

River North Urban Design Overlay

Attachment to Third Substitute of Ordinance No. BL2017-932
as adopted on May 15, 2018

MPC case #:
2017UD-005-001

Document Contact Information

Planning Department staff provides consultations for developing within the River North Urban Design Overlay. Call (615) 862-7190 to schedule a meeting.



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Section I: Introduction

Introduction

History and Overview

The East Nashville Community includes a portion of the “East Bank”—the area on the east bank of the Cumberland River. The bulk of the East Bank is in the Downtown Community; however, a portion of the East Bank from Spring Street on the south to the I-24/I-65 interchange to the north is in the East Nashville Community. This area is commonly referred to as “River North.” For years, this area has been home to light industrial and warehousing businesses and it also experienced severe flooding during the flood of 2010. As downtown redevelops, developers are looking to the East Bank, including the northern portion in East Nashville, for redevelopment opportunities. This area is envisioned to redevelop to greater intensity, with taller buildings, capitalizing upon its river location and proximity to downtown.

River North is conceptualized as a vibrant, mixed-use, active neighborhood. The activation of the Cumberland River and publicly accessible greenspace are both important aspects of the neighborhood’s development. The culture of creation within “Production Row,” is a key aspect of the neighborhood’s culture. Therefore, the music industry is encouraged to continue to locate within River North, and use the District for various uses. Re-use and adaptation of existing structures and elements within River North is encouraged as a part of the area’s development to respect the history of warehousing and light industry.

While portions of River North sit within a floodplain, various mitigation strategies are available to allow for sustainable development in this area. These strategies include, but are not limited to:

- Floodable underground detention basins
- Flow-through construction
- Development of infiltrative, sustainable landscapes
- Elevation of building sites

Intent

The goals of the Urban Design Overlay are as follows:

- Establish a compact mixed use development pattern distributed along a system of streets that transitions in scale from the core to the neighborhood.
- Ensure that buildings are oriented to and linked by a cohesive pedestrian system.
- Encourage a balance of transportation options for pedestrians, bicycles, vehicles and transit.
- Encourage high quality (function and aesthetic) open spaces for assembly, relaxation, civic events, display of public art and other similar purposes.
- Encourage a high level of pedestrian-generating activity along streets and a pedestrian friendly environment.
- Encourage environmentally sensitive development and green space.



Section I: Introduction

Location

Located along the East bank of the Cumberland River, River North is a mixed-use, urban neighborhood, and extension of the Downtown core.



Section I: Introduction

How to Use this Document

This document is to be used by developers, property owners, government officials, residents, and any individual who is interested in development or redevelopment of any property located within the UDO boundary.

A UDO is a zoning tool that requires unique physical design standards for development or redevelopment within a designated area that would otherwise not be ensured by the standard provisions of the zoning regulations. A UDO can modify base zoning standards such as setbacks, building height, floor area ratio, and parking per the provisions outlined in Section 17.36.320 of the Zoning Code. The standards established in this document vary from the underlying base zone district standards for the properties in the UDO. All provisions are regulatory in nature and have the same force and effect as the zoning regulations of the Metro Code. Any final plans submitted for approval under the UDO will be reviewed for adherence to these provisions and to the provisions of the base zoning that are not varied by the UDO. If a final plan is consistent with the UDO and the zoning standards it can be approved administratively by the Executive Director as expressed in the Planning Commission's bylaws and as clarified here.

The design standards established in the UDO are intended to direct future development in a manner that addresses strategies for site design including placement, massing and orientation of buildings, architectural treatment, landscaping and screening, general access and parking, and signage.

In some instances, desired standards that are beyond the authority of the zoning ordinance accompany the goals and objectives. These desired standards pertain to areas for which Metropolitan Government exercises final authority over design, construction and operation of facilities, such as public rights-of-way and stormwater detention and conveyance. The incorporation of these standards into any final development construction plans will depend on Metropolitan Government review for consistency with policies, laws, and related standards of various departments.

Overlapping Plans

Within the UDO boundary area, there may exist other regulations and design guidelines intended to work in conjunction with the UDO. Property owners and developers should consult with all departments and agencies during the development process to address any and all rules, regulations and policies. Property owners should consult with Metro Planning and Public Works to make the necessary improvements to the streetscape in accordance with the Major and Collector Street Plan and the Strategic Plan for Sidewalks and Bikeways and Title 17.20.120 Provision of sidewalks.

- If a property is zoned Specific Plan then all standards contained with the Specific Plan shall apply and the UDO standards would apply for any standard not addressed in the SP.
- If a property has a Planned Unit Development Overlay then the standards of the PUD shall apply and the UDO standards would apply for any standards not addressed in the PUD.
- Final construction drawings shall comply with the design regulations established by the Department of Public Works, in effect at the time of the approval of the preliminary development plan or final development plan or building permit, as applicable. Final design may vary based on field conditions.

Subdistricts

The River North UDO is organized by Subdistricts, as identified on the Regulating Plan. Subdistricts are smaller districts within the larger UDO area that are envisioned to have unique character and development standards.

To determine the standards which apply to a particular property:

- On the Regulating Plan, identify the Subdistrict in which the property is located.
- Consult the Subdistrict Standards section for the development standards relevant to the Subdistrict.
- Consult the General Standards section for guidance on development standards for all Subdistricts.

Section I: Introduction

Compliance, Modifications and Design Review

Compliance

All provisions of the Metro Zoning Code shall apply, unless otherwise addressed by the River North UDO standards. The UDO standards shall apply as follows:

New Development

Full Compliance with all standards of the UDO.

An addition to the square footage of an existing building:

The addition shall be in compliance with applicable standards of the UDO and shall not increase any degree of non-conformity.

A new structure on a lot with existing building(s):

The new structure shall be in compliance with applicable standards of the UDO and shall not increase any degree of non-conformity.

Signage Compliance:

Signage is per base Zoning District with review via the Codes Department

Redevelopment of existing riverfront building:

For the property located on the river, commonly referred to as “Cherokee Marine,” the property may be redeveloped and deviations from the UDO may be permitted via a minor modification. The development shall try, where possible, to comply with the terms of this UDO and the permitted uses in the base zone shall apply. Nevertheless, development shall be encouraged and allowed, including deviations, so long as the overall plan is consistent with the intent and purpose of the UDO.

Inclusionary Housing

Applicants shall provide two scenarios with proposed residential development. One scenario shall illustrate the residential development entitlements provided by the underlying zoning at the time this UDO was adopted, and the second scenario shall illustrate the residential development entitlements permitted by the UDO standards.

If residential entitlements provided by the UDO standards are greater and the proposed development involves five or more residential rental units, affordable or workforce housing shall be recognized as set forth in Ordinance Nos. BL2016-133, and BL2016-342, which authorizes Metro grants to offset the provision of affordable or workforce housing units.

If the underlying zoning for the property has changed since the adoption of this UDO, applicants shall provide a third scenario showing residential entitlements provided by the current zoning with the UDO applied. If the proposed development involves five or more residential rental units, affordable or workforce housing shall be recognized as set forth in Ordinance Nos. BL2016-133, and BL2016-342, which authorizes Metro grants to offset the provision of affordable or workforce housing units, due to residential development entitlements gained through the underlying zone change.

Section I: Introduction

Modifications to the Standards

An applicant may seek modifications to the standards of this document. Any standard within the UDO may be modified, insofar as the intent of the standard is being met, the modification results in an equal or better urban design for the neighborhood as a whole, and the modification does not impede or burden existing or future development of adjacent properties.

The River North UDO, the East Nashville Community Plan, the Major Street and Collector Plan, and any other policies and regulations from governing agencies shall be consulted when considering modifications.

Modifications may be approved by Planning staff, the Planning Commission or MDHA's Design Review Committee:

- Minor modifications – deviations of 20 percent or less, or minor deviations in non-numerical standards – may be approved by Planning Staff.
- Any determination made by the Planning Staff may be appealed to the Planning Commission by the applicant.
- Major modifications – deviations of more than 20 percent– and major deviations from non-numerical standards may be approved by either the Planning Commission or the MDHA Design Review Committee.
- For any property that falls within an MDHA Redevelopment District the Design Review Committee shall have jurisdiction to approve deviations.
- For modifications to overall height, the Executive Director of the Planning Department shall determine whether the developer has made reasonable efforts to use all appropriate bonuses. The Executive Director's decision may be appealed to the MDHA DRC if a Redevelopment District is in place. If it has been determined that all reasonable efforts have been made to use the Bonus Height Program, the applicant shall hold a community meeting with the property owners within 300 feet , providing notice to these owners, and the Planning Commission shall review the modification request and may grant additional height for exceptional design including but not limited to unique architecture, exceptionally strong streetscape and improvements to the project's relationship to surrounding properties.

Variances and Special Exceptions

Variances and special exceptions that are not specifically for standards of the River North UDO shall follow the procedures of the applicable chapters of the Zoning Code.

