

Verification of the improved chemistry solver

This material provides comparisons between standard solvers and improved solvers to verify the numerical consistency of the improved solvers with OpenFOAM-10. The comparisons include zero-dimensional constant pressure auto ignition and two-dimensional counter flow flame.

1. Zero-dimensional constant pressure auto ignition

Three ODE solvers, including Rodas34 algorithm, Rosenbrock34 algorithm and Seulex algorithm are selected for numerical verification. The ignition is solved using application chemFoam in foundation version OpenFOAM-10. The absolute tolerance and relative tolerance are 10^{-12} and 10^{-6} , respectively. The result using OpenFOAM standard chemistry solver and the improved chemistry solver is compared.

1.1 Hydrogen

Table S1. Operating condition of hydrogen/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|--------|-----------|------------|------|
| 10s21r | 1200 | 101325 | [1] |
| 15s75r | 1200 | 101325 | [2] |

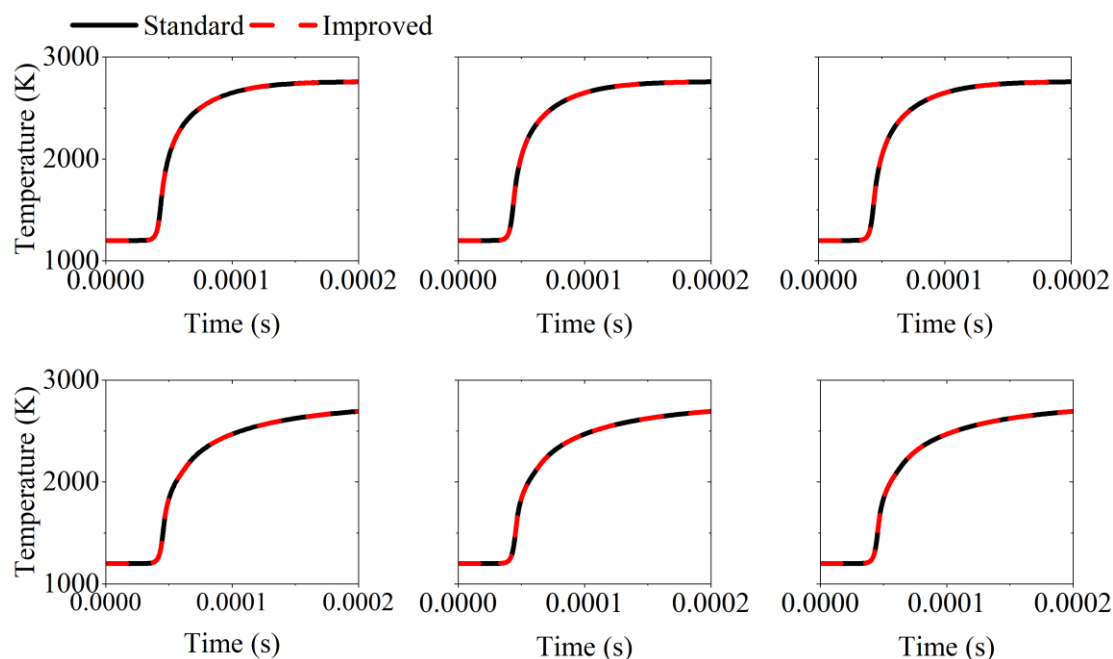


Fig. S1. Temperature profiles for hydrogen/air under constant-pressure autoignition conditions. The first row: 10s21r, the second row: 15s75r. Left: Rodas34 algorithm, middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.2 Methane

Table S2. Operating condition of methane/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|---------|-----------|------------|------|
| 22s104r | 1000 | 136789 | [3] |
| 53s325r | 1000 | 136789 | [4] |

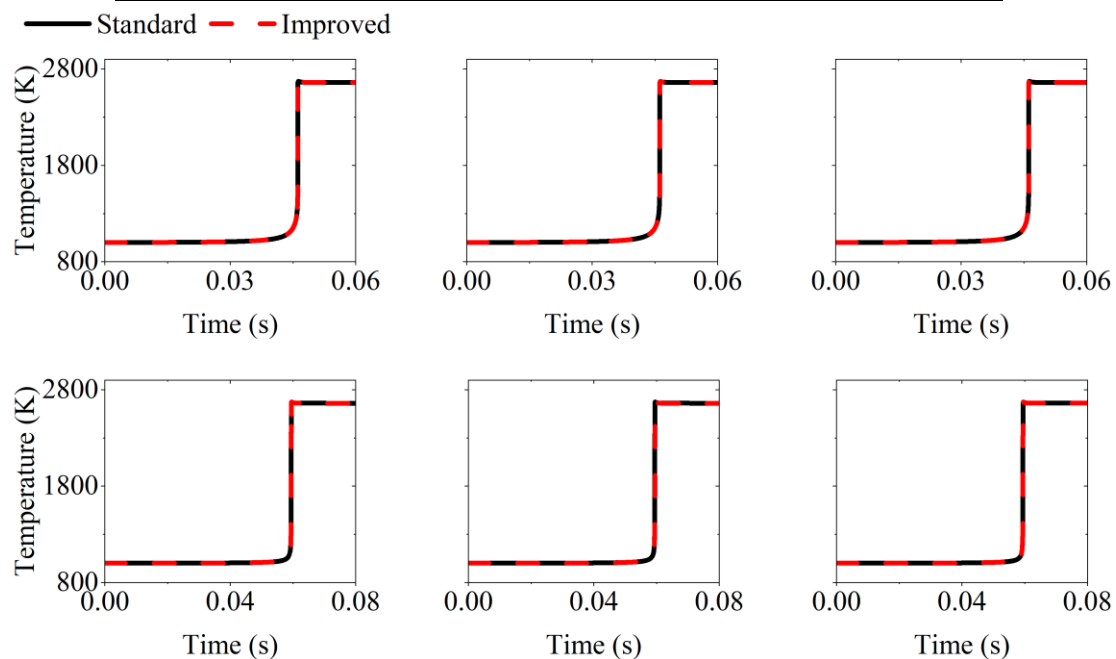


Fig. S2. Temperature profiles for methane/air under constant-pressure autoignition conditions. The first row: 10s21r, the second row: 15s75r. Left: Rodas34 algorithm, Middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.3 Ethylene

Table S3. Operating condition of ethylene /air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|---------|-----------|------------|------|
| 24s70r | 1000 | 202650 | [5] |
| 59s268r | 1000 | 202650 | [6] |

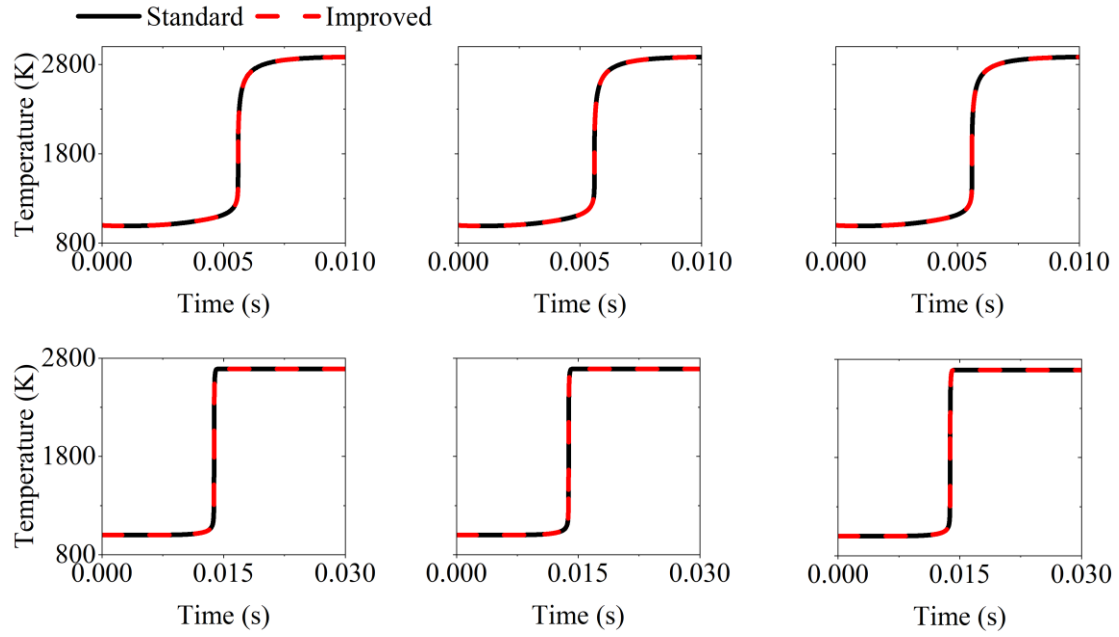


Fig. S3. Temperature profiles for ethylene/air under constant-pressure autoignition conditions. The first row: 24s70r, the second row: 59s268r. Left: Rodas34 algorithm, Middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.4 Ethanol

Table S4. Operating condition of ethanol/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|---------|-----------|------------|------|
| 39s379r | 1000 | 202650 | [7] |
| 57s383r | 1000 | 202650 | [8] |

