

## Advanced Robust Control | HW4 | amithr3

1. Using the pitch axis aircraft plant data (same as RSLQR design model in homework 3) design a Hinf state feedback controller to command Az. Include the 2<sup>nd</sup> order actuator in the design model as presented in class. Tune the Hinf controller to yield a similar rise time as your RSLQR controller.

List out all matrices used in the Hinf design, closed loop eigenvalues, and eigenvectors.

List the controller matrices  $(A_c, B_{c1}, B_{c2}, C_c, D_{c1}, D_{c2})$  implementing the Hinf control.

$$\dot{x}_c = A_c x_c + B_{c1} y + B_{c2} r$$

$$u = C_c x_c + D_{c1} y + D_{c2} r$$

where  $y = x_p$ .

Plant Model

$$\dot{x}_p = A_p x_p + B_p u$$

$$y = C_p x_p + D_p u$$

$x_p$  = AOA (rad), pitch rate q (rps), dele (rad), deledot (rps)

$u$  = delec (rad)

$y$  = Az (fps2), AOA (rad), pitch rate q (rps), dele (rad), deledot (rps)

Target lgcf = 1.2 Hz

WS SS Model

[ A B ]

[ C D ]

WS =

0 1.0000e+00  
3.7699e+00 5.0000e-01

WT SS Model

[ A B ]

[ C D ]

WT SS Model

[ A B ]

[ C D ]

WT =

-2.0000e+02 1.0000e+00  
-9.3024e+02 5.3582e+00

WC =

WT SS Model

[ A B ]

[ C D ]

0 0  
0 1.0000e-01

Gamma optimal = 1

K optimal = [ 11.3599 0.794031 -1.22049 -0.0106452 -0.0532245 -0.131007 ]

Norm EE opt = 5.0787e-06

gamma =

1.0020e+00

## Controller Matrices:

```
Ac = [ Ws.A      0.;  
       0.      Wt.A];  
Bc1 = [ Ws.B*[1 0 0 0 0]  
        Wt.B*[1 0 0 0 0]];  
Bc2 = [-Ws.B  
        0.];  
Cc = [ HinfSF.Kxref(:,5:6) ];  
Dc1 = [ 0. HinfSF.Kxref(:,1:4)];  
Dc2 = [ 0. ];
```

Ac =

```
0      0  
0 -200
```

Bc1 =

```
1      0      0      0      0  
1      0      0      0      0
```

Bc2 =

```
-1  
0
```

Cc =

```
-5.2052e-02 -1.3157e-01
```

Dc1 =

```
0      1.1136e+01      7.8214e-01      -1.2022e+00      -1.0492e-02
```

Dc2 =

```
0
```

Controller Model

```
[ Ac Bc1 Bc2 ]
```

HH =

```
0      0      1      0      0      0      0      -1  
0 -200      1      0      0      0      0      0
```

```
[ Cc Dc1 Dc2 ]
```

HH =

```
-5.2052e-02 -1.3157e-01      0      1.1136e+01      7.8214e-01      -1.2022e+00      -1.0492e-02      0
```

## Closed Loop Eigenvalues

Pole	Damping	Frequency (rad/TimeUnit)	Time Constan (TimeUnit)
-1.93e+02	1.00e+00	1.93e+02	5.17e-03
-6.02e+01	1.00e+00	6.02e+01	1.66e-02
-2.99e+01 + 3.63e+01i	6.36e-01	4.71e+01	3.34e-02
-2.99e+01 - 3.63e+01i	6.36e-01	4.71e+01	3.34e-02
-2.62e+01	1.00e+00	2.62e+01	3.82e-02
-9.60e+00	1.00e+00	9.60e+00	1.04e-01

