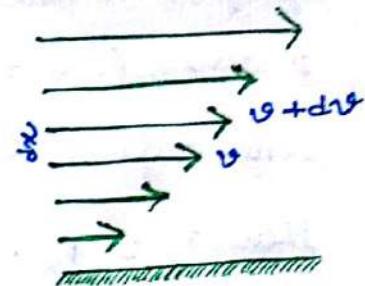


VISCOSEITY

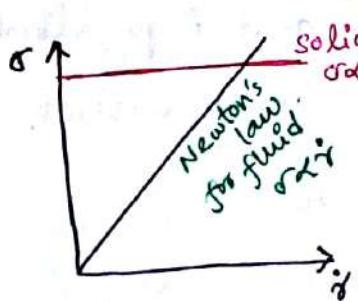
The central property that distinguishes a fluid from a solid is that, a fluid cannot sustain a "shear stress" for any period of time, meaning if a shear is applied to a fluid, it will move under the shear. Thicker liquids like paint, honey, cornstarch solution move less easily than fluids like water, glycerol or air. The measure of the ease with which a fluid yields is its viscosity.



When a liquid is at rest, we do not observe any rigidity or shape elasticity in it but when the liquid is in orderly motion (not turbulent, but streamline), there comes into play a tangential stress between any two layers of the fluid, that are moving relative to each other. Difference in velocities between these two layers gives rise to internal friction, as a result of which the faster layer tends to accelerate the slower one & vice versa.

Newton found that for a fluid moving in parallel layers, the shearing stress at any point where the velocity gradient $\frac{\partial v_x}{\partial y}$ perpendicular to the direction of motion, the frictional force F_x is proportional to area of fluid layer & $\frac{\partial v_x}{\partial y}$.

$$\therefore F_x \propto A \propto \frac{\partial v_x}{\partial y}$$

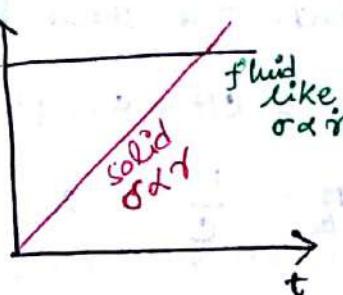


$$\therefore F_x = \eta A \frac{\partial v_x}{\partial y}$$

$$\therefore \frac{F_x}{A} = \eta \frac{\partial v_x}{\partial y}$$

$$\sigma = \eta \dot{\gamma}$$

↓ strain
rate
coefficient
of viscosity



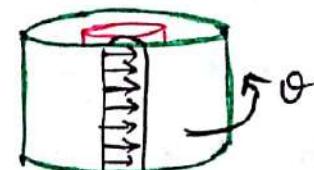
This is Newton's law of viscosity and fluid exhibiting such phenomena is called Newtonian fluid.

Compare with Hooke's law of elastic solid where stress & strain ($\sigma = Y\epsilon$, Y = Young's modulus) while for fluid stress & strain rate ($\sigma = \eta \dot{\gamma}$, η = coefficient of viscosity). If $A = 1$, $\frac{\partial v_y}{\partial x} = 1$ then $\eta = F_x$. So, coefficient of viscosity of a fluid is the tangential stress per unit velocity gradient. C.G.S. unit of η is "Poise". 1 Poise η means that a force of 1 dyne is required to maintain a velocity difference of 1 cm/sec between two layers of 1 square cm area which are 1 cm apart from each other.

$$\text{Dimension of } \eta: \quad \eta = \frac{F/A}{\frac{\partial v_y}{\partial x}}, \quad \therefore [\eta] = \frac{[MLT^{-2}]/[L]^2}{[LT^{-1}]/[L]} \\ = [ML^{-1}T^{-1}]$$

Fugitive elasticity:

Other than sliding planes geometry, Couette flow can be generated by sandwiching a liquid between two concentric cylinders with inner (outer) one stationary. From consideration of shape elasticity, tangential stress $\sigma = n\theta$ where n = modulus of rigidity and θ is the angle of shear.



$$\text{In the limit } \lim_{\theta \rightarrow 0}, \quad \sigma = n \tan \theta = n \frac{dy}{dx}$$

$$\text{from Newton's law of viscosity, } \sigma = \eta \frac{dv}{dx} = \eta \frac{d}{dx} \left(\frac{dy}{dt} \right) \\ = \eta \frac{d}{dt} \left(\frac{dy}{dx} \right) = \eta \frac{d\theta}{dt}.$$

$\frac{d\theta}{dt}$ represents the rate at which the shear brakes and is proportional to the angle of shear. $\therefore \frac{d\theta}{dt} = c\theta$, c = proportionality constant.

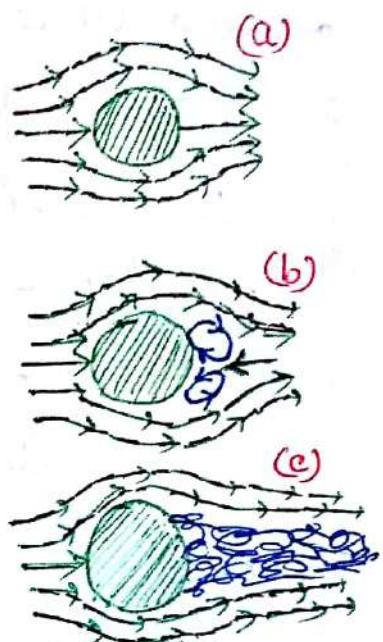
$$\therefore \sigma = \eta c\theta = n\theta \quad \text{or} \quad \eta = \frac{n}{c} \quad \therefore \eta \propto n$$

$\frac{1}{c}$ is the relaxation time of the medium fluid that measures the time taken by the shear to disappear, if force is taken off.

So the appearance of viscous force during streamline motion of a liquid is due to the existence of intermittent shear elasticity (fugitive elasticity). Maxwell stated that viscosity in a fluid is due to the existence of fugitive elasticity in it.

Streamline & Turbulent motion - Critical velocity & Reynold's number :

If fluid flow is such that magnitude & direction of velocity at any point is always same then its called a steady streamline flow. As in panel (a), no two streamlines can cross each other & the tangent to a line at any point gives the flow direction. In turbulent flow as panel (b) & (c) velocity magnitude & direction changes in irregular manner in terms of eddies, vortices, zigzag motion.



viscous flow around a circular cylinder

A difference of pressure is maintained between ends for flow of liquid through a tube (Poiseuille's flow). The layer of liquid in contact with the wall of the tube is at rest ("no-slip" condition where both normal & tangential component of velocity is zero). Velocity of the layer increases towards the axis of the tube. The streamline flow is maintained when the velocity is below a certain limit known as "Critical velocity".

When critical velocity is reached, in different parts of the liquid no layer travel in a straight line along the tube & when velocity is further increased, streamline motion is completely lost (turbulent).

Reynolds using dimensional analysis showed that in Poiseuille flow, critical velocity v is related to the fluid density ρ , radius of tube r & coefficient of viscosity η .

Suppose, $v = \text{Re}^x \eta^y r^z$ where Re = Reynold's number whose value is 1000 for narrow tubes. In general, for a liquid of high viscosity even for high velocity streamline motion is observed while for high density & wide bore of tube makes the motion turbulent.

Substituting dimensions, we have

$$[LT^{-1}] = [ML^{-1}T^{-1}]^x [ML^{-3}]^y [L]^z \\ = [M^{x+y}] [L^{-x-3y+z}] [T^{-z}]$$

Re is dimensionless number

Equating the powers of $[M]$, $[L]$ and $[T]$, we have

$$x + y = 0 \quad \left. \begin{array}{l} \\ \end{array} \right\} \quad x = 1, y = -1, z = -1$$

$$-x - 3y + z = 1 \quad \left. \begin{array}{l} \\ \end{array} \right\}$$

$$-x = -1$$

$$\therefore v = \text{Re} \eta^{\rho^{-1} r^{-1}}$$

$$\therefore \text{Re} = \frac{\rho v r}{\eta}$$

while discussing on motion of dry water, we will see that "vorticity" $\vec{\omega} = \vec{\nabla} \times \vec{v}$ follows a simple kinetic equation

$$\frac{\partial \vec{\omega}}{\partial t} + \vec{\nabla} \times (\vec{\omega} \times \vec{v}) = \frac{1}{\text{Re}} \vec{\nabla}^2 \vec{\omega}. \quad \text{This means that if}$$

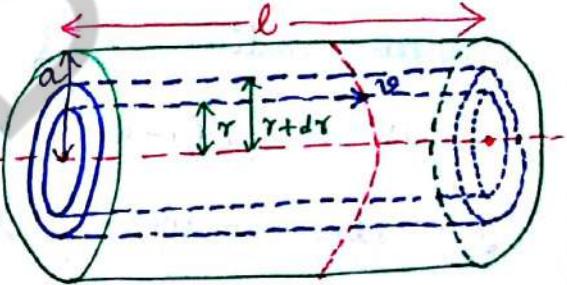
we solve the flow problem for v , for a certain cylinder with radius r , & then ask about flow for a different radius r_2 for a different fluid with velocity v_2 , the Reynold's number will be same means flows will appear same.

$$\therefore Re = \frac{\rho_1 v_1 r_1}{\eta_1} = \frac{\rho_2 v_2 r_2}{\eta_2} \text{. So we can determine the}$$

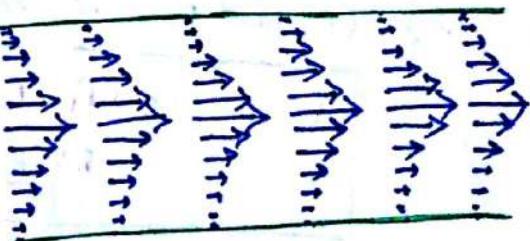
flow of air past an airplane wing without building an airplane to try but instead make a model with velocity to yield same Re . We can only apply so provided we are dealing with "incompressible" liquid & not with "compressible" gas. Otherwise speed of sound in terms of "Mach number" has to be taken into account. $Ma = \frac{\text{speed of sound in fluid}}{\text{speed of sound in air}}$. So for velocities near the speed of sound or above, the flows are the same in two situations if both "Ma" & "Re" are same for both situations.

Poiseuille's equation for flow of liquid through a horizontal narrow tube :

Consider a horizontal streamline motion of a liquid through a narrow tube. The lines are parallel to the axis of tube (no radial flow). Pressure varies along the length of tube & due to no-slip, velocity of the liquid gradually decreases radially from the axis towards the wall of the tube.



When steady state flow is attained, let v be the velocity at a distance r from the axis of tube & velocity gradient is $\frac{dv}{dr}$. So the tangential stress is $\eta \frac{dv}{dr}$. This force acts over the unit area of surface of cylinder at r in a direction opposite to the pressure gradient. So the total resisting force over the surface of the liquid cylinder is $2\pi r l \eta \frac{dv}{dr}$.