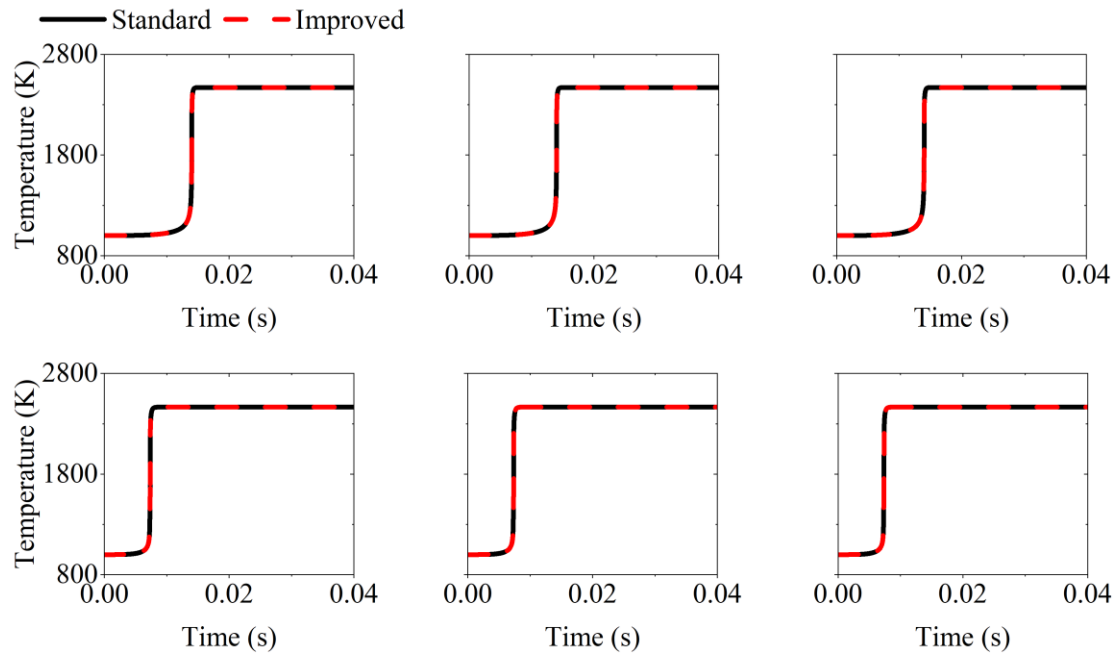


Fig. S4. Temperature profiles for ethanol/air under constant-pressure autoignition conditions. The

first row: 39s379r, the second row: 57s383r. Left: Rodas34 algorithm, Middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.5 N-heptane

Table S5. Operating condition of n-heptane/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|----------|-----------|------------|------|
| 46s115r | 700 | 2000000 | [9] |
| 68s283r | 700 | 2000000 | [10] |
| 188s939r | 700 | 2000000 | [11] |

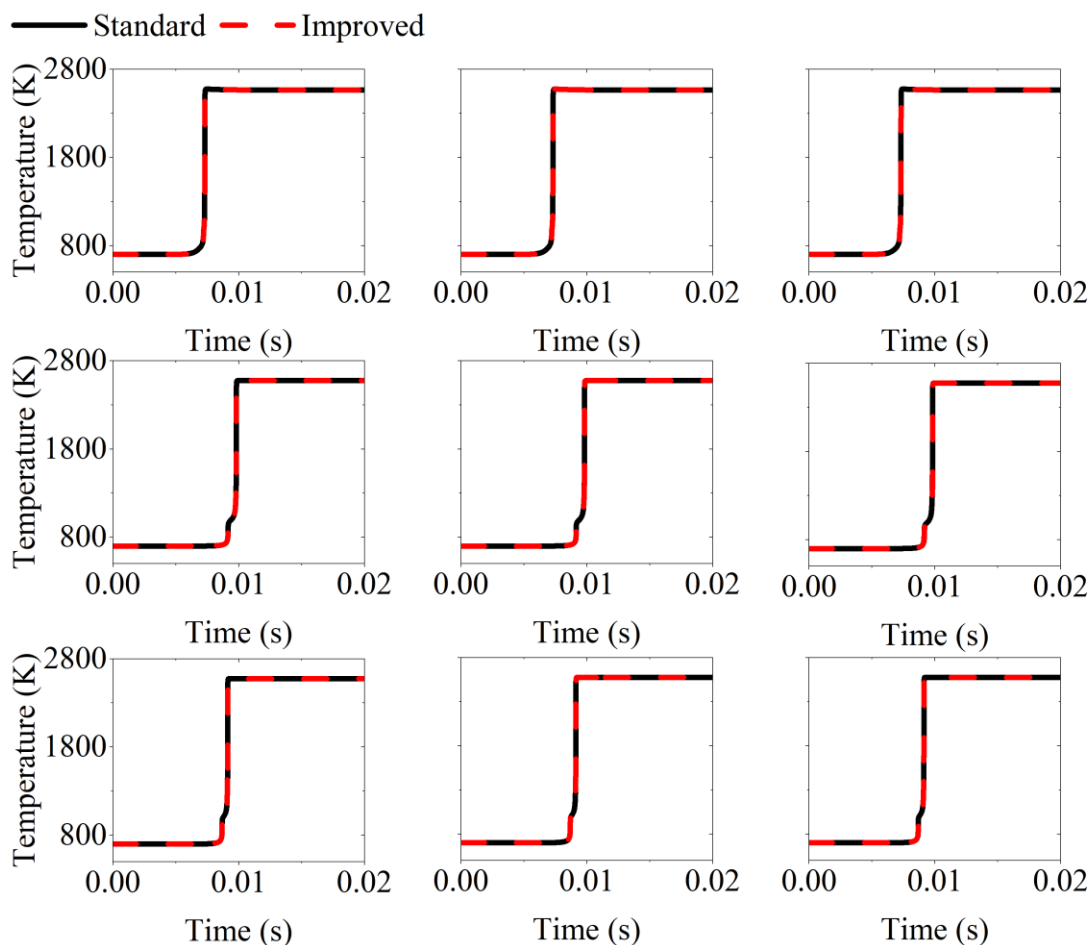


Fig. S5. Temperature profiles for n-heptane/air under constant-pressure autoignition conditions. The first row: 46s115r, the second row: 68s283r, the third row: 188s939r. Left: Rodas34 algorithm, middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.6 N-dodecane

Table S6. Operating condition of n-dodecane/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|---------|-----------|------------|------|
| 31s193r | 1000 | 2000000 | [12] |
| 54s268r | 1000 | 2000000 | [13] |

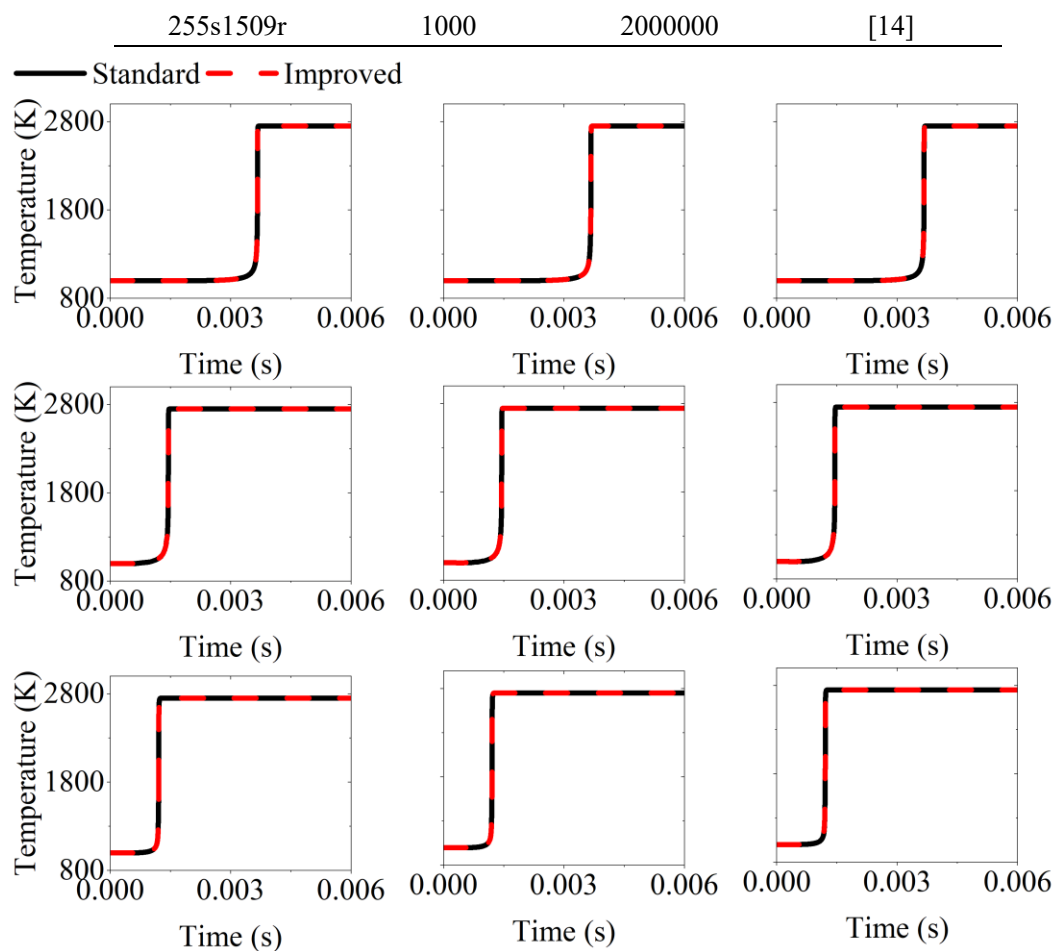


Fig. S6. Temperature profiles for n-heptane/air under constant-pressure autoignition conditions. The first row: 31s193r, the second row: 54s268r, the third row: 255s1509r. Left: Rodas34 algorithm, middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.7 Iso-octane

Table S7. Operating condition of iso-octane/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|-----------|-----------|------------|------|
| 140s643r | 700 | 2000000 | [15] |
| 874s3796r | 700 | 2000000 | [16] |

