

Rocky Project

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Link to final Rocky Demonstration video: https://drive.google.com/file/d/1nDenw_emLLbFz2i0xh1ZBsGk58QRZF7p/view?usp=sharing

1 Parameter Identification

1.1 Motor Constants

Per the project instructions, the motor has a transfer function (from the controlled input velocity to the actual output) of

$$M(s) = \frac{\frac{K}{\tau}}{s + \frac{1}{\tau}} \quad (1)$$

with K and τ being constants unique to each motor, and identifying those constants is critical for a well performing Rocky. To estimate those parameters, we held our Rocky upright and ran the motors for three seconds along the carpeted floor of MAC 128 while recording the measured motor speed using the motor test calibration sketch found in the appendix.

With the data in hand, we needed to now convert the motor transfer function into an equation for velocity in the time domain, since this the domain our measured data exists in. The procedure for that is below.

$$M(s) = \frac{V(s)}{V_c(s)} = \frac{\frac{K}{\tau}}{s + \frac{1}{\tau}} \quad (2)$$

$$V_c(s) = \frac{300}{s}$$

$$V(s) = \frac{300 \frac{K}{\tau}}{s(s + \frac{1}{\tau})}$$

Now we take the inverse Laplace transform using tables:

$$v(t) = 300k(1 - e^{-\frac{t}{\tau}})$$

To obtain estimates for our two motor parameters, we used MATLAB's curve-fitting toolbox to fit this curve onto our measured motor data (shown in Figure 1) and got $K = 0.0031$ and $\tau = 0.1044$

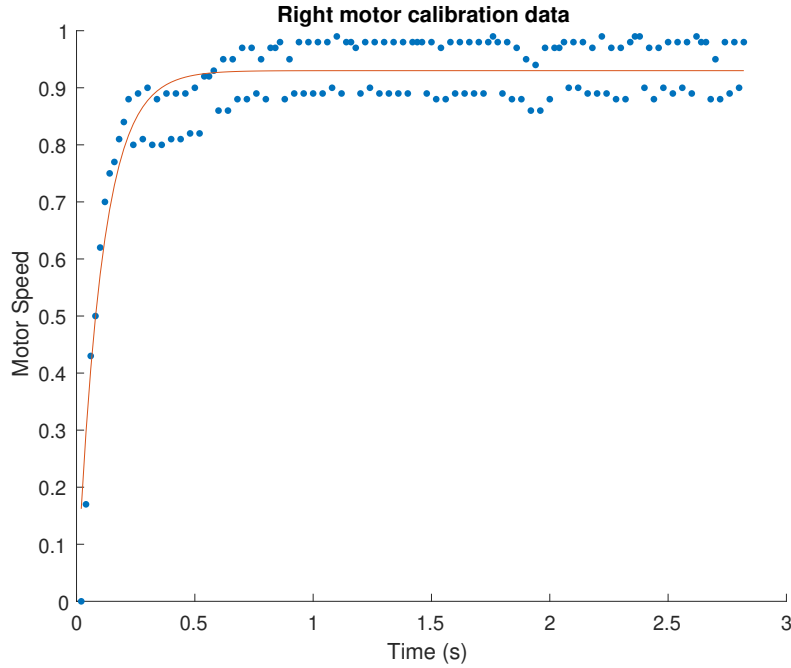


Figure 1: Right Motor Speed

1.2 Natural Frequency & Pendulum Length

In order to find our Rocky's natural frequency and the effective length of the pendulum body, we needed to calibrate its gyroscope. To do so, we started with the Rocky laying down horizontally on the table, and then picking it up and holding it vertically in the air as if it were balancing. This was done while running the gyro calibration sketch found in the appendix to track angle measurement offset.

After accounting for the angle correction needed, we could collect more gyro data to measure natural frequency. We compiled and loaded the gyro calibration sketch again with the Rocky (wheels off) laying flat. After loading, we opened the serial monitor and held the Rocky by two points at the top, allowing it to swing freely for a few seconds to collect angle measurement data. This data output was then copied into MATLAB and plotted to find the period (found experimentally by inspecting the data), which we plugged into the following equation to find natural frequency:

$$\omega_n = \frac{2\pi}{\text{period}} \text{ [rad/s]} \quad (3)$$

$$\omega_n = \frac{2\pi}{1.3} = 4.8332 \text{ [rad/s]}$$

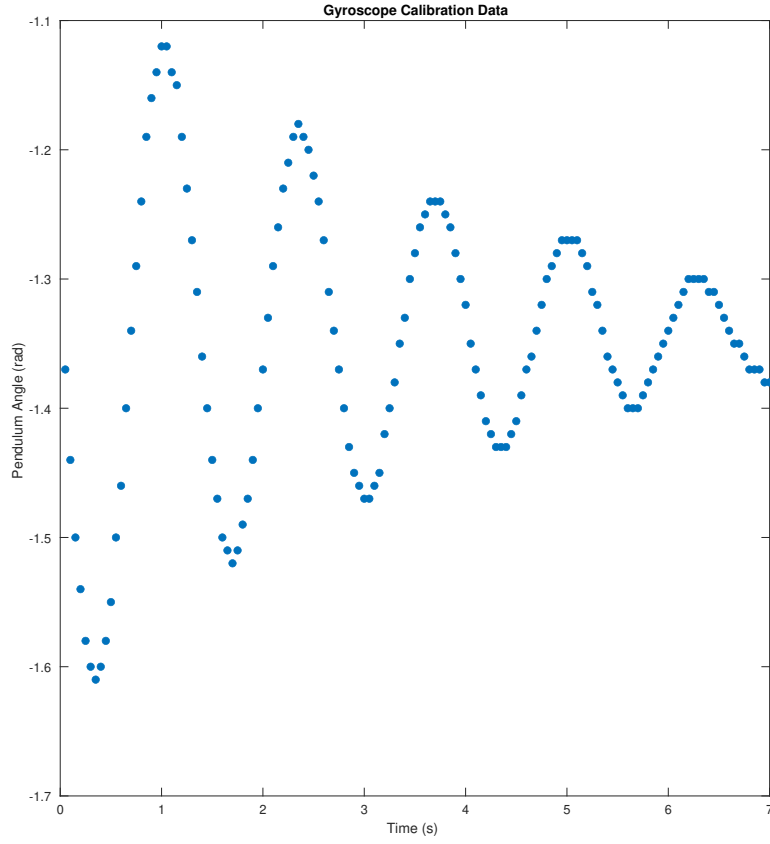


Figure 2: Gyroscope Calibration Data

Now that we have natural frequency, we can solve backwards for pendulum length using the provided approximation.

