

# Computational Physics Labwork: Numerical Hydrodynamics

Christoph Schäfer & Wilhelm Kley  
Institut für Astronomie & Astrophysik  
& Kepler Center for Astro and Particle Physics Tübingen

EBERHARD KARLS  
UNIVERSITÄT  
TÜBINGEN



# Hydrodynamics: Hydrodynamical Equations

The Euler equations in hydrodynamics read in the conservative form

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0 \quad (1)$$

$$\frac{\partial(\rho \mathbf{u})}{\partial t} + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = -\nabla p + \rho \mathbf{k} \quad (2)$$

$$\frac{\partial(\rho \epsilon)}{\partial t} + \nabla \cdot (\rho \epsilon \mathbf{u}) = -p \nabla \cdot \mathbf{u} \quad (3)$$

$\mathbf{u}$ : velocity,  $\mathbf{k}$ : specific external forces,  $\epsilon$  specific internal energy

These equations describe the conservation of mass, momentum and energy.

The closure condition is given by the equation of state (EOS)

$$p = (\gamma - 1) \rho \epsilon. \quad (4)$$

Using the EOS, we can also reformulate the energy equation (3) in an equation for the pressure

$$\frac{\partial p}{\partial t} + \nabla \cdot (p \mathbf{u}) = -(\gamma - 1) p \nabla \cdot \mathbf{u}. \quad (5)$$

## Hydrodynamics: Re-formulation of the Euler eqs

Write out the divergence terms on the left hand side and use the continuity equation for the momentum and energy equation to obtain

$$\frac{\partial \rho}{\partial t} + (\mathbf{u} \cdot \nabla) \rho = -\rho \nabla \cdot \mathbf{u} \quad (6)$$

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} \nabla p + \mathbf{k} \quad (7)$$

$$\frac{\partial p}{\partial t} + (\mathbf{u} \cdot \nabla) p = -\gamma p \nabla \cdot \mathbf{u}. \quad (8)$$

Since all terms are functions of the location ( $\mathbf{r}$ ) and time ( $t$ ), e.g., the density  $\rho(\mathbf{r}, t)$ , we can use the total derivative on the left hand side.

For the continuity equation, we get

$$\frac{D\rho}{Dt} = \frac{\partial \rho}{\partial t} + (\mathbf{u} \cdot \nabla) \rho = -\rho \nabla \cdot \mathbf{u}. \quad (9)$$

The operator

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla \quad (10)$$

is called Lagrangian derivative or material derivative and corresponds to the total time derivative  $d/dt$ .

Now with the help of the Lagrangian derivative, we can write

$$\frac{D\rho}{Dt} = -\rho \nabla \cdot \mathbf{u} \quad (11)$$

$$\frac{D\mathbf{u}}{Dt} = -\frac{1}{\rho} \nabla p + \mathbf{k} \quad (12)$$

$$\frac{Dp}{Dt} = -\gamma p \nabla \cdot \mathbf{u} \quad (13)$$

These equations describe the evolution of the quantities in a reference frame that moves with the flow.

This so-called Lagrangian representation is quite useful for radial star oscillations, which is a 1D problem with moving mass shells.

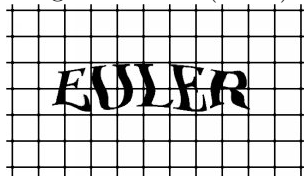
# Numerical Hydrodynamics: Challenge

Consider the full evolution of the time dependent hydrodynamical equations. The non-linear partial differential equations are solved numerically from continuum to discretisation



# Numerical Hydrodynamics: How to solve the hydro eqs...

grid schemes (Euler)



fixed grid

- flow through grid cells

$$\rho \left( \frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = -\nabla p$$

Methods:

- Finite Differences  
no conservation properties
- Finite Volume  
conservation properties
- Riemann-Solver  
wave properties
- Problem: Discontinuities

particle schemes (Lagrange)

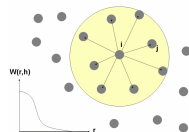


moving grid or particles

- fluid moves the grid or the particles

$$\rho \frac{d\mathbf{u}}{dt} = -\nabla p$$

Methods: Smoothed Particle Hydrodynamics



'smeared-out particles'

useful for open boundaries, self-gravity

# Numerical Hydrodynamics: Consider the 1D Euler eqs

They describe the conservation of mass, momentum and energy

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u)}{\partial x} = 0 \quad (14)$$

$$\frac{\partial(\rho u)}{\partial t} + \frac{\partial(\rho u u)}{\partial x} = -\frac{\partial p}{\partial x} \quad (15)$$

$$\frac{\partial(\rho \epsilon)}{\partial t} + \frac{\partial(\rho \epsilon u)}{\partial x} = -p \frac{\partial u}{\partial x}. \quad (16)$$

$\rho$ : density

$u$ : velocity

$p$ : pressure

$\epsilon$ : internal specific energy (energy/mass)

With EOS

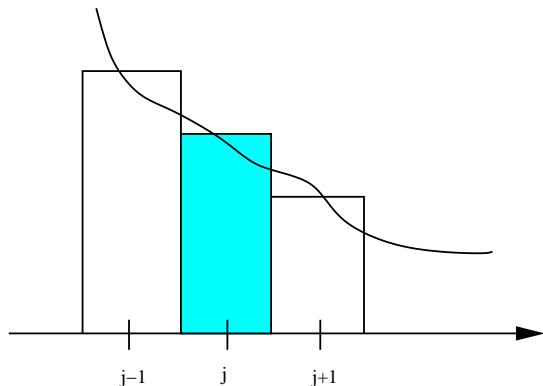
$$p = (\gamma - 1)\rho\epsilon \quad (17)$$

$\gamma$ : adiabatic exponent

**PDE in both time and space**

→ Discretisation is required for both time and space!

