


## PHYSICAL OPTICS

### (Diffraction and Holography)

- Books\*:
1. Opticks → Ghatak (6<sup>th</sup> Edition, Tata Mc Graw Hill)  
⇒ Standard textbook, Good for first time readers.
  2. Introduction to Geometrical and Physical Optics → B.K. Mathur (Old Book) ⇒ Good for concept building and theory learning.
  3. Fundamental of Optics (Tata McGraw Hill) → Jenkins & White ⇒ Concise book, good for Problem solving.
  4. Principles of Optics (Pergamon Press) → Born & Wolf ⇒ Very good book for theory learning.
  5. Feynman lectures on Physics Vol-1 → Feynman/Leighton/Sands (Narosa) ⇒ Short and concise for concept building.
  6. Optics → Hecht (Addison Wesley) ⇒ Good for problem solving and first time readers.
  7. Introduction to Holography → Toal (CRC Press) ⇒ New age book for basic holography principles.

Opticks 

Geometrical Optics deals with refraction and reflection at surfaces, lenses, Matrix method, dispersion through prism, Aberrations and eyepieces and it terms on the particle (corpuscular) theory of light using Fermat's principle. Physical optics on the other hand deals with wave theory of light as Fresnel-Hugen's principle and discusses on Interference and Coherence, Diffraction, Polarisation (Crystal Optics), Fiber optics and Holography.



## DIFFRACTION

Fermat's principle says that when a ray of light goes from one point to another through a set of media, it always follows a path along which the time taken is minimum.

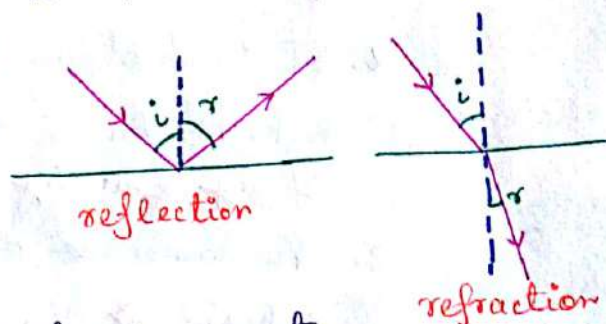
$\frac{dt}{dx} = 0$  yields the "law of reflection"

$i = r$  and the "Snell's

law of refraction"  $v_1 \sin i = v_2 \sin r$

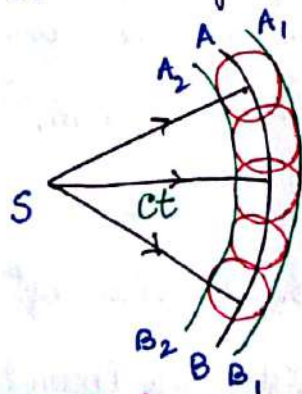
by conservation of the horizontal component of momentum.

The corpuscular model of light establish the rectilinear (straight line) propagation of light and propagation of light through vacuum.



## Wave theory and Huygens-Fresnel principle

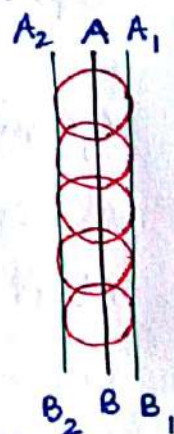
A source of light transmit wave that contain energy in all directions. A "wave front" is defined as the locus of all points which are in the same state of vibration (same phase). For example, circular ripples spreading out in a pond if a pebble is dropped, each circumferential point oscillating at same amplitude & same phase. Similarly for a light source, at a nearby location  $x = ct$  where AB is a spherical wavefront, while at large distance, AB is a plane wavefront.



spherical wavefront

Surface AB is called "primary wavefront".

The direction in which the wave is propagated is known as "ray" which is perpendicular to the wavefront.



plane wavefront

Huygen-Fresnel principle tells that all points on the primary wavefront are considered to be the centres of disturbance and they



transmit secondary waves in all direction with the same velocity as the primary. So A, B, surface that touch the spheres after  $ct_1$  distance is the "Secondary wavefront"

Using Huygen-Fresnel principle, law of reflection ( $i = r$ ), law of refraction ( $v_1 \sin i = v_2 \sin r$ ), refraction of spherical wave at concave spherical surface ( $\frac{\mu}{v} - \frac{1}{u} = \frac{\mu-1}{R}$ ) and convex spherical surface ( $\frac{\mu-1}{R} = \frac{1}{v} - \frac{1}{u}$ ), lens formula for thin convex / concave lens ( $\frac{1}{f} = (\mu-1)(\frac{1}{R_1} - \frac{1}{R_2})$ ) can be obtained.

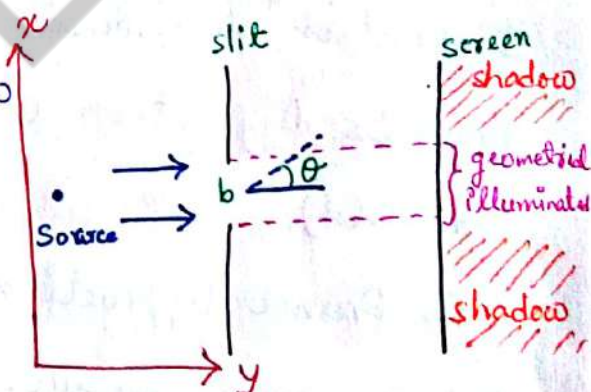
Why Diffraction? Wave-particle duality as in de Broglie's matter wave theory  $\lambda = \frac{h}{p}$  gives rise to Heisenberg's uncertainty principle  $\Delta x \Delta p_x \geq h$ .

If we illuminate a single slit (narrow opening) and if light propagation is rectilinear then there is no bending of light in the geometrical shadow.

But if a light quanta (photon) or electron pass through slit, then  $\Delta x \sim b$ , so  $\Delta p_x \sim \frac{h}{b}$ . As  $p_x = p \sin \theta$ , so  $\sin \theta \sim \frac{h}{pb} \sim \frac{\lambda}{b}$ .

When  $b \gg \lambda$ ,  $\sin \theta \rightarrow 0$  or almost no bending in geometrical shadow, while for  $b \sim \lambda$  then there will be significant bending.