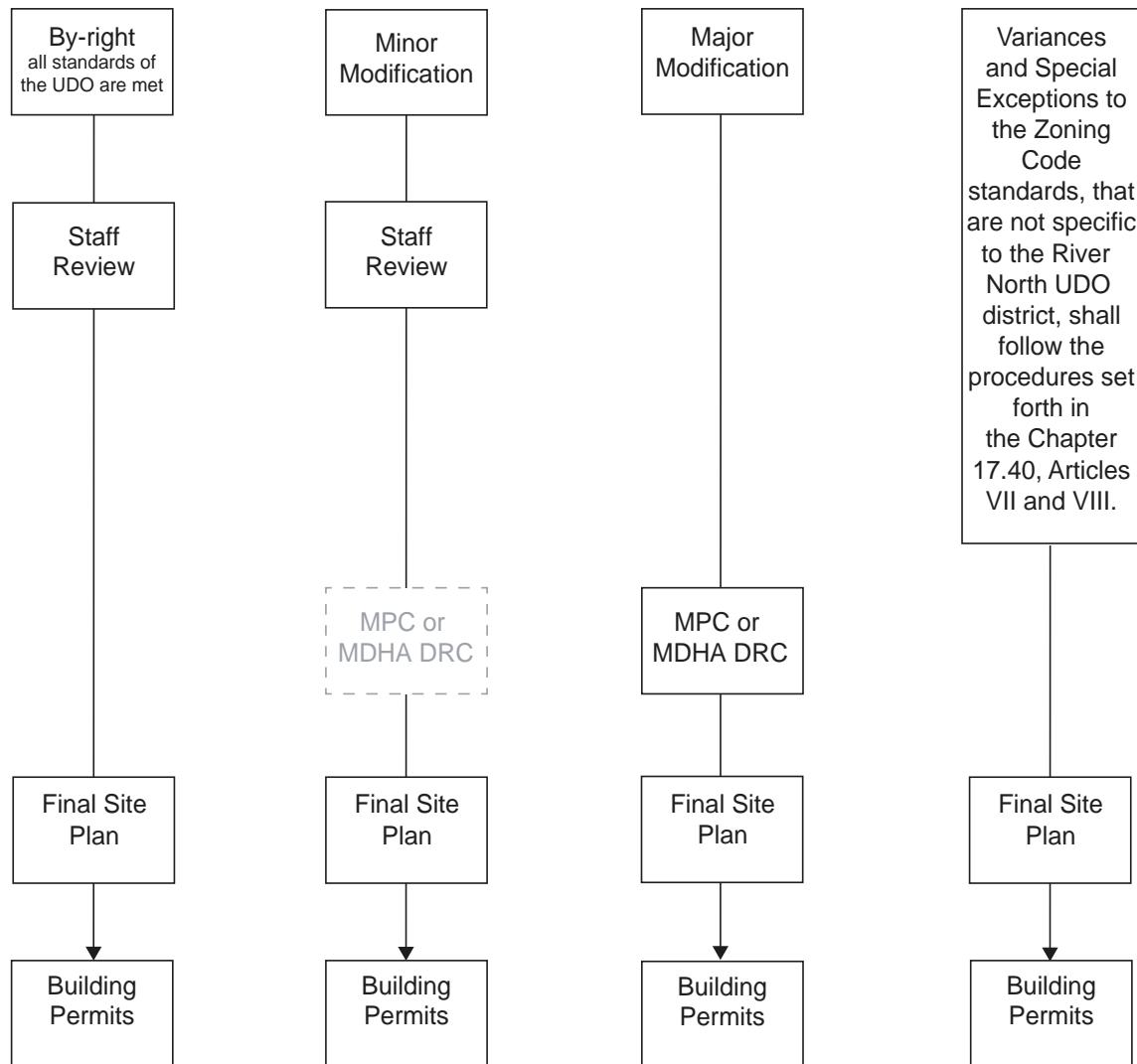
Variances and special exceptions shall not be applicable to the height standards of the UDO which are governed by the earlier procedure reference above. Standards specific to the River North UDO may be modified based on the Modifications section of this document.

Civic Buildings

For Civic Buildings within the UDO:

- The Metro Planning Commission or its designee shall make the final determination of compliance with the UDO standards.
- Civic Buildings within the River North UDO shall be iconic, shall not be prototypical design, and must respond to the materiality and form of the surrounding context.

Section I: Introduction



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Section II: Subdistrict Standards

Section II: Regulating Plan & Subdistricts

Illustrative Plan

River North is intended to be a dense, mixed-use, urban neighborhood. Connection to the surrounding neighborhoods is an important aspect of River North. Activated, consolidated, usable greenspace and open space are encouraged within the neighborhood.

