

Mujiburrehman
Gouri



Dynamic Load Carrying Capacity of a Robot Manipulator

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Prof. Dr.-Ing. Lothar Berger

Prof. Dr.-Ing. Raphael Ruf

Hochschule Ravensburg-Weingarten

Dipl.-Ing. Mavarick Ho
Neura Robotics GmbH

Overview

① Introduction

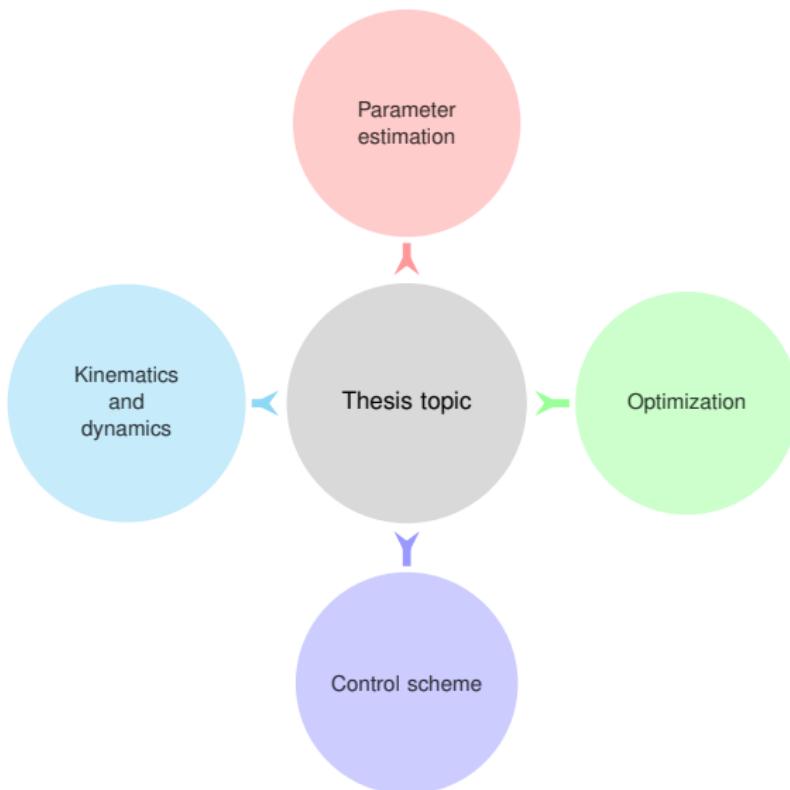
② Methodology

③ Results

④ Conclusion

Introduction

Topic of investigation



What is DLCC



- Maximum load robot can carry
- Joint torque decides the load carrying capacity of the robot
- Dynamic load depends upon the end-effector motion
- Payload capacity of LARA
- Payload capacity changes for configuration close or away from robot

Figure: LARA robot

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What is the Goal

- Incorporate robot dynamics in trajectory planning
- $\tau = H(q)\ddot{q} + c(q, \dot{q}) + \tau_g(q)$
- Robot motion can have joint jerks for payload exceeding limits
- Minimizing the joint jerks reduces the wear and tear
- Optimization problem is formulated

