# Rocky Project

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March 2024

## 1 Parameter Identification

### 1.1 Motor Constants

Per the project instructions, the motor has a transfer function (from the controlled input velocity to the actual output) of

$$M(s) = \frac{\frac{K}{\tau}}{s + \frac{1}{\tau}} \tag{1}$$

with $K$ and $\tau$ being constants unique to each motor, and identifying those constants is critical for a well performing Rocky. To estimate those parameters, we held our Rocky upright and ran the motors for three seconds along the carpeted floor of MAC 128 while recording the measured motor speed using the motor test calibration sketch found in the appendix.

With the data in hand, we needed to now convert the motor transfer function into an equation for velocity in the time domain, since this the domain our measured data exists in. The procedure for that is below.

$$M(s) = \frac{V(s)}{V_c(s)} = \frac{\frac{K}{\tau}}{s + \frac{1}{\tau}} \tag{2}$$

$$V_c(s) = \frac{300}{s}$$

$$V(s) = \frac{300\frac{K}{\tau}}{s(s + \frac{1}{\tau})}$$

Now we take the inverse Laplace transform using tables:

$$v(t) = 300k(1 - e^{\frac{-t}{\tau}})$$

To obtain estimates for our two motor parameters, we used MATLAB's curve-fitting toolbox to fit this curve onto our measured motor data (shown in Figure 1) and got $K = 0.0031$ and $\tau = 0.1044$

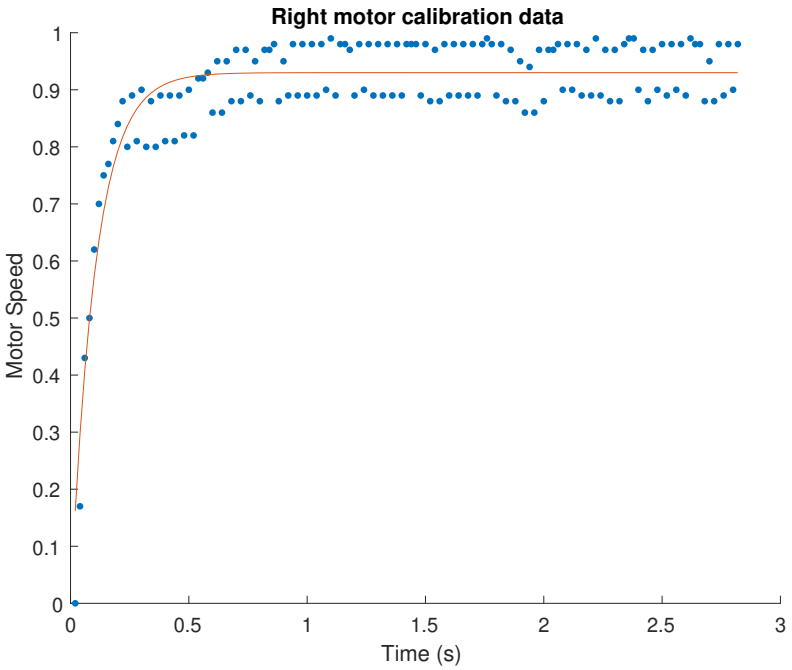


Figure 1: Right Motor Speed

## 1.2 Natural Frequency & Pendulum Length

In order to find our Rocky's natural frequency and the effective length of the pendulum body, we needed to calibrate its gyroscope. To do so, we started with the Rocky laying down horizontally on the table, and then picking it up and holding it vertically in the air as if it were balancing. This was done while running the gyro calibration sketch found in the appendix to track angle measurement offset.

After accounting for the angle correction needed, we could collect more gyro data to measure natural frequency. We compiled and loaded the gyro calibration sketch again with the Rocky (wheels off) laying flat. After loading, we opened the serial monitor and held the Rocky by two points at the top, allowing it to swing freely for a few seconds to collect angle measurement data. This data output was then copied into MATLAB and plotted to find the period (found experimentally by inspecting the data), which we plugged into the following equation to find natural frequency:

$$\omega_n = \frac{2\pi}{\text{period}} \ [rad/s] \tag{3}$$

$$\omega_n = \frac{2\pi}{1.3} = 4.8332 \ [rad/s]$$

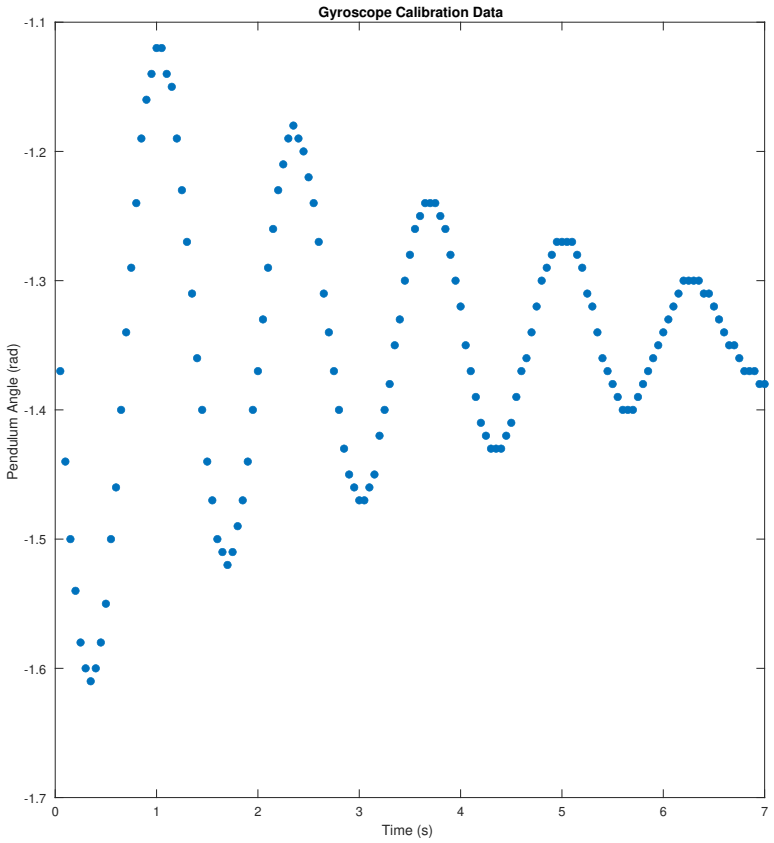


Figure 2: Gyroscope Calibration Data

Now that we have natural frequency, we can solve backwards for pendulum length using the provided approximation.