If P is the pressure difference between the ends of the tube,

then the active force is $P\pi r^2$ (As $P = \frac{F}{A} = \frac{F}{\pi r^2}$). This force tends to accelerate the liquid in cylinder and therefore in steady state, this accelerating force is balanced by the viscous retarding force,

$$P\pi r^2 = -\eta \frac{dv}{dr} 2\pi rl \quad (\because \frac{dv}{dr} < 0 \text{ as } v \text{ decreases with increasing } r)$$

$$\therefore r dr = -\frac{2\eta l}{P} dv$$

Integrating with the Boundary condition (B.C.) $v=0$ at $r=a$,

$$\int_r^a r dr = -\frac{2\eta l}{P} \int_{a^2}^0 dv \Rightarrow v = \frac{P}{4\eta l} (a^2 - r^2)$$

This is an equation for parabola. Now if dV is the volume of liquid that flows through the cylindrical shell per unit time between radius r & $r+dr$ then

$$dV = [\pi(r+dr)^2 - \pi r^2]v = 2\pi r dr v = \frac{\pi P}{2\eta l} (a^2 - r^2) r dr$$

\therefore Total volume of liquid passing through the tube per unit time

$$\begin{aligned} \therefore V &= \frac{\pi P}{2\eta l} \int_r^a (a^2 - r^2) r dr = \frac{\pi P}{2\eta l} \left(a^2 \int_r^a r dr - \int_r^a r^3 dr \right) \\ &= \frac{\pi P}{2\eta l} \left(\frac{a^4}{2} - \frac{a^4}{4} \right) = \frac{\pi P a^4}{8\eta l} \end{aligned}$$

If P_1 and P_2 are the pressure at two ends of the tube then

$$V = \frac{\pi (P_1 - P_2) a^4}{8\eta l}$$

This is known as Poiseuille's equation

Correction to Poiseuille's formula :

Poiseuille's equation $V = \frac{\pi P a^4}{8\eta l}$ is approximately true because two important factors are not taken into account. (a) pressure difference P is utilized partly in communicating kinetic energy to the liquid (b) acceleration of the liquid along the axis of the tube is neglected.

A finite acceleration at inlet of the tube becomes zero only after traversing a finite distance, so $1.64a$ is added to the length l . To find the kinetic energy correction, let's consider that ϕ is the effective pressure difference that overcomes viscosity.

The workdone against viscous force per unit time is ρV
 & Kinetic energy per unit time is $= \int_0^a \frac{1}{2} \rho 2\pi r dr v \cdot v^2$

$$= \int_0^a \rho \pi r^3 dr = \int_0^a \rho \pi \left(\frac{\phi}{4\eta l}\right)^3 (a^2 - r^2)^3 r dr = \rho \pi \left(\frac{\phi}{4\eta l}\right)^3 \int_0^a (a^2 - r^2)^3 r dr$$

$$= \rho \pi \left(\frac{\phi}{4\eta l}\right)^3 \frac{a^8}{8}. \quad \text{So total loss of energy} = \phi V + \rho \pi \left(\frac{\phi}{4\eta l}\right)^3 \frac{a^8}{8}$$

and this is equal to PV

$$\therefore PV + \rho \pi \left(\frac{\phi}{4\eta l}\right)^3 \frac{a^8}{8} = PV$$

$$\therefore \phi V + \frac{\rho}{\pi^2 a^4} \left(\frac{\pi \rho a^4}{8\eta l}\right)^3 = PV$$

$$\therefore \phi V + \frac{\rho V^3}{\pi^2 a^4} = PV \quad (\because V = \frac{\pi \rho a^4}{8\eta l})$$

$$\therefore \phi = P - \frac{\rho V^2}{\pi^2 a^4}$$

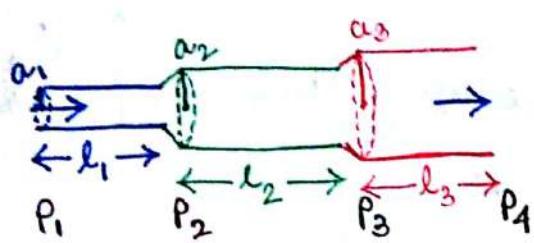
Experimentally it was found by Hagenbach, Couette & Wilberforce that correct form is $\phi = P - \frac{R \rho V^2}{\pi^2 a^4}$ with $R \approx 1$, differing for different scenario.

Corrected Poiseuille's formula is

$$V = \frac{\pi a^4}{8\eta(l+1.64a)} \left(P - \frac{R \rho V^2}{\pi^2 a^4}\right)$$

Flow of liquid through capillaries in series & parallel

Poiseuille's formula $V = \frac{P}{8\eta l/\pi a^4} = \frac{P}{R}$ can be compared with Ohm's law for flow of electric current through a resistance $i = \frac{E}{R}$. So the rate of flow of the liquid V corresponds to current i , pressure difference P to the potential difference E and $\frac{8\eta l}{\pi a^4}$ to the resistance R .



Consider a series connection of three capillaries with radius a_1, a_2, a_3 & length l_1, l_2, l_3 . Let P_1 & P_4 are the pressure at extreme ends & P_2, P_3 are

pressure at the junctions. As there is no accumulation of the liquid at the junction, so V must be equal through all capillaries, just like current is same through any resistance connected in series.

$$\text{So, } V = \frac{\pi(P_1 - P_2)a_1^4}{8\eta l_1} = \frac{\pi(P_2 - P_3)a_2^4}{8\eta l_2} = \frac{\pi(P_3 - P_4)a_3^4}{8\eta l_3}$$

$$\left. \begin{aligned} P_1 - P_2 &= \frac{8\eta l_1 V}{\pi a_1^4} \\ P_2 - P_3 &= \frac{8\eta l_2 V}{\pi a_2^4} \\ P_3 - P_4 &= \frac{8\eta l_3 V}{\pi a_3^4} \end{aligned} \right\}$$

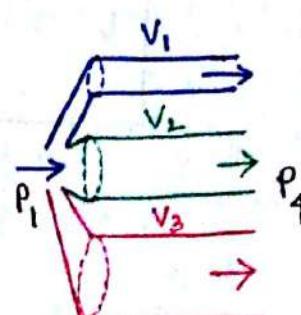
$$\text{Summing, } P_1 - P_4 = \frac{8\eta V}{\pi} \left[\frac{l_1}{a_1^4} + \frac{l_2}{a_2^4} + \frac{l_3}{a_3^4} \right]$$

$$\text{or } V = \frac{\pi P}{8\eta} \left[\frac{l_1}{a_1^4} + \frac{l_2}{a_2^4} + \frac{l_3}{a_3^4} \right]^{-1} \quad \text{--- (1)}$$

where $P = P_1 - P_4$ is pressure difference across

composite slab.

If we maintain $P = P_1 - P_4$ across ends of three capillaries connected in parallel, then volume of liquid flowing per unit time through them is $V = V_1 + V_2 + V_3 = \frac{\pi Pa_1^4}{8\eta l_1} + \frac{\pi Pa_2^4}{8\eta l_2} + \frac{\pi Pa_3^4}{8\eta l_3}$

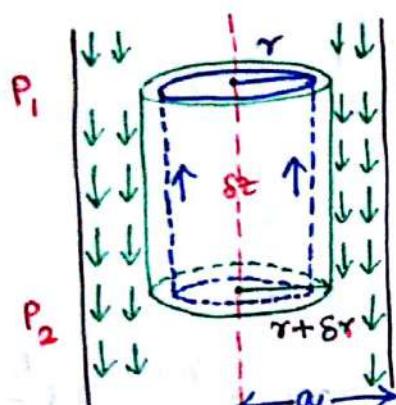


$$V = \frac{\pi P}{8\eta} \left(\frac{a_1^4}{l_1} + \frac{a_2^4}{l_2} + \frac{a_3^4}{l_3} \right) = P \left(\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} \right) \quad \text{--- (2)}$$

Comparing (1) and (2) we recover the effective resistance for an equivalent series connected viscous flow as $R = R_1 + R_2 + R_3$ while for parallel connected, $\frac{1}{R} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3}$ where

$$R_1 = \frac{8\eta l_1}{\pi a_1^4}, \quad R_2 = \frac{8\eta l_2}{\pi a_2^4}, \quad R_3 = \frac{8\eta l_3}{\pi a_3^4}.$$

Downward flow of a liquid through a vertical narrow tube:



Consider a vertical narrow tube through which a liquid flows steadily. Consider a cylindrical shell with radius r & $r + \delta r$ and length δz . So the viscous force on the inner shell wall in vertical upward direction is $2\pi r \delta z \eta \frac{dv}{dr}$. Viscous force on the outer wall in vertical downward direction is $2\pi r \delta z \eta \frac{dv}{dr} + \frac{d}{dr}(2\pi r \delta z \eta \frac{dv}{dr}) \delta r$.

Force due to pressure p on the upper annular flat surface of the element of the liquid cylinder in the vertical downward direction is $2\pi r \delta z p$ & similarly force due to pressure on the lower annular flat surface of the liquid cylinder in the upward direction is $2\pi r \delta z (p + \frac{dp}{dz} \delta z)$

At steady state, liquid acceleration = 0, resultant downward force is zero.

$$\therefore -2\pi r \delta z \eta \frac{dv}{dr} + 2\pi r \delta z \eta \frac{dv}{dr} + \frac{d}{dr}(2\pi r \delta z \eta \frac{dv}{dr}) \delta r + 2\pi r \delta z p - 2\pi r \delta z (p + \frac{dp}{dz} \delta z) = 0$$

$$\therefore 2\pi r \delta z \eta \frac{d}{dr} \left(r \frac{dv}{dr} \right) + 2\pi r \delta z \delta z p - 2\pi r \delta z \frac{dp}{dz} \delta z = 0$$

[Vertical downward force due to weight of cylindrical shell]

$$\text{or, } \eta \frac{d}{dr} \left(r \frac{dv}{dr} \right) + \rho g = r \frac{dp}{dz} \quad [\because \eta \neq \eta(r)]$$

$$\therefore \frac{dp}{dz} = \frac{\eta}{r} \frac{d}{dr} \left(r \frac{dv}{dr} \right) + \rho g. \quad - \frac{P_1 - P_2}{l} = \frac{\eta}{r} \frac{d}{dr} \left(r \frac{dv}{dr} \right) + \rho g$$

$$\therefore \left(\rho g + \frac{P_1 - P_2}{l} \right) r = -\eta \frac{d}{dr} \left(r \frac{dv}{dr} \right)$$

Integrating with B.C. $r=a, v=0$

$$\left(\rho g + \frac{P_1 - P_2}{l} \right) \frac{r^2}{2} + A = -\eta r \frac{dv}{dr}$$

$$\text{Integrating once again, } \left(\rho g + \frac{P_1 - P_2}{l} \right) \frac{r^2}{4} + A \ln r + B = -\eta v$$

at $r=0, v \neq \infty$ (remember $\ln 0 = -\infty$), A must be zero. & substituting $r=a, v=0$. $B = -\left(\rho g + \frac{P_1 - P_2}{l} \right) \frac{a^2}{4}$

$$\therefore \eta v = \left(\rho g + \frac{P_1 - P_2}{l} \right) \left(\frac{a^2 - r^2}{4} \right)$$

So the volume of liquid flowing per unit time is

$$V = \int_0^a 2\pi r dr v = \frac{\pi}{2\eta} \left(\rho g + \frac{P_1 - P_2}{l} \right) \int_0^a (a^2 - r^2) r dr = \frac{\pi a^4}{8\eta} \left(\rho g + \frac{P_1 - P_2}{l} \right)$$

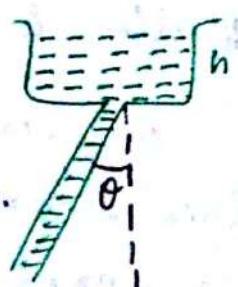
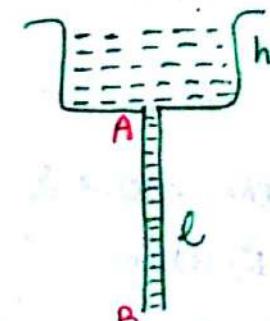
In liquid viscometer, a narrow tube is connected to a liquid container. $P_1 = \pi + \rho gh$ is the pressure at inlet A and $P_2 = \pi$ is the pressure at outlet B where π is the barometric pressure.

$$\therefore V = \frac{\pi a^4}{8\eta} \left(\rho g + \frac{\rho gh}{l} \right) = \boxed{\frac{\pi a^4}{8\eta l} \rho g (l+h)}$$

