

Analog IC Design

Lecture 13 gm/ID Design Methodology

Dr. Hesham A. Omran

Integrated Circuits Laboratory (ICL)
Electronics and Communications Eng. Dept.
Faculty of Engineering
Ain Shams University

Outline

- MOSFET figures-of-merit (FoM)
- ☐ SPICE vs square-law
- \square V^* and V_{Dsat}
- Subthreshold operation (weak inversion)
- ☐ Gm/ID design methodology

Outline

- MOSFET figures-of-merit (FoM)
- ☐ SPICE vs square-law
- \square V^* and V_{Dsat}
- Subthreshold operation (weak inversion)
- ☐ Gm/ID design methodology

MOSFET Figures-of-Merit (FoM)

☐ Intrinsic gain: gm*ro

☐ Intrinsic frequency (transit frequency): gm/Cgg

Current (transconductance) efficiency: gm/ID

Intrinsic Gain

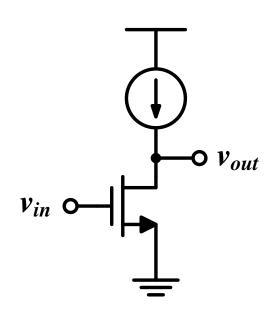
$$v_{out} = -(g_m v_{in}) r_o$$
$$|A_i| = \left| \frac{v_{out}}{v_{in}} \right| = g_m r_o$$

 \Box $g_m r_o$ is the max gain that can be obtained from a single transistor

$$g_m r_o = \frac{2I_D}{V_{ov}} \cdot \frac{1}{\lambda I_D} = \frac{2}{\lambda V_{ov}} = \frac{2V_A}{V_{ov}}$$



- Lower V_{ov} (or equivalently lower I_D): weak inversion and subthreshold operation
- Longer L (i.e., smaller λ)
- Both come at the expense of speed



Intrinsic Frequency

 \Box f_T is the frequency at which the MOSFET s.c. current gain drops to one (i.e., unity-gain frequency)

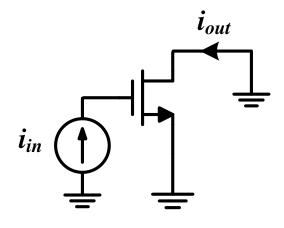
$$i_{out} = g_m v_{gs} = g_m \frac{\iota_{in}}{s C_{gg}}$$

$$@ i_{out} = i_{in}$$

$$f_T = \frac{g_m}{2\pi C_{gg}}$$

$$\approx \frac{1}{2\pi} \cdot \mu C_{ox} \frac{W}{L} V_{ov} \cdot \frac{1}{\frac{2}{3} W L C_{ox}}$$

$$\approx \frac{3\mu V_{ov}}{4\pi L^2}$$

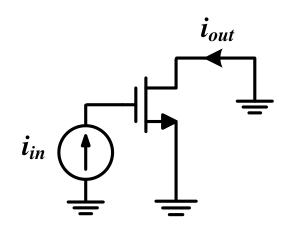


Intrinsic Frequency (Speed)

 \Box f_T is the frequency at which the MOSFET s.c. current gain drops to one (i.e., unity-gain frequency)

$$f_T \approx \frac{3\mu V_{ov}}{4\pi L^2}$$

- For higher speed
 - Higher V_{ov} (or equivalently higher I_D): strong inversion and higher power consumption
 - Shorter L (technology scaling helps!)
 - Just opposite to higher gain!
 - Analog design is all about trade-offs!
- lacktriangle After velocity sat, g_m and f_T saturate and become independent of V_{ov}



gm/ID

- ☐ gm/ID is the transconductance per unit current (a measure of energy efficiency)
 - How much transconductance (or GBW) can we get from each micro-amp of current

$$\frac{g_m}{I_D} = \frac{2}{V_{ov}}$$

- ☐ For higher efficiency
 - Lower V_{ov} (or equivalently lower I_D): weak inversion and subthreshold operation
 - Comes at the expense of speed

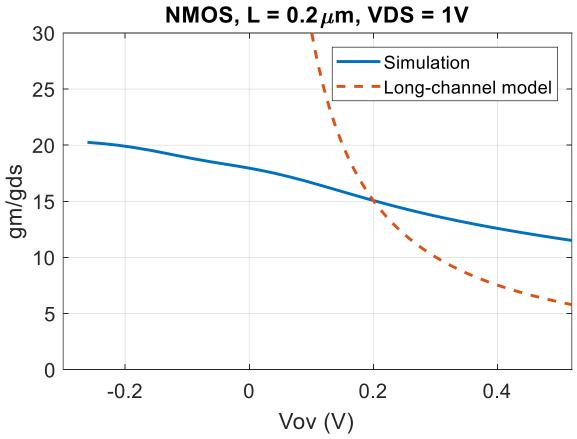
Outline

- MOSFET figures-of-merit (FoM)
- ☐ SPICE vs square-law
- \square V^* and V_{Dsat}
- Subthreshold operation (weak inversion)
- ☐ Gm/ID design methodology