$$\omega_n = \sqrt{g/l_{\text{eff}}} \quad (4)$$

This gives us an effective length $l_{\text{eff}} = 0.4195$.

2 Initial (3 pole) System

2.1 Pole Values

For our Initial System, the poles we chose were $-1 \pm 2\pi i$ and -10 . The imaginary poles were selected due to their rapidly decaying nature without the presence of large initial oscillations. The real pole was selected to be negative to influence the system to have a decaying response to return to steady state. After having a general idea of what our poles should look like we determined the ones we used through a few iterations of trial and error. We found that the larger the negative value of the real pole, the Rocky would return back to steady state quicker. This was juxtaposed with the limitations of the physical Rocky system that were only able to respond to input so fast.

2.2 Calculating Control Constants

From our selected poles we were able to derive our control constants: K_p and K_i . We did this by expanding our poles into a third order polynomial, find the target coefficients of the polynomial, reorder the coefficients to match the denominator polynomial, which is found from the closed loop transfer function:

$$H_{\text{Loop}} = \frac{1}{1 - (\Theta)MK} \quad (5)$$

Where Θ represents the transfer function from velocity to angle of a pendulum $\frac{-s}{s^2 - g/l}$, M represents the transfer function of a 1st order model of the motor $\frac{a*b}{s+a}$, and $K = K_p + \frac{K_i}{s}$ represents a transfer function of the PI angle controller. Lastly, the system of equations that set the coefficients of the target polynomial into actual polynomials is solved, outputting K_p and K_i as shown below. We found that this model failed to correct itself effectively. Despite the angle returning to zero radians, this outcome resulted in our Rocky continuously moving forward or backwards faster and faster, as well as driving away from its original location. This seemed to be due to it not make the necessary over correction, just barely making it back to zero before falling in the same direction it corrected itself from. This phenomenon is also visible in our Simulink plots, shown below.

