The Longitudinal Impact of a Rigid Mass Against an Elastic Bar

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1 Problem Statement

Figure. 1 illustrates the longitudinal impact of a rigid mass against an elastic bar. The rigid body has a mass m_2 and an initial velocity v_0 whereas the elastic bar is fixed at x=l and is free at the origin and has a mass m_1 , density ρ , length l with a cross-sectional area A and Young's modulus E. In the following, c is the wave speed.

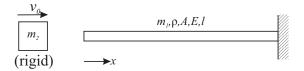


Figure 1: The problem geometry and coordinate system.

2 0 < ct < 2l **at** x = 0

At time interval 0 < ct < 2l, assuming that t = 0 is the time when the rigid mass hits the bar, a compressive forward wave f(ct - x) is generated at x = 0 which takes $t = \frac{2l}{c}$ for the generated wave f_0 to return to x = 0. The subscript zero denotes the number given to the generated wave. The displacement, u, and strain, ϵ , for this time interval are given here for convenience as it is used later in the subsequent sections.

$$u_0(x,t) = f_0 = \frac{lv_0}{Mc} \left(1 - e^{-\frac{M}{l}ct} \right)$$

$$\epsilon = -\frac{v_0}{c} e^{-\frac{M}{l}ct}$$
(1)

where

$$M = \frac{\rho Al}{m_2} = \frac{EAl}{m_2 c^2} \tag{2}$$

3 l < ct < 3l at x = l

As soon as the compressive backward wave $f_0(ct-x)$ arrives at the fixed boundary (x=l), it reflects as a compressive backward wave $g_1(ct+x)$. g_1 has a latency of $\frac{l}{c}$; therefore, this backward wave is written as $g_1(ct+x-2l)$. Writing and simplifying the relevant equations results in

$$g_1 = \frac{v_0 l}{cM} \left(e^{-\frac{M}{l} (ct + x - 2l)} - 1 \right)$$
 (3)

The subscript one represents the generated wave number.

4 2l < ct < 4l at x = 0

At this time interval, both the forward and backward wave contribute to the displacement and it can be written as

$$u_1(x,t) = f_1(ct - x - 2l) + g_1(ct + x - 2l)$$

= $f_1(\xi_1) + g_1(\xi_2)$ (4)

in which

$$\begin{cases} \xi_1 = ct - x - 2l \\ \xi_2 = ct + x - 2l \end{cases}$$

In Eq. 4, g_1 is substituted from Eq. 3 and f_1 is unknown.

4.1 Determination of f_1

One can write Newton's second law for Figure. 1 for 2l < ct < 4l at x = 0

$$-m_2 \frac{\partial u^2(x,t)}{\partial t^2} = -EA \frac{\partial u(x,t)}{\partial x}$$
$$m_2 c^2 (f_1''(\xi_1) + g_1''(\xi_2)) = EA(g_1'(\xi_2) - f_1'(\xi_1))$$

where the chain rule is utilized in calculating the derivatives, i.e., $\frac{\partial f_1}{\partial \xi_1} \frac{\partial \xi_1}{\partial t}$.

Because all the above calculations are done at the free end of the bar (x = 0), ξ_1 and ξ_2 can be replaced by $\xi = ct - 2l$.

$$m_2 c^2 (f_1''(\xi) + g_1''(\xi)) = EA(g_1'(\xi) - f_1'(\xi))$$

$$f_1''(\xi) + g_1''(\xi) = \frac{M}{I} (g_1'(\xi) - f_1'(\xi))$$
 (5)

M can be found from Eq. 2.

 g_1 and its derivatives in Eq. 5 can be calculated from Eq. 3.

$$\begin{split} g_1'(ct+x-2l) &= -\frac{v_0}{c}e^{-\frac{M}{l}}(ct+x-2l) \\ g_1'(\xi)_{\{x=0\}} &= -\frac{v_0}{c}e^{-\frac{M}{l}}\xi \\ g_1''(ct+x-2l) &= \frac{Mv_0}{lc}e^{-\frac{M}{l}}(ct+x-2l) \\ g_1''(\xi)_{\{x=0\}} &= \frac{Mv_0}{lc}e^{-\frac{M}{l}}\xi \end{split}$$

One should note that the above derivatives are taking w.r.t x.

