

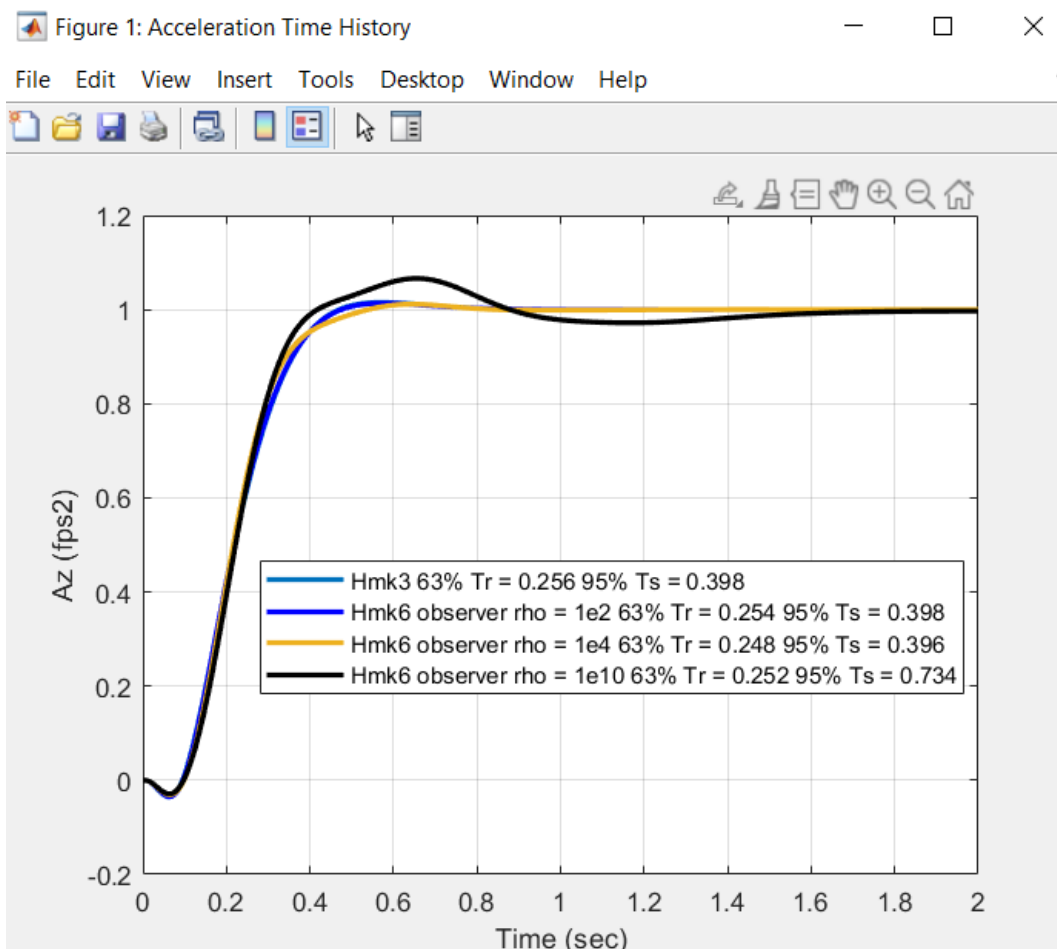
## HW6 | amithr3

The observer is:  $\dot{\hat{x}} = (\tilde{A} - \tilde{B}K_{lqr} - L_{\rho}C)\hat{x} + L_{\rho}y_{meas} + Fr$ , where  $r = A_{z_{cmd}}$  and  $y_{meas} = [e_I \quad q]^T$ .

This requires us to form the integral error  $e_I = \int (y_{reg} - r) = \int (A_z - A_{z_{cmd}})$  and make it available to the observer as a measurement. This method adds an additional integrator into the overall control architecture, and is shown in the following block diagram:

Simulate using a constant unit step command. Compare these LQG/LTR designs with the RSLQR state feedback controller. (Include the RSLQR and all three designs on each plot). Turn in plots of the accel command and response, pitch rate, and elevon deflection and rate. Analyze each controller in the frequency domain using a plant model that contains the actuator.

Plot Nyquist and Bode for  $L_u$ ,  $\sigma(I + L_u)$ ,  $\sigma(I + L_u^{-1})$ ,  $e_{A_z}/r = S$ ,  $A_z/r = T$ , and compute singular value margins at the plant input for each. Plot the noise-to-control and noise-to-control rate frequency responses.