Parameter	Value
K_p	1185
K_i	8883

2.3 Simulink model

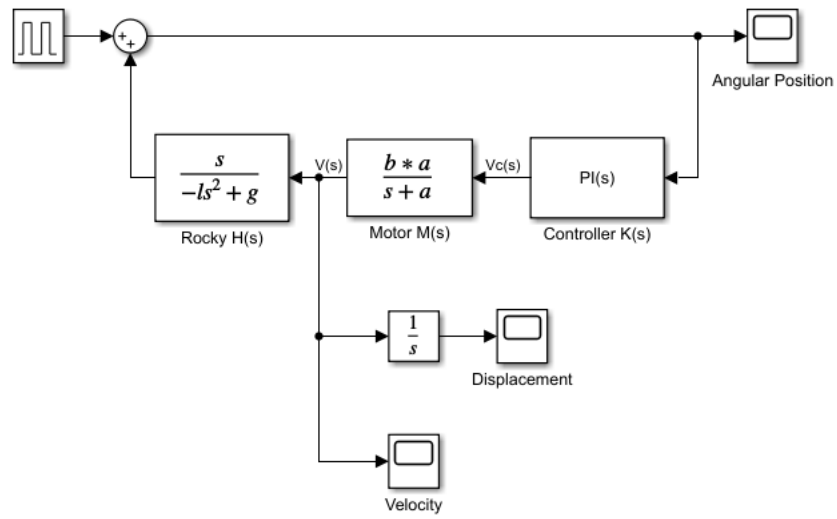


Figure 3: Block Diagram for 3 Pole System

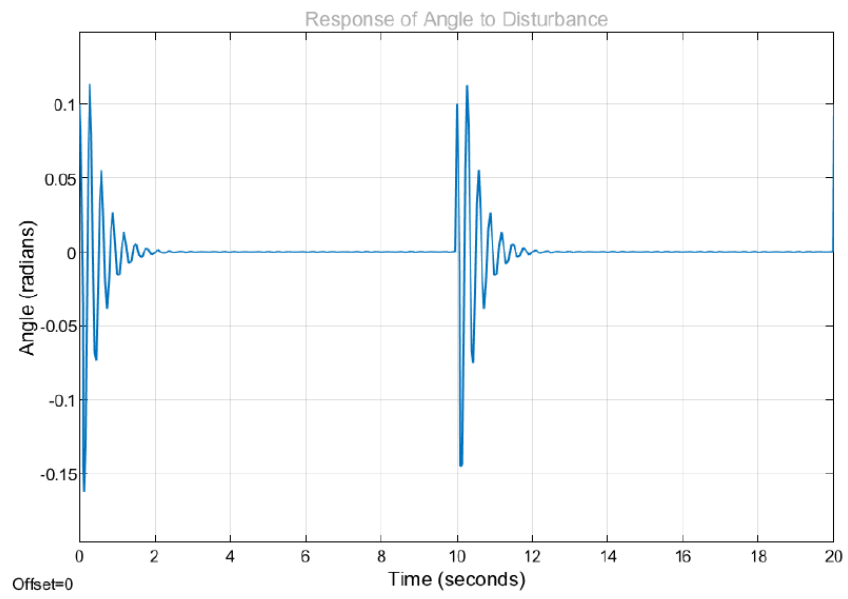


Figure 4: Angle Impulse Responses for 3 Pole System

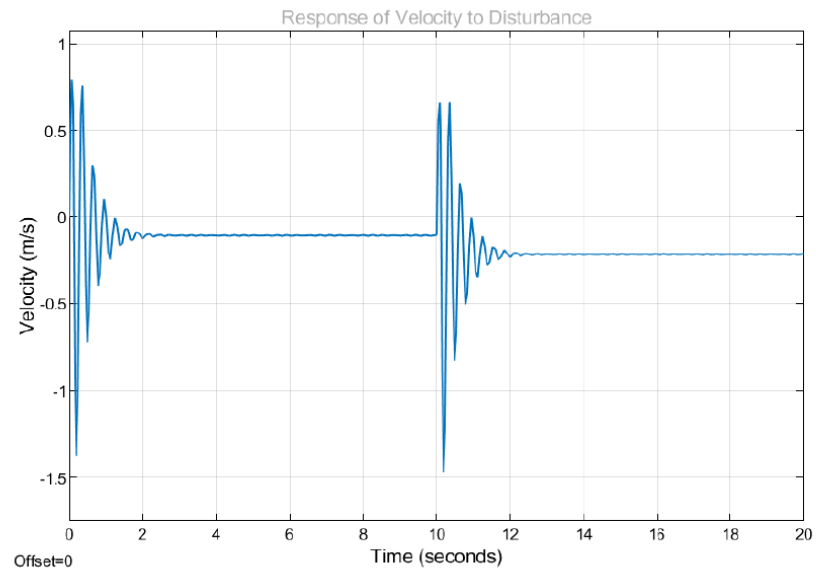


Figure 5: Velocity Impulse Responses for 3 Pole System

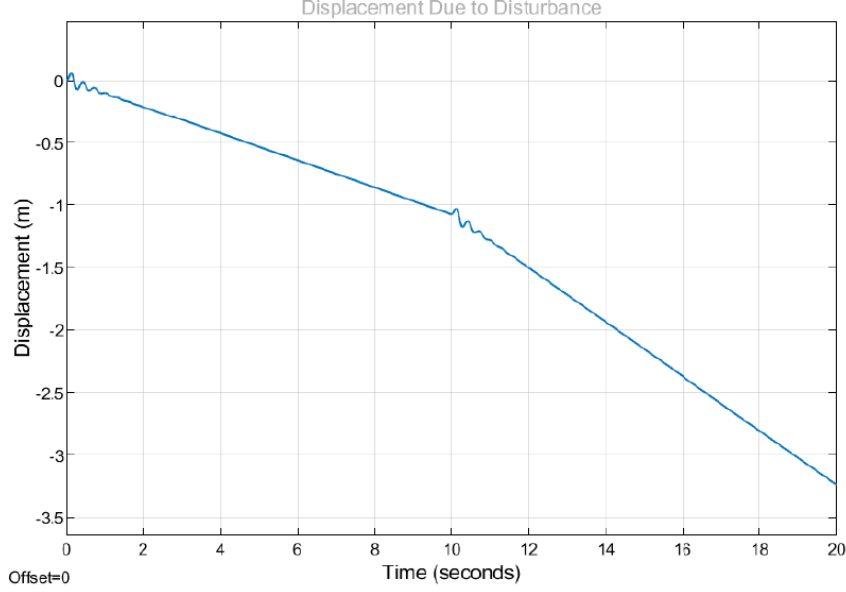


Figure 6: Displacement Impulse Responses for 3 Pole System

3 Balancing System

3.1 Pole Values

For our Revised System, the poles we chose were $-3.38 \pm 3.45i$, -10 , -4.8332 , and -4.8332 . The imaginary poles were selected due to their rapidly decaying nature without the presence of large initial oscillations. The real poles were selected to be negative to influence the system to have a decaying response to return to steady state. We combined trial and error with a bit of rough hand calculations to determine our poles this time we calculated our first and second (imaginary poles) and our fourth and fifth (real poles) with dampening values.

Those calculations were just choosing a damping ratio that seemed appropriate for both the angular position control loop and the motor velocity control loop (both of them being very slightly underdamped) and applying the following formula from Day 7 to find the corresponding poles assuming this was a 2 pole system.

$$p_{1,2} = -\zeta\omega_n \pm i\omega_n\sqrt{1 - \zeta^2}$$

After that, we just performed a bit of trial-and-error tuning in order to find exact values that worked well for us.

3.2 Calculating Control Constants

From our selected poles we were able to derive our control constants: K_p , K_i , J_p , J_i , and C_i . We did this by expanding our poles into a fifth order polynomial, finding the target coefficients of the polynomial, reordering the coefficients to match the denominator polynomial, which is found from the closed loop transfer function:

$$H_{\text{Loop}} = \frac{1}{1 - (\Theta)M_{fb}K} \quad (6)$$

Where Θ represents the transfer function from velocity to angle of a pendulum $\frac{\frac{-s}{l}}{s^2 - g/l}$, M_{fb} represents Black's formula of a 1st order model of the motor with a PI feedback controller (in order to ensure the Rocky balances in place) $\frac{a*b}{s+a+J(a+b)}$ and $J = J_p + \frac{J_i}{s} + \frac{C_i}{s^2}$, and $K = K_p + \frac{K_i}{s}$ represents a transfer function of the PI angle controller. Lastly, the system of equations that set the coefficients of the target polynomial into actual polynomials is solved, outputting our control parameters as given in the table below. We found this system was far more effective at balancing the Rocky, as it was able to maneuver back and forth in order to keep the Rocky balancing in one spot.

