

# **Ch3: Rigid-Body Motions – Part 2**

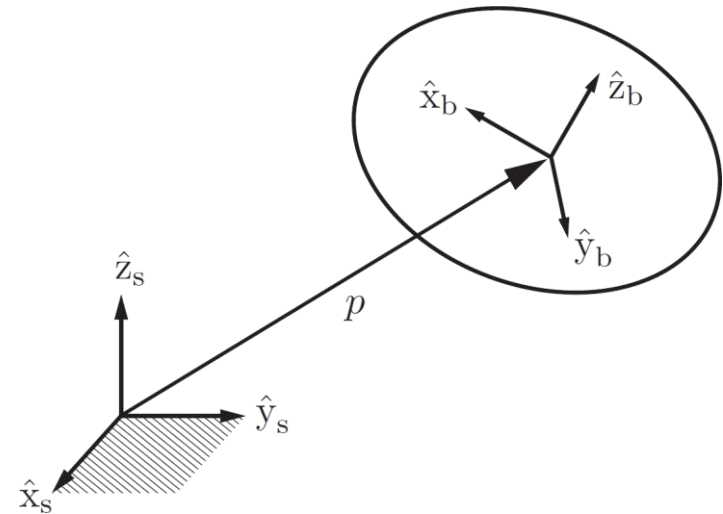
# Rigid-Body Motions

# Homogeneous Transformation Matrices

Rigid-body configuration can be represented by the pair  $(\mathbf{R}, \mathbf{p})$  ( $\mathbf{R} \in SO(3)$ ,  $\mathbf{p} \in \mathbb{R}^3$ ). We can package  $(\mathbf{R}, \mathbf{p})$  into a single  $4 \times 4$  matrix as

$$\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$

(an implicit representation of the C-space)



# Special Euclidean Group $SE(n)$

The **Special Euclidean Group**  $SE(3)$ , also known as the **group of rigid-body motions** or **homogeneous transformation matrices** in  $\mathbb{R}^3$ , is the set of all  $4 \times 4$  real matrices  $\mathbf{T}$  of the form

$$\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_1 \\ r_{21} & r_{22} & r_{23} & p_2 \\ r_{31} & r_{32} & r_{33} & p_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \begin{array}{l} \mathbf{T} \in SE(3) \\ \mathbf{R} \in SO(3) \\ \mathbf{p} \in \mathbb{R}^3 \end{array}$$

The **special Euclidean group**  $SE(2)$  is the set of all  $3 \times 3$  real matrices  $\mathbf{T}$  of the form

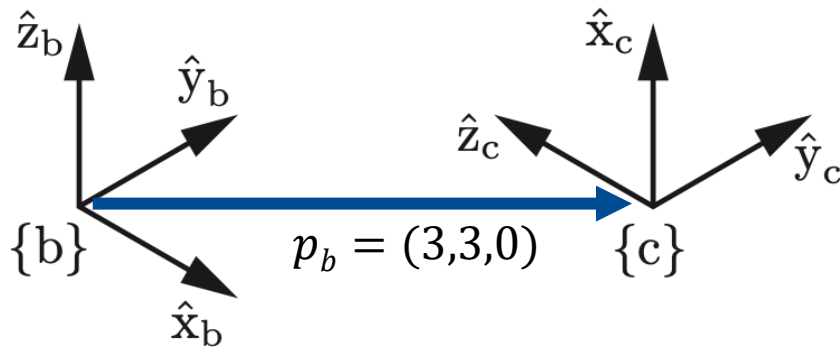
$$\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & p_1 \\ r_{21} & r_{22} & p_2 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta & p_1 \\ \sin \theta & \cos \theta & p_2 \\ 0 & 0 & 1 \end{bmatrix} \quad \begin{array}{l} \mathbf{T} \in SE(2) \\ \mathbf{R} \in SO(2) \\ \mathbf{p} \in \mathbb{R}^2 \\ \theta \in [0, 2\pi) \end{array}$$

$SE(2)$  is a subgroup of  $SE(3)$ :  $SE(2) \subset SE(3)$

$$\mathbf{T} = (\mathbf{R}, \mathbf{p}) \in SE(3)$$

$$SE(3) = \{(\mathbf{R}, \mathbf{p}) \mid \mathbf{R} \in SO(3), \mathbf{p} \in \mathbb{R}^3\}$$

# Example

 $T_{bc}?$

# Properties of Transformation Matrices

$SE(3)$  (or  $SE(2)$ ) is a **matrix (Lie) group** (and the group operation  $\bullet$  is matrix multiplication).

**Closure:**  $T_1 T_2 \in SE(3)$

**Associative:**  $(T_1 T_2) T_3 = T_1 (T_2 T_3)$  (but generally not commutative,  $T_1 T_2 \neq T_2 T_1$ )

**Identity:**  $\exists I \in SE(3)$  such that  $TI = IT = T$

**Inverse:**  $\exists T^{-1} \in SE(3)$  such that  $TT^{-1} = T^{-1}T = I$

$$T^{-1} = \begin{bmatrix} R & p \\ 0 & 1 \end{bmatrix}^{-1} = \begin{bmatrix} R^T & -R^T p \\ 0 & 1 \end{bmatrix}$$

**Note:**  $T$  preserves both distances and angles.

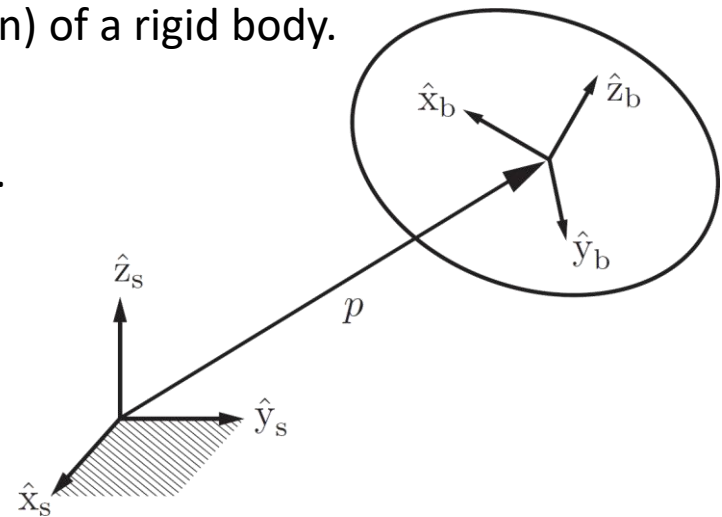
# Uses of Transformation Matrices (1)

(1) Representing configuration (position and orientation) of a rigid body.

Notation:  $T_{sb}$  is the configuration of  $\{b\}$  relative to  $\{s\}$ .

$$T_{sb} = \begin{bmatrix} R_{sb} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$

$$T_{sb}T_{bs} = I \quad \text{or} \quad T_{bs} = T_{sb}^{-1} = \begin{bmatrix} R_{sb}^T & -R_{sb}^T \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$



# Uses of Transformation Matrices (2)

(2) Changing the reference frame of a vector or frame.