V =

Columns 1 through 5

```

8.7622e-06 + 0.0000e+00i -4.3496e-04 + 0.0000e+00i -8.8610e-04 + 3.4807e-04i -8.8610e-04 - 3.4807e-04i -6.2125e-03 + 0.0000e+00i
-2.7789e-03 + 0.0000e+00i 2.9184e-02 + 0.0000e+00i 9.8450e-03 - 4.5657e-02i 9.8450e-03 + 4.5657e-02i 1.6245e-01 + 0.0000e+00i
-5.1199e-03 + 0.0000e+00i 1.6572e-02 + 0.0000e+00i -1.3420e-02 - 1.6292e-02i -1.3420e-02 + 1.6292e-02i 3.7700e-02 + 0.0000e+00i
9.8963e-01 + 0.0000e+00i -9.9829e-01 + 0.0000e+00i 9.9382e-01 + 0.0000e+00i 9.9382e-01 + 0.0000e+00i -9.8598e-01 + 0.0000e+00i
-4.9789e-03 + 0.0000e+00i 4.3903e-02 + 0.0000e+00i -4.1331e-03 - 9.4947e-02i -4.1331e-03 + 9.4947e-02i -1.0003e-03 + 0.0000e+00i
1.4344e-01 + 0.0000e+00i -1.8923e-02 + 0.0000e+00i 2.3334e-02 + 1.0843e-02i 2.3334e-02 - 1.0843e-02i 1.5048e-04 + 0.0000e+00i

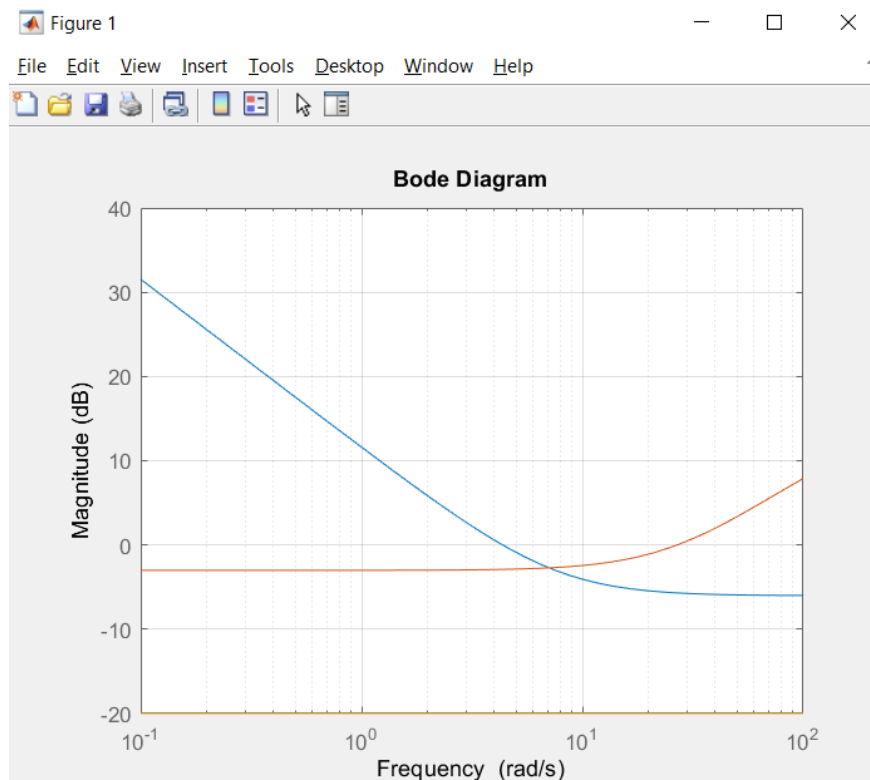
```