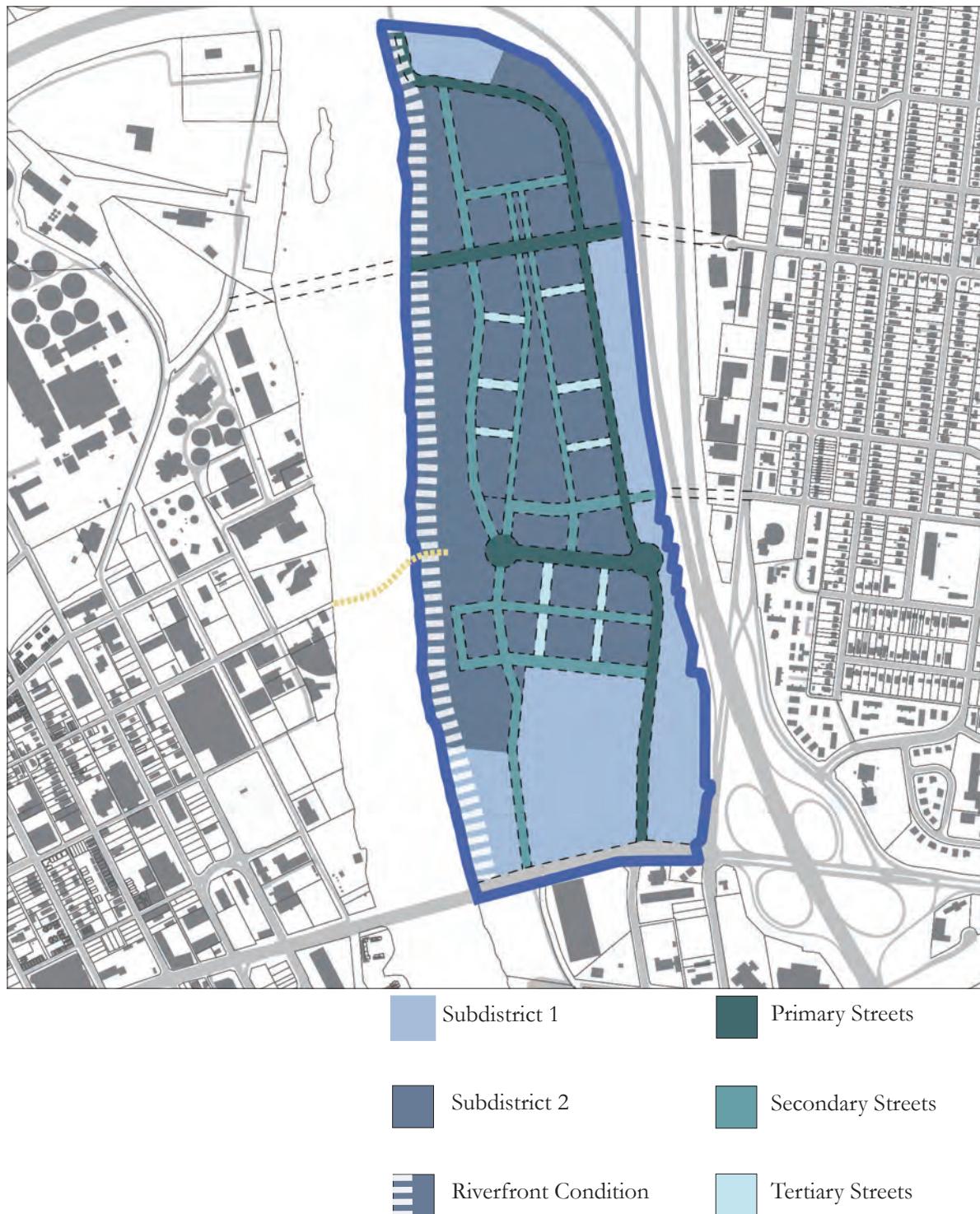


Illustrative Masterplan

Section II: Regulating Plan & Subdistricts

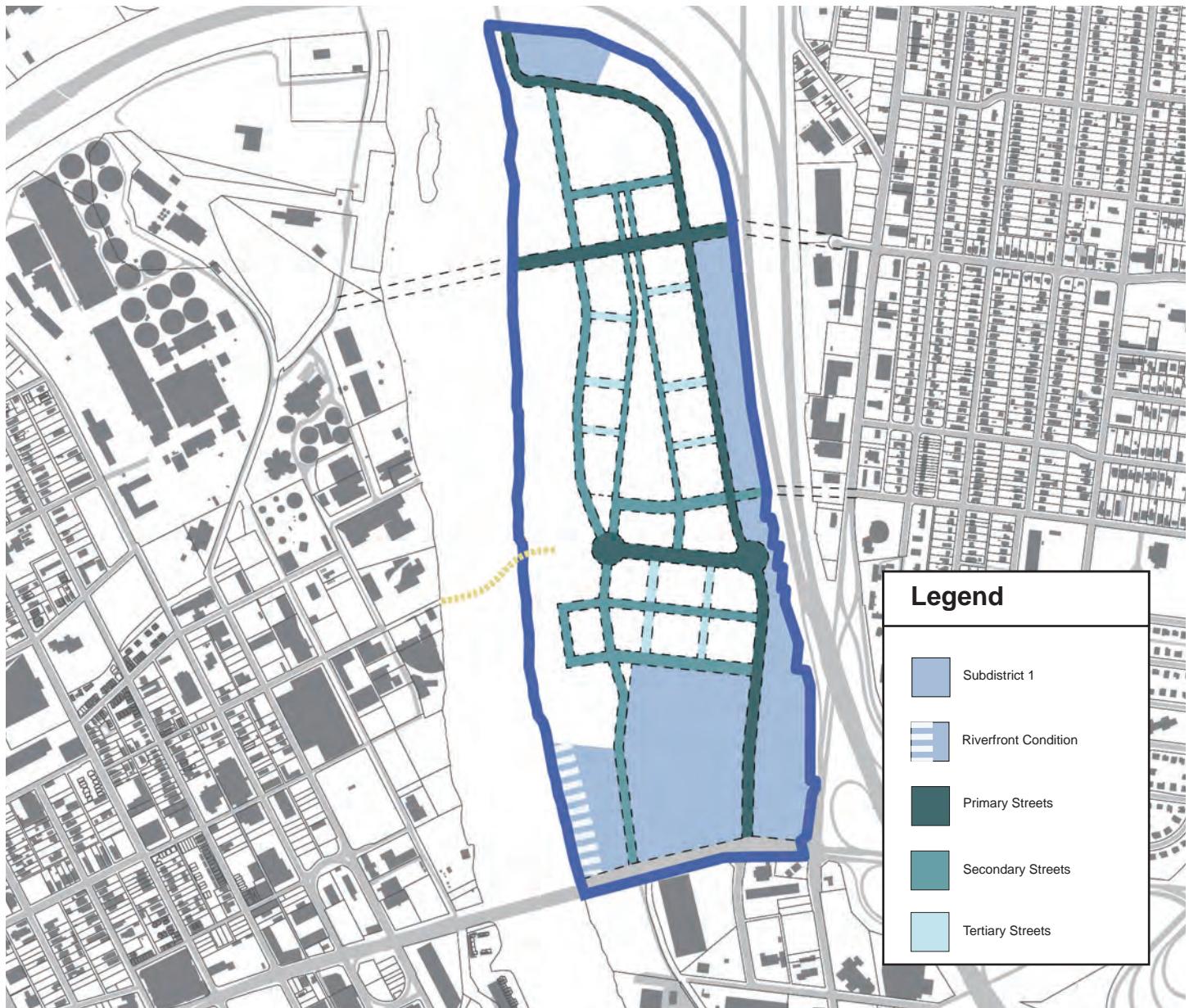
Regulating Plan

The Regulating Plan is the official zoning map of the UDO. The Regulating Plan shows the Subdistricts that govern the development standards for each property.



Section II: Regulating Plan & Subdistricts

Subdistrict 1: Regulating Plan



Subdistrict 1

Section II: Regulating Plan & Subdistricts

Subdistrict 1: Building Regulations

Frontage

| | |
|------------------------|--------|
| A Build-to Zone | 0'-15' |
|------------------------|--------|

B Facade Width

| | |
|------------------|--------------------------|
| Primary Streets | 60% of lot frontage min. |
| Secondary Street | 40% of lot frontage min. |
| Tertiary Street | 20% of lot frontage min. |

Remaining lot frontage may be used for pedestrian amenities and shall not be used for parking.

| | |
|------------------------------|--------------------------|
| C Min. building depth | 15' from building facade |
|------------------------------|--------------------------|

Height

| | |
|---------------|-----|
| D Min. | 14' |
|---------------|-----|

| | |
|---------------|------------|
| E Max. | 15 stories |
|---------------|------------|

Additional height available through the Bonus Height Program

Step-back *

Step-back required on all streets and Open Space

F Step-back between

Buildings taller than 7 stories by the 8th story

| | |
|-------------------------------|-----|
| G Min. step-back depth | 15' |
|-------------------------------|-----|

Side & Rear Setbacks

| | |
|---------------|----|
| H Min. | 0' |
|---------------|----|

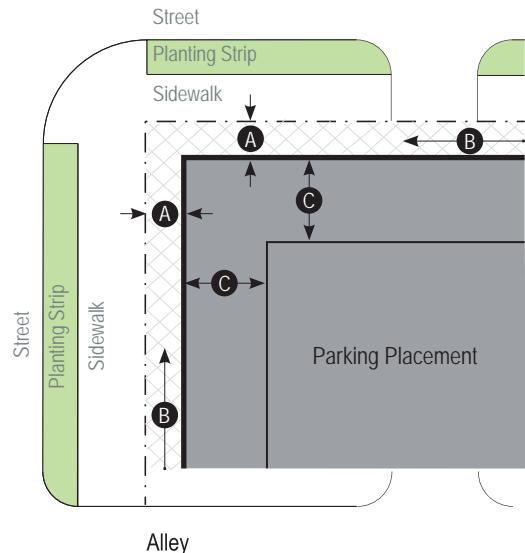
Sidewalk & Planting

Improvements to the sidewalk corridor according to the General Standards and the Major and Collector Street Plan

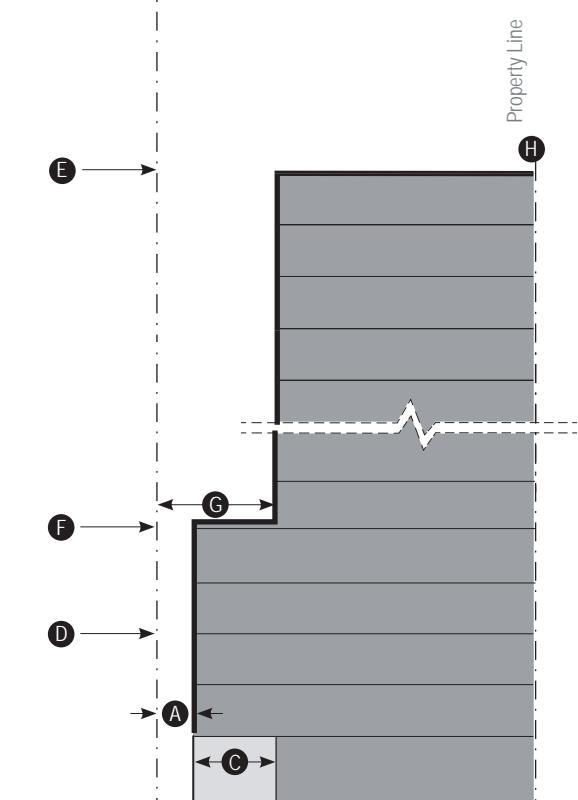
Riverfront Condition

By the 11th story, 20% min. of the total length of the Riverfront Condition frontage must be open to provide for views across the site

* See page 20 for full description of step-back.