The bending of light round corners and spreading of light waves into the geometrical shadow of an object is called Diffraction.





# Difference between Interference & Diffraction

## Interference

1. Result due to superposition of light from two different wavefront emanating from the same source.
2. Fringes may/may-not be of same width.
3. All bright bands are of uniform intensity
4. Points of minimum intensity are perfectly dark.

## Diffraction

1. Result due to superposition of light from different parts of the same wavefront.
2. Fringes are never of same width
3. All bright bands are of different intensity
4. Points of minimum intensity are not perfectly dark.

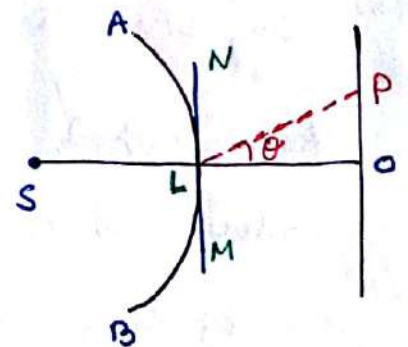
## Classification of Diffraction

Diffraction phenomena are divided into two distinct classes, as Fresnel's diffraction (near field) and Fraunhofer diffraction (far field).

In Fresnel diffraction, source of light & screen are at finite distance from aperture. No concave/convex lenses are used so that incident wavefront is either spherical/cylindrical but not planar. So phase of secondary wavefront isn't same in the plane of aperture.

### Fresnel's assumptions

- (a) A wavefront is divided into a large number of small area (Fresnel's zone). Secondary waves originating from various zones will interfere and the resultant effect can be noted at point P on the screen.





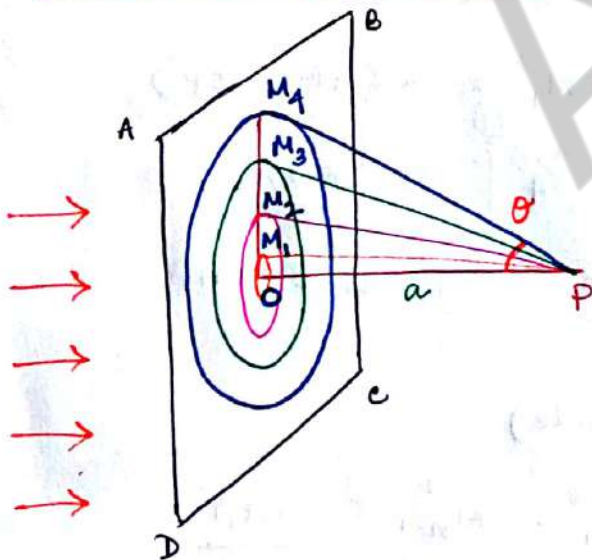
(b) Resultant at P due to a particular zone will depend on the distance of the point from the zone.

(c) Resultant at P will also depend on obliquity factor, which is proportional to  $(1 + \cos \theta)$ . So for a wavefront at L, maximum at O occurs for  $\theta = 0$ , while in LN or LM direction, intensity is half of O, as  $\theta = \pi/2$ . Along LS,  $\theta = \pi$ , so no intensity in reverse direction. (zone plate)

Fraunhofer diffraction occurs when source of light/screen are effectively infinite distances from aperture. Two convex lenses are used & incident wavefront is plane. Secondary wavelets from exposed portion of the wavefront at aperture are in the same phase at all points in plane of the aperture.

(plane transmission grating, concave reflection grating)

### Fresnel's half-period zone of a plane wavefront



- First half period zone  $a + \lambda/2$
- Second half period zone  $a + \lambda$
- Third half period zone  $a + 3\lambda/2$
- Fourth half period zone  $a + 2\lambda$

Let us consider a plane wavefront of a monochromatic light at any particular instant. We want to find out the resultant amplitude at P due to all the wavelets coming from this wavefront.

According to Huygen's principle, every point on the plane wavefront may be regarded as the origin of the secondary wavelets & therefore the resultant effect at P due to the whole wavefront will be equal to the resultant of all these secondary wavelets.



The wavefront is divided into a number of Fresnel's half period zones - from P drop a perpendicular on ABCD at O (pole of the wave). Let  $OP = a$  and P as centre & radius  $(a + \frac{\lambda}{2})$ , draw a sphere cutting the wavefront in a circle at  $M_1$ ,

$PM_1 = a + \frac{\lambda}{2}$  so that the secondary wavelets from O & from the points on the circumference of  $M_1$  on reaching P will differ in phase by  $\frac{2\pi}{\lambda} (PM_1 - OP) = \frac{2\pi}{\lambda} \times \frac{\lambda}{2} = \pi = \frac{T}{2}$  (half period)

Similarly other sphere of radii  $(a + \frac{2\lambda}{2})$ ,  $(a + \frac{3\lambda}{2})$ ,  $(a + \frac{4\lambda}{2})$ , ... can be drawn that intersect at  $M_2, M_3, M_4, \dots$  so that the whole wavefront can be divided into several half period zones.

Amplitude due to wavelets produced by each zone is

- (i) Directly proportional to the area of the zone which is approximately equal.
- (ii) Varies inversely with the distance of zone from P.
- (iii) Varies with the obliquity factor  $(1 + \cos \theta)$ .

$$\begin{aligned} \text{Area of 1st half period zone} &= \pi OM_1^2 = \pi (PM_1^2 - OP^2) \\ &= \pi [(a + \frac{\lambda}{2})^2 - a^2] = \pi [a\lambda + \frac{\lambda^2}{4}] \approx \pi a\lambda. \end{aligned}$$

$$\text{Similarly } OM_n^2 = PM_n^2 - OP^2 = (a + \frac{n\lambda}{2})^2 - a^2 = n a \lambda.$$

( $n^{\text{th}}$  circle)

$$OM_{n-1}^2 = a(n-1)\lambda \quad ((n-1)^{\text{th}} \text{ circle}).$$

$$\text{So Area of } n^{\text{th}} \text{ zone} = \pi (OM_n^2 - OM_{n-1}^2) = \pi a \lambda.$$

So radii of zone  $\propto \sqrt{n}$ .  
area of zone independent of  $n$



## Schuster's Method :

For visible light,  $\lambda \approx$  small & so area of zone  $= \pi a \lambda$  but if  $\lambda$  is not very small then the area of half period zones of higher order decreases gradually. If the phase of the wavelets coming from O is zero then the phase of wavelets from intermediate points between O and  $M_1$  will vary from 0 to  $\pi$  (because  $\frac{2\pi}{\lambda} (PM_1 - OP) = \pi$ ).