SPICE vs Square-Law: $g_m r_o$

 \square Square-law expects infinite $g_m r_o$ at $V_{ov} = 0$

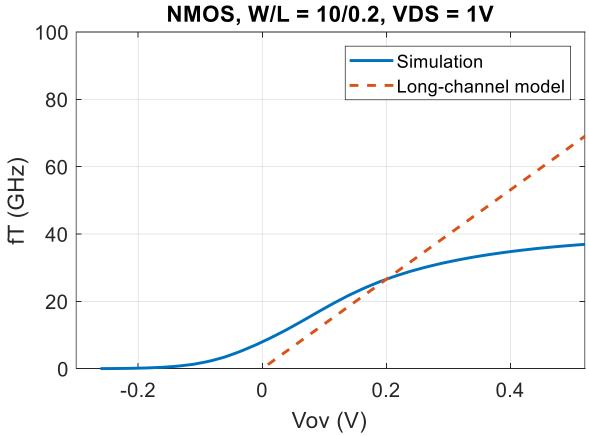
$$g_m r_o = \frac{2}{\lambda V_{ov}} = \frac{2V_A}{V_{ov}}$$



SPICE vs Square-Law: f_T

 \Box Square-law expects f_T increases linearly with V_{ov}

$$f_T = \frac{g_m}{2\pi C_{g,g}} \approx \frac{3\mu V_{ov}}{4\pi L^2}$$

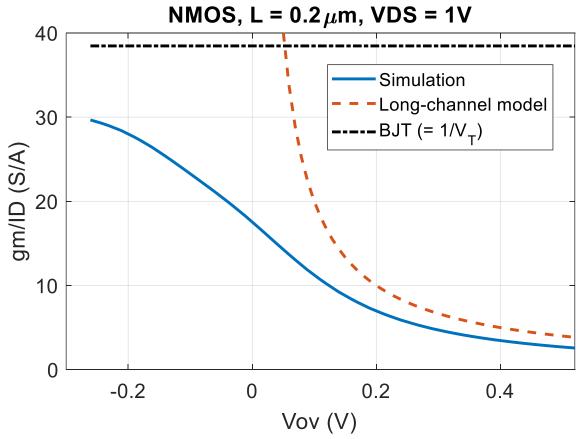


13: gm/ID Design

11

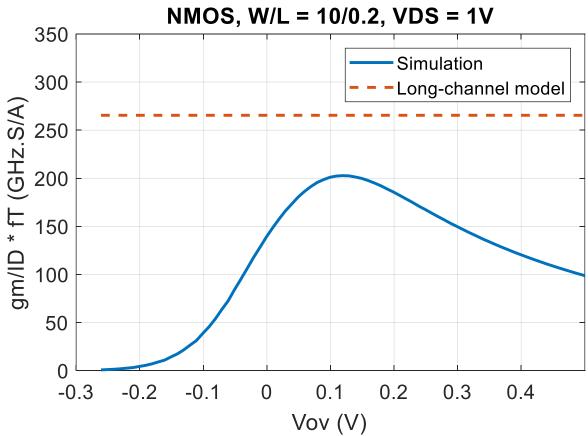
SPICE vs Square-Law: g_m/I_D

 \Box Square-law expects infinite g_m/I_D at $V_{ov}=0$ $\frac{g_m}{I_D}=\frac{2}{V_{ov}}$



SPICE vs Square-Law: The Sweet-Spot

- ☐ Global maximum in MI: Sweet-spot
 - Best compromise between efficiency and speed



SPICE vs Square-Law: Conclusions

- Square-law fails to describe SI <u>accurately</u>
 - Short channel effects (e.g., velocity sat.) are not considered
- Square-law fails to describe MI and WI completely
 - A completely different approach is required

Outline

- MOSFET figures-of-merit (FoM)
- ☐ SPICE vs square-law
- \square V^* and V_{Dsat}
- Subthreshold operation (weak inversion)
- ☐ Gm/ID design methodology

V-star (V^*)

- \square We used $g_m = \frac{2I_D}{V_{OV}}$ which is based on the square-law
- \Box For a real MOSFET $V_{ov} \neq \frac{2I_D}{g_m}$
- lacktriangle Let's define a new parameter called V-star (V^*) which is calculated from actual simulation data using the formula

$$V^* = \frac{2I_D}{g_m} \leftrightarrow g_m = \frac{2I_D}{V^*}$$

 \Box For a square-law device, $V^* = V_{ov}$, however, for a real MOSFET they are not equal.

