	Analytic	Simulation	Analytic
DC LG (dB)	28.57	28.465	22.55	22.444
DC LG	26.81	26.5	13.41	13.25
BW	187.17 KHz	191 KHz	187.17 KHz	191 KHz
UGF	5 MHz	5.0615 MHz	2.5 MHz	2.53 MHz

Analytic Results Agree with simulated ones in both cases of the input capacitor!

1.3 Gain Desensitization:

To sweep the gain, I can either sweep GM or ROUT, I tried both and both resulted in similar results:

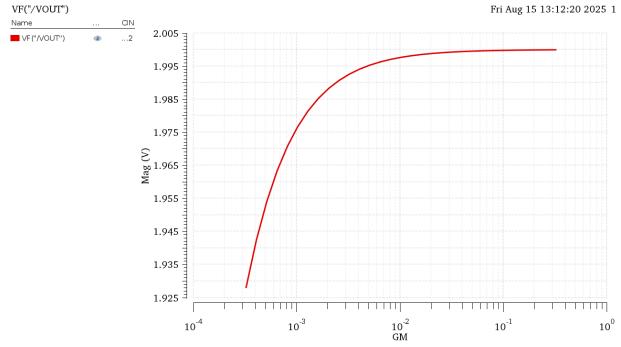
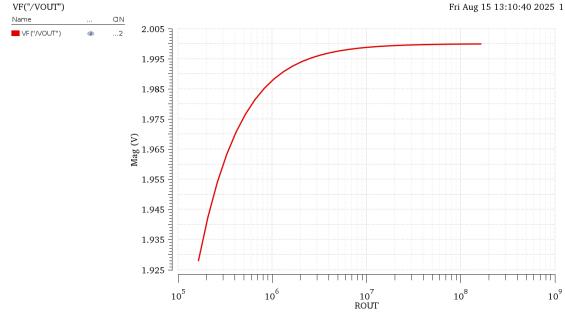


Figure 11 Gain Sweeping GM



$$A_{CL}\% = \frac{1.99982 - 1.928}{1.928} * 100 = 3.725\%$$

The Gain is much closer to its ideal value now (Ideal Value = 2) as we increase the Open Loop gain of the amplifier it easier to approximate closed loop gain as $\frac{1}{\beta}$. The percentage change would be even if we calculate for higher gains like the case of CIN = 4pF

Part 2: Feedback with Real 5T OTA

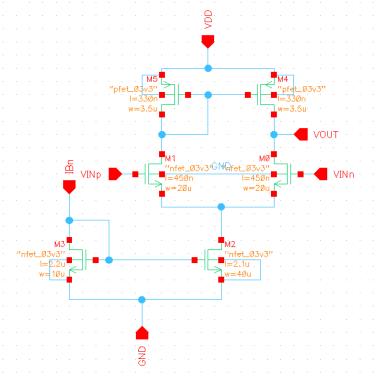


Figure 13 Real OTA Schematic

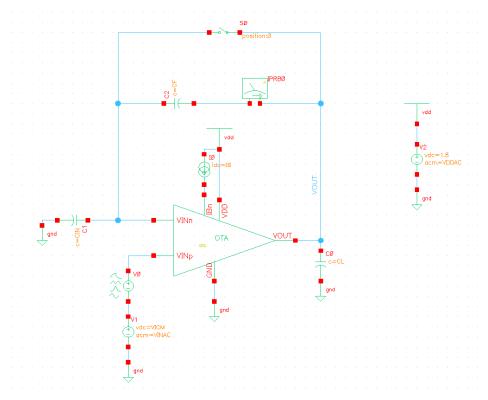


Figure 14 TB Schematic (Same as Part 1)