# Numerical Hydrodynamics: Discretisation



Consider the function:  $\psi(x, t)$   
discretise in space  
with the grid

$$\Delta x = \frac{x_{\max} - x_{\min}}{N}$$

$\psi_j^n$  denotes the value in cell center of  $\psi(x, t)$  at gridpoint  $x_j$  at time  $t^n$

$$\psi_j^n = \psi(x_j, t^n) \approx \frac{1}{\Delta x} \int_{(j-1/2)\Delta x}^{(j+1/2)\Delta x} \psi(x, n\Delta t) dx$$

$\psi_j^n$  is piecewise constant.  $j$  spatial index,  $n$  timestep.



Consider the equation

$$\frac{\partial \psi}{\partial t} = \mathcal{L}(\psi(\mathbf{x}, t)) \quad (18)$$

with the spatial differential operator  $\mathcal{L}$ .

Usual discretisation (1st order in time), at time  $t = t^n = n\Delta t$

$$\frac{\partial \psi}{\partial t} \approx \frac{\psi(t + \Delta t) - \psi(t)}{\Delta t} = \frac{\psi^{n+1} - \psi^n}{\Delta t} = L(\psi^n). \quad (19)$$

Now at the location of gridpoint  $\mathbf{x}_j$

$$\psi_j^{n+1} = \psi_j^n + \Delta t L(\psi_k^n). \quad (20)$$

$L(\psi_k^n)$ : discretised differential operator  $\mathcal{L}$  (here explicit) -  $k$  in  $L(\psi_k)$ : set of spatial indices

- e.g., for a 2nd order scheme  $k \in \{j-2, j-1, j, j+1, j+2\}$

(information from left and right of the grid point is required, 5-point stencil)

$$\frac{\partial \mathbf{A}}{\partial t} = \mathcal{L}_1(\mathbf{A}) + \mathcal{L}_2(\mathbf{A}) \quad (21)$$

$\mathcal{L}_i(\mathbf{A}), i = 1, 2$  are single differential operators acting on values  $\mathbf{A} = (\rho, \mathbf{u}, \epsilon)$ .

For ideal 1D hydro

$\mathcal{L}_1$  : advection

$\mathcal{L}_2$  : pressure, external forces

Divided into several substeps

$$\begin{aligned} \mathbf{A}^1 &= \mathbf{A}^n + \Delta t \mathcal{L}_1(\mathbf{A}^n) \\ \mathbf{A}^{n+1} = \mathbf{A}^2 &= \mathbf{A}^1 + \Delta t \mathcal{L}_2(\mathbf{A}^1) \end{aligned} \quad (22)$$

$\mathcal{L}_i$  is the differential operator to  $\mathcal{L}_i$ .

$$\begin{aligned}\frac{\partial \rho}{\partial t} &= -\frac{\partial(\rho u)}{\partial x} \\ \frac{\partial(\rho u)}{\partial t} &= -\frac{\partial(\rho u u)}{\partial x} \\ \frac{\partial(\rho \epsilon)}{\partial t} &= -\frac{\partial(\rho \epsilon u)}{\partial x}\end{aligned}$$

In conserved form

$$\frac{\partial \mathbf{u}}{\partial t} + \frac{\partial \mathbf{f}(\mathbf{u})}{\partial x} = 0 \quad (23)$$

It is for  $\mathbf{u} = (u_1, u_2, u_3)$  and  $\mathbf{f} = (f_1, f_2, f_3)$ :

$\mathbf{u} = (\rho, \rho u, \rho \epsilon)$  und  $\mathbf{f} = (\rho u, \rho u u, \rho \epsilon u)$ .

This first advection step yields:  $\rho^n \rightarrow \rho^1 = \rho^{n+1}, \quad u^n \rightarrow u^1, \quad \epsilon^n \rightarrow \epsilon^1$

Conservation of momentum

$$\frac{\partial u}{\partial t} = -\frac{1}{\rho} \frac{\partial p}{\partial x} \quad (24)$$

$$u_j^{n+1} = u_j - \Delta t \frac{1}{\bar{\rho}_j^{n+1}} \frac{(p_j - p_{j-1})}{\Delta x} \quad \text{for } j = 2, \dots, N \quad (25)$$

Conservation of energy

$$\frac{\partial \epsilon}{\partial t} = -\frac{p}{\rho} \frac{\partial u}{\partial x} \quad (26)$$

$$\epsilon_j^{n+1} = \epsilon_j - \Delta t \frac{p_j}{\bar{\rho}_j^{n+1}} \frac{(u_{j+1} - u_j)}{\Delta x} \quad \text{for } j = 1, \dots, N \quad (27)$$

on the right hand side, we use the current values for  $u$ ,  $\epsilon$  and  $p$ , which are  $u^1, p^1, \epsilon^1$ .

This step yields:  $u^1 \rightarrow u^{n+1}, \quad \epsilon^1 \rightarrow \epsilon^{n+1}$

The continuity equation reads

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u)}{\partial x} = 0, \quad (28)$$

where  $F^m = \rho u$  denotes the mass flux.

Using  $\rho \rightarrow \psi$  and a constant speed  $u \rightarrow a = \text{const.}$ , one obtains the **linear advection eq**

$$\frac{\partial \psi}{\partial t} + a \frac{\partial \psi}{\partial x} = 0. \quad (29)$$

For a constant velocity  $a$ , the solution is given by a wave moving to the right

$$\text{with } \psi(x, t = 0) = f(x) \quad \text{it is.} \quad \psi(x, t) = f(x - at)$$

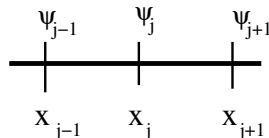
Here,  $f(x)$  denotes the initial condition at time  $t = 0$ , which gets transported by advection with constant velocity  $a$ .