$$\omega_n = \sqrt{g/l_{\text{eff}}} \tag{4}$$

This gives us an effective length $l_{\text{eff}} = 0.4195$.

# 2 Initial (3 pole) System

## 2.1 Pole Values

For our Initial System, the poles we chose were $-1 \pm 2\pi i$ and $-10$. The imaginary poles were selected due to their rapidly decaying nature without the presence

of large initial oscillations. The real pole was selected to negative be negative to influence the system to have a decaying response to return to steady state. After having a general idea of what our poles should look like we determined the ones we used through a few iterations of trial and error. We found that the larger the negative value of the real pole, the Rocky would return back to steady state quicker. This was juxtaposed with the limitations of the physical Rocky system that were only able to respond to input so fast.

## 2.2 Calculating Control Constants

From our selected poles we were able to derive our control constants: $K_p$ and $K_i$. We did this by expanding our poles into a third order polynomial, find the target coefficients of the polynomial, reorder the coefficients to match the denominator polynomial, which is found from the closed loop transfer function:

$$H_{\text{Cloop}} = \frac{1}{1 - (\Theta)MK} \tag{5}$$

Where $\Theta$ represents the transfer function from velocity to angle of a pendulum $\frac{\frac{-s}{l}}{s^2 - g/l}$, $M$ represents the transfer function of a 1st order model of the motor $\frac{a*b}{s+a}$, and $K = K_p + \frac{K_i}{s}$ represents a transfer function of the PI angle controller. Lastly, the system of equations that set the coefficients of the target polynomial into actual polynomials is solved, outputting $K_p$ and $K_i$ as shown below. We found that the this model failed to correct itself effectively. Despite the angle returning to zero radians, this outcome resulted in our Rocky continuously moving forward or backwards faster and faster, as well as driving away from its original location. This seemed to be due to it not make the necessary over correction, just barely making it back to zero before falling in the same direction it corrected itself from. This phenomenon is also visible in our Simulink plots, shown below.