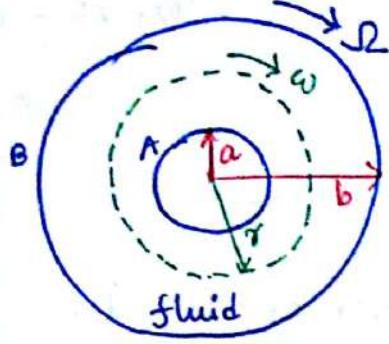
For inclined liquid viscometer, acceleration due to gravity g has $g \cos \theta$ component along vertical direction.

$$\text{So, } V = \frac{\pi a^4}{8\eta} \left(\rho g \cos \theta + \frac{P_1 - P_2}{l} \right) = \frac{\pi a^4}{8\eta} \left(\rho g \cos \theta + \frac{\rho gh}{l} \right)$$

$$= \boxed{\frac{\pi a^4}{8\eta l} \rho g (l \cos \theta + h)}$$



Torque on a cylinder immersed in a rotating fluid



A viscous liquid is filled within two coaxial cylinders A & B with cylinder B rotating about common axis with constant angular velocity Ω . The torque on A due to rotation B is required. The innermost layer of fluid at A is zero velocity (no-slip), a, b, l are the radii of A & B cylinder and length. Suppose the fluid at a distance r rotates with angular velocity ω . Its linear velocity is $r\omega$ and velocity gradient

$$\text{is } \frac{d}{dr}(r\omega) = r \frac{d\omega}{dr} + \omega \stackrel{\text{no viscosity effect.}}{\rightarrow}$$

∴ Viscous force on the side of fluid cylinder is

$$F = \eta 2\pi r l r \frac{d\omega}{dr} \text{ & then the viscous torque } \Gamma = F \cdot r \\ = 2\pi \eta l r^3 \frac{d\omega}{dr}$$

As the fluid rotates in steady state, torque on inner cylinder is in clockwise direction

$$\Gamma \text{ or } \Gamma \frac{dr}{r^3} = 2\pi \eta l d\omega$$

$$\text{Integrating, } r \int_a^b \frac{dr}{r^3} = 2\pi \eta l \int_0^l d\omega$$

$$\text{or } \frac{1}{2} \left(\frac{1}{a^2} - \frac{1}{b^2} \right) = 2\pi \eta l \Omega \quad \text{or}$$

$$\boxed{\Gamma = \frac{4\pi \eta l \Omega a^2 b^2}{b^2 - a^2}}$$

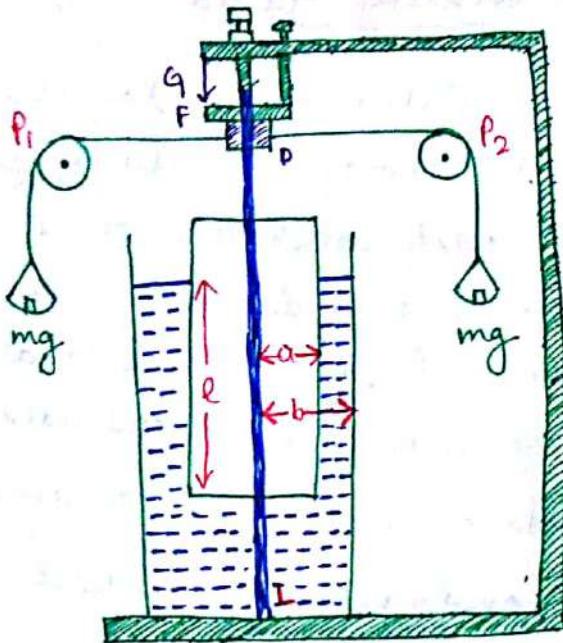
Suppose now A rotates with Ω & Γ is the clockwise torque

$$\Gamma = -2\pi \eta l r^3 \frac{d\omega}{dr} \quad (\Gamma < 0 \text{ as } \frac{d\omega}{dr} < 0 \text{ as } \omega \text{ decreases with increasing } r)$$

$$\therefore -\Gamma \int_a^b \frac{dr}{r^3} = 2\pi \eta l \int_\Omega^0 d\omega \quad \text{or } \frac{1}{2} \left(\frac{1}{b^2} - \frac{1}{a^2} \right) = -2\pi \eta l \Omega$$

$$\text{or } \boxed{\Gamma = \frac{4\pi \eta l \Omega a^2 b^2}{b^2 - a^2}}$$

Searle's viscometer uses this technique for measurement of η of highly viscous liquids. Two weights rotate the inner



Searle's viscometer

cylinder by ball-bearing pulleys while the outer cylinder is fixed with the fluid in between. We know

$$\tau = \frac{4\pi\eta l D^2 a^2 b^2}{b^2 - a^2} = mgd$$

where d = diameter of drum D.

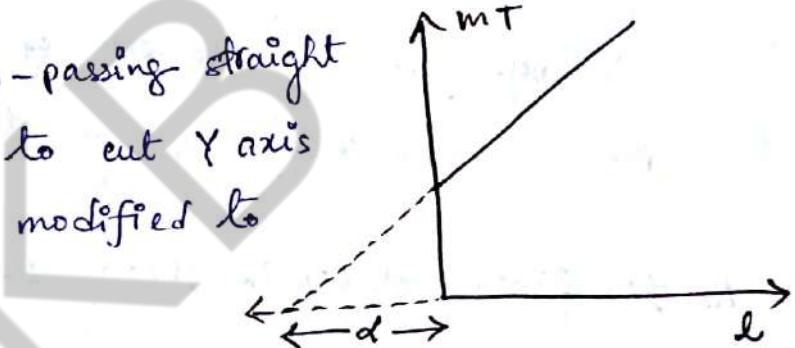
$$\therefore \eta = \frac{gd(b^2 - a^2)}{4\pi D^2 a^2 b^2} \frac{m}{l} \text{ and as}$$

$T = \frac{2\pi}{\Omega}$ is the time period of rotation

$$\eta = \frac{gd(b^2 - a^2)}{8\pi^2 a^2 b^2} \frac{mT}{l}. \text{ for a given liquid, } \frac{mT}{l} = \text{constant}$$

Though it should be a origin-passing straight line, but experimentally found to cut Y axis so that the above expression is modified to accommodate

$$\eta = \frac{gd(b^2 - a^2)}{8\pi^2 a^2 b^2} \frac{mT}{l + d}$$



Viscosity of high viscous liquids

Stoke's law : Viscous resisting force on a small sphere falling through a liquid of infinite extent is $F = 6\pi\eta arv$ where v = terminal velocity of the sphere, a = radius.

viscous retarding force = effective gravitational force.

$$\frac{4}{3}\pi a^3 (\rho - \sigma) g = 6\pi\eta arv, \begin{cases} \rho = \text{density of the sphere} \\ \sigma = \text{density of the liquid.} \end{cases}$$

$$\therefore \eta = \frac{2}{9} \frac{a^2 (\rho - \sigma) g}{v}$$

In practice in cylindrical vessel due to confinement, boundary effect due to wall & bottom of cylinder is corrected to yield

$$\eta = \frac{2}{9} \frac{a^2 (\rho - \sigma) g}{\nu (1 + 2.4 \frac{a}{R}) (1 + 3.3 \frac{a}{h})} \quad R = \text{radius of cylinder}, \quad h = \text{height of liquid.}$$

Using dimensional analysis $F = 6\pi\eta a v$ can be deduced as

$$F = K a^x \eta^y v^z, \quad K = \text{dimensionless number.}$$

$$\propto [MLT^{-2}] = [L]^x [ML^{-1}T^{-1}]^y [LT^{-1}]^z = M^y L^{x-y+z} T^{-y-z}$$

equating the powers of M, L, T , $y=1, x-y+z=1, -y-z=-2$

$$\therefore x=y=z=1 \quad \therefore F = K \eta a v$$

By solving $\eta \nabla^2 \vec{v} - \vec{\nabla} p = 0$ for a sphere in a liquid with incompressibility constraint $\vec{\nabla} \cdot \vec{v} = 0$, Stokes calculated $K = 6\pi$.

$$\therefore F = 6\pi\eta a v.$$

Observe that from $v = \frac{2}{9} \frac{ga^2(\rho - \sigma)}{\eta}$, $v \propto a^2$. For raindrop of radius $a = 10^{-3}$ cm falling through air with $\eta = 1.8 \times 10^{-4}$ poise terminal velocity $v = \frac{2 \times 981 \times 10^{-6}}{9 \times 1.8 \times 10^{-4}} = 1.2 \text{ cm/sec.}$

$$\rho = 1, \sigma \rightarrow 0 \text{ for air.}$$

That is why raindrops fall with slow rate. $v \neq f(p)$ as $\eta \neq \eta(p)$. Notice also that it's independent of mass.

Bigger raindrops fall rapidly through air as Stoke's law does not hold if $a > 0.01$ cm because of turbulence, where $F \propto \sqrt{v}$.

If $\sigma > \rho$ then $v < 0$ meaning if density of fluid > density of body, then body moves through the fluid in the upward direction. This is the reason, why air bubbles in water or in any other liquid rise up.

Equation of motion of a body falling through a viscous medium

Viscous force \propto velocity (instantaneous), but now we have downward force mg due to gravity for sedimentation & no thermal (Brownian) force.

$$m \frac{d^2x}{dt^2} = mg - f = mg - \gamma \frac{dx}{dt}$$

$$\therefore \frac{d}{dt} \left(\frac{dx}{dt} \right) = g - \frac{\gamma}{m} \frac{dx}{dt} \quad \therefore \frac{dv}{dt} = g - \frac{\gamma}{m} v$$

$$\therefore \frac{dv}{g - \frac{\gamma}{m} v} = dt \quad \therefore -\frac{m}{\gamma} \frac{d(g - \frac{\gamma}{m} v)}{g - \frac{\gamma}{m} v} = dt$$

$$\therefore \int \frac{d(g - \frac{\gamma}{m} v)}{g - \frac{\gamma}{m} v} = -\frac{\gamma}{m} \int dt + C$$

$$\therefore \ln(g - \frac{\gamma}{m} v) = -\frac{\gamma}{m} t + C. \quad \text{Now substitute the boundary condition, } t=0, v=0 \quad \therefore C = \ln g.$$

$$\therefore \ln(1 - \frac{\gamma v}{mg}) = -\frac{\gamma t}{m} \quad \therefore v = \frac{mg}{\gamma} (1 - e^{-\frac{\gamma t}{m}}). \\ \approx \frac{mg}{\gamma} \quad (\text{if } \frac{\gamma t}{m} \gg)$$

So the maximum (terminal) velocity is $v = mg/\gamma$

$$\text{Again, } \frac{dx}{dt} = \frac{mg}{\gamma} (1 - e^{-\frac{\gamma t}{m}})$$

$$\text{Integrating, } x = \frac{mg}{\gamma} \left(t + \frac{m}{\gamma} e^{-\frac{\gamma t}{m}} \right) + C'. \quad \text{Again substitute the B.C. at } t=0, x=0.$$

$$\therefore C' = -\frac{m^2 g}{\gamma^2}$$

$$\therefore x = \frac{mg}{\gamma} \left(t + \frac{m}{\gamma} e^{-\frac{\gamma t}{m}} \right) - \frac{m^2 g}{\gamma^2} \\ = \frac{mgt}{\gamma} + ge^{-\frac{\gamma t}{m}} - \frac{m^2 g}{\gamma^2}$$

Flow of Gas through a narrow tube

Unlike incompressible liquids (density is independent of pressure), gas is compressible (density \propto pressure). So for a liquid, volume flowing through any cross-section in a given time is constant while for a gas, mass flowing through a cross-section in a given time is constant.

$$\therefore \rho \propto P \text{ & } \rho V = \text{constant} \quad \text{or} \quad PV = \text{constant} \quad (\text{Boyle's law})$$

Let us consider an elemental length dx with pressure difference dP within the tube, & is small compared to the tube so that density variation within $dx \ll\ll$ so that we can still write Poiseuille's equation for flowing liquid

$$V = - \frac{\pi a^4}{8\eta} \frac{dP}{dx}. \quad \text{It's negative because } \frac{dP}{dx} < 0 \text{ so that } V > 0$$

If P_1 & P_2 are pressure of gas at inlet & outlet end with V_1 volume entering per unit time, then

$$P_1 V_1 = PV = -P \frac{\pi a^4}{8\eta} \frac{dP}{dx}$$

$$\text{or } \int_0^l P_1 V_1 dx = - \frac{\pi a^4}{8\eta} \int_{P_1}^{P_2} P dP = - \frac{\pi a^4}{8\eta} \frac{P_2^2 - P_1^2}{2}$$

$$\text{or } P_1 V_1 l = \frac{\pi a^4 (P_1^2 - P_2^2)}{16\eta} \quad \text{or} \quad P_1 V_1 = \frac{\pi a^4 (P_1^2 - P_2^2)}{16\eta l}$$

$$\text{and } \eta = \frac{\pi a^4 (P_1^2 - P_2^2)}{16 P_1 V_1 l}. \quad \text{Here we have assumed "no-slip"}$$

or no relative motion between tube wall & adjacent gas layers, which breaks down at low pressure. The corrected form

$$\therefore \eta = \frac{\pi a^4 (P_1^2 - P_2^2)}{16 P_1 V_1 l} \left(1 + \frac{4\lambda}{a}\right) - \frac{\rho V_1}{8\pi l} (K + \ln \frac{P_1}{P_2})$$

λ = slipping coefficient (constant for gas) & K depends on apparatus.

