

Elastic Materials

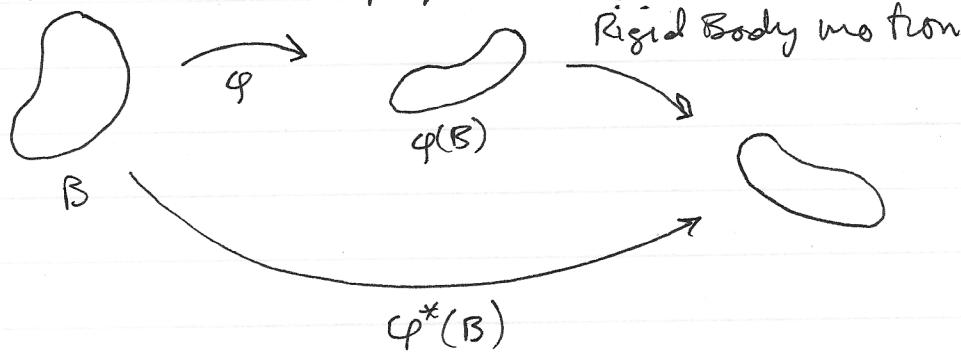
To model specific materials :

- General principles :
 - Material Frame Indifference (Objectivity)
 - Material symmetry (isotropy, etc.)
 - Internal constraints (incompress.)

- Modeling :
 - Phenomenological (fit experiments)
 - Statistical Mechanics
 - multiscale simulation/modelling
 - homogenization

Material Frame Indifference

Invariance w.r.t. superposed rigid rotations..



Ex.

i.e., nothing important should change if you tilt your head while watching the deformed body.

$$\text{Rigid Motion } x = QX + b = \varphi^R(X)$$

$$b \in \mathbb{R}^3$$

$$Q \in SO(3) = \{ Q \in \mathbb{R}^{3 \times 3} \text{ s.t. } Q^T Q = 1 \text{ & } \det Q = +1 \}$$

$$\therefore F^* = \nabla \varphi^* = \nabla \varphi^R(\varphi(X)) = Q F$$

$$w(F) \text{ is Frame indifferent / Objective} \iff \boxed{w(F) = w(QF) \quad \forall Q \in SO(3) \quad \forall F}$$

can show (cf. Holzapfel or Mal's notes)

$$w \text{ is MFI} \iff w(G) \quad G = F^T F \quad G_{ij} = F_{li} F_{lj}$$

What about Piola-Kirchhoff Stress P_{ij} ?

$$P_{ij} = \frac{\partial w}{\partial F_{ij}}(F)$$

$$w(F) = w(QF) \quad \forall Q \in SO(3)$$

$$P_{ij}^* = \frac{\partial w}{\partial F_{ij}}(QF)$$

$$F \rightarrow F + dF$$

$$w(Q(F + dF)) = w(F + dF)$$

$$\cancel{w(QF)} + \frac{\partial w}{\partial F_{ij}}(QF) Q_{ij} dF_{jj} = \cancel{w(F)} + \frac{\partial w(F)}{\partial F_{ij}} dF_{ij}$$

$$\Rightarrow P_{ij}(QF) Q_{ij} dF_{jj} = P_{ij}(F) dF_{jj}$$

$$\forall dF_{jj}$$



$$P_{ij}(QF) Q_{ij} = P_{ij}(F)$$

$$Q^T P^* = P$$

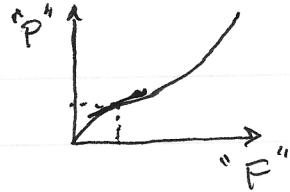
or

$$\boxed{P_{ij}(QF) = Q_{ij} P_{ij}}$$

$$P^* = Q P$$

$$\boxed{P_{ij}^* Q_{ij} Q_{kj} = P_{ij}(F) Q_{kj}}$$

In general $P(F)$ will not be linear.
 → Incremental Constitutive Relations



$$w(F) \rightarrow P_{ij} = \frac{\partial w}{\partial F_{ij}}(F)$$

$$\text{Perturb } F \rightarrow F + dF \Rightarrow P + dP$$

$$dP_{ij} = \frac{\partial P_{ij}(F)}{\partial F_{kl}} dF_{kl} = \underbrace{\frac{\partial^2 w}{\partial F_{ij} \partial F_{kl}}(F)}_{\text{Elastic Moduli}} dF_{kl}$$