| Parameter | Value |
|---|---|
| $K_p$ | 1185 |
| $K_i$ | 8883 |

## 2.3 Simulink model

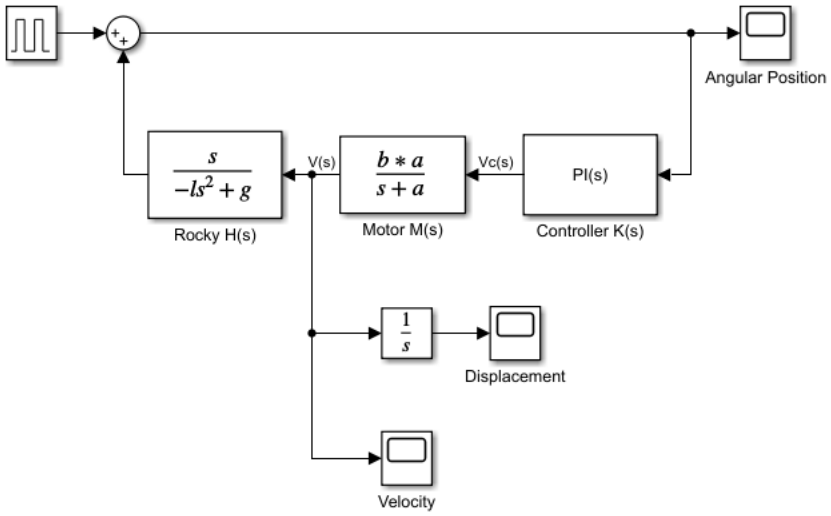


Figure 3: Block Diagram for 3 Pole System

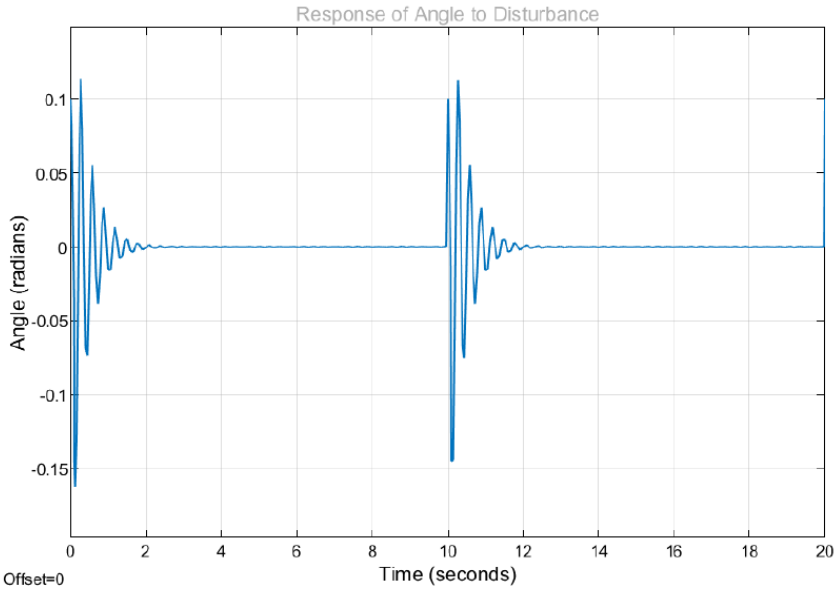


Figure 4: Angle Impulse Responses for 3 Pole System

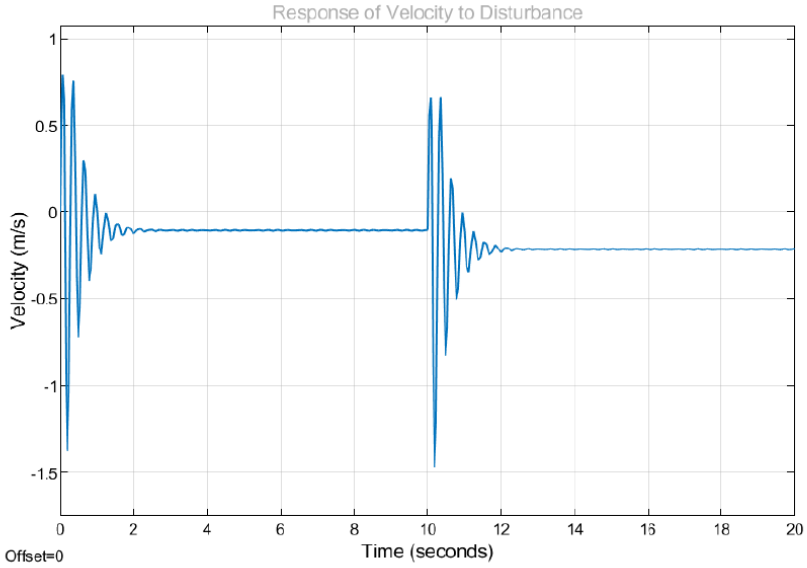


Figure 5: Velocity Impulse Responses for 3 Pole System

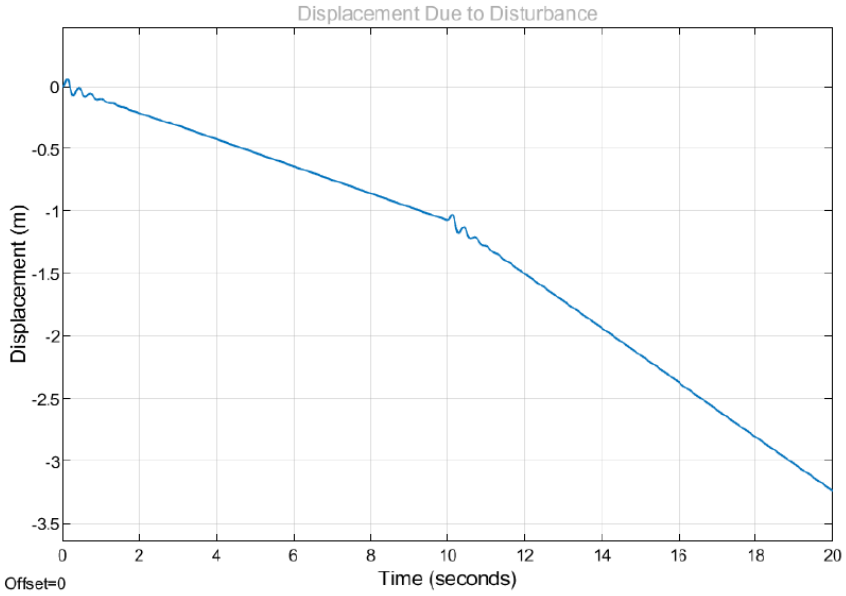


Figure 6: Displacement Impulse Responses for 3 Pole System

# 3 Balancing System

## 3.1 Pole Values

For our Revised System, the poles we chose were $-3.38 \pm 3.45i$, $-10$, $-4.8332$, and $-4.8332$. The imaginary poles were selected due to their rapidly decaying nature without the presence of large initial oscillations. The real poles were selected to be negative to influence the system to have a decaying response to return to steady state. We combined trial and error with a bit of rough hand calculations to determine our poles this. time we calculated our first and second (imaginary poles) and our fourth and fifth (real poles) with dampening values.

Those calculations were just choosing a damping ratio that seemed appropriate for both the angular position control loop and the motor velocity control loop (both of them being very slightly underdamped) and applying the following formula from Day 7 to find the corresponsing poles assuming this was a 2 pole system.

$$p_{1,2} = -\zeta\omega_n \pm i\omega_n\sqrt{1-\zeta^2}$$

After that, we just performed a bit of trial-and-error tuning in order to find exact values that worked well for us.

