

# HBI User's guide

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## 1 Introduction

Fortran90 software HBI performs 3-dimensional quasi-dynamic numerical simulations of sequences of earthquakes and aseismic slip (SEAS). It can handle arbitrary geometry such as branches, step-overs, and rough faults in an elastic half-space. 2D problems can also be done in the same code. The computation is accelerated by taking advantage of Lattice Hierarchical matrices. HACApK, open-source software for H-matrices, is called for constructing and operating H-matrices.

The latest versions can be found at <https://github.com/sozawa94/hbi>. Please feel free to contact So Ozawa ([sozawa@eps.s.u-tokyo.ac.jp](mailto:sozawa@eps.s.u-tokyo.ac.jp)), if you have any questions.

## 2 License

This software is freely available under the MIT license. If you write a paper using this code, please cite the following manuscript.

So Ozawa, Akihiro Ida, Tetsuya Hoshino, Ryosuke Ando, "Large-scale earthquake sequence simulations of 3D geometrically complex faults using the boundary element method accelerated by lattice H-matrices on distributed memory computer systems", arXiv:2110.12165

## 3 How to run

Download the source codes from github. Type:

```
git clone http://github.com/sozawa94/hbi
```

To compile and link the code, type

```
make
```

You may need to modify `Makefile` depending on your environment.

To run a simulation, type:

```
./lhbiem (inputfile)
```

or use MPI parallelization

```
mpirun -np 16 ./lhbiem (inputfile)
```

Some examples of input files are included in the directory. Or, run the code in parallel. **The number of MPI processes must be a squared number.**

As an example, `examples/bp5t.in` and corresponding geometry and parameter files are included. This problem setting is a triangular element version of BP5 (vertical strike-slip fault) in the SEAS project (<https://strike.scec.org/cvws/seas/>). Other input files are also available.

The standard output first shows the information about (lattice) H-matrices (approximated integration kernel). Then, time-step and time (measured by year) are recorded. Other output files are mentioned later.

## 4 Problem setting

### 4.1 Description of Input file

Different simulations can be performed by modifying the input file, instead of modifying the source code. The input variable list is:

name	type	meaning
jobnumber	integer	job number (name of output files)
problem	character	dimension, planar or nonplanar, mesh etc...
ncellg	integer	number of elements
nstep	integer	maximum number of time steps
interval	integer	output & checkpointing every this time steps
dtinit	real	initial time step width
geometry_file	character	name of geometry file
parameter_file	character	name of parameter file
parameterfromfile	logical	true if parameters are read from parameter_file
restart	logical	true if restarting a suspended job
backslip	logical	true if loading is added by backflip
vpl	real	the velocity of backslip (m/s) (used if backflip=T)
sr	real	the stressing rate (MPa/s) (used if backslip=F)
tmax	real	maximum time (s)
sigmaconst	logical	true if normal stress is kept constant
ds	real	element size (km) (used in 2dp, 3dp, 3dhr)
imax	integer	the number of elements in slip-parallel direction (used in 3dp)
jmax	integer	the number of elements in slip-perpendicular direction (used in 3dp)
crake	real	rake angle (deg) in 3D problems (not used if parameterfromfile=T)
a	real	a in RSF (not used if parameterfromfile=T)
b	real	b in RSF (not used if parameterfromfile=T)
dc	real	dc in RSF (not used if parameterfromfile=T)
f0	real	f0 in RSF (not used if parameterfromfile=T)
tauinit	real	initial shear stress (MPa) (not used if parameterfromfile=T)
sigmainit	real	initial normal stress (MPa) (not used if parameterfromfile=T)
velinit	real	initial slip rate (m/s) (not used if parameterfromfile=T)
eps_h	real	error allowance in H matrix (default: 1e-4)
eps_r	real	error allowance in Runge-Kutta (default: 1e-4)
velmax	real	computation stop if maximum velocity is above this value (default:1e7)
velmin	real	computation stop if maximum velocity is below this value (default:1e-16)
limitsigma	logical	true if you want to limit normal stress
maxsig	real	maximum normal stress (MPa) (used if limitsigma=T)
minsig	real	minimum normal stress (MPa)(used if limitsigma=T)

### 4.2 Problem

The list of problems are follows:

problem	description
2dp	2D planar fault in full-space(plane strain)
2dn	2D nonplanar fault in full-space(plane strain)
3dp	3D planar squared elements in full-space
3dph	3D planar squared elements in half-space
3dnt	3D nonplanar triangular elements in full-space
3dhr	3D nonplanar rectangular elements in half-space
3dht	3D nonplanar triangular elements in half-space

**3dhr** have some limitations due to the use of Okada's code, in which the two parallel sides must be horizontal and the length of the sides must be uniform over all elements.