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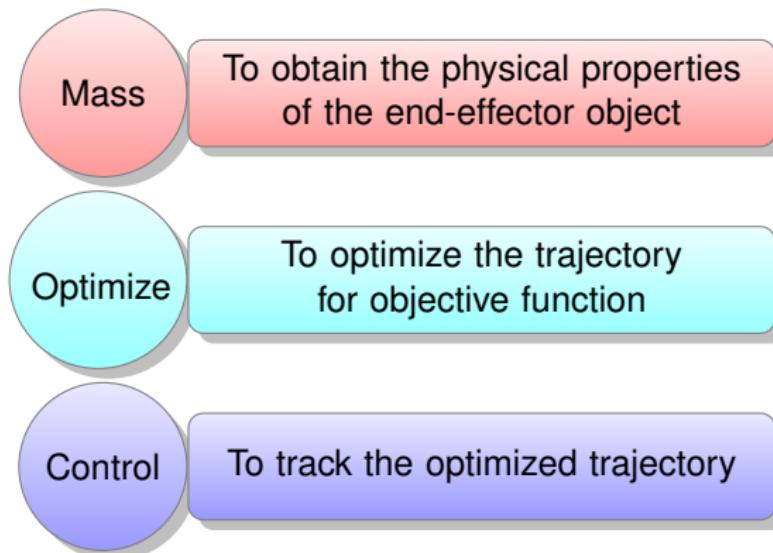
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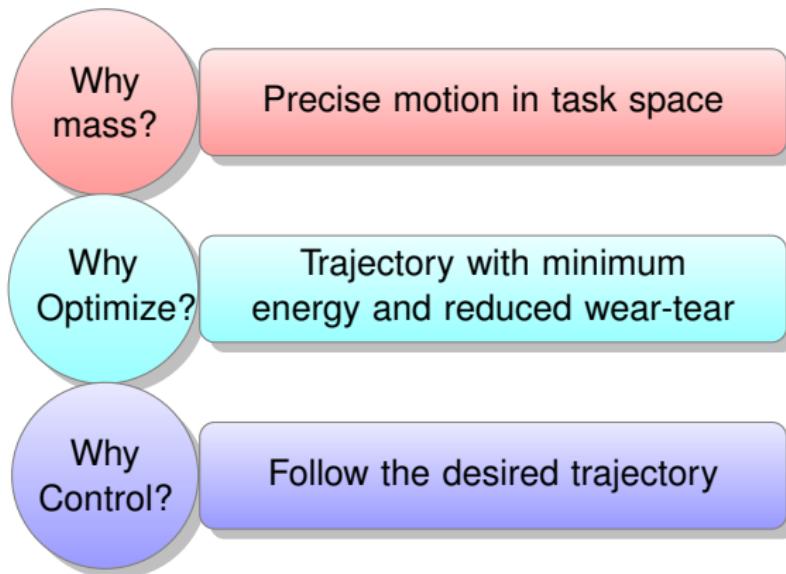
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Problem statement



Topic importance



Methodology

Inertial parameter estimation

A rigid body in space has following physical parameters,

- ① Mass
- ② Centre of mass
- ③ Moment of inertia

Inertial parameter estimation

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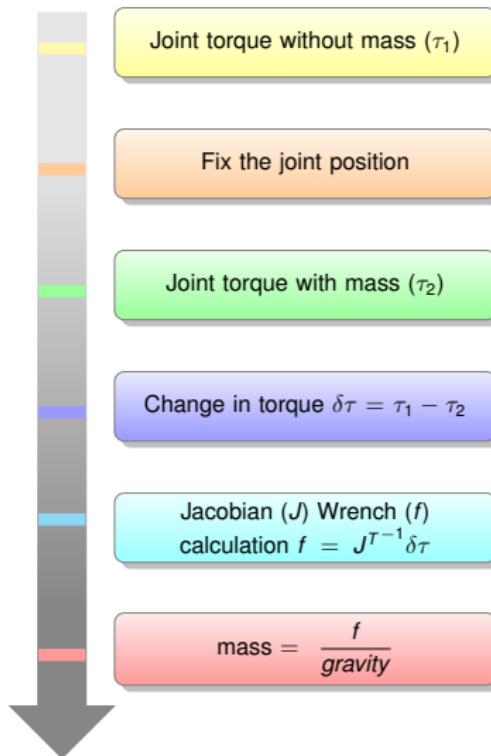
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Inertial parameter estimation

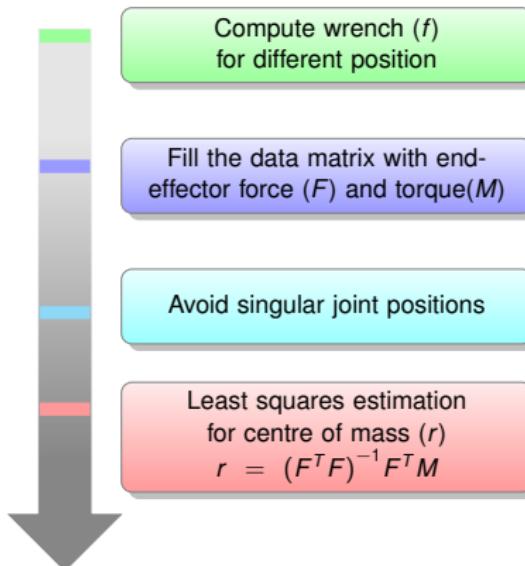
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Mass estimation