### 3.2 Calculating Control Constants

From our selected poles we were able to derive our control constants: $K_p$, $K_i$, $J_p$, $J_i$, and $C_i$. We did this by expanding our poles into a fifth order polynomial, finding the target coefficients of the polynomial, reordering the coefficients to match the denominator polynomial, which is found from the closed loop transfer function:

$$H_{\text{Cloop}} = \frac{1}{1 - (\Theta)M_{fb}K} \tag{6}$$

Where $\Theta$ represents the transfer function from velocity to angle of a pendulum $\frac{\frac{-s}{l}}{s^2 - g/l}$, $M_{fb}$ represents Black's formula of a 1st order model of the motor with a PI feedback controller (in order to ensure the Rocky balances in place) $\frac{a*b}{s+a+J(a+b)}$ and $J = J_p + \frac{J_i}{s} + \frac{C_i}{s^2}$, and $K = K_p + \frac{K_i}{s}$ represents a transfer function of the PI angle controller. Lastly, the system of equations that set the coefficients of the target polynomial into actual polynomials is solved, outputting our control parameters as given in the table below. We found this system was far more effective at balancing the Rocky, as it was able to maneuver back and forth in order to keep the Rocky balancing in one spot.

| Parameter | Value |
|---|---|
| $K_p$ | 33819 |
| $K_i$ | 172920 |
| $J_p$ | 2169 |
| $J_i$ | -27530 |
| $C_i$ | -43550 |

