

## Video 2.1a Vijay Kumar and Ani Hsieh



## **Introduction to Lagrangian Mechanics**

# Vijay Kumar and Ani Hsieh University of Pennsylvania



## **Analytical Mechanics**

- Aristotle
- Galileo
- Bernoulli

- Euler
- Lagrange
- D'Alembert

- 1. Principle of Virtual Work: Static equilibrium of a particle, system of N particles, rigid bodies, system of rigid bodies
- 2. D'Alembert's Principle: Incorporate inertial forces for dynamic analysis
  - 3. Lagrange's Equations of Motion



## **Generalized Coordinate(s)**

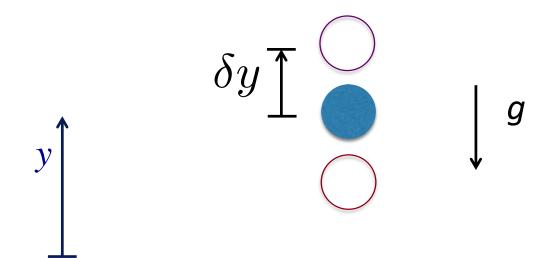
A minimal set of coordinates required to describe the configuration of a system

No. of generalized coordinates = no. of degrees of freedom



## **Virtual Displacements**

Virtual displacements are small displacements consistent with the constraints



A particle of mass *m* constrained to move vertically

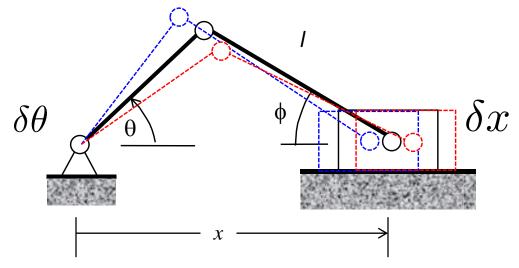
generalized

coordinate y



## **Virtual Displacements**

Virtual displacements are small displacements consistent with the constraints



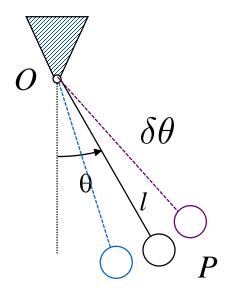
The slider crank mechanism: a single degree of freedom linkage





## **Virtual Displacements**

Virtual displacements are small displacements consistent with the constraints



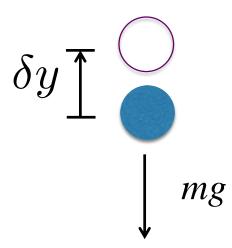
The pendulum: a single degree of freedom linkage



generalized coordinate  $\theta$ 

## **Virtual Work**

The work done by applied (external) forces through the virtual displacement,  $\delta W$ 



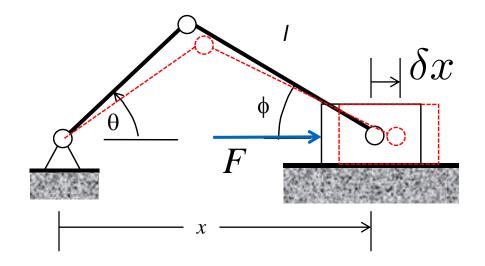
A particle of mass *m* constrained to move vertically



$$\delta W = -mg\delta y$$

## **Virtual Work**

The work done by applied (external) forces through the virtual displacement,  $\delta W$ 



The slider crank mechanism: a single degree of freedom linkage

$$\delta W = F \delta x$$



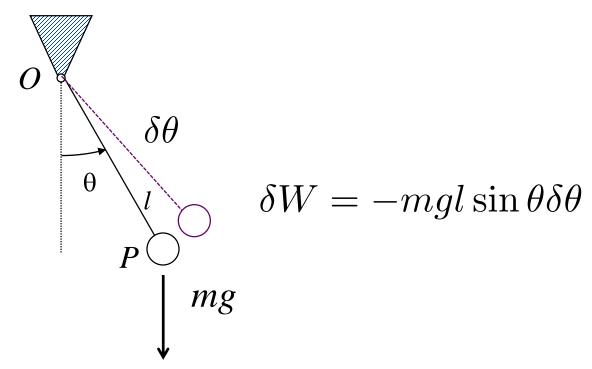


## Video 2.1b Vijay Kumar and Ani Hsieh



## **Virtual Work**

The work done by applied (external) forces through the virtual displacement,  $\delta W$ 



The pendulum: a single degree of freedom linkage



## The Principle of Virtual Work

The virtual work done by all applied (external) forces through any virtual displacement is zero

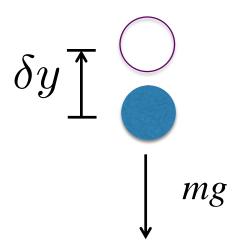


The system is in equilibrium



## **Static Equilibrium**

$$\delta W = 0$$

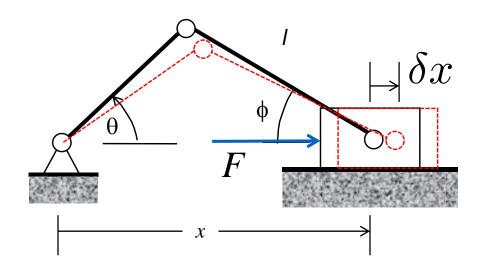


$$\delta W = -mg\delta y = 0$$



## **Static Equilibrium**

$$\delta W = 0$$

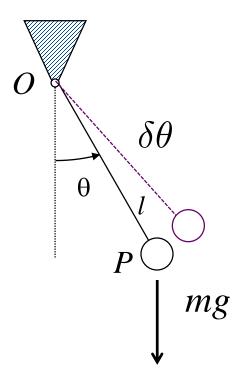


$$\delta W = F \delta x = 0$$



## **Static Equilibrium**

$$\delta W = -mgl\sin\theta\delta\theta = 0$$

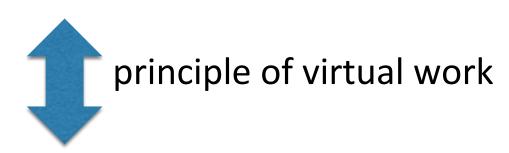




## D'Alembert's Principle

The virtual work done by all applied (external) forces through any virtual displacement is zero

include inertial forces



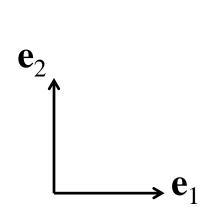
The system is in *static* equilibrium Equations of motion for the system inertial force = - mass x acceleration