Parameter	Value
K_p	33819
K_i	172920
J_p	2169
J_i	-27530
C_i	-43550

3.3 Simulink model

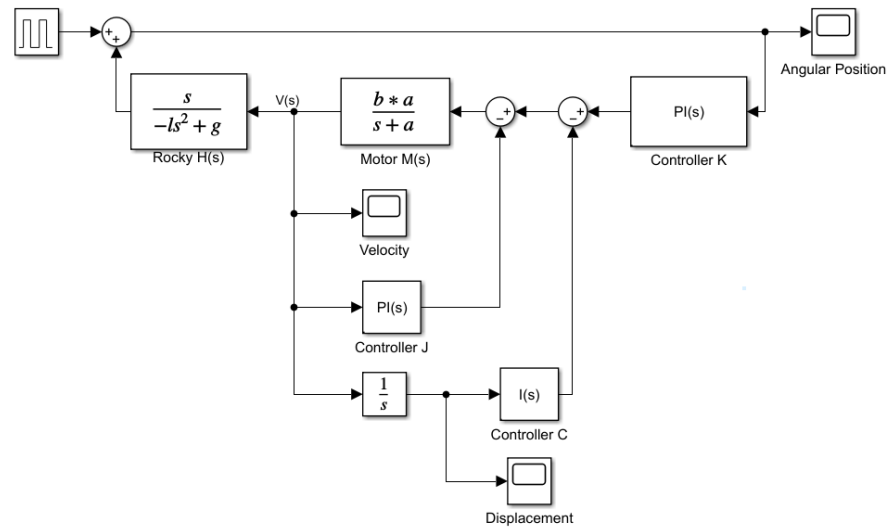


Figure 7: Block Diagram for 5 Pole System

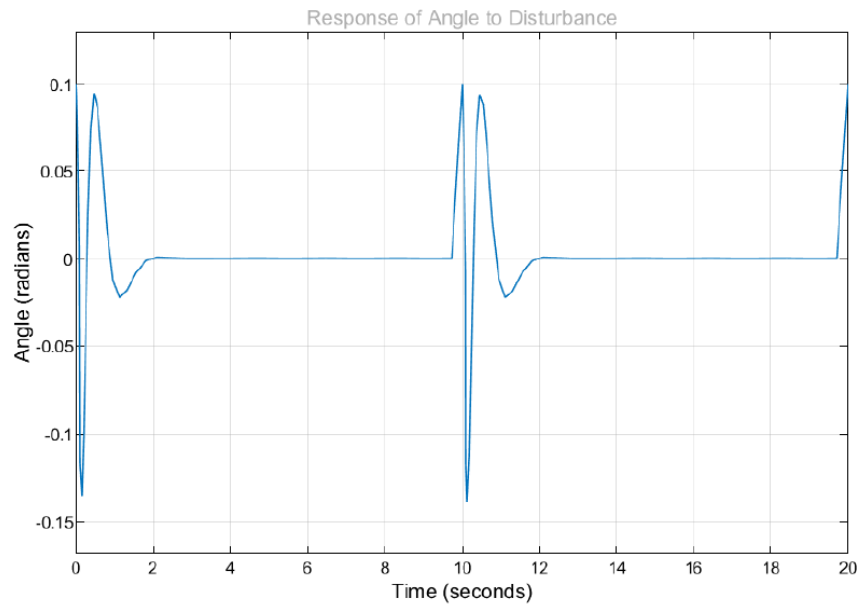


Figure 8: Angle Impulse Responses for 5 Pole System

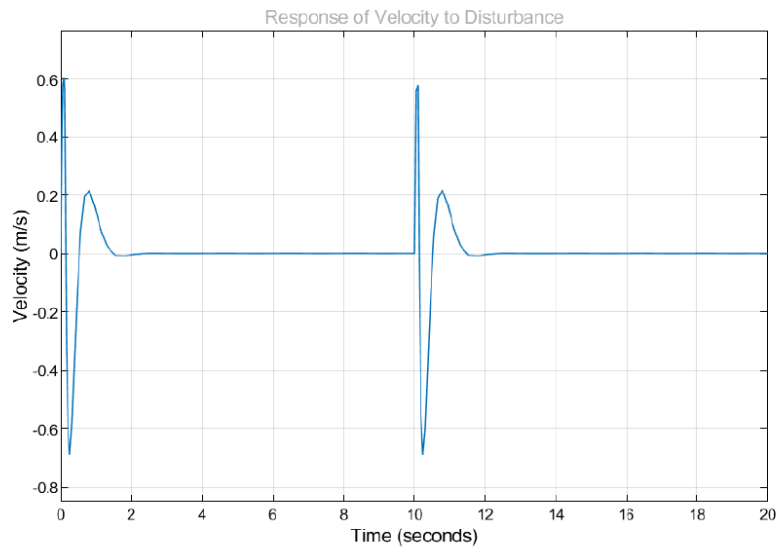


Figure 9: Velocity Impulse Responses for 5 Pole System

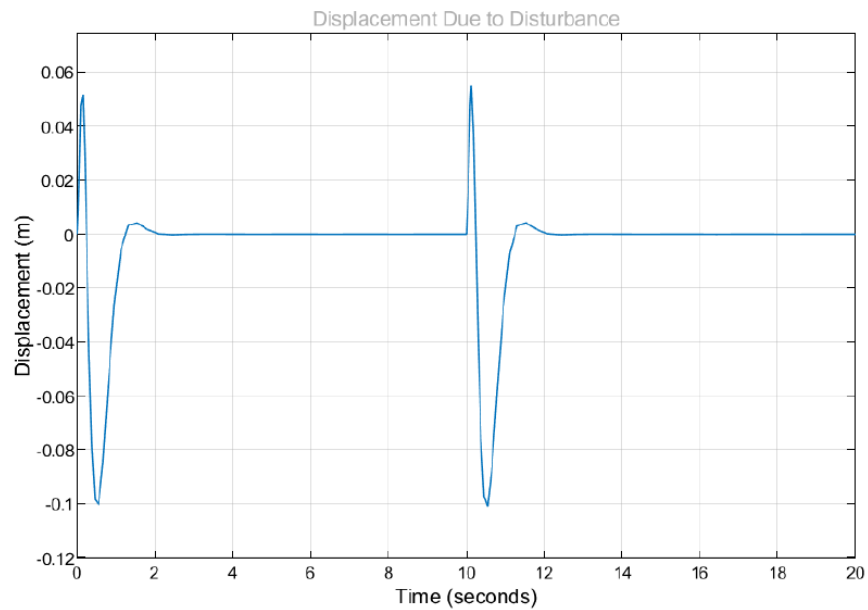


Figure 10: Displacement Impulse Responses for 5 Pole System

4 Appendix

4.1 Miscellaneous Math/Parameter Estimation - MATLAB

```

1  %% MOTOR PARAMETER ESTIMATION
2  t = .02:.02:.02*141;
3  l = data(:, 1)';
4  r = data(:, 1)';
5
6  % from cftool with custom equation
7  K = 0.0031
8  tau = 0.1044
9  hold on
10 plot(t, r, '.', 'MarkerSize', 10)
11 plot(t, 300*K*(1-exp(-t/tau)))
12 xlabel("Time (s)")
13 ylabel("Motor Speed")
14 title("Right motor calibration data")
15

```

```

16 %% GYROSCOPE CALIBRATION
17 t = .05:.05:.05*140;
18 figure
19 plot(t, gyro, '.')
20 title("Gyroscope Calibration Data")
21 xlabel("Time (s)")
22 ylabel("Pendulum Angle")
23
24 wn = 2*pi * (1/1.3)
25 leff = 9.8 / wn^2

```

4.2 3 Pole System Parameter Calculation - MATLAB

```

1 % Rocky_closed_loop_poles_23.m
2 %
3 % 1) Symbolically calculates closed loop transfer function of a disturbance
4 % rejection PI control system for Rocky.
5 % No motor model (M =1). With motor model (1st order TF)
6 %
7 % 2) Specify location of (target)poles based on desired response. The number of
8 % poles = denominator polynomial of closed loop TF
9 %
10 % 3) Extract the closed loop denominator poly and set = polynomial of target
11 % poles
12 %
13 % 4) Solve for Ki, Kp to match coefficients of polynomials. In general,
14 % this will be underdefined and will not be able to place poles in exact
15 % locations. In this, the control constants can be found exactly
16 %
17 % 5) Plot impulse and step response to see closed-loop behavior.
18 %
19 % based on code by SG. last modified 2/25/23 CL
20
21 clear all;
22 close all;
23
24 syms s a b l g Kp Ki % define symbolic variables
25
26 Hvtheta = -s/l/(s^2-g/l); % TF from velocity to angle of pendulum
27
28 K = Kp + Ki/s; % TF of the PI angle controller
29 M = a*b/(s+a) % TF of motor (1st order model)