Dependence of Viscosity on pressure & temperature

Liquids: η of liquids increases rapidly with pressure. However for water, glycerol, η decreases with pressure. η decreases rapidly with increase in temperature. For pure liquids $\eta = \frac{A}{(1+BT)^n}$ with A,B,n depending on nature of liquid. For liquid mixture there is no one recipe.

Gases: Using kinetic theory of gases & experiment, established in

- (i) At high pressures, η increases with pressure increment.
- (ii) At moderate pressures, η is independent of pressure.
- (iii) At low pressures, $\eta \propto P$.

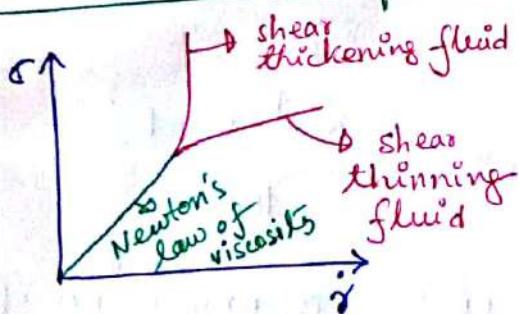
(i) At high temperature, η rapidly increases with temperature & for Mercury $\eta = \alpha T^{1.6}$ (Kinetic theory $\eta = KT^{0.5}$).

(ii) At moderate temperature, $\eta = \eta_0 \frac{\alpha T^{0.5}}{1 + \frac{S}{T}}$, η_0 is at 0°C

$$\alpha, S = \text{constants}$$

(iii) At low temperature, no one formula agrees well.

Non-Newtonian liquids



$\sigma \propto \dot{\gamma}$ is thixotropic fluid

sol \leftrightarrow gel transition, both property of solid & fluid \rightarrow Glass!!

Examples: shear thinning \rightarrow "colloid"
e.g. paint, milk, blood.

Shear thickening: cornstarch solvent, molten chocolate.



Displacement of fluid particles are usually non-affine even if Couette flow is established with linear flow profile.

Fluid Motion

Ideal Fluids - The flow of "dry" water

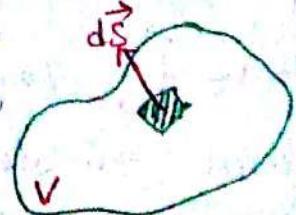
Fluid dynamics concerns with the motion of fluids (liquid & gas) in a macroscopic sense to regard as a continuous medium. Infinitely small elements of volume - fluid particle & point in a fluid means very small compared to volume of body but large compared to the molecular distance.

The Equation of Continuity: Mathematically, the state of a moving fluid is given by the fluid velocity distribution over space & time, $\vec{v} = \vec{v}(x, y, z, t)$ and of any two thermodynamic quantities, say, pressure $p(x, y, z, t)$ and density $\rho(x, y, z, t)$. So if given 3-components of velocity, pressure & density, state of the fluid is completely determined. Additionally, a conducting fluid will carry an electric current whose density $\vec{j} = \vec{j}(x, y, z, t)$. Similarly temperature or Magnetic field have similar effect.

We neglect first EM field, temperature variation & assume that density is constant or variation in pressure is very small (or the fluid is incompressible). So if the flow velocity is much less than the speed of sound wave in the fluid, density variation can be neglected.

$$\rho = \text{constant}$$

Conservation of Mass: If matter flows away then there must be decrease in the amount of matter left behind. The mass of fluid flowing in unit time through a surface element $d\vec{s}$ bounding the volume is $\rho \vec{v} \cdot d\vec{s}$ & its positive if flowing out (negative otherwise), so that the total mass is $\oint \rho \vec{v} \cdot d\vec{s}$



Decrease in fluid mass per unit time is $-\frac{\partial}{\partial t} \int \rho dV$.

Therefore $\frac{\partial}{\partial t} \int_V \rho dV = - \oint_S \rho \vec{v} \cdot d\vec{s} = \int_V \vec{\nabla} \cdot (\rho \vec{v}) dV$ using.

Green's theorem. $\therefore \int_V \left[\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v}) \right] dV = 0$. Since this equation must hold for any volume V , the integrand must vanish. So

$$\boxed{\frac{\partial \rho}{\partial t} + \vec{\nabla} \cdot (\rho \vec{v}) = 0}$$

$\vec{j} = \rho \vec{v}$ = mass flux density.

This is the hydrodynamic equation of continuity leading to conservation of mass. For incompressible fluid $\rho = \text{constant}$ & so $\vec{\nabla} \cdot \vec{v} = 0$. Like magnetic field \vec{B} , fluid velocity has zero divergence.

Euler's equation of motion: Change of velocity due to forces, torques, so that Newton's 2nd law become,

Rate of increase of momentum = Sum of forces of fluid particle on fluid particle.

There are 2 types of forces on fluid particles,

- Surface forces \Rightarrow - pressure force, viscous force, gravity force
- Body forces \Rightarrow - centrifugal force, Coriolis force, EM force.

So total force acting on the volume = $-\oint_S \vec{P} d\vec{S} = -\int_V \vec{\nabla} P dV$

So fluid surrounding any volume element dV exerts a force $-\vec{\nabla} P dV$ or $-\vec{F}$ per unit volume. There are external forces like electromagnetic, gravity. For conservative force with ϕ = potential per unit mass, $-\rho \vec{\nabla} \phi$ = force density, otherwise for non-conservative force \vec{f}_{ext} has to be taken care. Due to shearing stress in a flowing fluid, there are internal force per unit volume \vec{f}_{visc} , so that Newton's law become,

$$\rho \frac{d\vec{v}}{dt} = -\vec{\nabla}p - \rho \vec{\nabla}\phi + f_{visc} \xrightarrow{\text{dry water/ thin liquid}} \text{(inviscid flow)}$$

The derivative $\frac{d\vec{v}}{dt}$ denotes not the change of rate of the fluid velocity at a fixed point in space but the rate of change of the velocity of a given fluid particle as it moves about in space. So to express $\frac{d\vec{v}}{dt}$ in terms of quantities referring to fixed in-space we see composition from two parts, ① change during dt in the velocity at a fixed point in space, ② velocity difference at same instant at two points $d\vec{r}$ apart.

$$\begin{aligned}\therefore \rho \frac{d\vec{v}}{dt} &= \rho \frac{\partial \vec{v}}{\partial t} + \frac{\rho}{dt} \left(dx \frac{\partial \vec{v}}{\partial x} + dy \frac{\partial \vec{v}}{\partial y} + dz \frac{\partial \vec{v}}{\partial z} \right) \\ &= \rho \frac{\partial \vec{v}}{\partial t} + \rho \left(\frac{d\vec{r}}{dt} \cdot \vec{\nabla} \right) \vec{v} = \rho \partial_t \vec{v} + \rho (\vec{v} \cdot \vec{\nabla}) \vec{v}\end{aligned}$$

Note that there can be acceleration even though $\frac{\partial \vec{v}}{\partial t} = 0$ so that velocity at a given point is not changing, e.g. water flowing in a circle at constant speed is accelerating due to change in direction of the centripetal acceleration.

$$\therefore \frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{\nabla}) \vec{v} = -\frac{\vec{\nabla}p}{\rho} - \vec{\nabla}\phi$$

Euler's
Equation

If we define $\vec{\Omega} = \vec{\nabla} \times \vec{v}$, then using the vector identity

$$(\vec{v} \cdot \vec{\nabla}) \vec{v} = (\vec{\nabla} \times \vec{v}) \times \vec{v} + \frac{1}{2} \vec{\nabla} (\vec{v} \cdot \vec{v}) = \vec{\Omega} \times \vec{v} + \frac{1}{2} \vec{\nabla} v^2$$

$$\therefore \frac{\partial \vec{v}}{\partial t} + \vec{\Omega} \times \vec{v} + \frac{1}{2} \vec{\nabla} v^2 = -\frac{\vec{\nabla} p}{\rho} - \vec{\nabla}\phi$$

$\vec{\Omega}$ is called the "vorticity" & for an irrotational flow, $|\vec{\Omega}| = 0$

Circulation of a vector field around any arbitrary closed loop in a fluid at a given instant is

$$\text{Circulation } \Gamma = \oint_C \vec{v} \cdot d\vec{l} \quad (\text{line integral})$$

Circulation = $\int_{\Gamma} \vec{\nabla} \times \vec{v} \cdot d\vec{s}$ (using Stoke's theorem)
 $= \int_S \vec{\Omega} \cdot d\vec{s}$. So vorticity $\vec{\Omega}$ is the circulation around a unit area & perpendicular to the direction of $\vec{\Omega}$.

Conservation of circulation:

Change in circulation around a "fluid contour" moving over space = $\frac{d}{dt} \oint_C \vec{v} \cdot d\vec{l}$ = $\oint_C \frac{d\vec{v}}{dt} \cdot d\vec{l} + \oint_C \vec{v} \cdot \frac{d\vec{l}}{dt}$

Now $\vec{v} \cdot \frac{d\vec{l}}{dt} = \vec{v} \cdot \delta \frac{d\vec{l}}{dt} = \vec{v} \cdot \delta \vec{v} = \frac{1}{2} \delta(v^2)$. and then $\oint_C \frac{1}{2} \delta(v^2) = 0$ as total differential along closed contour = 0.

$$\begin{aligned} \therefore \frac{d\Gamma}{dt} &= \oint_C \frac{d\vec{v}}{dt} \cdot d\vec{l} = \oint_C \left(\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{\nabla}) \vec{v} \right) \cdot d\vec{l} \\ &= - \oint_C \vec{\nabla} \left(\frac{P + \phi}{\rho} \right) \cdot d\vec{l} \quad (\text{Using Euler's equation}) \\ &= - \oint_S \vec{\nabla} \times \vec{\nabla} \left(\frac{P + \phi}{\rho} \right) \cdot d\vec{S} = 0. \end{aligned}$$

$\therefore \oint \vec{v} \cdot d\vec{l} = \text{constant}$ (Kelvin's theorem of conservation of circulation)

So for irrotational flow, $\frac{\partial \vec{v}}{\partial t} = 0$ & so $\vec{\nabla} \cdot \vec{v} = 0$ & $\vec{\nabla} \times \vec{v} = 0$. It is also called "Potential flow". As $\vec{\nabla} \times \vec{v} = 0$ on streamlines, steady flow past any body with a uniform incident flow at infinity must be a potential flow.