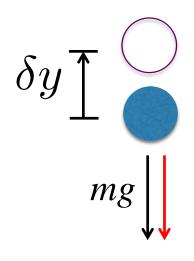


## D'Alembert's Principle

## acceleration

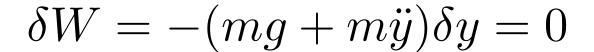
$$\mathbf{a} = \ddot{y}\mathbf{e}_2$$





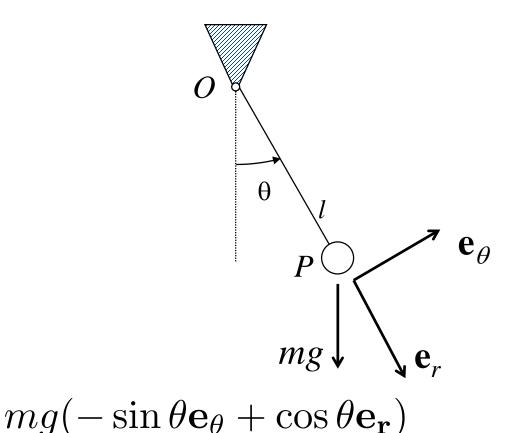
## inertial force

$$-m\ddot{y}\mathbf{e}_2$$





## D'Alembert's Principle



acceleration

$$\mathbf{a} = l(\ddot{\theta}\mathbf{e}_{\theta} - \dot{\theta}^2\mathbf{e}_r)$$

inertial force

$$-ml(\ddot{\theta}\mathbf{e}_{\theta} - \dot{\theta}^2\mathbf{e}_r)$$

equation of motion

$$\ddot{\theta} + \frac{g}{l}\sin\theta = 0$$



$$\delta W = (-ml^2\ddot{\theta} - mgl\sin\theta)\delta\theta = 0$$

# D'Alembert's principle with generalized coordinates

generalized coordinate  $\delta W = (Q + Q^*)\delta q = 0$ contribution contribution from from inertial external force(s) force(s)

Particle in the vertical plane

$$\delta W = -(mg + m\ddot{y})\delta y = 0$$

Simple pendulum

$$\delta W = (-ml^2\ddot{\theta} - mgl\sin\theta)\delta\theta = 0$$



## The Key Idea

The contribution from the inertial forces can be expressed as a function of the kinetic energy and its derivatives

$$Q^{\star} = -\left[\frac{d}{dt}\left(\frac{\partial \mathcal{K}}{\partial \dot{q}}\right) - \frac{\partial \mathcal{K}}{\partial q}\right]$$



## Lagrange's Equation of Motion

$$\left[ \frac{d}{dt} \left( \frac{\partial \mathcal{K}}{\partial \dot{q}} \right) - \frac{\partial \mathcal{K}}{\partial q} \right] = Q$$

# Particle in the vertical plane

$$\mathcal{K} = \frac{1}{2}m\dot{y}^2 \quad Q^* = -m\ddot{y} \quad Q = -mg$$

# Simple pendulum



$$Q^{\star} = -ml^2 \ddot{\theta}$$

# Lagrange's Equation of Motion for a **Conservative System**

## Conservative System

There exists a scalar function such that all applied forces are given by the gradient of the potential function

Gravitational force is conservative Scalar function is the potential energy

# Standard Form of Lagrange's Equation of Motion

$$\left[\frac{d}{dt}\left(\frac{\partial \mathcal{K}}{\partial \dot{q}}\right) - \frac{\partial \mathcal{K}}{\partial q}\right] = Q \qquad Q = -\frac{d}{dq}\mathcal{P}$$

# The Lagrangian

$$\mathcal{L} = \mathcal{K} - \mathcal{P}$$

$$\left[ \frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial \dot{q}} \right) - \frac{\partial \mathcal{L}}{\partial q} \right] = 0$$



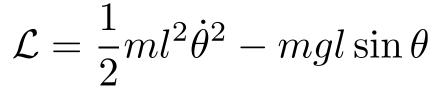
## Lagrange's Equation of Motion

$$\left[ \frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial \dot{q}} \right) - \frac{\partial \mathcal{L}}{\partial q} \right] = 0$$

# Particle in the vertical plane

$$\mathcal{L} = \frac{1}{2}m\dot{y}^2 - mgy$$

# Simple pendulum







# Video 2.2 Vijay Kumar and Ani Hsieh



## **Newton Euler Equations**

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## **Analytical Mechanics**

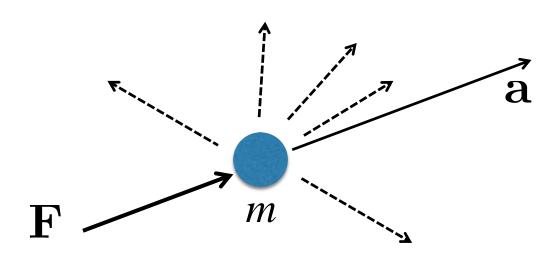
- Principle of Virtual Work: Static equilibrium of a particle, system of N particles, rigid bodies, system of rigid bodies
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$$\left[ \frac{d}{dt} \left( \frac{\partial \mathcal{K}}{\partial \dot{q}} \right) - \frac{\partial \mathcal{K}}{\partial q} \right] = Q$$



## **Newton Euler Equations**

## Recall Newton's 2<sup>nd</sup> law of motion



$$\mathbf{F} = m\mathbf{a}$$

net external force = inertia x acceleration

## **Newton Euler Equations**

Newton's equations of motion for a translating rigid body

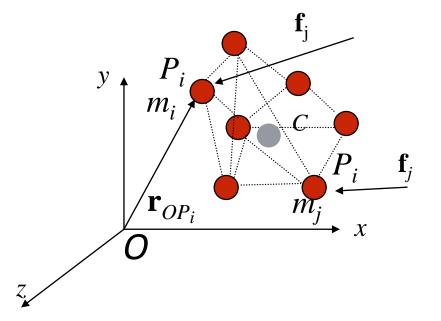
Euler's equations of motion for a rotating rigid body



## **Motion of Systems of Particles**

#### Center of Mass

$$\mathbf{r}_C = \frac{1}{m} \sum_{i=1}^k m_i \mathbf{r}_{OP_i}$$



Newton's equations of motion

$$\mathbf{F} = \sum_{i=1}^{k} \mathbf{f}_i = \mathbf{m} \mathbf{a}_C$$



net external force = total mass x

acceleration, of center of mass

## **Newton's Second Law for a System of Particles**

The center of mass for a system of particles, S, accelerates in an inertial frame, A, as if it were a single particle with mass m (equal to the total mass of the system) acted upon by a force equal to the net external force.