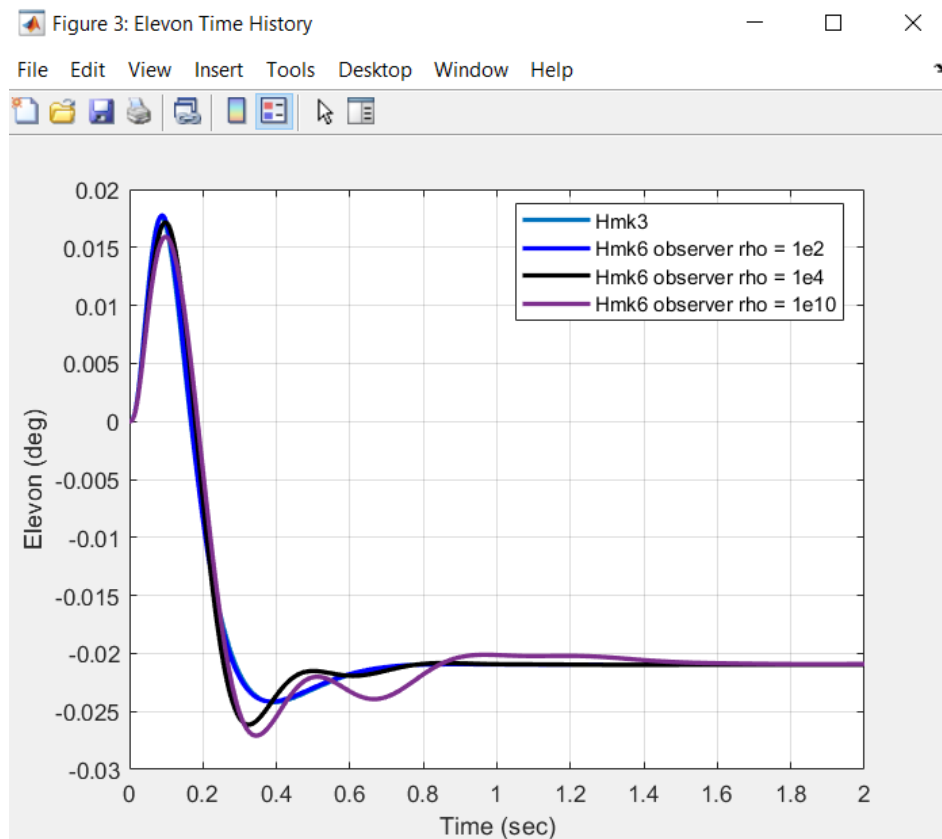
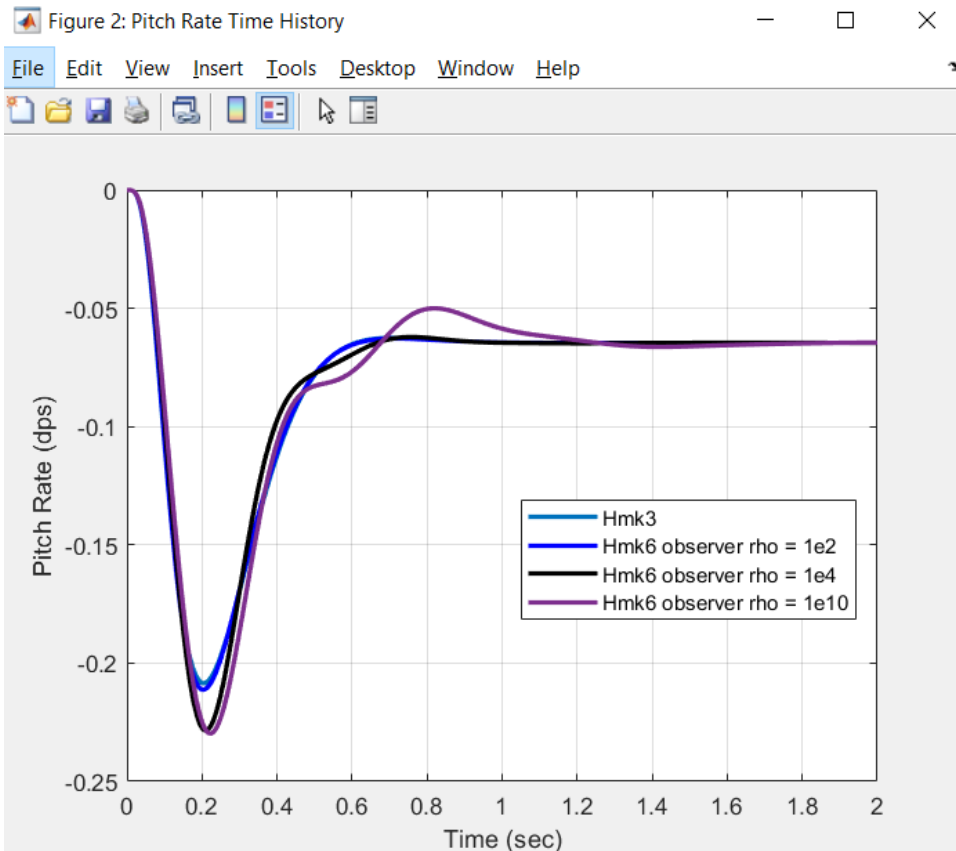


