Forced Oscillation - Resonance.

If we apply external force to damped oscillator, then the applied force tends to keep the oscillator oscillator oscillating. The force needs to be periodic and not necessarily equal to the natural freq. wo if the freq of applied force is same as the natural freq. of the oscillator, the phenomenon of resonance or resonante absorption occurs. In such cases, the amp. of oscillation increases enormously.

Differential egn of forced oscillations.

Consider a body of mass 'm' undergoing damped harmonic motion.

Suppose ext. force Fe = Fo sinpt

is applied on it.

Exec. of applied force = \$\frac{1}{27}\$

Freq. of applied force = P/2TT
Amp " = Fo.

forces acting on the Oscillator 6
1) Restoring force = -kx

2) Damping force = -b dx/dn

3) Applied force = Fosin bt o's Net force F = Fosimpt-bdx-kn or $m\frac{d^2x}{dt^2} + b\frac{dx}{dt} + kx = F_0 \sin \beta t$ $\frac{d^2x}{dt^2} + 2r \frac{dx}{dt} + \omega_0^2 x = fo sinpt$ where $\frac{b}{m} = 2r$, $\frac{k}{m} = \omega_0^2$, $\frac{f_0}{m} = fo$ If RHS = 0, then egn becomes same as damped oscillator. Steady state function
Let $x = A sin(bt - \phi)$ be a particular som where of is the phase difference b/w the applied force and displacement of the Oscillator.

$$\frac{d^2x}{dt} = \rho A \cos(\rho t - \phi)$$

$$\frac{d^2x}{dt^2} = -\beta^2 A \sin(\rho t - \phi)$$

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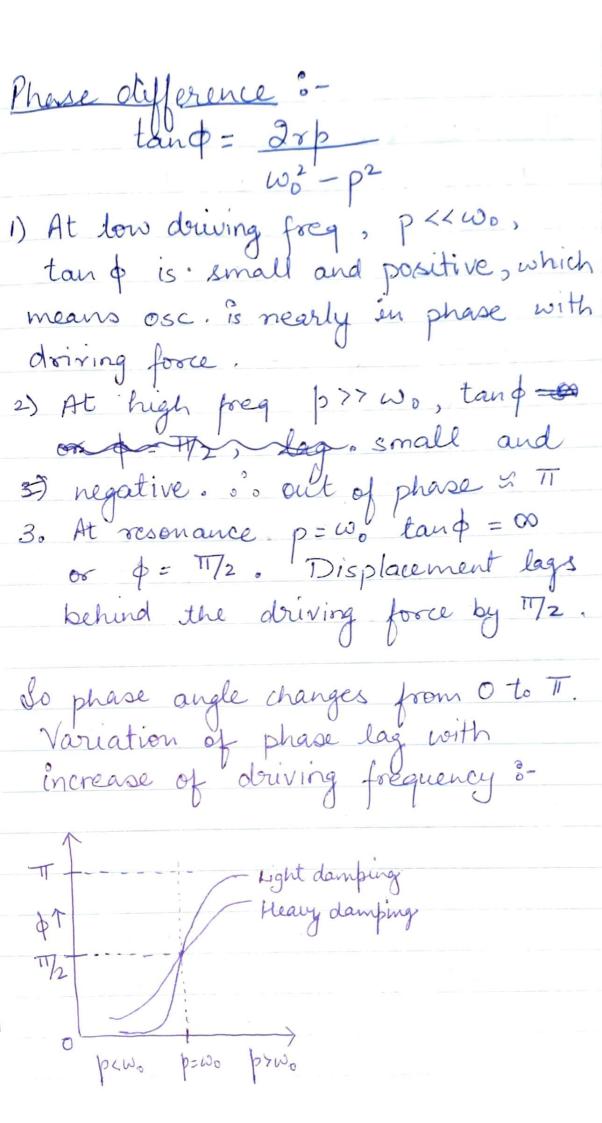
Again dividing (1) by (2) $tan \phi = \frac{2rb}{\omega_o^2 - p^2}$ or phase difference by n forced oscillator and the applied force $\phi = \tan^{-1}\left(\frac{2rp}{\omega_0^2 - p^2}\right)$ And finally. $x = \frac{fo}{\sqrt{(w_0^2 - b^2)^2 + 4r^2b^2}} \sin(bt - \phi)$ which is the som of forced ose having same freg = p/2TI but lagging behind in phase

Amplitude Resonance &

Acc. to egn (3), the amplitude
depends on wo-p, the difference
in freq. b/w ascillator and force.
applied. Smaller the differences
larger the amplitude.

CASE-I : At very low driving freq P << Wo, Then Ass for = Folm = Fo Wo K/m = K which means amp depends only on force const. CASE-II: At very high driving freq p>>wo, then $A \times f_0 = \frac{F_0/m}{p^2} = \frac{F_0}{mp^2}$ amp decreases with as pinc. and depends on mass. Resonant driving forequency The foreg at which the amp. of the oscillator is maximum is k/a resonant frequency. For this denominator of Amp. should be minimum? $\frac{d}{dp} \left[(w_0^2 - p^2)^2 + 4r^2 p^2 \right] = 0$ $2(w_0^2 - p^2)(-2p) + 4r^2(2p) = 0$

or $\omega_0^2 - p^2 = 2\gamma^2$ P=PR= [W,2-2+2] · · freq = PR = \ \w^2 - 282 211 211 which is slightly less than natural frequency wo/2TT and than damped freq \(\sum_0^2 - \mathbf{3}\tau^2\) Amax = $\frac{fo}{2r(\omega_0^2 - \gamma^2)^{1/2}}$ Also w2-2x2=p2 0x 80, $A_{max} = \frac{f_0}{2 \cdot (p^2 + 8^2)^{1/2}}$ showing that smaller the value of Amax. When damping is small; r ->0, the resonant freq. I natural freq. In ideal case, when there is no damping, amp will become infinite but since damping is never zero, so amp finite and controls the