$$\mathbf{F} = m \frac{d\mathbf{v}_C}{dt}$$

Linear momentum

$$\mathbf{L} = m\mathbf{v}_C$$

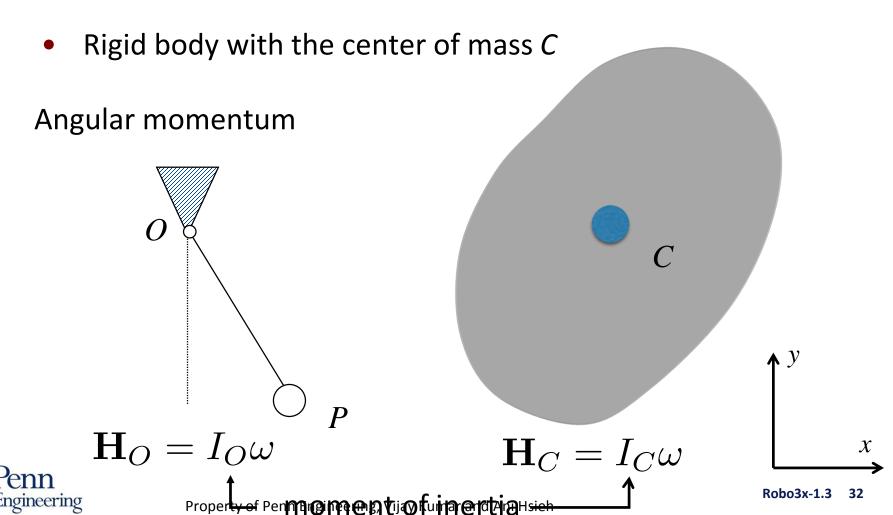
$$\mathbf{F} = rac{d\mathbf{L}}{dt}$$

Rate of change of linear momentum in an inertial frame is equal to the net external force acting on the system.



## **Equations of Motion for a Rotating Rigid Body**

Rigid body with a point O fixed in an inertial frame



## **Equations of Motion for a Rotating Rigid Body**

- Rigid body with a point O fixed in an inertial frame
- Rigid body with the center of mass C

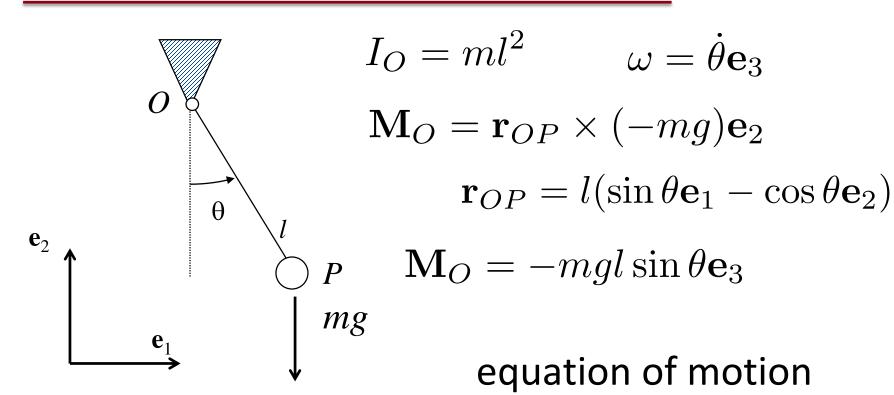
The rate of change of angular momentum of a rigid body (or a system of rigidly connected particles) in an inertial frame with O or C as an origin is equal to the net external moment acting (with the same origin) on the body.

$$\frac{d\mathbf{H}_O}{dt} = \frac{d(I_O\omega)}{dt} = \mathbf{M}_O$$

$$\frac{d\mathbf{H}_C}{dt} = \frac{d(I_C\omega)}{dt} = \mathbf{M}_C$$



## **Example**

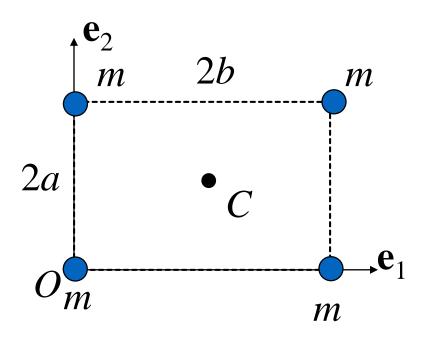


$$\frac{d\mathbf{H}_O}{dt} = \frac{d(I_O\omega)}{dt} = \mathbf{M}_O$$

$$\ddot{\theta} + \frac{g}{l}\sin\theta = 0$$



## **Moment of Inertia of Planar Objects**



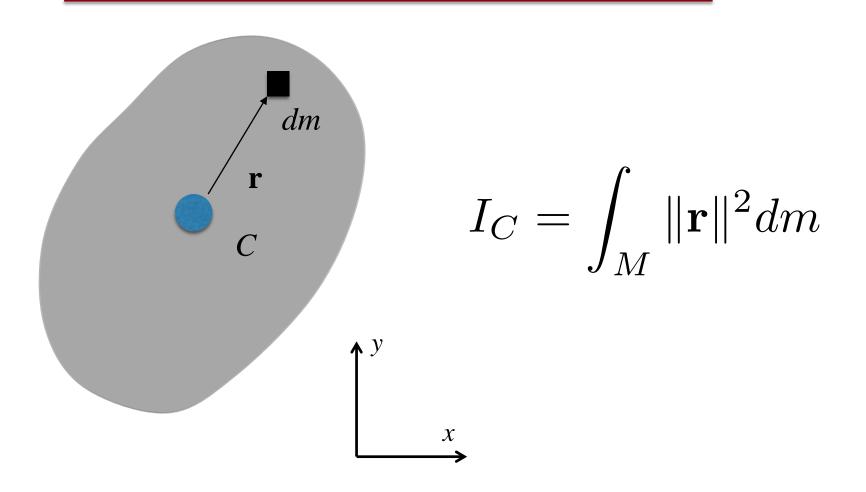
$$I_O = \sum_i m_i ||\mathbf{r}_{OP_i}||^2$$
$$8m(a^2 + b^2)$$