30 % M = 1; % TF without motor
31 %

```

```

32 %
33 % closed loop transfer function from disturbance d(t) to theta(t)
34 Hcloop = 1/(1-Hvtheta*M*K) % use this for no motor feedback
35
36 pretty(simplify(Hcloop)) % to display the total transfer function
37
38 % Substitute parameters and solve
39 % system parameters
40 g = 9.81;
41 l = 0.4195; %effective length
42 a = 1/0.1044; %nominal motor parameters
43 b = 0.0031; %nominal motor parameters
44
45 Hcloop_sub = subs(Hcloop) % sub parameter values into Hcloop
46
47 % specify locations of the target poles,
48 % choose # based on order of Htot denominator
49 % e.g., want some oscillations, want fast decay, etc.
50 p1 = -1 + 2*pi*i % dominant pole pair
51 p2 = -1 - 2*pi*i % dominant pole pair
52 p3 = -10
53
54
55 % target characteristic polynomial
56 % if motor model (TF) is added, order of polynomial will increase
57 tgt_char_poly = (s-p1)*(s-p2)*(s-p3)
58 npoly = 3
59
60
61 % get the denominator from Hcloop_sub
62 [n d] = numden(Hcloop_sub)
63
64 % find the coefficients of the denominator polynomial TF
65 coeffs_denom = coeffs(d, s)
66
67 % divide through the coefficient of the highest power term
68 coeffs_denom = coeffs(d, s)/(coeffs_denom(end))
69
70 % find coefficients of the target characteristic polynomial
71 coeffs_tgt = coeffs(tgt_char_poly, s)
72
73 % solve the system of equations setting the coefficients of the
74 % polynomial in the target to the actual polynomials
75 solutions = solve(coeffs_denom(1:npoly-1) == coeffs_tgt(1:npoly-1), Kp, Ki)
76
77 % display the solutions as double precision numbers
78 Kp = double(solutions.Kp)

```

```

79 Ki = double(solutions.Ki)
80
81 % reorder coefficients for the check polynomial
82 for ii = 1:length(coeffs_denom)
83     chk_coeffs_denom(ii) = coeffs_denom(length(coeffs_denom) + 1 - ii);
84 end
85 closed_loop_poles = vpa (roots(subs(chk_coeffs_denom)), npoly )
86
87
88 % Plot impulse response of closed-loop system
89 TFstring = char(subs(Hcloop));
90 % Define 's' as transfer function variable
91 s = tf('s');
92 % Evaluate the expression
93 eval(['TFH = ',TFstring]);
94 figure (1)
95 impulse(TFH); %plot the impulse reponse
96 %figure(2)
97 %step(TFH) %plot the step response