∴ Average phase of all wavelets from 1<sup>st</sup> zone  $= \frac{0 + \pi}{2} = \frac{\pi}{2}$ .

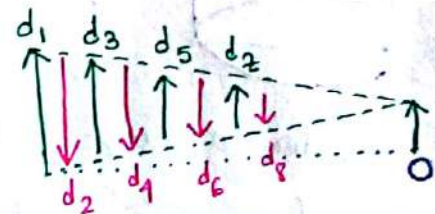
Similarly phase difference of wavelets from  $M_1$  &  $M_2$  will be between  $\pi$  and  $2\pi$ , so that average phase of all wavelets from 2<sup>nd</sup> zone  $= \frac{\pi + 2\pi}{2} = \frac{3\pi}{2}$ , from 3<sup>rd</sup> zone  $\frac{5\pi}{2}$ , from 4<sup>th</sup> zone  $\frac{7\pi}{2}$  & so on...

Resultant phase-difference between two consecutive zones  $= \pi$ .

Resultant phase-difference between two alternate zones  $= 2\pi$ .

So if resultant from 1<sup>st</sup> half period zone is **positive** then 2<sup>nd</sup> half period zone is **negative**.

Amplitude decreases due to obliquity factor  $(1 + \cos \theta)$ , so resultant amplitude



$$D = d_1 - d_2 + d_3 - d_4 + d_5 - \dots \pm d_n.$$

(i) If  $n = \text{odd}$ , to a first approximation  $d_2 = \frac{d_1 + d_3}{2}$ ,  $d_4 = \frac{d_3 + d_5}{2}$

$$\begin{aligned} \text{So that } D &= \frac{d_1}{2} + \left( \frac{d_1 + d_3}{2} - d_2 \right) + \left( \frac{d_3 + d_5}{2} - d_4 \right) + \dots + \frac{d_n}{2} \\ &= \frac{d_1}{2} + \frac{d_n}{2}. \end{aligned}$$

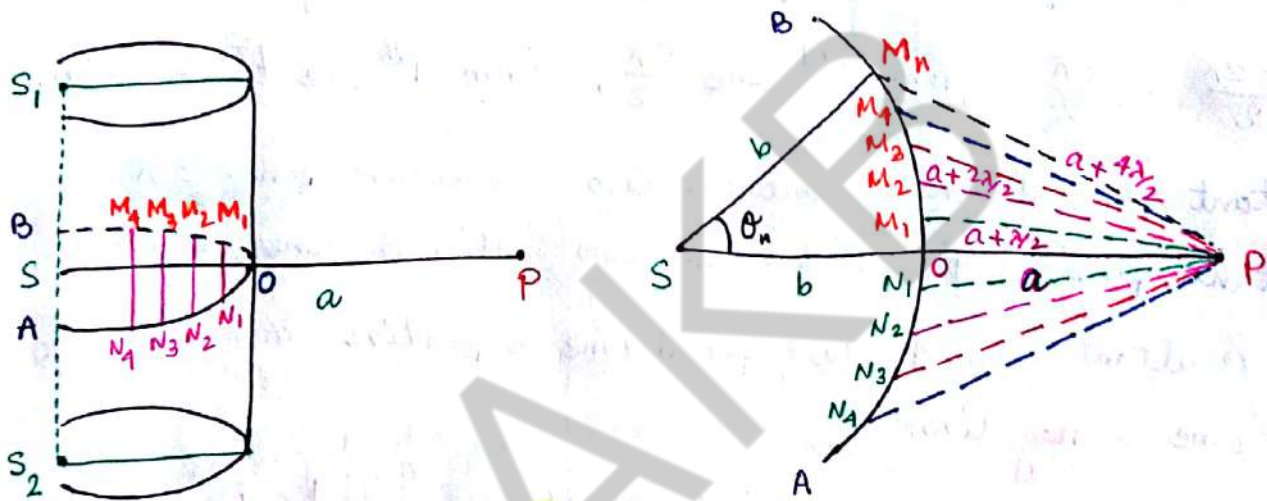
(ii) If  $n = \text{even}$ ,  $D = \frac{d_1}{2} + \frac{d_{n-1}}{2} - d_n$

If  $n$  is very large, then effect from  $n^{\text{th}}$  zone is negligible &

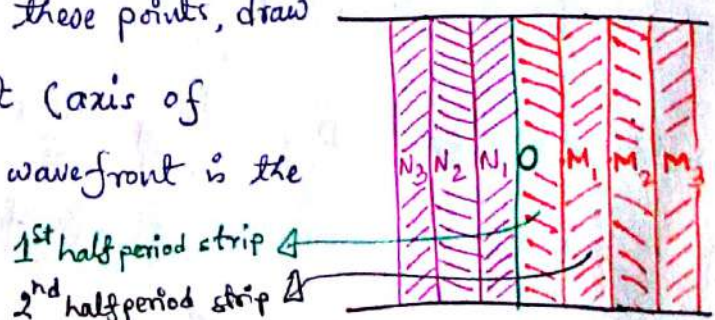


resultant amplitude due to whole wave is  $D = \frac{d_1}{2}$  as 1.52  
 intensity  $I = D^2 = \frac{d_1^2}{4}$ . If an obstacle is placed at O then  
 the resultant disturbance at P is = half the disturbance due to  
 wavelets from the 1<sup>st</sup> half-period zone with one-fourth the intensity.  
 If obstacle at O blocks a considerable number of half-period  
 zones, effect is negligible & no light is received at P - or light  
travels approximately in a straight line.