Bernoulli's theorem from Euler's equation, taking $\vec{v} \cdot$ operation

$$\vec{v} \cdot \vec{\nabla} \times \vec{v} = 0 \text{ & so }$$

$$\vec{v} \cdot \vec{\nabla} \left(\frac{P}{\rho} + \phi + \frac{1}{2} v^2 \right) = 0 \quad \text{for steady streamline flow}$$

$$\frac{\partial v}{\partial t} = 0.$$

So for a small displacement in the direction of the fluid velocity

$$\frac{P}{\rho} + \phi + \frac{1}{2}v^2 = \text{constant}$$

for all points along a streamline.

This is called Bernoulli's equation for potential flow. The constant in R.H.S. is constant along any given streamline but is different for different streamlines, while for a potential flow (irrotational), it is constant throughout the fluid.

$$\frac{P}{\rho} + \phi + \frac{1}{2}v^2 = \text{constant}$$

(everywhere)

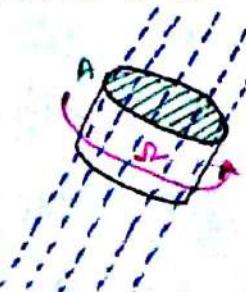
Vortex lines In terms of vorticity, we have already noted the Euler's equation, $\frac{\partial \vec{v}}{\partial t} + \vec{\omega} \times \vec{v} + \frac{1}{2} \vec{\nabla} v^2 = - \frac{\vec{\nabla} P}{\rho} - \vec{\nabla} \phi$. By taking a curl, we can permanently eliminate pressure, so that for an incompressible liquid,

$$\vec{\nabla} \cdot \vec{v} = 0, \quad \vec{\omega} = \vec{\nabla} \times \vec{v} \quad \text{and} \quad \frac{\partial \vec{\omega}}{\partial t} + \vec{\nabla} \times (\vec{\omega} \times \vec{v}) = 0$$

describes

the velocity field everywhere. Also, if $\vec{\omega} = 0$ at any time t , $\frac{\partial \vec{\omega}}{\partial t} = 0$ so at all time $\vec{\omega} = 0$ or the flow remains permanently irrotational. The equations to be solved are $\vec{\nabla} \cdot \vec{v} = 0, \vec{\nabla} \times \vec{v} = 0$

As Helmholtz proposed, imagine that in the fluid we want to draw vortex lines, rather than streamline. Vortex lines are field lines in the direction of $\vec{\omega}$ and density proportional to the magnitude $|\vec{\omega}|$. They are similar to magnetic induction \vec{B} , without any beginning or end, revolving in closed loops, and move with the fluid. Suppose at time t , a small cylinder of



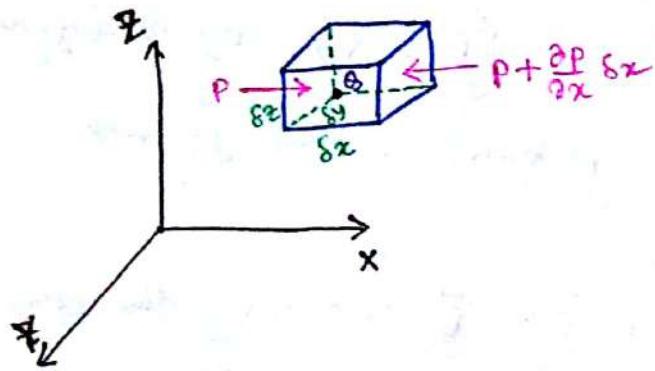
the liquid with axis parallel to vortex lines is transported at $t+dt$ to another cylinder with area A_2 .

$$\text{So, } \omega_1 A_1 = \omega_2 A_2 \quad \text{as } \omega \propto \text{density}$$

because mass is same in both situation, we see $A_1 = \pi r_1^2$
and $A_2 = \pi r_2^2$ and $M_1 = M_2$ gives.

$\pi M_1 r_1^2 \Omega_1 = \pi M_2 r_2^2 \Omega_2 \Rightarrow L_1 = L_2$ or in the absence
of viscosity, angular momentum of an element of the fluid is
invariant. This is "ideal" "dry" water case as it means if $\vec{\Omega} = 0$
then $\vec{\Omega}$ cannot be created or there will not be any vorticity.

Fluid Statics : Condition of Equilibrium of a fluid



Consider a container of fluid at rest, & within it an infinitesimal rectangular parallelepiped is taken in which at point Q, we calculate the body force. f_x, f_y, f_z are components

of the body force \vec{F} at $Q(x, y, z)$. Now, force due to pressure p on the elemental area $\delta y \delta z$ along x-axis is $p \delta y \delta z$. & force on opposite face of the parallelopiped is $-(p + \frac{\partial p}{\partial x} \delta x) \delta y \delta z$.

$$\therefore \text{The resultant force} = p \delta y \delta z - (p + \frac{\partial p}{\partial x} \delta x) \delta y \delta z \\ = - \frac{\partial p}{\partial x} \delta x \delta y \delta z.$$

So for equilibrium under the action of the body force

$$F_x = \rho \delta x \delta y \delta z - \frac{\partial p}{\partial x} \delta x \delta y \delta z = 0 \quad \text{or, } f_x = \frac{1}{\rho} \frac{\partial p}{\partial x}$$

Similarly for y and z direction, $f_y = \frac{1}{\rho} \frac{\partial p}{\partial y} \Rightarrow f_z = \frac{1}{\rho} \frac{\partial p}{\partial z}$.

$$\therefore \vec{F} = \frac{1}{\rho} \vec{\nabla} p \quad \text{and for } \rho = \text{constant}, \vec{\nabla} \times \vec{F} = 0.$$

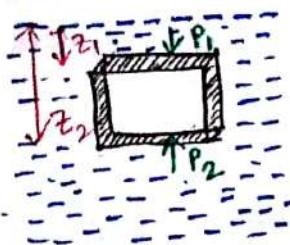
If the force is gravity then $f_z = -g$, $f_x = f_y = 0$.

$$\text{So, } -g - \frac{1}{\rho} \frac{dp}{dz} = 0 \quad \Rightarrow \quad dp = -g \rho dz.$$

$\therefore P = -\rho g z + C$ where at $z=0$, $P=P_0$ gives $C=P_0$

$\therefore P = P_0 - \rho g z$ Equation of hydrostatics for incompressible liquid

As $P-P_0$ does not depend on P_0 or pressure exerted by external forces on the fluid is transmitted equally in all directions. This is Pascal's principle.



Again, consider a body immersed in a fluid with pressure P_1 & P_2 at upper & lower surface, then

$$P_1 = -\rho g z_1 + C_1, P_2 = -\rho g z_2 + C_2$$

$$\therefore (P_1 - P_2) = \rho g (z_2 - z_1).$$

$\therefore (P_1 - P_2)A = \text{thrust} = \rho g A(z_2 - z_1) = \text{weight of the fluid dispersed in upward direction.}$

This is the Archimede's principle.

This can be easily derived from Bernoulli's theorem

$$\frac{v^2}{2} + \frac{P}{\rho} + gh = \text{constant by substituting } v=0, h=2.$$

For compressible gases, Boyle's law give $P \propto \rho$.

$$\therefore \frac{P}{P_0} = \frac{\rho}{\rho_0}. \text{ So from } dP = -g\rho dz \text{ we get } dP = -g dz \frac{\rho_0}{P_0} P$$

$$\therefore \frac{dP}{P} = -\frac{g \rho_0}{P_0} dz \quad \therefore \int_{P_0}^P \frac{dP}{P} = -\frac{\rho_0 g}{P_0} \int_0^z dz$$

$$\therefore \ln \frac{P}{P_0} = -\frac{\rho_0 g z}{P_0} \quad [\text{where } P_0 = \text{pressure at surface of earth or } z=0.]$$

$$\therefore P = P_0 e^{-\frac{\rho_0 g z}{P_0}}$$

This expression correctly shows exponential fall of pressure with distance but flawed as temperature variation is not accounted for. But

from $\frac{dP}{dz} = -\rho g$, using Clausius-Clapeyron's equation

$$P = n k_B T \quad (k_B = \text{Boltzmann's constant} = 1.38 \times 10^{-23} \text{ J/K} = \frac{R}{N})$$

$$= \frac{\text{universal gas constant}}{\text{Avogadro Number}} = \frac{8.314 \text{ J/mol K}}{6.023 \times 10^{23}} \quad M = \text{molecular weight of gas.}$$

$$\text{So } \frac{dp}{dz} = -\rho g = -\frac{Mg}{RT} p$$

$$[\text{As, } mn = \rho, \quad [\text{As } p = n k_B T]$$

$$mn = M \quad = \frac{\rho}{M} \frac{R}{N} T$$

$$k_B = \frac{R}{N} \quad = \frac{\rho R}{M} T$$

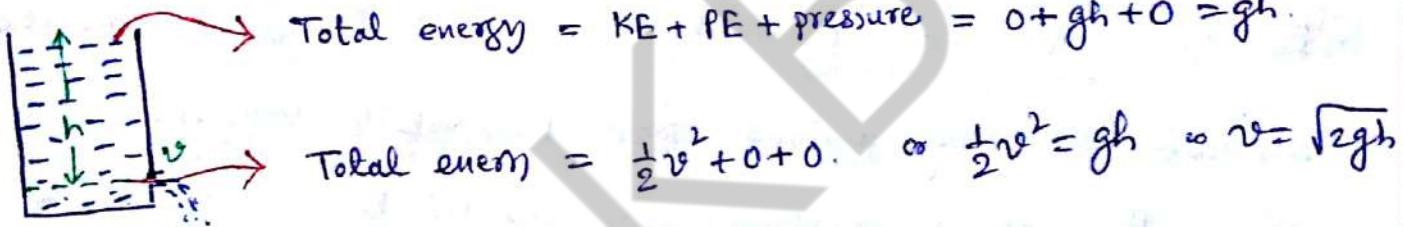
$$\therefore \frac{dp}{p} = -\frac{Mg}{RT} dz$$

$$\therefore \ln p = -\frac{Mg}{RT} z + \ln p_0$$

$$\therefore p = p_0 e^{-Mgz/RT}$$

This is called "law of atmosphere."

Torricelli's theorem Velocity of efflux of a liquid through an orifice is equal to the velocity attained by a body in falling freely from the surface of the liquid to the orifice.



Eulerian and Lagrangian description of conservation laws

The rate of change of a field variable $\phi(t, \vec{x})$ with respect to fixed position of space is called Eulerian derivative $\frac{\partial \phi}{\partial t}$ while derivative following a moving parcel is called Lagrangian derivative or substantial derivative or material derivative $\frac{D\phi}{Dt}$

$$\frac{D\phi}{Dt} = \frac{\partial \phi}{\partial t} + \vec{V} \cdot \vec{\nabla} \phi$$

local rate of change

convective rate of change

So changes in the properties of a moving fluid can be measured either on a fixed point in space

while fluid particles are crossing it (Eulerian) or by following a fluid parcel along its path (Lagrangian)

$$\text{Eulerian } \vec{v}(t, \vec{x}(\vec{x}_0, t)) = \frac{\partial}{\partial t} \vec{x}(t, \vec{x}_0)$$

Reynold's Transport theorem As we have defined our conservation laws in Lagrangian description, Reynold's transport theorem gives the Eulerian equivalent of the integral taken over a moving material volume of a fluid.

$$\left(\frac{d\phi}{dt} \right)_{\text{material volume}} = \frac{d}{dt} \int_V \psi \rho dV + \iint_S \psi \rho \vec{v} \cdot \hat{n} ds, \quad [\psi = \frac{d\phi}{dm} = \text{amount of } \phi \text{ per unit mass}]$$

$$= \int_V \left[\frac{\partial}{\partial t} (\psi \rho) + \vec{\nabla} \cdot (\rho \vec{v} \psi) \right] dV = \int_V \left[\frac{D}{Dt} (\rho \psi) + \rho \vec{v} \cdot \vec{\nabla} \psi \right] dV$$

Notice that conservation law indicate no source or sink meaning

$\frac{d\phi}{dm} = 0$ or $\frac{dm}{dt} = 0$, meaning $\psi = \frac{d\phi}{dm} = 1$ when $\phi = m$.

$$\boxed{\frac{D\rho}{Dt} + \rho \vec{\nabla} \cdot \vec{v} = 0}$$
 mass conservation law in Eulerian coordinate system.