2.1 Closed Loop Gian vs Frequency:

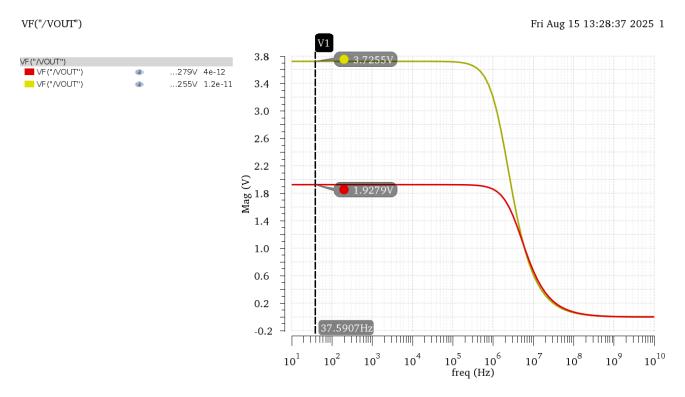


Figure 15 Gain in Mag

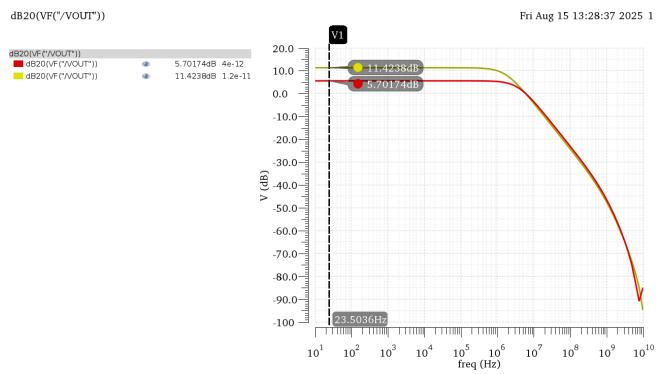


Figure 16 Gain in dB

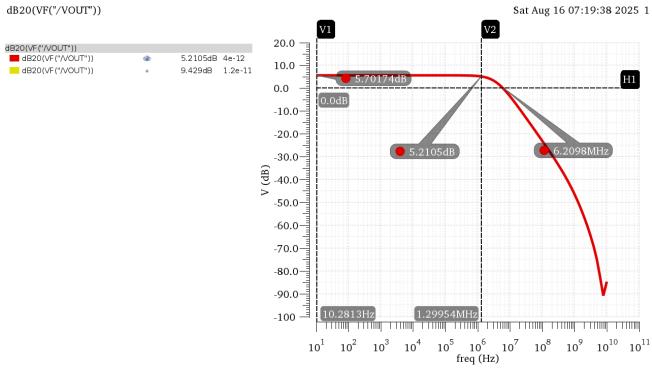


Figure 17 DC LG Bode Plot Annotated at CIN = 4pF

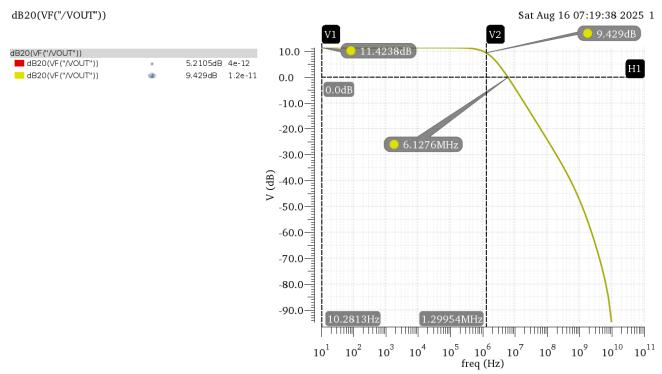


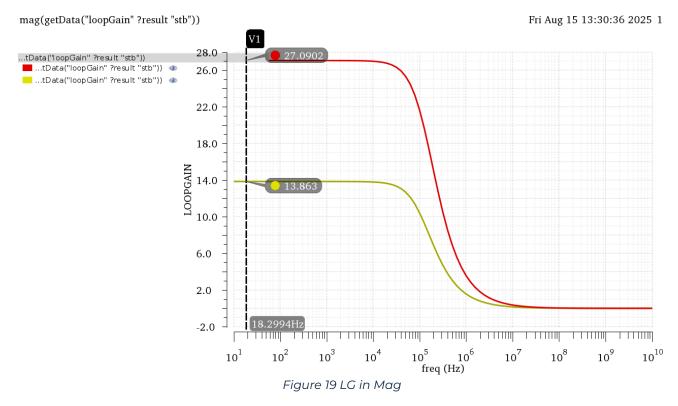
Figure 18 DC LG Bode Plot Annotated at CIN = 12pF