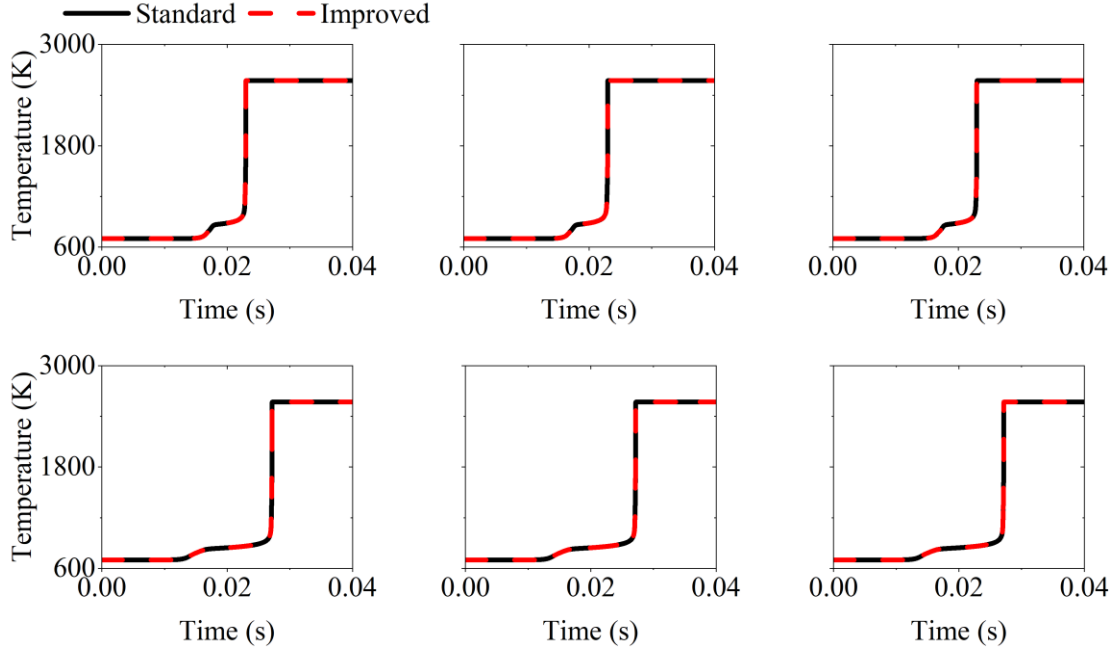


Fig. S7. Temperature profiles for iso-octane/air under constant-pressure autoignition conditions. The first row: 140s643r, the second row: 874s3796r. Left: Rodas34 algorithm, middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.8 Kerosene

Table S8. Operating condition of kerosene/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|--------|-----------|------------|------|
| 30s77r | 800 | 2000000 | [17] |
| 28s92r | 1100 | 2000000 | [18] |

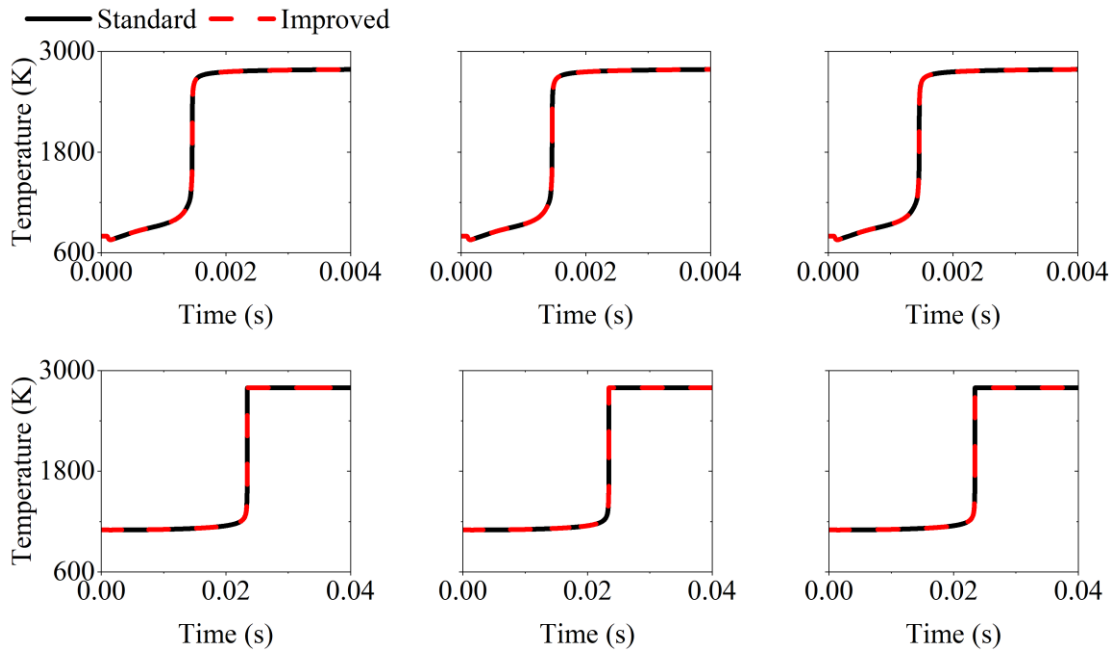


Fig. S8. Temperature profiles for kerosene/air under constant-pressure autoignition conditions. The first row: 30s77r, the second row: 28s92r. Left: Rodas34 algorithm, middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.9 Dimethyl Ether

Table S9. Operating condition of dimethyl ether/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|---------|-----------|------------|------|
| 26s71r | 700 | 2000000 | [19] |
| 39s175r | 700 | 2000000 | [20] |
| 79s351r | 700 | 2000000 | [21] |

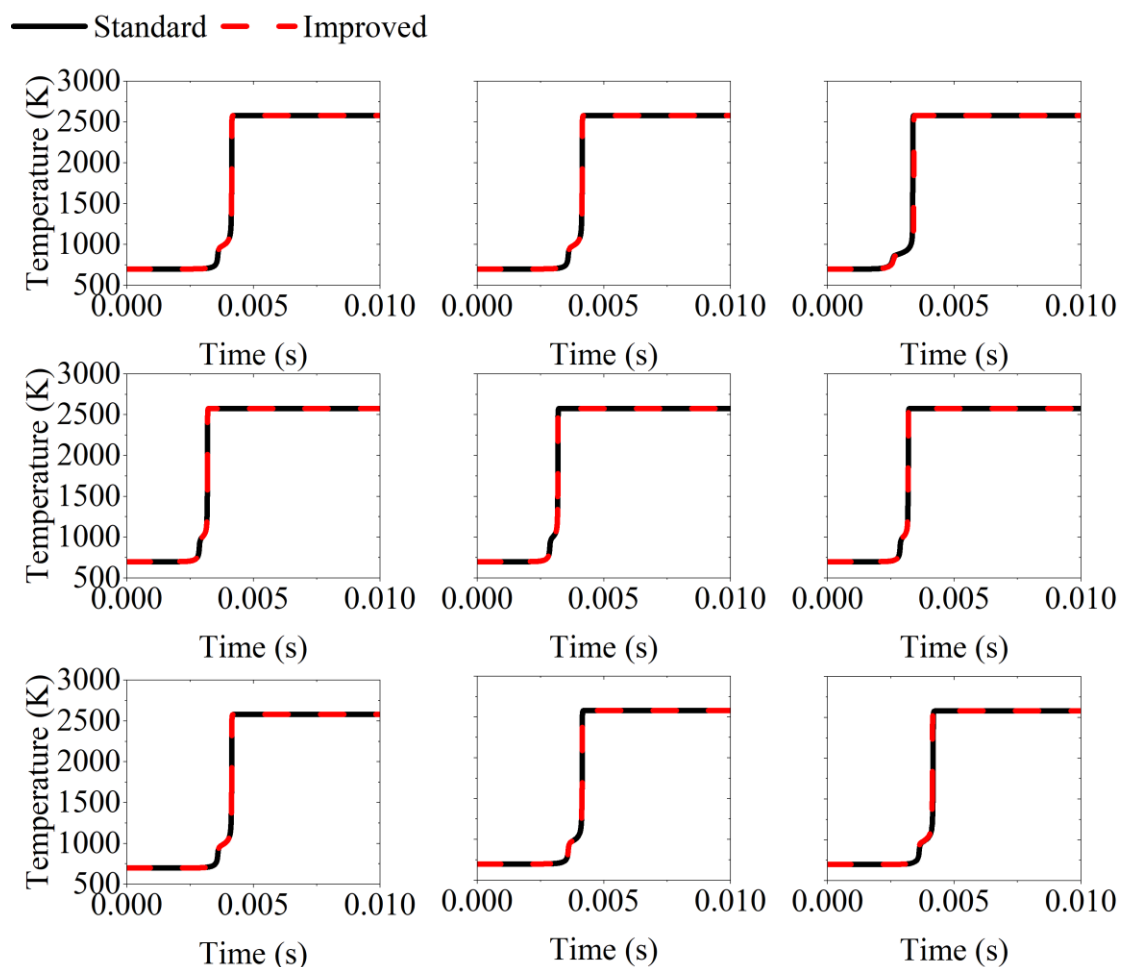


Fig. S9. Temperature profiles for dimethyl ether/air under constant-pressure autoignition conditions. The first row: 26s71r, the second row: 39s175r, the third row: 79s351r. Left: Rodas34 algorithm, middle: Rosenbrock34 algorithm, right: Seulex algorithm.

1.10 Ammonia

Table S10. Operating condition of ammonia/air constant pressure auto ignition

| Size | T_0 (K) | P_0 (Pa) | Refs |
|---------|-----------|------------|------|
| 59s356r | 1300 | 100000 | [22] |

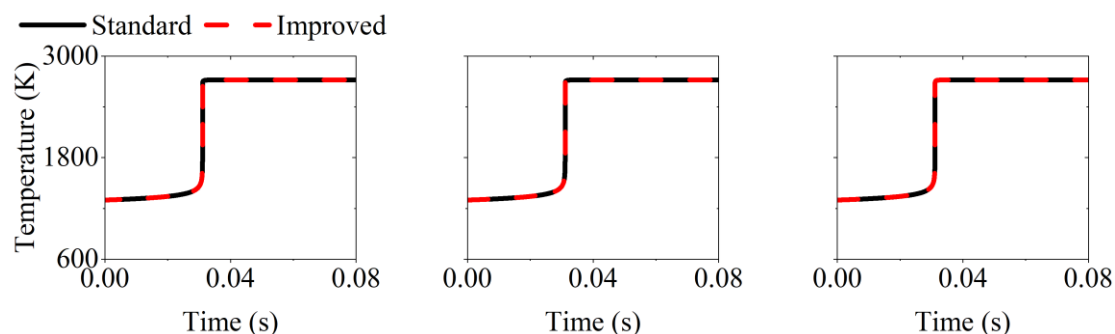


Fig. S10. Temperature profiles for ammonia/air under constant-pressure autoignition conditions. Left: Rodas34 algorithm, middle: Rosenbrock34 algorithm, right: Seulex algorithm.