### 4.3 Physical variables and constants

The following units are assumed:

quantity	unit
time	s
location	km
displacement	m
slip velocity	m/s
wave speed	km/s
shear modulus	GPa
stress	MPa

Fundamental physical constants are set in `m_const.f90`. The default values are

quantity	value
rigidity	32.04GPa
P-wave speed	6.000 km/s
S-wave speed	3.464 km/s
reference slip rate on RSF	1 $\mu$ m/s

### 4.4 Fault geometry

In the case of 2dp and 3dp, a fault geometry is characterized uniquely by its element size **ds** and the number of elements **ncellg** or (**imax**, **jmax**). These are specified in the input file. For 3dph, it is assumed that the fault cuts the free surface. Thus, the geometry is characterized by (**imax**(along-strike), **jmax**(along-dip), **ds**, **dipangle**). See also Figure 1. Note: **ds** should be small enough to resolve the process zone; otherwise, slip rate oscillation would occur.

For other problems, an additional **geometry\_file** is necessary.

#### 4.4.1 2dn

The coordinates of two edges of a straight line have the geometrical information of an element. **xel<xer** is necessary. **geomerty\_file** has the following format:

```
xel(1) xer(1) yel(1) yer(1)
xel(2) xer(2) yel(2) yer(2)
...
```

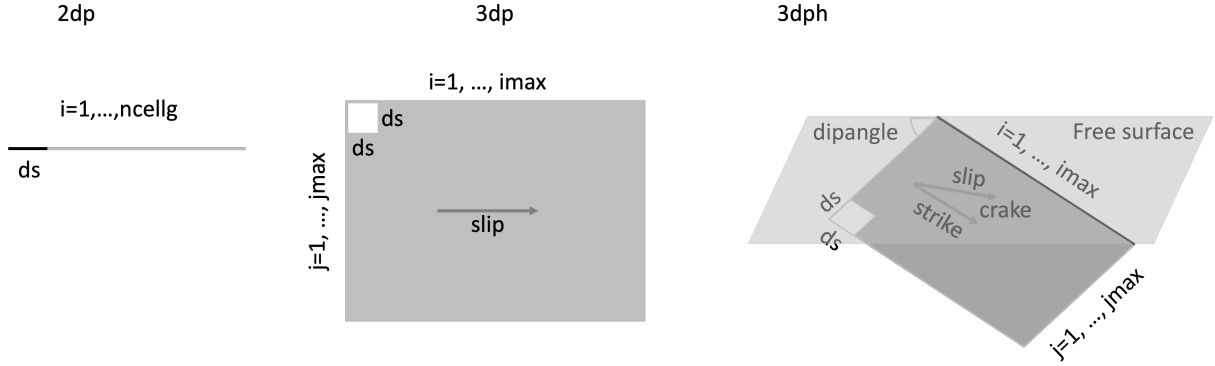


Figure 1: Fault geometry

#### 4.4.2 3d triangular mesh

The coordinates of three edges of a triangle has the geometrical information of an element. `geometry_file` should have STL (ASCII) format:

```
facet normal normal_vector(1:3)
  outer loop
    vertex xs1 ys1 zs1
    vertex xs2 ys2 zs2
    vertex xs3 ys3 zs3
  endloop
endfacet
```

This structure repeats `ncellg` times. For `3dht`,  $z=0$  is the free surface and all the elements must be located under the free surface.

#### 4.4.3 3D rectangular mesh

Under construction...

### 4.5 Parameters and Initial conditions

The following parameter and initial values are necessary for each element.

#### 4.5.1 Rake angle

In 3D problems, it is also necessary to specify the direction of slip (rake angle) for each element. The rake angle is defined as 90=reverse faulting, 0=right-lateral strike-slip faulting, and -90=normal faulting. The code does not allow for time-varying slip direction. 2D problems do not use rake values. Uniform case, set `crake` in `inputfile`.

#### 4.5.2 Friction parameters

HBI uses the regularized version of the rate and state friction (RSF) law, which is employed in the SEAS benchmark problems (Erickson et al., 2020). The friction coefficient are given by

$$\tau/\sigma = a \sinh^{-1}(V e^{\phi/a} / 2V_0). \quad (1)$$

The state evolution is governed by the aging law

$$\frac{d\phi}{dt} = \frac{bV_0}{d_c} \exp[(f_0 - \phi)/b] - \frac{bV}{d_c}. \quad (2)$$

The values of parameters  $(a, b, d_c, f_0)$  are set in `inputfile` in the case of uniform parameters.

#### 4.5.3 Initial conditions

The initial condition is uniquely determined by the value of normal stress, shear stress, and slip rate at each element (the state variable is determined by these three accordingly). In the case of uniform initial values of  $(\sigma, \tau, V)$ , these values are set in `inputfile` as `sigmainit`, `tauint`, and `velinit`.

#### 4.5.4 External loading

To have repeated ruptures on the same fault, external loading is necessary. `taudot` and `sigdot` are the stressing rates for shear and normal stresses, respectively. In the uniform case, `taudot` is `sr` and `sigdot` is zero. the value of `sr` must be specified in `inputfile`.

Alternatively, the code has "backslip loading option. If `backslip=T`, then the loading is added by slip deficit rate, that is,

$$\dot{\tau}_i = -V_{pl} \sum_j K_{ij} \quad (3)$$

$$\dot{\sigma}_i = -V_{pl} \sum_j L_{ij} \quad (4)$$

where  $K_{ij}$  and  $L_{ij}$  are kernel matrices for shear and nor,a; stresses, respectively. The value of `vpl` must be specified in `inputfile`. Spatially non-uniform backslip has not been implemented.