### Fresnel's half-period strip of a cylindrical wavefront



Consider a long and narrow slit  $S_1S_2$ , when illuminated by monochromatic light of wavelength  $\lambda$ , produces cylindrical wavefront. To find the resultant amplitude, the wavefront can be divided into half period strips, with O as pole. Consider an equatorial section AOB through O in plane of paper. With P as centre & radius  $(a + \frac{\lambda}{2})$ ,  $(a + \frac{2\lambda}{2})$ , ... etc, draw arcs that cut AOB at point  $M_1N_1$ ,  $M_2N_2$ , ... etc. Through these points, draw lines parallel to length of slit (axis of wavefront) and the area of the wavefront is the half period strip.





Amplitude of the waves reaching P due to wavelets produced by each half-period strip is

- (i) Directly proportional to the area of the strip (not equal)
- (ii) Average distance of strip from P
- (iii) Varies with the obliquity factor  $(1 + \cos \theta)$

As length of strip is same, so areas are proportional to arcs  $OM_1, M_1M_2, M_2M_3, \dots$  where  $PM_n = a + \frac{n\lambda}{2}$

from triangle  $PM_nS$ , we have  $PM_n^2 = SM_n^2 + PS^2 - 2SM_nPS \cos \theta_n$

$$\left(a + \frac{n\lambda}{2}\right)^2 = b^2 + (a+b)^2 - 2b(a+b) \cos \theta_n$$

$(1 - \cos \theta_n \approx \frac{\theta_n^2}{2})$

$$a^2 + an\lambda + \frac{n^2\lambda^2}{4} = b^2 + a^2 + 2ab - 2ab - 2b^2 + b(a+b)\theta_n^2$$

$$an\lambda = b(a+b)\theta_n^2 \quad \therefore \theta_n = \sqrt{\frac{an\lambda}{b(a+b)}} = K\sqrt{n}$$

Now  $OM_n = b\theta_n = bK\sqrt{n}$

So  $OM_1 = bK, OM_2 = bK\sqrt{2}, OM_3 = bK\sqrt{3}$

So  $M_1M_2 = bK(\sqrt{2} - 1) = 0.414 bK$

$M_2M_3 = bK(\sqrt{3} - \sqrt{2}) = 0.318 bK$

$M_3M_4 = bK(\sqrt{4} - \sqrt{3}) = 0.268 bK, M_4M_5 = 0.236 bK, \dots$

So area of strip initially decreases rapidly & then for increasing order more slowly. and because of opposite sign they cancel out each other. So the resultant at P is only due to first few half period strips.

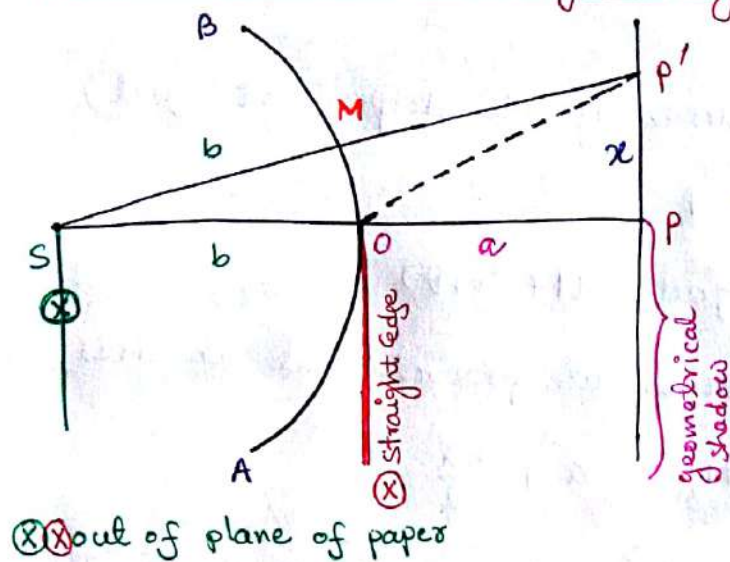
$$D = d_1 - d_2 + d_3 - d_4 + \dots \approx \frac{d_1}{2} \quad \begin{matrix} \text{(left side)} \\ \text{(from half wavefront)} \end{matrix}$$

$$\approx \frac{d_1}{2} \quad \begin{matrix} \text{(from right side half wavefront)} \end{matrix}$$

So resultant due to whole wavefront  $= \frac{d_1}{2} \pm \frac{d_1}{2} = d_1 \text{ (n odd)}$   
 $= 0 \text{ (n even)}$



# Diffraction at a straight edge



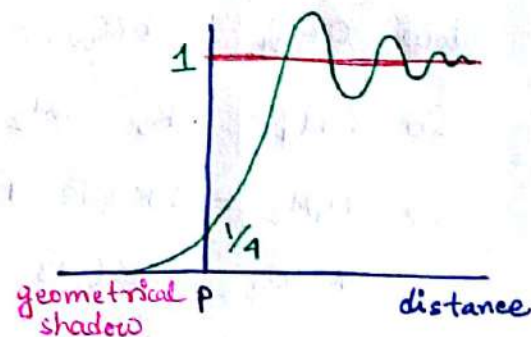
Consider a straight edge at O and an illuminated narrow slit S parallel to each other. Dark & bright bands of unequal width of varying intensity is observed in geometrical shadow.

We study intensity at P' with M as pole and construct Fresnel's half-period strip. The effect at P' depends upon the number of half-period strips contained in OM & BM.

Due to straight edge, the effect at P is due to the upper half of the wavefront only, so displacement at P is  $\frac{1}{2}$  of the displacement for whole wavefront or  $\frac{1}{4}$  of the full wavelet intensity.