$$I_C = \sum_i m_i \|\mathbf{r}_{PC_i}\|^2$$

$$4m(a^2+b^2)$$



## **Moment of Inertia of Planar Objects**







#### Video 2.3 Vijay Kumar and Ani Hsieh



#### **Dynamics and Control**

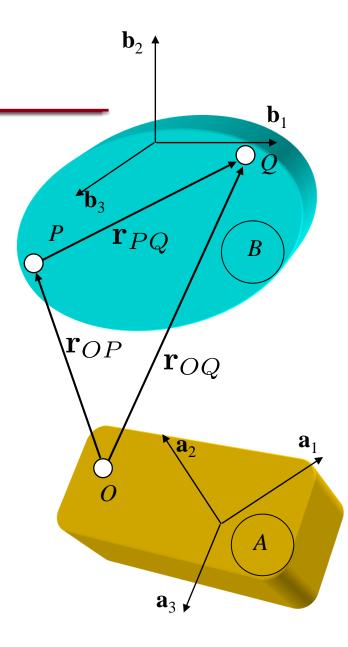
Acceleration Analysis: Revisited

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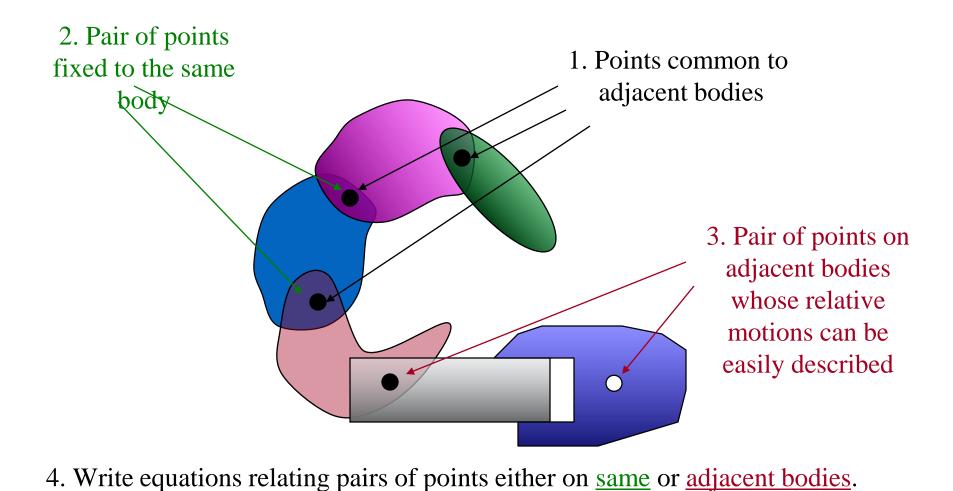
#### **Position Vectors**

- Reference frame A
  - Origin ()
  - Basis vectors  $\{\mathbf{a}_1, \mathbf{a}_2, \mathbf{a}_3\}$
- Position Vectors
  - Position vectors for P and Q in A  $\mathbf{r}_{OP}$   $\mathbf{r}_{OQ}$
  - Position vector of Q in B  $\mathbf{r}_{PQ}$





#### General Approach to Analyzing Multi-Body System

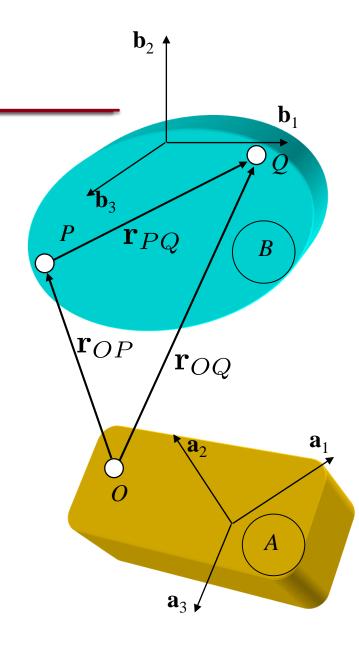


#### **Position Analysis**

$$\mathbf{r}_{OQ} = \mathbf{r}_{OP} + \mathbf{r}_{PQ}$$

$$q_1 \mathbf{a}_1 + q_2 \mathbf{a}_2 + q_3 \mathbf{a}_3$$
  
=  $p_1 \mathbf{a}_1 + p_2 \mathbf{a}_2 + p_3 \mathbf{a}_3$   
+  $q'_1 \mathbf{b}_1 + q'_2 \mathbf{b}_2 + q'_3 \mathbf{b}_3$ 

$$\begin{bmatrix} q_1 \\ q_2 \\ q_3 \end{bmatrix} = \begin{bmatrix} p_1 \\ p_2 \\ p_3 \end{bmatrix} + \mathbf{R}_{AB} \begin{bmatrix} q_1' \\ q_2' \\ q_3' \end{bmatrix}$$





#### **Velocity Analysis**

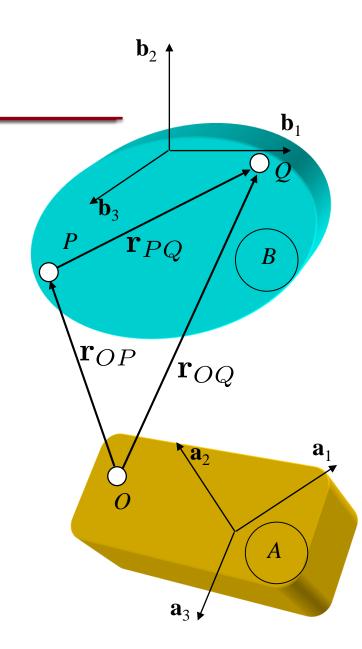
$$\mathbf{r}_{OQ} = \mathbf{r}_{OP} + \mathbf{r}_{PQ}$$

$$egin{bmatrix} \dot{q}_1 \ \dot{q}_2 \ \dot{q}_3 \end{bmatrix} = egin{bmatrix} \dot{p}_1 \ \dot{p}_2 \ \dot{p}_3 \end{bmatrix} + \mathbf{\dot{R}}_{AB} \mathbf{R}_{AB}^T egin{bmatrix} q_1 - p_1 \ q_2 - p_2 \ q_3 - p_3 \end{bmatrix}$$