2. Two-dimensional counter flow flame

Three ODE solvers, including Rodas34 algorithm, Rosenbrock34 algorithm and Seulex algorithm are selected for numerical verification. The counter flow flame is solved using application reactingFoam in foundation version OpenFOAM-10. The absolute tolerance and relative tolerance are 10^{-8} and 10^{-4} , respectively. The result using OpenFOAM standard chemistry solver and the improved chemistry solver is compared.

Table S11. Operating condition of methane/air counter flow flame

| fuel | T_{fuel} (K) | T_{air} (K) | U_{fuel} (m/s) | U_{air} (m/s) | P_{env} (Pa) | Chemistry mechanism |
|------------|-----------------------|----------------------|-------------------------|------------------------|-----------------------|---------------------|
| methane | 293 | 293 | 0.1 | 0.1 | 100000 | [22] |
| ammonia | 293 | 293 | 0.1 | 0.1 | 100000 | [23] |
| n-dodecane | 500 | 500 | 0.1 | 0.1 | 100000 | [13] |

2.1 Methane

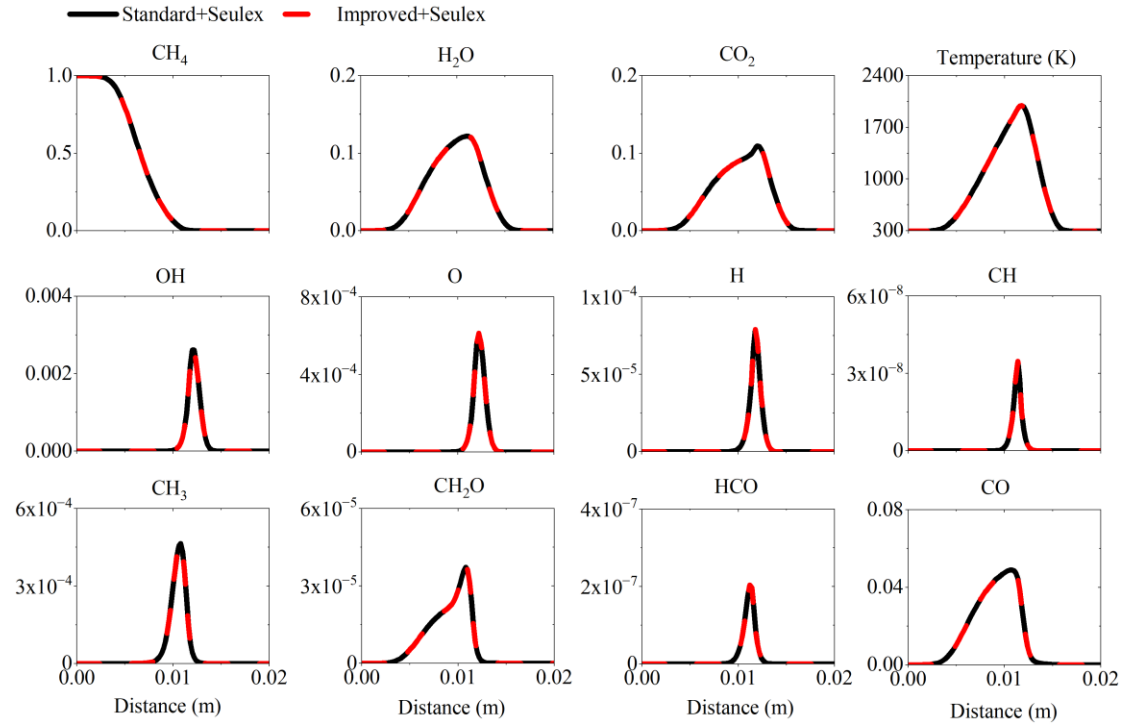


Fig. S11. Species mass fraction and temperature (K) profiles for counter flow flame of methane/air. The ODE algorithm is Seulex.

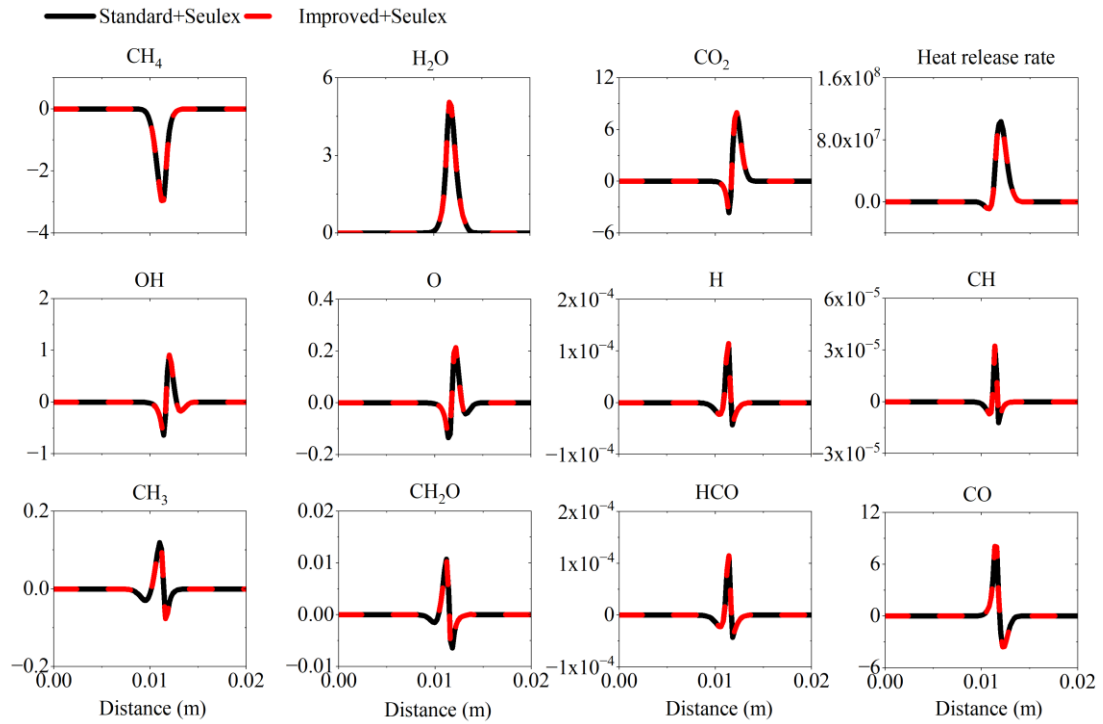


Fig. S12. Species production rate (kg/m³/s) and heat release rate (W/m³) profiles for counter flow flame of methane/air. The ODE algorithm is Seulex.

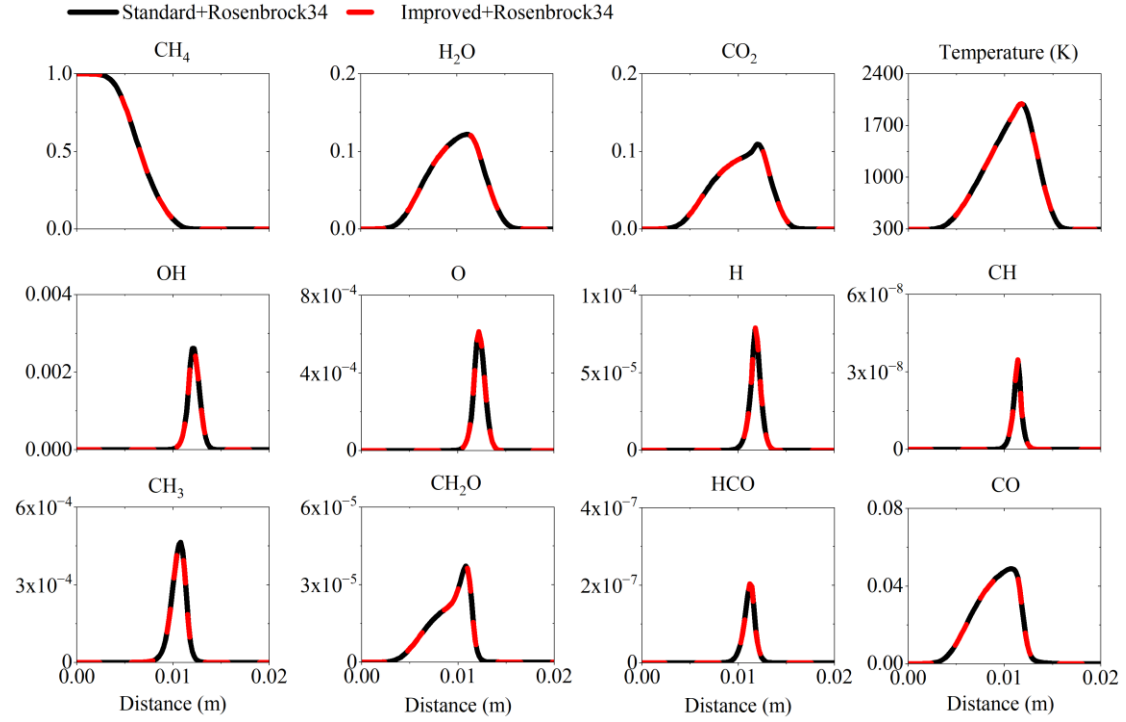


Fig. S13. Species mass fraction and temperature (K) profiles for counter flow flame of methane/air. The ODE algorithm is Rosenbrock34.