# of half-period strips contained in BM depends on the path difference  $OP' - MP'$

$$\text{Now } OP' = \sqrt{a^2 + x^2} = a \left(1 + \frac{x^2}{a^2}\right)^{\frac{1}{2}} \\ \approx a \left(1 + \frac{x^2}{2a^2}\right) = a + \frac{x^2}{2a}$$



$$SP' = \sqrt{(a+b)^2 + x^2} = a+b + \frac{x^2}{2(a+b)}$$

$$\therefore MP' = SP' - SM = a + \frac{x^2}{2(a+b)}$$

$$\therefore \text{Path difference } OP' - MP' = a + \frac{x^2}{2a} - a - \frac{x^2}{2(a+b)} = \frac{bx^2}{2a(a+b)}$$

for the displacement to be maximum,

$$\frac{bx^2}{2a(a+b)} = (2n+1) \frac{\lambda}{2} \quad \text{or} \quad x = \left[ \frac{a(a+b)(2n+1)\lambda}{b} \right]^{\frac{1}{2}}, n=0,1,2,\dots$$

$x \propto \sqrt{2n+1}$  (bright band)



For the displacement to be minimum,  $\frac{bx^2}{2a(a+b)} = n\lambda$

$$\therefore x = \left[ \frac{2a(a+b)n\lambda}{b} \right]^{1/2}, \quad n=1, 2, 3, \quad x \propto \sqrt{n} \text{ (dark band)}$$

Using these, wavelength of light can be found.

CW A narrow slit illuminated by light of  $\lambda = 5890 \text{ \AA}$  is located at a distance of  $0.1 \text{ m}$  from a straight edge. If the measurements are made at a distance of  $0.5 \text{ m}$  from the edge, calculate the distance between 1<sup>st</sup> & 2<sup>nd</sup> dark band.

For  $n^{\text{th}}$  dark band  $x = \sqrt{\frac{2a(a+b)n\lambda}{b}}$

$$a = 0.5 \text{ m}$$

$$b = 0.1 \text{ m}$$

$$\lambda = 5890 \times 10^{-10} \text{ m}$$

$$\therefore x_2 - x_1 = \sqrt{\frac{2a(a+b)\lambda}{b}} (\sqrt{2} - 1)$$

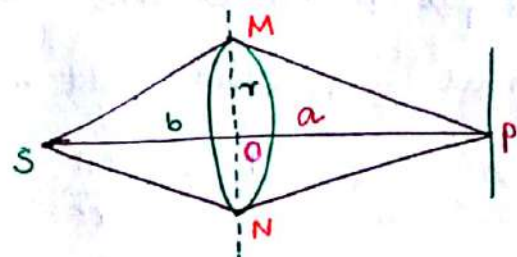
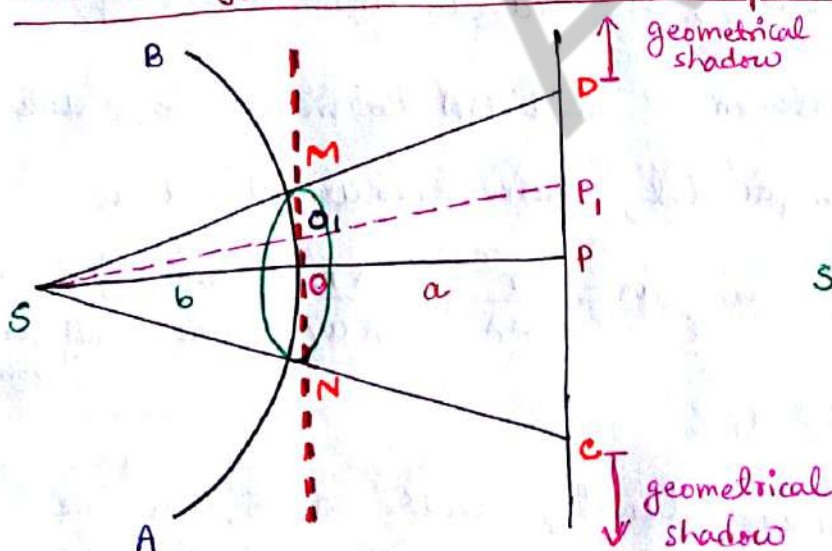
$$= 0.7786 \times 10^{-3} \text{ m}$$

# Read about diffraction of light by a thin wire. Fringe width

$$\beta = \frac{D\lambda}{d}, \quad D = \text{distance between obstacle \& crosswire of Eyepiece,}$$

$$\lambda = \text{wavelength of light.}$$

### Fresnel's diffraction at a circular aperture



From a point source  $S$  a wavefront (spherical) touches a circular aperture  $MN$ . To calculate the amplitude at screen  $P$ , we need to divide the wavefront  $MON$  into Fresnel's half-period zones about the pole  $O$ .



### Intensity at an axial point P :

If only the 1<sup>st</sup> half period zone is exposed then amplitude at P is twice the amplitude if the whole wavefront is exposed, or intensity will be four times. Let the amplitude is  $d_1$ .

If the screen is moved towards the aperture so that 1<sup>st</sup> & 2<sup>nd</sup> half-period zones are exposed then amplitude  $= d_1 - d_2 \approx 0$  as  $d_1 \approx d_2$  so dark & bright fringes will form as more half-period zones are exposed.

Path difference for waves reaching P along SMP & SOP is

$$= (SM + MP) - (SO + OP) = \sqrt{b^2 + r^2} + \sqrt{a^2 + r^2} - (b + a)$$

$$\approx b\left(1 + \frac{r^2}{2b^2}\right) + a\left(1 + \frac{r^2}{2a^2}\right) - (b + a) = \frac{r^2}{2}\left(\frac{1}{a} + \frac{1}{b}\right)$$

If the aperture contains  $n$  half-period zones then path difference is  $\frac{n\lambda}{2}$ . So  $\frac{r^2}{2}\left(\frac{1}{a} + \frac{1}{b}\right) = \frac{n\lambda}{2}$  or  $\frac{1}{a} + \frac{1}{b} = \frac{n\lambda}{r^2}$ .

$n = \text{even}$  (minimum intensity),  $n = \text{odd}$  (maximum intensity).