# Numerical Hydrodynamics: Linear advection

FTCS: *Forward Time Centered Space* scheme

$$\frac{\partial \psi}{\partial t} + a \frac{\partial \psi}{\partial x} = 0 \quad (30)$$

with grid



we write

$$\left. \frac{\partial \psi}{\partial t} \right|_j^n = \frac{\psi_j^{n+1} - \psi_j^n}{\Delta t} \quad (31)$$

$$\left. \frac{\partial \psi}{\partial x} \right|_j^n = \frac{\psi_{j+1}^n - \psi_{j-1}^n}{2 \Delta x}, \quad (32)$$

and it follows

$$\psi_j^{n+1} = \psi_j^n - \frac{a \Delta t}{2 \Delta x} (\psi_{j+1}^n - \psi_{j-1}^n). \quad (33)$$

Seems well justified but is unstable for all time step sizes  $\Delta t$ !

# Numerical Hydrodynamics: Upwind scheme I

$$\frac{\partial \psi}{\partial t} + \frac{\partial a \psi}{\partial x} = 0 \quad (34)$$

oder

$$\frac{\partial \psi}{\partial t} + a \frac{\partial \psi}{\partial x} = 0 \quad (35)$$

$a$ : constant (velocity)  $> 0$

$\psi(x, t)$ , arbitrary transport value

Change of  $\psi$  in cell  $j$

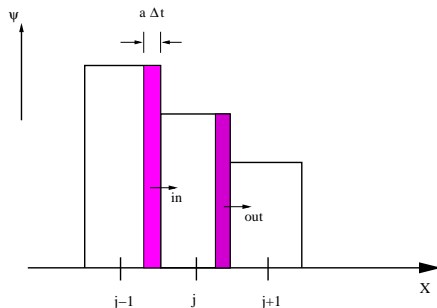
$$\psi_j^{n+1} \Delta x = \psi_j^n \Delta x + \Delta t (F_{\text{in}} - F_{\text{out}}). \quad (36)$$

The **flux**  $F_{\text{in}}$  for constant  $\psi_j$  is given by

$$F_{\text{in}} = a \psi_{j-1}^n \quad (37)$$

$$F_{\text{out}} = a \psi_j^n. \quad (38)$$

**Upwind scheme** Information comes from upstream



Pink regions are transported in neighbouring cells.

# Numerical Hydrodynamics: Upwind scheme II

Extension for non-constant states

$$F_{\text{in}} = a \psi_I \left( x_{j-1/2} - \frac{a\Delta t}{2} \right). \quad (39)$$

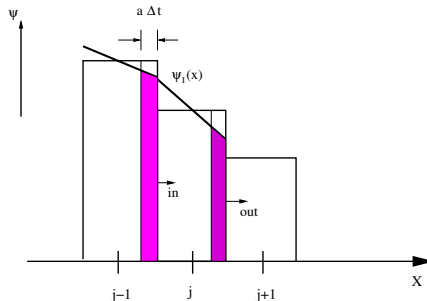
$\psi_I(x)$  polynomial of interpolation

Using linear interpolation (just a line)

$$\underbrace{F_{\text{in}} = a \left[ \underbrace{\psi_{j-1}^n}_{\text{1st order}} + \frac{1}{2}(1 - \sigma)\Delta\psi_{j-1} \right]}_{\text{2nd order}} \quad (40)$$

with  $\sigma \equiv a\Delta t/\Delta x$

$$\Delta\psi_j \approx \left. \frac{\partial\psi}{\partial x} \right|_{x_j} \Delta x$$



$$\psi_I(x) = \psi_j^n + \frac{x - x_j}{\Delta x} \Delta\psi_j \quad (41)$$

$\Delta\psi_j$  some approximation to the derivative, see next slide

**2nd order upwind**

$\psi_I(x)$  is calculated in the centers of the pink regions



# Numerical Hydrodynamics: Approximations for the derivative

Different schemes:

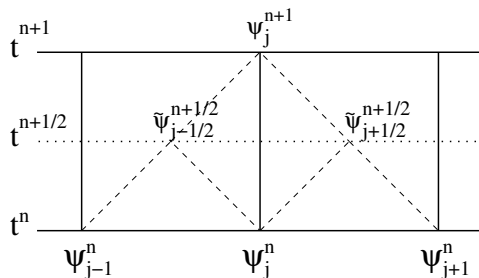
- a)  $\Delta\psi_j = 0$  upwind, 1st order, piecewise constant
- b)  $\Delta\psi_j = \frac{1}{2} (\psi_{j+1} - \psi_{j-1})$  Fromm, centred derivative
- c)  $\Delta\psi_j = \psi_j - \psi_{j-1}$  Beam-Warming, upwind derivative
- d)  $\Delta\psi_j = \psi_{j+1} - \psi_j$  Lax-Wendroff, downwind derivative

Often 2nd order upwind (van Leer scheme) **Geometric mean**  
(conserves monotonicity)

$$\Delta\psi_j = \begin{cases} 2 \frac{(\psi_{j+1} - \psi_j)(\psi_j - \psi_{j-1})}{(\psi_{j+1} - \psi_{j-1})} & \text{if } (\psi_{j+1} - \psi_j)(\psi_j - \psi_{j-1}) > 0 \\ 0 & \text{else} \end{cases} \quad (42)$$

The derivatives are calculated at the specific substep of the timestep, see below.