Figure 4: Elevon Rate Time History

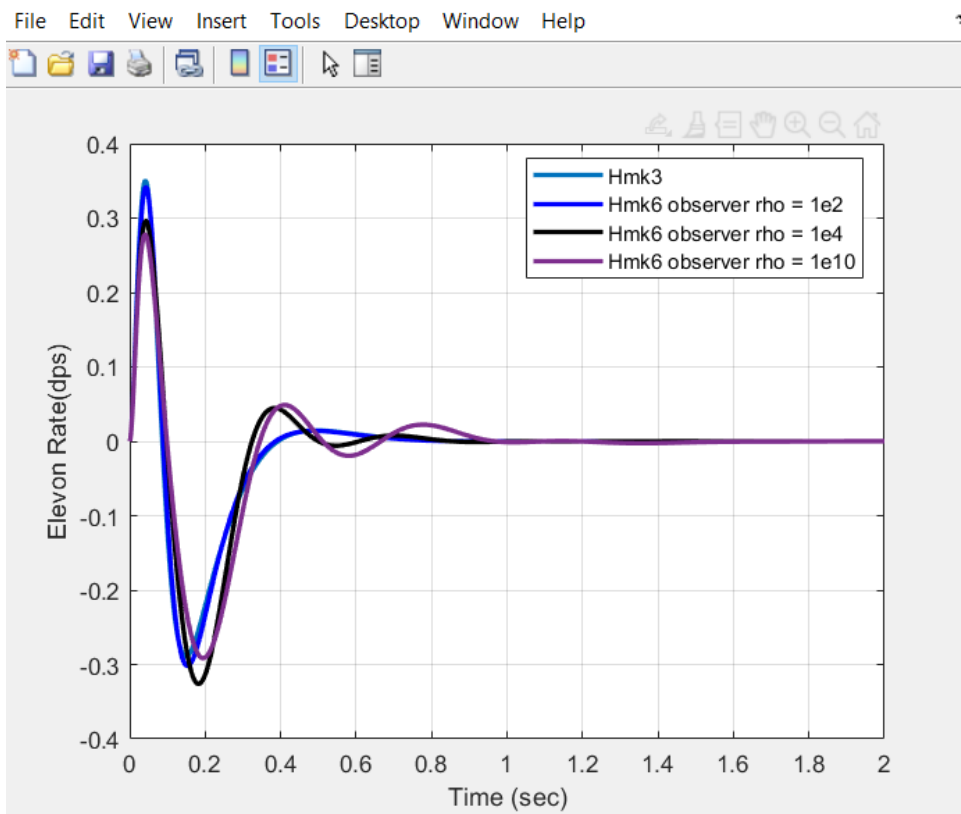
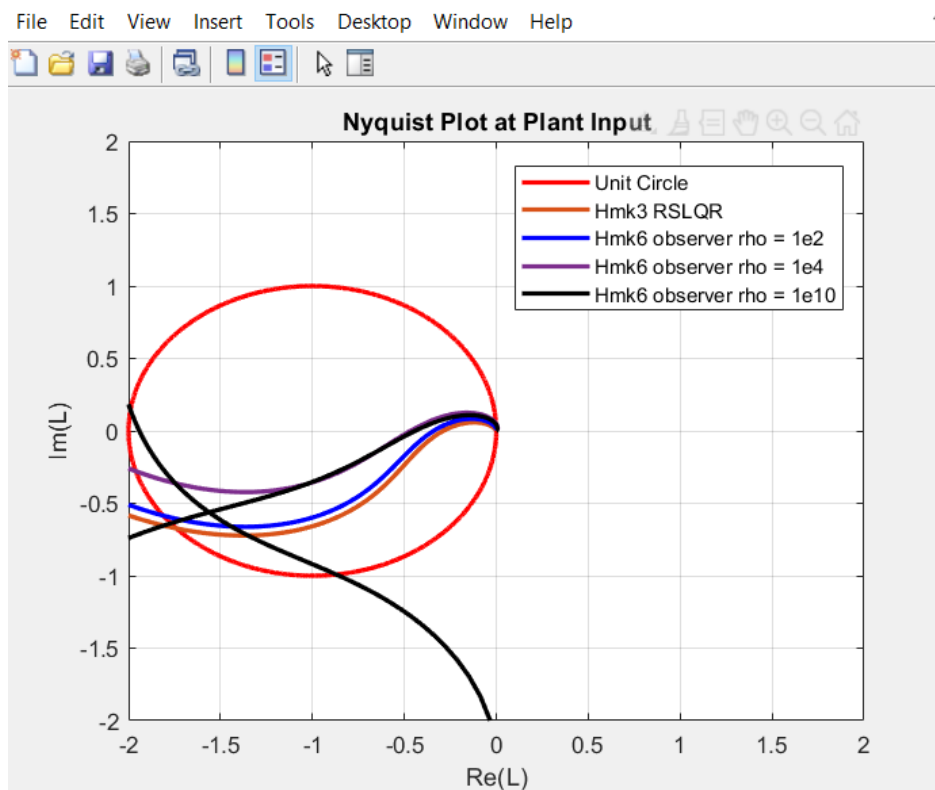