### 3.3 Simulink model

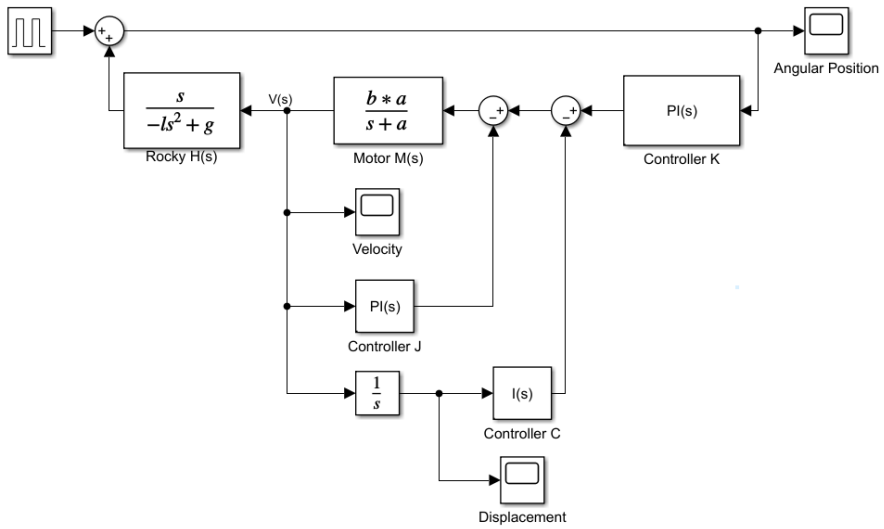


Figure 7: Block Diagram for 5 Pole System

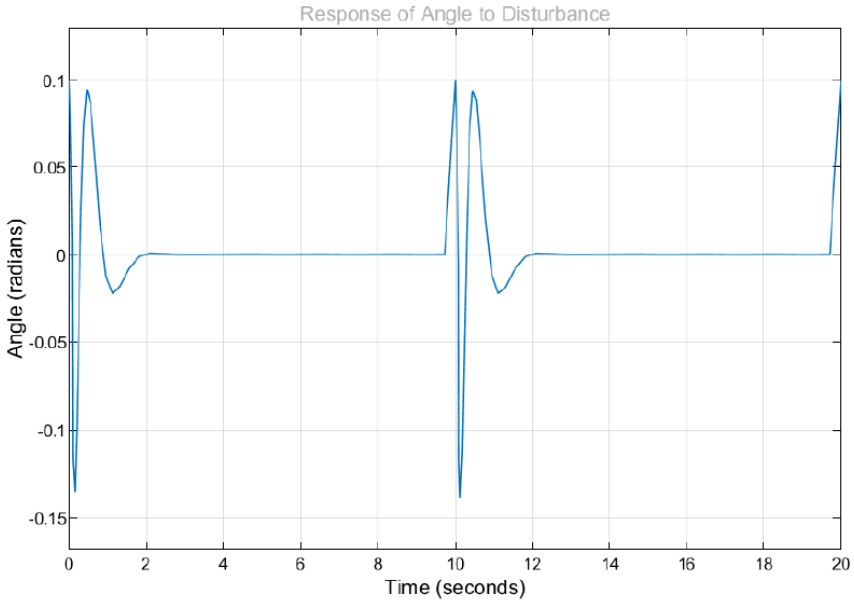


Figure 8: Angle Impulse Responses for 5 Pole System

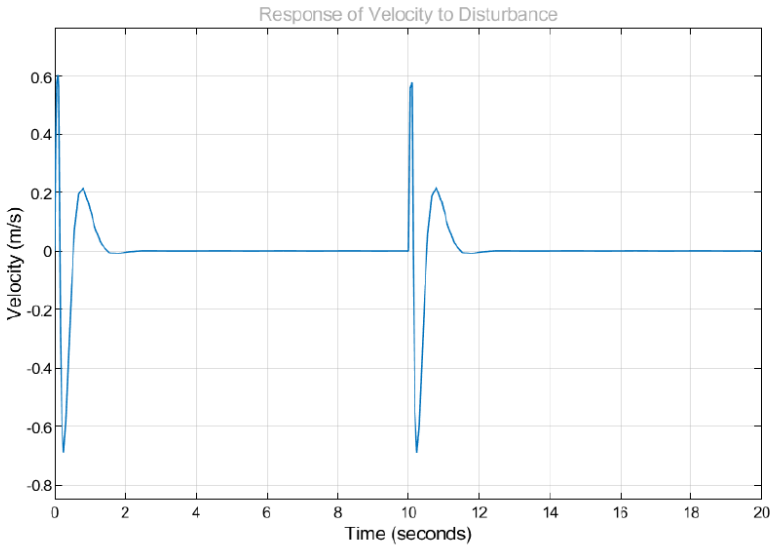


Figure 9: Velocity Impulse Responses for 5 Pole System

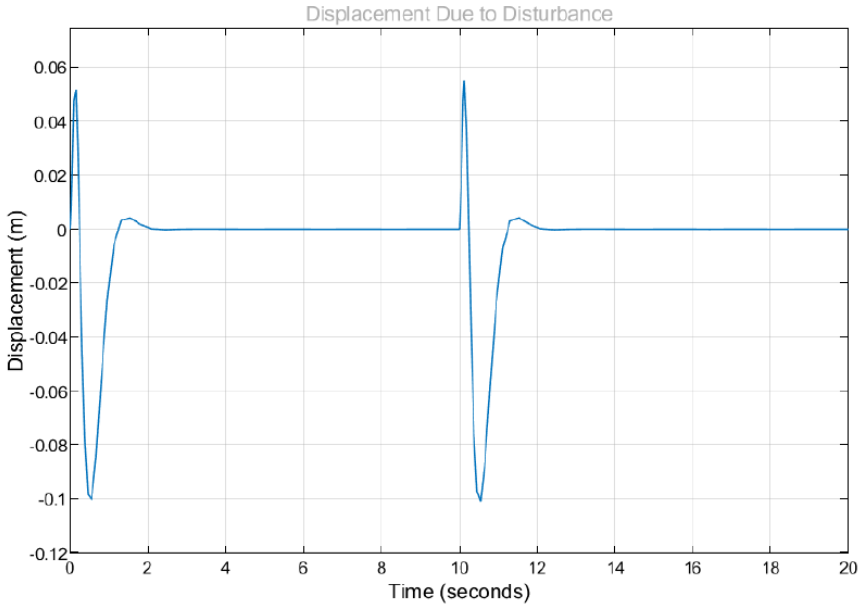


Figure 10: Displacement Impulse Responses for 5 Pole System

# 4 Appendix

## 4.1 Miscellaneous Math/Parameter Estimation - MATLAB

```
%% MOTOR PARAMETER ESTIMATION
t = .02:.02:.02*141;
l = data(:, 1)';
r = data(:, 1)';

% from cftool with custom equation
K = 0.0031
tau = 0.1044
hold on
plot(t, r, '.', 'MarkerSize', 10)
plot(t, 300*K*(1-exp(-t/tau)))
xlabel("Time (s)")
ylabel("Motor Speed")
title("Right motor calibration data")

%% GYROSCOPE CALIBRATION
t = .05:.05:.05*140;
figure
plot(t, gyro, '.')
title("Gyroscope Calibration Data")
xlabel("Time (s)")
ylabel("Pendulum Angle")

wn = 2*pi * (1/1.3)
leff = 9.8 / wn^2
```

## 4.2 3 Pole System Parameter Calculation - MATLAB

```
% Rocky_closed_loop_poles_23.m
%
% 1) Symbolically calculates closed loop transfer function of a disturbannce
% rejection PI control system for Rocky.
% No motor model (M =1). With motor model (1st order TF)
%
% 2) Specify location of (target)poles based on desired reponse. The number of
% poles = denominator polynomial of closed loop TF
%
% 3) Extract the closed loop denomiator poly and set = polynomial of target
% poles
```

```
%
% 4) Solve for Ki, Kp  to match coefficients of polynomials. In general,
% this will be underdefined and will not be able to place poles in exact
% locations. In this, the control constants can be found exactly
%
% 5) Plot impulse and step response to see closed-loop behavior.
%
% based on code by SG. last modified 2/25/23 CL

clear all;
close all;

syms s a b l g Kp Ki    % define symbolic variables

Hvtheta = -s/l/(s^2-g/l);       % TF from velocity to angle of pendulum

K = Kp + Ki/s;                  % TF of the PI angle controller
M = a*b/(s+a)                   % TF of motor (1st order model)
%  M = 1;                       % TF without motor
%
%