# Numerical Hydrodynamics: Lax-Wendroff scheme



Schematic overview for Lax-Wendroff

makes use of spatial and time centred differences

2nd order in space and time

Doing two steps:

Predictor step (at time  $t^{n+1/2}$ )

$$\tilde{\psi}_{j+1/2}^{n+1/2} = \frac{1}{2} (\psi_j^n + \psi_{j+1}^n) - \frac{\sigma}{2} (\psi_{j+1}^n - \psi_j^n). \quad (43)$$

Followed by corrector step (to time  $t^{n+1}$ )

$$\psi_j^{n+1} = \psi_j^n - \sigma \left( \tilde{\psi}_{j+1/2}^{n+1/2} - \tilde{\psi}_{j-1/2}^{n+1/2} \right). \quad (44)$$

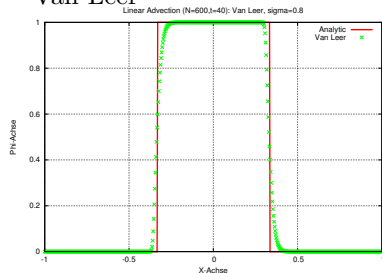
# Numerical Hydrodynamics: Example: Linear advection

$\psi(x)$

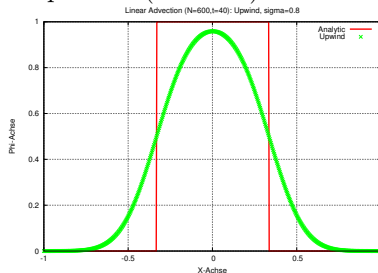
Rectangular function:  
width 0.6 in interval  $[-1, 1]$   
velocity  $a = 1$ , until  $t = 40$   
periodic boundary conditions  
 $\sigma = a\Delta t/\Delta x = 0.8$

(Courant number)

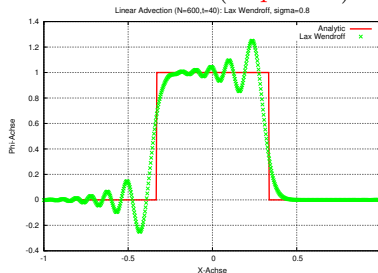
Van Leer



upwind - (diffusive)



Lax-Wendroff - (dispersive)



# Numerical Hydrodynamics: Stability analysis I

Assume a Fourier series for the solution (von Neumann 1940/50).

Consider only one term of the series and check its growth

$$\psi_j^n = V^n e^{i\theta j}, \quad (45)$$

with the definition of  $\theta$  using the grid size  $\Delta x$  and the total length  $L$

$$\theta = \frac{2\pi\Delta x}{L}. \quad (46)$$

Now, consider the upwind scheme with  $\sigma = a\Delta t/\Delta x$

$$\psi_j^{n+1} - \psi_j^n + \sigma(\psi_j^n - \psi_{j-1}^n) = 0. \quad (47)$$

Inserting (45) yields

$$V^{n+1} e^{i\theta j} = V^n e^{i\theta j} + \sigma V^n \left[ e^{i\theta(j-1)} - e^{i\theta j} \right].$$

Divide by  $V^n$  and  $e^{i\theta j}$  eventually gives

$$\frac{V^{n+1}}{V^n} = 1 + \sigma (e^{-i\theta} - 1). \quad (48)$$

The square of the absolute value finally is

$$\begin{aligned}\lambda(\theta) \equiv \left| \frac{V^{n+1}}{V^n} \right|^2 &= [1 + \sigma(e^{-i\theta} - 1)] [1 + \sigma(e^{i\theta} - 1)] \\ &= 1 + \sigma(e^{-i\theta} + e^{i\theta} - 2) - \sigma^2(e^{-i\theta} + e^{i\theta} - 2) \\ &= 1 + \sigma(1 - \sigma)(2 \cos \theta - 2) \\ &= 1 - 4\sigma(1 - \sigma) \sin^2 \left( \frac{\theta}{2} \right).\end{aligned}\tag{49}$$

The scheme is stable if the amplification factor  $\lambda(\theta)$  is smaller than one. Hence, the upwind scheme is stable for  $0 < \sigma < 1$ , because then  $\lambda < 1$ , or

$$\Delta t < f_{\text{CFL}} \frac{\Delta x}{a}\tag{50}$$

with the Courant number  $f_{\text{CFL}} < 1$ .

**Theorem:** *Courant-Friedrich-Levy* There is no explicit, consistent, stable finite difference scheme which is conditionless stable ( $\forall \Delta t$ ).

Consider the upwind scheme with  $\sigma = a\Delta t/\Delta x$

$$\psi_j^{n+1} - \psi_j^n + \sigma(\psi_j^n - \psi_{j-1}^n) = 0. \quad (51)$$

Replace differences with derivatives, (Taylor expansion up to 2nd order)

$$\frac{\partial \psi}{\partial t} \Delta t + \frac{1}{2} \frac{\partial^2 \psi}{\partial t^2} \Delta t^2 + \mathcal{O}(\Delta t^3) + \sigma \left( \frac{\partial \psi}{\partial x} \Delta x - \frac{1}{2} \frac{\partial^2 \psi}{\partial x^2} \Delta x^2 \right) + \mathcal{O}(\Delta t \Delta x^2) = 0. \quad (52)$$

Divide by  $\Delta t$ , replace  $\sigma$

$$\frac{\partial \psi}{\partial t} + a \frac{\partial \psi}{\partial x} + \frac{1}{2} \left( \frac{\partial^2 \psi}{\partial t^2} \Delta t - a \frac{\partial^2 \psi}{\partial x^2} \Delta x \right) + \mathcal{O}(\Delta t^2) + \mathcal{O}(\Delta x^2) = 0. \quad (53)$$

Use the wave equation  $\psi_{tt} = a^2 \psi_{xx}$  to obtain the modified equation (index M)

$$\frac{\partial \psi_M}{\partial t} + a \frac{\partial \psi_M}{\partial x} = \frac{1}{2} a \Delta x (1 - \sigma) \frac{\partial^2 \psi_M}{\partial x^2}. \quad (54)$$

This means, the FDE adds a diffuse term to the original PDE.

with the coefficient of diffusion

$$D = \frac{1}{2} a \Delta x (1 - \sigma). \quad (55)$$

Only for positive  $D$ , ( $D > 0$ ) this is a diffusive term, which means  $\sigma < 1$ . Hence, for the upwind scheme, we have get diffusion.