Column 6

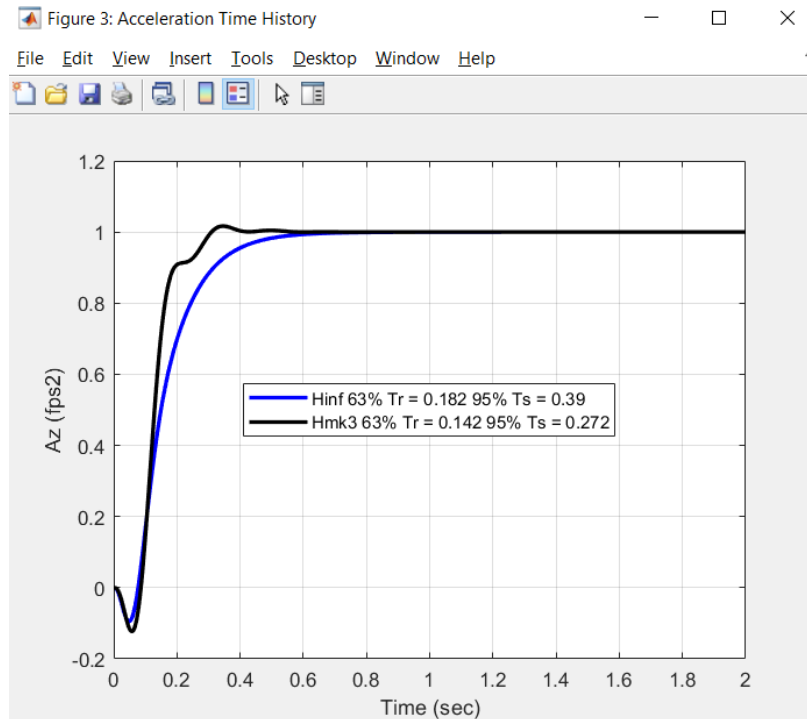
```

-8.7084e-03 + 0.0000e+00i
7.2834e-02 + 0.0000e+00i
2.7076e-03 + 0.0000e+00i
-2.5998e-02 + 0.0000e+00i
-9.9570e-01 + 0.0000e+00i
5.0212e-02 + 0.0000e+00i

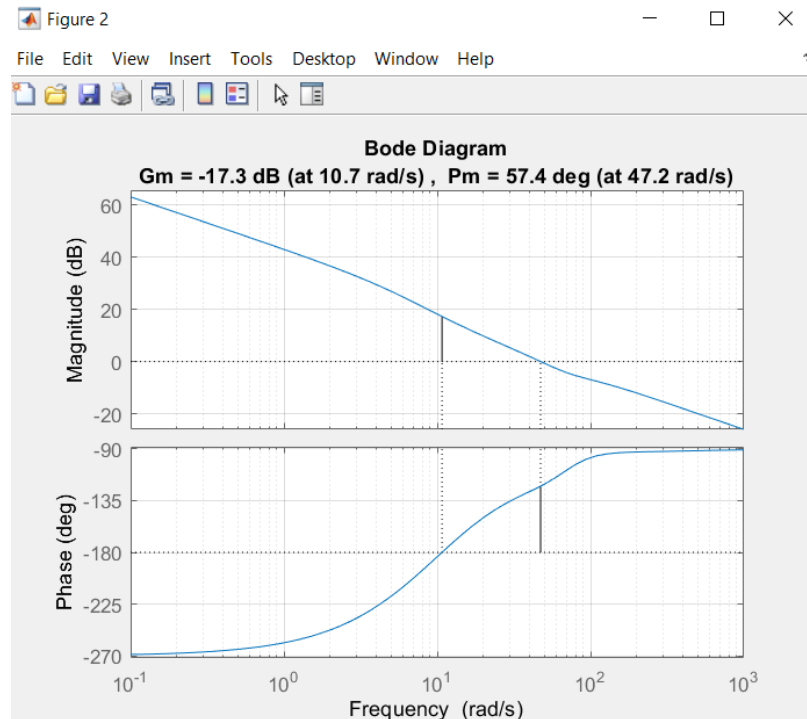
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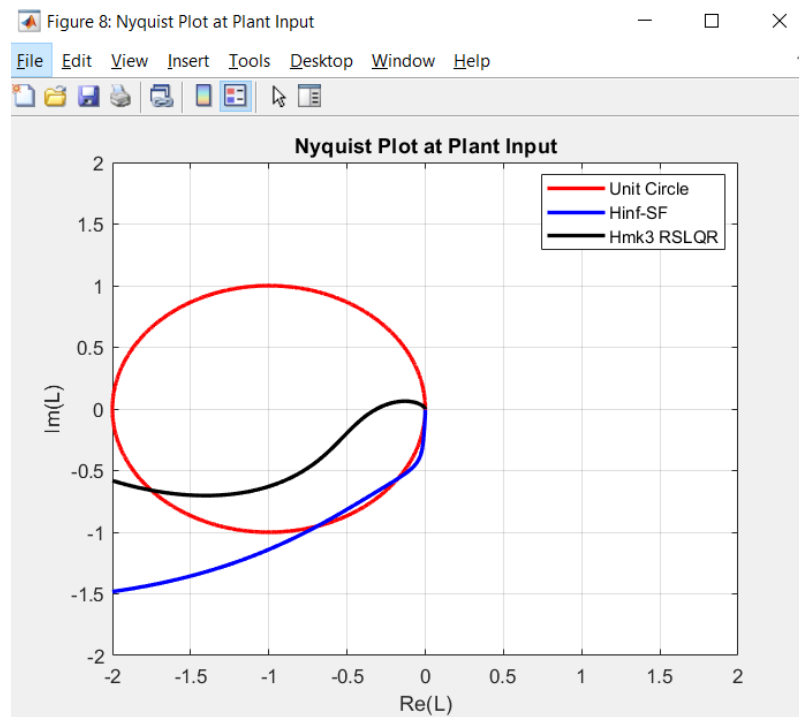
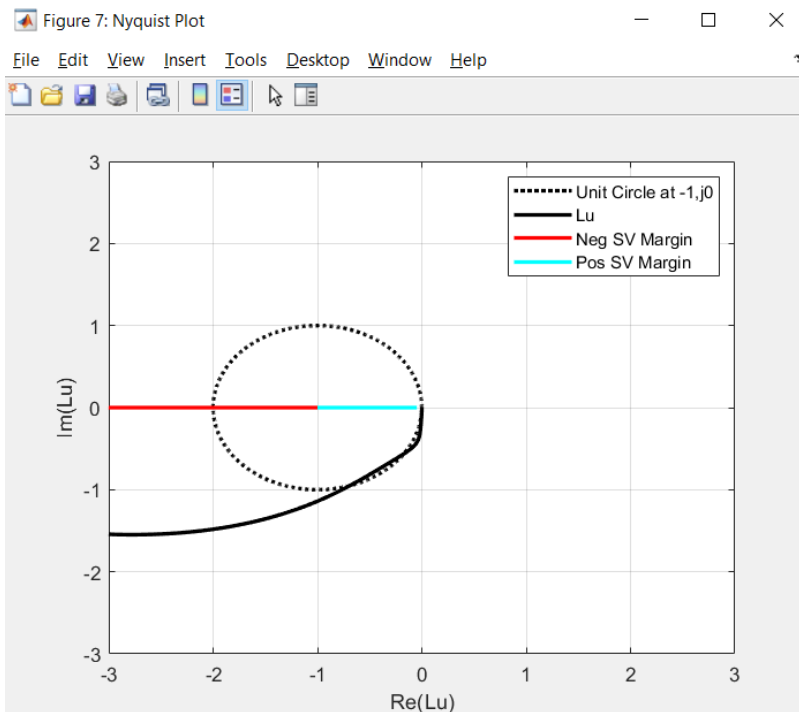


- a) Simulate the closed loop system to a unit step Az command. Plot the RSLQR response with the Hinf response. Compute the rise time and settling time. Label on the plot.

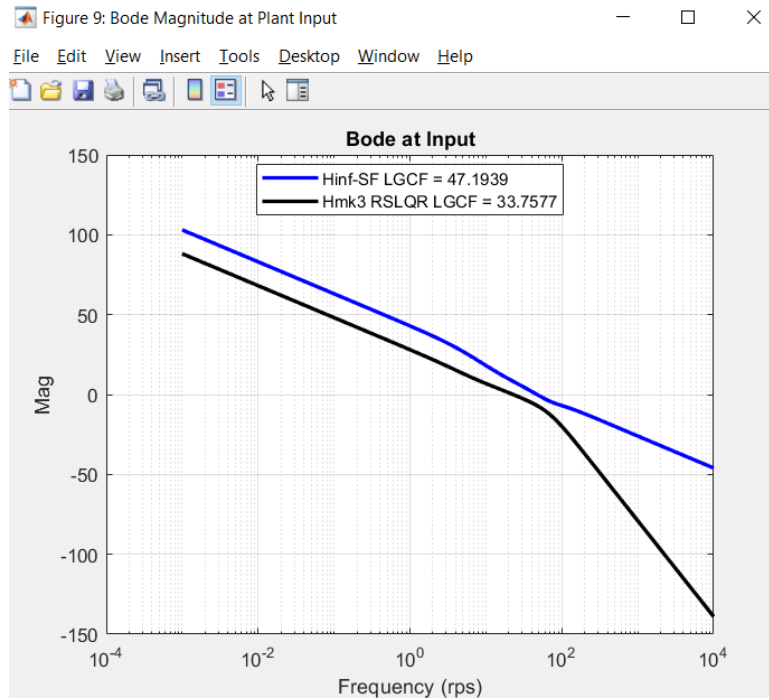


- b) Plot a Nyquist plot and identify on the plot the gain and phase margins, loop gain and phase crossover frequencies. Plot the RSLQR Nyquist with the Hinf Nyquist.