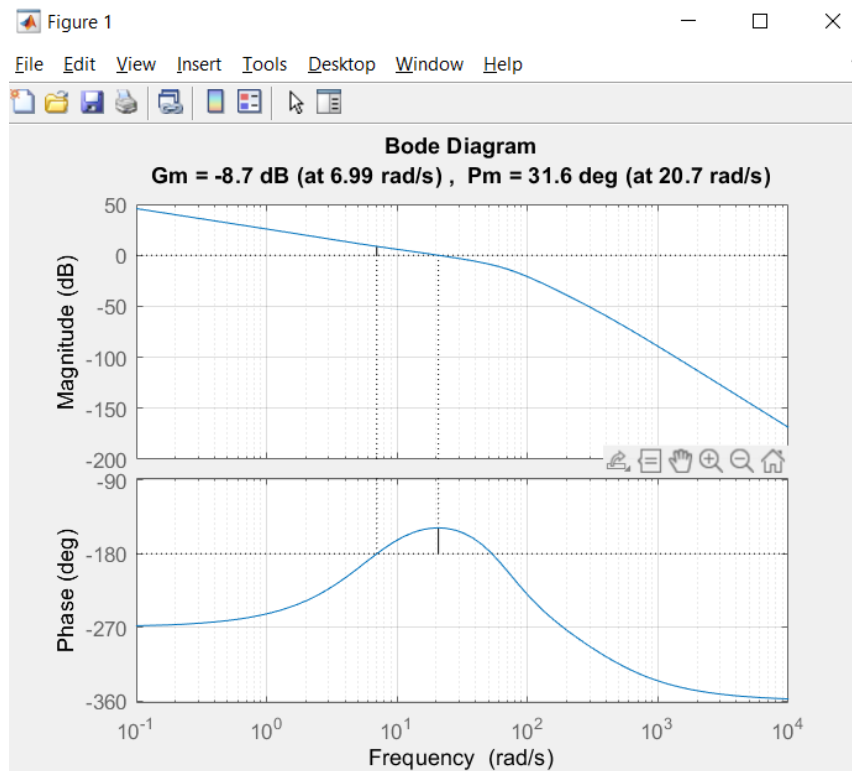
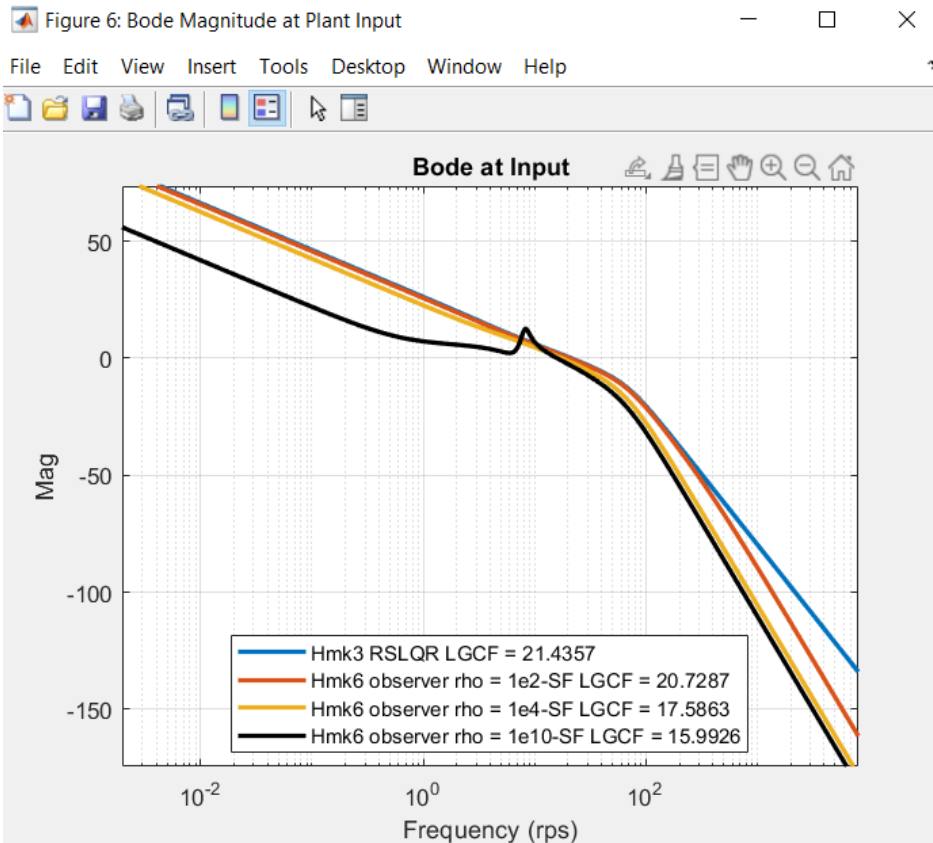
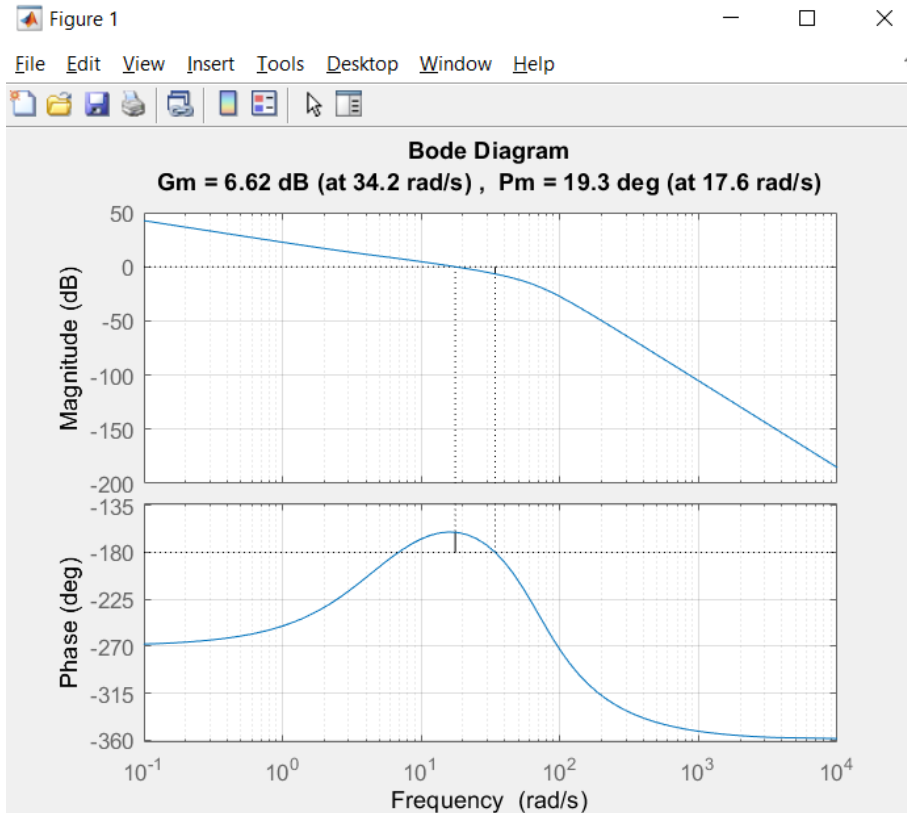


