The Impact Analysis of Two Identical Bars Using The Wave Equation and d'Alembert Solution

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The d'Alembert solution to wave equation in one-dimension, Eq. 1, includes two main terms: (a) f(x+ct) which indicates a backward wave moving in the negative direction of x-axis (see Figure. 1 for the direction of x-axis) and (b) f(x-ct) that is a forward wave moving in the positive direction of x-axis.

$$u(x,t) = \frac{1}{2} [f(x+ct) + f(x-ct)] \tag{1}$$

Invoking the chain role and assuming linear elasticity, the velocity, v, and longitudinal stress, σ , can be calculated from the following equations.

$$v(x,t) = \frac{\partial u(x,t)}{\partial t} = cf'(x+ct) - cf'(x-ct)$$

$$\sigma(x,t) = E\epsilon = E\frac{\partial u(x,t)}{\partial x} = E[f'(x+ct) - f'(x-ct)]$$
(2)

in which E is the Young's modulus and ϵ is longitudinal strain.

In the case of impact of two identical bars with similar ρ , A and l, to avoid misinterpretation as well as input conflict in Maple, we may use the following forms of wave equation where the second backward wave is replaced with letter g and subscripts 1 and 2 denotes bars s1 and s2, respectively.

$$u_1(x,t) = \frac{1}{2} [g_1(x+ct) + f_1(x-ct)]$$

$$u_2(x,t) = \frac{1}{2} [g_2(x+ct) + f_2(x-ct)]$$
(3)

Consequently, v and σ become

$$v_1(x,t) = cg'_1(x+ct) - cf'_1(x-ct)$$

$$\sigma_1(x,t) = E[g'_1(x+ct) - f'_1(x-ct)]$$

$$v_2(x,t) = cg'_2(x+ct) - cf'_2(x-ct)$$

$$\sigma_2(x,t) = E[g'_2(x+ct) - f'_2(x-ct)]$$
(4)

The set of equations in Eq. 4 along with suitable initial and boundary conditions can be used in analyzing the impact of bars.

Suppose the problem in Figure. 1 where the bar s1 hits the stationary bar s2. The problem can be broken into different time intervals.

2 t = 0

At t = 0, both bars are stress-free and the bar s1 has the initial velocity v_0 . As s1 hits s2, a compressive wave is generated at the contact area and propagates towards the left and right in s1 and s2, respectively which are essentially g_1 and f_2 terms in Eq. 3. At this time the following initial and boundary conditions can be written.

$$v_{1}(x,0) = v_{0} \Rightarrow cg'_{1}(x) - cf'_{1}(x) = v_{0}$$

$$\sigma_{1}(x,0) = 0 \Rightarrow E[g'_{1}(x) - f'_{1}(x)] = 0$$

$$v_{2}(x,0) = 0 \Rightarrow cg'_{2}(x) - cf'_{2}(x) = 0$$

$$\sigma_{2}(x,0) = 0 \Rightarrow E[g'_{2}(x) - f'_{2}(x)] = 0$$
(5)

Using dsolve command from Maple gives

$$g_1(x) = \frac{v_0 x}{2c} + c_2$$

$$f_1(x) = -\frac{v_0 x}{2c} + c_4$$

$$g_2(x) = c_1$$

$$f_2(x) = c_3$$
(6)

 c_1 to c_4 are constants and are not required to be determined as they vanish in calculating velocity and longitudinal stress. Eq. 6 shows that at t=0, s1 is characterized by the two backward $(g_1(x+ct))$ and forward $(f_1(x-ct))$ waves. Substituting Eq. 6 in Eq. 5 gives

$$v_1(x,0) = v_0$$

$$\sigma_1(x,0) = 0$$

$$v_2(x,0) = 0$$

$$\sigma_2(x,0) = 0$$
(7)

which concludes the velocity and longitudinal stress at t=0.

3
$$0 < t < \frac{l}{c}$$

After impact, the initial and boundary condition for the solution of the set of equations in Eq. 4 require updating. To find the velocity of both bars after impact we use Newton's third law.

$$\begin{cases} \sigma_1 = \rho c(v' - v_0) \\ \sigma_2 = \rho c(-v' - 0) \end{cases} \xrightarrow{\underline{\sigma_1 = \sigma_2}} v_0 - v' = v' \Rightarrow v' = \frac{v_0}{2}$$

The initial and boundary conditions update accordingly.