Figures-of-Merit Revisited

lacktriangle Redefine the figures-of-merit in terms of V^*

$$g_m r_o = \frac{2I_D}{V^*} \cdot \frac{1}{\lambda I_D} = \frac{2}{\lambda V^*} = \frac{2V_A}{V^*}$$

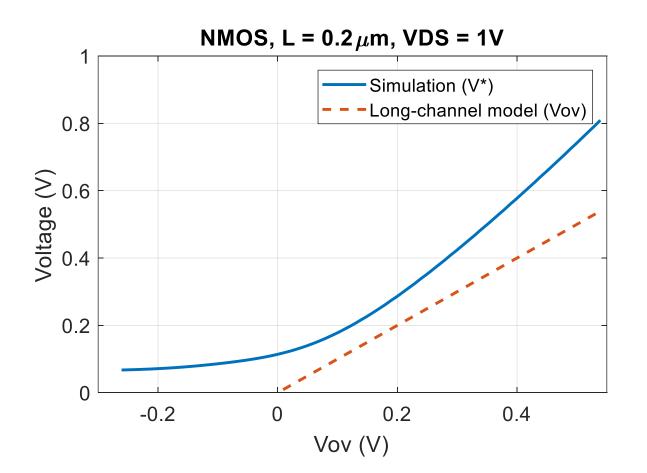
$$f_T = \frac{g_m}{2\pi C_{gg}} = \frac{1}{2\pi} \cdot \frac{2I_D}{V^*} \cdot \frac{1}{C_{gg}}$$

$$\frac{g_m}{I_D} = \frac{2}{V^*}$$

lacktriangle Does V^* continue to decrease as V_{ov} goes towards weak inversion?

$oldsymbol{V}^*$ vs $oldsymbol{V_{ov}}$

- \square SI: $V^* > V_{ov} \rightarrow g_m = \frac{2I_D}{V^*}$ is less than square-law expectations
- □ WI: $V^* \approx constant \rightarrow$ Why?

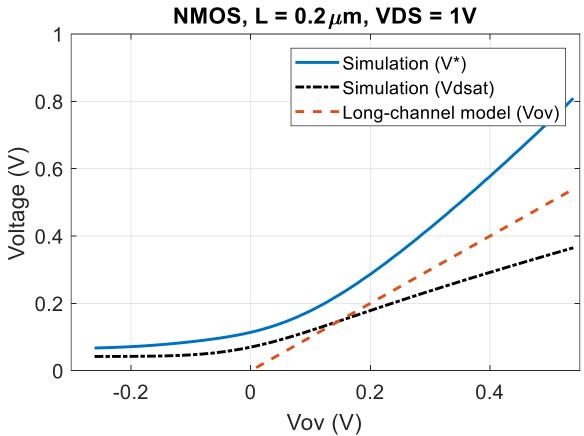


Drain Saturation Voltage (V_{Dsat})

- \Box In general MOSFET is in saturation if $V_{DS} > V_{Dsat}$
- \Box The definition of V_{Dsat} is a bit **vague**
 - I_D keeps increasing if $V_{DS} > V_{Dsat}$ due to CLM/DIBL
 - r_o is quite low at edge of saturation $(V_{DS} = V_{Dsat})$
 - r_o increases by multiple folds by biasing the MOSFET deeper into saturation
 - For a square-law device: $V_{Dsat} = V_{ov}$
 - In actual model V_{Dsat} is a bit complex parameter
 - V^* is usually larger than V_{Dsat}
 - ullet As an approximation we can use $V_{DS}>V^*$ as sat. condition
 - Guarantees biasing the MOSFET a bit deeper into saturation

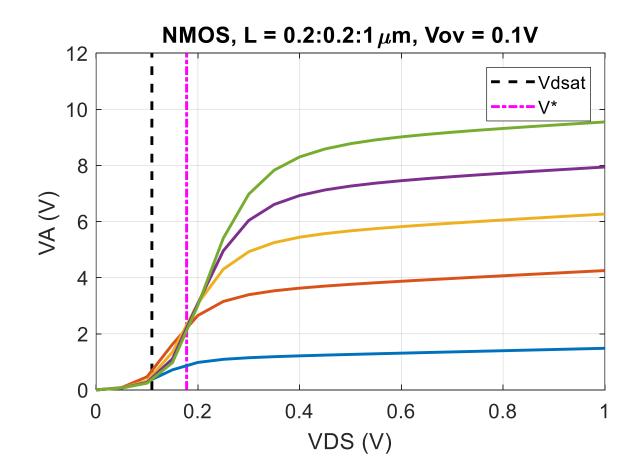
V^* vs V_{Dsat} vs V_{ov}

- $\Box V_{Dsat} < V_{ov}$ in SI but $V_{Dsat} > V_{ov}$ in WI
- \square V^* always $> V_{Dsat}$



Is V_{Dsat} really meaningful?