Subscript Cancellation Rule:

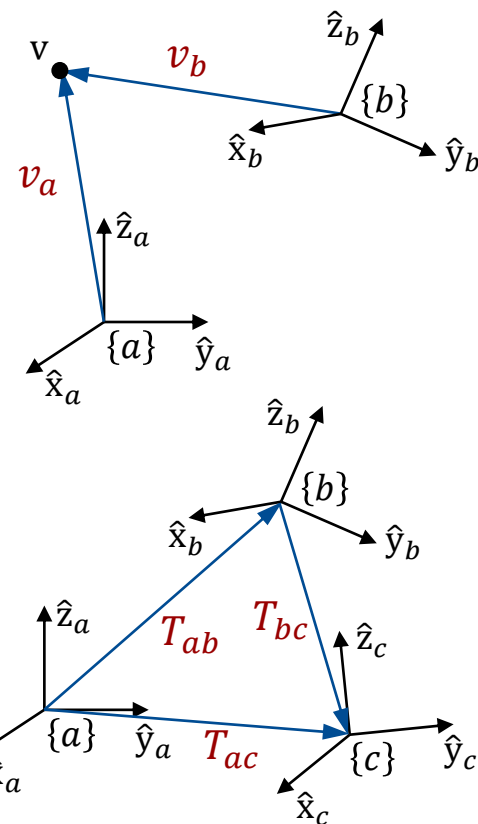
$$\mathbf{T}_{ab} \mathbf{v}_b = \mathbf{T}_{a\cancel{b}} \mathbf{v}_{\cancel{b}} = \mathbf{v}_a$$

$$\mathbf{T}_{ab} \mathbf{T}_{bc} = \mathbf{T}_{a\cancel{b}} \mathbf{T}_{\cancel{b}c} = \mathbf{T}_{ac}$$

$\mathbf{T}_{ab}$  can be viewed as a mathematical operator that changes the reference frame from  $\{b\}$  to  $\{a\}$ .

**Note:** To calculate  $\mathbf{T}\mathbf{v}$ , we append a “1” to  $\mathbf{v}$  and it is called **homogeneous coordinates** representation of  $\mathbf{v}$ .

$$\mathbf{v} = [v_1 \ v_2 \ v_3 \ 1]^T$$





# Uses of Transformation Matrices (3)

(3) Displacing (rotating and translating) a vector or frame.

$$\mathbf{T} = (\mathbf{R}, \mathbf{p}) = (\text{Rot}(\hat{\boldsymbol{\omega}}, \theta), \mathbf{p}) = \text{Trans}(\mathbf{p})\text{Rot}(\hat{\boldsymbol{\omega}}, \theta)$$

$$\text{Trans}(\mathbf{p}) = \begin{bmatrix} \mathbf{I} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$

$$\text{Rot}(\hat{\boldsymbol{\omega}}, \theta) = \begin{bmatrix} \mathbf{R} & \mathbf{0} \\ \mathbf{0} & 1 \end{bmatrix}$$

$\mathbf{T}$  can be viewed as a **mathematical operator** that rotates a frame or vector about a unit axis  $\hat{\boldsymbol{\omega}} = (\hat{\omega}_1, \hat{\omega}_2, \hat{\omega}_3)$  by an amount  $\theta$  + translating it by  $\mathbf{p}$ .

# Uses of Transformation Matrices (3) (cont.)

- Rotation of vector  $\mathbf{v}$  about a unit axis  $\hat{\omega}$  (expressed in the same frame) by an amount  $\theta$  and translation of it by  $\mathbf{p}$  (expressed in the same frame) is vector  $\mathbf{v}'$  expressed in the same frame:

$$\mathbf{v}' = \mathbf{T}\mathbf{v} = \text{Trans}(\mathbf{p})\text{Rot}(\hat{\omega}, \theta)\mathbf{v}$$

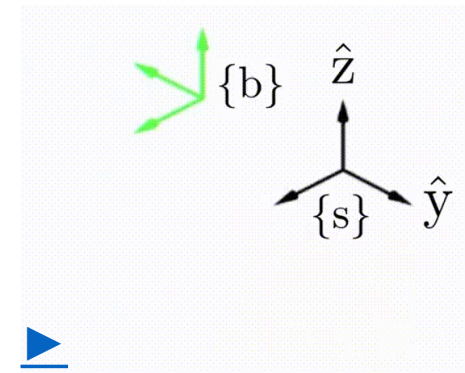
← Interpretation

- Fixed-frame Transformation:**

2. Translating it by  $\mathbf{p}$  in  $\{s\}$  to get  $\{b'\}$
1. Rotating  $\{b\}$  by  $\theta$  about  $\hat{\omega}$  in  $\{s\}$  (this moves  $\{b\}$  origin)

$$\mathbf{T}_{sb'} = \mathbf{T}\mathbf{T}_{sb} = \text{Trans}(\mathbf{p})\text{Rot}(\hat{\omega}, \theta)\mathbf{T}_{sb}$$

← Interpretation

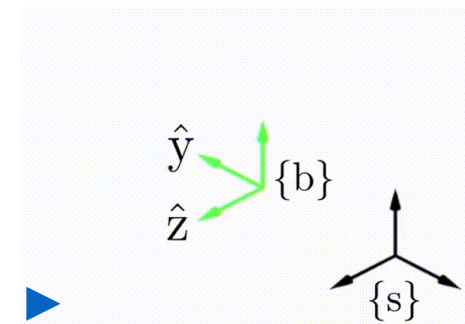


- Body-frame Transformation:**

1. Translating  $\{b\}$  by  $\mathbf{p}$  in  $\{b\}$
2. Rotating it by  $\theta$  about  $\hat{\omega}$  in the new body frame to get  $\{b''\}$

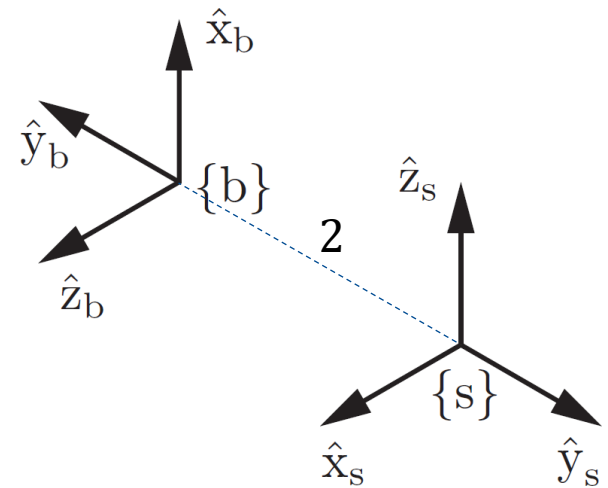
$$\mathbf{T}_{sb''} = \mathbf{T}_{sb}\mathbf{T} = \mathbf{T}_{sb}\text{Trans}(\mathbf{p})\text{Rot}(\hat{\omega}, \theta)$$

→ Interpretation



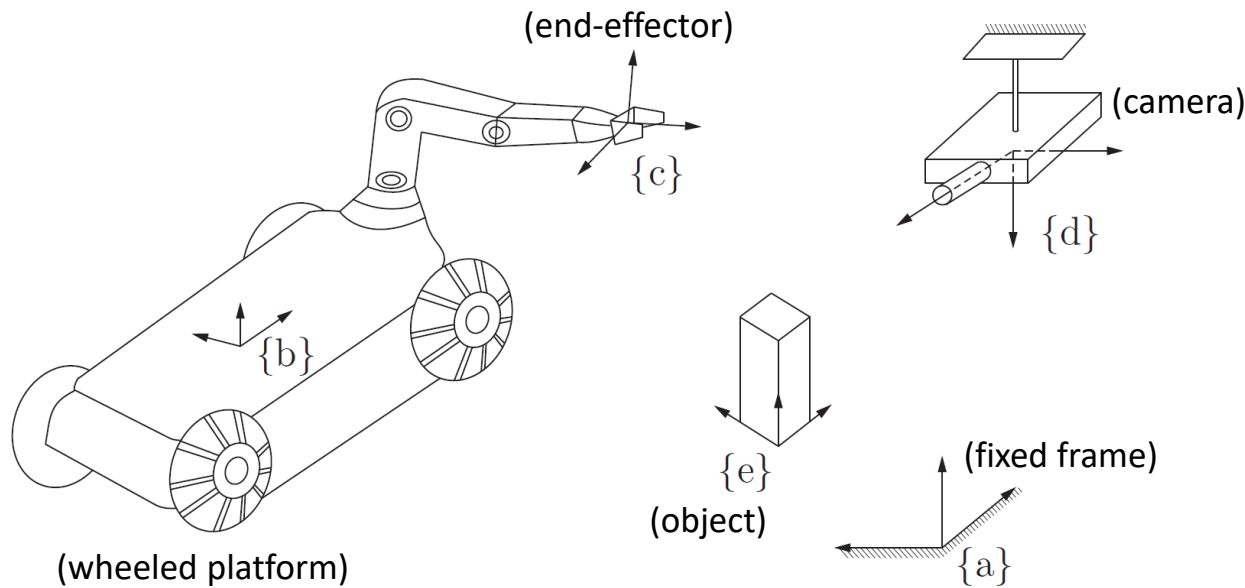
# Example

Fixed-frame and body-frame transformations corresponding to  $\hat{\omega} = (0,0,1)$ ,  $\theta = 90^\circ$ , and  $\mathbf{p} = (0,2,0)$ .