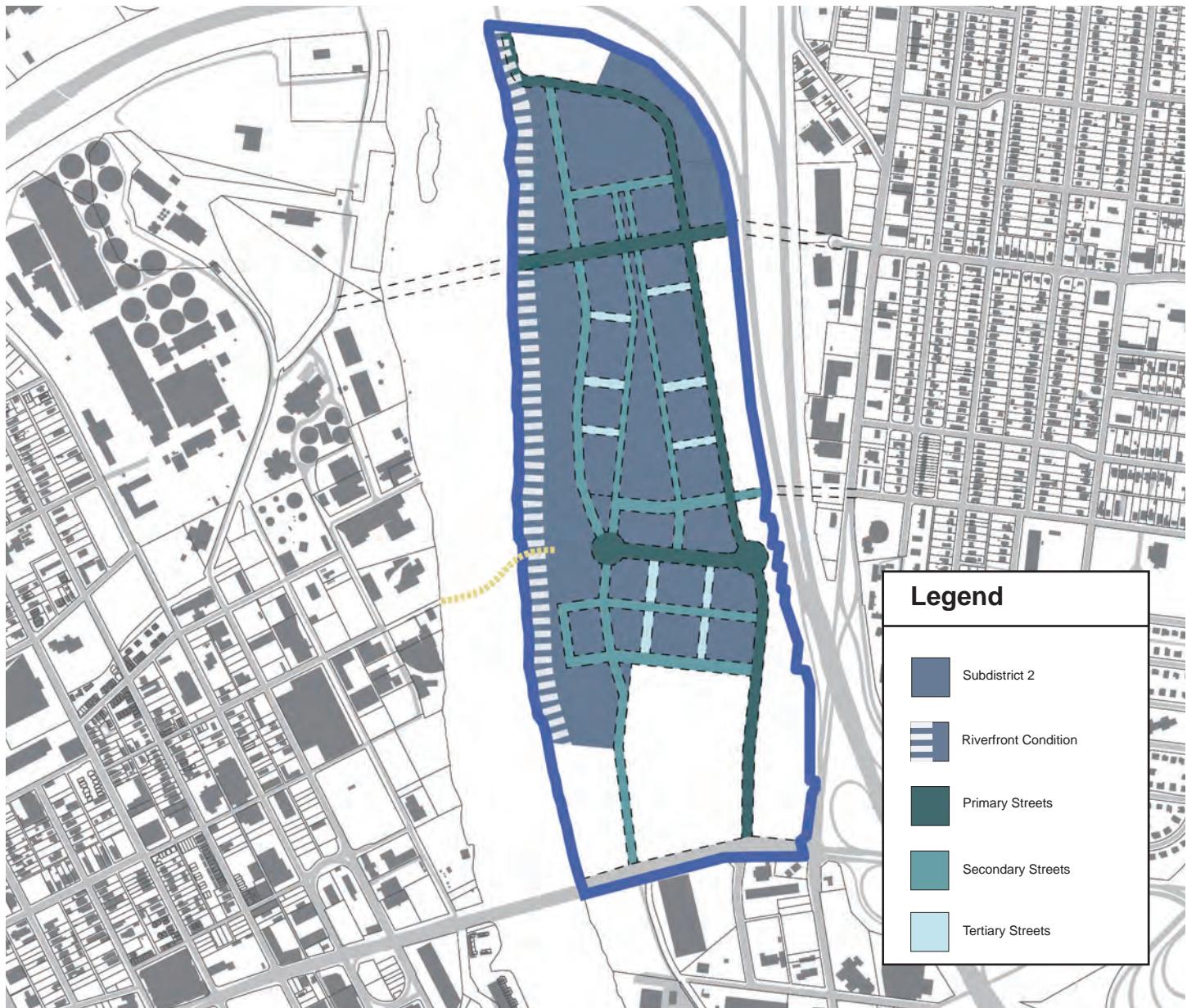
Building Plan



Building Section

Section II: Regulating Plan & Subdistricts

Subdistrict 2: Regulating Plan



Subdistrict 2

Section II: Regulating Plan & Subdistricts

Subdistrict 2: Building Regulations

Frontage

| | |
|------------------------|--------|
| A Build-to Zone | 0'-15' |
|------------------------|--------|

B Facade Width

| | |
|------------------|--------------------------|
| Primary Streets | 60% of lot frontage min. |
| Secondary Street | 40% of lot frontage min. |
| Tertiary Street | 20% of lot frontage min. |

Remaining lot frontage may be used for pedestrian amenities and shall not be used for parking.

| | |
|------------------------------|--------------------------|
| C Min. building depth | 15' from building facade |
|------------------------------|--------------------------|

Height

| | |
|---------------|-----|
| D Min. | 14' |
|---------------|-----|

| | |
|---------------|------------|
| E Max. | 25 stories |
|---------------|------------|

Additional height available through the Bonus Height Program

Step-back *

Step-back required on all streets and Open Space

F Step-back between

Buildings taller than 7 stories by the 8th story

| | |
|-------------------------------|-----|
| G Min. step-back depth | 15' |
|-------------------------------|-----|

Side & Rear Setbacks

| | |
|---------------|----|
| H Min. | 0' |
|---------------|----|

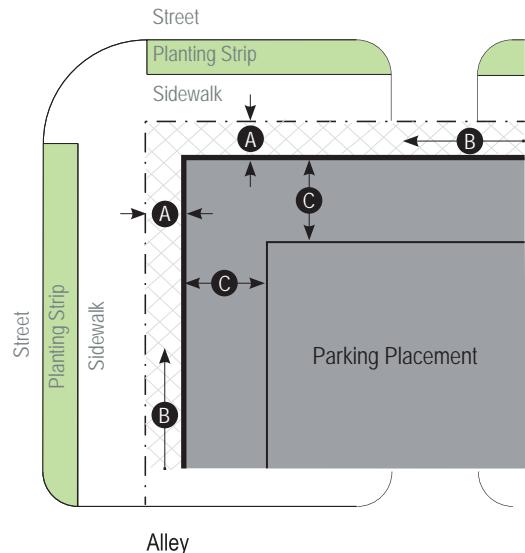
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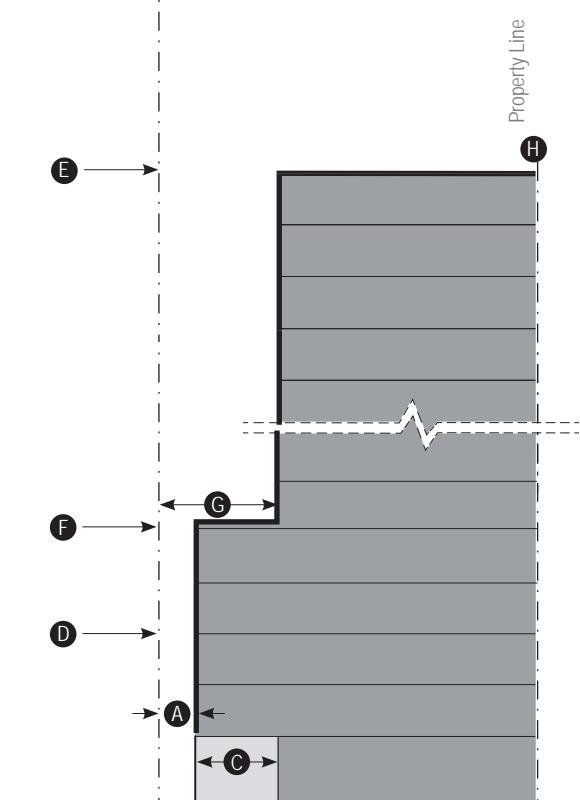
Riverfront Condition

By the 11th story, 20% min. of the total length of the Riverfront Condition frontage must be open to provide for views across the site

* See page 20 for full description of step-back.



Building Plan



Building Section

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Section III: General Standards

Section III: General Standards

General Standards

Measurement from “Grade”

- Unless otherwise indicated, reference to measurements of height shall be calculated using the average elevation along the public right-of-way fronting the property. Thus, grade will generally be measured from the public sidewalk, not from grade on site.
 - When buildings are set back from the property line more than 15 feet, grade shall be measured as the average existing elevation at the building façade.
- In the event that the base flood elevation, as established by FEMA, is higher than the sidewalk or grade elevations, the height of the first story, shall be measured from 1 foot above the base flood elevation.

Measurement of Height

- Unless otherwise specified herein, the height of buildings shall be measured in stories.
- The maximum height for an individual story shall not exceed 25 feet from finished floor to finished floor for each of the first 2 stories, 18 feet floor to floor above the second story, and 25 feet for the top story of buildings greater than 5 stories.
- Where a parking liner exists, 2 liner stories shall be counted as a single story, and any number of parking levels may be concealed behind it.
- The maximum height for a raised foundation is 6 feet above grade.
- Basements are not considered stories for the purposes of determining building height.
- Building height shall be measured from each Street Frontage (excluding alleys) or Open Space.
- The height of fences, walls and hedges shall be measured in feet from the average sidewalk elevation.

Base Zoning Clarifications

- All properties within the UDO shall be exempt from the Floor Area Ratio (FAR) requirements of the underlying base Zoning districts.
- All properties within the UDO shall be exempt from the Height Control Plane, height limitations, Step-back, and front, rear, and side Setback requirements of the underlying base Zoning districts (including Height Control Planes from adjacent residential districts).
- Impervious Surface Ratio is per the base Zoning District.
- There is no minimum lot size within the UDO.
- Landscaping standards and required buffers shall be controlled by the general standards of this document and are exempt from the requirements of the base Zoning districts.
- Plans within the River North UDO shall comply with the Metro Tree Ordinance Standards.

Step-backs

- Within the River North UDO, the step-back is defined as the required minimum distance the upper stories of a building must be stepped back from the outer edge of the build-to-zone, along all applicable frontages.
- To allow for massing variation, stories within the range may be permitted to step-back to a lesser extent or not at all, so long as the minimum step-back depth is met by the required step-back story.

Section III: General Standards

General Standards

Frontages

A Frontage is the specific way in which the building face addresses the street. It is the transition and interaction between the private and public realms. Building Frontages define the character and form of the public spaces within each neighborhood. The following standards shall apply to all development within the River North UDO.

- Buildings shall front a street (excluding alleys), open space, and/or a pedestrian passage.
- Facade Width
 - The minimum facade width is the minimum amount of the frontage that must be defined by a building, and is designated as a percentage of the frontage.
 - Every property shall establish one Principal Frontage along a street.
 - When a lot fronts more than one street the following priority shall be given when establishing the Principal Frontage: Primary Street, Secondary Street, Tertiary Street, Other Street.
 - In the instance a property fronts multiple Primary Streets, any may be chosen as the Principal Frontage.
 - Along a Minor Frontage, modifications may be granted for the reduction of ground level garage Liners and or glazing requirements.
 - For parcels larger than [1] Acre in size, frontage requirements may be further reduced by minor modification.
- Open Space Frontages
 - Facade width and active use requirements shall apply to these frontages the same as a street frontage.
 - All buildings fronting open space shall have a minimum of one primary pedestrian entrance on the open space.