```

4.3 5 Pole System Parameter Calculation - MATLAB

```

1 % Rocky_5_closed_loop_poles.m
2 %
3 % 1) Symbolically calculates closed loop transfer function of PI disturbance
4 % rejection control system for Rocky.
5 % No motor model (M=1). With motor model (1st order TF)
6 %
7 % 2) Specify location of (target)poles based on desired response. The number of
8 % poles = denominator polynomial of closed loop TF
9 %
10 % 3) Extract the closed loop denominator poly and set = polynomial of target
11 % poles
12 %
13 % 4) Solve for Ki, Kp, Ji, Jp, Ci to match coefficients of polynomials. In
14 % ↪ general,
15 % this will be underdefined and will not be able to place poles in exact
16 % locations. In this case (5th order), the control constants can be found
17 % ↪ exactly
18 %
19 % 5) Plot impulse response to see closed-loop behavior.
20 %
21 % based on code by SG. last modified 3/8/22 CL

```

```

21 clear all;
22 close all;
23
24 syms s a b l g Kp Ki Jp Ji Ci % define symbolic variables
25
26 Hvtheta = -s/l/(s^2-g/l); % TF from velocity to angle of pendulum
27
28 K = Kp + Ki/s; % TF of the PI angle controller
29 M = a*b/(s+a); % TF of motor (1st order model)
30 % M = 1; % TF without motor
31 %
32 J = Jp + Ji/s + Ci/s^2; % TF of controller around motor-combinedz PI of
   ↪ x and v
33 Mfb = M/(1+M*J); % Black's formula to get tf for motor with PI
   ↪ feedback control
34
35 %
36 % closed loop transfer function from disturbance d(t) to theta(t)
37 % Hcloop = 1/(1-Hvtheta*M*K) % use this for no motor feedback
38 % with motor feedback
39 Hcloop = 1/(1-Hvtheta*Mfb*K) % use this for motor with feedback
40
41 pretty(simplify(Hcloop)) % to display the total transfer function
42
43 % Substitute parameters and solve
44 % system parameters
45 g = 9.81;
46 l = .4195; %effective length
47 a = 1/.1044; %nominal motor parameters
48 b = .0031; %nominal motor parameters
49
50 Hcloop_sub = subs(Hcloop) % sub parameter values into Hcloop
51
52 % specify locations of the target poles,
53 % choose # based on order of Htot denominator
54 % e.g., want some oscillations, want fast decay, etc.
55
56 % p1 = -1 + 2*pi*i % dominant pole pair
57 % p2 = -1 - 2*pi*i % dominant pole pair
58 % p3 = -10
59 % p4 = -8
60 % p5 = -8.
61
62 p1 = -1 + 2*i % dominant pole pair
63 p2 = -1 - 2*i % dominant pole pair
64 p3 = -6
65 p4 = -42 % dominant pole pair

```



```

66 p5 = -24      % dominant pole pair
67
68 % target characteristic polynomial
69 % if motor model (TF) is added, order of polynomial will increase
70 % tgt_char_poly = (s-p1)*(s-p2)*(s-p3)
71
72 % check polynomial-expand to fifth order
73 tgt_char_poly = (s-p1)*(s-p2)*(s-p3)*(s-p4)*(s-p5)
74 exp_tgt_char_poly = expand(tgt_char_poly)
75
76 % get the denominator from Hcloop_sub
77 [n d] = numden(Hcloop_sub)
78
79 % find the coefficients of the denominator polynomial TF
80 coeffs_denom = coeffs(d, s)
81
82 % divide through the coefficient of the highest power term
83 coeffs_denom = coeffs(d, s)/(coeffs_denom(end))
84 % num_coeff_denom = length(coeffs_denom)
85
86 % find coefficients of the target characteristic polynomial
87 coeffs_tgt = coeffs(tgt_char_poly, s)
88 % num_coeff_tgt = length(coeffs_tgt)
89
90 % for check. reorder the coefficients to match the denominator polynomial
91 for ii = 1:length(coeffs_denom)
92     reord_coeffs_tgt(ii) = coeffs_tgt(length(coeffs_tgt) + 1 - ii);
93 end
94 % check roots of target polynomial-should be same as selected poles
95 roots_target = vpa(roots(reord_coeffs_tgt),4)
96
97
98 % solve the system of equations setting the coefficients of the
99 % polynomial in the target to the actual polynomials
100 solutions = solve(coeffs_denom(1:5) == coeffs_tgt(1:5), Jp, Ji, Kp, Ki, Ci);
101
102 % display the solutions as double precision numbers
103 Kp = double(solutions.Kp)
104 Ki = double(solutions.Ki)
105 Ji = double(solutions.Ji)
106 Jp = double(solutions.Jp)
107 Ci = double(solutions.Ci)
108
109 %write out denominator polynomial
110 aaa = vpa(subs(coeffs_denom),4)
111
112 % reorder coefficients for the check polynomial

```

```

113 for ii = 1:length(coeffs_denom)
114     chk_coeffs_denom(ii) = coeffs_denom(length(coeffs_denom) + 1 - ii);
115 end
116
117 % check poles should be same as chosen input poles
118 check_closed_loop_poles = vpa (roots(subs(chk_coeffs_denom)), 4)
119
120 % write out target polynomial
121 % bbb = vpa( expand(
122     ↪ (s-check_closed_loop_poles(1))*(s-check_closed_loop_poles(2)) ...
123     %      *(s-check_closed_loop_poles(3))*(s-check_closed_loop_poles(4)) ...
124     %      *(s-check_closed_loop_poles(5)) ) )
125
126
127 % Plot impulse and step responses of closed-loop system
128 TFstring = char(subs(Hcloop));
129 % Define 's' as transfer function variable
130 s = tf('s');
131 % Evaluate the expression
132 eval(['TFH = ',TFstring]);
133 figure (1)
134 impulse(TFH); %plot the impulse reponse
135 figure(2)
136 step(TFH) %plot the step response