# Example

A robot arm mounted on a wheeled mobile platform moving in a room, and a camera fixed to the ceiling. The robot must pick up an object with body frame  $\{e\}$ . What is the configuration of the object relative to the robot hand,  $T_{ce}$ , given  $T_{db}$ ,  $T_{de}$ ,  $T_{bc}$ , and  $T_{ad}$ ?

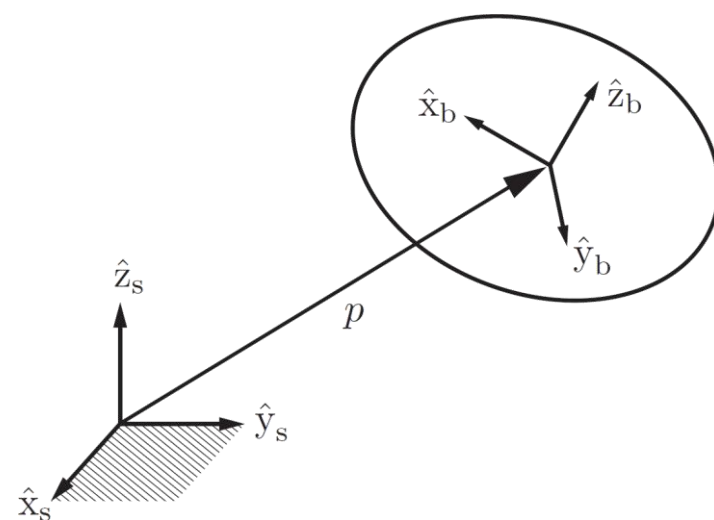


# Twists

# Spatial Velocity or Twist

Finding both the linear and angular velocity of frame  $\{b\}$  attached to a moving body.

$$\mathbf{T}(t) = \begin{bmatrix} \mathbf{R}(t) & \mathbf{p}(t) \\ \mathbf{0} & 1 \end{bmatrix} : \mathbf{T}_{sb} \text{ at time } t$$



# Body Twist

Similar to  $R^{-1}\dot{R} = [\omega_b]$ , let's compute  $T^{-1}\dot{T}$ :

$$\begin{aligned}
 T^{-1}\dot{T} &= \begin{bmatrix} R^T & -R^T p \\ \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \dot{R} & \dot{p} \\ \mathbf{0} & 0 \end{bmatrix} \\
 &= \begin{bmatrix} R^T \dot{R} & R^T \dot{p} \\ \mathbf{0} & 0 \end{bmatrix} \\
 &= \begin{bmatrix} [\omega_b] & v_b \\ \mathbf{0} & 0 \end{bmatrix} \xrightarrow[\substack{v_b \in \mathbb{R}^3 \\ [\omega_b] \in so(3)}]{\text{red arrow}} \mathcal{V}_b = \begin{bmatrix} \omega_b \\ v_b \end{bmatrix} \in \mathbb{R}^6
 \end{aligned}$$

$\mathcal{V}_b$  is defined as **Body Twist**  
(or spatial velocity in the body frame)

$$T^{-1}\dot{T} = [\mathcal{V}_b] = \begin{bmatrix} [\omega_b] & v_b \\ \mathbf{0} & 0 \end{bmatrix} \in se(3)$$

The set of all  $4 \times 4$  matrices of this form is called  $se(3)$  and comprises the  $4 \times 4$  matrix representations of the **body twists** associated with the rigid-body configurations  $SE(3)$ .

( $se(3)$  is called the Lie algebra of the Lie group  $SE(3)$ )

# Spatial Twist

Similar to  $\dot{R}R^{-1} = [\omega_s]$ , let's compute  $\dot{T}T^{-1}$ :

$$\begin{aligned}
 \dot{T}T^{-1} &= \begin{bmatrix} \dot{R} & \dot{p} \\ \mathbf{0} & 0 \end{bmatrix} \begin{bmatrix} R^T & -R^T p \\ \mathbf{0} & 1 \end{bmatrix} \\
 &= \begin{bmatrix} \dot{R}R^T & \dot{p} - \dot{R}R^T p \\ \mathbf{0} & 0 \end{bmatrix} \\
 &= \begin{bmatrix} [\omega_s] & v_s \\ \mathbf{0} & 0 \end{bmatrix} \xrightarrow[\substack{v_s \in \mathbb{R}^3 \\ [\omega_s] \in so(3)}]{\text{red arrow}} \mathcal{V}_s = \begin{bmatrix} \omega_s \\ v_s \end{bmatrix} \in \mathbb{R}^6
 \end{aligned}$$

$\mathcal{V}_s$  is defined as **Spatial Twist**  
(or spatial velocity in the space frame)

$$\dot{T}T^{-1} = [\mathcal{V}_s] = \begin{bmatrix} [\omega_s] & v_s \\ \mathbf{0} & 0 \end{bmatrix} \in se(3)$$

The set of all  $4 \times 4$  matrices of this form is called  $se(3)$  and comprises the  $4 \times 4$  matrix representations of the **spatial twists** associated with the rigid-body configurations  $SE(3)$ .



# Adjoint Map

~~$$\mathbf{v}_s = \mathbf{T}_{sb} \mathbf{v}_b$$

$\downarrow$   
 $4 \times 4$

$\downarrow$   
 $6 \times 6$~~

$$\begin{aligned} [\mathbf{v}_b] &= \mathbf{T}^{-1} \dot{\mathbf{T}} \\ [\mathbf{v}_s] &= \dot{\mathbf{T}} \mathbf{T}^{-1} \end{aligned}$$

$$\longrightarrow [\mathbf{v}_s] = \mathbf{T} [\mathbf{v}_b] \mathbf{T}^{-1} \longrightarrow$$

$$[\mathbf{v}_s] = \begin{bmatrix} \mathbf{R}[\boldsymbol{\omega}_b] \mathbf{R}^T & -\mathbf{R}[\boldsymbol{\omega}_b] \mathbf{R}^T \mathbf{p} + \mathbf{R} \mathbf{v}_b \\ \mathbf{0} & \mathbf{0} \end{bmatrix} \quad \xrightarrow{\begin{array}{l} \mathbf{R}[\boldsymbol{\omega}] \mathbf{R}^T = [\mathbf{R} \boldsymbol{\omega}] \\ [\boldsymbol{\omega}] \mathbf{p} = -[\mathbf{p}] \boldsymbol{\omega} \quad \mathbf{p}, \boldsymbol{\omega} \in \mathbb{R}^3 \end{array}}$$

$$\mathbf{v}_s = \begin{bmatrix} \boldsymbol{\omega}_s \\ \mathbf{v}_s \end{bmatrix} = \begin{bmatrix} \mathbf{R} & \mathbf{0} \\ [\mathbf{p}] \mathbf{R} & \mathbf{R} \end{bmatrix} \begin{bmatrix} \boldsymbol{\omega}_b \\ \mathbf{v}_b \end{bmatrix} = [\text{Ad}_{\mathbf{T}_{sb}}] \mathbf{v}_b$$

$$[\text{Ad}_{\mathbf{T}}] = \begin{bmatrix} \mathbf{R} & \mathbf{0} \\ [\mathbf{p}] \mathbf{R} & \mathbf{R} \end{bmatrix} \in \mathbb{R}^{6 \times 6} \quad \text{Adjoint Map associated with } \mathbf{T} \text{ or Adjoint Representation of } \mathbf{T}$$

$$\mathbf{v}_s = [\text{Ad}_{\mathbf{T}_{sb}}] \mathbf{v}_b = \text{Ad}_{\mathbf{T}_{sb}}(\mathbf{v}_b)$$

$$\text{Similarly, } \mathbf{v}_b = [\text{Ad}_{\mathbf{T}_{bs}}] \mathbf{v}_s = \text{Ad}_{\mathbf{T}_{bs}}(\mathbf{v}_s)$$