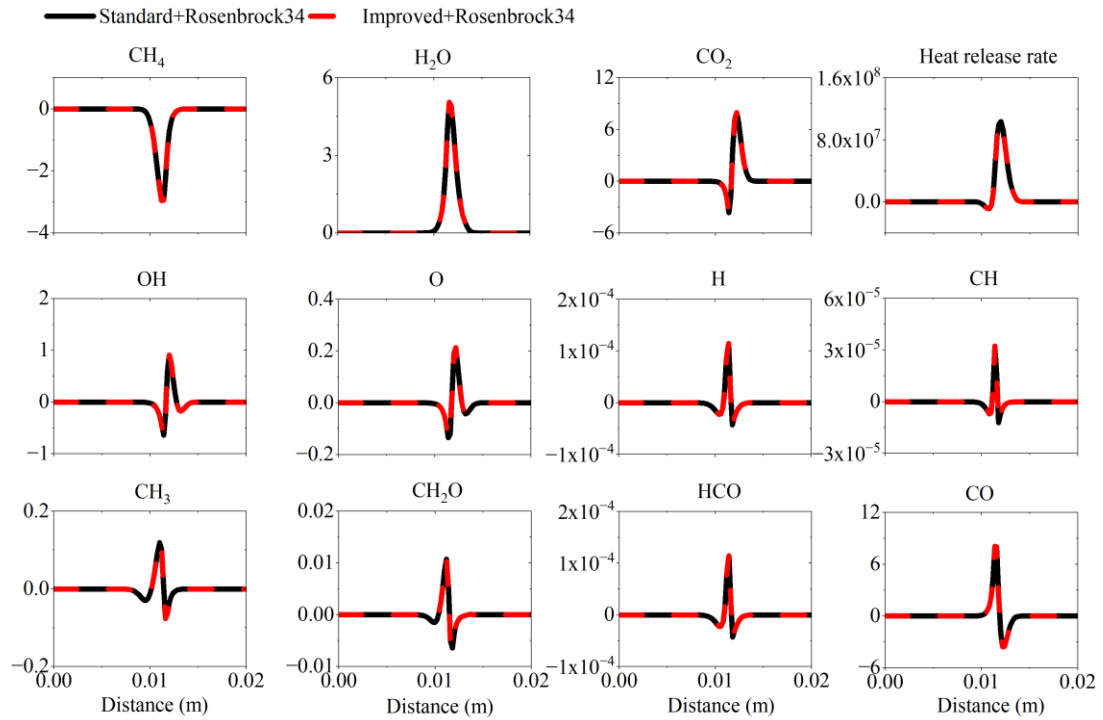


Fig. S14. Species production rate ($\text{kg/m}^3/\text{s}$) and heat release rate (W/m^3) profiles for counter flow flame of methane/air. The ODE algorithm is Rosenbrock34.

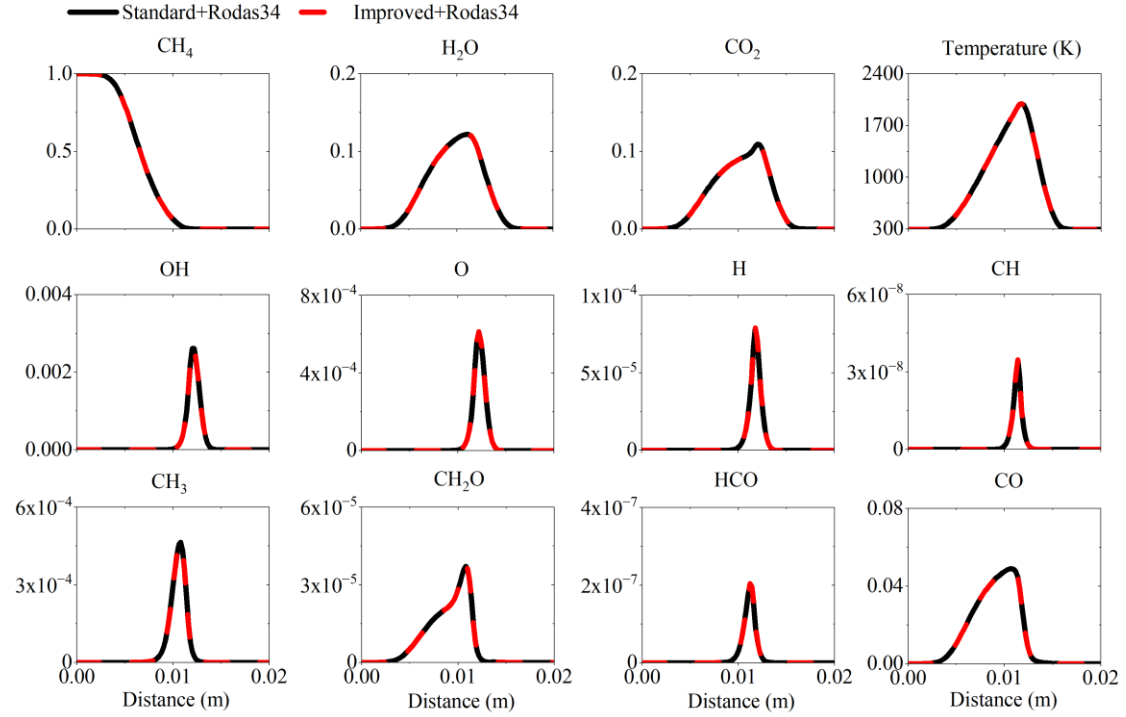


Fig. S15. Species mass fraction and temperature (K) profiles for counter flow flame of methane/air. The ODE algorithm is Rodas34.

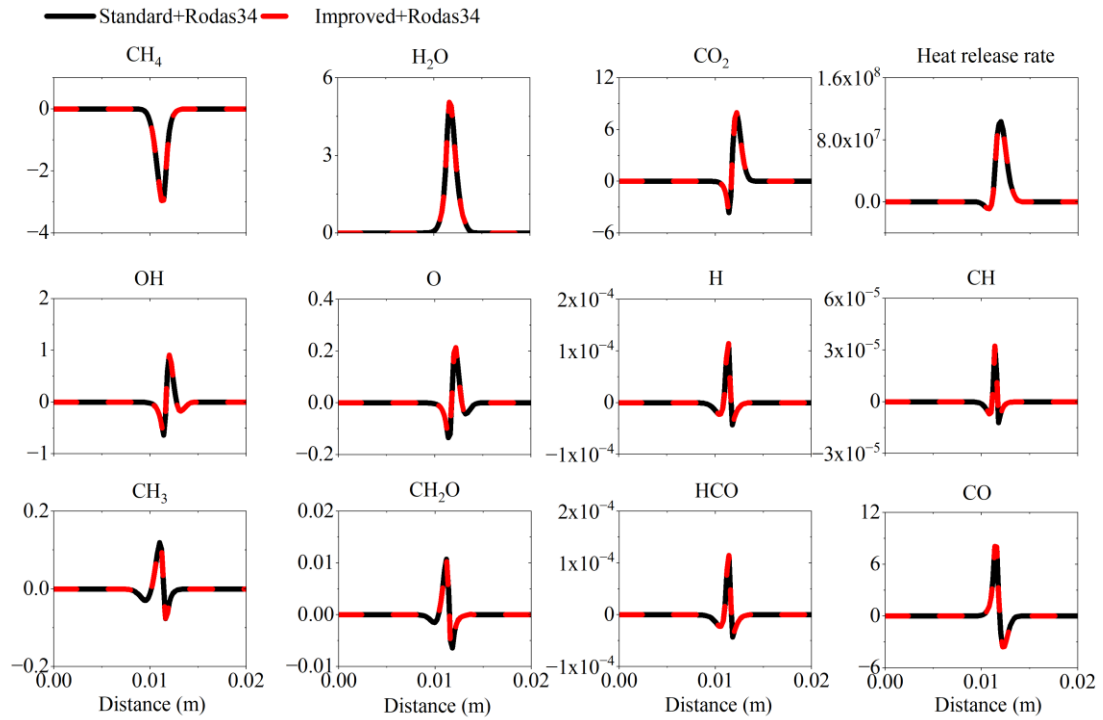


Fig. S16. Species production rate ($\text{kg/m}^3/\text{s}$) and heat release rate (W/m^3) profiles for counter flow flame of methane/air. The ODE algorithm is Rodas34.

2.2 Ammonia

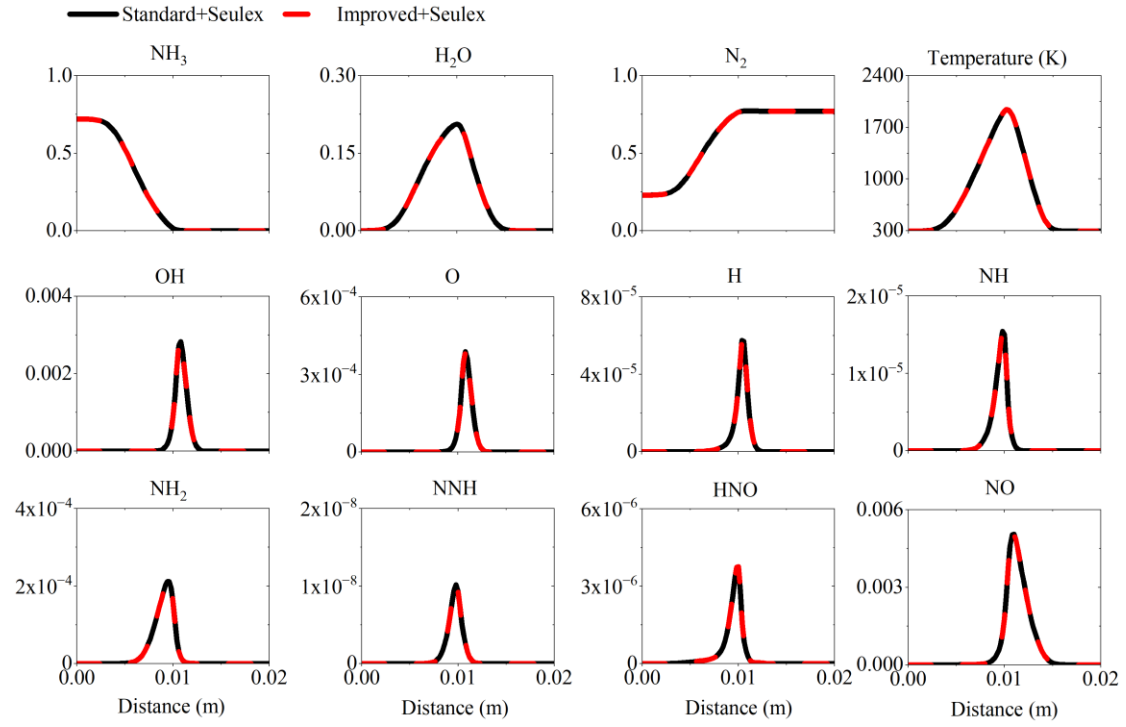


Fig. S17. Species mass fraction and temperature (K) profiles for counter flow flame of ammonia/air. The ODE algorithm is Seulex.

