Extended Kalman Filter for Fixed-Wing Aircraft Dynamics

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1 Introduction

The goal of this project is to implement an extended Kalman filter (EKF) to estimate a fixed-wing airraft state vector from noisy sensor measurements. The first iteration of this project will be focused only on the longitudinal dynamics.

2 Aircraft Model

The nonlinear longitudinal dynamics for conventional fixed-wing aircraft can be written as follows [1, 2]

$$\dot{U} = -QW - g\sin\theta + \frac{X}{m}$$

$$\dot{W} = QU + g\cos\theta + \frac{Z}{m}$$

$$\dot{Q} = \frac{M}{I_{yy}}$$

$$\dot{\theta} = Q$$
(1)

The forces and moments can be broken down as follows

$$X = qS\left(C_X(\alpha) + \frac{\bar{c}}{2V_T}C_{X_Q}Q + C_{X_{\delta_e}}\delta_e\right) + X_{t_0} + X_{\delta_t}\delta_t$$

$$Z = qS\left(C_Z(\alpha) + \frac{\bar{c}}{2V_T}C_{Z_Q}Q + C_{Z_{\delta_e}}\delta_e\right)$$

$$M = qS\bar{c}\left(C_M(\alpha) + \frac{\bar{c}}{2V_T}C_{M_Q}Q + C_{M_{\delta_e}}\delta_e\right)$$
(2)

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Considering a trim condition in a cruise level flight, the nonlinear system 1 can be further simplified to be on the following from

$$\dot{U} = -QW - g\cos\theta_0\Delta\theta + X_U\Delta U + X_W\Delta W + X_{\delta_e}\delta_e + X_{\delta_t}\delta_t
\dot{W} = QU - g\sin\theta_0\Delta\theta + Z_U\Delta U + Z_W\Delta W + Z_{\delta_e}\delta_e
\dot{Q} = M_U\Delta U + M_W\Delta W + M_QQ + M_{\delta_e}\delta_e + M_{\delta_t}\delta_t
\dot{\theta} = Q$$
(3)

The nonlinear system 1 can be linearized and written in a standard linear system form as follows [1, 2]

$$\begin{bmatrix} \dot{U} \\ \dot{W} \\ \dot{Q} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} X_u & X_w & 0 & -g\cos\theta_0 \\ Z_u & Z_w & U_0 & -g\sin\theta_0 \\ M_u & M_w & M_q & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} U \\ W \\ Q \\ \theta \end{bmatrix} + \begin{bmatrix} X_{\delta_e} & X_{\delta_t} \\ Z_{\delta_e} & 0 \\ M_{\delta_e} & M_{\delta_t} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} \delta_e \\ \delta_t \end{bmatrix}$$
(4)

In this project we will consider the longitudinal model of the aircraft "DELTA" given in [3, PP. 561–563] whose parameters are given as follows (at $U_0 = 75 \ m/s$ and $\theta_0 = 2.7^{\circ}$)

$$m = 300000kg$$

$$X_U = -0.02$$

$$X_W = 0.1$$

$$Z_U = -0.23$$

$$Z_W = -0.634$$

$$M_U = -2.55 * 10^{-5}$$

$$M_W = -0.005$$

$$M_Q = -0.61$$

$$X_{\delta_e} = 0.14$$

$$Z_{\delta_e} = -2.9$$

$$M_{\delta_e} = -0.64$$

$$X_{\delta_t} = 1.56$$

$$M_{\delta_t} = 0.0054$$
(5)

where δ_t is considered to be from the trim thrust. As such, δ_t is allowed the between 1 and -0.56 [4].

3 Extended Kalman Filter Equations

In this section, we will summarize the continuous-discrete EKF equations as presented by Crassidis and Junkins [5]. The EKF considers a nonlinear system

with process and measurment noise as follows

$$\dot{\boldsymbol{x}}(t) = \boldsymbol{f}(\boldsymbol{x}(t), \boldsymbol{u}(t), t) + G(t)\boldsymbol{w}(t), \ \boldsymbol{w}(t) \sim N(0, Q(t))$$

$$\tilde{\boldsymbol{y}}_k = \boldsymbol{h}(\boldsymbol{x}_k) + \boldsymbol{v}_k, \ \boldsymbol{v}_k \sim N(0, R_k)$$
(6)

where the overscript symbol $\tilde{}$ denotes a measured quantity and the subscript symbol k denotes the value at time step k. Also, x is the state vector, u is the control input vector, u is the process noise vector, and v is the measurment noise vector.