3x3 skew symmetric

$$\hat{\omega}_{AB} \begin{bmatrix} q_1 - p_1 \\ q_2 - p_2 \\ q_3 - p_3 \end{bmatrix} = \omega_{AB} \times \mathbf{r}_{PQ}$$

$$\mathbf{v}_Q = \mathbf{v}_P + \omega_{AB} \times \mathbf{r}_{PQ}$$





#### **Acceleration Analysis**

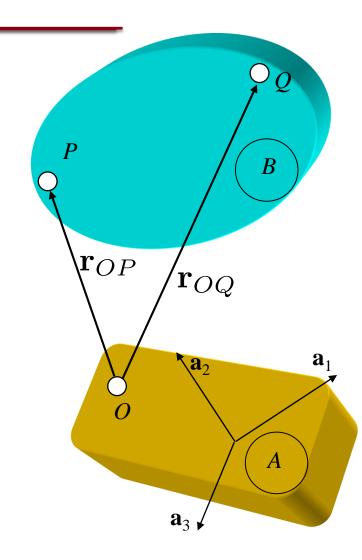
Acceleration of P and Q in A

$$\mathbf{a}_P = \ddot{p}_1 \mathbf{a}_1 + \ddot{p}_2 \mathbf{a}_2 + \ddot{p}_3 \mathbf{a}_3$$

$$\begin{bmatrix} \ddot{p}_1 \\ \ddot{p}_2 \\ \ddot{p}_3 \end{bmatrix}$$

$$\mathbf{a}_Q = \ddot{q}_1 \mathbf{a}_1 + \ddot{q}_2 \mathbf{a}_2 + \ddot{q}_3 \mathbf{a}_3$$

$$\begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \\ \ddot{q}_3 \end{bmatrix}$$





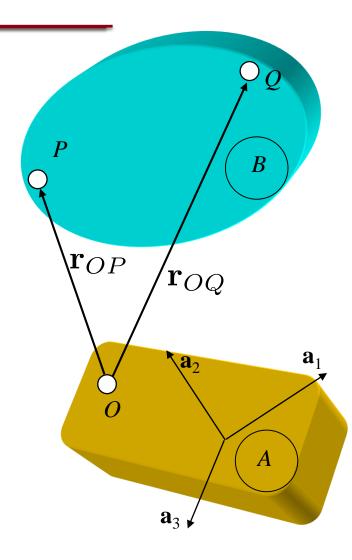
#### **Angular Acceleration**

The angular acceleration of B in A, is defined as the derivative of the angular velocity of *B* in *A*:

$$\alpha_{AB} = \frac{d\omega_{AB}}{dt}$$

$$\hat{\omega}_{AB} = \dot{\mathbf{R}}_{AB} \mathbf{R}_{AB}^T$$

$$\hat{\alpha}_{AB} = \ddot{\mathbf{R}}_{AB} \mathbf{R}_{AB}^T + \dot{\mathbf{R}}_{AB} \dot{\mathbf{R}}_{AB}^T$$



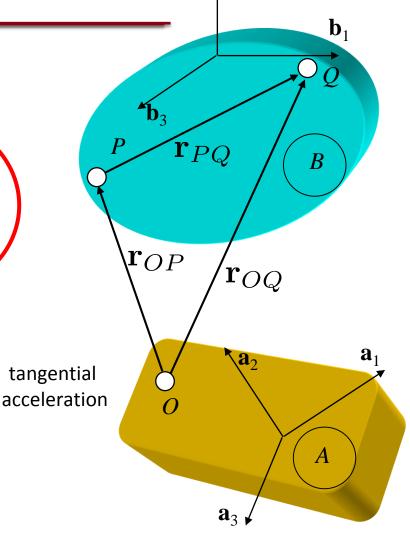


#### **Acceleration Analysis**

$$\mathbf{v}_Q = \mathbf{v}_P + \omega_{AB} \times \mathbf{r}_{PQ}$$

$$\mathbf{a}_Q = \mathbf{a}_P + \dot{\omega}_{AB} \times \mathbf{r}_{PQ} + \omega_{AB} \times \dot{\mathbf{r}}_{PQ}$$

$$\mathbf{a}_{Q} = \mathbf{a}_{P} + \dot{\omega}_{AB} \times \mathbf{r}_{PQ}$$
 $+ \omega_{AB} \times (\omega_{AB} \times \mathbf{r}_{PQ})$ 



 $\mathbf{b}_2$ 

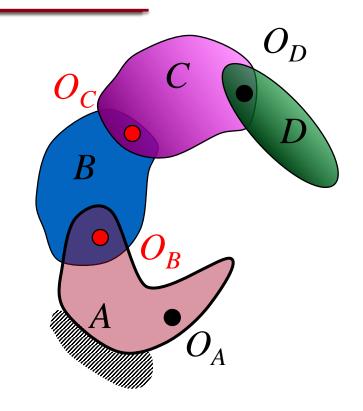


#### **Serial Chain of Rigid Bodies**

$$\mathbf{r}_{O_AO_C} = \mathbf{r}_{O_AO_B} + \mathbf{r}_{O_BO_C}$$

$$\mathbf{v}_{O_C} = \mathbf{v}_{O_B} + \omega_{AB} \times \mathbf{r}_{O_B O_C}$$

$$\mathbf{a}_{O_C} = \mathbf{a}_{O_B} + \dot{\omega}_{AB} \times \mathbf{r}_{O_B O_C} + \omega_{AB} \times (\omega_{AB} \times \mathbf{r}_{O_B O_C})$$

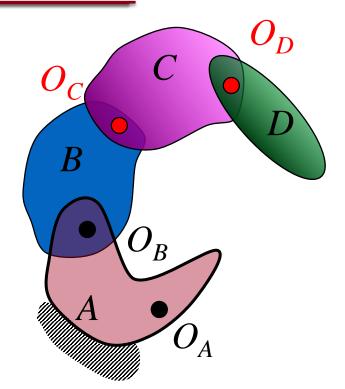


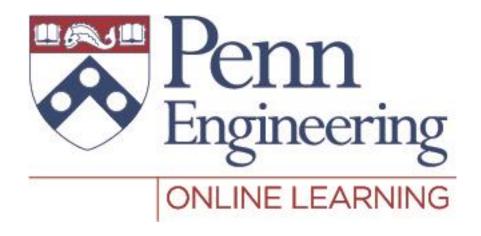
#### **Serial Chain of Rigid Bodies**

$$\mathbf{r}_{O_A O_D} = \mathbf{r}_{O_A O_C} + \mathbf{r}_{O_C O_D}$$

$$\mathbf{v}_{O_D} = \mathbf{v}_{O_C} + \omega_{AC} \times \mathbf{r}_{O_C O_D}$$

$$\mathbf{a}_{O_D} = \mathbf{a}_{O_C} + \dot{\omega}_{AC} \times \mathbf{r}_{O_C O_D} + \omega_{AC} \times (\omega_{AC} \times \mathbf{r}_{O_C O_D})$$