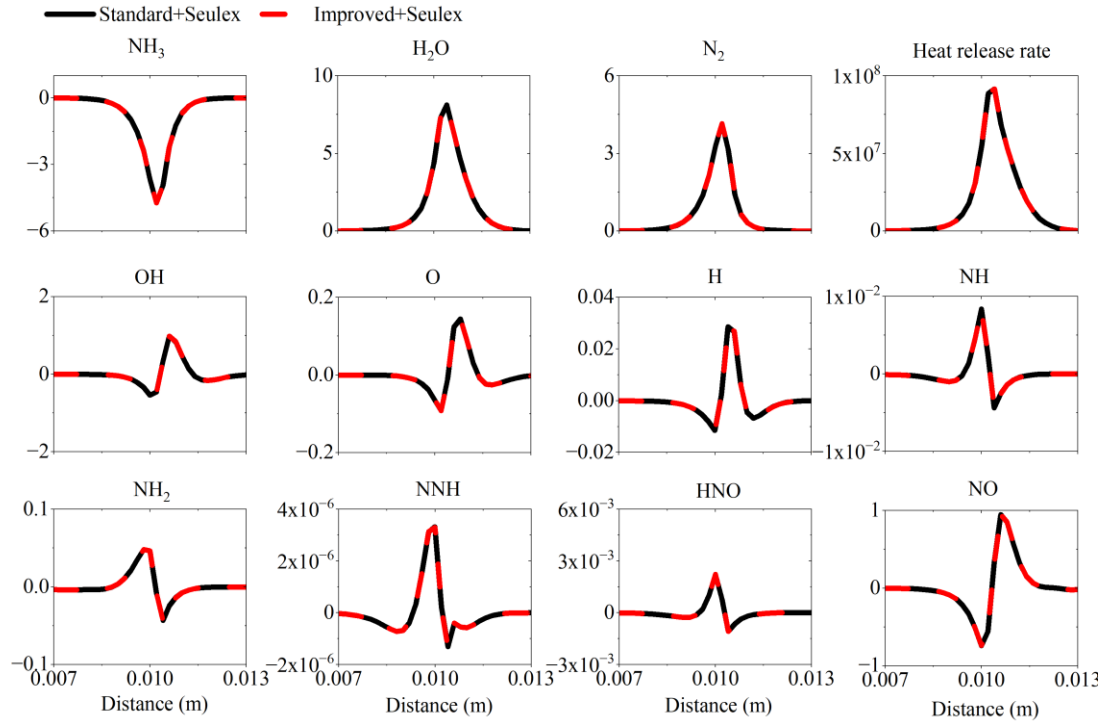


Fig. S18. Species production rate ($\text{kg}/\text{m}^3/\text{s}$) and heat release rate (W/m^3) profiles for counter flow flame of ammonia/air. The ODE algorithm is Seulex.

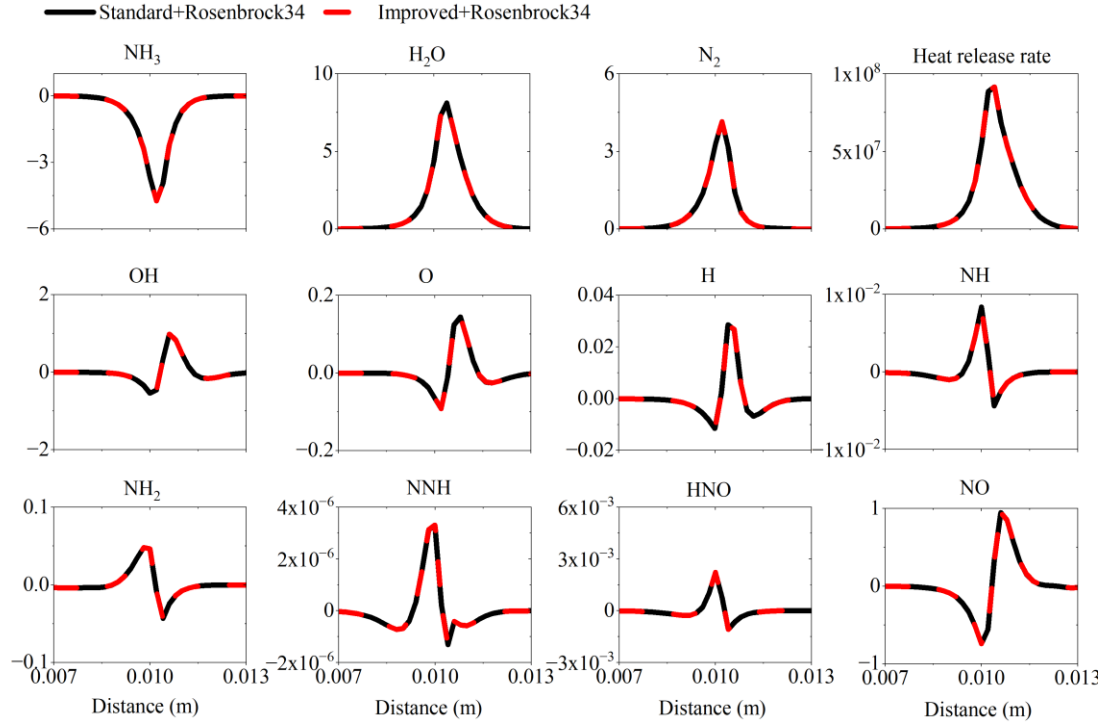


Fig. S19. Species mass fraction and temperature (K) profiles for counter flow flame of ammonia/air. The ODE algorithm is Rosenbrock34.

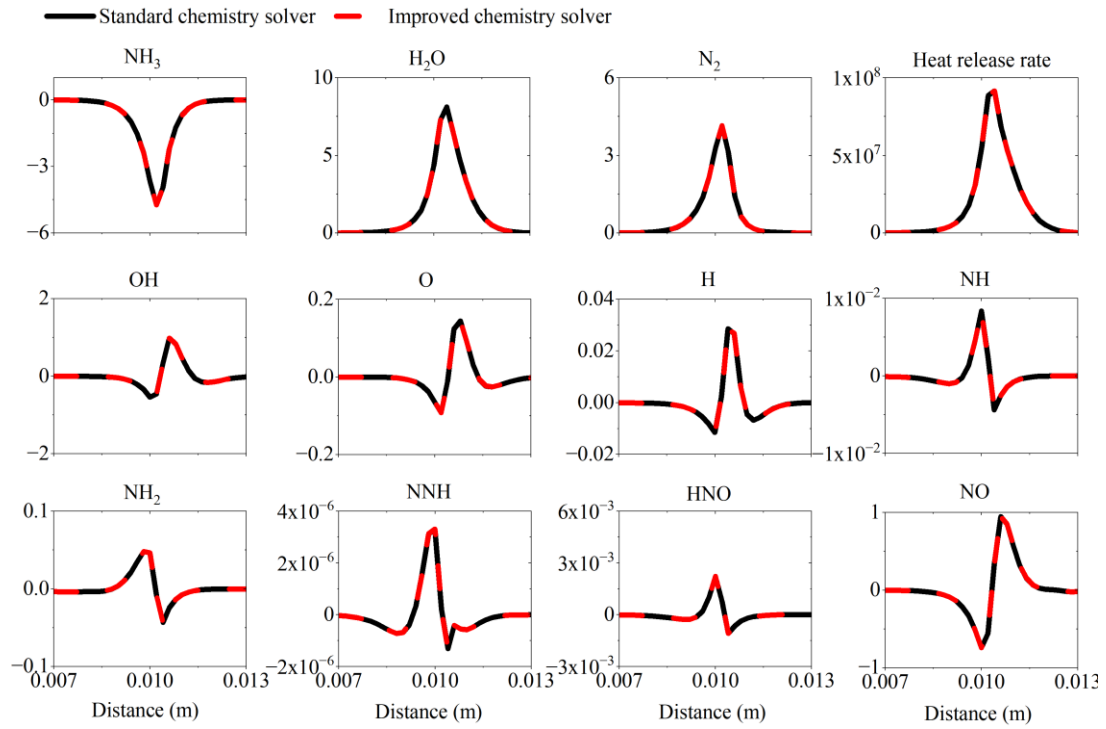


Fig. S20. Species production rate ($\text{kg/m}^3/\text{s}$) and heat release rate (W/m^3) profiles for counter flow flame of ammonia/air. The ODE algorithm is Rosenbrock34.

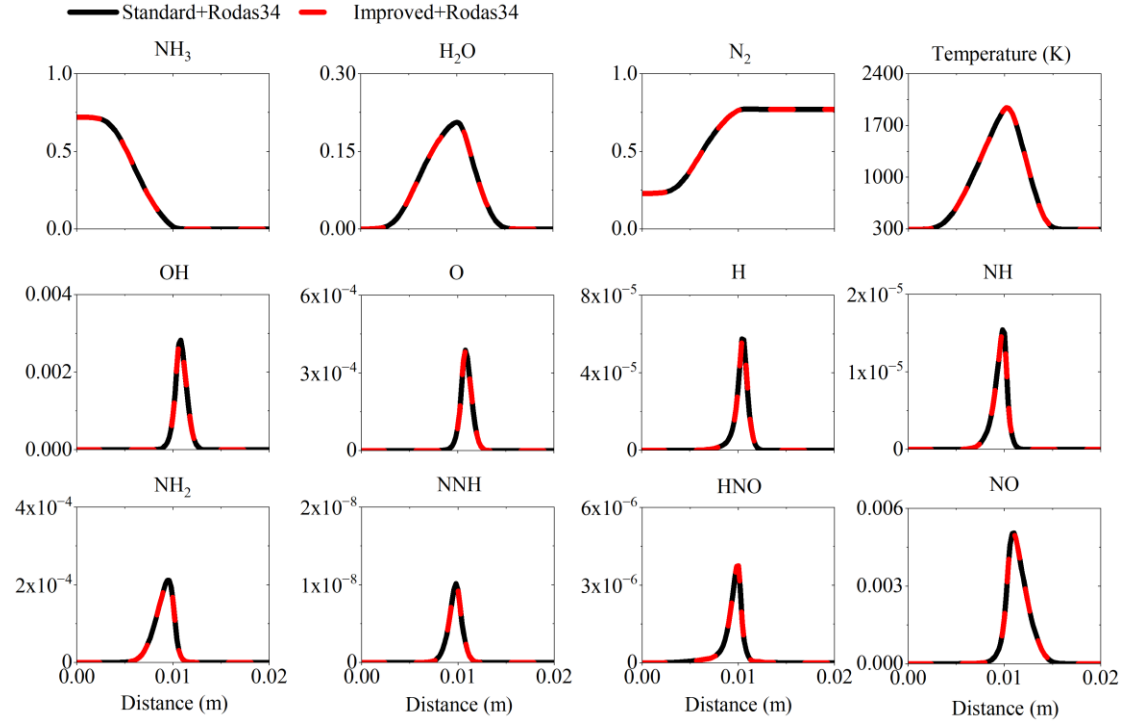


Fig. S21. Species mass fraction and temperature (K) profiles for counter flow flame of ammonia/air. The ODE algorithm is Rodas34.