Section III: General Standards

General Standards

Build-to Zone

- The Build-to Zone is the specified depth along a property's street frontage(s) in which the required minimum facade width must be located.
- Depending on site conditions, the front of the Build-to Zone may begin at different locations.
 - When the existing streetscape and sidewalk meets with the Major and Collector Street Plan, the Build-to Zone begins at the back of the required streetscape (including sidewalk zones).
 - When the existing streetscape and sidewalk does not meet with the Major and Collector Street Plan, the sidewalk shall be widened on site and the Build-to Zone begins at the back of the new streetscape (including sidewalk zones).
 - When utility or pedestrian easements exist along the street frontage of a property, the Build-to Zone shall begin at the back of the easement.
 - When buildings front an Open Space, the Build-to Zone shall begin at the back of the Open Space.
- Attachments
 - Structures, including porches, stoops, and balconies may encroach into the Build-to Zone.
 - Elements such as stairs, awnings, and landscaping may encroach beyond the Build-to Zone. Any encroachments into the right-of-way must follow the Mandatory Referral process.
- When calculating the minimum facade width, access to structured parking shall not be counted as part of the required facade width, and access to surface parking shall not be counted part of the required façade width. That is, access to surface parking is allowed in the “remaining” area, after the facade width requirement has been met.

Entrances

- All buildings shall have at least one direct functional pedestrian entrance, along the principal frontage. This may be access to a lobby shared by individual tenants.
 - Whether opening to the circulation network or other public space, the functional entry must be connected to a sidewalk or equivalent provision for walking.
 - If the public space is a square, park, or plaza, it must be at least 50 feet (15 meters) deep, measured at a point perpendicular to each entry.
- Buildings with multiple ground floor commercial tenants shall provide at least one direct pedestrian entrance for each tenant space oriented to the frontage, or submit a shared access plan for staff review.
- Corner entrances are appropriate on corner lots.

Section III: General Standards

General Standards

Active Use

- An active ground floor use requirement shall mean a habitable space occupied by retail, office, residential, institutional or recreational uses, specifically excluding parking and mechanical uses. Minimum 15 feet in depth.
- Active uses are those programmed spaces that generate pedestrian street activity and interaction. Hallways, storage rooms, fitness centers, and other ancillary spaces shall not qualify as an active use.
- An active use is required on the ground floor of all streets, open spaces and greenways other than Tertiary streets.
- The term “active use” and ground level “building liner” are synonymous.
- Active ground floor uses must match the facade width percentage requirements. For example, if 60% facade width min. is required along a lot’s frontage, then 60% min. of the lot’s frontage must also consist of an active ground floor use.

Glazing and Massing

- Openings for vehicular access to parking structures on the first floor shall be included in calculation of total facade area.
- All street and open space level exterior windows must have a minimum light transmission of 60 percent.
 - Modifications may be permitted in so far as it is determined that tinting does not substantially diminish the effect of the building wall or the pedestrian character of the street.

Section III: General Standards

Frontage Types: Storefront Frontage

The Storefront Frontage has a limited Build-to Zone that is close to the street, with building entrances accessible at sidewalk grade. The Storefront Frontage has substantial glazing on the facade at ground level, space for pedestrian-oriented signage, awnings, retail display, and other design features conducive with creating an active commercial streetscape.

The Storefront Frontage is commonly used for general commercial, office, retail, restaurant, lobby, etc.



Section III: General Standards

Frontage Types: Storefront Frontage

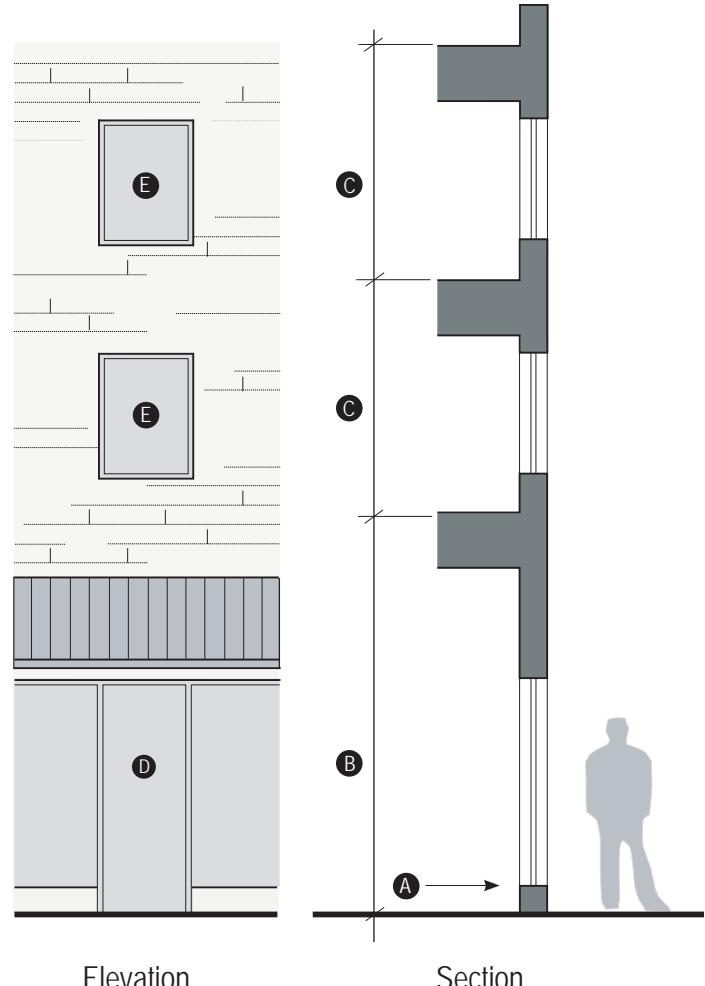
Storefront Frontage

| | |
|---------------------------------------|-------------------------|
| A Max. sill height | 3 ft |
| B Min. ground floor height | 14 ft from grade |
| C Min. upper floor(s) height | 10 ft floor to floor |
| D Min. ground floor glazing* | |
| Principal Frontage | 40% floor to floor |
| Minor Frontage | 30% floor to floor |
| E Min. upper floor(s) openings | 25% from floor to floor |

Notes

Where Storefront frontage is allowed, modifications may be given to allow for a Storefront arcade. All Storefront Frontage standards shall be met on the facade behind the arcade.

*All grade-level retail shall provide clear vision glass between 3' and 8' above grade for a minimum of 60% of its frontage area.



Elevation

Section

Section III: General Standards

Frontage Types: Stoop Frontage

The Stoop Frontage has a limited to moderate Build-to Zone with the first floor elevated from the sidewalk grade. This frontage type utilizes a stoop - a small landing connecting a building entrance to the sidewalk by a stair or ramp - to transition from the public sidewalk or open space into the building.

Stoops are generally provided externally, but may be provided internally as necessitated for ADA compliance.

The Stoop Frontage is generally used for residential and live-work buildings, but may be appropriate for other uses.



Section III: General Standards

Frontage Types: Stoop Frontage

Porch Frontage

A First floor elevation

| | |
|------|-----------------|
| Min. | 24" from grade |
| Max. | 5 ft from grade |

B Min. ground floor openings 30% floor to floor

C Min. upper floor(s) openings 25% from floor to floor

Stoop

D Min. porch depth 5 ft

E Stoops may extend into the Build-to Zone.

F Steps may extend into the Build-to Zone, but may not encroach into the public Right-of-Way.

Notes

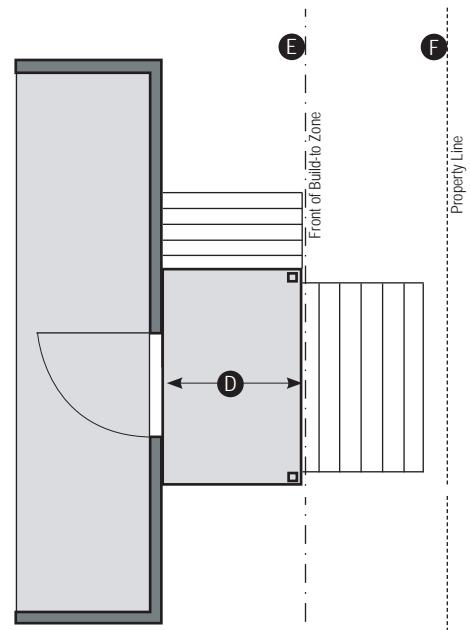
Greater first floor elevation allowed by modification for:

- Property with significant elevation change across the site at the street frontage.
- Development that incorporates below grade basement floors that are accessible from the exterior of the building.

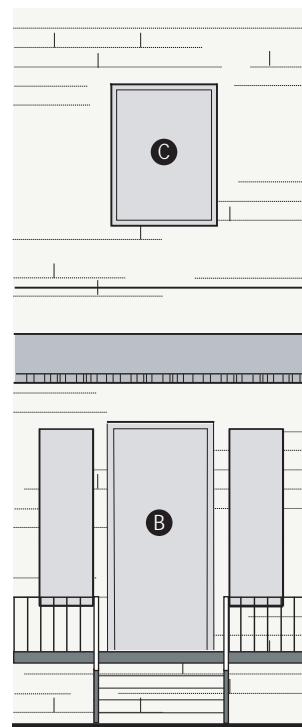
Transition to first floor elevation may be accommodated on the interior of the building to allow for compliance with ADA accessibility requirements.

