Vupiter DC Power Supply

Date: October 30, 2020

Senior Design Project Proposal

Team Members:

Chase Flatau
Alex Jones
Rice Shelley
Al Spies



Auburn University

Department of Electrical and Computer Engineering

Contents

1	Pro	Project Description						
2	Technical Description							
	2.1	Constraints						
		2.1.1	Economical	2				
		2.1.2	Environmental	2				
		2.1.3	Manufacturability	3				
		2.1.4	Health and Safety	3				
		2.1.5	Usefulness	3				
	2.2	Standa	ards	3				
		2.2.1	UL 1310 Class 2 Power Units Standard for Safety	3				
		2.2.2	Universal Serial Bus Version 2.0	4				
		2.2.3	USB Test and Measurement Class Specification	4				
		2.2.4	Standard Commands for Programmable Instruments (SCPI)	4				
	2.3	Power	Stages	4				
		2.3.1	Topology 1 - Linear mode devices only	4				
		2.3.2	Topology 2 - Switch mode devices only	5				
		2.3.3	Topologies 3 and 4 - Mixed mode supplies	6				
	2.4	Micro-	-Controller	7				
	2.5	User I	interface	7				
3	Maı	Ianagement Approach						
4	Buc	$egin{align*} \mathbf{Budget} \ \mathbf{Sudget} \ $						
5	Timeline 1							
6	Faci	ilities		10				
7	Dis	positio	on Agreement	10				

1 Project Description

DC power supplies are easily one of the most important pieces of test equipment in a lab while simultaneously being the most basic in concept. The focus of the Vupiter project will be to create a low-cost open-source versatile benchtop power supply. To make Vupiter versatile we will provide a computer interface that will allow power users to automate testing and data collection, in addition to the typical front-panel control. This computer interface will allow Vupiter to be useful in a much larger domain of experimentation than could be explored with it. Community expansion on this computer interface and the design as a whole will be enabled through thorough documentation at every stage. We will be documenting not just the technical details but also the decision making process along the way meaning Vupiter will be able to serve simultaneously as a useful lab tool and as a teaching tool. This level of documentation is the critical element frequently missing from most open source hardware projects, even other open source supplies, that prevents them from becoming truly community projects.

2 Technical Description

The design of the Vupiter lab power supply takes in to consideration usability, safety, and economic feasibility. The Vupiter lab power supply will offer three independent channels controllable with a physical front panel. In addition to the physical control panel PC control will also be provide facilitated by a USB interface. The affordability of the design is addressed via choosing cheap yet powerful micro-controllers and designing a front panel that is usable yet economical.

2.1 Constraints

2.1.1 Economical

The primary purpose of a Vupiter power supply is to make desktop experimentation for hobbyist versatile, convenient, and low cost without sacrificing precision. Devices with comparable function and control resolution that are currently in the market range from \$300 to \$700. The economical constraint for this project is keeping build cost less than \$100 dollars to provide an affordable option for all electronic enthusiast, regardless of budgets. This difference in cost will be recouped by not having make a profit or pay staff to support users.

2.1.2 Environmental

Vupiter is intended for standard lab usage use so there's a strict ban on toxic materials with all components. Toxic materials are an environmental concern due to the possibility of these materials being discarded and also the environmental effects of the

components creation, so special attention will be paid in the component selection process so that we only consider safe options.

Energy efficiency is also a major topic of concern globally so the design process will have to adhere to reasonable levels of efficiency. This is accomplished via switch-mode supplies that are followed by linear stages so that we can meet both the performance and efficiency requirements.

2.1.3 Manufacturability

In order to ensure that hobbyists and factories can both product the design, we will be constraining or PCB 2-layers with only one side populated by surface mount components. By avoiding through-hole components and only populating one side of the board we can drastically simplify automated PCB assembly. To further assist hobbyists we will be limiting our passive component size to 0603 or above, and banning the use of ball grid arrays or other difficult to hand solder IC packages in favor of packages with exposed leads such as quad flat packs.

2.1.4 Health and Safety

Well-being of users, or anyone in close proximity, is the highest priority of the design process and creates constraints for the device. Constraints include a fuse in the first stage of the power supply, opto-isolation of the front panel, no sharp edges, and an ergonomic user interface to maximize comfort under standard usage.