% closed loop transfer function from disturbance d(t)totheta(t)
Hcloop = 1/(1-Hvtheta*M*K)    % use this for no motor feedback

pretty(simplify(Hcloop))       % to display the total transfer function

% Substitute parameters and solve
% system parameters
g = 9.81;
l = 0.4195;   %effective length
a = 1/0.1044;           %nominal motor parameters
b = 0.0031;        %nominal motor parameters

Hcloop_sub = subs(Hcloop) % sub parameter values into Hcloop

% specify locations of the target poles,
% choose # based on order of Htot denominator
% e.g., want some oscillations, want fast decay, etc.
p1 = -1 + 2*pi*i    % dominant pole pair
p2 = -1 - 2*pi*i    % dominant pole pair
p3 = -10


% target characteristic polynomial
% if motor model (TF) is added, order of polynomial will increases
tgt_char_poly = (s-p1)*(s-p2)*(s-p3)
npoly = 3
```

```
59
60
61  % get the denominator from Hcloop_sub
62  [n d] = numden(Hcloop_sub)
63
64  % find the coefficients of the denominator polynomial TF
65  coeffs_denom = coeffs(d, s)
66
67  % divide though the coefficient of the highest power term
68  coeffs_denom = coeffs(d, s)/(coeffs_denom(end))
69
70  % find coefficients of the target charecteristic polynomial
71  coeffs_tgt = coeffs(tgt_char_poly, s)
72
73  % solve the system of equations setting the coefficients of the
74  % polynomial in the target to the actual polynomials
75  solutions = solve(coeffs_denom(1:npoly-1) == coeffs_tgt(1:npoly-1),  Kp, Ki)
76
77  % display the solutions as double precision numbers
78  Kp = double(solutions.Kp)
79  Ki = double(solutions.Ki)
80
81  % reorder coefficients for the check polynomial
82  for ii = 1:length(coeffs_denom)
83      chk_coeffs_denom(ii) = coeffs_denom(length(coeffs_denom) + 1 - ii);
84  end
85  closed_loop_poles = vpa (roots(subs(chk_coeffs_denom)), npoly )
86
87
88  % Plot impulse response of closed-loop system
89      TFstring = char(subs(Hcloop));
90      % Define 's' as transfer function variable
91      s = tf('s');
92      % Evaluate the expression
93      eval(['TFH = ',TFstring]);
94      figure (1)
95      impulse(TFH);   %plot the impulse reponse
96      %figure(2)
97      %step(TFH)       %plot the step response
```