# Adjoint Map Properties

- Let  $\mathbf{T}_1, \mathbf{T}_2 \in SE(3)$  and  $\mathcal{V} = (\boldsymbol{\omega}, \mathbf{v})$ . Then,

$$[\text{Ad}_{\mathbf{T}_1}][\text{Ad}_{\mathbf{T}_2}]\mathcal{V} = [\text{Ad}_{\mathbf{T}_1\mathbf{T}_2}]\mathcal{V} \quad \text{or} \quad \text{Ad}_{\mathbf{T}_1}(\text{Ad}_{\mathbf{T}_2}(\mathcal{V})) = \text{Ad}_{\mathbf{T}_1\mathbf{T}_2}(\mathcal{V})$$

- For any  $\mathbf{T} \in SE(3)$ ,  $[\text{Ad}_{\mathbf{T}}]^{-1} = [\text{Ad}_{\mathbf{T}^{-1}}]$
- For any two frames  $\{c\}$  and  $\{d\}$ , a twist represented as  $\mathcal{V}_c$  in  $\{c\}$  is related to its representation  $\mathcal{V}_d$  in  $\{d\}$  by

$$\mathcal{V}_c = [\text{Ad}_{\mathbf{T}_{cd}}]\mathcal{V}_d \qquad \mathcal{V}_d = [\text{Ad}_{\mathbf{T}_{dc}}]\mathcal{V}_c$$

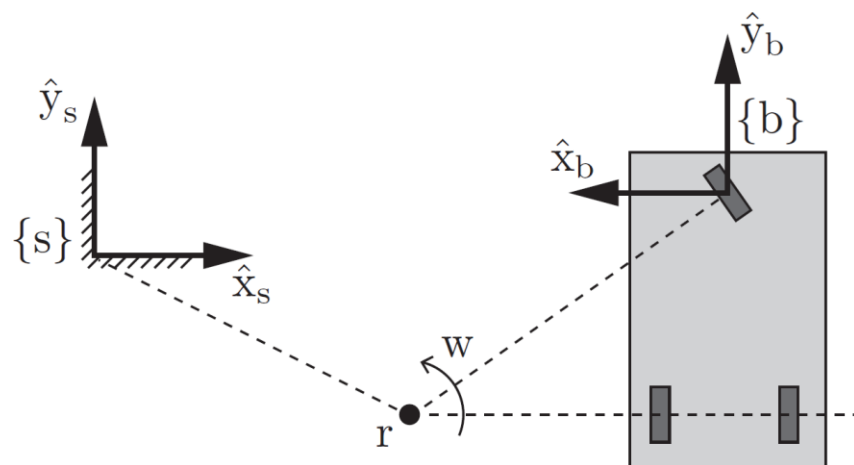
(changing the reference frame of a twist)

# Example

Consider a three-wheeled car with a single steerable front wheel, driving on a plane. The angle of the front wheel of the car causes the car's motion to be a pure angular velocity  $2 \text{ rad/s}$  about an axis out of the page at the point  $r$  in the plane. Find  $\mathcal{V}_s$  and  $\mathcal{V}_b$  when

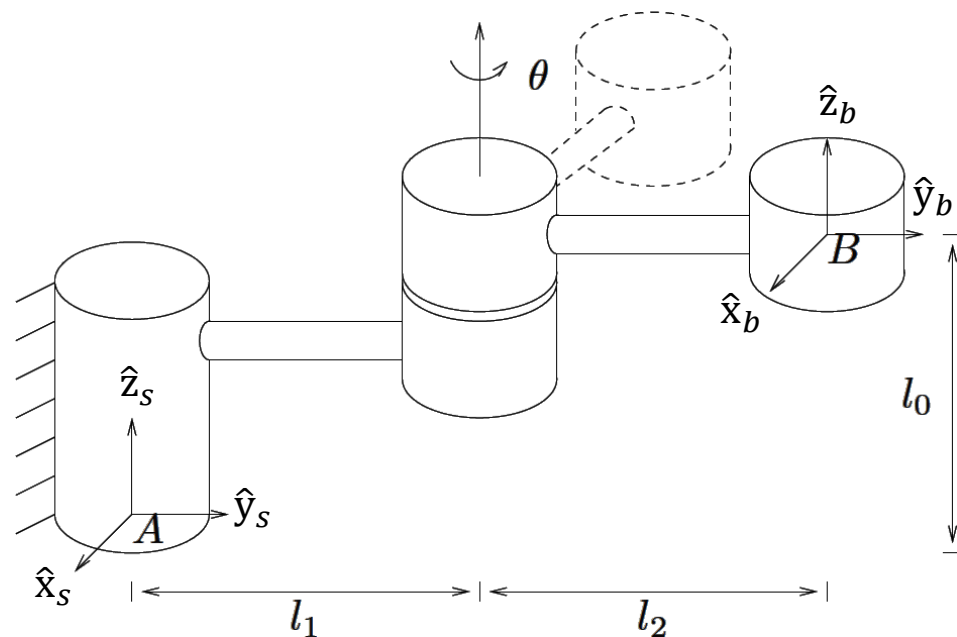
$$r_s = (2, -1, 0)$$

$$r_b = (2, -1.4, 0)$$



# Example

Find  $\mathcal{V}_s$  and  $\mathcal{V}_b$  for the shown one degree of freedom manipulator.



# Screw Interpretation of a Twist

Any rigid-body velocity or twist  $\mathcal{V}$  is equivalent to the instantaneous velocity  $\dot{\theta}$  about some screw axis  $\mathcal{S}$  (i.e., rotating about the axis while also translating along the axis).

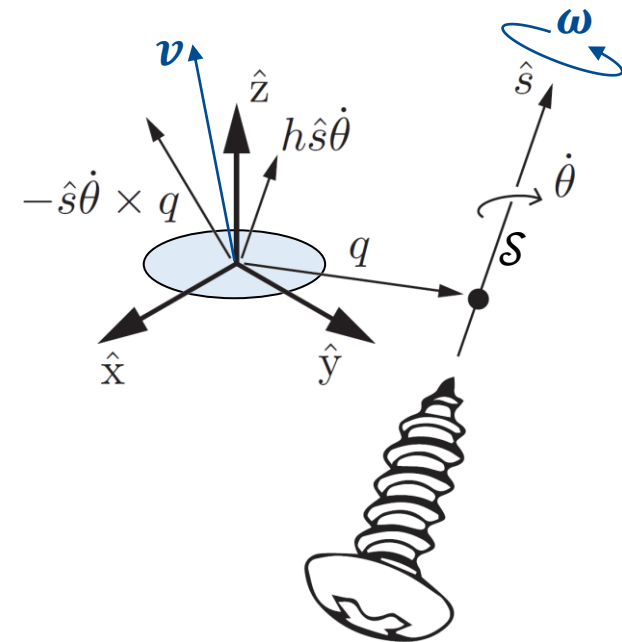
A screw axis  $\mathcal{S}$  represented by a point  $\mathbf{q} \in \mathbb{R}^3$  on the axis, a unit vector  $\hat{\mathbf{s}} \in S^2$  in the direction of the axis, and a pitch  $h \in \mathbb{R}$  (linear velocity along the axis / angular velocity  $\dot{\theta}$  about the axis) as  $\{\mathbf{q}, \hat{\mathbf{s}}, h\}$ .