Figure 5: Nyquist Plot at Plant Input

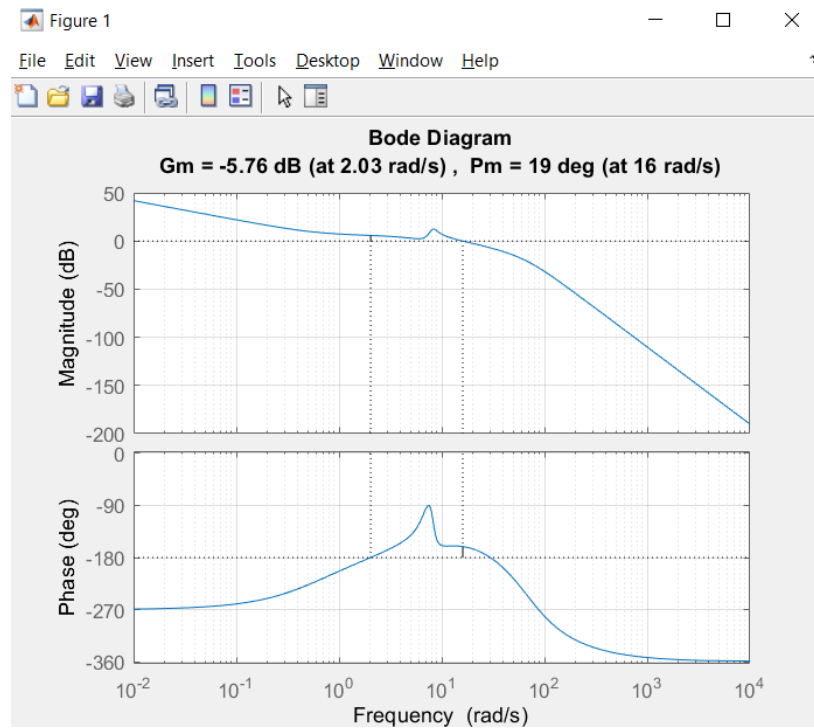




Rho =  $10^2$



$\text{Rho} = 10^4$



$\text{Rho} = 10^{10}$