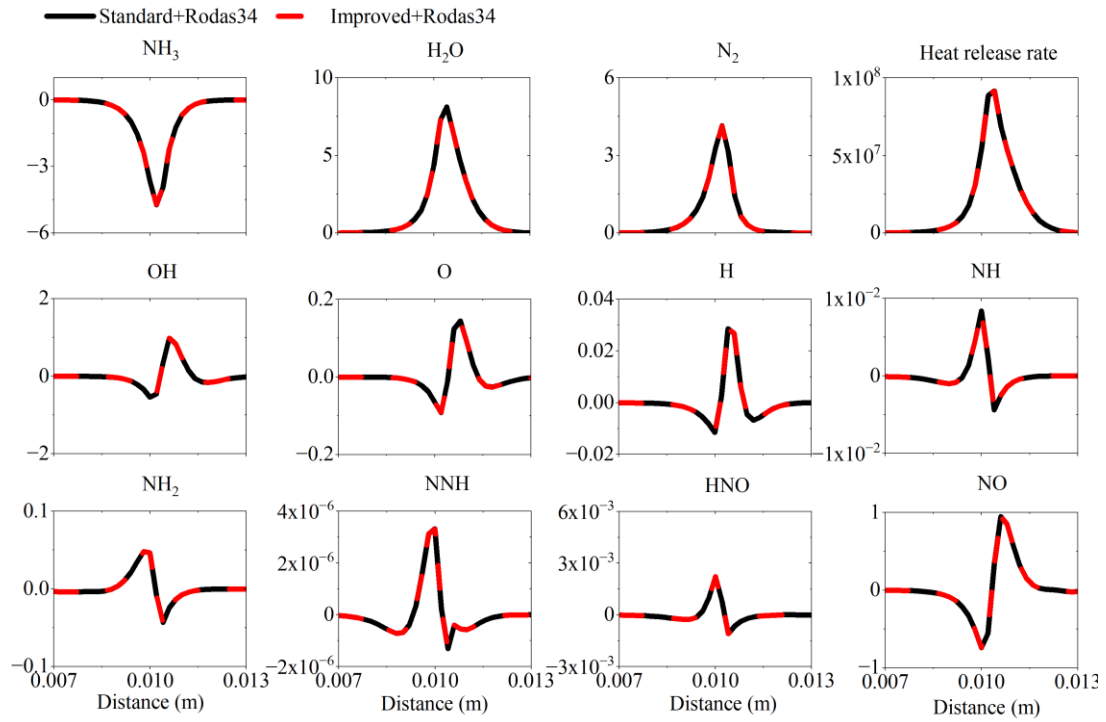


Fig. S22. Species production rate ($\text{kg/m}^3/\text{s}$) and heat release rate (W/m^3) profiles for counter flow flame of ammonia/air. The ODE algorithm is Rodas34.

2.3 N-dodecane

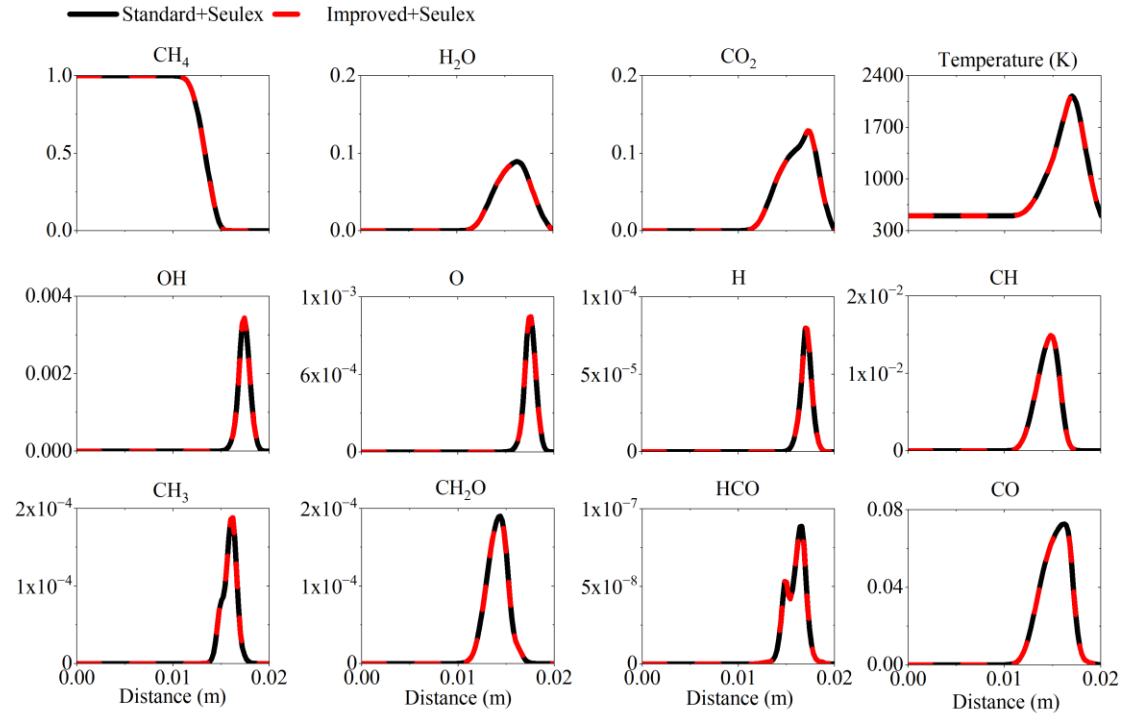


Fig. S23. Species mass fraction and temperature (K) profiles for counter flow flame of N-dodecane/air. The ODE algorithm is Seulex.

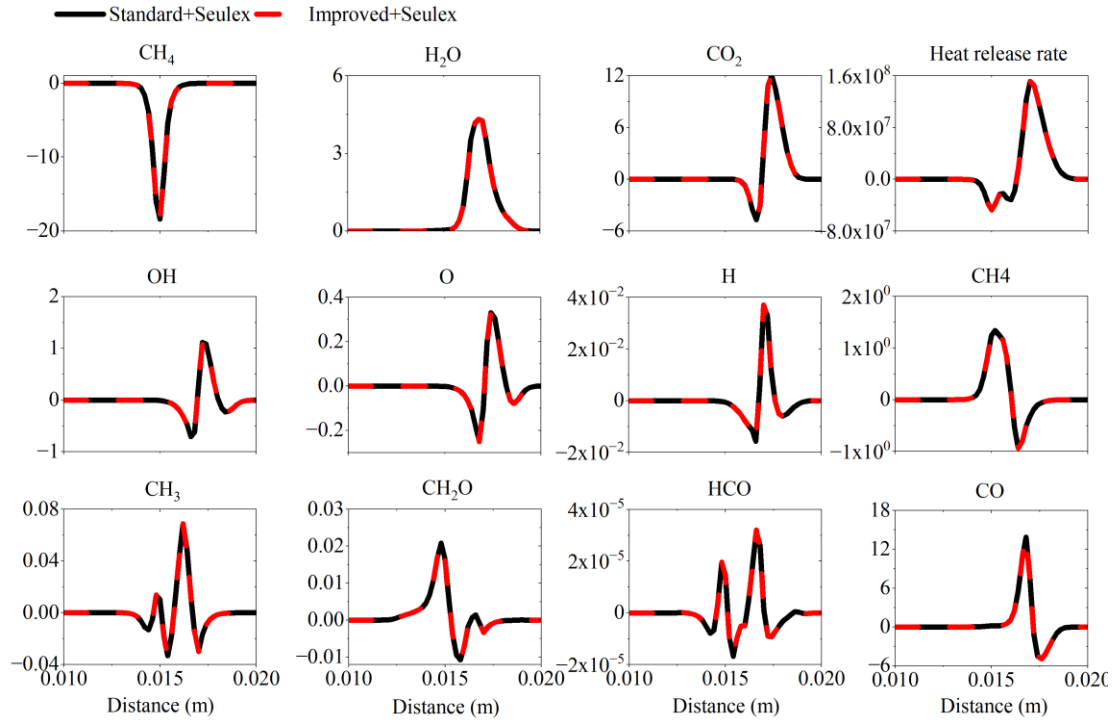


Fig. S24. Species production rate ($\text{kg/m}^3/\text{s}$) and heat release rate (W/m^3) profiles for counter flow flame of N-dodecane/air. The ODE algorithm is Seulex.