## 4.3 5 Pole System Parameter Calculation - MATLAB

```
1  % Rocky_5_closed_loop_poles.m
2  %
```

```
% 1) Symbolically calculates closed loop transfer function of PI disturbannce
% rejection control system for Rocky.
% No motor model (M =1). With motor model (1st order TF)
%
% 2) Specify location of (target)poles based on desired reponse. The number of
% poles = denominator polynomial of closed loop TF
%
% 3) Extract the closed loop denomiator poly and set = polynomial of target
% poles
%
% 4) Solve for Ki, Kp, Ji, Jp, Ci to match coefficients of polynomials. In
↪ general,
% this will be underdefined and will not be able to place poles in exact
% locations. In this case (5th order), the control constants can be found
↪ exactly
%
% 5) Plot impulse response to see closed-loop behavior.
%
% based on code by SG. last modified 3/8/22 CL

clear all;
close all;

syms s a b l g Kp Ki Jp Ji Ci   % define symbolic variables

Hvtheta = -s/l/(s^2-g/l);       % TF from velocity to angle of pendulum

K = Kp + Ki/s;                  % TF of the PI angle controller
M = a*b/(s+a);                  % TF of motor (1st order model)
% M = 1;                        % TF without motor
%
J = Jp + Ji/s + Ci/s^2;         % TF of controller around motor-combinedz PI of
↪ x and v
Mfb = M/(1+M*J);                % Black's formula to get tf for motor with PI
↪ feedback control

%
% closed loop transfer function from disturbance d(t)totheta(t)
% Hcloop = 1/(1-Hvtheta*M*K)    % use this for no motor feedback
% with motor feedback
Hcloop = 1/(1-Hvtheta*Mfb*K)    % use this for motor with feedback

pretty(simplify(Hcloop))       % to display the total transfer function

% Substitute parameters and solve
% system parameters
g = 9.81;
```

```
l = .4195;  %effective length
a = 1/.1044;           %nominal motor parameters
b = .0031;        %nominal motor parameters

Hcloop_sub = subs(Hcloop) % sub parameter values into Hcloop

% specify locations of the target poles,
% choose # based on order of Htot denominator
% e.g., want some oscillations, want fast decay, etc.

% p1 = -1 + 2*pi*i    % dominant pole pair
% p2 = -1 - 2*pi*i    % dominant pole pair
% p3 = -10
% p4 = -8
% p5 = -8.

p1 = -1 + 2*i   % dominant pole pair
p2 = -1 -2*i    % dominant pole pair
p3 = -6
p4 = -42    % dominant pole pair
p5 = -24     % dominant pole pair

% target characteristic polynomial
% if motor model (TF) is added, order of polynomial will increases
% tgt_char_poly = (s-p1)*(s-p2)*(s-p3)

% check polynomial-expand to fifth order
tgt_char_poly = (s-p1)*(s-p2)*(s-p3)*(s-p4)*(s-p5)
exp_tgt_char_poly = expand(tgt_char_poly)

% get the denominator from Hcloop_sub
[n d] = numden(Hcloop_sub)

% find the coefficients of the denominator polynomial TF
coeffs_denom = coeffs(d, s)

% divide though the coefficient of the highest power term
coeffs_denom = coeffs(d, s)/(coeffs_denom(end))
% num_coeff_denom = length(coeffs_denom)

% find coefficients of the target charecteristic polynomial
coeffs_tgt = coeffs(tgt_char_poly, s)
% num_coeff_tgt = length(coeffs_tgt)

% for check. reorder the coefficients to match the denomimator polynomial
for ii = 1:length(coeffs_denom)
    reord_coeffs_tgt(ii) = coeffs_tgt(length(coeffs_tgt) + 1 - ii);
```

```
end
% check roots of target polynomial-should be same as selected poles
roots_target = vpa(roots(reord_coeffs_tgt),4)


% solve the system of equations setting the coefficients of the
% polynomial in the target to the actual polynomials
solutions = solve(coeffs_denom(1:5) == coeffs_tgt(1:5), Jp, Ji,  Kp, Ki, Ci);

% display the solutions as double precision numbers
Kp = double(solutions.Kp)
Ki = double(solutions.Ki)
Ji = double(solutions.Ji)
Jp = double(solutions.Jp)
Ci = double(solutions.Ci)

%write out denominator polynomial
aaa = vpa(subs(coeffs_denom),4)

% reorder coefficients for the check polynomial
for ii = 1:length(coeffs_denom)
    chk_coeffs_denom(ii) = coeffs_denom(length(coeffs_denom) + 1 - ii);
end

% check poles should be same as chosen input poles
check_closed_loop_poles = vpa (roots(subs(chk_coeffs_denom)), 4)

% write out target polynomial
% bbb = vpa( expand(
↪  (s-check_closed_loop_poles(1))*(s-check_closed_loop_poles(2)) ...
%     *(s-check_closed_loop_poles(3))*(s-check_closed_loop_poles(4)) ...
%     *(s-check_closed_loop_poles(5)) ) )



% Plot impulse and step responses of closed-loop system
    TFstring = char(subs(Hcloop));
    % Define 's' as transfer function variable
    s = tf('s');
    % Evaluate the expression
    eval(['TFH = ',TFstring]);
    figure (1)
    impulse(TFH);   %plot the impulse reponse
    figure(2)
    step(TFH)       %plot the step response
```