Figure 7: Return Difference at Plant Input

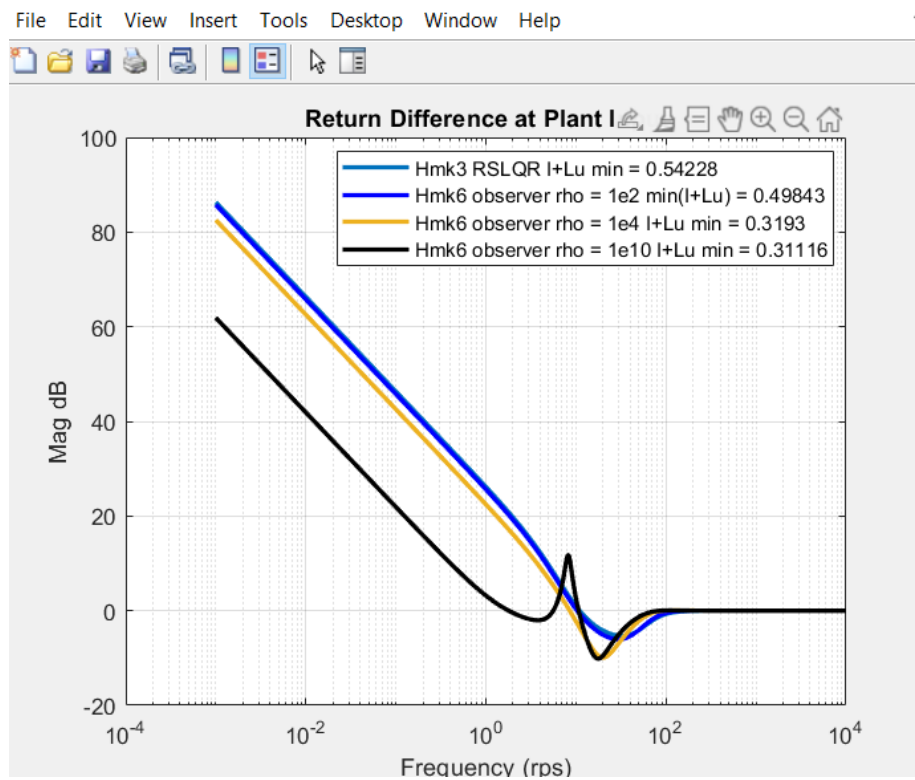
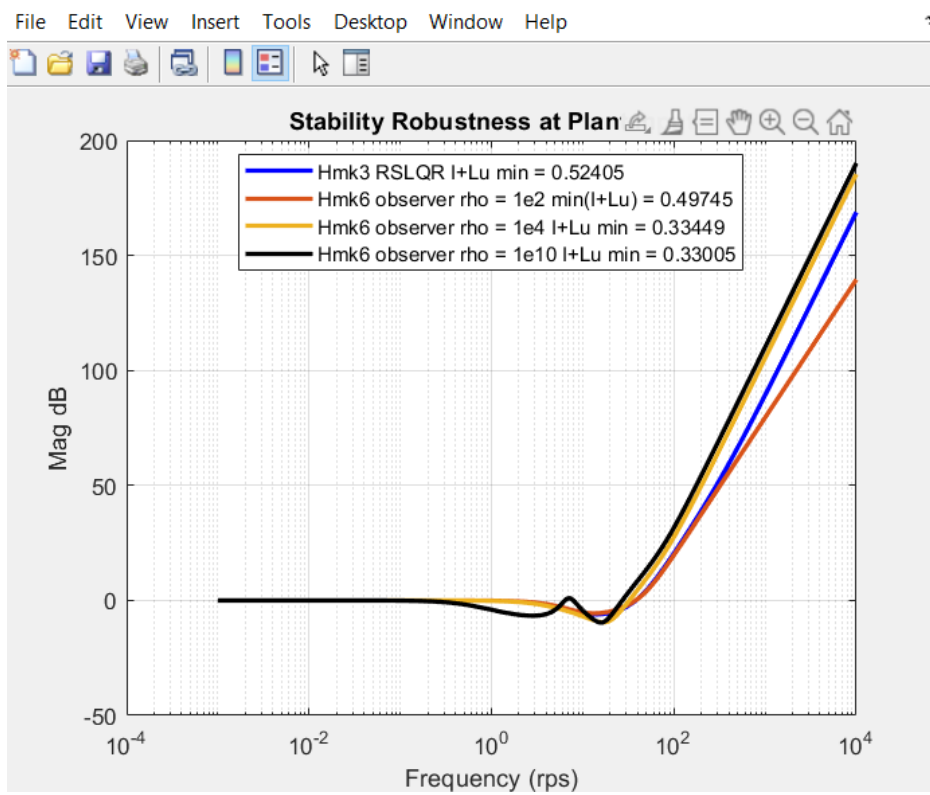