Centre of mass

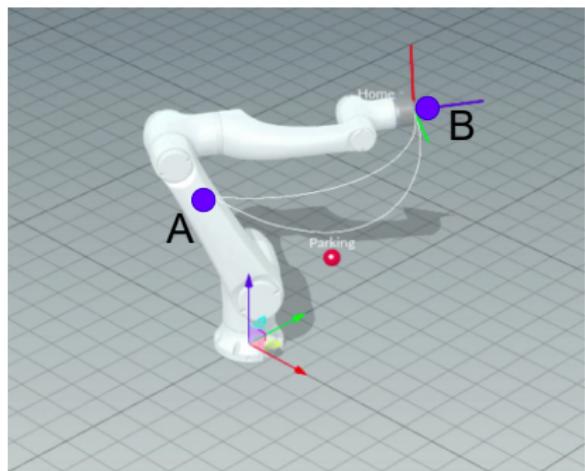


Optimization

Optimization problem is formulated for trajectory planning

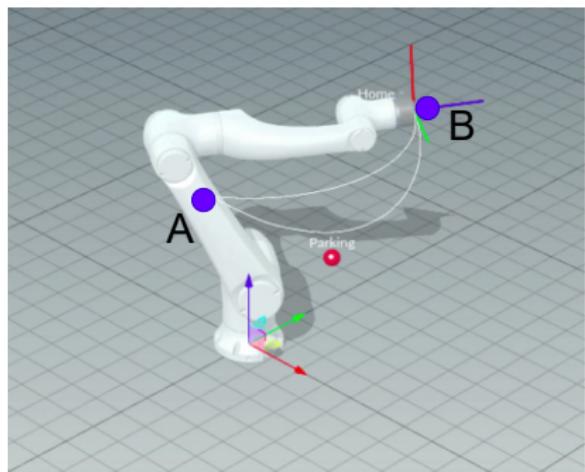
- ① Cost functional formulation

Cost functional



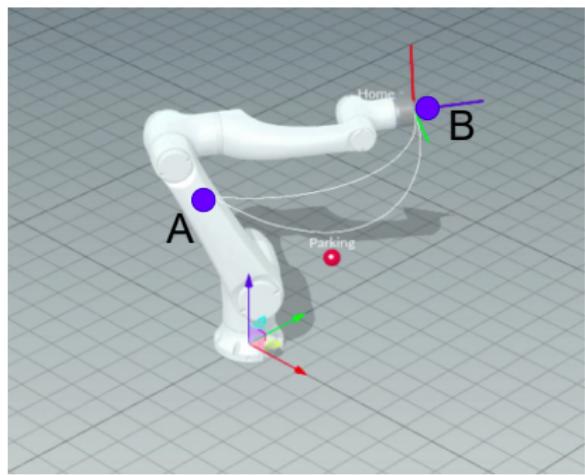
- Robot motion from initial to goal position
- First objective is to track the desired trajectory
- Secondary objective is to minimize the energy

Cost functional



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First objective

- Tracking of desired (x_d) and current position (x_c) as $x_d - x_c$
- Nonlinear functions and inverse kinematics
- Tracking of velocity profile $\dot{x}_d - \dot{x}_c$
- Using jacobian(J), $\dot{x} = J_{(q)}\dot{q}$

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Second objective

- Kinetic energy of the robot, $K.E = \frac{1}{2} \dot{q}^T H \dot{q}$
- Complex nonlinear terms and computation effort
- Joint acceleration for minimum energy, $K.E \approx \sum_{n=1}^N (\ddot{q}^T \ddot{q})$

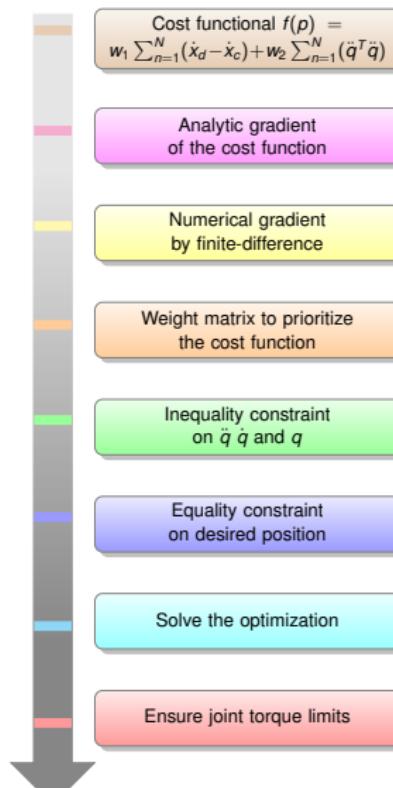
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Problem formulation



Results

Inertial parameter estimation

- Friction is absent in robot simulation, $I_F = 0$
- Friction is present in robot hardware, $I_F \neq 0$
- $\tau = H(q)\ddot{q} + c(q, \dot{q}) + \tau_g(q) + I_F$