So incompressibility ($\vec{\nabla} \cdot \vec{v} = 0$) means $\frac{D\rho}{Dt} = 0$, or ρ is not a constant but ρ does not change along a streamline.

In presence of external force \vec{f} per unit volume, the non-conservative form with $\psi = \vec{v}$ is

check:
$$\frac{D}{Dt} (\rho \vec{v}) + \rho \vec{v} \cdot \vec{\nabla} \cdot \vec{v} = \vec{f}$$

$\therefore \rho \frac{D\vec{v}}{Dt} + \vec{v} \left(\frac{D\rho}{Dt} + \rho \vec{\nabla} \cdot \vec{v} \right) = \vec{f}$ $\therefore \rho \frac{D\vec{v}}{Dt} = \vec{f}$ (continuity)

Using Reynold's Transport theorem, we find the conservative form

$$\frac{\partial}{\partial t} (\rho \vec{v}) + \vec{\nabla} \cdot (\rho \vec{v} \vec{v}) = \vec{f} = \vec{f}_{\text{surface}} + \vec{f}_{\text{body}}$$

↳ Dyadic product

Now $\int_V \vec{f}_s dV = \int_V \vec{\sigma} \cdot \hat{n} ds = \int_V \vec{\nabla} \cdot \vec{\sigma} dV$ where $\vec{\sigma} = \text{Stress tensor or stress matrix}$.

$$\vec{\sigma} = - \begin{pmatrix} p & 0 & 0 \\ 0 & p & 0 \\ 0 & 0 & p \end{pmatrix} + \begin{pmatrix} \sigma_{xx} + p & \sigma_{xy} & \sigma_{xz} \\ \sigma_{yx} & \sigma_{yy} + p & \sigma_{yz} \\ \sigma_{zx} & \sigma_{zy} & \sigma_{zz} + p \end{pmatrix}$$

$$= -P \mathbb{I} + \vec{\tau}$$

$\vec{\tau}$ Deviatoric / Viscous stress tensor.

↳ Thermodynamic pressure ($= n k_B T$) . So $\vec{\nabla} \cdot \vec{\tau} = -\vec{\nabla} P + \vec{\nabla} \cdot \vec{\tau}$.

$$\vec{f}_b = \rho \vec{g} - 2\rho \vec{\omega} \times \vec{v} - \rho \vec{\omega} \times (\vec{\omega} \times \vec{r}).$$

gravity vorticity centrifugal force centrifugal forces

are dependent on position but not velocity, so they can be absorbed into a modified pressure & hence effectively ignored. Coriolis force however has to be treated explicitly.

So conservation of momentum equation becomes,

$$\boxed{\frac{\partial}{\partial t}(\rho \vec{v}) + \vec{\nabla} \cdot (\rho \vec{v} \vec{v}) = -\vec{\nabla} P + \vec{\nabla} \cdot \vec{\tau} + \vec{f}_b}$$

Stress tensor for Newtonian fluid

$$\vec{\tau} = \eta \left\{ \vec{\nabla} \vec{v} + (\vec{\nabla} \vec{v})^T \right\} + \lambda (\vec{\nabla} \cdot \vec{v}) \mathbb{I}$$

η viscosity coefficient (molecular) λ viscosity coefficient (bulk)

$$\begin{aligned} \text{So } \frac{\partial}{\partial t}(\rho \vec{v}) + \vec{\nabla} \cdot (\rho \vec{v} \vec{v}) &= -\vec{\nabla} P + \vec{\nabla} \cdot [\eta \left\{ \vec{\nabla} \vec{v} + (\vec{\nabla} \vec{v})^T \right\}] \\ &\quad + \vec{\nabla} (\lambda \vec{\nabla} \cdot \vec{v}) + \vec{f}_b \\ &= -\vec{\nabla} P + \eta \vec{\nabla}^2 \vec{v} + \vec{f}_b = -\vec{\nabla} P + \vec{f}_b \end{aligned}$$

incompressible flow
inviscid flow

Similarly energy conservation equation can be derived.

General form

$$\frac{\partial}{\partial t}(\rho \phi) + \vec{\nabla} \cdot (\rho \vec{v} \phi) = \vec{\nabla} \cdot (\Gamma \vec{\nabla} \phi) + Q$$

[unsteady term] [convection term] [diffusion term] [source term]

$$\text{Like Reynolds number } Re = \frac{\rho v L}{\eta} = \frac{\text{advection (inertia)}}{\text{diffusion (viscous)}}$$

reveals the boundary layer characteristic of the flow if momentum

Fluxes are in same direction, e.g. if diffusion is in the cross-stream direction then Re conveys the flow regime.

Similarly Schmidt number

$$Sc = \frac{\text{momentum diffusivity}}{\text{mass diffusivity}}$$

$$\text{Pelet number } Pe = \frac{\text{adjective transport}}{\text{diffusive transport}} = Re \times Sc$$

$$\text{where } Pr = \text{Prandtl number} = \frac{\text{hydrodynamic boundary layer}}{\text{thermal boundary layer}} \\ = \frac{\text{convection}}{\text{conduction}}$$

$$\text{Grashof number} = \frac{\text{buoyancy force}}{\text{viscous force}}$$

$$\text{Mach number} = \frac{\text{object speed}}{\text{speed of sound}} \quad \text{where } v_{\text{sound}} = \sqrt{\gamma \left(\frac{\partial P}{\partial \rho} \right)_T} \\ = \sqrt{RT} \quad (\text{ideal gas}) \\ \gamma = C_p/C_v$$

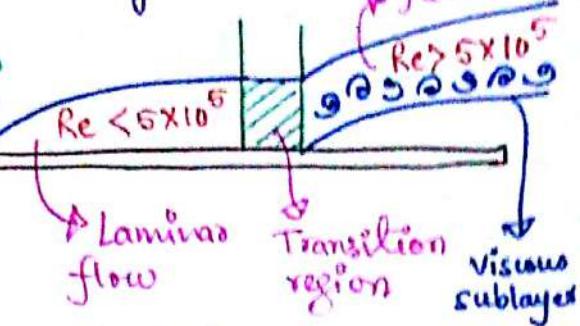
$M < 0.2$ is incompressible flow.

$M < 1$ is subsonic flow.

$M = 1$ is sonic flow.

$M < 5$ is supersonic flow

$M > 5$ is hypersonic flow.



Laminar flow Transition region Viscous sublayer

flow classification

Euler equation in Lagrangian form

$$\rho \left(\frac{\partial \vec{v}}{\partial t} + (\vec{v} \cdot \vec{\nabla}) \vec{v} \right) = - \vec{\nabla} P - \rho \vec{\nabla} \phi + \eta \vec{\nabla}^2 \vec{v} \quad \& \quad \vec{\Omega} = \vec{\nabla} \times \vec{v}$$

$$\text{gives, } \frac{\partial \vec{\Omega}}{\partial t} + \vec{\nabla} \times (\vec{\rho} \times \vec{v}) = \frac{\eta}{\rho} \vec{\nabla}^2 \vec{\Omega}$$

$$\Leftrightarrow \text{specific viscosity} = \frac{1}{Re}$$

If we non-dimensionalize this equation (see Feynman lectures, vol 2 section 41.3), then $\frac{\partial \vec{\Omega}}{\partial t} + \vec{\nabla} \times (\vec{\Omega} \times \vec{v}) = \frac{1}{Re} \vec{\nabla}^2 \vec{\Omega}$

So if Mach number & Reynolds number are same then velocities near or above sound speed in two scenarios are equivalent.

ELASTICITY

Elastic Properties of Matter

when an external force acts on a body, relative displacement of its various parts takes place. By exerting a restoring force, particles tend to come back to their original position.

$$\text{Stress} = \frac{\text{Restoring force}}{\text{cross-sectional area}} = \frac{F}{A}.$$

Strain is defined as the ratio of change of length, volume or shape to the original length, volume or shape.

$$\text{Young's Modulus: } Y = \frac{\text{applied load per unit cross-section}}{\text{increase in length per unit length}} = \frac{\text{longitudinal stress}}{\text{longitudinal strain}} = \frac{F/A}{\ell/L} = \frac{FL}{AL}$$

Unit (CGS): stress σ = dynes/cm², (SI) = Newton/m².
strain = no unit (pure number).

$\therefore Y = \text{dynes/cm}^2$ (CGS) or N/m^2 (SI). Dimension of Y is

$$[Y] = \left[\frac{ML^{-2}T^{-2}}{L \cdot L^2} \right] = [ML^{-1}T^{-2}].$$

Bulk Modulus: (volume elasticity)

$$K = \frac{\text{compressive or tensile force per unit area}}{\text{decrease or increase in volume per unit volume}}$$

$$= \frac{\text{compressional or dilational pressure}}{\text{volume strain}} = - \frac{dP}{dV}.$$

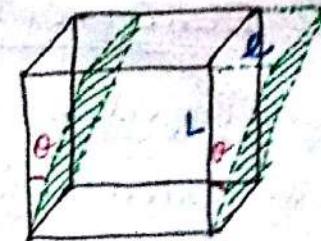
$$\therefore K = \text{dynes/cm}^2 \text{ or } N/m^2 \text{ as, } [K] = \left[\frac{ML^{-2}T^{-2}}{L^3 \cdot L^{-3}} \right] = [ML^{-1}T^{-2}]$$

Negative sign means increase in applied pressure causes decrease in volume.

$$\text{Rigidity Modulus: } n = \frac{\text{tangential stress}}{\text{angle of shear or shearing strain}}$$

Consider a solid cube, whose lower face is fixed and a tangential force F is applied over the upper face, so that its

displaced to a new position. As each horizontal layer of the cube is displaced with displacement proportional to its distance from the fixed lower plane,



$$\text{shearing strain} = \frac{l}{L} = \tan \theta \approx \theta \quad \text{if } \theta \rightarrow 0^{\circ} \text{ (usually)} \quad (\theta)$$

$$\therefore n = \frac{F/A}{\theta} = \frac{F}{AO} \quad [n] = [ML^{-1}T^{-2}] \text{ & unit is}$$

dynes/cm² or N/m² as θ is a pure number.

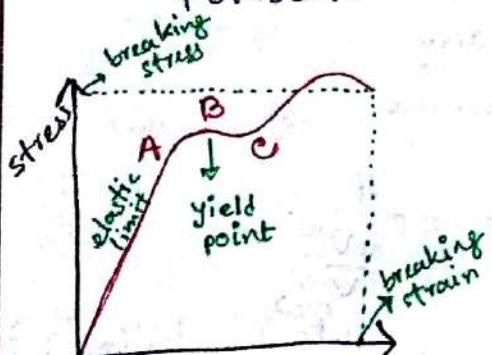
Poisson's Ratio: When a wire is stretched, its length increases but its diameter decreases. When an elongation is produced by a longitudinal stress in a certain direction, a contraction results in the lateral dimensions of the body under strain.

$$\sigma = \frac{\text{lateral strain}}{\text{longitudinal strain}} = \frac{d/D}{L/L} = \frac{dL}{DL} \quad \text{where}$$

D = diameter of the wire, d = decrease in diameter.