2.1.5 Usefulness

From our team's experience using power supplies we have identified a number of minimum performance targets that are necessary to keep Vupiter useful in a lab setting while still maintaining simplicity of design. The target will be three independently isolated channels capable of 0-30V and 0-5A regulation at 10mV and 10mA resolution. Physically, the supply should sit flat on a level surface, and have a flat top, to allow for stacking of other instruments.

2.2 Standards

2.2.1 UL 1310 Class 2 Power Units Standard for Safety

The UL 1310 standard outlines and classifies power supplies. A class two power supply cannot exceed an output of 30 Volts and 8 Amperes. The Vupiter lab supply would be considered a class two power supply under the UL 1310 standard. UL 1310 covers both indoor and outdoor power supplies however the primary environment for the Vupiter lab supply is intended to be indoors. This class of power supply is intended primarily to provide power to low voltage electrical devices.

2.2.2 Universal Serial Bus Version 2.0

The Vupiter power supply can be interfaced with a PC over the USB 2.0 protocol. Data transmission will be at a rate of 12 Mb/s. The Vupiter power supply will be a slave device and have a USB type B port located on the front panel. Compliance with the standard is assured by the microcontroller vendor.

2.2.3 USB Test and Measurement Class Specification

USBTMC will be used on top of the USB 2.0 protocol for communication with the power supply. USBTMC will be a support medium for the SCPI command interface. The interface will provide plug and play communication at a lower cost when compared to other common lab equipment interfaces.

2.2.4 Standard Commands for Programmable Instruments (SCPI)

SCPI is used to define the commands for controlling programmable test and measurement devices. The Vupiter power supply will use SCPI as the top level command interface between itself and PC desktop software. The SCPI functionality class DCP-SUPPLY will be implemented into the design. The DCPSUPPLY class will ensure that other SCPI DC power supply control software can be used with the Vupiter power supply.

2.3 Power Stages

Benchtop power supplies are frequently attached to sensitive and poorly characterized devices meaning that the supply is subject to more rigorous and varied performance requirements than a typical specialized supply. These performance requirements can be roughly broken down into output noise and output step response requirements. These two criteria will be considered in addition to our budgetary and environmental requirements when evaluating designs. Four topologies for the power supply section of this project are explored and explained below, addressing these criteria. The final tallying of their pros and cons can be seen in Table 1.

2.3.1 Topology 1 - Linear mode devices only

This topology is by far the simplest as all it does is transform and rectify mains voltage, and then burn any excess voltage as heat in order to control the final output voltages. This results in a very high quality output, as there are no elements injecting noise and the entire voltage range is available for step response. Those benefits are exactly its downfall sadly, as the requirement on the transformer for it to work at 60 Hz requires that cycle by cycle it must be able to store a large amount of energy in the H-field. This implies a physically large design, as the more energy that needs to be stored, the greater the amount of ferrous core needed. Not only does this make for bulky and heavy

transformers, but it also greatly increases the cost. Aside from this, the linear element also has issues, shown in the diagram in red. As we cannot adjust the output of the rectifier, that linear element has to turn all the excess voltage into heat. This means that the power supply running at a low voltage output but drawing high amperage would need to dissipate nearly 200 Watts would undoubtedly require heat sinking and active cooling, also driving up the price and weight of the power supply.

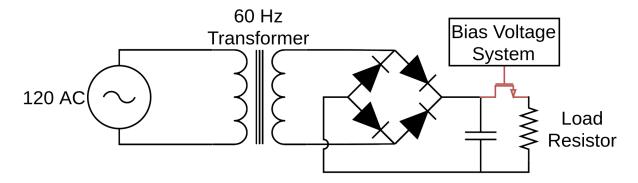


Figure 1: Entirely linear mode design

2.3.2 Topology 2 - Switch mode devices only

To address the issues with linear regulation, let's examine a purely switch mode regulator. As can be seen in Figure 2, line voltage is immediately rectified. This gives us an approximately 300V DC supply. From that 300V supply, we switch it at high frequency through a transformer. Due to this ability to increase the frequency, we can decrease the size and price of the transformer drastically. From the output we have to rectify again, and then we go on to our final regulation stage which is a buck converter. This buck converter is able to control the output voltage at high efficiency, but due to its requirement for high output capacitance, current limiting and voltage recovery speed suffer. Even worse, the buck converter both fails to filter noise from the first switched converter stage, and also injects noise at its switching frequency. This noise, and the poor current limiting results in a low quality output that would make this power supply useless in a large number of applications. That being said, this design has a low cost and extremely high efficiency, as no part of it is dissipating power intentionally, allowing it to reduce the size of some parts and completely eliminating other items such as heat sinks and fans.