Entries shall not be recessed more than 4 feet from the facade of the building.

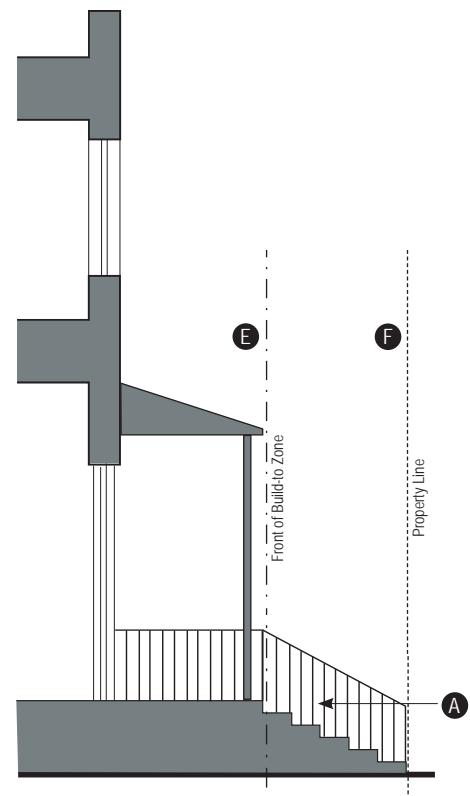
Doors shall face the street.



Plan



Elevation



Section

Section III: General Standards

Frontage Types: Porch Frontage

The Porch Frontage has a moderate Build-to Zone with the first floor elevated from the sidewalk grade. The Porch Frontage utilizes a porch - an open air room appended to the mass of a building with floor and roof but no walls on at least two sides - to transition from the public sidewalk or open space into the building.

The Porch Frontage is primarily used for residential buildings.



Section III: General Standards

Frontage Types: Porch Frontage

Porch Frontage

A First floor elevation

| | |
|------|-----------------|
| Min. | 18" from grade |
| Max. | 5 ft from grade |

B Min. ground floor openings

30% floor to floor

C Min. upper floor(s) openings

25% from floor to floor

Porch

D Min. porch depth

5 ft

E Porches may extend into the front of the Build-to Zone.

F Steps may extend into the Build-to Zone, but may not encroach into the public Right-of-Way.

Notes

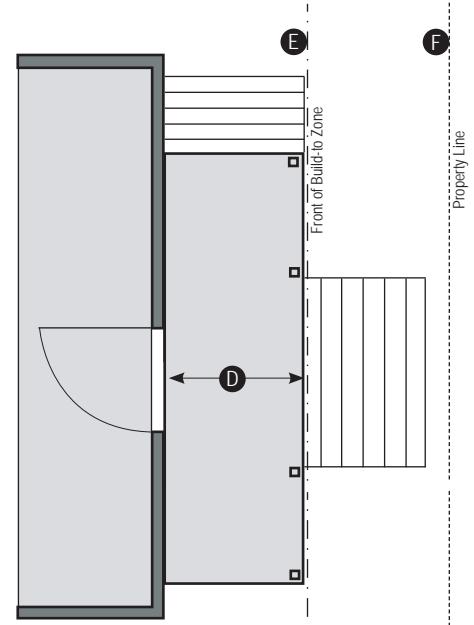
Greater first floor elevation allowed by modification for:

- Property with significant elevation change across the site at the street frontage.
- Development that incorporates below grade basement floors that are accessible from the exterior of the building.

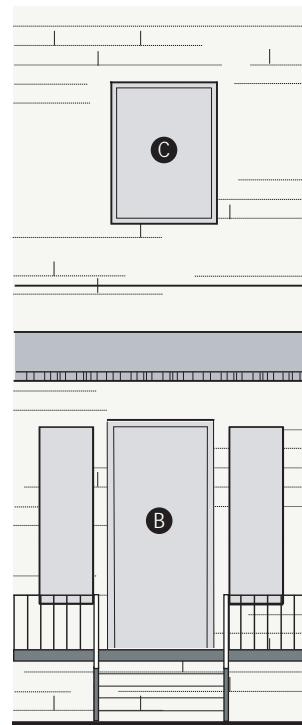
Transition to first floor elevation may be accommodated on the interior of the building to allow for compliance with ADA accessibility requirements.

Entries shall not be recessed more than 4 feet from the facade of the building.

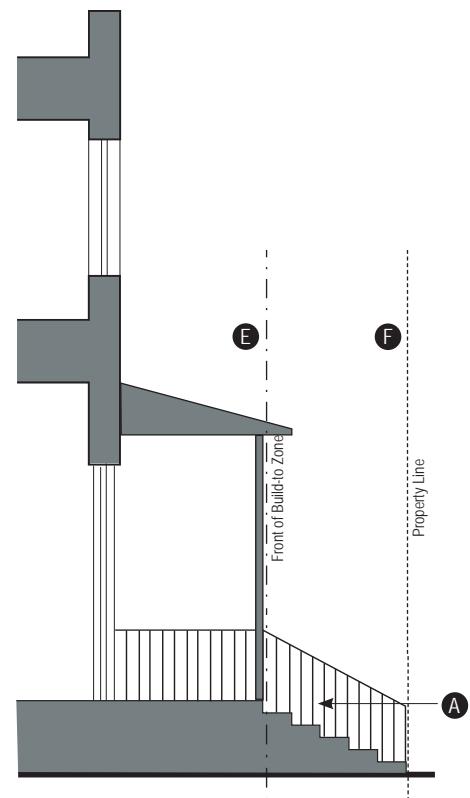
Doors shall face the street.



Plan



Elevation



Section

Section II: General Standards

Frontage Types: Civic Frontage

Civic buildings are designed and constructed for community use or benefit by governmental, cultural, educational, public welfare, or religious organizations. Civic buildings are inherently unique structures that present opportunities for unusual and iconic design within the urban fabric.

Civic buildings should be designed with prominence and monumentality.

A Civic building shall be oriented to streets and public spaces and follow the intent of the particular subdistrict in which it is located with regard to pedestrian orientation, massing, and articulation.

Key architectural features should act as community focal points. Where possible, street axes should be terminated by the primary building form or architectural feature. Towers, spires, and other vertical forms are encouraged.

Civic buildings may include the following: community buildings, libraries, post offices, schools, religious institutions, publicly owned recreational facilities, museums, performing arts buildings, and municipal buildings.

Civic buildings shall be reviewed by modification pursuant to the procedure outlined on page 9 of the UDO.



Section III: General Standards

Canopies and Awnings

Canopies

(A) Clearance

| | |
|-----------------------|-----|
| Minimum from sidewalk | 8' |
| Maximum | 25' |

(B) Maximum projection

within 2' of curb

(C) Maximum canopy height

4'

Encroachments in the public right-of-way must meet Metropolitan Government's current clearance standards and be approved under the mandatory referral process prior to installation.

Awnings

(A) Clearance

| | |
|-----------------------|----|
| Minimum from sidewalk | 8' |
|-----------------------|----|

(B) Maximum projection

| | |
|--------------|----------------|
| First floor | 4' from facade |
| Upper floors | not permitted |

(C) Maximum awning height

5'

The name and logo of the establishment are the only advertising permitted on awnings. All shall follow the Sign Standards.

No awning shall exceed 25 feet in length.

Awnings shall not be constructed of materials that are glossy in finish.

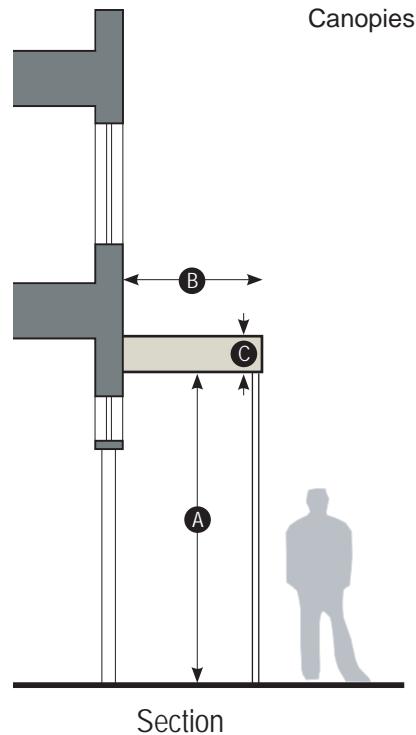
Encroachments in the public right-of-way must meet Metropolitan Government's current clearance standards and be approved under the mandatory referral process prior to installation.

Canopy and Awning standards do not apply to brise soleil or sun-shades.