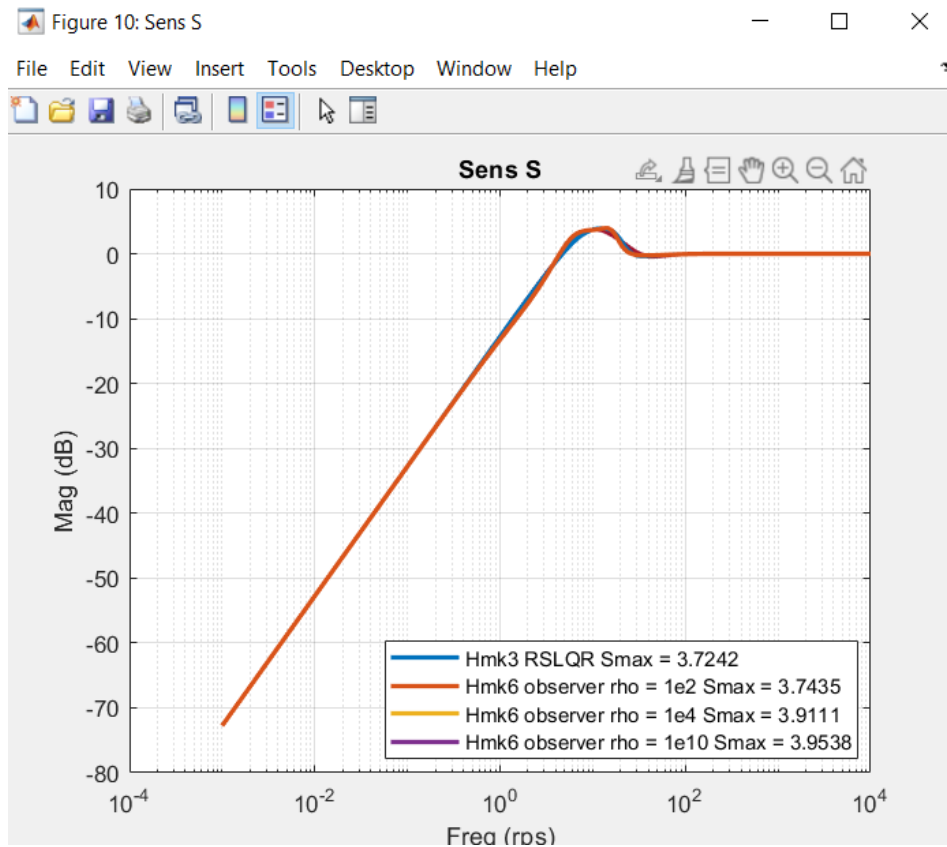
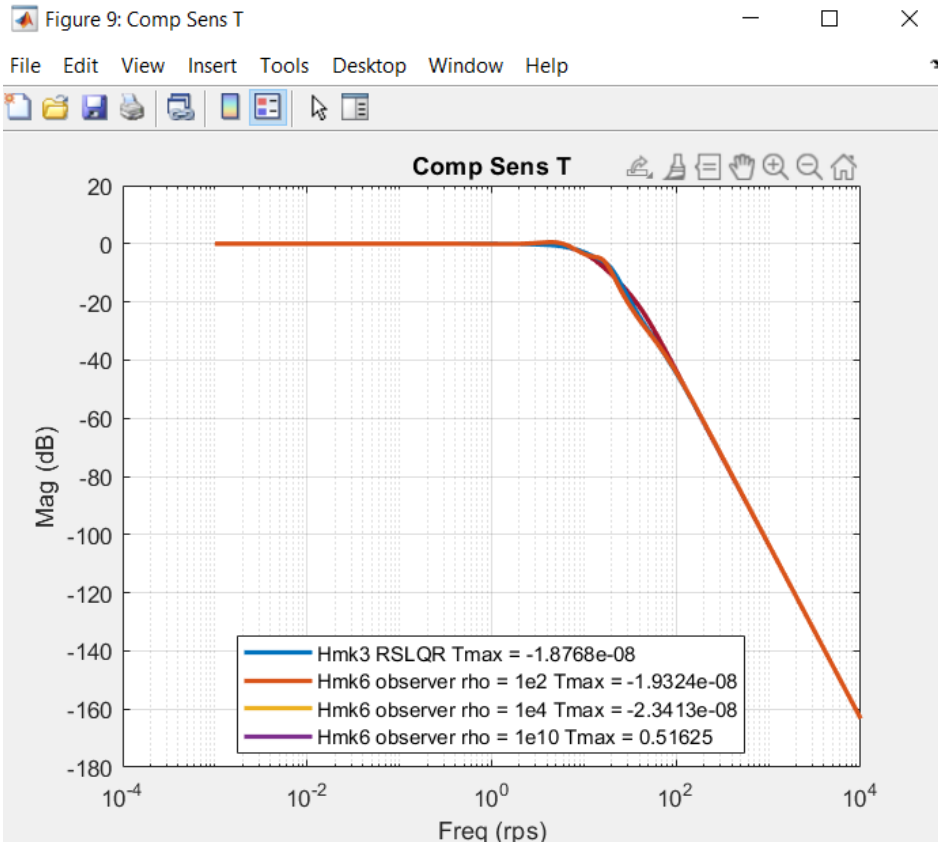
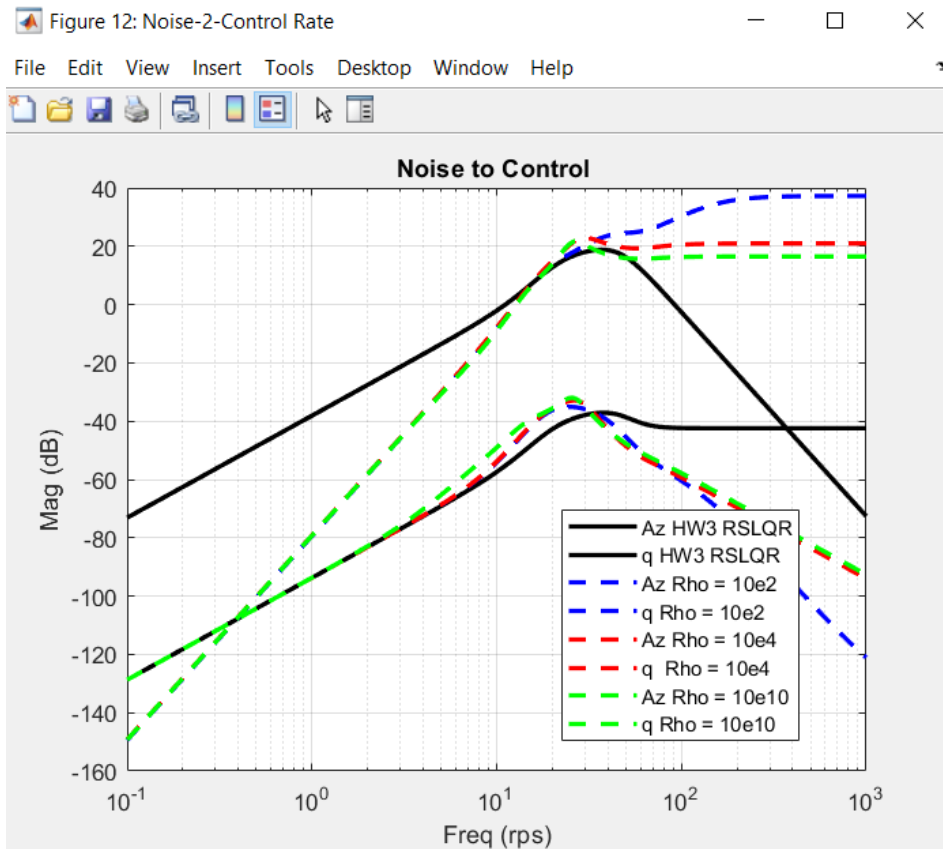
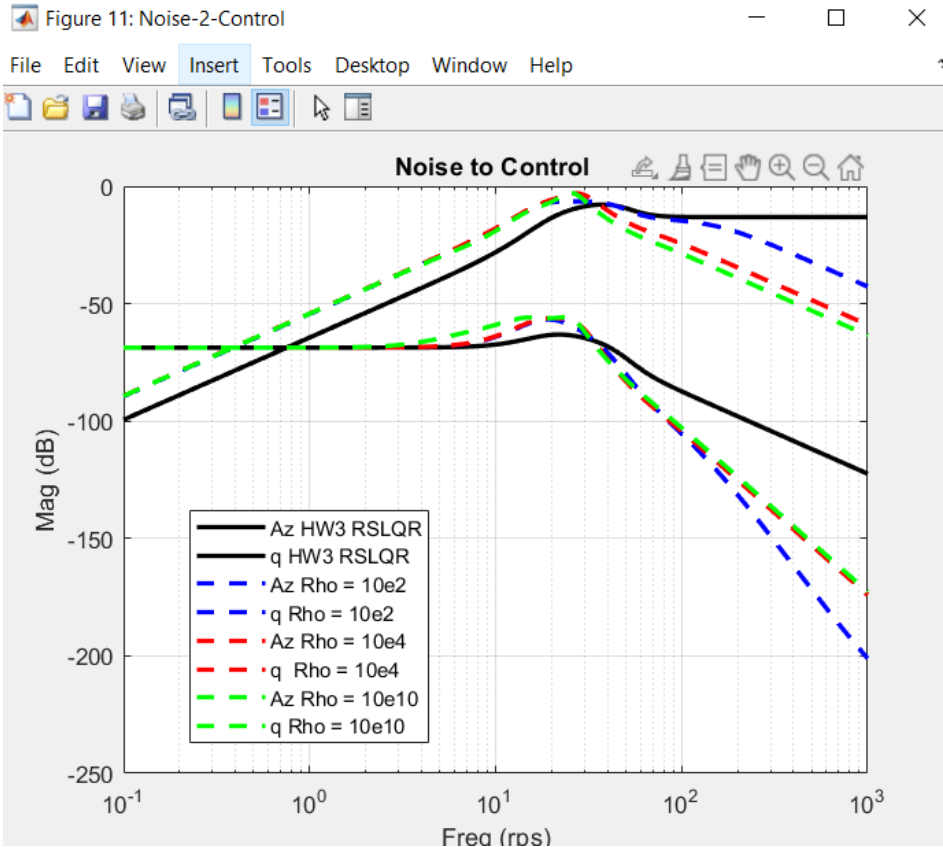