$$C_{ijkl}(F) = \frac{\partial^2 w}{\partial F_{ij} \partial F_{kl}}(F) \quad \text{Lagrangian Elastic Moduli}$$

$$\text{MFI for } C_{ijkl}: \quad P_{ij}(Q(F+dF)) \otimes_{ij} = P_{jj}(F+dF)$$

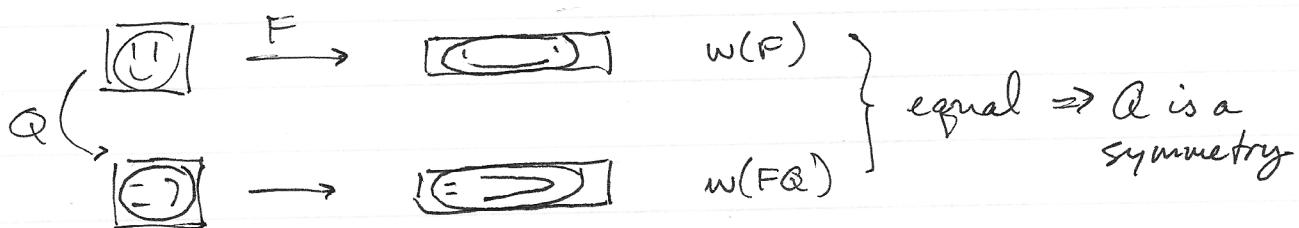
$$C_{ijkl}(QF) = Q_{im} Q_{kn} C_{mnl}(F)$$

Material Symmetry

$Q \in SO(3)$ is a symmetry of $w \Leftrightarrow w(FQ) = w(F) \forall F$

Pre-multiply w w/ $Q \Rightarrow$ Rotate, then deform.

MFI = post-mult. \Rightarrow Deform, then rotate.



If any $Q \in SO(3)$ is a symmetry \rightarrow Isotropic

Elastic material is isotropic $\Leftrightarrow w = w(I_1, I_2, I_3)$

$$\begin{cases} I_1 = \text{tr}(C) \\ I_2 = \frac{1}{2} [\text{tr}(C^2) - \text{tr}(C)^2] \\ I_3 = \det(C) = J^2 \end{cases} \quad C = F^T F$$

invariants of C form complete & irreducible set of invariants for isotropic material

Examples of Hyperelastic Materials

Biomaterials and polymers are only materials which exhibit large strain reversible behavior.

Incompressible mats. $J=1$

$$w(F) = w(F) + p(J-1)$$

$$\Rightarrow P_{ij} = \frac{\partial w}{\partial F_{ij}} + pF_{ji}^{-1}$$

$$\frac{\partial J}{\partial F_{ij}} = J^m F_{ji}^{-1}$$

Ex Neo-Hookean Mat.

$$w = \frac{\mu}{2} \text{tr}(C)$$

$$\frac{\partial w}{\partial F_{ij}} = \frac{\mu}{2} \frac{\partial}{\partial F_{ij}} \text{tr}(C) = \frac{\mu}{2} (C_{kl} \delta_{kl}) = \frac{\mu}{2} \frac{\partial}{\partial F_{ij}} (F_{mk} F_{ml} \delta_{kl})$$

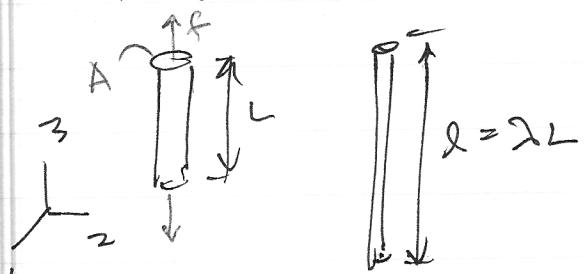
$$= \frac{\mu}{2} (\delta_{im} \delta_{jk} F_{ml} \delta_{kl} + F_{mk} \delta_{im} \delta_{jl} \delta_{kl})$$