Thus, twist  $\mathcal{V}$  can be represented as

$$\mathcal{V} = \begin{bmatrix} \boldsymbol{\omega} \\ \mathbf{v} \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{s}}\dot{\theta} \\ -\hat{\mathbf{s}}\dot{\theta} \times \mathbf{q} + h\dot{\theta}\hat{\mathbf{s}} \end{bmatrix}$$

Due to rotation about  $\mathcal{S}$   
(which is in the plane orthogonal to  $\hat{\mathbf{s}}$ )

Due to translation along  $\mathcal{S}$   
(which is in the direction of  $\hat{\mathbf{s}}$ )



# Screw Interpretation of a Twist

Instead of representing the screw axis  $\mathcal{S}$  as  $\{\mathbf{q}, \hat{\mathbf{s}}, h\}$  (with the non-uniqueness of  $\mathbf{q}$ ), we represent a “unit” screw axis as a vector as

$$\mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} \in \mathbb{R}^6 \quad \text{where} \quad \mathbf{v} = \mathbf{S}\dot{\theta} \in \mathbb{R}^6 \quad \mathbf{S}_\omega, \mathbf{S}_v \in \mathbb{R}^3$$

Finding  $\mathbf{S}$  by having  $\mathbf{v}$ :

**(a)** If  $\|\boldsymbol{\omega}\| \neq 0$  ( $\equiv$  rotation with/without translation along  $\hat{\mathbf{s}}$ ):

$$\begin{aligned} \mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} &= \mathbf{v} / \|\boldsymbol{\omega}\| = \begin{bmatrix} \boldsymbol{\omega} / \|\boldsymbol{\omega}\| \\ \mathbf{v} / \|\boldsymbol{\omega}\| \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{s}} \\ -\hat{\mathbf{s}} \times \mathbf{q} + h\hat{\mathbf{s}} \end{bmatrix} \\ &= \begin{bmatrix} \text{angular velocity when } \dot{\theta} = 1 \\ \text{linear velocity of origin when } \dot{\theta} = 1 \end{bmatrix} \end{aligned}$$

Pitch  $h$  is finite,  $h = \boldsymbol{\omega}^T \mathbf{v} / \|\boldsymbol{\omega}\|^2$   
 $\hat{\mathbf{s}} = \boldsymbol{\omega} / \|\boldsymbol{\omega}\|, \quad \|\mathbf{S}_\omega\| = 1$   
 $\dot{\theta} = \|\boldsymbol{\omega}\|$  is interpreted as angular velocity about  $\hat{\mathbf{s}}$

**(b)** If  $\|\boldsymbol{\omega}\| = 0$  ( $\equiv$  pure translation along  $\hat{\mathbf{s}}$ ):

$$\begin{aligned} \mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} &= \mathbf{v} / \|\mathbf{v}\| = \begin{bmatrix} \mathbf{0} \\ \mathbf{v} / \|\mathbf{v}\| \end{bmatrix} = \begin{bmatrix} \mathbf{0} \\ \hat{\mathbf{s}} \end{bmatrix} \\ &= \begin{bmatrix} \mathbf{0} \\ \text{normalized linear velocity of origin} \end{bmatrix} \end{aligned}$$

Pitch  $h$  is infinite,  $\|\mathbf{S}_\omega\| = 0$   
 $\hat{\mathbf{s}} = \mathbf{v} / \|\mathbf{v}\|, \quad \|\mathbf{S}_v\| = 1$   
 $\dot{\theta} = \|\mathbf{v}\|$  is interpreted as linear velocity along  $\hat{\mathbf{s}}$

# Screw Interpretation of a Twist

- ❖ Since a screw axis  $\mathcal{S}$  is just a normalized twist, the  $4 \times 4$  matrix representation  $[\mathcal{S}]$  of  $\mathcal{S} = (\mathcal{S}_\omega, \mathcal{S}_v)$  is

$$[\mathcal{S}] = \begin{bmatrix} [\mathcal{S}_\omega] & \mathcal{S}_v \\ \mathbf{0} & 0 \end{bmatrix} \in se(3) \qquad [\mathcal{V}] = [\mathcal{S}] \dot{\theta} \in se(3)$$

- ❖ Relation between a screw axis represented as  $\mathcal{S}_a$  in a frame  $\{a\}$  and  $\mathcal{S}_b$  in a frame  $\{b\}$ :

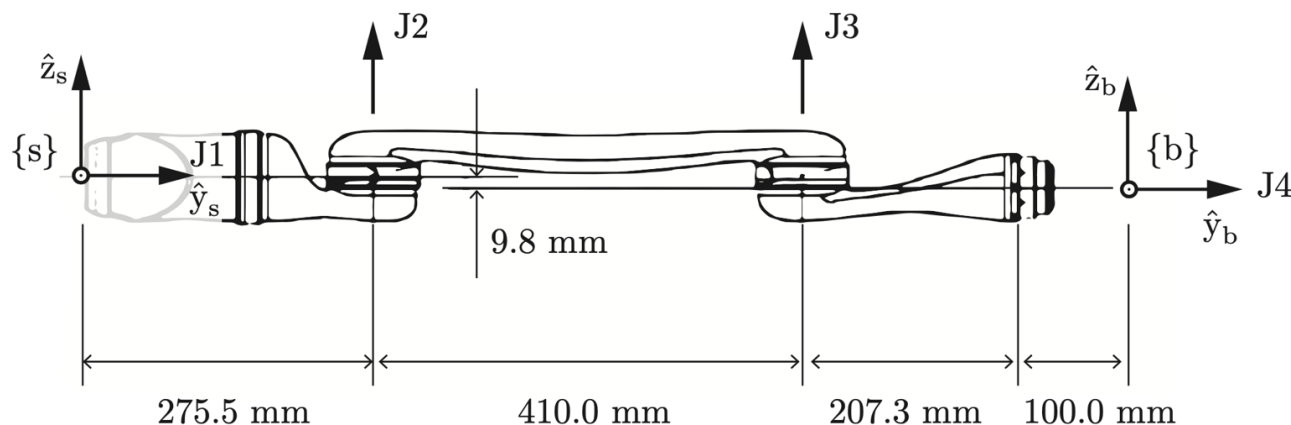
$$\mathcal{S}_a = [\text{Ad}_{T_{ab}}] \mathcal{S}_b$$

$$\mathcal{S}_b = [\text{Ad}_{T_{ba}}] \mathcal{S}_a$$

(changing the reference frame of a screw axis)

# Example

Kinova lightweight 4-dof arm:



What are the screw axis  $\mathcal{S}_b$  and  $\mathcal{S}_s$  for J4 and J2?