#### Video 2.4 Vijay Kumar and Ani Hsieh



#### **Newton Euler Equations (continued)**

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#### **Newton Euler Equations**

#### Newton's equations of motion

A rigid body B accelerates in an inertial frame A as if it were a single particle with the same mass m (equal to the total mass of the system) acted upon by a force equal to the net external force.

$$\mathbf{F} = m \frac{d\mathbf{v}_C}{dt}$$

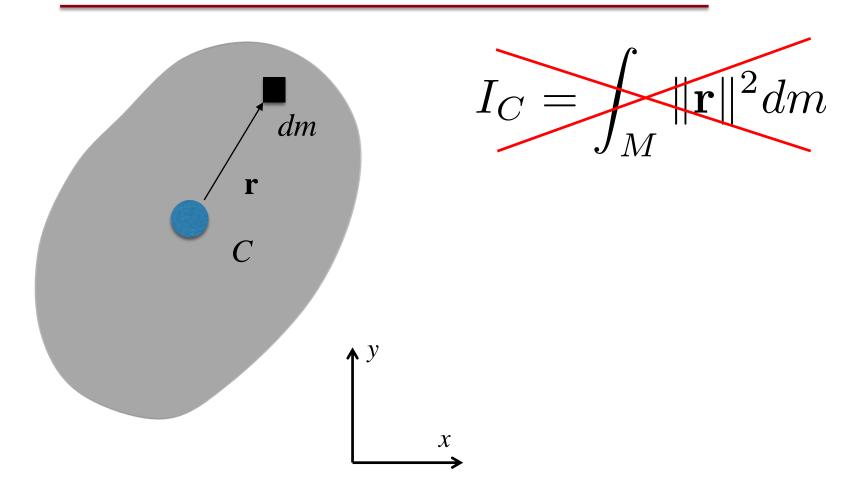
#### Euler's equations of motion

The rate of change of angular momentum of the rigid body B with the center of mass C as the origin in A is equal to the resultant moment of all external forces acting on the body with C as the origin



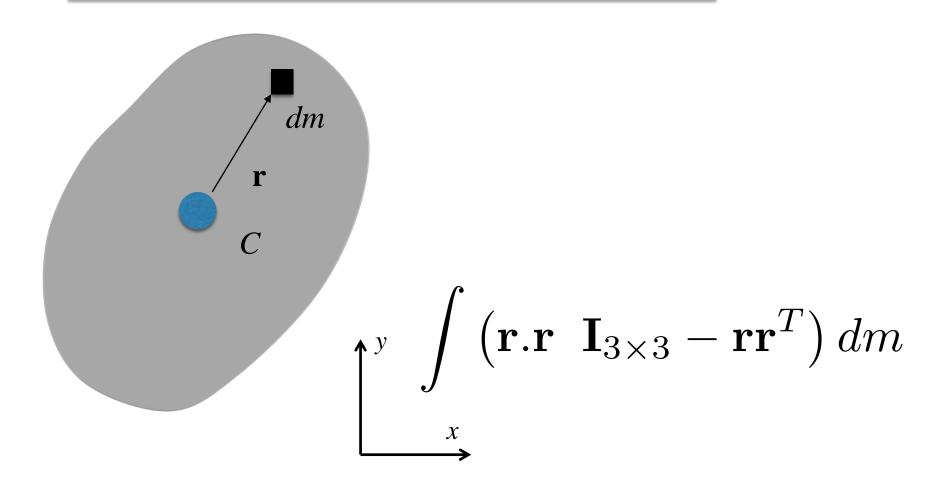
$$\mathbf{M}_C = rac{\mathbf{I}_C \omega}{dt}$$
Property of Penn Engineering, Vijay Kumar and Ani Hsieh

#### Moment of Inertia of 3-D Objects?



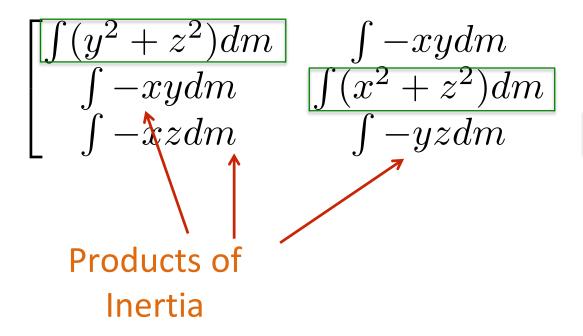


#### **Inertia Tensor of 3-D Objects**





#### **Inertia Dyadic**

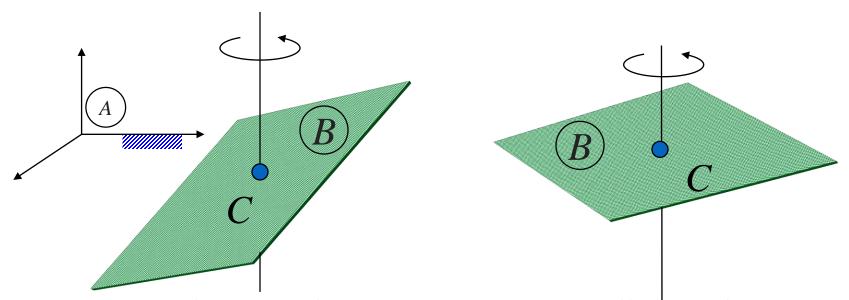


**Principal** Moments of Inertia



# **Example: Rectangular Plate Rotating about Axis through Center of Mass**

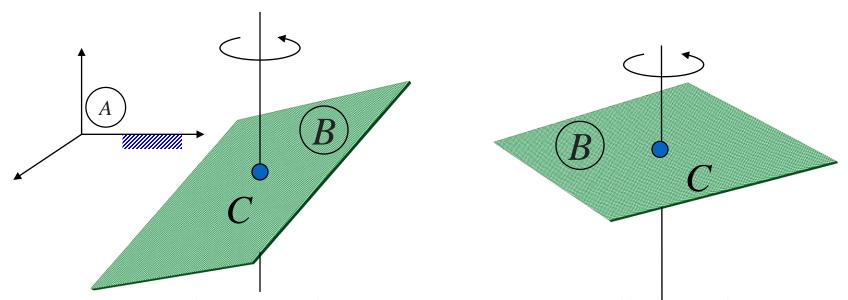
$$\begin{bmatrix} \int (y^2 + z^2) dm & \int -xy dm & \int -xz dm \\ \int -xy dm & \int (x^2 + z^2) dm & \int -yz dm \\ \int -xz dm & \int -yz dm & \int (x^2 + y^2) dm \end{bmatrix}$$