```

4.4 Balancing Rocky Sketch - ARDUINO

```

1 // Start the robot flat on the ground
2 // compile and load the code
3 // wait for code to load (look for "done uploading" in the Arduino IDE)
4 // wait for red LED to flash on board
5 // gently lift body of rocky to upright position
6 // this will enable the balancing algorithm
7 // wait for the buzzer
8 // let go
9 //
10 // The balancing algorithm is implemented in BalanceRocky()
11 // which you should modify to get the balancing to work
12 //
13
14 #include <Balboa32U4.h>
15 #include <Wire.h>
16 #include <LSM6.h>

```

```

17  #include "Balance.h"
18
19
20  extern int32_t angle_accum;
21  extern int32_t speedLeft;
22  extern int32_t driveLeft;
23  extern int32_t distanceRight;
24  extern int32_t speedRight;
25  extern int32_t distanceLeft;
26  extern int32_t distanceRight;
27  float speedCont = 0;
28  float displacement_m = 0;
29  int16_t limitCount = 0;
30  uint32_t cur_time = 0;
31  float distLeft_m;
32  float distRight_m;
33
34
35  extern uint32_t delta_ms;
36  float measured_speedL = 0;
37  float measured_speedR = 0;
38  float desSpeedL=0;
39  float desSpeedR =0;
40  float dist_accumL_m = 0;
41  float dist_accumR_m = 0;
42  float dist_accum = 0;
43  float speed_err_left = 0;
44  float speed_err_right = 0;
45  float speed_err_left_acc = 0;
46  float speed_err_right_acc = 0;
47  float errAccumRight_m = 0;
48  float errAccumLeft_m = 0;
49  float prevDistLeft_m = 0;
50  float prevDistRight_m = 0;
51  float angle_rad_diff = 0;
52  float angle_rad;           // this is the angle in radians
53  float angle_rad_accum = 0; // this is the accumulated angle in radians
54  float angle_prev_rad = 0; // previous angle measurement
55  extern int32_t displacement;
56  int32_t prev_displacement=0;
57  uint32_t prev_time;
58
59  #define G_RATIO (162.5)
60
61
62
63  LSM6 imu;

```

```

64 Balboa32U4Motors motors;
65 Balboa32U4Encoders encoders;
66 Balboa32U4Buzzer buzzer;
67 Balboa32U4ButtonA buttonA;
68
69
70 #define FIXED_ANGLE_CORRECTION (0.27) // ***** Replace the value 0.25 with the
    ↪ value you obtained from the Gyro calibration procedure
71
72
73
74
75
76 //////////////////////////////////////////////////////////////////////////////////////////////////////////////////////////////////
77 // This is the main function that performs the balancing
78 // It gets called approximately once every 10 ms by the code in loop()
79 // You should make modifications to this function to perform your
80 // balancing
81 //////////////////////////////////////////////////////////////////////////////////////////////////////////////////////////////////
82
83 void BalanceRocky()
84 {
85
86     // *****Enter the control parameters here
87
88     // float Kp = 30370;
89     // float Ki = 154230;
90     // float Ci = -8709.9;
91     // float Jp = 2169.5;
92     // float Ji = -19442;
93     float Kp = 6879.2;
94     float Ki = 33267;
95     float Ci = -7847.4;
96     float Jp = 567.3923;
97     float Ji = -6306.2;
98
99
100
101
102     float v_c_L, v_c_R; // these are the control velocities to be sent to the
    ↪ motors
103     float v_d = 0; // this is the desired speed produced by the angle controller
104
105
106     // Variables available to you are:
107     // angle_rad - angle in radians
108     // angle_rad_accum - integral of angle

```

```

109 // measured_speedR - right wheel speed (m/s)
110 // measured_speedL - left wheel speed (m/s)
111 // distLeft_m - distance traveled by left wheel in meters
112 // distRight_m - distance traveled by right wheel in meters (this is the
    ↳ integral of the velocities)
113 // dist_accum - integral of the distance
114
115 // *** enter an equation for v_d in terms of the variables available ****
116 v_d = Kp*angle_rad + Ki * angle_rad_accum ; // this is the desired velocity
    ↳ from the angle controller
117
118
119
120 // The next two lines implement the feedback controller for the motor. Two
    ↳ separate velocities are calculated.
121 // v_j =
122 //
123 // We use a trick here by criss-crossing the distance from left to right and
124 // right to left. This helps ensure that the Left and Right motors are
    ↳ balanced
125
126 // *** enter equations for input signals for v_c (left and right) in terms of
    ↳ the variables available ****
127 //v_c_R = 0.84 * v_d; // CHANGE HERE TO FIX MOTORS
128 //v_c_L = 1 * v_d;
129 v_c_R = v_d - (Jp*measured_speedR + Ji*distRight_m + Ci*dist_accum);
130 v_c_L = v_d - (Jp*measured_speedR + Ji*distRight_m + Ci*dist_accum);
131
132 // save desired speed for debugging
133 desSpeedL = v_c_L;
134 desSpeedR = v_c_R;
135 Serial.println(v_d);
136
137 // the motor control signal has to be between +- 300. So clip the values to
    ↳ be within that range
138 // here
139 if(v_c_L > 300) v_c_L = 300;
140 if(v_c_R > 300) v_c_R = 300;
141 if(v_c_L < -300) v_c_L = -300;
142 if(v_c_R < -300) v_c_R = -300;
143
144 // Set the motor speeds
145 motors.setSpeeds((int16_t) (v_c_L), (int16_t)(v_c_R));
146
147 }
148
149

