

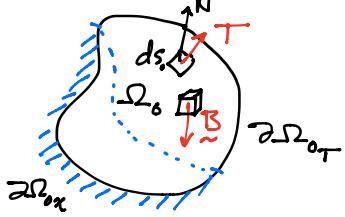
## DYNAMICS

BVP of continuum dynamics

Cons. lin. momentum

$$\hookrightarrow \nabla \cdot \underline{P} + \rho_0 \underline{B} = \rho_0 \ddot{\underline{x}} \quad \text{in } \Omega_0 \quad (*)$$

$\ddot{\underline{x}}(\underline{x}, t)$  = material acceleration



$$\underline{P} \cdot \underline{N} = \underline{T} \quad \text{on } \partial\Omega_0$$

$$\underline{x}(\underline{x}, t) = \bar{\underline{x}}(\underline{x}, t) \quad \text{on } \partial\Omega_0$$

Initial conditions:

$$\underline{x}(\underline{x}, 0) = \underline{x}_0(\underline{x}) \quad \text{init. def. mapping}$$

$$\dot{\underline{x}}(\underline{x}, 0) = \underline{v}_0(\underline{x}) \quad \text{init. material velocity}$$

Hypoplastic constitutive law:

$$\underline{P} = \frac{\partial W}{\partial \underline{x}} \quad P_{ij} = \frac{\partial w}{\partial F_{ij}}$$

Q/ How do we approximate the dynamical IBVP? Is there a variational principle?

Hamilton's Principle:

$$\text{Action: } \mathcal{I}[x] = \int_{t_1}^{t_2} \underline{L}[\underline{x}, \dot{\underline{x}}] dt$$

*Lagrangian*

$$\underline{L}[\underline{x}, \dot{\underline{x}}] = \int_{\Omega_0} \left\{ \frac{1}{2} \rho_0 |\dot{\underline{x}}|^2 - w(\nabla \underline{x}) \right\} dV_0$$

Hamilton:  $\delta I = 0$  for trajectory of system and all admissible variations

E-L equations  $\Leftrightarrow$  equations of motion (\*)

This is not a minimum principle  $\Rightarrow$  Cannot apply Rayleigh-Ritz  
But we can formulate minimum principles for dynamics by means  
of Time Discretization.

Two strategies for dynamics:

- Traditional: Discretize eqns of motion directly
- Variational: Discretize  $I$  in time  
 $\Rightarrow$  action sum + stationarity  $\rightarrow$  discrete eqns. of motion

Discretize time:  $t_0, t_1, t_2, \dots, t_n, t_{n+1} = t_n + \Delta t, \dots$

Newmark's algorithm (standard for struct. dynamics)

Denote:  $\underline{v}(\underline{x}, t) = \dot{\underline{x}}(\underline{x}, t) =$  material velocity

$\underline{a}(\underline{x}, t) = \ddot{\underline{x}}(\underline{x}, t) =$  " acceleration

Problem: given  $\{\underline{x}_n, \underline{v}_n\}$  @ time  $t_n$  ( $\Rightarrow \underline{f}_n \underline{A}_n = \nabla \cdot \underline{P}(\nabla \underline{x}_n) + \underline{g}_n \underline{B}_n$ )  
want to compute  $\{\underline{x}_{n+1}, \underline{v}_{n+1}, \underline{A}_{n+1}\}$  @  $t_{n+1}$

$$\left. \begin{array}{l}
 \text{Newmark eqns.} \quad \begin{aligned}
 X_{n+1} &= X_n + \Delta t V_n + \Delta t^2 \left[ \left( \frac{1}{2} - \beta \right) A_n + \beta A_{n+1} \right] \\
 V_{n+1} &= V_n + \Delta t \left[ (1 - \gamma) A_n + \gamma A_{n+1} \right] \\
 \nabla \cdot P(X_{n+1}) + f_0 B_{n+1} &= f_0 A_{n+1}
 \end{aligned} \right\} \quad (**)
 \end{array} \right.$$

(System of nonlinear PDEs in unknowns  $\{X_{n+1}, V_{n+1}, A_{n+1}\}$ .

$(**)$   $\rightarrow$  continuum incremental (time-discretized) problem. Apply FEM to this.

Want: a minimum principle for  $X_{n+1}$ .

Let  $X_{n+1}^{pre} = X_n + \Delta t V_n + \Delta t^2 \left( \frac{1}{2} - \beta \right) A_n$  = Newmark Predictor for  $X_{n+1}$ .