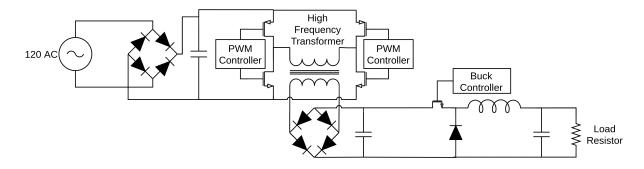


Figure 2: Entirely switch mode design

2.3.3 Topologies 3 and 4 - Mixed mode supplies

These two topologies are together as they share a single concept and block diagram, but there are major differences in their feedback loops and how they respond. As can be seen in Figure 3, these topologies are composed of different pieces from topologies one and two, earning them their name as mixed mode rather than linear or switch exclusively. These two are using the high frequency transformer stage from the switch mode design, followed by a linear regulator on the output. This allows us to eliminate the high cost 60 Hz transformer while still maintaining the benefits of linear regulation. The switch mode elements here still inject noise, but as they are followed by a linear stage, that noise can be filtered both by passive elements and by the linear elements, ensuring a high quality output regulation.

The first of our two topologies in this domain is a fixed mixed mode design. This means that the voltage output of the second rectifier is controlled to a fixed value, I.E. if the desired voltage is 20V, the transformer will target 25V and allow the additional 5V to be dissipated in the linear stage. The benefit here is higher efficiency than the linear only design as we can decrease the supply voltage at low output voltages while still maintaining strong regulation.

The alternative to this is a floating mixed mode design whereby the output of the second rectifier is regulated to always be just slightly above the dropout of the linear stage. This ensures exceptionally high efficiency as the linear element is dissipating at most 10 Watts even with a short circuit across its output. Where this is problematic is when reacting to large step inputs both on the load or the command side, as the maximum positive output voltage slew is dictated by the switched elements rather than the linear elements which can react almost instantly. Another point off for this design is the difficulty of designing a floating switch mode section. This can drastically complicate feedback loops and if done improperly will result in an unstable output. Due to this, floating output voltages are infrequent, driving up the cost to design one as controller IC choice is limited.

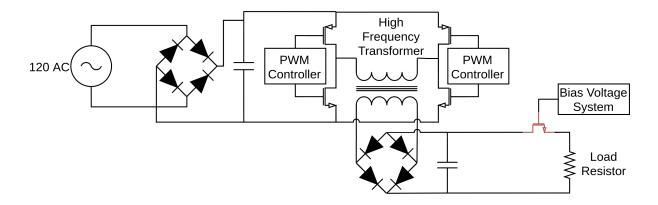


Figure 3: Mixed modality design

				Options	
Criteria Weight		Linear	SMPS	Fixed Mixed	Floating Mixed
Efficiency	1		0		-
Cost	2		0	-	
Noise	2	++	0	+	+
Step Response	2	++	0	++	+
Design Effort	1	+	0	-	
+	9	0	6	4	
0	0	5	0	0	
-	9	0	4	7	
Net Sco	0	0	2	-3	

Table 1: Pugh table for power stage topology selection

2.4 Micro-Controller

Price and USB support were the biggest concern when considering a MCU for the project. Four Candidates were considered, and the results are explained below with a summary in Table 2. The Raspberry PI was not a strong candidate due to its price and lack of ADC/DAC hardware. The STM32's tool chain lacks linux support and is not especially intuitive. ATmega 2560 lacks USB support which will be important for the communication between power supply to PC. The ATmega Samd51 has decent tools and all the required hardware at a good price point. In addition to the above mentioned benefits the Samd51 does not require many external components making PCB design simpler. A development board has been selected for the Samd so that software development may begin before the PCB is designed.