Lax-Wendroff yields

$$\frac{\partial \psi_M}{\partial t} + a \frac{\partial \psi_M}{\partial x} = \frac{\Delta t^2 a}{\sigma} (\sigma^2 - 1) \frac{\partial^3 \psi_M}{\partial x^3}. \quad (56)$$

This eq has the form

$$\psi_t + a \psi_x = \mu \psi_{xxx}, \quad (57)$$

where

$$\mu = \frac{\Delta t^2 a}{\sigma} (\sigma^2 - 1). \quad (58)$$

This causes dispersion: Waves are too slow ( $\mu < 0$ ), we get oscillations behind discontinuities.

According to the analysis on the last slides, the size of the timestep  $\Delta t$  has to be limited to obtain stable numerical evolution. In case of linear advection with speed  $a$ , it is

$$\Delta t < \frac{\Delta x}{a}. \quad (59)$$

In the more general case, the important transport speed of information is given by the sound speed ( $c_s$ ), and we obtain the **Courant-Friedrich-Lewy** condition

$$\Delta t < \frac{\Delta x}{c_s + |\mathbf{u}|}. \quad (60)$$

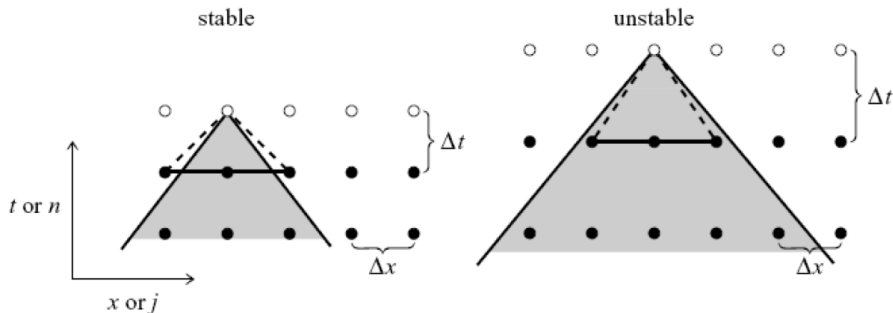
This means essentially, information is not allowed to change over the size of one grid cell during one timestep. To enforce this, one uses

$$\Delta t = f_C \frac{\Delta x}{c_s + |\mathbf{u}|}, \quad (61)$$

with the **Courant number**  $f_C < 1$ .



# Numerical Hydrodynamics: Size of time step - graphical

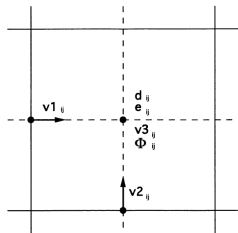


The numerical region of dependency (dashed area) has to be larger than the physical region of dependency (gray area):  $\Delta x / \Delta t > \alpha$ .

The total information of the sound cone has to be considered.

# Numerical Hydrodynamics: Multi-dimensional

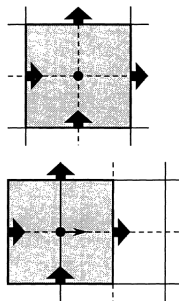
grid definitions (in 2D, **staggered**):  
scalars in cell centre  
(here:  $\rho, \epsilon, p, v_3, \psi$ )  
vectors at interfaces  
(here:  $v_1, v_2$ )



Fluxes through cell interfaces:

top: mass flux

bottom: x-momentum (grid moved!)



taken from ZEUS-2D: A radiation magnetohydrodynamics code for astrophysical flows in two space dimensions. I in The Astrophysical Journal Suppl., von Jim Stone und Mike Norman, 1992.

Use **operator splitting und directional splitting**:  $x$  and  $y$  directions are treated one after other. First  $x$ -scans, then  $y$ -scans.

# Numerical Hydrodynamics: Summary

Numerical schemes should reflect conservation properties.

- Write down the eqs in conserved form.

Numerical schemes should reflect wave properties.

- shock-capturing schemes, Riemann solver

Numerical schemes have to be able to treat discontinuities

- diffusion ( $\Rightarrow$  stability), either explicitly (artificial viscosity) or implicitly (by construction of scheme)

Free codes on the web:

ZEUS: <http://www.astro.princeton.edu/~jstone/zeus.html>  
classical upwind code, 2nd order, staggered grid, RMHD

ATHENA: <https://trac.princeton.edu/Athena/>  
ZEUS successor: Riemann solver, centred grid, MHD

NIRVANA: <http://nirvana-code.aip.de/>  
3D, AMR, Finite Volume code, MHD

PLUTO: <http://plutocode.ph.unito.it/>  
3D, relativistic, Riemann solver/Finite Volume, MHD

GADGET: <http://www.mpa-garching.mpg.de/galform/gadget/>  
SPH-Code, tree code, self-gravity

Consider the 1D equation (motion in  $x$ -direction):

Using Euler eqs with EOS  $p = (\gamma - 1)\rho\epsilon$ , we obtain

$$\left. \begin{aligned} \frac{\partial \rho}{\partial t} + \frac{\partial(\rho u)}{\partial x} &= 0 \\ \frac{\partial(\rho u)}{\partial t} + \frac{\partial(\rho u u)}{\partial x} &= -\frac{\partial p}{\partial x} \\ \frac{\partial(\rho \epsilon)}{\partial t} + \frac{\partial(\rho \epsilon u)}{\partial x} &= -p \frac{\partial u}{\partial x} \end{aligned} \right\} \Rightarrow \begin{aligned} \frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + \rho \frac{\partial u}{\partial x} &= 0 \\ \frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + \frac{1}{\rho} \frac{\partial p}{\partial x} &= 0 \\ \frac{\partial p}{\partial t} + u \frac{\partial p}{\partial x} + \gamma p \frac{\partial u}{\partial x} &= 0 \end{aligned},$$

or written in vectorial form

$$\frac{\partial \mathbf{W}}{\partial t} + \mathbf{A} \frac{\partial \mathbf{W}}{\partial x} = 0, \quad (62)$$

with

$$\mathbf{W} = \begin{pmatrix} \rho \\ u \\ p \end{pmatrix} \quad \text{und} \quad \mathbf{A} = \begin{pmatrix} u & \rho & 0 \\ 0 & u & 1/\rho \\ 0 & \gamma p & u \end{pmatrix} \quad (63)$$

The eqs are nonlinear and coupled!