$$= \frac{\mu}{2} (F_{ij} + F_{ji}) = \mu F_{ij}$$

$$P_{ij} = \mu F_{ij} + p J F_{ji}^{-1}$$

$$J-1 = 0$$

Tension test



$$\lambda = \text{stretch ratio} = \frac{\partial x_3}{\partial X_3} = F_{33}$$

$$P = \sigma/A \quad \text{nominal stress}$$

$$F = \begin{pmatrix} \lambda^{1/2} & 0 & 0 \\ 0 & \lambda^{1/2} & 0 \\ 0 & 0 & \lambda \end{pmatrix} \quad J = \det(F) = 1$$

$$P = \mu F + p J F^{-1} = \mu \begin{pmatrix} \lambda^{1/2} & 0 & 0 \\ 0 & \lambda^{1/2} & 0 \\ 0 & 0 & \lambda \end{pmatrix} + p J \begin{pmatrix} \lambda^{1/2} & 0 & 0 \\ 0 & \lambda^{1/2} & 0 \\ 0 & 0 & \lambda \end{pmatrix}$$

$$P_{11} = P_{22} = 0 = \mu \lambda^{1/2} + p J \lambda^{1/2} = \mu / \sqrt{2} + p / \sqrt{2}$$

$$\Rightarrow P = -\frac{\mu}{\lambda}$$

$$P_{33} = P = \mu \lambda + (-\frac{\mu}{\lambda}) \frac{\lambda^2}{2} = \mu \lambda - \frac{\mu}{2}$$

Ex 2 St. Venant - Kirchhoff Model

"Linear" hyperelastic model.

$$S_{IJ} = \lambda(E_{KK})\delta_{IJ} + 2\mu E_{IJ} = C_{IJKL}E_{KL}$$

$$\Rightarrow w(c) = \frac{1}{2}S_{IJ}E_{IJ} = \frac{1}{2}C_{IJKL}E_{IJ}E_{KL}$$

uniaxial Response

$$E = \begin{pmatrix} \lambda & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$E = \frac{1}{2}(C - I) = \frac{1}{2} \begin{pmatrix} \lambda^2 - 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

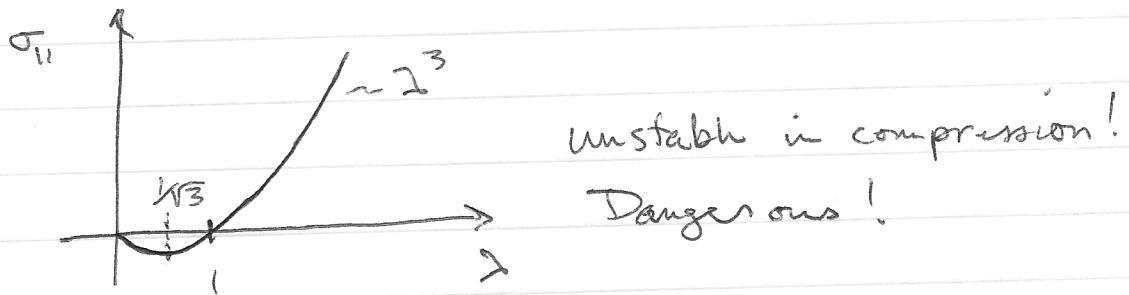
$$S_{11} = (\lambda_0 + 2\mu_0)E_{11} = \frac{\lambda_0 + 2\mu_0}{2}(\lambda^2 - 1)$$

~~$\lambda^2 = \frac{1}{2}(\lambda^3 + 1)$~~

$$\sigma_{11} = \frac{1}{2}FSF^T \Rightarrow \sigma_{11} = \lambda S_{11} = (\lambda_0 + 2\mu_0) \frac{\lambda}{2}(\lambda^2 - 1)$$

$$\lambda \rightarrow \infty \Rightarrow \sigma_{11} \rightarrow \infty \text{ Good}$$

$$\lambda \rightarrow 0 \Rightarrow \sigma_{11} \rightarrow 0 \text{ No Good}$$



Ex 3 Mooney Rivlin Materials

$$w(c) = \frac{1}{2} [\alpha_1(I_1 - 3) + \alpha_2(I_3 - 3)]$$

$$\alpha_1 = \text{const}, \quad \alpha_2 = \text{const}$$

$$J = 1 \text{ incompressible}$$

Ex 4 Neo-Hookean extended to compressible Range

$$w(C) = \frac{1}{2} \lambda_0 (\log(J))^2 - \mu_0 \log(J) + \frac{\mu_0}{2} (I_1 - 3)$$