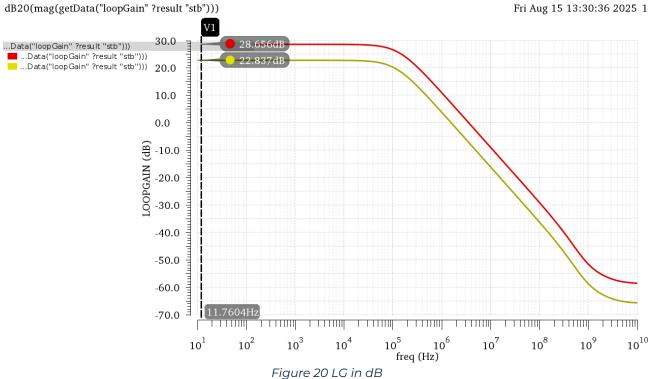
	CIN = 4pF		CIN = 12pF	
	Behavioral	5T OTA	Behavioral	5T OTA
DC Gain (dB)	5.703	5.702	11.42	11.42
DC Gain	1.928	1.928	3.722	3.726
BW	5.19E+06	3.76E+06	2.69E+06	1.70E+06
GBW	1.00E+07	7.27E+06	1.00E+07	6.37E+06

The Bandwidth and consequently the GBW are much smaller than Part 1:

The bandwidth in the OTA is much smaller because the Behavioral model took only CL in consideration when calculating the bandwidth due to the buffer in the behavioral model making ROUT = ∞ thus the effect of the loading effect is not seen. While in the real OTA , the ROUT seen in the actual ROUT of the amplifier thus contributing to the pole of the output node making it smaller.

2.2 Loop Gain vs Frequency:





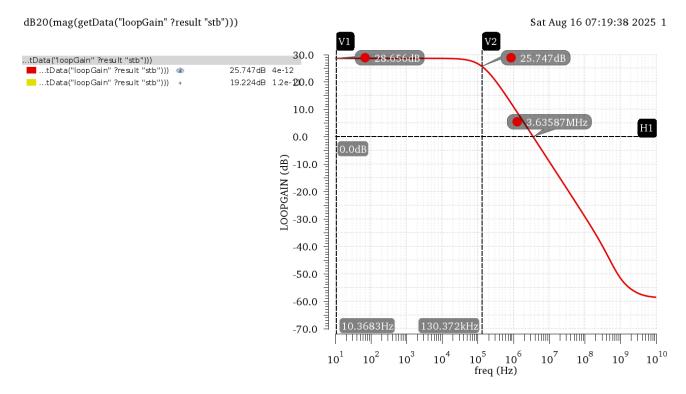


Figure 21 LG Bode Plot Annotated at CIN = 4pF

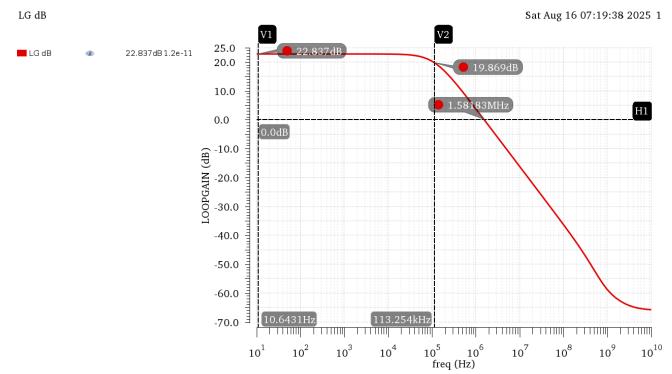


Figure 22 LG Bode Plot Annotated at CIN = 12pF

	CIN = 4pF		CIN = 12pF	
	Behavioral	5T OTA	Behavioral	5T OTA
DC LG (dB)	28.57	28.66	22.55	22.84
DC LG	26.81	27.09	13.41	13.86
BW	187.17 KHz	1.34E+05	187.17 KHz	1.15E+05
UGF	5 MHz	3.66E+06	2.5 MHz	1.58E+06