De-coupling by diagonalisation of  $\mathbf{A}$ .

# Hydrodynamics: Diagonalisation

Eigenvalues (EV)

$$\begin{aligned}\det(\mathbf{A}) &= \begin{vmatrix} u - \lambda & \rho & 0 \\ 0 & u - \lambda & 1/\rho \\ 0 & \gamma p & u - \lambda \end{vmatrix} = (u - \lambda) \begin{vmatrix} u - \lambda & 1/\rho \\ \gamma p & u - \lambda \end{vmatrix} \\ &= (u - \lambda) [(u - \lambda)^2 - \gamma p / \rho] = 0.\end{aligned}\tag{64}$$

We get

$$\begin{aligned}\lambda_0 &= u \\ \lambda_{\pm} &= u \pm c_s\end{aligned}\tag{65}$$

with **sound speed**

$$c_s^2 = \frac{\gamma p}{\rho}.\tag{66}$$

The EVs provide characteristic velocities, which are the speeds of information transport. It is combined from fluid- ( $u$ ) and sound speed ( $c_s$ ). Three real EVs which are the components of the diagonalised matrix

$$\mathbf{Q}^{-1} \mathbf{A} \mathbf{Q} = \Lambda\tag{67}$$

$\mathbf{Q}$  is given by the eigenvectors to the EVs ( $\lambda_i$ ,  $i = 0, +, -$ ) and  $\Lambda$  a diagonal matrix.

# Hydrodynamics: Charakteristic variables

$\mathbf{Q}$  can be calculated as

$$\mathbf{Q} = \begin{pmatrix} 1 & \frac{1}{2} \frac{\rho}{c_s} & -\frac{1}{2} \frac{\rho}{c_s} \\ 0 & \frac{1}{2} & \frac{1}{2} \\ 0 & \frac{1}{2} \rho c_s & -\frac{1}{2} \rho c_s \end{pmatrix} \quad \text{and} \quad \mathbf{Q}^{-1} = \begin{pmatrix} 1 & 0 & -\frac{1}{c_s^2} \\ 0 & 1 & \frac{1}{\rho c_s} \\ 0 & 1 & -\frac{1}{\rho c_s} \end{pmatrix}.$$

Now, consider the vector equation

$$\frac{\partial \mathbf{W}}{\partial t} + \mathbf{A} \frac{\partial \mathbf{W}}{\partial x} = 0 \quad (68)$$

and

$$\mathbf{Q}^{-1} \mathbf{A} \mathbf{Q} = \Lambda.$$

Define:

$$d\mathbf{v} \equiv \mathbf{Q}^{-1} d\mathbf{W} \quad \text{and hence} \quad d\mathbf{W} = \mathbf{Q} d\mathbf{v} \quad (69)$$

Multiply eq. (68) with  $\mathbf{Q}^{-1}$

$$\frac{\partial \mathbf{v}}{\partial t} + \Lambda \frac{\partial \mathbf{v}}{\partial x} = 0. \quad (70)$$

$\mathbf{v} = (v_0, v_+, v_-)$  are **characteristic variables**:  $v_i = \text{const.}$  on the curves

$$\frac{dx}{dt} = \lambda_i$$

# Hydrodynamics: What is variable $v_0$ ?

From the definition

$$dv_0 = d\rho - \frac{1}{c_s^2} dp \quad (71)$$

$$\frac{\partial v_0}{\partial t} + \lambda_0 \frac{\partial v_0}{\partial x} = 0 \quad \text{with} \quad \lambda_0 = u \quad (72)$$

What is  $dv_0$ ?

From thermodynamics (First law for specific quantities):

$$T ds = d\epsilon + p d\left(\frac{1}{\rho}\right) = d\epsilon - \frac{p}{\rho^2} d\left(\frac{1}{\rho}\right), \quad (73)$$

with  $p = (\gamma - 1)\rho\epsilon$ ,  $\epsilon = c_v T$ ,  $\gamma = c_p/c_v$  one obtains

$$ds = -\frac{c_p}{\rho} \left[ d\rho - \frac{dp}{c_s^2} \right] = -\frac{c_p}{\rho} dv_0 \quad (74)$$

$$\implies \frac{\partial s}{\partial t} + u \frac{\partial s}{\partial x} = 0, \quad (75)$$

which means **s is const. along streamlines**, or

$$\frac{ds}{dt} = 0. \quad (76)$$

For the other characteristic variables, it is

$$\frac{\partial v_{\pm}}{\partial t} + (u \pm c_s) \frac{\partial v_{\pm}}{\partial x} = 0, \quad (77)$$

with

$$dv_{\pm} = du \pm \frac{1}{\rho c_s} dp, \quad (78)$$

it follows

$$v_{\pm} = u \pm \int \frac{dp}{\rho c_s}. \quad (79)$$

Assume constant entropy everywhere (i.e.,  $p = K\rho^{\gamma}$ )

$$\implies v_{\pm} = u \pm \frac{2c_s}{\gamma - 1}. \quad (80)$$

**Riemann invariants:**  $v_{\pm} = \text{const.}$  along curves

$$\frac{dx}{dt} = u \pm c_s.$$



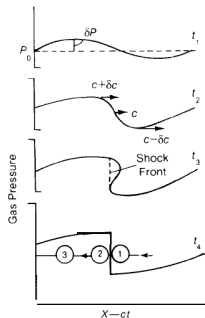
# Hydrodynamic: Steepening of sound waves