- \Box $r_o = \frac{V_A}{I_D}$ is quite low at $V_{DS} = V_{Dsat} \rightarrow$ Longer L doesn't help!
- \square r_o increases order of magnitude by going deeper into saturation
 - Longer L helps only when V_{DS} is large



Outline

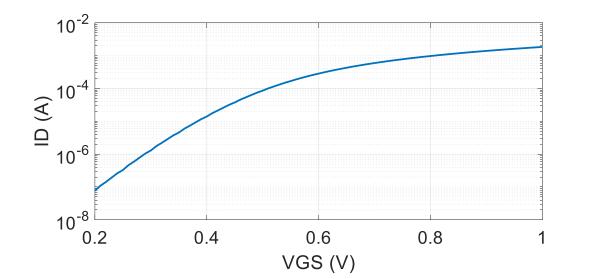
- MOSFET figures-of-merit (FoM)
- ☐ SPICE vs square-law
- \square V^* and V_{Dsat}
- Subthreshold operation (weak inversion)
- ☐ Gm/ID design methodology

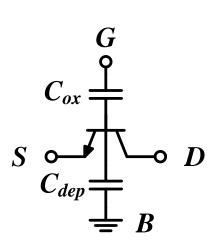
Subthreshold Operation (Weak Inversion)

- ☐ MOSFET behaves as a BJT (npn for an NMOS) with its base coupled to the gate through capacitive divider
 - Subthreshold current depends exponentially on V_{GS}
 - For $V_{DS} > V_{DSat}$ (saturation):

$$I_D \approx I_0 \frac{W}{L} e^{\frac{V_{GS} - V_{TH}}{nV_T}}$$

$$n = \frac{C_{ox} + C_{dep}}{C_{ox}} \approx 1.2 \rightarrow 1.5$$





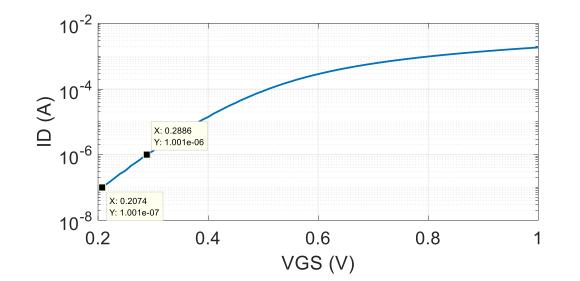
Subthreshold Slope (S)

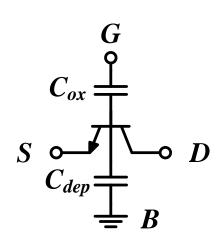
$$I_D = I_0 \frac{W}{L} e^{\frac{V_{GS} - V_{TH}}{nV_T}}$$

$$\log I_D = \log I_0 \frac{W}{L} e^{\frac{-V_{TH}}{nV_T}} + \frac{V_{GS}}{nV_T} \log e$$

$$S = \left(\frac{\partial \log I_D}{\partial V_{GS}}\right)^{-1} = \frac{nV_T}{\log e} = nV_T \ln 10 = n \times 60 \text{ mV/decade}$$

 \square Example: $S = 0.2886 - 02074 \approx 81 mV/decade <math>\rightarrow n \approx 1.35$





V* in Weak Inversion

$$I_{D} = I_{Do} \frac{W}{L} e^{\frac{V_{GS}}{nV_{T}}}$$

$$g_{m} = \frac{\partial I_{D}}{\partial V_{GS}} = \frac{I_{D}}{nV_{T}} = \frac{2I_{D}}{V^{*}}$$

$$V^{*} = 2nV_{T}$$

At the boundary between exponential weak inversion (WI) and quadratic strong inversion (SI): a.k.a. the onset of strong inversion

$$V^* = V_{ov}$$
$$V_{ov} = 2nV_T \approx (1.2 \rightarrow 1.5) \times 52mV \approx 60 \rightarrow 80 \ mV$$

- ☐ The region between WI (exponential behavior) and SI (square-law behavior) is referred to as moderate inversion (MI)
 - No simple models for this region (a.k.a. near-threshold operation)

Subthreshold Intrinsic Gain

$$g_m r_o = \frac{2I_D}{V^*} \cdot \frac{1}{\lambda I_D} = \frac{2}{\lambda V^*} = \frac{1}{\lambda n V_T} = \frac{V_A}{n V_T}$$

- \square Independent of V_{ov}
- ☐ Gain does not improve as we go deeper in subthreshold

Subthreshold Current Efficiency

$$\frac{g_m}{I_D} = \frac{2}{V^*} = \frac{1}{nV_T}$$

- lacksquare Independent of V_{ov}
- Efficiency does not improve as we go deeper in subthreshold