Parameter (unit)	Actual value	Estimated value
mass (kg)	5	5.15
center of mass (m)	x	0.04
	y	0.04
	z	0.0
		-0.0004

Table: Robot simulation

Parameter (unit)	Actual value	Estimated value
mass (kg)	4	23.7
center of mass (m)	x	0.15
	y	0.0
	z	0.075
		0.1698
		0.3842
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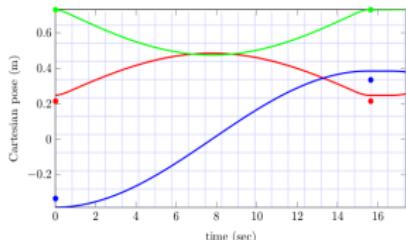
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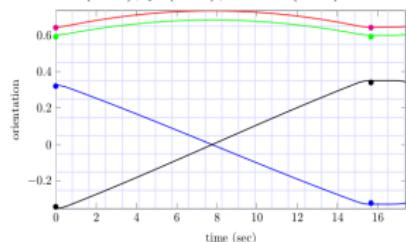
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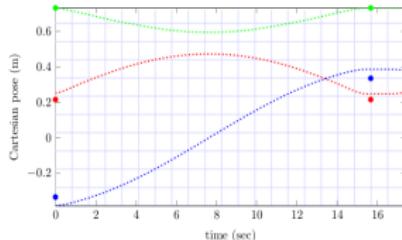
Optimization



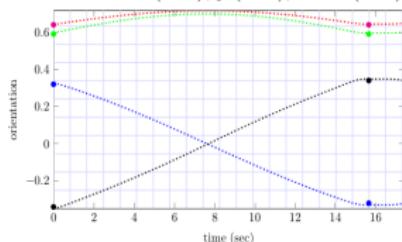
(a) input cartesian pose of the end-effector in x (—), y (—), and z (—).



(c) input end-effector orientation q_x (—), q_y (—), q_z (—), and w (—).

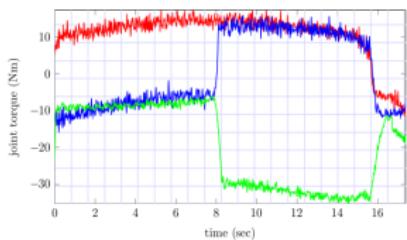


(b) optimized cartesian pose of the end-effector in x (—), y (—), and z (—).

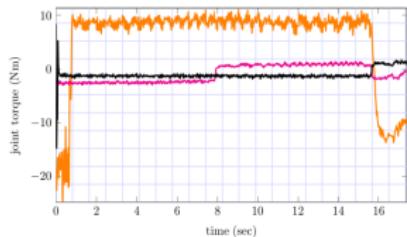


(d) optimized end-effector orientation q_x (—), q_y (—), q_z (—), and w (—).

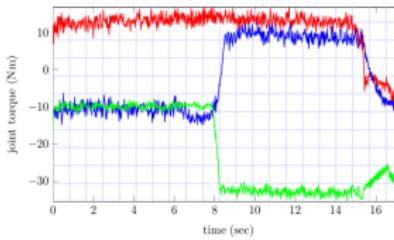
Figure: cartesian pose



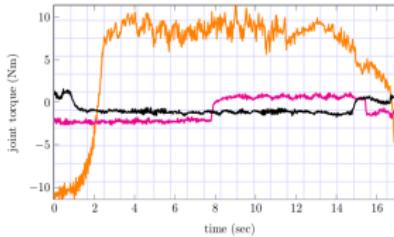
(a) input joint torque for joint 1 (—), joint 2 (—), and joint 3 (—).



(c) input joint torque for joint 4 (—), joint 5 (—), and joint 6 (—).



(b) optimized joint torque for joint 1 (—), joint 2 (—), and joint 3 (—).



(d) optimized joint torque for joint 4 (—), joint 5 (—), and joint 6 (—).

Figure: joint torque

Trajectory before optimization

Trajectory after optimization

Conclusion

Key findings

- Mass of the object is estimated using wrench analysis
- Torque due to friction (I_F) in robot joints affects the estimation
- Desired trajectory is followed with minimum acceleration
- Proposed formulation is faster to converge $\sim 300 - 600$ ms

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limitations

- Does not directly follow the cartesian position, $x_d - x_c$
- The proposed approach only consider the joint acceleration
- Approximate solution to the given optimization problem
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Thank you for your attention!