Then

$$X_{n+1} = X_{n+1}^{pre} + \underbrace{\beta \Delta t^2 A_{n+1}}_{\text{Newmark corrector for } X_{n+1}}$$

Notice  $\frac{X_{n+1} - X_{n+1}^{pre}}{\beta \Delta t^2} = A_{n+1}$  looks like a sort of discrete time derivative

Insert this into  $(**.3)$

$$\nabla \cdot P(X_{n+1}) + f_0 B_0 = f_0 \frac{X_{n+1} - X_{n+1}^{pre}}{\beta \Delta t^2}$$

The  $A_{n+1}$  term appears as a sort of body force that is linear in  $X_{n+1}$ !  
Can we derive that force from a potential?

Potential Energy extended to include inertia terms:

$$\mathcal{I}[\chi_{n+1}] = \int_{\Omega_0} \left\{ \frac{1}{2} \rho_0 \frac{|\chi_{n+1} - \chi_{n+1}^{prev}|^2}{\beta \Delta t^2} + w(\nabla \chi) \right\} dV_0 - \int_{\Omega_0} \rho_0 \mathbf{B}_{n+1} \cdot \chi_{n+1} dV_0 - \int_{\partial \Omega_{0+}} T \cdot \chi_{n+1} dA$$

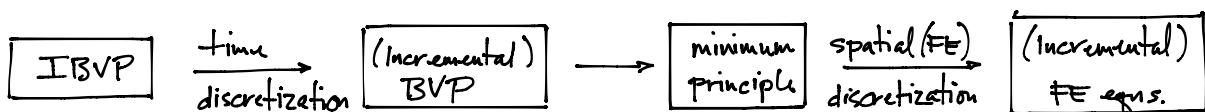
$$\min \mathcal{I} \rightarrow \delta \mathcal{I} = \int_{\Omega_0} \rho_0 \mathbf{A}_{n+1} \cdot \delta \chi_{n+1} + \frac{\partial w}{\partial F} : \nabla \delta \chi_{n+1} - \rho_0 \mathbf{B}_{n+1} \cdot \delta \chi_{n+1} dV_0 - \int_{\partial \Omega_{0+}} T \cdot \delta \chi_{n+1} dA$$

Divergence theorem,

$$\delta \mathcal{I} = \int_{\Omega_0} \left( -\nabla \cdot \mathbf{P}_{n+1} - \rho_0 \mathbf{B}_{n+1} + \rho_0 \mathbf{A}_{n+1} \right) \cdot \delta \chi_{n+1} dV_0 + \int_{\partial \Omega_{0+}} (\mathbf{P}_{n+1} \cdot \mathbf{N} - T_{n+1}) \delta \chi_{n+1} dA$$

$$\begin{array}{lll} E-L \text{ eqns.} & \nabla \cdot \mathbf{P}_{n+1} + \rho_0 \mathbf{B}_{n+1} = \rho_0 \mathbf{T}_{n+1} & \text{in } \Omega_0 \\ \text{NBes} & \mathbf{P}_{n+1} \cdot \mathbf{N} = T_{n+1} & \text{on } \partial \Omega_{0+} \end{array} \quad \begin{array}{l} \text{"Equivalent"} \\ \text{static problem} \end{array}$$

- i) E-L eqns of  $\mathcal{I}_{n+1}$  are the time-discretized eqns. of motion for  $\chi_{n+1}$ .
- ii) Assumption: minimizers define the "stable" configurations at  $t_{n+1}$
- iii) Inertia stabilizes the functional to some extent. We could stabilize more by adding viscosity. (Just wait.)



## Finite Element Discretization

Apply Rayleigh-Ritz to (\*)

$$\underline{x}(\underline{x}, t) = \sum_{a=1}^N x_a(t) \underline{N}_a(\underline{x})$$

Discrete time:

independant of time

$$\underline{x}_n(\underline{x}) = \sum_a x_a^n \underline{N}_a(\underline{x})$$

$$\underline{x}_{n+1}(\underline{x}) = \sum_a \underline{x}_a^{n+1} \underline{N}_a(\underline{x})$$

$\underline{x}_{n+1}$  (array of position DoF @  $t_{n+1}$ )

Potential energy:

$$I_{n+1}(\underline{x}_{n+1}) = \int_{\Omega} \frac{\rho_0}{2\beta \Delta t^2} \left| \sum_a (x_a^{n+1} - x_a^{pre,n+1}) N_a \right|^2 dV_0 + \int_{\Omega} w(F_{n+1}) dV_0 + F.T.$$

$$= \sum_{a,b} \frac{1}{2\beta \Delta t^2} \underbrace{\left( \int_{\Omega} \rho_0 \delta_{ik} N_a N_b dV_0 \right)}_{\text{mass matrix}} (x_{ia}^{n+1} - x_{ia}^{pre,n+1}) (x_{lb}^{n+1} - x_{lb}^{pre,n+1})$$

+ ...