Figure 8: Stability Robustness at Plant Input









## Singular Value Margins

Homework 3 RSLQR

Singular value margins

Min Singular value I+Lu = 0.54228

Min Singular value I+invLu = 0.52405

Singular value gain margins = [-6.4488 dB, 6.7879 dB ]

Singular value phase margins = [ +/-31.4639 deg ]

Hmk6\_observer\_rho1 = e2

Singular value margins

Min Singular value I+Lu = 0.49843

Min Singular value I+invLu = 0.49745

Singular value gain margins = [-5.9765 dB, 5.9935 dB ]

Singular value phase margins = [ +/-28.8624 deg ]

Hmk6\_observer\_rho1 = e4

Singular value margins

Min Singular value I+Lu = 0.3193

Min Singular value I+invLu = 0.33449

Singular value gain margins = [-3.5369 dB, 3.3409 dB ]

Singular value phase margins = [ +/-19.2552 deg ]

Hmk6\_observer\_rho1 = e10

Singular value margins

Min Singular value I+Lu = 0.31116

Min Singular value I+invLu = 0.33005

Singular value gain margins = [-3.4791 dB, 3.2376 dB ]

Singular value phase margins = [ +/-18.9973 deg ]

For  $\rho = 10^2$ , List out your observer design matrices  $(\tilde{A}, C, Q, R, L_\rho)$ . List the controller matrices  $(A_c, B_{c_1}, B_{c_2}, C_c, D_{c_1}, D_{c_2})$  implementing the controller.

$$\tilde{A} =$$

$$\begin{bmatrix} 0 & -1.1569\text{e}+03 & 0 \\ 0 & -1.3046\text{e}+00 & 1.0000\text{e}+00 \\ 0 & 4.7711\text{e}+01 & 0 \end{bmatrix}$$

$$C =$$

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$Q =$$

$$\begin{bmatrix} 3.6080\text{e}+02 & 4.0687\text{e}-01 & 1.9912\text{e}+02 \\ 4.0687\text{e}-01 & 1.8588\text{e}-03 & 2.2455\text{e}-01 \\ 1.9912\text{e}+02 & 2.2455\text{e}-01 & 1.0990\text{e}+02 \end{bmatrix}$$

$$R =$$

$$\begin{bmatrix} 6.2500\text{e}-01 & 0 \\ 0 & 1.0000\text{e}-03 \end{bmatrix}$$

$$L =$$

$$\begin{bmatrix} 1.2979\text{e}+01 & 5.6878\text{e}+02 \\ -4.7012\text{e}-02 & 1.7985\text{e}+00 \\ 9.1005\text{e}-01 & 3.3099\text{e}+02 \end{bmatrix}$$

## Common Controller

Ac =

0	0	0	0
1.2979e+01	-1.1542e+01	-1.5956e+03	-6.1073e+02
-4.7012e-02	4.8633e-02	-1.7994e+00	-8.4582e-01
9.1005e-01	-1.1704e-01	-1.9443e+02	-3.5414e+02

Bc1 =

1.0000e+00	0	0	0	0
0	0	5.6878e+02	0	0
0	0	1.7985e+00	0	0
0	0	3.3099e+02	0	0

Bc2 =

-1
-1
0
0

Cc =

0	-7.5646e-03	2.3099e+00	2.2086e-01
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Dc1 =

0	0	0	0	0
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Dc2 =

0
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