Subthreshold Intrinsic Speed

$$f_T = \frac{g_m}{2\pi C_{gg}}$$

$$\approx \frac{1}{2\pi} \cdot \frac{2I_D}{V^*} \cdot \frac{1}{C_{gg}}$$

$$\approx \frac{I_D}{2\pi n V_T C_{gg}}$$

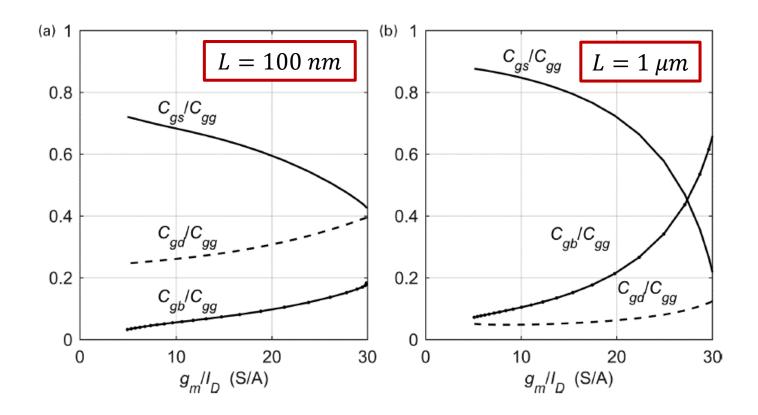
- \square Speed (f_T) continues to degrade as we go deeper in subthreshold
 - I_D decreases exponentially

Near-Threshold (MI) Biasing

- Operating the MOSFET in the near-threshold (moderate inversion) region is becoming increasingly popular.
 - We already reap most of WI benefits
 - Higher gain
 - Higher efficiency
 - Some degradation in speed (f_T is already very high for short L)
- Going deeper into WI is seldom useful
 - Minor/no benefit in gain
 - Minor/no benefit in efficiency
 - Exponential degradation in speed
 - Exponential increase in area and parasitics
 - But may be useful if we intentionally need very low I_D (ultra low power applications)

MOSFET Capacitance in WI vs SI

- \Box For SI: $C_{gb} \approx 0$, $C_{gs} \gg C_{gd}$
- □ For WI: C_{gb} ↑, $C_{gs} \approx C_{gd}$
 - For long channel C_{gb} in WI is more significant
 - For short channel, source and drain still hide the bulk even in WI



Outline

- MOSFET figures-of-merit (FoM)
- ☐ SPICE vs square-law
- \square V^* and V_{Dsat}
- Subthreshold operation (weak inversion)
- ☐ Gm/ID design methodology

Don't be a SPICE Monkey!

- In absence of a clear methodology for hand analysis, many designers tend to converge toward a "SPICE monkey" design methodology.
 - No hand calculations, iterate in SPICE until the circuit "somehow" meets the specifications
 - Typically results in sub-optimal designs, uninformed design decisions, etc.
- → A SPICE monkey is someone who does not use hand analysis to figure out how to design a circuit, but rather plugs stuff into SPICE and uses whatever value works.

13: gm/ID Design [Murmann, EE214B, Stanford]

gm/ID Design Methodology

- ☐ Traditionally, square-law was used in hand analysis to obtain initial design point
 - But short channel and moderate/weak inversion devices do not obey the square law
 - Square law is seldom used in nowadays designs
- \Box The popular approach nowadays is using gm/ID (or equivalently V*) design methodology
- Perform DC sweeps for both PMOS and NMOS to generate design charts vs gm/ID
 - Or use look-up tables (LUTs) and access them using any programming language (MATLAB, Python, etc.)
- Use these charts (LUTs) to design your circuit to meet required specs

The Design Problem

- MOSFET is a function of five variables
 - 3 (voltages) + 2 (sizing)
- Strictly: the designer needs to specify 5 DOF for every device in the circuit
 - (VGS, VDS, VSB, W, L)
- For analog IC design, MOS is usually biased in saturation (essentially a VCCS)
 - VGS is the primary voltage controlling the device behavior
 - VDS is of secondary importance: set to VDSAT + margin
 - VSB is of tertiary importance: usually imposed by circuit topology
- Practically: the designer worries about 3 DOF
 - (VGS, W, L)
- We usually set the device current (using current mirrors) rather than the device voltage
 - (ID, W, L)

DOFs in Conventional Design Flow

- ☐ While tweaking a circuit in the simulator, the designer plays with 3 DOFs
 - (ID, W, L)
 - Sweeping any DOF (ID, W, L) changes the bias point (inversion level) of the device
 - The "search-range" of W can be quite large (depends on both ID and L)
- \Box The old fix:
 - Switch to (ID, Vov, L) instead of (ID, W, L)
 - But short channel and moderate/weak inversion devices do not obey the square law
- \Box The new fix:
 - Switch to (ID, V*, L)