Sharpness of resonanace -Amp. of forced oscillations attains peak value when freq. of applied force = resonance freg. But below and above it, the amp falls. If fall in amp. for a small change in freq. from resonant value is high, then the resonance is soud to be sharp, while if the fall in amp is small, then the resonance is said to be glat. Effect of damping on the sharpness of resonance - $A = \frac{fo^2}{\sqrt{(w_0^2 - p^2)^2 + 4x^2}}$

10 Smaller the damping, sharper due resonance and vice-versa

2. At low driving freq, amp is nearly
the same for all values of damping.
3. As pincreases, A increases. A increases more for low r. At h = 0, A = a at resonance. 4. Further increase in p beyond for reduces the amp. 5. With increase in damping, peak moves to the left. 6. With inc in 'r', peak flattens.

Power absorption by forced oscillator Ang power absorbed per cycle is equal to the arg. power dissipated after steady state

18 reached. To find the expression: $x = \frac{f_0}{\left[\left(\omega_0^2 - p^2\right)^2 + 4\gamma^2 p^2\right]^{\frac{1}{2}}} \sin\left(pt - \phi\right)$ where $f_0 = \frac{F_0}{m}$ and so on ---Instantaneous velocity: $v = \frac{dx}{dt} = \frac{f \cdot p}{\left((w_0^2 - p^2)^2 + 4x^2p^2\right)^{1/2}}$ Power absorbed: $P = FU = (Fosinpt). \qquad fob cos(pt-\phi)$ $= \frac{mf_0^2 p}{(\omega_0^2 - p^2)^2 + 4r^2p^2/2}$ $= \frac{mf_0^2 p}{(\omega_0^2 - p^2)^2 + 4r^2p^2/2} + \sin^2 pt \sin \phi$ Taking untegral from 0 to T and find avg. $Var = m \int_{0}^{2} b \left(\frac{1}{2} \sin b \right)$ $\left[\left(\frac{\omega^{2} - \rho^{2}}{2} \right)^{2} + 4r^{2} b^{2} \right] \left(\frac{1}{2} \sin b \right)$ Since $tan \phi = \frac{2rp}{\omega_o^2 - p^2}$ $\Rightarrow sin \phi = \frac{2rp}{\omega_o^2 - p^2 + 4r^2p^2}$ from eqn 1

Maximum power absorption The denominator should be min and for that $(w^2 - p^2)^2 = 0$ And Pav (max) = mforp2 = 4x2p2 $=\frac{mfo^2}{2b/m}=\frac{m^2fo^2}{2b}.$ Bandwidth of resonance curve: As seen above max power is absorbed Power vs. freg. curve is as ?

W, and W2 correspond to the value = Pmax

Pav
$$(max) = \frac{mf_0^2}{4r}$$

At w , and w , $P_{av} = \frac{1}{8}P_{av}(max)$

or

 $\frac{mf_0^2rp^2}{(w_0^2-p^2)^2+4r^2p^2} = \frac{1}{9} \cdot \frac{mf_0^2}{4r}$
 $(w_0^2-p^2)^2+4r^2p^2 = 8r^2p^2$
 $(w_0^2-p^2)^2=4r^2p^2$
 $w_0^2-p^2=\pm 2rp$
 w_0+p .

If w_2-w , is the bandwidth of oscillator then $w_2-p=\frac{2rp}{w_0+p}$
 w_0+p
 w_0+p

is the resonance 2 vice-verse.

Since
$$w_2 - w_1 = 2\tau$$
.

 $|w_0 - w_1| = |w_2 - w_0| = \Delta p = \tau$

This change Δp in the value of driving freq. p for which the ang. power absorbed by the driven oscillator falls from its max value P max to half this value is the half width of the ang. power absorbed.

Quality factor in Terms of half—bandwith.

 $Q = 2\pi E$
 PT

Energy = $K \cdot E + P \cdot E = \frac{1}{2} m p^2 A^2 \cos^2(pt - p)$

Energy =
$$k.E + P.E = \frac{1}{2}mp^2A^2\cos^2(pt - p)$$

 $+\frac{1}{2}m\omega_0^2A^2\sin^2(pt - p)$
 $=\frac{1}{4}mp^2A^2 + \frac{1}{4}m\omega_0^2A^2$
 $=\frac{1}{4}mA^2(p^2+\omega_0^2)$

$$\left(\frac{mA^2p^2}{2C}\right)$$
 x T $= 2T/p$

$$\theta = \frac{1}{2} \left(\frac{p^2 + \omega_0^2}{p^2} \right) \cdot \mathcal{L} = \frac{1}{2} \left(\frac{1 + \omega_0^2}{p^2} \right) p^2$$
At resonance $p = p_R = \omega_0$

$$\theta = \frac{1}{2} \times 2 p^2 = p^2 = \omega_0 \mathcal{L} = \frac{\omega_0}{2 \Delta p}.$$
At low damping, \mathcal{L} is large so
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At low damping, \mathcal{L} is large sonance sharp:

$$\frac{\text{Velocity Resonance}}{x = A \sin(p_1 - \phi)} = \frac{f_0 \sin(p_1 - \phi)}{\int (\omega_0^2 - p^2)^2 + 4\pi^2 p^2}$$

$$\psi = \frac{1}{2} \left(\frac{p^2 + \omega_0^2}{p^2} \right) \cdot \frac{1}{2} \left(\frac{p^2}{p^2} \right) \cdot \frac{1}{2} \left(\frac{p^2}{p^2}$$