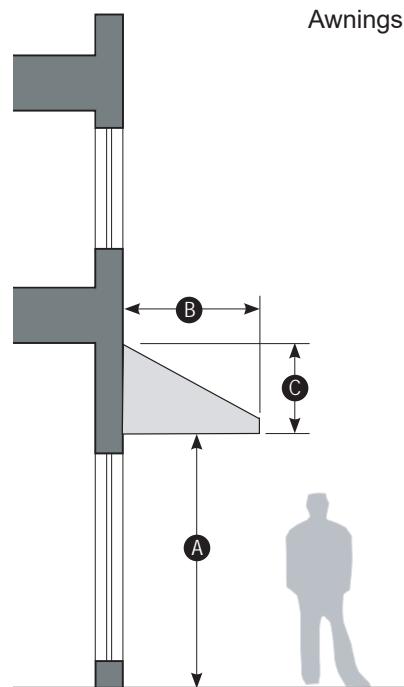
Auto-oriented canopies and awnings

Auto-oriented canopies and awnings, for uses such as drive-thrus and gas station pumps, may be attached to a building according to the following:

- The building shall comply with all Frontage standards.
- The canopy and/or awning shall be lower in height than the primary building.
- The setback of the canopy and/or awning shall be a minimum of 15 feet from the back of the front facade of the building.
- A drive-through canopy and/or awning shall not be located along the principal frontage.



Section



Section

Section III: General Standards

Street Character

The public right-of-way, including streets, sidewalks and public utility infrastructure, plays both a functional and social role in the life of the city and its citizens. Streets organize the city, help to define space, and link destinations. The street is also a public place where people congregate, shop, socialize and live. Active, attractive streets are critical to the continued growth and success of River North. The UDO includes urban design tools to make working, living and playing in River North lively, safe and comfortable.

The UDO uses Street Types as an urban design and organizing tool. All streets are classified on the Regulating Plan as Primary, Secondary, Tertiary, Other, or Alley. The location of vehicular access from all other streets shall be determined on a case-by-case basis. NashvilleNext calls for a strong emphasis on expanding other modes of transportation including walking, cycling and transit. The UDO emphasizes walking, cycling and transit as primary modes of transportation within River North through the urban design of individual buildings, blocks, and neighborhoods.

All Streets

- Streets refer to publicly or privately owned right-of-way. They are intended for use by pedestrian, bicycle, transit and vehicular traffic and provide access to property.
- Streets consist of vehicular lanes and the Sidewalk Corridor. The vehicular lanes, in a variety of widths, provide traffic and parking capacity and may include bicycle paths. The Sidewalk Corridor contributes to the urban character of each neighborhood. It may include pedestrian paths, landscaped planters, street furnishings and street trees.
- Pedestrian safety, comfort, and accessibility should be a primary consideration of street design and dimensioning.
- When alleys are present, vehicular access from alleys is encouraged. Vehicular access from public streets shall be considered in the following order: Other Streets, Tertiary Streets, Secondary Streets, and then Primary Streets as approved by Metro departments.
- Final construction plans shall comply with Metro Public Works standards and specifications.

Street Types

Primary Street

Primary Streets accommodate high levels of pedestrian activity and high levels of vehicular traffic. On Primary Streets, active uses – residential, retail, restaurant or office – lining parking structures and on the first floor of buildings, and restricted vehicular access enhance the pedestrian experience. Primary streets provide the opportunity for more intense, urban development including shallow Build-to Zones and, in some cases, increased building height. Pedestrian comfort on these streets is of highest importance. Primary streets should have a continuous street wall, wide sidewalks between 14 and 20 feet to provide room for street furniture such as benches, trash receptacles, and bicycle parking. Primary Streets have the highest level of urban activity such as, outdoor dining, retail displays, and community activities like markets, parades, and music. Street trees provide protection from the sun and rain, reduce stormwater runoff and air pollution, and provide aesthetic value to the city. Trees should be planted in wells with tree grates to allow for the uninterrupted flow of pedestrian traffic.

Section III: General Standards

Street Character

Secondary Street

Secondary Streets have moderate levels of pedestrian activity and moderate levels of vehicular traffic. Secondary Streets may be mixed-use or more residential in character. The Build-to Zone is generally shallow, and building heights are limited. In mixed-use areas, a continuous street wall should be maintained and sidewalks should be between 12 and 16 feet wide to accommodate pedestrian traffic. In residential areas, the required minimum façade width is limited – allowing for more space between buildings – and sidewalks may be narrower. Both tree wells and open landscaped planters are appropriate depending on sidewalk width.

Tertiary Street

Tertiary Streets are the less important than Primary and Secondary streets. They may function as “back of house” for buildings with multiple street frontages. Care should be taken to make these streets as pedestrian-friendly as possible while accommodating loading and access needs. Unless appropriately designed to share street space, an 8 foot sidewalk is a minimal dimension for walking accommodations in a highly urbanized area such as River North.

Other Street

Other Streets are streets that do not fall into any of the other street categories. They may have high or moderate levels of vehicular traffic, but often have no access to property and limited pedestrian activity. Building height along these streets is regulated by the other property frontages. Buildings do not front on these streets and may be built up to the property line.

Alley

Alleys are service roads that provide shared access to property. Public utilities as well as access to mechanical equipment and trash should be located off an alley whenever possible. Alleys are encouraged for access and loading.

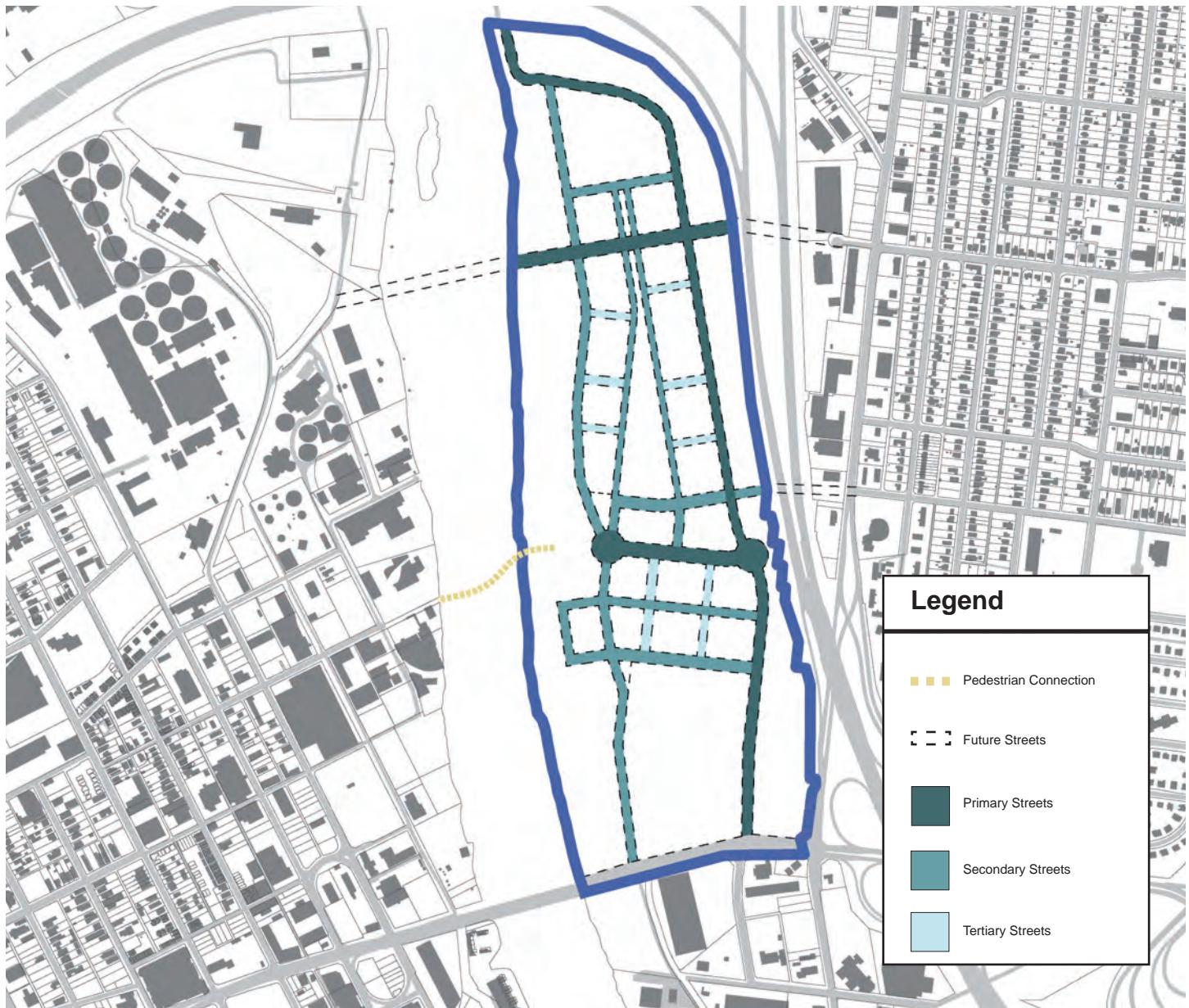
Sidewalk Corridor

The Sidewalk Corridor is the portion of the right-of way between the vehicular lanes and the property line or building façade.