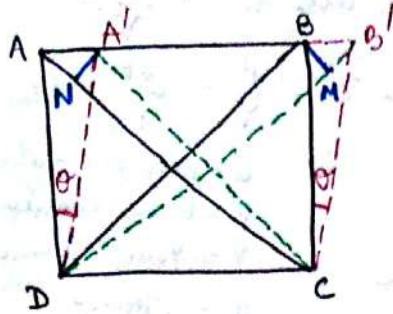
L = length of the wire, L = increase in length.

Poisson's ratio is a dimensionless number.



Stress or strain is called the elastic limit or Hooke's law (point A), so that if stress is removed, an elastic body regains its original shape. After point A, the curve is bent towards strain is a maximum point B (permanent set). After point B, elongation is faster than AB. So after yield point B, elongation increases rapidly with rapid contraction of the area of cross-section of the wire until the breaking stress is reached, where snapping occurs. It's called fracture.

Shear \equiv Elongation (extension) strain + compression strain



Suppose in $ABCD$ cube of $AB = BC = CD = DA = L$ the base CD is fixed and after applying a tangential force F the distorted cube is $A'B'CD$ with $AA' = BB' = l$ & $\angle A'DA' = \theta$.

Now $DB = DM = \sqrt{2}L$. As θ (angle of shear) is very small, so $\triangle AAN$ & $\triangle BMB'$ are isosceles right angle triangle with $\angle A'AN = \angle BB'M = 45^\circ$

$$\therefore B'M = BB' \cos 45^\circ = \frac{l}{\sqrt{2}}$$

So Elongation (extension) strain along DB diagonal is

$$\frac{B'M}{DB} = \frac{l}{\sqrt{2}} \times \frac{1}{L\sqrt{2}} = \frac{l}{2L} = \frac{\theta}{2} \quad \text{as } \frac{l}{L} = \tan \theta \approx \theta.$$

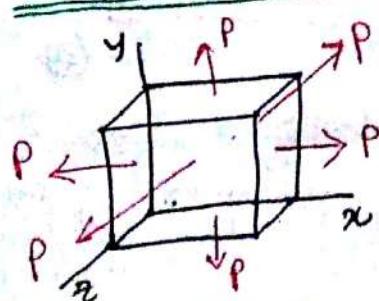
Similarly, compression strain along diagonal $AC = \frac{AN}{AC}$

$$= \frac{AA' \cos 45^\circ}{L\sqrt{2}} = \frac{l}{\sqrt{2}} \times \frac{1}{L\sqrt{2}} = \frac{l}{2L} = \frac{\theta}{2}.$$

So shear θ is equivalent to an extension and a compression strain at right angle to each other with each of value $\theta/2$.

Look for a proof that a shearing stress is equivalent to a linear tensile stress and an equal compression stress mutually at right angles.

Relation between γ, K, n, σ for a homogeneous isotropic medium



Suppose a cube in a strained medium is subjected to uniform tensile stress P over each face. So linear strain along x axis due to tensile stress along x axis is $\frac{P}{Y}$. Linear strain along

x axis due to tensile stress along y -axis is $-\frac{\sigma P}{Y}$. Also, linear strain along x -axis due to tensile stress along z -axis is $-\frac{\sigma P}{Y}$.

So the resultant linear strain along x axis $\gamma = \frac{P}{Y} - \frac{2\sigma P}{Y}$.
Similarly so for y and z axis.

If $\frac{\delta V}{V}$ is the volume strain then $\frac{\delta V}{V} = \frac{P}{K}$

for spherically isotropic system,

$$\frac{\delta V}{V} = \frac{\frac{4}{3}\pi [x(1+\gamma)x(1+\gamma)x(1+\gamma)] - \frac{1}{3}\pi r^3}{\frac{1}{3}\pi r^3} = \gamma + 3\sigma + O(\sigma^2) \dots \text{---} 1$$

$= 3\sigma$. (Cubical expansion is 3 times linear expansion)

$$\therefore \frac{\delta V}{V} = 3\sigma = \frac{3P}{Y}(1-2\sigma) = \frac{P}{K}$$

Now suppose that the cube is subjected to a tensile stress along x axis & an equal compressional stress along y axis.

So linear strain along x axis due to tensile stress along x axis is $\frac{P}{Y}$. Also,

linear strain along x axis due to compressional stress along y axis is $-\frac{\sigma P}{Y}$. So the resultant linear strain along x axis is

$$\gamma_x = \frac{P}{Y} + \frac{\sigma P}{Y}. \text{ Resultant linear strain along } y \text{ axis } \gamma_y = -\frac{P}{Y} - \frac{\sigma P}{Y}$$

$$\text{and resultant linear strain along } z \text{ axis } \gamma_z = -\frac{\sigma P}{Y} + \frac{\sigma P}{Y} = 0$$

We know $\theta = \frac{P}{n}$ and $\frac{\theta}{2} = \frac{P}{Y}(1+\sigma)$

as $\theta = \frac{\theta_x}{2}$. So $\frac{P}{2n} = \frac{P}{Y}(1+\sigma)$

θ = angle of shear
 n = modulus of rigidity

$$Y = 2n(1+\sigma)$$

L ②

From ① and ②, we have $\frac{Y}{K} = 3-6\sigma$ and $\frac{Y}{n} = 2+2\sigma$

$$\therefore Y\left(\frac{1}{K} + \frac{1}{n}\right) = 5-4\sigma = 5-4\left(\frac{Y-2n}{2n}\right)$$

$$Y = \frac{9nK}{n+3K}$$

Again from ① and ②, $\frac{Y}{3K} = 1 - 2\sigma$ and $\frac{Y}{2n} = 1 + \sigma$

$$n\sigma = Y \frac{3K - 2n}{18Kn} = \frac{9Kn}{n+3K} \frac{3K - 2n}{18Kn} = \frac{3K - 2n}{6K + 2n}$$

$$\sigma = \frac{3K - 2n}{6K + 2n}$$

$$\text{or } 3K(1 - 2\sigma) = 2n(1 + \sigma), n, K > 0.$$

When $\sigma > \frac{1}{2}$, $3K(1 - 2\sigma) < 0$ but $2n(1 + \sigma) > 0$. } $3K(1 - 2\sigma) \neq 2n(1 + \sigma)$
when $\sigma < -1$, $3K(1 - 2\sigma) > 0$ but $2n(1 + \sigma) < 0$ } violation

$$\therefore -1 < \sigma < \frac{1}{2}.$$

The Torsion cylinder and shear Waves

Consider a cylinder of length l and radius a with clamped (fixed) lower end and a torque is applied at upper end, because of that cylinder is twisted through an angle. If an elemental point

A is displaced to A' , then $\theta = AA' = r\phi$

where ϕ = angle of twist and r is radius of elemental cylinder.

$\therefore r\phi = \theta \Rightarrow \theta = r\phi/l$. Due to elasticity, there will

be a restoring torque. To calculate this, consider the shell of thickness dr , length dx at r distance apart. So tangential stress = $\frac{f}{drdx}$ and

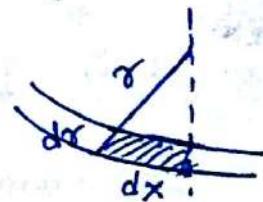
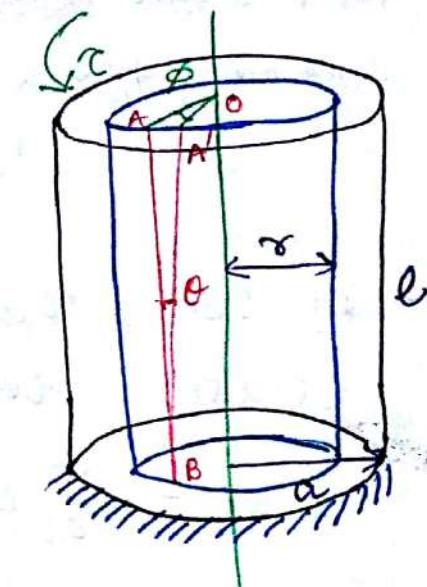
$$\text{rigidity modulus } n = \frac{\text{tangential stress}}{\text{angle of shear}} = \frac{f/drdx}{\phi} = \frac{F/drdx}{r\phi/l}$$

$$= \frac{Fl}{r\phi drdx}. \quad \therefore F = \frac{n\phi}{l} r dr dx.$$

Moment of this force about cylinder axis = $F \cdot r = \frac{n\phi}{l} r^2 dr dx$

$$\text{So restoring torque over entire surface } \delta \tau = \frac{n\phi}{l} r^2 dr \sum dx$$

$$[2dx = 2\pi r] = \frac{2\pi n\phi}{l} r^3 dr$$

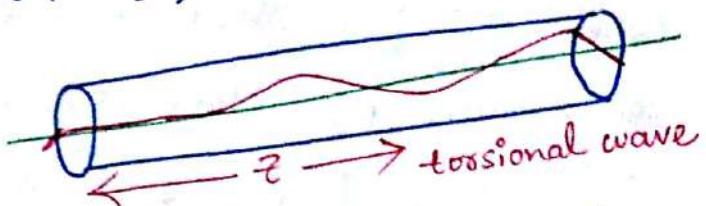


∴ Total restoring torque for the entire cylindrical bar

$$\tau = \frac{2\pi n \phi}{l} \int_{r_1}^{r_2} r^3 dr = \frac{\pi n a^4}{2l} \phi, \quad \frac{\tau}{\phi} = \text{torsional rigidity}$$

for hollow cylinder with inner & outer radii r_1 & r_2

$$\tau = \frac{2\pi n \phi}{l} \int_{r_2}^{r_1} r^3 dr = \frac{n\pi \phi}{2l} (r_1^4 - r_2^4)$$



For a static torsion, torque is

same everywhere & proportional to ϕ/l . If its nonuniform then

$$\tau(z) = \frac{n\pi a^4}{2l} \left(\frac{\partial \phi}{\partial z} \right) \quad \rightarrow \text{local torsional strain}$$

If $\tau(z)$ & $\tau(z+dz)$ are the torque at two ends then

$$\tau(z+dz) = \tau(z) + \frac{\partial \tau}{\partial z} dz \quad \text{and so, } \Delta \tau = \tau(z+dz) - \tau(z)$$

$$\therefore \Delta \tau = \frac{\partial \tau}{\partial z} dz = \frac{n\pi a^4}{2} \frac{\partial^2 \phi}{\partial z^2} dz \quad \text{--- (1)}$$

The effect of this incremental torque is to yield angular acceleration of the slice of mass $(\pi a^2 dz) \rho$ or moment of inertia $\frac{1}{2} m a^2 = \frac{\pi}{2} \rho a^4 dz$, so that the restoring couple is $I \alpha = I \frac{d^2 \phi}{dt^2} = \frac{\pi \rho a^4}{2} dz \frac{\partial^2 \phi}{\partial t^2}$. --- (2)

So, from (1) & (2)

$$\frac{n\pi a^4}{2} \frac{\partial^2 \phi}{\partial z^2} dz = \frac{\pi \rho a^4}{2} \frac{\partial^2 \phi}{\partial t^2} dz$$

$$\therefore \boxed{\frac{\partial^2 \phi}{\partial t^2} = \frac{n}{\rho} \frac{\partial^2 \phi}{\partial z^2}}$$

Wave equation in 1 dimension with

$$v_{\text{shear}} = \sqrt{\frac{n}{\rho}} = \text{shear speed}$$

So denser the rod for same stiffness the slower the waves & independent of radius of rod. Torsional waves are special example of shear waves, which are those in which the strains do not change the material volume, but in torsional waves, shear stresses are distributed on a circle and move with same speed.