Is the angular momentum parallel to the

## **Example: Rectangular Plate Rotating about Axis through Center of Mass**

$$\begin{bmatrix} I_{xx} & \times & \times \\ \times & I_{yy} & \times \\ \times & \times & I_{zz} \end{bmatrix} \qquad \begin{bmatrix} I_{xx} & 0 & 0 \\ 0 & I_{yy} & 0 \\ 0 & 0 & I_{zz} \end{bmatrix}$$



Is the angular momentum parallel to the

#### **Principal Axes and Principal Moments**

#### Principal axis

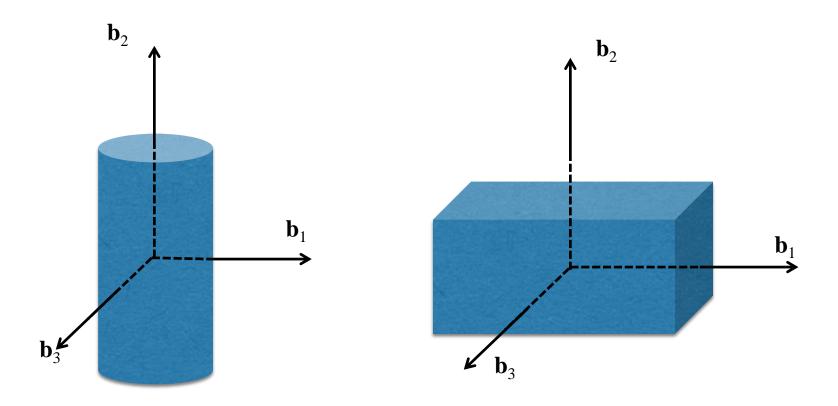
- u is a unit vector along a principal axis if I u is parallel to
   u
- There are 3 independent principal axes!

#### Principal moment of inertia

The moment of inertia with respect to a principal axis, u<sup>T</sup>
 I u, is called a principal moment of inertia.



#### **Examples**



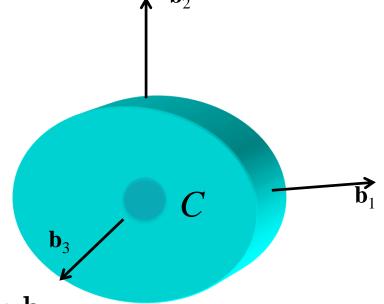


$$\mathbf{H}_C = \mathbf{I}_C \omega_{AB}$$

#### In frame B

$$\omega_{AB} = \omega_1 \mathbf{b}_1 + \omega_2 \mathbf{b}_2 + \omega_3 \mathbf{b}_3$$

$$\begin{bmatrix} I_{11} & 0 & 0 \\ 0 & I_{22} & 0 \\ 0 & 0 & I_{33} \end{bmatrix}$$



$$\mathbf{H}_C = I_{11}\omega_1\mathbf{b}_1 + I_{22}\omega_2\mathbf{b}_2 + I_{33}\omega_3\mathbf{b}_3$$

$$\mathbf{H}_C = egin{bmatrix} I_{11}\omega_1 \ I_{22}\omega_2 \ I_{33}\omega_3 \end{bmatrix}$$

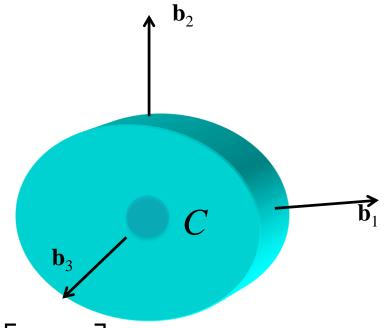


 $\mathbf{H}_C = \mathbf{I}_C \omega_{AB}$ 

need to differentiate in A

In frame A

$$\mathbf{H}_C = \mathbf{R}_{AB} egin{bmatrix} I_{11}\omega_1 \ I_{22}\omega_2 \ I_{33}\omega_3 \end{bmatrix}$$



$$\dot{\mathbf{H}}_C = \mathbf{R}_{AB} egin{bmatrix} I_{11}\dot{\omega}_1 \ I_{22}\dot{\omega}_2 \ I_{33}\dot{\omega}_3 \end{bmatrix} + \dot{\mathbf{R}}_{AB} egin{bmatrix} I_{11}\omega_1 \ I_{22}\omega_2 \ I_{33}\omega_3 \end{bmatrix}$$



Transform back to frame B

$$\begin{split} \dot{\mathbf{H}}_{C} = & \mathbf{R}_{AB} \begin{bmatrix} I_{11}\dot{\omega}_{1} \\ I_{22}\dot{\omega}_{2} \\ I_{33}\dot{\omega}_{3} \end{bmatrix} + \dot{\mathbf{R}}_{AB} \begin{bmatrix} I_{11}\omega_{1} \\ I_{22}\omega_{2} \\ I_{33}\omega_{3} \end{bmatrix} \\ \hat{\omega}_{AB} = & \mathbf{R}_{AB}^{T}\mathbf{R}_{AB} \\ \text{angular velocity in frame } \mathbf{B} \end{split}$$

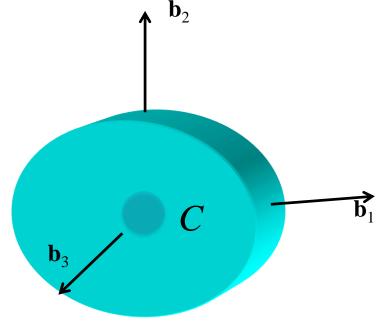
$$\dot{\mathbf{H}}_{C} = \begin{bmatrix} I_{11}\dot{\omega}_{1} \\ I_{22}\dot{\omega}_{2} \\ I_{33}\dot{\omega}_{3} \end{bmatrix} + \begin{bmatrix} 0 & -\omega_{3} & \omega_{2} \\ \omega_{3} & 0 & -\omega_{1} \\ -\omega_{2} & \omega_{1} & 0 \end{bmatrix} \begin{bmatrix} I_{11}\omega_{1} \\ I_{22}\omega_{2} \\ I_{33}\omega_{3} \end{bmatrix}$$