UGF is much smaller than in Part 1:

Due to the same reason stated previously, The buffer isolated Rout from seeing the loading effect thus only CL contributed to the Pole, but in the real OTA at the output node the loading effect of the added capacitors is seen such that the capacitance seen is $\mathcal{C}_L + \left(\mathcal{C}_{in}//\mathcal{C}_f\right)$ Contributing to a lower bandwidth thus a lower UGF.

2.3 Gain Desensitization:

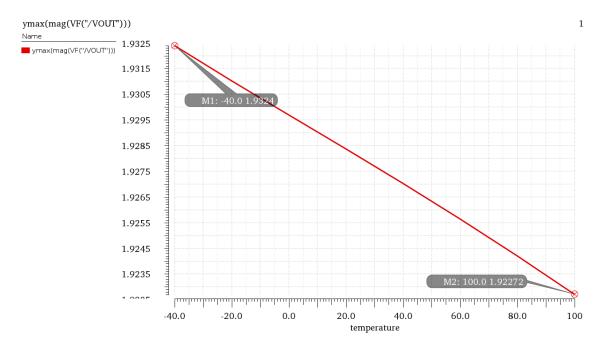


Figure 23 ACL in Mag vs Temp (Extreme Points Annotated)

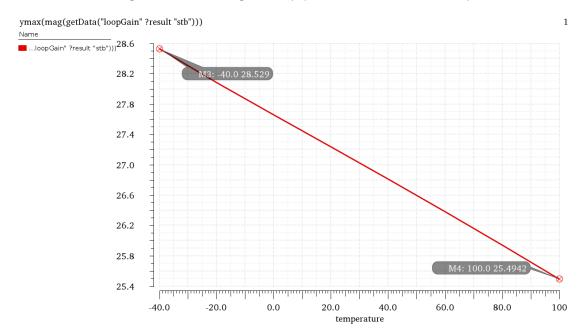


Figure 24 LG in Mag vs Temp (Extreme Points Annotated)

$$A_{CL}\%_{temp} = \frac{1.9324 - 1.92272}{1.928} * 100 = \textbf{0}.\textbf{5}\%, \ LG\%_{temp} = \frac{28.529 - 25.4942}{27.09} * 100 = \textbf{11}.\textbf{2}\%$$

The percentage change in LG is much more pronounced than the percentage change of ACL, as ACL depends on the ratio of capacitances (Which isn't affected by temperature much) much more heavily due to the big gain of AOL while LG depends on AOL which depends on the active components of the circuit whose parameters change heavily by temperature and process variations. This demonstrates the importance of feedback in desensitizing against PVT.