DOFs in gm/ID Design Methodology

- ☐ V* or gm/ID design methodology enables "orthogonal" DOFs
 - (ID, V*, L) or (ID, gm/ID, L)
 - gm/ID sets the inversion level independent of ID and L
 - When ID and/or L changes: Look up the new W in the LUTs (gm/ID kept unchanged)
 - Search-range of gm/ID is limited (typically 3 to 30)
 - gm/ID can be replaced by JD = ID/W for deep subthreshold design

gm/ID Design Methodology

- \square V_{ov} has a vague physical meaning and does not help the designer's intuition any more
- On the contrary
 - gm/ID is a key MOSFET FoM
 - gm/ID captures the relation between the basic function of the transistor (the transconductance) and the most valuable resource (the power consumption)
 - The range of gm/ID values doesn't differ much from one device to another and from one technology to another
 - gm/ID can be a thought as a normalized measure for the device inversion level
- Conclusion: use gm/ID as your primary design variable
 - Plot everything vs gm/ID

Quiz

- \square Assume n = 1.5 and $V_{ov} < 0.5V$.
- Assume square-law is valid in strong inversion.
- ☐ Calculate gm/ID range.
- \square Calculate the gm/ID at the sweet spot ($V^* = 200mV$).

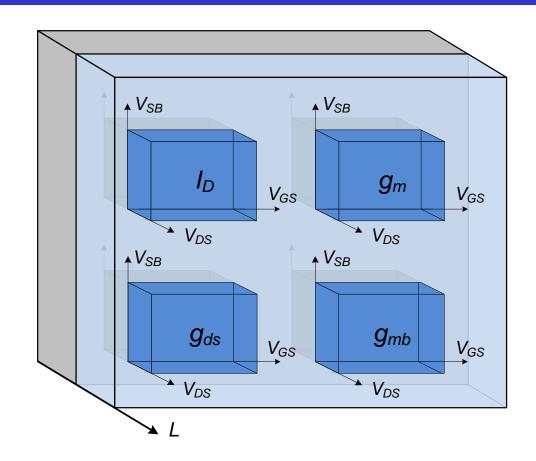
Quiz

- \square Assume n = 1.5 and $V_{ov} < 0.5V$.
- ☐ Assume square-law is valid in strong inversion.
- Calculate gm/ID range.
- \square Calculate the gm/ID at the sweet spot ($V^* = 200mV$).

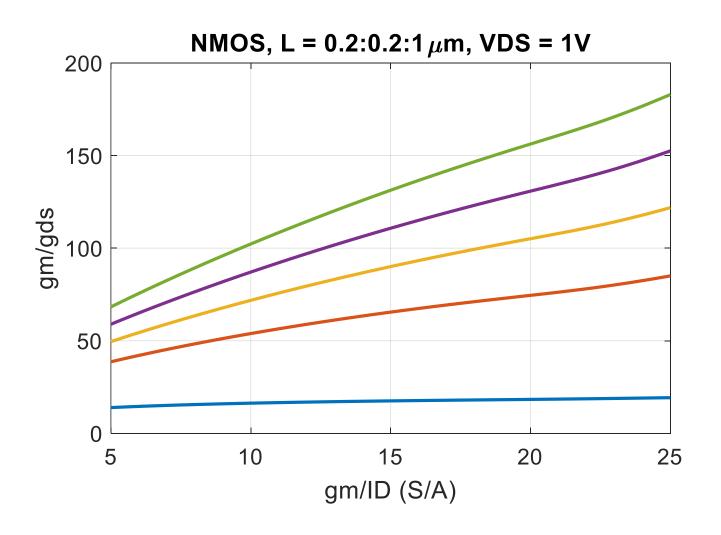
- $\square \frac{gm}{ID} = \frac{2}{V^*} = 4 \rightarrow 25$

The Lookup Table (LUT)

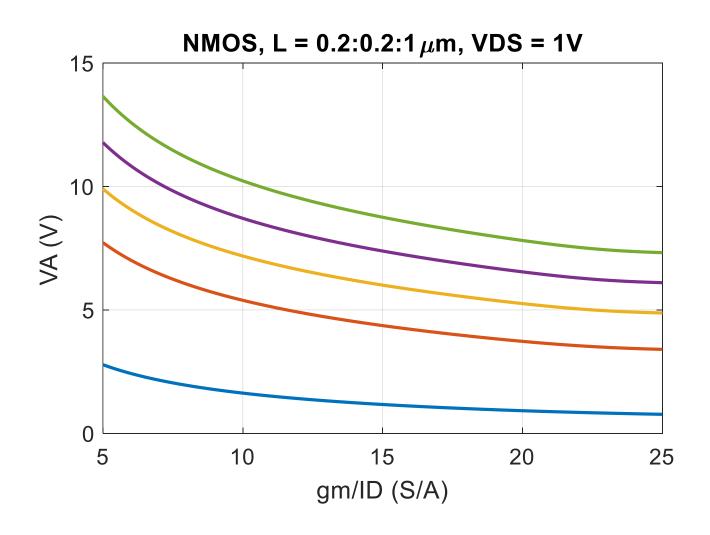
- MOSFET is a function of five variables
 - 3 (voltages) + 2 (sizing)
- All MOSFET parameters are proportional to width
 - Narrow-width effects ignored (not common in analog IC design)
 - Use normalized quantities (cross multiplication)
- ☐ Degrees of freedom (DOFs) reduced to 4
 - VGS, VDS, VSB, and L
- ☐ Simulate a reference device
 - Sweep the 4 DOFs
 - Construct a 4D LUT for every parameter
- May ignore VDS and VSB dependence to plot 2D parametric charts