#### 4.5.5 Format of parameterfile

If you want to use non-uniform parameters and initial values, set `parameterfromfile T` in `inputfile` and create `parameter_file`. `parameter_file` has following structure:

```
rake(1) a(1) b(1) dc(1) f0(1) tau(1) sigma(1) vel(1) taudot(1) sigdot(1)
rake(2) a(2) b(2) dc(2) f0(2) tau(2) sigma(2) vel(2) taudot(2) sigdot(2)
...
```

#### 4.6 Stop control

The simulation stops when any of the following is satisfied.

1. the time-step reaches `nstep`
2. the slip rate is greater than `velmax`.
3. the slip rate is smaller than `velmin`.
4. the physical time reaches `tmax`.

#### 4.7 Restart

If `restart=T`, then the code reads the distributed output file to set the initial condition and restarts the simulation from the last checkpoint (the last time field variables were saved). The description of `inputfile` must be the same (other than `restart`), including the job number, and other parameters.

## 4.8 Useful functions

If `sigmaconst=T`, then normal stresses do not change with time as assumed in many studies. If `sigmaconst=F` (as the default value), the normal stress changes with time. The code can fail if the normal stress becomes very large or small values. To avoid this, the user can set limits on the value of normal stress by setting `limitsigma=T`. In this case, `maxsig` and `minsig` are maximum and minimum normal stresses which should be stated in `inputfile`.

If the geometry file has some issues, the simulation does not work well. By setting `foward=T`, the code computes the stress change from uniform slip on the fault and saves the result in `output/stressX.dat`. Users can use this function for debugging.

## 5 Visualization

ASCII files `monitorX.dat` and `eventX.dat` have global information.

`monitorX.dat` records the following information at every time step.

```
timestep time max(log10(vel)) mean(disp) mean(tau/sigma) max(sigma) min(sigma)
error-of-RK stepwidth wall-clock-time
```

For example, if you want to view the temporal change of the maximum slip rate in `gnuplot`, type

```
pl 'monitorX.dat' u 2:3 w l
```

The earthquake catalog is saved in `eventX.dat`. This file lists the event number, the onset time, and moment magnitude. In 2D problems the moment magnitude does not have meaning.//

The field data are saved in binary stream files. `xyzX.R.dat` is the coordinates of the elements. `velX.R.dat`, `tauX.R.dat`, `sigmaX.R.dat`, and `slipX.R.dat` are slip velocity, shear stress, normal stress, and slip every `interval` time steps, respectively. These are binary stream files.

The code `outd.f90` gathers distributed output files into a single unified ASCII file. Use like

```
ifort outd.f90 -o outd
./outd X N
```

where `X` is the `jobnumber` and `N` is the number of output files (0 - N-1), where  $N = \sqrt{N_p}$  and  $N_p$  is the number of MPI processes. `fieldX.dat` will be generated.

`fieldX.dat` has following structure

```
x(1) y(1) z(1) vel(1) tau(1) sigma(1) disp(1)
x(2) y(2) z(2) vel(2) tau(2) sigma(2) disp(2)
...
x(ncellg) y(ncellg) z(ncellg) vel(ncellg) tau(ncellg) sigma(ncellg) disp(ncellg)
---blank line---
---blank line---
x(1) y(1) z(1) vel(1) tau(1) sigma(1) disp(1)
x(2) y(2) z(2) vel(2) tau(2) sigma(2) disp(2)
...
x(ncellg) y(ncellg) z(ncellg) vel(ncellg) tau(ncellg) sigma(ncellg) disp(ncellg)
---blank line---
---blank line---
...
```

You can visualize the result with `gnuplot` using this file like:

```
pl 'fieldX.dat' u 1:3:4 index 5 lc palette pt 7
```

This will shows the snapshots of slip rate. We are planning to move on to a more sophisticated way in a future version.

## 6 References

Tse & Rice (1986) and Rice (1993) are early examples of earthquake cycle simulations on a planar fault with rate and state friction. For nonplanar fault geometry, Segall (2010) is a great reference to the theoretical foundation of the BEM kernel. For the implementation of `2dn`, we use the formula in Ando et al. (2007). `3dnt/3dht` is based on the expression by Nikkhoo & Walter (2015). The time-stepping algorithm is based on "Numerical Recipe for Fortran90" (Press et al. 2007).

## 7 Acknowledgements

I learned a lot about the method from Nobuki Kame and Makiko Ohtani when I was an undergraduate student. The basic structure of `HBI` is derived from the codes developed by them. `HACApK` library used in `HBI` was primarily developed by Akihiro Ida. I used a code for dynamic rupture simulations developed by Ryosuke Ando as a reference regarding 3D problems. I also thank Brittany Erickson, Eric M. Dunham, Pierre Romanet, and Tetsuya Hoshino for their suggestions that improved the performance, accuracy, stability, and readability of the code.