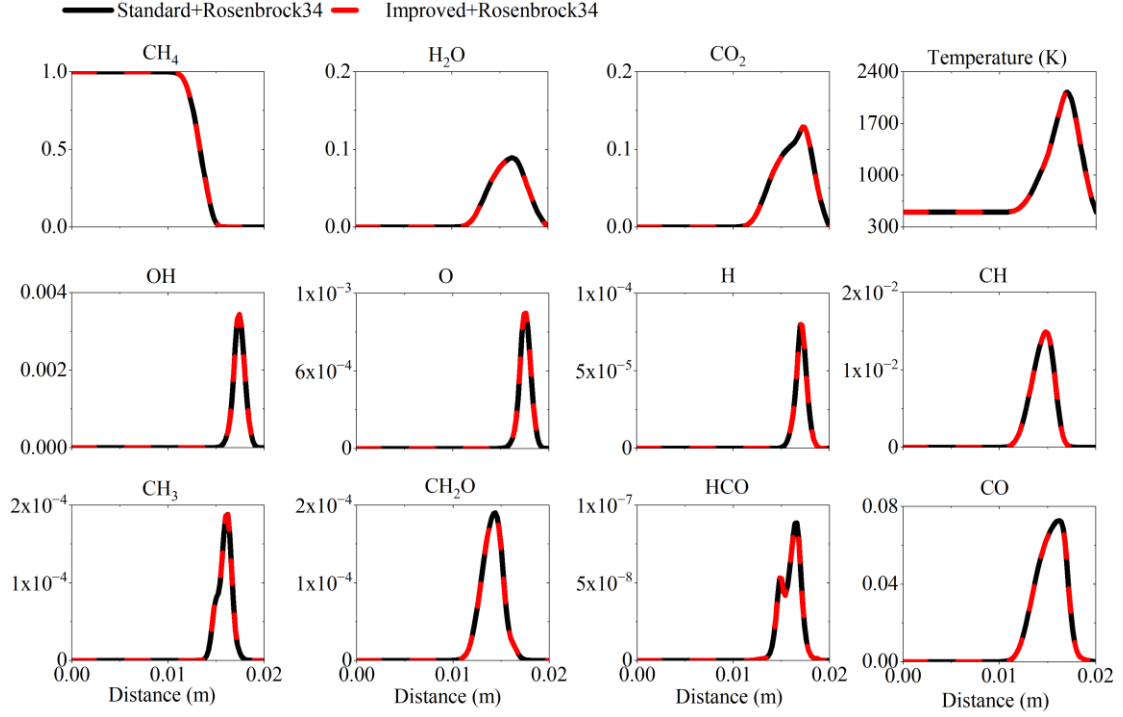


Fig. S25. Species mass fraction and temperature (K) profiles for counter flow flame of N-dodecane/air. The ODE algorithm is Rosenbrock34.

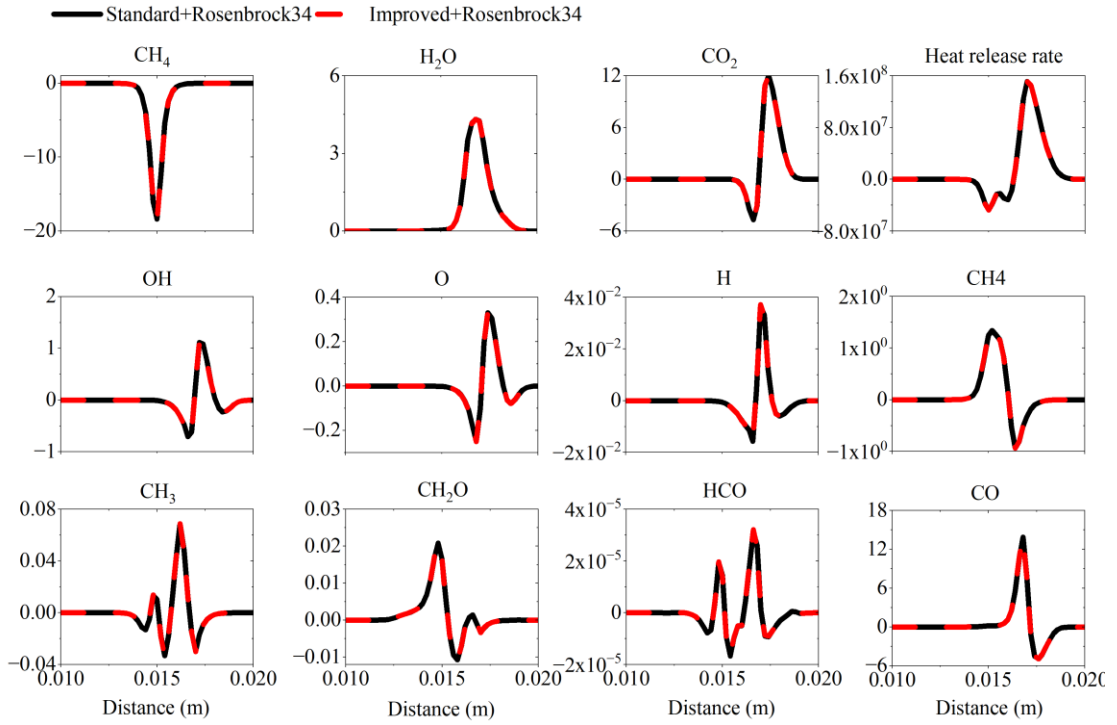


Fig. S26. Species production rate ($\text{kg/m}^3/\text{s}$) and heat release rate (W/m^3) profiles for counter flow flame of N-dodecane/air. The ODE algorithm is Rosenbrock34.

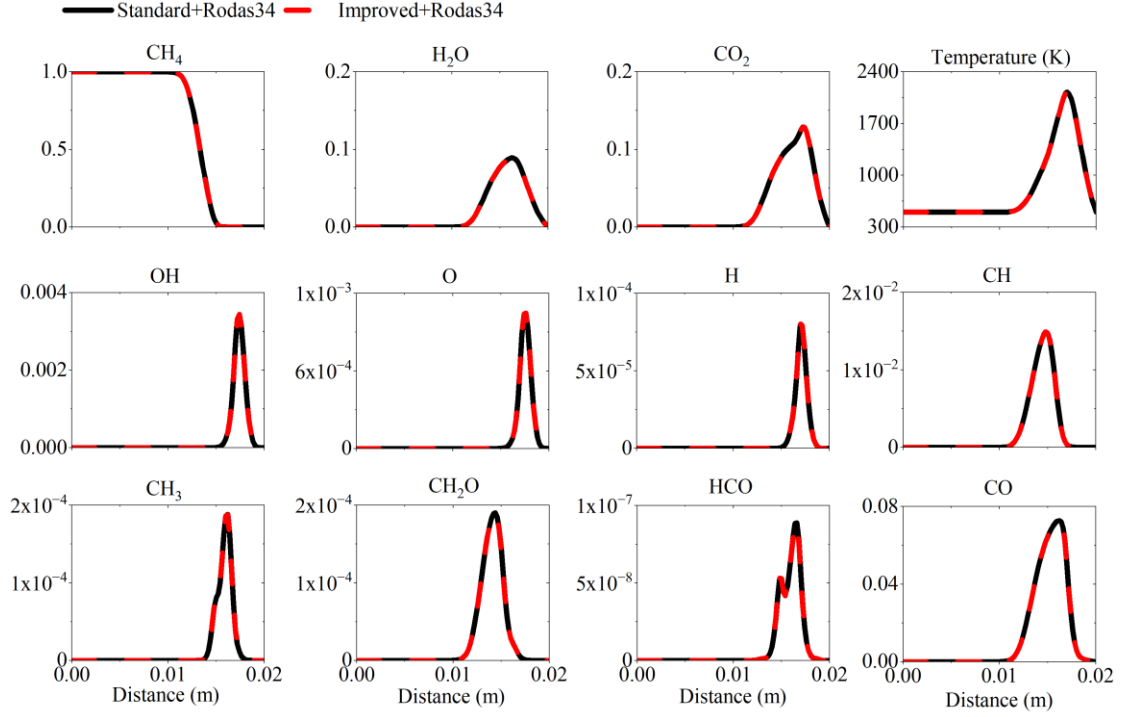


Fig. S27. Species mass fraction and temperature (K) profiles for counter flow flame of N-dodecane/air. The ODE algorithm is Rodas34.

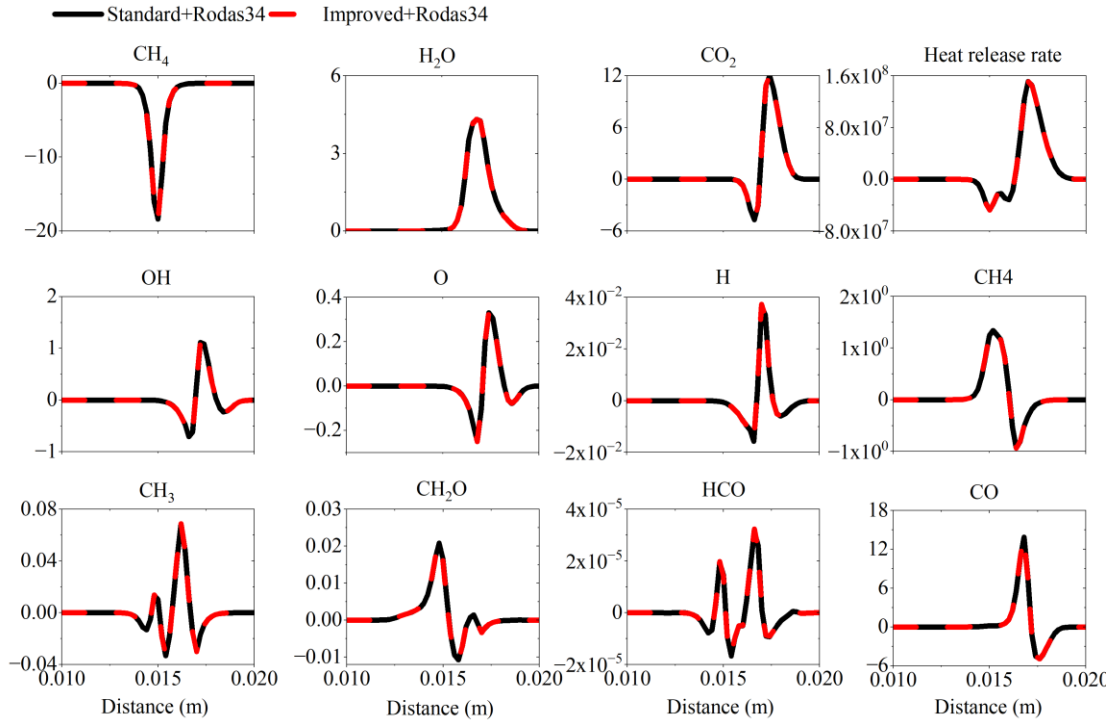


Fig. S28. Species production rate ($\text{kg/m}^3/\text{s}$) and heat release rate (W/m^3) profiles for counter flow flame of N-dodecane/air. The ODE algorithm is Rodas34.

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