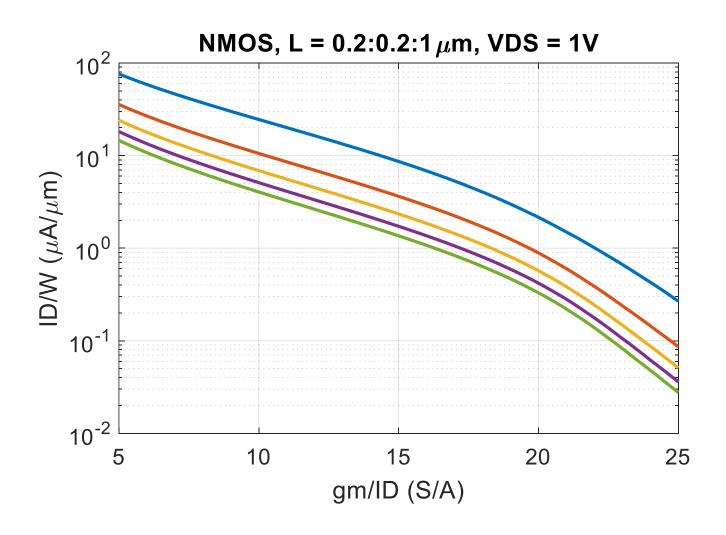
gm/ID Charts: $g_m r_o$



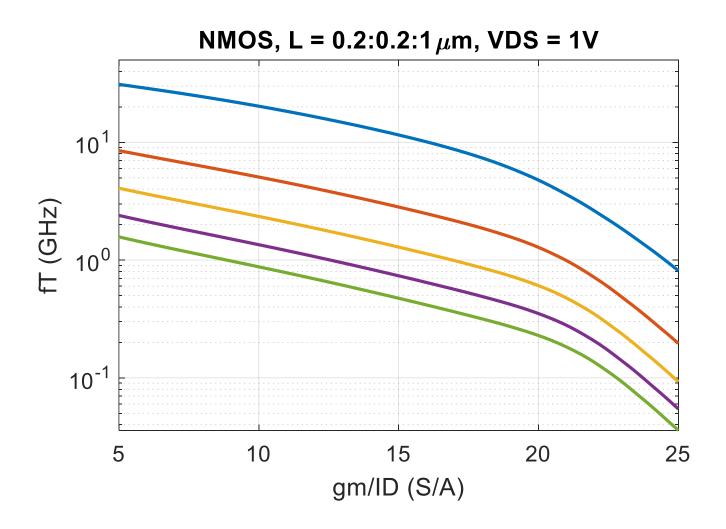
gm/ID Charts: V_A



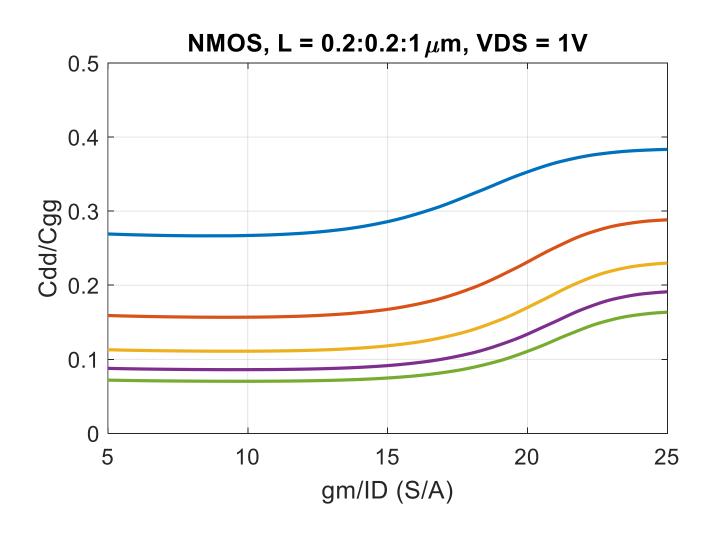
gm/ID Charts: I_D/W



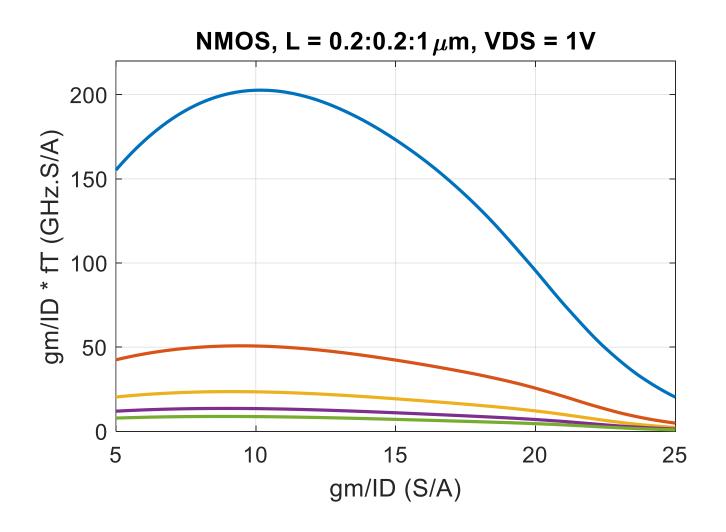
gm/ID Charts: f_T



gm/ID Charts: C_{dd}/C_{gg}



gm/ID Charts: $g_m/I_D \cdot f_T$



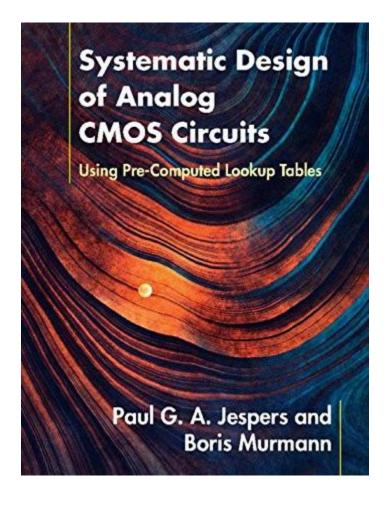
Analog Design Trade-offs

- ☐ There are always tradeoffs between gain, speed, and energy efficiency.
- The design knobs to control the tradeoffs: gm/ID and L.
- Choice of gm/ID
 - Large gm/ID: high efficiency (low power), large swing (low V*), high gain (low V*)
 - Small gm/ID: high speed, small area
- lacksquare Choice of L
 - Long L: high r_o , good matching, low flicker noise (more later)
 - Short L: high speed, small area
- Finding the best compromise for design tradeoffs given required specs is your job as a designer.