2.4 Transient Analysis:

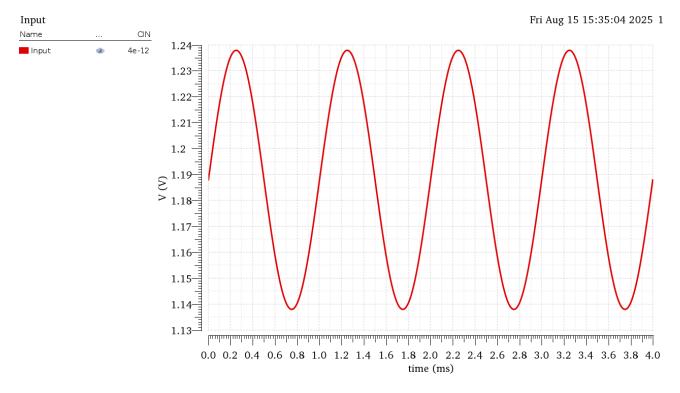


Figure 25 Input Signal

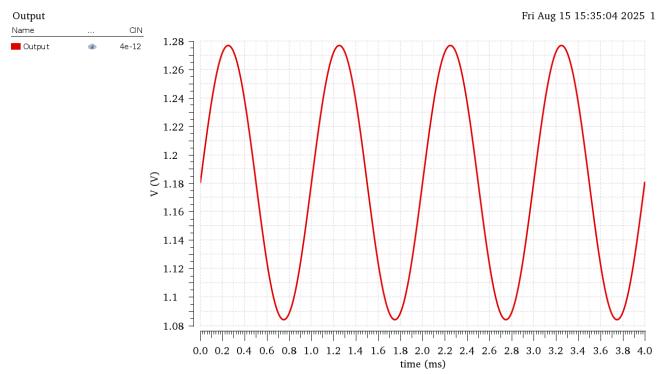


Figure 26 Output Signal

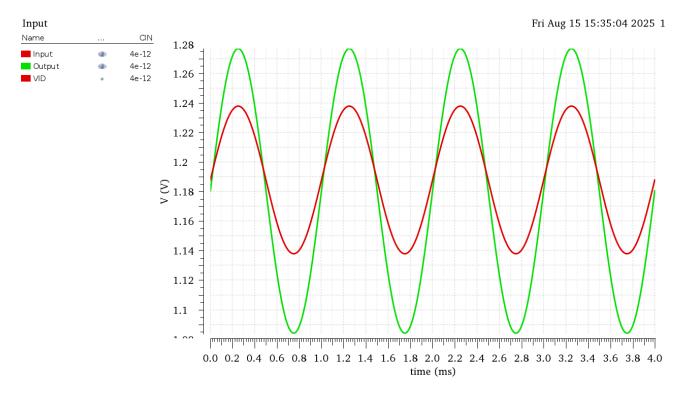
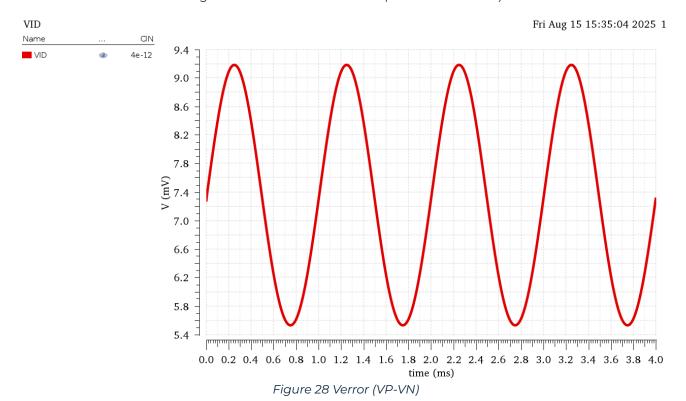


Figure 27 VIn and Vout Overlaid (To Showcase Gain)



	VIN	VOUT	VID
Peak to Peak (V)	1.00E-01	1.93E-01	3.66E-03

$$\frac{V_{OUT}}{V_{err}} = \frac{193m}{3.66m} = 52.732 = A_{OL}$$

 $\frac{V_{OUT}}{V_{err}}=\frac{193m}{3.66m}=52.732=A_{OL}$ The relationship between the Output Voltage and Error Voltage or the Differential Input voltage of the amplifier is the Open Loop Gain.