If we put a convex lens between S and MN to make the plane wavefront (incident light is parallel, source lies at  $\infty$ ) then

$$b = \infty, \quad \therefore \frac{1}{a} = \frac{n\lambda}{r^2} \quad \text{or} \quad n = \frac{r^2}{a\lambda} = \frac{\pi r^2}{\pi a\lambda} = \frac{\text{area of aperture}}{\text{area of half-period zone.}}$$

### Intensity at a non-axial point P<sub>1</sub> :

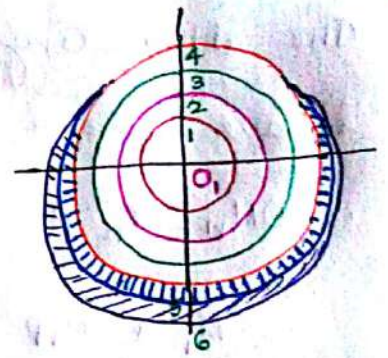
Suppose at P we have maximum intensity with  $n = 5$ . As we move up to P<sub>1</sub>, the pole shifts to O<sub>1</sub>. Here suppose only 4 zones are completely exposed while  $\frac{1}{2}$  of 5<sup>th</sup> and 6<sup>th</sup> zone are exposed, so that resultant displacement at P<sub>1</sub>

$$= d_1 - d_2 + d_3 - d_4 + \frac{d_5}{2} - \frac{d_6}{2}$$



$$= \frac{d_1}{2} + \left( \frac{d_1 + d_3}{2} - d_2 \right) + \left( \frac{d_3 + d_5}{2} - d_4 \right) - \frac{d_6}{2}$$

$$= \frac{d_1}{2} - \frac{d_6}{2}. \text{ So the intensity will be minimum.}$$



If we move up to  $P_2$  then intensity will be maximum as first 3 zones are completely exposed and  $\frac{1}{2}$  of 4th, 5th, 6th, 7th zones are exposed. So there will be concentric alternating bright & dark rings.

### Diffraction at a circular obstacle

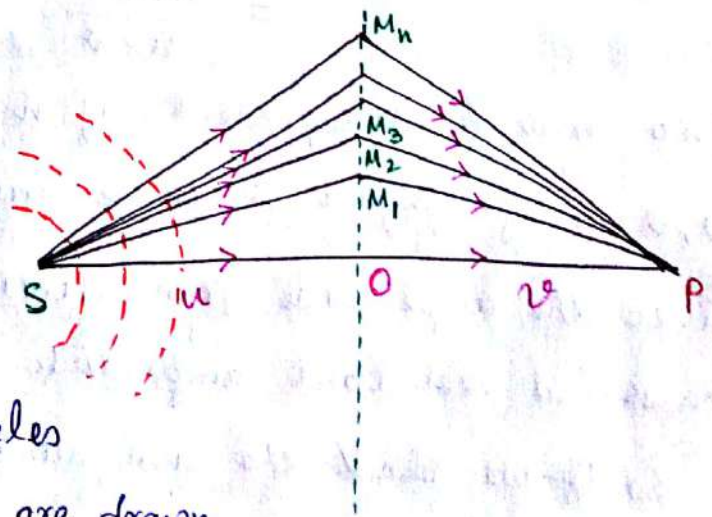
Here if the obstacle obstruct only the 1st half-period zone then at  $P$ , displacement =  $-d_2 + d_3 - d_4 + d_5 \dots = -\frac{d_2}{2}$ .  $\therefore I \propto \frac{d_2^2}{4}$ .

If size of obstacle is increased or point  $P$  is brought near so that 2nd, 3rd, ... etc zones are obstructed then displacement is  $\frac{d_3}{2}, -\frac{d_4}{2}$ , or  $I \propto \frac{d_3^2}{4}, \frac{d_4^2}{4}, \dots$ . So  $P$  remain always bright, which is actually the geometrical shadow.

For any other point  $P_1, P_2$ , etc within the geometrical shadow, diffracted waves interfere due to phase difference & produce interference band (circular). Outside the geometrical shadow, we get diffraction band of unequal width.

### Zone Plate

The idea of Fresnel's half period zone can be used to construct a transparent plate on which circles with radii proportional to  $\sqrt{n}$  are drawn.





The alternating annular zones are blocked, so that the plate behaves like a convex lens. So by construction  $OM_1 = r_1$ ,  $OM_2 = r_2$ ,  $\dots$   $OM_n = r_n$  are the radius of the circles and

$$SM_1 + M_1P = SO + OP + \frac{\lambda}{2}$$

$$SM_2 + M_2P = SO + OP + \lambda$$

$$\vdots$$

$$SM_n + M_nP = SO + OP + n\lambda/2 \quad \text{--- (1)}$$

So annular rings are half-period zones, consecutive zone differs by  $\lambda/2$ .

If  $SO = u$ ,  $OP = v$  then  $SM_n = \sqrt{SO^2 + OM_n^2} = \sqrt{u^2 + r_n^2} \simeq u \left(1 + \frac{r_n^2}{2u^2}\right)$   
 $= u + \frac{r_n^2}{2u}$ , ( $u \gg r_n$ ).

Similarly  $M_nP = \sqrt{v^2 + r_n^2} \simeq v + \frac{r_n^2}{2v}$ .

So from equation (1),  $u + \frac{r_n^2}{2u} + v + \frac{r_n^2}{2v} = u + v + n\lambda/2$

$$r_n^2 \left(\frac{1}{u} + \frac{1}{v}\right) = n\lambda$$

Applying the sign convention  $u \rightarrow -u$ ,  $r_n^2 = \frac{n\lambda uv}{u-v}$

So  $r_n \propto \sqrt{n}$  for  $\lambda, u, v = \text{constant}$ .

$$\begin{aligned} \text{Area of } n^{\text{th}} \text{ zone} &= \pi(r_n^2 - r_{n-1}^2) = \pi \left[ \frac{n\lambda uv}{u-v} - \frac{(n-1)\lambda uv}{u-v} \right] \\ &= \frac{\pi\lambda uv}{u-v} \neq f(n) \end{aligned}$$

So area is independent of  $n$  & decreases for decreasing  $u, v$  or if object or image are brought near to the zone plate. Since the amplitude from alternate zones will have opposite phases so resultant amplitude at P will be  $d = d_1 - d_2 + d_3 - d_4 + \dots$

So if we block the even number or the odd number of half period zones then the resultant amplitude at P will be either



$$d = d_1 + d_3 + d_5 + \dots \quad \text{or} \quad d = d_2 + d_4 + d_6 + \dots$$

So intensity at P is many times brighter than that due to all exposed zones, so that light from S can be focussed at P. So the result is similar to a convex lens. When  $u = \infty$ ,  $v = f$  so that  $\frac{1}{u} + \frac{1}{v} = \frac{1}{f}$  where  $f = \frac{r_n^2}{n\lambda}$  is the focal length of the zoneplate. So zoneplate acts like a convex lens.