Thank you!

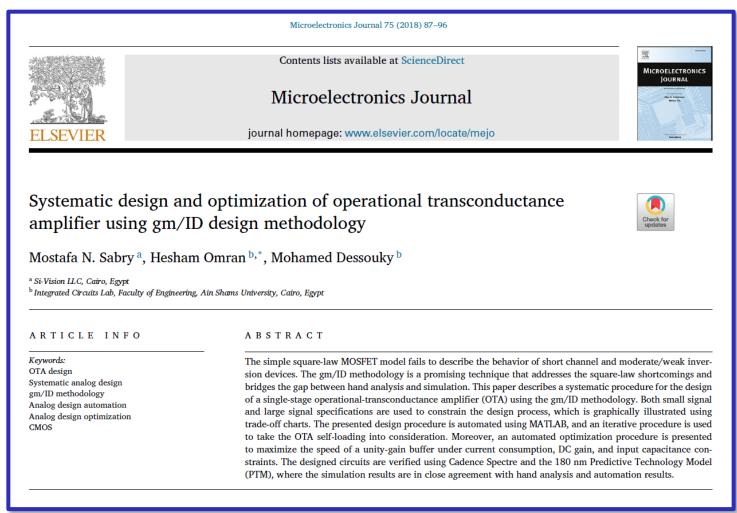
References (1/3)

P. Jespers and B. Murmann, Systematic Design of Analog CMOS Circuits Using Pre-Computed Lookup Tables, Cambridge University Press, 2017.



References (2/3)

M. N. Sabry, H. Omran and M. Dessouky, "Systematic design and optimization of operational transconductance amplifier using gm/ID design methodology," *Microelectronics Journal*, vol. 75, pp. 87-96, May 2018.



References (3/3)

- B. Murmann, Gm/ID Starter Kit. [Online]. Available: https://web.stanford.edu/~murmann/gmid
- ☐ B. Murmann, EE214 Course Reader, Stanford University.
- ☐ B. Razavi, "Design of Analog CMOS Integrated Circuits," McGraw-Hill, 2nd ed., 2017.
- ☐ T. C. Carusone, D. Johns, and K. W. Martin, "Analog Integrated Circuit Design," 2nd ed., Wiley, 2012.