$$v_{1}(x,t) = \frac{v_{0}}{2} \Rightarrow cg'_{1}(x) - cf'_{1}(x) = \frac{v_{0}}{2}$$

$$\sigma_{1}(x,t) = -\frac{\rho c v_{0}}{2} \Rightarrow E[g'_{1}(x) - f'_{1}(x)] = -\frac{\rho c v_{0}}{2}$$

$$v_{2}(x,t) = \frac{v_{0}}{2} \Rightarrow cg'_{2}(x) - cf'_{2}(x) = \frac{v_{0}}{2}$$

$$\sigma_{2}(x,t) = -\frac{\rho c v_{0}}{2} \Rightarrow E[g'_{2}(x) - f'_{2}(x)] = -\frac{\rho c v_{0}}{2}$$
(8)

The following answers are obtained from Maple.

$$g_{1}(x) = -\frac{\rho c v_{0}}{4E} x + \frac{v_{0}}{4c} x + c_{2}$$

$$f_{1}(x) = -\frac{\rho c v_{0}}{4E} x - \frac{v_{0}}{4c} x + c_{4}$$

$$g_{2}(x) = -\frac{\rho c v_{0}}{4E} x + \frac{v_{0}}{4c} x + c_{1}$$

$$f_{2}(x) = -\frac{\rho c v_{0}}{4E} x - \frac{v_{0}}{4c} x + c_{3}$$
(9)

Here, the interaction of the generated backward and forward waves represents the velocity and longitudinal stress. Plug-in Eq. 9 in Eq. 8, we get the velocity and longitudinal stress.

$$v_{1}(x,0) = \frac{v_{0}}{2}$$

$$\sigma_{1}(x,0) = -\frac{\rho c v_{0}}{2}$$

$$v_{2}(x,0) = \frac{v_{0}}{2}$$

$$\sigma_{2}(x,0) = -\frac{\rho c v_{0}}{2}$$
(10)

which also has been determined from Newton's third law.

4
$$\frac{l}{c} < t < \frac{2l}{c}$$

At this time interval, the generated compressive waves reflect as tensile wave (unloading wave) due to free boundary conditions on the left and right sides of s1 and s2. The generated tensile wave make both bars stress-free and the velocities can be calculated from stress equations.

$$-\sigma_{1c} + \sigma_{1t} = 0 \Rightarrow \rho c \left(-\frac{v_0}{2} + v'' \right) \Rightarrow v'' = \frac{v_0}{2}$$

The subscript c and t denote compressive and tensile waves. Using the above result, one is able to calculate the velocity of each bar.

For s1,

$$\frac{v_0}{2} - \frac{v_0}{2} = 0$$

For s2,

$$\frac{v_0}{2} + \frac{v_0}{2} = v_0$$

The initial and boundary conditions are

$$v_{1}(x,0) = 0 \Rightarrow cg'_{1}(x) - cf'_{1}(x) = 0$$

$$\sigma_{1}(x,0) = 0 \Rightarrow E[g'_{1}(x) - f'_{1}(x)] = 0$$

$$v_{2}(x,0) = v_{0} \Rightarrow cg'_{2}(x) - cf'_{2}(x) = v_{0}$$

$$\sigma_{2}(x,0) = 0 \Rightarrow E[g'_{2}(x) - f'_{2}(x)] = 0$$
(11)

Solving the above set of differential equations results in

$$g_1(x) = c_2$$

$$f_1(x) = c_4$$

$$g_2(x) = \frac{v_0 x}{2c} + c_1$$

$$f_2(x) = -\frac{v_0 x}{2c} + c_3$$
(12)

As it can be inferred from Eq. 12 The velocity and longitudinal stress are characterized by the backward $(g_2(x+ct))$ and forward $(f_2(x-ct))$ waves of s2 and are

$$v_1(x,0) = 0$$

 $\sigma_1(x,0) = 0$
 $v_2(x,0) = v_0$
 $\sigma_2(x,0) = 0$ (13)

Figure. 1 summarises the above explanation.

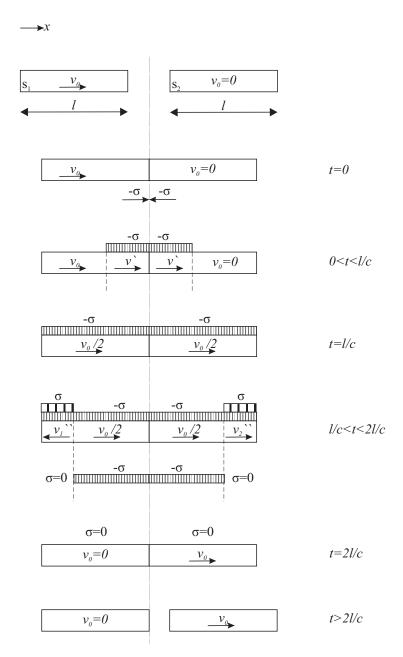


Figure 1: Different steps in the impact of two identical bars, one stationary and another with an initial velocity.