$$M_{iakb} = \int_{\Omega} \rho_0 \delta_{ik} N_a N_b dV_0$$

$$R-R: \min I_{n+1} \rightarrow S I_{n+1} = 0$$

$$\underbrace{M \frac{x_{n+1} - x_{n+1}^{pre}}{2\beta \Delta t^2}}_{\underline{a}_{n+1}} + \underline{f}^{int}(x_{n+1}) - \underline{f}^{ext} = 0$$

$$x_{n+1} = x_n + \Delta t \underline{v}_n + \Delta t^2 \left[ \left( \frac{1-\beta}{2} \right) \underline{a}_n + \beta \underline{a}_{n+1} \right]$$

$$v_{n+1} = v_n + \Delta t \left[ (1-\gamma) \underline{a}_n + \gamma \underline{a}_{n+1} \right]$$

$$M \underline{a}_{n+1} + \underline{f}^{int}(x_{n+1}) = \underline{f}^{ext}_{n+1}$$

## SPECIAL CASES

$$\text{Explicit Dynamics: } f = 0 \quad \underline{x}_{n+1} = \underline{x}_{n+1}^{\text{prev}}$$

$$\underline{\alpha}_{n+1} = \underline{M}^{-1} [f_{n+1}^{\text{ext}} - f^{\text{int}}(\underline{x}_{n+1})]$$

$$\underline{\alpha}_{n+1} = \underline{\alpha}_n + \Delta t [(1-\gamma) \underline{\alpha}_n + \gamma \underline{\alpha}_{n+1}]$$

Comments:

- i) Only efficient if  $\underline{M}$  is diagonal. Then  $\underline{M}^{-1}$  is trivial.

Example: Row-sum lumping

$$M_{iia}^L = \int_V p_o N_a dV_o = \sum_b \int_V p_o N_a \underline{N_b} dV_o = \sum_b M_{iab}$$

(no sum on  $i$  or  $a$ )

$$\sum_b \underline{N_b} = 1$$

See Hughes or Zienkiewicz & Taylor for more on this.

- ii) Explicit Newmark is only conditionally stable.

Courant-Friedrichs-Lowy condition: An elastic wave should travel a distance smaller than the size of an element,  $h$ , in a time step,  $\Delta t$ .

$$\Delta x = c \Delta t < h$$

$$c = \sqrt{E/\rho} = \text{speed of sound in material}$$

Use this as a rough guide.

If you exceed stability threshold ( $\Delta t > h/c$ ) oscillations will grow without bound.

Implicit Dynamics:  $\beta \neq 0$

Newton-Raphson, "traditional" approach.

i) Initialize  $k=0$

$$x_{n+1}^{(0)} = x_{n+1}^{pr} = x_n + \Delta t v_n^- + (\frac{1}{2} - \beta) \Delta t^2 a_n$$

$$v_{n+1}^{(0)} = v_{n+1}^{pr} = v_n^- + (1-\gamma) \Delta t a_n$$

$$a_{n+1}^{(0)} = 0$$

ii) Linearize eqns about  $x_{n+1}^{(k)}, v_{n+1}^{(k)}, a_{n+1}^{(k)}$

$$x_{n+1}^{(k+1)} = x_{n+1}^{(k)} + \Delta x$$

$$v_{n+1}^{(k+1)} = v_{n+1}^{(k)} + \Delta v \quad \Delta v = \gamma \Delta t \Delta x$$

$$a_{n+1}^{(k+1)} = a_{n+1}^{(k)} + \Delta a \quad \Delta a = \Delta x / \beta \Delta t^2 \quad \left. \right\} \Delta v = \frac{\gamma}{\beta \Delta t} \Delta x$$

$$M \Delta x + \underbrace{\frac{\partial f^{int}}{\partial x}(x_{n+1}^{(k)})}_{\text{tangent stiffness}} \Delta x = f_{n+1}^{ext} - f^{int}(x_{n+1}^{(k)}) = -r(x_{n+1}^{(k)})$$

tangent stiffness

$$\text{iii) Solve } \left( \frac{1}{\beta \Delta t^2} M + K \right) \Delta x = -r(x_{n+1}^{(k)})$$

$$\text{iv) } x_{n+1}^{(k+1)} = x_{n+1}^{(k)} + \Delta x \quad v_{n+1}^{(k+1)} = \dots \quad a_{n+1}^{(k+1)} = \dots$$

v) If  $|r| > tol$   $k \leftarrow k+1$ . Go to ii)

$$\text{Else } x_{n+1} = x_{n+1}^{(k)}.$$

Unconditional Stability for  $\gamma \geq \frac{1}{2}$   $\beta \geq \frac{1}{4}(\gamma + \frac{1}{2})^2$ . (See Hughes)