Replacing $g_1'(\xi)$ and $g_1''(\xi)$ from above set of equations and using the dsolve command from Maple, the solution to Eq. 5 is

$$f_1(\xi) = \frac{(2Mv_0\xi - Bcl + 2lv_0)}{Mc} e^{-\frac{M}{l}\xi} + D$$
 (6)

where B and D are constants and can be determined from initial conditions. In order to find B and D, we use the continuity principle of displacements and velocity where both the initial displacement and velocity in Eq. 4 should have the same value of u and v at ct=2l in Eq. 1, that is

For the displacement:

$$u_{1\{x=0,ct=2l\}} = u_{0\{x=0,ct=2l\}}$$

$$f_{1\{x=0,ct=2l\}} + g_{1\{x=0,ct=2l\}} = f_{0\{x=0,ct=2l\}}$$
(7)

For the velocity:

$$v_{1\{x=0,ct=2l\}} = v_{0\{x=0,ct=2l\}}$$

$$\frac{\partial}{\partial t} f_{1\{x=0,ct=2l\}} + \frac{\partial}{\partial t} g_{1\{x=0,ct=2l\}} = \frac{\partial}{\partial t} f_{0\{x=0,ct=2l\}}$$
(8)

Solving Eq. 7 and Eq. 8 simultaneously

$$B = \frac{v_0}{c}(e^{-2M} + 1)$$
 , $D = 0$

As a result

$$f_1(\xi) = \frac{v_0}{Mc} (2M\xi - le^{-2M} + l)e^{-\frac{M}{l}\xi}$$
(9)

5 Displacement and Strain Plots

The displacement for 2l < ct < 4l can be found by plugging-in Eq. 3 and Eq. 9 into Eq. 4.

$$u_{1}(x,t) = \frac{v_{0}}{Mc} \left\{ \left[2M\left(ct - 2l - x\right) - l\left(e^{-2M} + 1\right) + 2l\right] e^{-\frac{M}{l}\left(ct - 2l - x\right)} + l\left(e^{-\frac{M}{l}\left(ct - 2l + x\right)} - 1\right) \right\}$$

$$(10)$$

Figure. 2 shows the piecewise combination of Eq. 1 and Eq. 10 for 0 < ct < 4l for c = 1, l = 1, M = 1 at the free side of the elastic bar (x = 0). As expected, the displacement plot is continuous.

The strain can be calculated by taking the derivative of displacements from Eq. 1 and Eq. 10 w.r.t x.

$$\begin{cases} \epsilon_0 = \frac{v_0}{c} e^{-\frac{M}{l}ct} &, 0 < ct < 2l \\ \epsilon_1 = \frac{v_0}{c} \left\{ \left(\frac{2M(ct - 2l - x) - l(e^{-2M} + 1) + 2l}{l} - 2 \right) e^{-\frac{M}{l}(ct - 2l - x)} - e^{-\frac{M}{l}(ct - 2l + x)} \right\} &, 2l < ct < 4l \end{cases}$$

$$\tag{11}$$

Eq. 11 is plotted in Figure. 3. As it is seen, the discontinuity in the strain plot occurs at t=2l where the strain jumps to higher but negative value. It is also evident that for 0 < ct < 2l, the strain does not become zero as it appears in form of an exponential function (see Eq. 11₁), while the strain and subsequently the stress (due to linear elastic assumption between stress and strain) vanishes at around 3l. To find the corresponding time, we may solve Eq. 11₂ for t.

$$t = \frac{1}{2} \frac{4Ml + 2Mx + le^{-2M} + l + le^{-\frac{2M}{l}x}}{Mc}$$

If we remove x from above equation

$$t = \frac{1}{2} \frac{4Ml + l e^{-2M} + 2l}{Mc} \tag{12}$$

and for c = 1, l = 1, M = 1, the time at which stress vanishes is 3.068s.

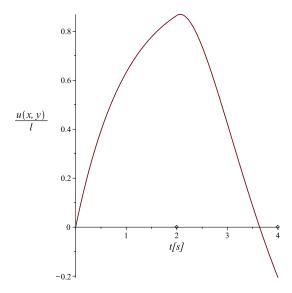


Figure 2: Normalized displacement against time for $c=1,\,l=1,\,M=1$ at the free side of the elastic bar (x=0).

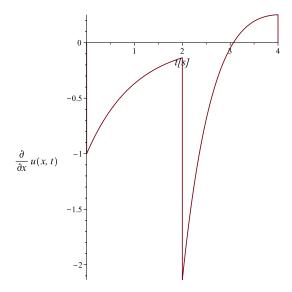


Figure 3: Strain against time for $c=1,\ l=1,\ M=1$ at the free side of the elastic bar (x=0).