```

```

150
151 void setup()
152 {
153     // Uncomment these lines if your motors are reversed.
154     // motors.flipLeftMotor(true);
155     // motors.flipRightMotor(true);
156
157     Serial.begin(9600);
158     prev_time = 0;
159     displacement = 0;
160     ledYellow(0);
161     ledRed(1);
162     balanceSetup();
163     ledRed(0);
164     angle_accum = 0;
165
166     ledGreen(0);
167     ledYellow(0);
168 }
169
170
171
172 int16_t time_count = 0;
173 extern int16_t angle_prev;
174 int16_t start_flag = 0;
175 int16_t start_counter = 0;
176 void lyingDown();
177 extern bool isBalancingStatus;
178 extern bool balanceUpdateDelayedStatus;
179
180 void UpdateSensors()
181 {
182     static uint16_t lastMillis;
183     uint16_t ms = millis();
184
185     // Perform the balance updates at 100 Hz.
186     balanceUpdateDelayedStatus = ms - lastMillis > UPDATE_TIME_MS + 1;
187     lastMillis = ms;
188
189     // call functions to integrate encoders and gyros
190     balanceUpdateSensors();
191
192     if (imu.a.x < 0)
193     {
194         lyingDown();
195         isBalancingStatus = false;
196     }

```

```

197     else
198     {
199         isBalancingStatus = true;
200     }
201 }
202
203
204
205 void GetMotorAndAngleMeasurements()
206 {
207     // convert distance calculation into meters
208     // and integrate distance
209     distLeft_m =
210     ↪ ((float)distanceLeft)/((float)G_RATIO)/12.0*80.0/1000.0*3.14159;
211     distRight_m =
212     ↪ ((float)distanceRight)/((float)G_RATIO)/12.0*80.0/1000.0*3.14159;
213     ↪
214     dist_accum += (distLeft_m+distRight_m)*0.01/2.0;
215
216     // compute left and right wheel speed in meters/s
217     measured_speedL =
218     ↪ speedLeft/((float)G_RATIO)/12.0*80.0/1000.0*3.14159*100.0;
219     measured_speedR =
220     ↪ speedRight/((float)G_RATIO)/12.0*80.0/1000.0*3.14159*100.0;
221
222     prevDistLeft_m = distLeft_m;
223     prevDistRight_m = distRight_m;
224
225     // this integrates the angle
226     angle_rad_accum += angle_rad*0.01;
227     // this is the derivative of the angle
228     angle_rad_diff = (angle_rad-angle_prev_rad)/0.01;
229     angle_prev_rad = angle_rad;
230
231 }
232
233 void balanceResetAccumulators()
234 {
235     errAccumLeft_m = 0.0;
236     errAccumRight_m = 0.0;
237     speed_err_left_acc = 0.0;
238     speed_err_right_acc = 0.0;
239 }

```

```

239 void loop()
240 {
241     static uint32_t prev_print_time = 0;    // this variable is to control how
        ↳ often we print on the serial monitor
242     int16_t distanceDiff;    // this stores the difference in distance in encoder
        ↳ clicks that was traversed by the right vs the left wheel
243     static float del_theta = 0;
244     char enableLongTermGyroCorrection = 1;

245
246     cur_time = millis();    // get the current time in milliseconds
247
248
249     if((cur_time - prev_time) > UPDATE_TIME_MS){
250         UpdateSensors();    // run the sensor updates.
251
252         // calculate the angle in radians. The FIXED_ANGLE_CORRECTION term comes
        ↳ from the angle calibration procedure (separate sketch available for
        ↳ this)
253         // del_theta corrects for long-term drift
254         angle_rad = ((float)angle)/1000/180*3.14159 - FIXED_ANGLE_CORRECTION -
        ↳ del_theta;

255
256         if(angle_rad > 0.1 || angle_rad < -0.1)    // If angle is not within +- 6
        ↳ degrees, reset counter that waits for start
257         {
258             start_counter = 0;
259         }

260
261
262         if(angle_rad > -0.1 && angle_rad < 0.1 && ! start_flag)
263         {
264             // increment the start counter
265             start_counter++;
266             // If the start counter is greater than 30, this means that the angle has
        ↳ been within +- 6 degrees for 0.3 seconds, then set the start_flag
267             if(start_counter > 30)
268             {
269                 balanceResetEncoders();
270                 start_flag = 1;
271                 buzzer.playFrequency(DIV_BY_10 | 445, 1000, 15);
272                 Serial.println("Starting");
273                 ledYellow(1);
274             }
275         }

276
277
278         // every UPDATE_TIME_MS, if the start_flag has been set, do the balancing

```



```

279     if(start_flag)
280     {
281         GetMotorAndAngleMeasurements();
282         if(enableLongTermGyroCorrection)
283             del_theta = 0.999*del_theta + 0.001*angle_rad; // assume that the robot
                ↳ is standing. Smooth out the angle to correct for long-term gyro drift
284
285         // Control the robot
286         BalanceRocky();
287     }
288     prev_time = cur_time;
289 }
290 // if the robot is more than 45 degrees, shut down the motor
291 if(start_flag && angle_rad > .78)
292 {
293     motors.setSpeeds(0,0);
294     start_flag = 0;
295 }
296 else if(start_flag && angle_rad < -0.78)
297 {
298     motors.setSpeeds(0,0);
299     start_flag = 0;
300 }
301
302 // kill switch
303 if(buttonA.getSingleDebouncePress())
304 {
305     motors.setSpeeds(0,0);
306     while(!buttonA.getSingleDebouncePress());
307 }
308
309 if(cur_time - prev_print_time > 103) // do the printing every 105 ms. Don't
    ↳ want to do it for an integer multiple of 10ms to not hog the processor
310 {
311     Serial.print(angle_rad);
312     Serial.print("\t");
313     Serial.print(distLeft_m);
314     Serial.print("\t");
315     Serial.print(measured_speedL);
316     Serial.print("\t");
317     Serial.print(measured_speedR);
318     Serial.print("\t");
319     Serial.println(speedCont);
320     prev_print_time = cur_time;
321 }
322
323

```