Linearisation of the Euler eqs yields wave equation for a perturbation

Example for receding shockwave

$$\frac{\partial^2 \rho_1}{\partial t^2} = c_s^2 \frac{\partial^2 \rho_1}{\partial x^2} \quad (81)$$

however!:  $c_s$  is not constant  $\Rightarrow$  steepening



$\Rightarrow$  discontinuities

$\equiv$  Jump: sub-supersonic

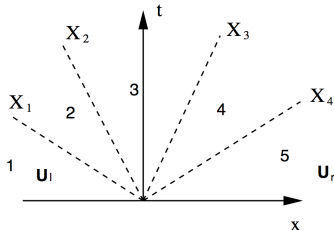
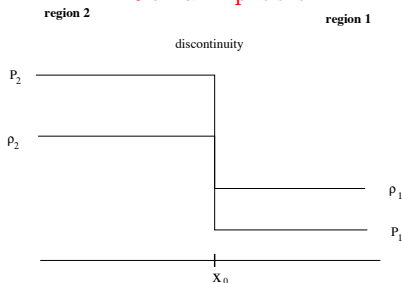


Copyright, 1968,  
by Gabriele Wauer

# Examples: Shocktube

Discontinuity in the initial data in a tube at location  $x_0$ , (1D)

## Riemann problem

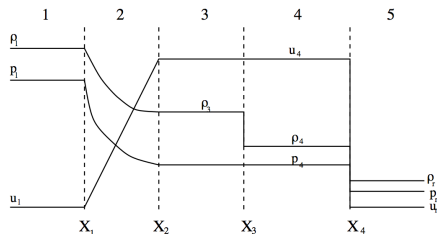


pressure ( $p$ ) and density ( $\rho$ ) jump, we obtain - a shock to the right ( $X_4$ )

(supersonic  $u_{sh} > c_s$ )

- a contact discontinuity density jump (along  $X_3$ )

- a rarefaction wave (between  $X_1$  and  $X_2$ )



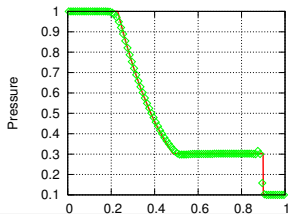
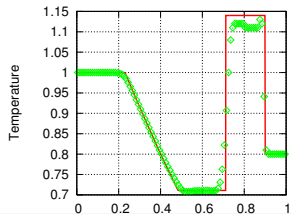
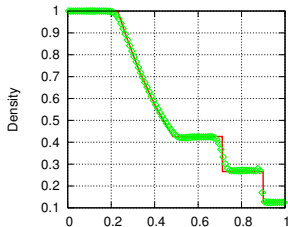
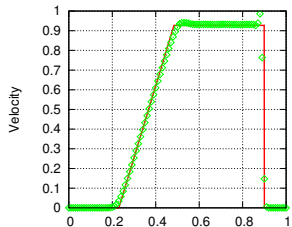
## Examples: Sod shocktube

Standard testproblem for numerical hydrodynamis,  $x \in [0, 1]$  with  $X_0 = 0.5$ ,  $\gamma = 1.4$

$\rho_1 = 1.0, p_1 = 1.0, \epsilon_1 = 2.5, T_1 = 1$ , and  $\rho_2 = 0.1, p_2 = 0.125, \epsilon_2 = 2.0, T_2 = 0.8$

Solution using van Leer scheme at  $t = 0.228$

Shock-Tube: Sod; Mono: Geometric Mean; Nx=100, Nt=228, dt=0.001



red: exact  
green:  
numerical

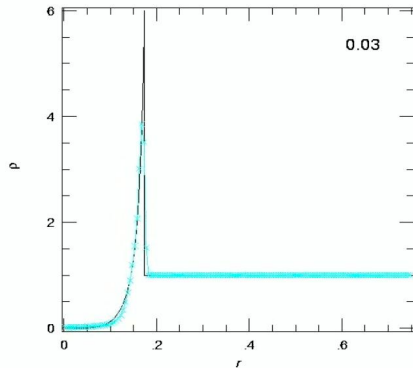
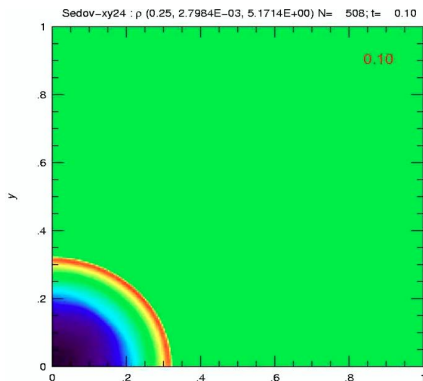
## Examples: Sedov explosion

A model for exploding bombs (Sedov & Taylor, 1950er), analytical solution by Sedov

Standard test problem for  $i$  1D, for  $x, y \in [0, 1] \times [0, 1]$

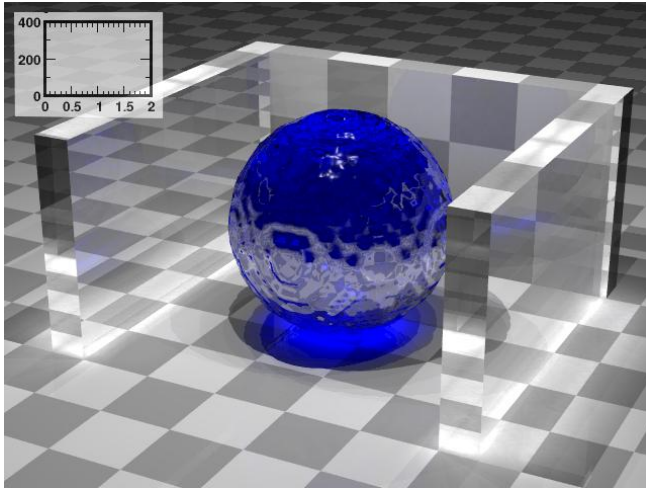
Energy deposit at origin,  $E = 1$ , in  $\rho = 1$ ,  $\gamma = 1.4$ ,  $200 \times 200$  grid points