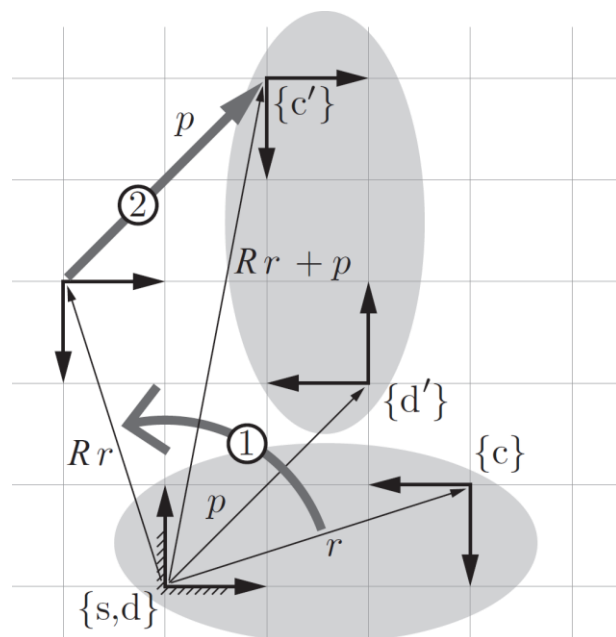
# Exponential Coordinate Representation of Rigid-Body Motion

# Screw Motion

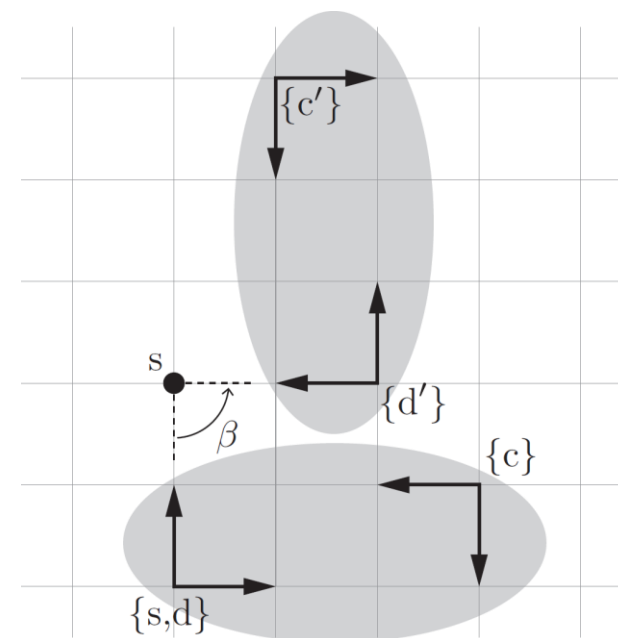
Instead of viewing a displacement as a rotation followed by a translation, both rotation and translation can be performed simultaneously.

Planar example of a screw motion:

The displacement can be viewed as a rotation of  $\beta = 90^\circ$  about a fixed point  $s$ .



$\equiv$



# Exponential Coordinates of Rigid-Body Motions

Chasles–Mozzi theorem states that every rigid-body displacement can be expressed as a finite rotation and translation about a fixed screw axis in space.

This theorem motivates a six-parameter representation of a configuration (or a homogeneous transformation  $\mathbf{T} \in SE(3)$ ) called the **exponential coordinates** as  $\mathbf{S}\theta \in \mathbb{R}^6$ , where  $\mathbf{S}$  is the screw axis and  $\theta$  is the distance that must be traveled along the screw axis to take a frame from the origin  $\mathbf{I}$  to  $\mathbf{T}$ .

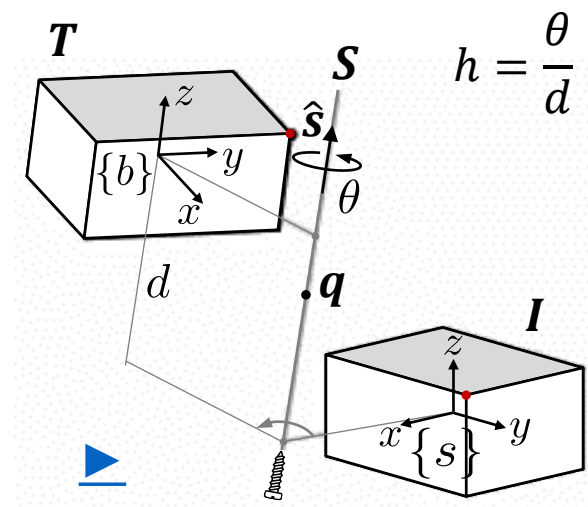
**Note:**  $\mathbf{T}$  is equivalent to the displacement obtained by rotating a frame from  $\mathbf{I}$  about  $\mathbf{S}$

- by an angle  $\theta$ , or
- at a speed  $\dot{\theta} = 1$  rad/s for  $\theta$ s, or
- at a speed  $\dot{\theta} = \theta$  for unit time, or
- by twist  $\mathcal{V}$  for unit time.

**Constant Screw Motion:**  
A rotation  $\theta$  + a translation  $d$  about/along a fixed screw axis  $\mathbf{S}$ .

$$\mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{s}} \\ -\hat{\mathbf{s}} \times \mathbf{q} + h\hat{\mathbf{s}} \end{bmatrix} \quad (\text{for rotation with/without translation along } \hat{\mathbf{s}})$$

$$\mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} = \begin{bmatrix} \mathbf{0} \\ \hat{\mathbf{s}} \end{bmatrix} \quad (\text{for pure translation along } \hat{\mathbf{s}})$$



# Exponential Coordinates of Rigid-Body Motions

As with rotations, we can define a matrix exponential (exp) and matrix logarithm (log). For any transformation matrix  $\mathbf{T} \in SE(3)$ , we can always find a screw axis  $\mathbf{S} = (\mathbf{S}_\omega, \mathbf{S}_v) \in \mathbb{R}^6$  ( $\|\mathbf{S}_\omega\| = 1$  or  $\mathbf{S}_\omega = \mathbf{0}$ ,  $\|\mathbf{S}_v\| = 1$ ) and scalar  $\theta \in \mathbb{R}$  such that  $\mathbf{T} = e^{[\mathbf{S}]\theta}$ .

$$\text{exp: } [\mathbf{S}]\theta \in se(3) \rightarrow \mathbf{T} \in SE(3) \quad : \quad e^{[\mathbf{S}]\theta} = \mathbf{T} = (\mathbf{R}, \mathbf{p})$$

$$\text{log: } \mathbf{T} \in SE(3) \rightarrow [\mathbf{S}]\theta \in se(3) \quad : \quad \log(\mathbf{T}) = [\mathbf{S}]\theta$$

$\mathbf{S}\theta \in \mathbb{R}^6$  : Exponential coordinates of  $\mathbf{T} \in SE(3)$

$[\mathbf{S}]\theta = [\mathbf{S}\theta] \in se(3)$  : Matrix logarithm of  $\mathbf{T}$  (inverse of the matrix exponential)

For a given  $\mathbf{S}$ : ( $\mathbf{S}_a = [\text{Ad}_{\mathbf{T}_{ab}}]\mathbf{S}_b$ )

$\mathbf{S}$  is expressed in  $\{b\}$

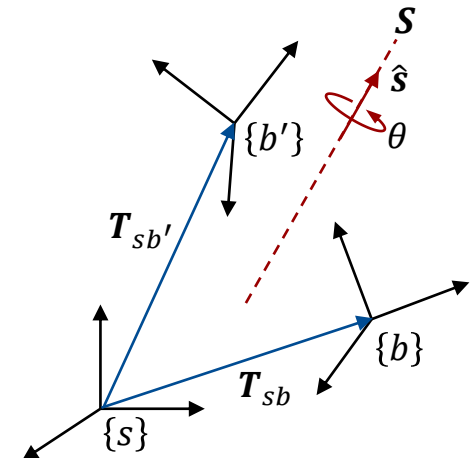
Body-frame displacement:

$$\mathbf{T}_{sb'} = \mathbf{T}_{sb} e^{[\mathbf{S}_b]\theta}$$

Fixed-frame displacement:

$$\mathbf{T}_{sb'} = e^{[\mathbf{S}_s]\theta} \mathbf{T}_{sb}$$

$\mathbf{S}$  is expressed in  $\{s\}$



# Matrix Exponential

$$\text{exp: } [S]\theta \in se(3) \rightarrow T \in SE(3) \quad : \quad e^{[S]\theta} = T = (R, p)$$

❖ Finding  $T = (R, p)$  by having  $S = (S_\omega, S_v)$  and  $\theta$ :