### Construction of zoneplate:

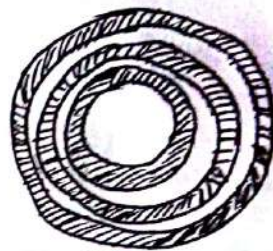
Zoneplate is a system of areas corresponding to half-period zones.

Concentric circles with radii  $\propto$

Natural number are drawn on a white paper/glass. Alternate zones are painted black - if odd zones are transparent & even zones are opaque then it's a positive zone plate, otherwise a negative zone plate.



negative zone plate



positive zone plate

### Phase reversal in a zoneplate:

R.W. Wood coated the even no. zones with a thin film of transparent substance made of Gelatin mixed with  $K_2Cr_2O_7$ , instead of painting them black. As a result, the phase of the waves traversing the even number zones change phase  $\pi$ , producing intensity at P 4-fold as

$$d = d_1 + d_2 + d_3 + d_4 + \dots$$

Such type of zoneplates are used as objectives of telescope, photographic camera etc.



## Difference between a zoneplate & convex lens

(i) For a particular wavelength, a convex lens has a single focal length, but for a zone plate, there are a number of focal lengths between the plate and bright focus (multiple foci)

$f = \frac{r_n^2}{n\lambda}$ . So for a fixed distance of object, lens produces one image whereas zoneplate produces a number of images. Depending on the position of screen, it may contain 3 or 5 or 7 half-period zone & intensity of image decreases with decreasing focal length

$$f_1 = \frac{r_n^2}{n\lambda}, f_2 = \frac{r_n^2}{3n\lambda}, f_3 = \frac{r_n^2}{5n\lambda}, \dots$$

(ii) Light in passing through the lens takes equal time to go from S to P through any part of lens whereas in a zoneplate disturbances from any transparent zone reach P one-period later than the disturbances from the next inner zone.

(iii) Focal length of a lens is  $\frac{1}{f} = (\mu - 1) \left( \frac{1}{R_1} - \frac{1}{R_2} \right)$  whereas for zoneplate is  $\frac{1}{f} = \frac{n\lambda}{r_n^2}$ .

(iv) Focal length of lens is proportional to  $\lambda$ , so is greater for red rays than violet. Focal length is inversely proportional to  $\lambda$  for zoneplate & so is greater for violet than red rays.

Q What is the radius of 1<sup>st</sup> zone of a zoneplate of focal length 0.2 m for a light of wavelength 5000 Å?

$$\lambda = 5000 \text{ Å} = 5 \times 10^{-7} \text{ m}, f = 0.2 \text{ m}, n = 1, \text{ so } f = \frac{r_1^2}{\lambda}$$

$$\therefore r_1 = \sqrt{f\lambda} = 3.16 \times 10^{-4} \text{ m}.$$



CW Calculate the radii of the first 3 clear elements of a zone plate which is designed to bring a parallel beam of light of wavelength  $6000 \text{ \AA}$  to the first focus at a distance of 2 metres.

parallel light means  $u = \infty$ ,  $v = f$  (first focus)

$$v = f = 2 \text{ m.}, \lambda = 6000 \text{ \AA} = 6 \times 10^{-7} \text{ m.}, r_n = \sqrt{n \lambda f}.$$

$$\text{For 1st clear zone } n=1, r_1 = \sqrt{\lambda f} = 1.095 \times 10^{-3} \text{ m.}$$

$$\text{For 2nd clear zone } n=3, r_2 = \sqrt{3 \lambda f} = 1.897 \times 10^{-3} \text{ m.}$$

$$\text{For 3rd clear zone } n=5, r_3 = \sqrt{5 \lambda f} = 2.449 \times 10^{-3} \text{ m.}$$

CW A plane wavefront ( $\lambda = 6000 \text{ \AA}$ ) advancing towards a point is divided into a number of half-period zones. Amplitude contribution of these half-period zones is 1, 0.98, 0.96, ... 0. Compare the intensities at the point when first 31 & 36 halfperiod zone are only exposed.

$$d_1 = 1, d_2 = 0.98, d_3 = 0.96, \dots d_n = 0.$$

$$\text{So } \frac{d_1 + d_3}{2} = d_2, \quad d_1 - d_2 = 1 - 0.98 = 0.02$$

$$d_{31} = 1 - 30 \times 0.02 = 0.40$$

$$d_{35} = 1 - 34 \times 0.02 = 0.32$$

$$d_{36} = 1 - 35 \times 0.02 = 0.30$$

$$\text{So resultant amplitude of 31 zones} = \frac{d_1}{2} + \frac{d_{31}}{2} = \frac{1}{2} + \frac{0.4}{2} = 0.7$$

$$\text{resultant amplitude of 36 zones} = \frac{d_1}{2} + \frac{d_{35}}{2} - d_{36}$$

$$= \frac{1}{2} + \frac{0.32}{2} - 0.3 = 0.36.$$

$$\therefore \frac{I_{31}}{I_{36}} = \frac{0.7^2}{0.36^2} = 3.78.$$

CW A zoneplate is found to give series of images of a point source on the axis. If the strongest and the 2nd strongest images are at distances of 0.3 m and 0.06 m respectively from the zoneplate (both on same side) calculate the distance of the source from the zoneplate, principle focal length



and radius of 1<sup>st</sup> zone for  $\lambda = 5 \times 10^{-7} \text{ m}$ .

$$\lambda = 5 \times 10^{-7} \text{ m}, \quad v_1 = 0.3 \text{ m}, \quad v_2 = 0.06 \text{ m}.$$

$$f_1 = \frac{r_n^2}{\lambda}, \quad f_2 = \frac{r_n^2}{3\lambda} \quad \therefore f_2 = f_1/3.$$