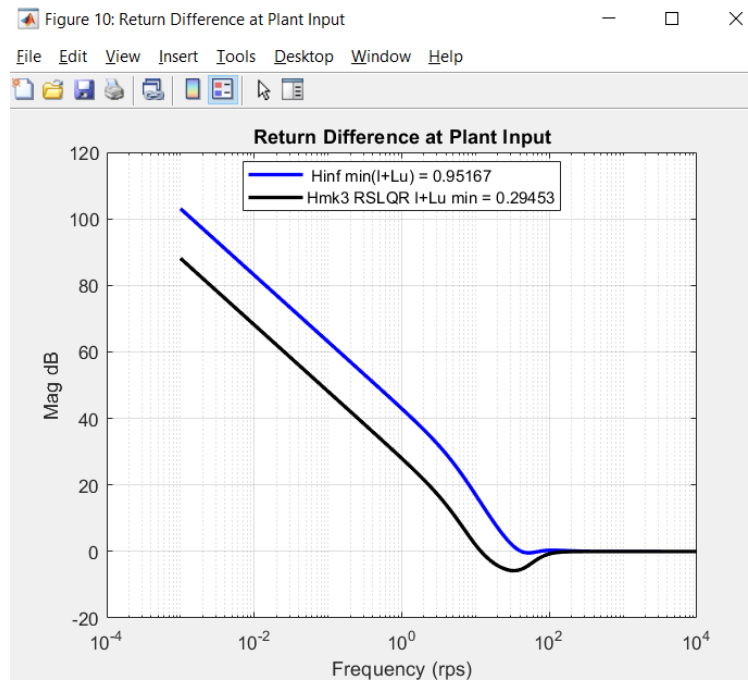




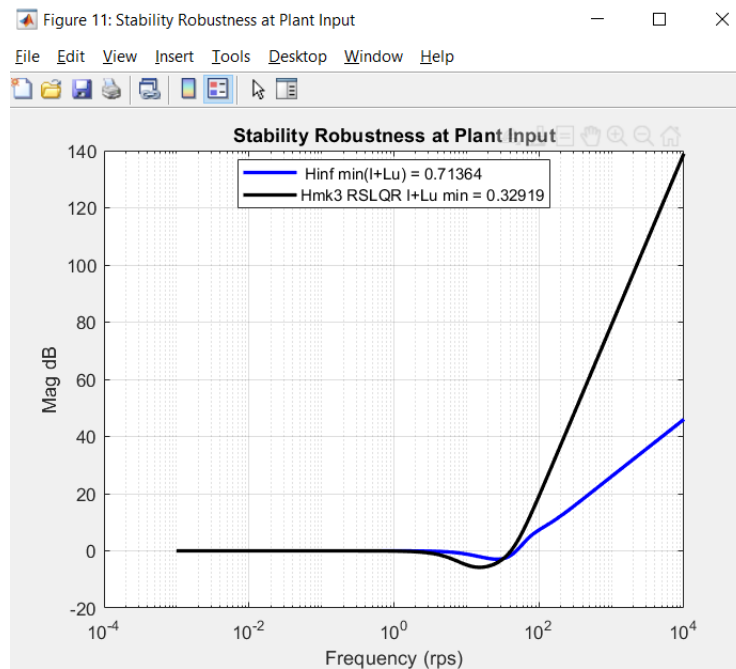
- c) Plot a Bode plot and identify on the plot the gain and phase margins, loop gain and phase crossover frequencies. Plot the RSLQR Bode with the Hinf Bode.



- d) Plot the minimum singular value of the return difference matrix in dB vs frequency. Identify on the plot the minimum value of the return difference matrix (not in dB). Plot the RSLQR  $\underline{\sigma}(I + L_u)$  including the actuator in the plant model



- e) Plot the minimum singular value of the stability robustness matrix in dB vs frequency. Identify on the plot the minimum value of the stability robustness matrix (not in dB). Plot