**(a)** If  $\|S_\omega\| = 1$ :

$$e^{[S]\theta} = \begin{bmatrix} e^{[S_\omega]\theta} & G(\theta)S_v \\ \mathbf{0} & 1 \end{bmatrix} = \begin{bmatrix} R & p \\ \mathbf{0} & 1 \end{bmatrix}$$

$$G(\theta) = I\theta + (1 - \cos \theta)[S_\omega] + (\theta - \sin \theta)[S_\omega]^2 \in \mathbb{R}^{3 \times 3}$$

**(b)** If  $S_\omega = \mathbf{0}$  ( $\|S_v\| = 1$ ):

$$e^{[S]\theta} = \begin{bmatrix} I & S_v\theta \\ \mathbf{0} & 1 \end{bmatrix} = \begin{bmatrix} R & p \\ \mathbf{0} & 1 \end{bmatrix}$$

# Matrix Logarithm

$$\log: \quad \mathbf{T} \in SE(3) \quad \rightarrow \quad [\mathbf{S}]\theta \in se(3) \quad : \quad \log(\mathbf{T}) = [\mathbf{S}]\theta$$

❖ Finding  $\mathbf{S} = (\mathbf{S}_\omega, \mathbf{S}_v)$  and  $\theta \in [0, \pi]$  by having  $\mathbf{T} = (\mathbf{R}, \mathbf{p})$ :

**(a)** If  $\mathbf{R} = \mathbf{I}$ , then set  $\mathbf{S}_\omega = \mathbf{0}$ ,  $\mathbf{S}_v = \mathbf{p}/\|\mathbf{p}\|$ , and  $\theta = \|\mathbf{p}\|$ .

**(b)** Otherwise, use the matrix logarithm  $\log(\mathbf{R}) = [\mathbf{S}_\omega]\theta$  to determine  $\mathbf{S}_\omega$  ( $\hat{\boldsymbol{\omega}}$  in the  $SO(3)$  algorithm) and  $\theta \in [0, \pi]$ . Then,  $\mathbf{S}_v$  is calculated as

$$\mathbf{S}_v = \mathbf{G}^{-1}(\theta)\mathbf{p}$$

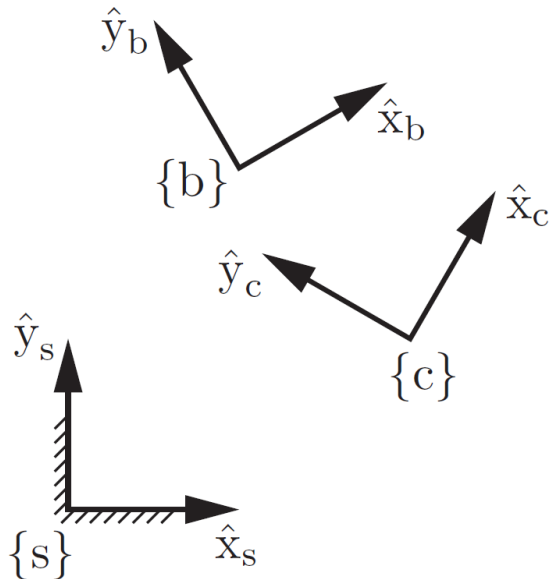
$$\mathbf{G}^{-1}(\theta) = \frac{1}{\theta}\mathbf{I} - \frac{1}{2}[\mathbf{S}_\omega] + \left(\frac{1}{\theta} - \frac{1}{2}\cot\frac{\theta}{2}\right)[\mathbf{S}_\omega]^2 \in \mathbb{R}^{3 \times 3}$$

# Example

The initial frame  $\{b\}$  and final frame  $\{c\}$  are given. Find the screw motion that displaces the frame at  $T_{sb}$  to  $T_{sc}$ .

$$T_{sb} = \begin{bmatrix} \cos 30^\circ & -\sin 30^\circ & 0 & 1 \\ \sin 30^\circ & \cos 30^\circ & 0 & 2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_{sc} = \begin{bmatrix} \cos 60^\circ & -\sin 60^\circ & 0 & 2 \\ \sin 60^\circ & \cos 60^\circ & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



# Wrenches



# wrench

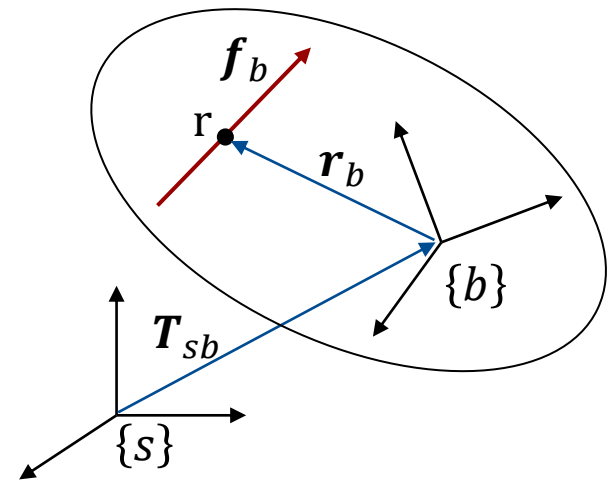
Consider a linear force  $\mathbf{f}$  acting on a rigid body at a point  $\mathbf{r}$ . Both  $\mathbf{f}_b \in \mathbb{R}^3$  and  $\mathbf{r}_b \in \mathbb{R}^3$  are represented in  $\{b\}$ . This force creates a torque or moment  $\mathbf{m}_b \in \mathbb{R}^3$  in  $\{b\}$  as

$$\mathbf{m}_b = \mathbf{r}_b \times \mathbf{f}_b$$

We can package the moment and force together in a single six-dimensional vector called **wrench** (or **spatial force**) in  $\{b\}$  as

$$\mathcal{F}_b = \begin{bmatrix} \mathbf{m}_b \\ \mathbf{f}_b \end{bmatrix} \in \mathbb{R}^6$$

$$\mathcal{F}_s = ?$$



# wrench

The **power** is a coordinate-independent quantity, i.e., the power generated (or dissipated) by an  $(\mathcal{F}, \mathcal{V})$  pair (wrench and twist) must be the same regardless of the frame in which it is represented:

$$(\mathcal{V} \cdot \mathcal{F} = \text{power})$$

$$\mathcal{V}_s^T \mathcal{F}_s = \mathcal{V}_b^T \mathcal{F}_b = \text{power}$$

$$(\mathcal{V}_b = [\text{Ad}_{T_{bs}}] \mathcal{V}_s)$$

$$\begin{aligned} \mathcal{V}_s^T \mathcal{F}_s &= ([\text{Ad}_{T_{bs}}] \mathcal{V}_s)^T \mathcal{F}_b \\ &= \mathcal{V}_s^T [\text{Ad}_{T_{bs}}]^T \mathcal{F}_b \end{aligned}$$