Inside a solid material there are compressional / longitudinal waves as well as on the surface Rayleigh or Love waves. In them, strains are neither purely longitudinal or transverse. Longitudinal waves travel faster than shear waves

$$v_{\text{long}} = \sqrt{\frac{1-\sigma}{(1+\sigma)(1-2\sigma)} \frac{Y}{\rho}}$$

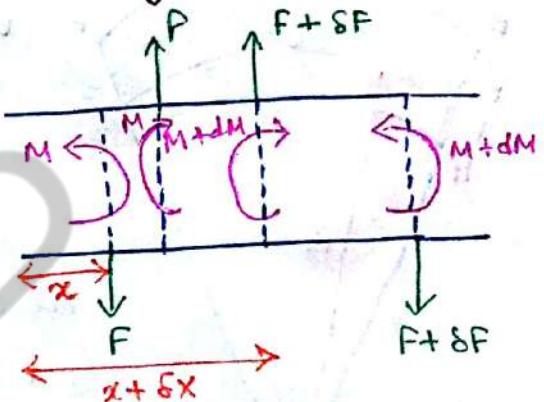
and $Y > \rho$, as $Y = 2n(1+\sigma)$, so

$$v_{\text{long}} > v_{\text{shear}}$$

ρ & σ can be measured by measuring ρ and v_{long} , v_{shear} , e.g. in earthquake, distance between quakes can be measured like this.

Bending of Beam: General method for determining deflection due to bending:

Let w be the weight per unit length of the beam. Let us consider an element δx , the left edge of which is at a distance x from the origin and the right edge at $x + \delta x$ from the origin.



During downward displacement of the element, shearing stress at left face is F & at right face is $F + \delta F$. The corresponding internal resisting moment at the left face due to the left hand portion of the beam is M in the counterclockwise direction and at the right hand portion of the beam is $M + \delta M$ in the clockwise direction.

Considering equilibrium of the δx element due to force balance

$$F + \delta F = F + w \delta x$$

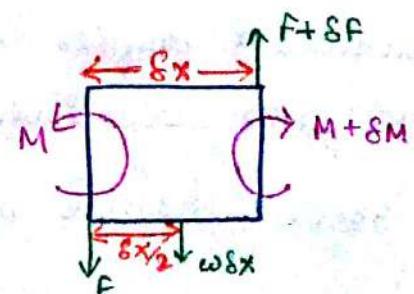
$$\Rightarrow \frac{\delta F}{\delta x} = w$$

In the limit $\delta x \rightarrow 0$, $\frac{dF}{dx} = w$.

Considering the moment equation,

$$M + \delta M + w \cdot \frac{\delta x}{2} = M + (F + \delta F) \delta x$$

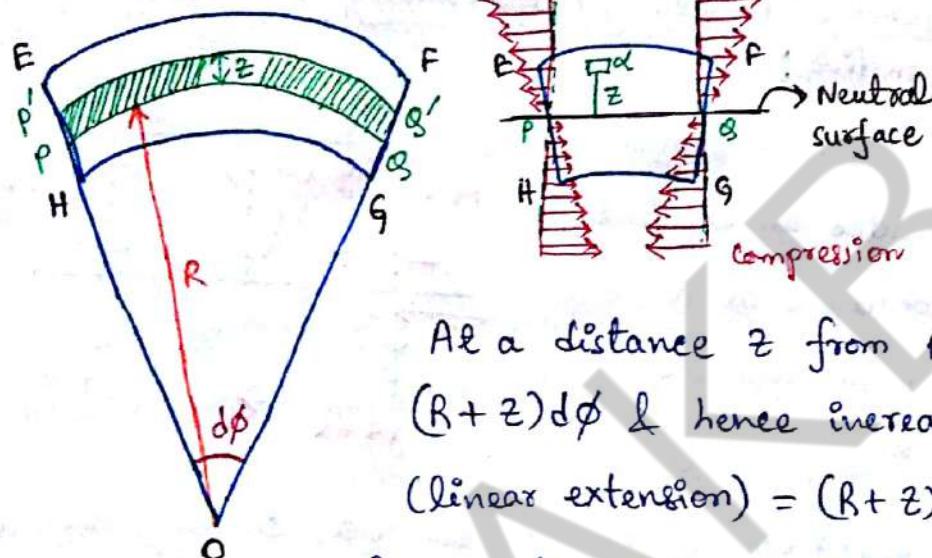
$$\lim_{\delta x \rightarrow 0}, \delta M = F \delta x \Rightarrow \frac{dM}{dx} = F$$



We will use these two equations to determine the depression of a loaded beam.

Internal Bending Moment

A body whose length is much greater than its cross-sectional area is called a beam. When such a beam is bent by an applied torque, tensile forces act on some layers of the beam and compressional forces act on other layers, as a result of which, filaments of the beam nearest the outside curve of the bent beam are extended and the filaments nearest the inside curve get compressed. In between them, there is a surface (called Neutral surface) on which the filaments remain unaltered.



Let us consider a small portion of bent beam $EFGH$ with length PQ and breadth EH . O is the center of curvature.

At a distance z from PQ , length of filament is $(R+z)d\phi$ & hence increase in length of filament (linear extension) = $(R+z)d\phi - R d\phi = z d\phi$.

The linear extensional strain = $\frac{z d\phi}{R d\phi} = \frac{z}{R}$. If d is the cross-section of filament then longitudinal force f to resist elongation $f = \frac{\alpha Y Z}{R}$, below neutral surface this is the force to resist compression. If two filaments are equal distance from the neutral axis then they form a couple. For infinitely many equidistant couples comes into play the internal bending moment with same magnitude as external bending moment.

Total internal moment = $\sum f z = \frac{Y}{R} \sum_{\text{all filaments}} \alpha z^2$. $\sum \alpha z^2$ is called

the geometrical moment of inertia, having same (equivalence) as moment of inertia with $m \Leftrightarrow \alpha$. So $\sum \alpha z^2 = A k^2$ where

A is the total area EFGH and K is the radius of gyration of the surface about the neutral axis. $YI = YAK^2$ is called the flexural rigidity. Radius of curvature $\frac{1}{R} = \frac{\frac{d^2y}{dx^2}}{\left[1 + \left(\frac{dy}{dx}\right)^2\right]^{\frac{3}{2}}}$ and if bending is small, $\frac{dy}{dx} < 1$ & so

$$\frac{1}{R} = \frac{\frac{d^2y}{dx^2}}{\left[1 + \left(\frac{dy}{dx}\right)^2\right]^{\frac{3}{2}}} \text{ So internal bending moment} = YI \frac{d^2y}{dx^2}$$

for rectangular beam, $A = ab$ and $K^2 = \frac{b^2}{12}$, a = breadth, b = thickness.

$$\therefore \text{Bending moment} = \frac{Yab^3}{12R}$$

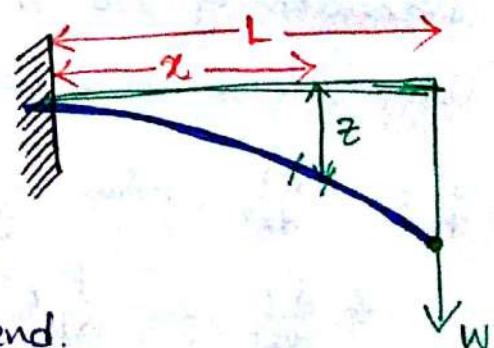
for circular beam, $A = \pi r^2$, $K^2 = \frac{r^2}{4}$, Bending moment = $\frac{Y\pi r^4}{4R}$

$M = \frac{Y}{R} \int z^2 dA$ So on the stiffness of the beam is proportional to Y and moment of inertia I , to make the stiffest possible beam with a given amount of steel, the mass has to be as distant from neutral surface gives larger I , but also curvature won't be much due to buckling/twisting. So structural beams are made in the form of I and H.

Cantilever

A cantilever is a uniform beam supported in such a way that both position and slope are fixed in one end (cement wall) and a concentrated force W acts on free end.

What is the shape of the beam $z(x)$?



If beam is long in comparison to cross section, $\frac{1}{R} = \frac{\frac{d^2z}{dx^2}}{\sqrt{1 + \left(\frac{dz}{dx}\right)^2}} \approx \frac{\frac{d^2z}{dx^2}}{\left(1 + \frac{1}{2}\left(\frac{dz}{dx}\right)^2\right)} \approx \frac{d^2z}{dx^2}$

Bending moment M is equal to the torque about the neutral axis of any cross section then $M(x) = W(L-x)$

$$\text{So from moment equation, } W(L-x) = \frac{YI}{R} = YI \frac{d^2z}{dx^2}$$

$$\text{or } \frac{d^2z}{dx^2} = \frac{W}{YI} (L-x), \text{ Integrating, } \frac{dz}{dx}$$

$$YI \frac{dz}{dx} = W(Lx - \frac{x^2}{2}) + C_1. \text{ Now at } x=0, \frac{dz}{dx} = 0, \text{ so, } C_1 = 0.$$

$$\text{Integrating once again, } YI z = W\left(\frac{Lx^2}{2} - \frac{x^3}{6}\right) + C_2$$

$$\text{Again at } x=0, z=0. \text{ so } C_2 = 0.$$

$$z = \frac{W}{YI} \left(\frac{Lx^2}{2} - \frac{x^3}{6} \right)$$

shape of the beam

Displacement of the end is $x=L$.

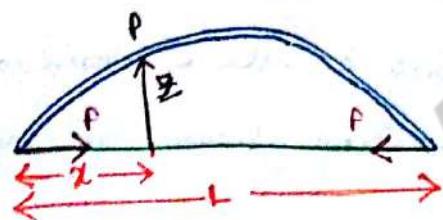
$z = \frac{W}{YI} \frac{L^3}{3}$. Substituting I for rectangular or circular beam, exact expression can be obtained. But $z \propto L^3$.

But cross section do change and for incompressible material, $\epsilon=0.5$

$$\text{as } V = \pi r^2 l = \text{constant} \Rightarrow dV = 0 = 2\pi r d\sigma L + r^2 dL$$

$$\text{so } \frac{dL}{L} = -2 \frac{d\sigma}{r} \text{ or } \sigma = -\frac{d\sigma}{\frac{dL}{L}} = \frac{1}{2} = 0.5. \text{ (rubber)}$$

Buckling



Consider a straight rod in bent shape by two opposite forces that push the two ends of the rod. What is the shape of the rod and magnitude of force? \rightarrow Euler force

Deflection of rod is $z(x)$. So bending moment M at $P=Fz$.

Using the beam equation, $\frac{YI}{R} = Fz$ and for small deflection

$$\frac{1}{R} = -\frac{d^2z}{dx^2} \text{ (minus sign because curvature is downward).}$$

$$\therefore \frac{d^2z}{dx^2} = -\frac{F}{YI} z \quad \text{which is SHM equation of sine wave. So}$$

for small deflection, wavelength λ of sinewave $= 2 \times L$.

$$z = A \sin \frac{\pi x}{L}, \frac{d^2z}{dx^2} = -\frac{A\pi^2}{L^2} \sin \frac{\pi x}{L} = -\frac{\pi^2}{L^2} z. \quad \text{--- (2)}$$

$\text{From (1) and (2)} \therefore \frac{F}{YI} = \frac{\pi^2}{L^2}$ or $F = YI \frac{\pi^2}{L^2}$. So for small bendings the force is independent of the bending displacement z . Below this Euler force, there will be no bending at all & for above this

force there will be large amount of bending \rightarrow buckling. If loading on 2nd floor of a building exceeds Euler force, the building will collapse.