The EKF can be initialized as follows

$$\hat{\boldsymbol{x}}(t_0) = \hat{\boldsymbol{x}}_0$$

$$P_0 = E\{\widetilde{\boldsymbol{x}}(t_0)\widetilde{\boldsymbol{x}}^T(t_0)\}$$
(7)

where the overscript symbol $\hat{}$ denotes an estimated quantity and P is the state estimate error covariance matrix.

The Kalman gain, updated state, and updated state estimate error covariance can be obtained as follows

$$K_{k} = P_{k}^{-} C_{k}^{T} \left(C_{k} P_{k}^{-} C_{k}^{T} + R_{k} \right)^{-1}$$

$$C_{k} \equiv \frac{\partial \mathbf{h}}{\partial \mathbf{x}} \Big|_{\hat{\mathbf{x}}_{k}^{-}}$$

$$\hat{\mathbf{x}}_{k}^{+} = \hat{\mathbf{x}}_{k}^{-} + K_{k} \left(\tilde{\mathbf{y}}_{k} - \mathbf{h}(\hat{\mathbf{x}}_{k}^{-}) \right)$$

$$P_{k}^{+} = \left(I - K_{k} C_{k} \right) P_{k}^{-}$$
(8)

where the superscript symbol ⁻ denotes the state/covariance after the propagation step but before the update step. On the other hand, the superscript symbol ⁺ denotes the state/covariance after the update step.

Finally, the state and state estimate error covariance can be propagated as follows

$$\dot{\boldsymbol{x}}(t) = \boldsymbol{f}(\boldsymbol{x}(t), \boldsymbol{u}(t), t)
\dot{P}(t) = A(t)P(t) + P(t)A^{T}(t) + G(t)Q(t)G^{T}(t)
A(t) \equiv \frac{\partial \boldsymbol{f}}{\partial \boldsymbol{x}}\Big|_{\hat{\boldsymbol{x}}(t), \boldsymbol{u}(t)}$$
(9)

4 Algorithm Structure

Figure 1 shows a simple sketch of the algorithm structure. There are two classes implemented in this project: LongDynamics and EKF. The first one encapsulates the nonlinear dynamic system equations for the fixed-wing aircraft longitudinal dynamics, whereas the second one encapsulates the EKF algorithm

implementation. The *LongDynamics* class relies on an external package (odeint [6]) for time propagation (numerical integration). In addition, there are some helper functions to load the dataset and compute the root mean square error.

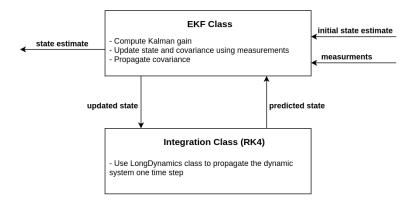


Figure 1: EKF algorithm structure.

5 Results

Figures 2 and 3 show the estimated angle of attack and pitch rate versus the measured and true ones.

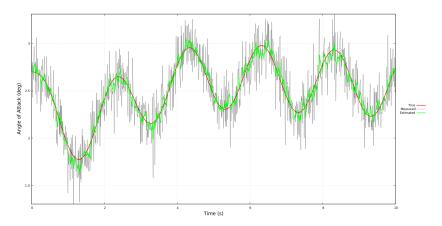


Figure 2: A comparison between the estiamted, measured and true angle of attack.

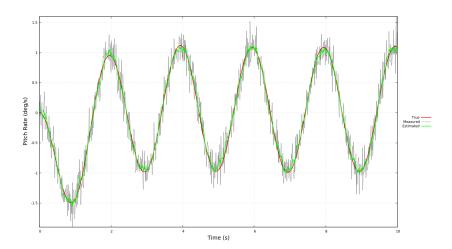


Figure 3: A comparison between the estiamted, measured and true ptich rate.

References

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- [6] odeint http://headmyshoulder.github.io/odeint-v2/.