the RSLQR  $\underline{\sigma}(I + L_u^{-1})$  including the actuator in the plant model with the Hinf  $\underline{\sigma}(I + L_u^{-1})$  (both plant models should have the actuator in them).



- f) Compute the singular value gain and phase margins for the system (at the plant input) and compare them with the RSLQR margins (both plant models should have the actuator in them).

Homework 4 Hinf SF

Singular value margins

Min Singular value I+Lu = 0.95167

Min Singular value I+invLu = 0.71364

Singular value gain margins = [-10.8619 dB, 26.3152 dB ]

Singular value phase margins = [ +/-56.8273 deg ]

Homework 3 RSLQR

Singular value margins

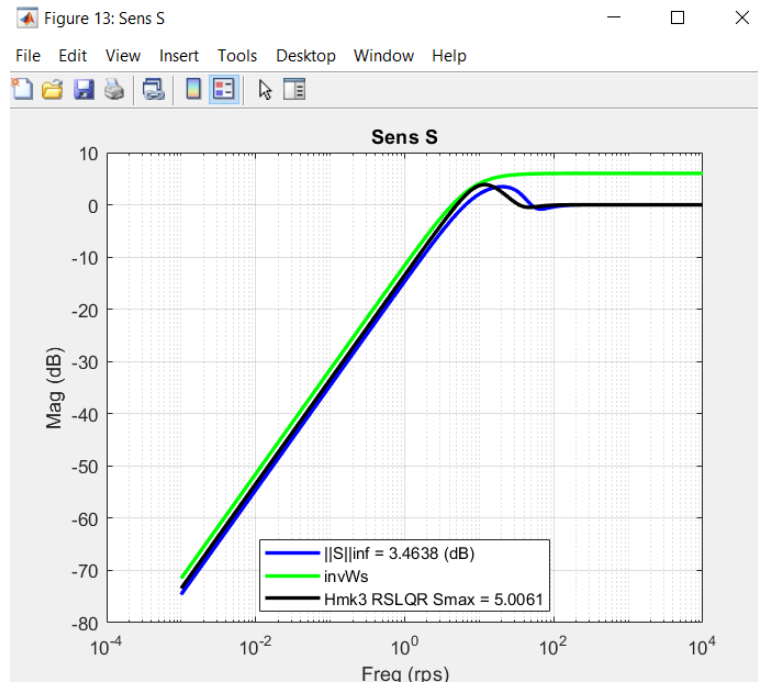
Min Singular value I+Lu = 0.29453

Min Singular value I+invLu = 0.32919

Singular value gain margins = [-3.468 dB, 3.0305 dB ]

Singular value phase margins = [ +/-18.9475 deg ]

- g) Compute the sensitivity function  $e/r = S$  (at the output). Plot the RSLQR  $e/r = S$  including the actuator in the plant model with the Hinf  $e/r = S$  (both plant models should have the actuator in them). Plot your Weighting filter  $W_S$  with these two frequency responses.



- h) Compute the complementary sensitivity  $y/r = T$  (at the output). Plot the RSLQR  $A_z / A_{zc} = T$  including the actuator in the plant model with the Hinf  $A_z / A_{zc} = T$  (both plant models should have the actuator in them). Plot your Weighting filter  $W_T$  with these two frequency responses.