Solution using van Leer scheme, plotted quantity is density



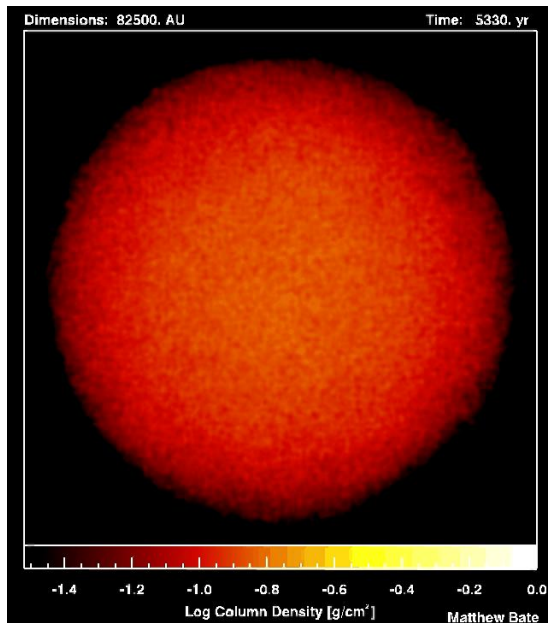
## Examples: Liquid drop: SPH

Sphere of water ( $R=30\text{cm}$ ), basin ( $1\times 1\text{ m}$ ,  $60\text{cm}$  height) including surface tension, time in seconds (TU-München, 2002)



(url)

# Examples: Stellar formation: SPH



molecular cloud

mass:

$50 M_{\odot}$

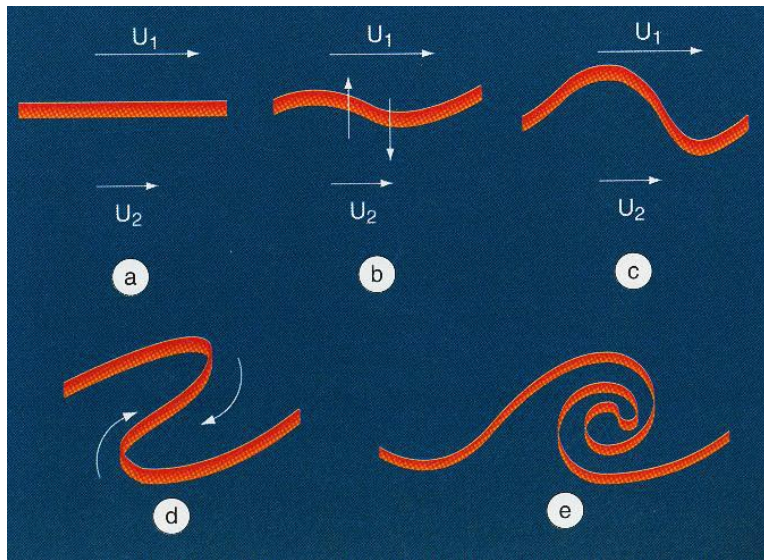
diameter:

$1.2 \text{ ly} = 76,000 \text{ au}$

temperature:

10 K (M. Bate, 2002)

## Examples: Kelvin-Helmholtz instability



KHI is a shear instability: jump in tangential component leads to instability

## Examples: KHI in atmosphere



(Boulder (NCAR), USA)

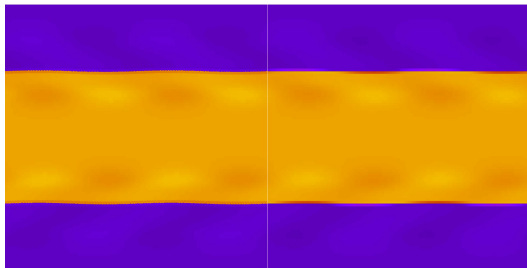


# Examples: KHI: Simulation

direct comparison: moving vs. fixed grid

left: moving grid (Voronoi tessellation)

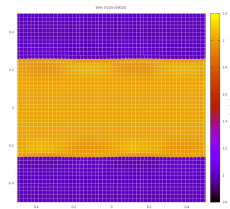
right: fixed squared grid (Euler)



(Kevin Schaal, Tübingen)

Youtube channel

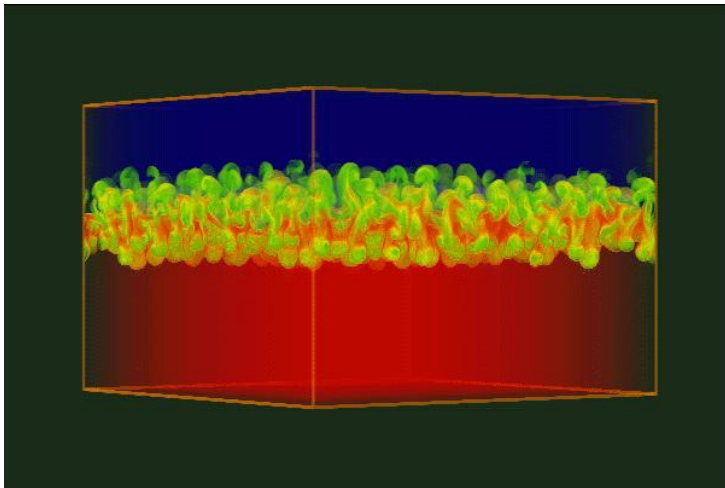
with moving grid



## Examples: Rayleigh-Taylor instability

PPM Code, 128 Knoten, ASCI Blue-Pacific ID System at LLNL

$512^3$  grid points (LLNL, 1999)



(web)