		Options			
Criteria Weight		ATMega Samd51	ATMega 2560	Raspberry Pi	STM32
ADC and DAC 3		+	0	-	+
Price 5		+	0	-	+
USB support 5		+	0	+	+
Tools	2	0	0	+	+
Libraries	1	-	0	+	-
+		13	0	8	13
0		1	5	0	0
_		1	0	8	3
Net Sco	re	12	0	0	10

Table 2: Pugh table for micro-controller selection

2.5 User Interface

The user interface can be broken into two subsections, the information display and the controls. The main criteria for these two subsections are cost, implementation, and

versatility of function in design. For the display, three options were considered: seven segment displays, a TFT screen, and a touchscreen. The touchscreen simplifies our component count by unifying the display and the interface, but it lacks tactile feedback ruining the user experience, and even worse is rather expensive. Seven-segment displays are a classic and robust solution but the shear quantity required to display three channels would be two expensive and have a cluttered display. The intermediary solution of a non-touchscreen with a discrete interface fixes these issues and is relatively inexpensive. These results are summarized in Table 3

			${f Options}$	
Criteria	Weight	LTC-4627JR 4 Digit Seven Segment Display	Hx8357B TFT Screen	Mikroe-495 touchscreen display
Price	3	0	+	-
Usability	2	-	0	+
Quality	1	-	0	+
Durability	1 1	+	0	-
Implementation	2	+	0	-
+		3	3	3
0		1	4	0
-		3	0	-6
Net Sco	re	0	3	-3

Table 3: Pugh table for display selection

For the user interface, once again three options of encoder, matrix button array, and the touchscreen were considered against the same criteria. The touchscreen has the same issues as above of being expensive and lacking tactile feedback. A keypad, while robust and relatively cheap, would make fine adjustments difficult and menu navigation unintuitive. This leaves us with encoders, which allow for fine adjustment, provide tactile feedback, and are relatively cheap. Intuitive menu navigation can be achieved by having three encoders, two dedicated to voltage and current control with the third managing the switching between channels and any other menu options. These results are summarized in Table 4

			Options	
Criteria	Weight	4x3 Matrix Keypad	Encoders	Mikroe-495 touchscreen display
Price	3	-	+	-
Usability	2	-	+	0
Quality	1	-	+	-
Durability	1 1	0	+	-
Implementation	2	0	+	-
+		0	9	0
0		2	0	1
_		-6	0	-7
Net Scor	re	-6	9	-7

Table 4: Pugh table for user interface selection

3 Management Approach

Our team holds weekly meetings on Wednesday morning at 9 AM to discuss progress and work on team tasks. These meeting are done on our discord server which is also how we communicate outside of meetings. Documentation and version control is done through GitHub. The team is roughly split into two groups with Alex Jones and Chase Flatau working on power stages while Rice Shelley and Al Spies work on firmware. Each team communicates within separate channels for internal communication, and any major decisions or issues are run by the entire team at the weekly meetings. The overall project lead is Alex Jones.

Meeting minutes are recorded weekly by Al Spies and can be accessed on our website: https://ams0187.github.io/Vupiter/

All files, including this proposal are hosted on our github:

https://github.com/ams0187/Vupiter

4 Budget

In order to be competitive with market alternatives, our target cost is \$100. Each member will donate \$25 to purchase the necessary materials. The finished product will be assembled in each members' private workspace; therefore, consumables such as solder will count as donations but will still be counted into the final price. The current targets for each subsection are: \$25 are for front panel display and button/knobs, \$50 for the power stages and PCBs, and \$25 for the casing of the supply.

5 Timeline

The project timeline can be accessed here: https://aub.ie/vupiterTL

6 Facilities

The facilities that will be utilized are Auburn's SPaRC Lab and individual members' home workshops. In the event that these labs are insufficient, the ECE shop will be contacted for assistance

7 Disposition Agreement

All members agree that the final physical product will donated to SPaRC and that all documentation, code, and intellectual property will be released on GitHub under the MIT licence. By signing on the next page each member acknowledges and agrees to the above statements.

Name	Signature
Chase Flatau	
Alex Jones	
Rice Shelley	
Al Spies	