If  $u$  is the distance of the object from zone plate then

$$\frac{1}{u} = \frac{1}{v_1} - \frac{1}{f_1} \quad \text{and} \quad \frac{1}{u} = \frac{1}{v_2} - \frac{1}{f_2}$$

$$\therefore \frac{1}{v_1} - \frac{1}{f_1} = \frac{1}{v_2} - \frac{3}{f_1} \quad \therefore \frac{2}{f_1} = \frac{1}{v_2} - \frac{1}{v_1} = \frac{1}{0.06} - \frac{1}{0.3}$$

$$\therefore f_1 = 0.15 \text{ m.} \rightarrow \text{principal focal length}$$

$$\text{Now } r_1 = \sqrt{f_1 \lambda} = 0.274 \times 10^{-4} \text{ m.} \quad \text{radius of 1<sup>st</sup> zone and from}$$

$$\frac{1}{u} = \frac{1}{v_1} - \frac{1}{f_1} = \frac{1}{0.3} - \frac{1}{0.15}, \quad u = -0.3 \text{ m.}$$

$\rightarrow$  distance from source to zone plate

### Fraunhofer Diffraction (far-field)

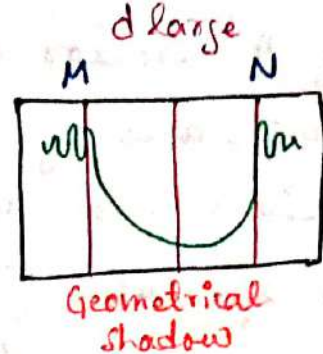
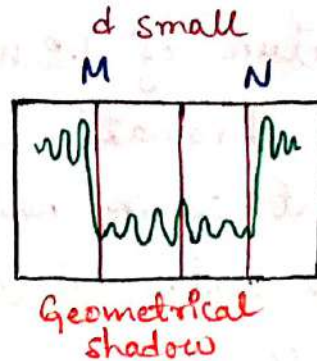
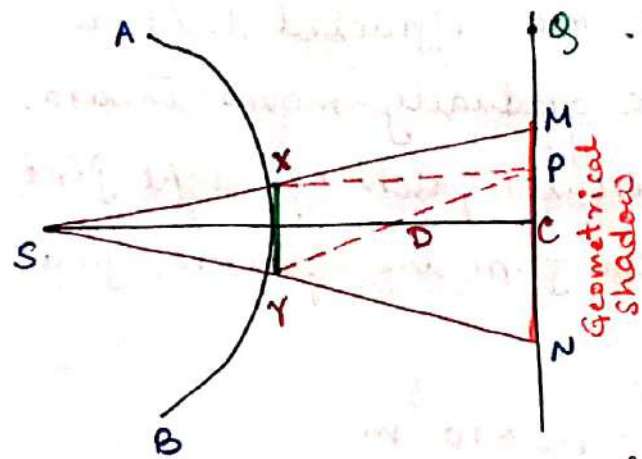
Single slit diffraction : A single slit is a vacant space which is obstructed by two sharp opaque regions. When a monochromatic light is incident on such a slit, it is found that the intensity on the opposite side has a variation and maximum & minimum brightness are observed, which are called diffraction bands. This phenomena occurs due to diffraction of light.

#### Theory :

Let a parallel beam of monochromatic light of wavelength  $\lambda$  is incident on a narrow slit of width  $a$  in a direction making an angle  $i$  with the normal. After diffraction, they are scattered in various direction. We will calculate the intensity at screen due to the rays diffracted at an angle  $\theta$  with the normal.



# Diffraction at a wire



$S$  = rectangular slit,  $XY$  = wire with thickness  $d$ . At point  $Q$  outside the

geometrical shadow intensity distribution is same as straight edge at  $X$  and so diffraction bands of unequal width is formed above  $M$  & below  $N$ . These bands are independent of thickness of wire and effect on other side is negligible (because wire stops the important half-period strips).

Within geometric shadow, interference fringes appear. Effect due to  $AX$  of cylindrical wavefront at  $P$  in geometrical shadow is entirely due to few half-period strips at  $X$ , so a small luminous source can be thought at  $X$ . Similarly for  $BY$  portion,  $Y$  is a luminous source. If  $PY - PX = n\lambda$ , point  $P$  will be bright and  $= (2n+1)\frac{\lambda}{2}$ ,  $P$  will be dark.

Equal interference fringe width  $\beta = \frac{D}{d} \lambda$ .

$D$  = distance of screen from obstacle (wire)

$d$  = thickness of obstacle (wire diameter).

point  $C$  will be always bright as waves from  $X$  &  $Y$  always meet in phase. for moderate value of  $d$  pattern is shown, while as  $d$  is increased,  $\beta$  decreases finally to disappear, so only diffraction band above  $M$  & below  $N$  is seen.



QW A circular aperture of 1.2 mm diameter is illuminated by plane waves of monochromatic light. The diffracted light is received on a distant screen which is gradually moved towards the aperture. If the centre of the circular patch of light first becomes dark, when the screen is 30 cm from the aperture, find the wavelength of light used.

Aperture diameter  $2r = 1.2 \text{ mm} = 1.2 \times 10^{-3} \text{ m}$

So radius  $r = 0.6 \times 10^{-3} \text{ m}$ ,  $a = 30 \text{ cm} = 0.3 \text{ m}$ .

for the first minimum on the axial point, the aperture must have 2 half-period zones. So,  $n = \frac{\pi r^2}{\pi a \lambda} = 2$ .

$$\therefore \lambda = \frac{r^2}{2a} = \frac{(0.6 \times 10^{-3})^2}{2 \times 0.3} = 6 \times 10^{-7} \text{ m} = 6000 \text{ \AA}.$$

QW Light of wavelength 6000 Å passes through a narrow circular aperture of radius  $0.9 \times 10^{-3} \text{ m}$ . At what distance along the axis will the first maximum intensity be observed?

$\lambda = 6000 \times 10^{-10} \text{ m}$ ,  $r = 0.9 \times 10^{-3} \text{ m}$ .  $a = ?$

for first maximum intensity  $a^2 + r^2 = \left(a + \frac{\lambda}{2}\right)^2$

$$\therefore a^2 + r^2 = a^2 + \frac{\lambda^2}{4} + 2a\lambda/2 \quad \therefore r^2 = a\lambda.$$

$$\therefore a = \frac{r^2}{\lambda} = \frac{(0.9 \times 10^{-3})^2}{6000 \times 10^{-10}} = 1.35 \text{ m}.$$