$$I_1 = \text{tr } C \quad J = \det E \quad C = E^T E$$

Usefull Formulae:

$$\frac{\partial F_{Ji}}{\partial F_{KL}}^{-1} = -F_{JK}^{-1} F_{Li}^{-1}$$

$$\frac{\partial J}{\partial F_{ij}} = J F_{Ji}^{-1}$$

$$P_{ij} = \frac{\partial w}{\partial F_{ij}} = (\lambda_0 \log(J) - \mu_0) F_{Ji}^{-1} + \mu_0 F_{ij}$$

$$C_{ijkl} = \frac{\partial P_{ij}}{\partial F_{kl}} = \lambda_0 F_{Ji}^{-1} F_{Lk}^{-1} + \mu_0 \delta_{ik} \delta_{jl} \cancel{A(\lambda_0 \mu_0)}$$

$$- (\lambda_0 \log(J) - \mu_0) F_{Jk}^{-1} F_{Li}^{-1}$$

Uniaxial Stress-Strain Curve

$$F = \begin{pmatrix} \lambda' & 0 & 0 \\ 0 & \lambda' & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad \lambda = l/L \quad \lambda' = \text{transverse stretch ratio}$$

$$J = (\lambda')^2 \lambda$$

$$P = (\lambda_0 \log(\lambda'^2 \lambda) - \mu_0) \begin{pmatrix} V_2' & V_2' & V_2 \\ V_2' & V_2' & V_2 \\ V_2 & V_2 & 1 \end{pmatrix} + \mu_0 \begin{pmatrix} \lambda' & \lambda' & \lambda \\ \lambda' & \lambda' & \lambda \\ \lambda & \lambda & 1 \end{pmatrix}$$

Boundary Conditions: Transverse tractions = 0

$$P = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & P \end{pmatrix} = (\lambda_0 \log(\lambda'^2 \lambda) - \mu_0) \begin{pmatrix} V_2' & V_2' & V_2 \\ V_2' & V_2' & V_2 \\ V_2 & V_2 & 1 \end{pmatrix} + \mu_0 \begin{pmatrix} \lambda' & \lambda' & \lambda \\ \lambda' & \lambda' & \lambda \\ \lambda & \lambda & 1 \end{pmatrix}$$

$$J \neq 0 \Rightarrow \lambda' \neq 0 \Rightarrow 0 = [\lambda_0 \log(\lambda'^2 \lambda) - \mu_0] + \mu_0 (\lambda')^2$$

$$P = [\lambda_0 \log(\lambda'^2 \lambda) - \mu_0] V_2 + \mu_0 \lambda$$

Cauchy Stress $\underline{\sigma} = \underline{J}' \underline{P} \underline{E}^T$
 $\sigma = P / (\lambda')^2$

$$\Rightarrow \sigma = [\lambda_0 \log(\lambda'^2) + -\mu_0] + \mu_0 (\lambda')^2 \quad (*)$$

$$\lambda' = \frac{\mu_0}{\sigma} \left[\left(\frac{\lambda}{\lambda'} \right)^2 - 1 \right]$$

(*) is a nonlinear equation for λ' as a fn. of λ .
 say $f(\lambda') = 0$. Can solve with a Newton iterative procedure.

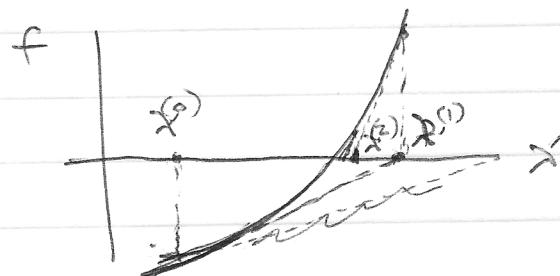
Starting $\lambda' \rightarrow f(\lambda') \neq 0$

$$f(\lambda + d\lambda) \approx f(\lambda) + \frac{df}{d\lambda}(\lambda) d\lambda$$

find $d\lambda$ s.t. $f(\lambda + d\lambda) = 0$

$$\Rightarrow f(\lambda) + \frac{df}{d\lambda}(\lambda) d\lambda = 0 \Rightarrow d\lambda = -\left(\frac{df(\lambda)}{d\lambda}\right)^{-1} f(\lambda)$$

since f non linear, have to iterate.



Solving (*) find