## 4.4 Balancing Rocky Sketch - ARDUINO

```
// Start the robot flat on the ground
// compile and load the code
// wait for code to load (look for "done uploading" in the Arduino IDE)
// wait for red LED to flash on board
// gently lift body of rocky to upright position
// this will enable the balancing algorithm
// wait for the buzzer
// let go
//
// The balancing algorithm is implemented in BalanceRocky()
// which you should modify to get the balancing to work
//

#include <Balboa32U4.h>
#include <Wire.h>
#include <LSM6.h>
#include "Balance.h"


extern int32_t angle_accum;
extern int32_t speedLeft;
extern int32_t driveLeft;
extern int32_t distanceRight;
extern int32_t speedRight;
extern int32_t distanceLeft;
extern int32_t distanceRight;
float speedCont = 0;
float displacement_m = 0;
int16_t limitCount = 0;
uint32_t cur_time = 0;
float distLeft_m;
float distRight_m;


extern uint32_t delta_ms;
float measured_speedL = 0;
float measured_speedR = 0;
float desSpeedL=0;
float desSpeedR =0;
float dist_accumL_m = 0;
float dist_accumR_m = 0;
float dist_accum = 0;
float speed_err_left = 0;
float speed_err_right = 0;
float speed_err_left_acc = 0;
```

```
46  float speed_err_right_acc = 0;
47  float errAccumRight_m = 0;
48  float errAccumLeft_m = 0;
49  float prevDistLeft_m = 0;
50  float prevDistRight_m = 0;
51  float angle_rad_diff = 0;
52  float angle_rad;                // this is the angle in radians
53  float angle_rad_accum = 0;      // this is the accumulated angle in radians
54  float angle_prev_rad = 0; // previous angle measurement
55  extern int32_t displacement;
56  int32_t prev_displacement=0;
57  uint32_t prev_time;
58
59  #define G_RATIO (162.5)
60
61
62
63  LSM6 imu;
64  Balboa32U4Motors motors;
65  Balboa32U4Encoders encoders;
66  Balboa32U4Buzzer buzzer;
67  Balboa32U4ButtonA buttonA;
68
69
70  #define FIXED_ANGLE_CORRECTION (0.27)  // ***** Replace the value 0.25 with the
    ↪  value you obtained from the Gyro calibration procedure
71
72
73
74
75
76  ////////////////////////////////////////////////////////////////////////////
77  // This is the main function that performs the balancing
78  // It gets called approximately once every 10 ms  by the code in loop()
79  // You should make modifications to this function to perform your
80  // balancing
81  ////////////////////////////////////////////////////////////////////////////
82
83  void BalanceRocky()
84  {
85
86      // **************Enter the control parameters here
87
88    // float Kp = 30370;
89    // float Ki = 154230;
90    // float Ci = -8709.9;
91    // float Jp = 2169.5;
```

```
92    // float Ji = -19442;
93    float Kp = 6879.2;
94    float Ki = 33267;
95    float Ci = -7847.4;
96    float Jp = 567.3923;
97    float Ji = -6306.2;
98
99
100
101
102     float v_c_L, v_c_R; // these are the control velocities to be sent to the
      ↪  motors
103     float v_d = 0; // this is the desired speed produced by the angle controller
104
105
106    // Variables available to you are:
107    // angle_rad  - angle in radians
108    // angle_rad_accum - integral of angle
109    // measured_speedR - right wheel speed (m/s)
110    // measured_speedL - left wheel speed (m/s)
111    // distLeft_m - distance traveled by left wheel in meters
112    // distRight_m - distance traveled by right wheel in meters  (this is the
      ↪  integral of the velocities)
113    // dist_accum - integral of the distance
114
115    // *** enter an equation for v_d in terms of the variables available ****
116     v_d =  Kp*angle_rad + Ki * angle_rad_accum ; // this is the desired velocity
      ↪  from the angle controller
117
118
119
120   // The next two lines implement the feedback controller for the motor. Two
      ↪  separate velocities are calculated.
121  //   v_j =
122   //
123   // We use a trick here by criss-crossing the distance from left to right and
124   // right to left. This helps ensure that the Left and Right motors are
      ↪  balanced
125
126   // *** enter equations for input signals for v_c (left and right) in terms of
      ↪  the variables available ****
127     //v_c_R = 0.84 * v_d; // CHANGE HERE TO FIX MOTORS
128     //v_c_L = 1 * v_d;
129     v_c_R = v_d - (Jp*measured_speedR + Ji*distRight_m + Ci*dist_accum);
130     v_c_L = v_d - (Jp*measured_speedR + Ji*distRight_m + Ci*dist_accum);
131
132     // save desired speed for debugging
```

```
    desSpeedL = v_c_L;
    desSpeedR = v_c_R;
    Serial.println(v_d);

    // the motor control signal has to be between +- 300. So clip the values to
    ↪  be within that range
    // here
    if(v_c_L > 300) v_c_L = 300;
    if(v_c_R > 300) v_c_R = 300;
    if(v_c_L < -300) v_c_L = -300;
    if(v_c_R < -300) v_c_R = -300;

    // Set the motor speeds
    motors.setSpeeds((int16_t) (v_c_L), (int16_t)(v_c_R));

}



void setup()
{
  // Uncomment these lines if your motors are reversed.
  // motors.flipLeftMotor(true);
  // motors.flipRightMotor(true);

  Serial.begin(9600);
  prev_time = 0;
  displacement = 0;
  ledYellow(0);
  ledRed(1);
  balanceSetup();
  ledRed(0);
  angle_accum = 0;

  ledGreen(0);
  ledYellow(0);
}



int16_t time_count = 0;
extern int16_t angle_prev;
int16_t start_flag = 0;
int16_t start_counter = 0;
void lyingDown();
extern bool isBalancingStatus;
extern bool balanceUpdateDelayedStatus;
```

```
179
180 void UpdateSensors()
181 {
182   static uint16_t lastMillis;
183   uint16_t ms = millis();
184
185   // Perform the balance updates at 100 Hz.
186   balanceUpdateDelayedStatus = ms - lastMillis > UPDATE_TIME_MS + 1;
187   lastMillis = ms;
188
189   // call functions to integrate encoders and gyros
190   balanceUpdateSensors();
191
192   if (imu.a.x < 0)
193   {
194     lyingDown();
195     isBalancingStatus = false;
196   }
197   else
198   {
199     isBalancingStatus = true;
200   }
201 }
202
203
204
205 void GetMotorAndAngleMeasurements()
206 {
207     // convert distance calculation into meters
208     // and integrate distance
209     distLeft_m =
    ↪  ((float)distanceLeft)/((float)G_RATIO)/12.0*80.0/1000.0*3.14159;
210     distRight_m =
    ↪  ((float)distanceRight)/((float)G_RATIO)/12.0*80.0/1000.0*3.14159;
    ↪
211     dist_accum += (distLeft_m+distRight_m)*0.01/2.0;
212
213     // compute left and right wheel speed in meters/s
214     measured_speedL =
    ↪  speedLeft/((float)G_RATIO)/12.0*80.0/1000.0*3.14159*100.0;
215     measured_speedR =
    ↪  speedRight/((float)G_RATIO)/12.0*80.0/1000.0*3.14159*100.0;
216
217     prevDistLeft_m = distLeft_m;
218     prevDistRight_m = distRight_m;
219
220
```

```
221     // this integrates the angle
222     angle_rad_accum += angle_rad*0.01;
223     // this is the derivative of the angle
224     angle_rad_diff = (angle_rad-angle_prev_rad)/0.01;
225     angle_prev_rad  = angle_rad;
226 
227 }
228 
229 void balanceResetAccumulators()
230 {
231     errAccumLeft_m = 0.0;
232     errAccumRight_m = 0.0;
233     speed_err_left_acc = 0.0;
234     speed_err_right_acc = 0.0;
235 }
236 
237 
238 
239 void loop()
240 {
241   static uint32_t prev_print_time = 0;   // this variable is to control how
    ↪  often we print on the serial monitor
242   int16_t distanceDiff;    // this stores the difference in distance in encoder
    ↪  clicks that was traversed by the right vs the left wheel
243   static float del_theta = 0;
244   char enableLongTermGyroCorrection = 1;
245 
246   cur_time = millis();                    // get the current time in miliseconds
247 
248 
249   if((cur_time - prev_time) > UPDATE_TIME_MS){
250     UpdateSensors();                     // run the sensor updates.
251 
252     // calculate the angle in radians. The FIXED_ANGLE_CORRECTION term comes
    ↪  from the angle calibration procedure (separate sketch available for
    ↪  this)
253     // del_theta corrects for long-term drift
254     angle_rad = ((float)angle)/1000/180*3.14159 - FIXED_ANGLE_CORRECTION -
    ↪  del_theta;
255 
256     if(angle_rad > 0.1 || angle_rad < -0.1)      // If angle is not within +- 6
    ↪  degrees, reset counter that waits for start
257     {
258       start_counter = 0;
259    }
260 
261 
```

```
  if(angle_rad > -0.1 && angle_rad < 0.1 && ! start_flag)
  {
    // increment the start counter
    start_counter++;
    // If the start counter is greater than 30, this means that the angle has
    ↪  been within +- 6 degrees for 0.3 seconds, then set the start_flag
    if(start_counter > 30)
    {
      balanceResetEncoders();
      start_flag = 1;
      buzzer.playFrequency(DIV_BY_10 | 445, 1000, 15);
      Serial.println("Starting");
      ledYellow(1);
    }
  }


  // every UPDATE_TIME_MS, if the start_flag has been set, do the balancing
  if(start_flag)
  {
    GetMotorAndAngleMeasurements();
    if(enableLongTermGyroCorrection)
      del_theta = 0.999*del_theta + 0.001*angle_rad;  // assume that the robot
      ↪  is standing. Smooth out the angle to correct for long-term gyro drift

    // Control the robot
    BalanceRocky();
  }
  prev_time = cur_time;
  }
// if the robot is more than 45 degrees, shut down the motor
  if(start_flag && angle_rad > .78)
  {
    motors.setSpeeds(0,0);
    start_flag = 0;
  }
  else if(start_flag && angle_rad < -0.78)
  {
    motors.setSpeeds(0,0);
    start_flag = 0;
  }

// kill switch
  if(buttonA.getSingleDebouncedPress())
  {
      motors.setSpeeds(0,0);
      while(!buttonA.getSingleDebouncedPress());
```

```
307   }
308
309 if(cur_time - prev_print_time > 103)   // do the printing every 105 ms. Don't
    ↪  want to do it for an integer multiple of 10ms to not hog the processor
310   {
311         Serial.print(angle_rad);
312         Serial.print("\t");
313         Serial.print(distLeft_m);
314         Serial.print("\t");
315         Serial.print(measured_speedL);
316         Serial.print("\t");
317         Serial.print(measured_speedR);
318         Serial.print("\t");
319        Serial.println(speedCont);
320        prev_print_time = cur_time;
321   }
322
323
324 }
```