Since this must hold for all  $\mathcal{V}_s$

$$\mathcal{F}_s = [\text{Ad}_{T_{bs}}]^T \mathcal{F}_b$$

spatial wrench

body wrench

---

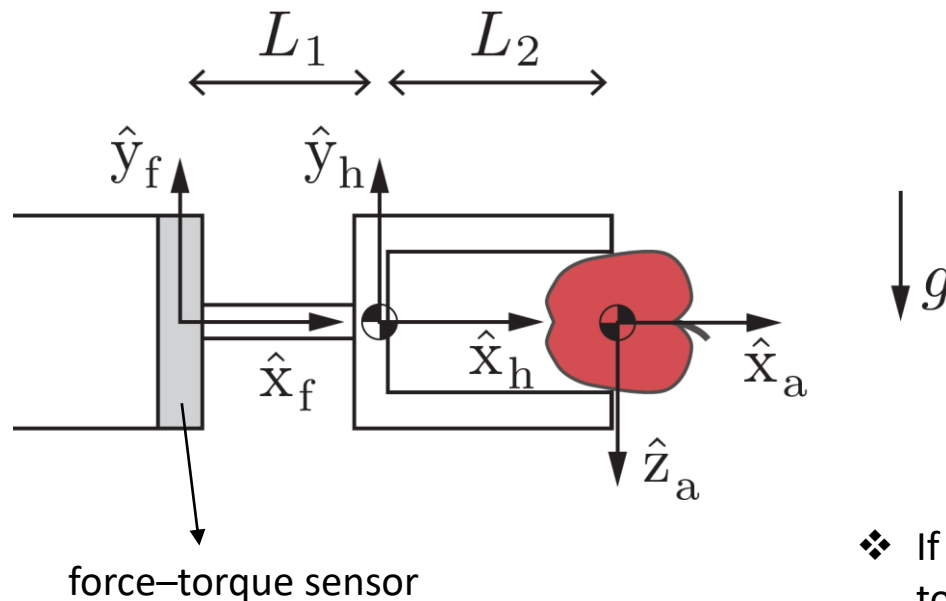

$$\mathcal{F}_a = [\text{Ad}_{T_{ba}}]^T \mathcal{F}_b$$

$$\mathcal{F}_b = [\text{Ad}_{T_{ab}}]^T \mathcal{F}_a$$

(changing the reference frame of a twist)

# Example

The robot hand shown is holding an apple with a mass of 0.1 kg in a gravitational field  $g=10 \text{ m/s}^2$ . The mass of the hand is 0.5 kg,  $L_1=10 \text{ cm}$ , and  $L_2=15 \text{ cm}$ . What is the force and torque measured by the six-axis force–torque sensor between the hand and the robot arm?



- ❖ If more than one wrench acts on a rigid body, the total wrench on the body is simply the vector sum of the individual wrenches, provided that the wrenches are expressed in the same frame.

# Review

Rotations	Rigid-Body Motions
$R \in SO(3) : 3 \times 3$ matrices $R^T R = I, \det R = 1$	$T \in SE(3) : 4 \times 4$ matrices $T = \begin{bmatrix} R & p \\ 0 & 1 \end{bmatrix},$ where $R \in SO(3), p \in \mathbb{R}^3$
$R^{-1} = R^T$	$T^{-1} = \begin{bmatrix} R^T & -R^T p \\ 0 & 1 \end{bmatrix}$
change of coordinate frame: $R_{ab} R_{bc} = R_{ac}, \quad R_{ab} p_b = p_a$	change of coordinate frame: $T_{ab} T_{bc} = T_{ac}, \quad T_{ab} p_b = p_a$

# Review

---

rotating a frame  $\{b\}$ :

$$R = \text{Rot}(\hat{\omega}, \theta)$$

$$R_{sb'} = RR_{sb}:$$

rotate  $\theta$  about  $\hat{\omega}_s = \hat{\omega}$ 

$$R_{sb''} = R_{sb}R:$$

rotate  $\theta$  about  $\hat{\omega}_b = \hat{\omega}$ 

displacing a frame  $\{b\}$ :

$$T = \begin{bmatrix} \text{Rot}(\hat{\omega}, \theta) & p \\ 0 & 1 \end{bmatrix}$$

 $T_{sb'} = TT_{sb}$ : rotate  $\theta$  about  $\hat{\omega}_s = \hat{\omega}$   
(moves  $\{b\}$  origin), translate  $p$  in  $\{s\}$ 
 $T_{sb''} = T_{sb}T$ : translate  $p$  in  $\{b\}$ ,  
rotate  $\theta$  about  $\hat{\omega}$  in new body frame

---

unit rotation axis is  $\hat{\omega} \in \mathbb{R}^3$ ,

where  $\|\hat{\omega}\| = 1$ 

“unit” screw axis is  $\mathcal{S} = \begin{bmatrix} \omega \\ v \end{bmatrix} \in \mathbb{R}^6$ ,

where either (i)  $\|\omega\| = 1$  or  
(ii)  $\omega = 0$  and  $\|v\| = 1$ 


---

for a screw axis  $\{q, \hat{s}, h\}$  with finite  $h$ ,

$$\mathcal{S} = \begin{bmatrix} \omega \\ v \end{bmatrix} = \begin{bmatrix} \hat{s} \\ -\hat{s} \times q + h\hat{s} \end{bmatrix}$$

---

angular velocity is  $\omega = \hat{\omega}\dot{\theta}$ 

twist is  $\mathcal{V} = \mathcal{S}\dot{\theta}$ 


---

# Review

for any 3-vector, e.g.,  $\omega \in \mathbb{R}^3$ ,

$$[\omega] = \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix} \in so(3)$$

identities,  $\omega, x \in \mathbb{R}^3, R \in SO(3)$ :

$$\begin{aligned} [\omega] &= -[\omega]^T, [\omega]x = -[x]\omega, \\ [\omega][x] &= ([x][\omega])^T, R[\omega]R^T = [R\omega] \end{aligned}$$

$$\text{for } \mathcal{V} = \begin{bmatrix} \omega \\ v \end{bmatrix} \in \mathbb{R}^6,$$

$$[\mathcal{V}] = \begin{bmatrix} [\omega] & v \\ 0 & 0 \end{bmatrix} \in se(3)$$

(the pair  $(\omega, v)$  can be a twist  $\mathcal{V}$   
or a “unit” screw axis  $\mathcal{S}$ ,  
depending on the context)

$$\dot{R}R^{-1} = [\omega_s], \quad R^{-1}\dot{R} = [\omega_b]$$

$$\dot{T}T^{-1} = [\mathcal{V}_s], \quad T^{-1}\dot{T} = [\mathcal{V}_b]$$

$$[\text{Ad}_T] = \begin{bmatrix} R & 0 \\ [p]R & R \end{bmatrix} \in \mathbb{R}^{6 \times 6}$$

$$\text{identities: } [\text{Ad}_T]^{-1} = [\text{Ad}_{T^{-1}}],$$

$$[\text{Ad}_{T_1}][\text{Ad}_{T_2}] = [\text{Ad}_{T_1 T_2}]$$

change of coordinate frame:

$$\hat{\omega}_a = R_{ab}\hat{\omega}_b, \quad \omega_a = R_{ab}\omega_b$$

change of coordinate frame:

$$\mathcal{S}_a = [\text{Ad}_{T_{ab}}]\mathcal{S}_b, \quad \mathcal{V}_a = [\text{Ad}_{T_{ab}}]\mathcal{V}_b$$

# Review

exp coords for $R \in SO(3)$ : $\hat{\omega}\theta \in \mathbb{R}^3$	exp coords for $T \in SE(3)$ : $\mathcal{S}\theta \in \mathbb{R}^6$
$\exp : [\hat{\omega}]\theta \in so(3) \rightarrow R \in SO(3)$ $R = \text{Rot}(\hat{\omega}, \theta) = e^{[\hat{\omega}]\theta} =$ $I + \sin \theta [\hat{\omega}] + (1 - \cos \theta) [\hat{\omega}]^2$	$\exp : [\mathcal{S}]\theta \in se(3) \rightarrow T \in SE(3)$ $T = e^{[\mathcal{S}]\theta} = \begin{bmatrix} e^{[\omega]\theta} & * \\ 0 & 1 \end{bmatrix}$ where $*$ = $(I\theta + (1 - \cos \theta)[\omega] + (\theta - \sin \theta)[\omega]^2)v$
$\log : R \in SO(3) \rightarrow [\hat{\omega}]\theta \in so(3)$	$\log : T \in SE(3) \rightarrow [\mathcal{S}]\theta \in se(3)$
moment change of coord frame: $m_a = R_{ab}m_b$	wrench change of coord frame: $\mathcal{F}_a = (m_a, f_a) = [\text{Ad}_{T_{ba}}]^T \mathcal{F}_b$