1. frame  $B(\mathbf{b}_i)$  along principal axes

2. center of mass as origin

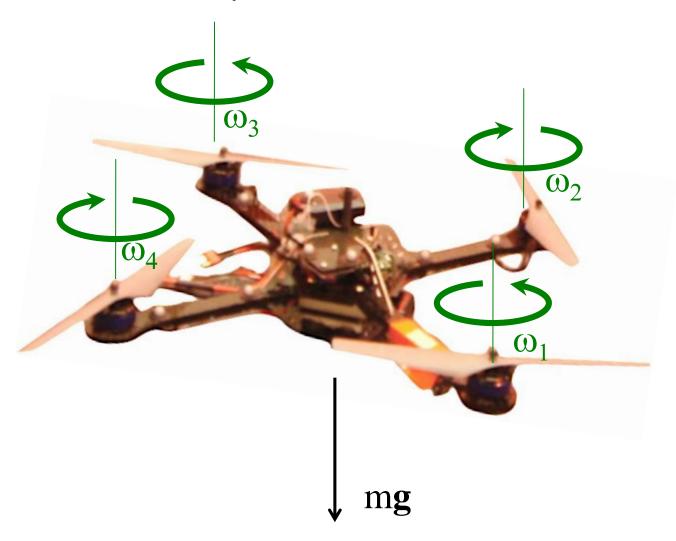
3. all components along  $\mathbf{b}_i$ 



$$\begin{bmatrix} I_{11}\dot{\omega}_1\\I_{22}\dot{\omega}_2\\I_{33}\dot{\omega}_3 \end{bmatrix} + \begin{bmatrix} 0 & -\omega_3 & \omega_2\\\omega_3 & 0 & -\omega_1\\-\omega_2 & \omega_1 & 0 \end{bmatrix} \begin{bmatrix} I_{11}\omega_1\\I_{22}\omega_2\\I_{33}\omega_3 \end{bmatrix} = \mathbf{M}_C$$

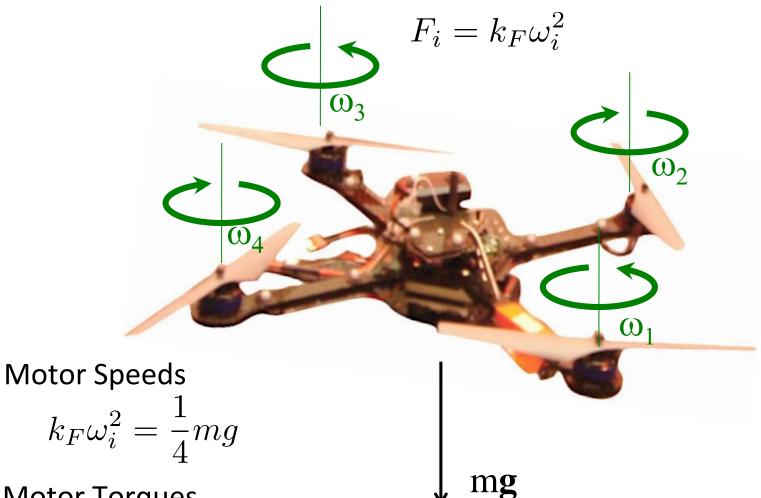


## Quadrotor



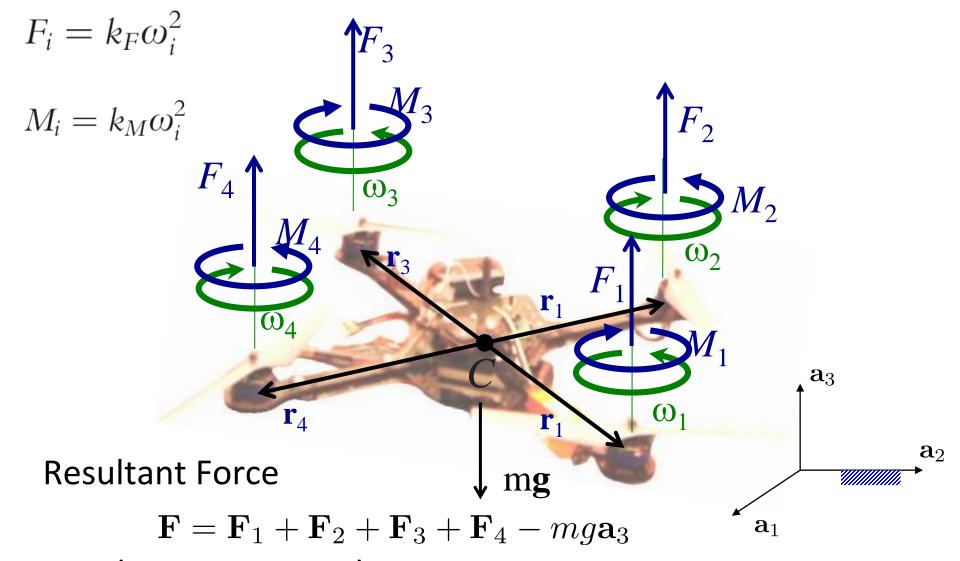


## Static Equilibrium (Hover)



**Motor Torques** 

$$au_i = k_M \omega_i^2$$



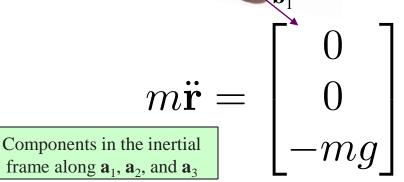
Resultant Moment about C

 $\mathbf{M} = \mathbf{r}_1 \times \mathbf{F}_1 + \mathbf{r}_2 \times \mathbf{F}_2 + \mathbf{r}_3 \times \mathbf{F}_3 + \mathbf{r}_4 \times \mathbf{F}_4$ 



# Newton-Euler Equations

$$\omega_{AB} = p\mathbf{b}_1 + q\mathbf{b}_2 + r\mathbf{b}_3$$



Rotation of thrust vector from 
$$B$$
 to  $A$   $R_{AB}$   $R_{A$ 

$$I\begin{bmatrix} \dot{p} \\ \dot{q} \\ \dot{r} \end{bmatrix} = \begin{bmatrix} L(F_2 - F_4) \\ L(F_3 - F_1) \\ M_1 - M_2 + M_3 - M_4 \end{bmatrix} - \begin{bmatrix} p \\ q \\ r \end{bmatrix} \times I\begin{bmatrix} p \\ q \\ r \end{bmatrix}$$



Components in the body frame along  $\mathbf{b}_1$ ,  $\mathbf{b}_2$ , and  $\mathbf{b}_3$ , the principal axes