Using FIN=BW=134KHz

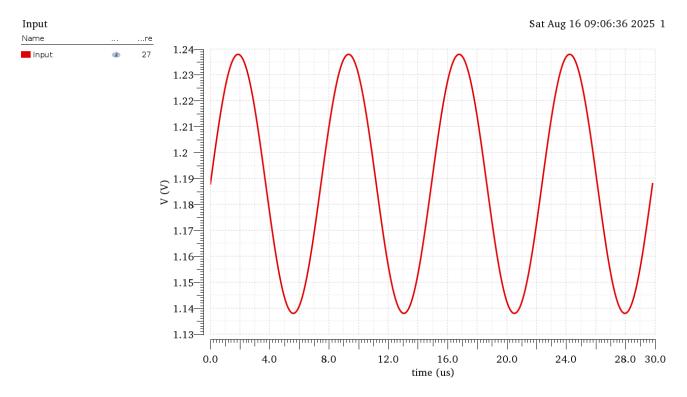


Figure 29 Input Signal at FIN=134KHz

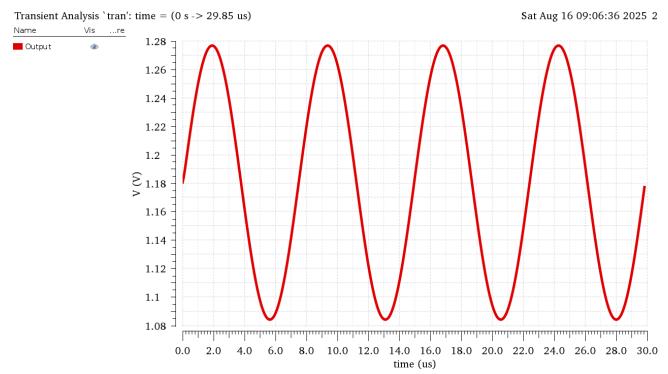


Figure 30 Output Signal at FIN=134KHz

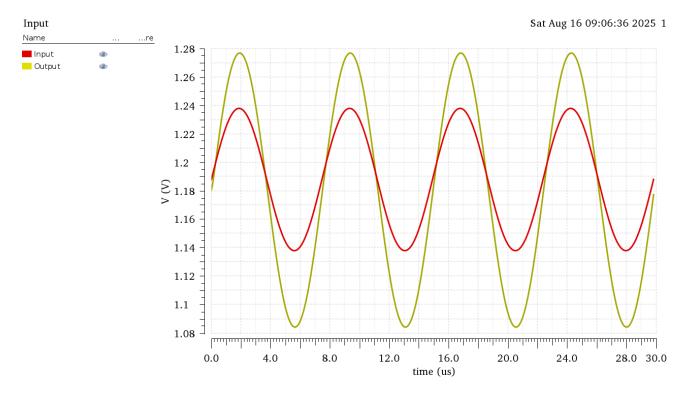


Figure 31 Vout and Vin Overlaid FIN=134KHz

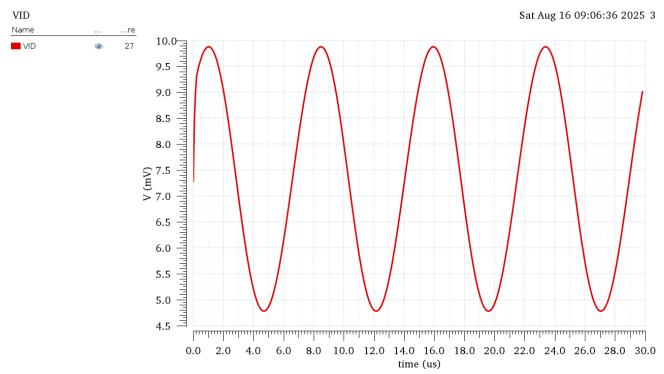


Figure 32 Verror at FIN=134KHz

	VIN	VOUT	VID
Peak to Peak (V)	1.00E-01	1.93E-01	5.10E-03

$$\frac{V_{OUT}}{V_{err}} = \frac{193m}{5.1m} = 37.671 = \frac{52.732}{\sqrt{2}} = \frac{A_{OL}}{\sqrt{2}}$$

The relationship between the Output Voltage and Error Voltage or the Differential Input voltage of the amplifier is the Open Loop Gain divided by root 2 as the Input signal is at the cutoff frequency.