- The primary function of the Sidewalk Corridor is to provide a safe, comfortable, and convenient route for pedestrian travel that is separated from vehicular movements.
- The Sidewalk Corridor is a public space that should include pedestrian amenities such as seating, shade trees, bike racks, places to congregate, trash and recycling receptacles and outdoor dining.
- The Sidewalk Corridor may accommodate public utilities such as electric poles and vaults, water and sewer lines, bus stops and traffic signals.
- The Sidewalk Corridor may also accommodate separated bikeway facilities by providing protection to cyclists from traffic. This may be achieved by an adjacent grass strip or planting zone and may function as a dedicated facility meant for cyclists only, or mixed with pedestrian traffic like a multi-use path.
- As property develops, property owners shall consult with Metro Planning and Public Works to make the necessary improvements to the streetscape in accordance with the *Major and Collector Street Plan* and the *Strategic Plan for Sidewalks*.

Section III: General Standards

Street Character: Future Streets



Proposed Street Network

Section III: General Standards

Street Character: Future Streets

Future Streets

This area will see significant growth and change over the next few years. The Future Streets Plan show how streets could be realigned, connected and created in the future to improve mobility within the area.

Properties near an area highlighted for change on the Future Streets Plan shall consult with the Planning Department and the Department of Public Works to discuss the potential change.

Any future street listed in the UDO as a future street can be moved or realigned prior to construction and the designation for that street can be changed. When a street is moved, relocated or the designation is changed prior to construction this is a modification that may be approved by the Planning Department with a recommendation from Public Works.

Section III: General Standards

Street Character

Street Trees

Shade-producing street trees shall be planted in the public right-of-way along the length of the lot frontage at a maximum spacing of forty feet or in accordance with the regulations of Metro departments and agencies.

Tree Quality

Tree species shall be chosen from the Urban Forestry Recommended and Prohibited Tree and Shrub List based on tree size and planting area provided or an alternative species deemed appropriate by the Urban Forester.

- At planting trees, shall meet the requirements for street trees set out in the American Standard for Nursery Stock.
- All nursery stock used as street trees shall be vigorous, healthy and free of diseases or infestation.
- No species considered invasive in the project's context according to USDA or other state agriculture services shall be allowed.
- Planting Area Dimension
 - The following standards are minimum standards. All development is encouraged to provide street trees with the largest area of pervious surface and volume of soil that can be accommodated.
 - Trees shall be accommodated in planting areas that follow Metro Public Works' *Street Tree Standards and Specifications*.
 - The minimum pervious opening at grade shall be 24 square feet.
 - Tree vaults shall have the capability to drain water.
 - Planting areas shall not inhibit ingress/egress from buildings or pedestrian traffic along the Sidewalk Corridor.

Section III: General Standards

Parking and Access: General

Parking and Access: General

- No parking is required within the boundaries of the UDO.
- No onsite parking is allowed between the street and the building.

Parking and Access General Standards

- 17.20.050 Handicapped Parking, 17.20.060 Parking area design standards, and 17.20.130 Loading space requirements shall apply.

Valet and drop-off areas

- They shall be located within the right of way when space allows. If not provided in the right of way they shall be located internal to the development.
- Where driveways to parking facilities or drop off areas cross the Sidewalk Corridor, priority should be given to the pedestrian realm and the following shall be required:
 - The UDO and the MCSP sidewalks and tree planting standards shall be maintained for any pedestrian island that is created.
 - Bollards or other devices shall be used to separate the pedestrian and vehicular areas.
 - Distinction behind vehicular lane and pedestrian areas shall be indicated through changes in grade, color, texture and/or material.
- Curbside management plans are required. Consolidation of drop-off locations to a single location for multiple properties is highly recommended.

Stormwater

- Utilize LDI strategies in Metro Water Services Stormwater BMPs for hardscape including parking and drive lanes.
- Prior to Final Site Plan approval, projects must demonstrate stormwater and flood mitigation design, and floodplain management.

Section III: General Standards

Parking and Access: Specific to Structured Parking

Vehicular Access

- Vehicular openings to parking structures shall not exceed thirty-five feet in width.
- Vehicular openings shall have a minimum spacing of thirty five feet.

Pedestrian Access

- All parking structures shall have a clearly marked pedestrian entrance, separate from vehicular access, on street frontages. A publicly accessible building lobby may meet this requirement.

Location and Lining

- On the ground level, parking structures shall be located behind a liner building with an active use that is a minimum of 15 feet deep.
- Where no ground level liner is provided (due to modifications or other reasons), facade treatment/cladding shall be required on all street, open space, and pedestrian ways. Cladding shall help to activate the street level with its design cues that integrate with the architectural characteristics of the habitable portion of the building, and of the surrounding built context. Openings for natural ventilation are permissible when well integrated into the facade design.
- Upper level habitable liners are encouraged on all streets. See the Bonus Height Program for more information on bonuses for Upper Level Garage Liners.
- Upper level facade treatments /cladding is required on all street, open space and pedestrian ways (such as greenways frontages, including any portions of facades visible from a given frontage, including Interstate frontages. Facade treatments shall integrate or complement the architectural characteristics of the habitable portion of the building and the surrounding built context. Openings for natural ventilation are permissible when integrated into the facade design. Landscape buffering may be considered as an alternative at appropriate locations, such as Interstate frontages.
- Underground parking that is visible from the street, shall not extend beyond the façade of the building unless it is screened. Underground parking that is completely below grade may extend beyond the façade of the building. Underground parking may not encroach into the right-of-way.

Section III: General Standards

Parking and Access: Specific to Surface Parking

General Standards for Surface Parking

- Parking area screening and landscaping standards shall apply to all surface parking lots including, but not limited to, public and private parking facilities, driveways and access aisles, the outdoor display of automobiles and other vehicles that are for sale or lease.
- Surface Parking is best suited at the side or rear of a building, leaving the building frontage facing the circulation route.

Perimeter Screening Standards for Surface Parking

- Parking areas adjacent to public streets and open space shall be separated from the edge of the right-of-way and/or easements and property lines by a perimeter landscape strip a minimum of five feet in width which shall be landscaped per the standards of this section.
 - All perimeter landscape strips adjacent to public streets and open space shall include a transparent fence or knee wall in accordance with the Fence and Wall Standards.
- Parking areas shall be separated from adjacent side lot lines (with the exception of cross-access points) by a perimeter landscape strip a minimum of 5 feet in width, which shall be landscaped per the standards of this section.
 - A two and one-half foot landscape strip may be provided if the required trees are to be planted in tree islands located adjacent to the property line.
 - Two adjacent properties may share equally in the establishment of a 5 foot (minimum) planting strip along the common property line. In instances where the common perimeter planting strip is part of a plan for shared access, each owner may count the respective area contributed toward that common planting strip toward the interior planting area requirements for the lot. Conversely, a shared parking lot across property lines may be developed with no side lot perimeter planting strip, dependent upon the design and functional use of the space.
- Surface Parking Lots shall provide cross-access to all adjacent development and parking lots.

Interior Planting Requirements

- Parking areas shall be landscaped in accordance with the interior planting requirements of Title 17.24.160.
- Parking areas with less than twelve thousand square feet in total area shall be exempt from the interior and side lot line planting requirements.

Landscape Materials

- Perimeter landscape strips along public streets, open space and side lot lines.
 - Trees shall be installed at a rate of one tree for every thirty feet of frontage. Spacing may be adjusted with the approval of the Urban Forester based upon tree species, the presence of utilities, and the dimensions of the planting strip.
 - Evergreen shrubs and trees shall be installed at appropriate spacing to fully screen vehicles to a minimum height of two and one-half feet.
 - Plantings within fifteen feet of driveways or street intersections shall be maintained to a maximum height of two and one-half feet.
 - Plantings shall not obstruct views onto site as to impede the security of users.
- Tree and shrub species shall be chosen from the Urban Forestry Recommended and Prohibited Tree and Shrub List or an alternative species deemed appropriate by the Urban Forester.
- At planting, trees shall be a minimum of six feet in height and two caliper inches.
- All landscaping shall be in a functioning bio-swale, or irrigated using drip irrigation or sub-surface irrigation. If drought-tolerant species are used, no irrigation is required.
- At planting, all landscaping shall meet the standards for size, form and quality set out in the American Standard for Nursery Stock (ANSI Z60.1, latest edition).
- All nursery stock shall be vigorous, healthy and free of diseases or infestation.

Section III: General Standards

Mechanical, Service, and Loading

Applicability

The following elements shall be shielded from view from adjacent public streets, pedestrian corridors, and open spaces.

- Refuse collection, dumpsters, recycling bins, and refuse handling areas that accommodate a dumpster or five or more trash or recycling cans.
- Building or ground-mounted mechanical equipment, including, but not limited, to transformers, back-flow preventors, telephone risers, equipment cabinets, generators, or similar devices.
- Mechanical equipment on roofs shall be fully screened.
- Air conditioning or similar HVAC equipment.
- Loading docks, berths, or similar spaces including, but not limited to, service entrances and maintenance areas.
- Outdoor storage of materials, equipment, and vehicles.

Location and Access

- Applicable site elements shall be located along the alley, along an interior property line, or internal to the property.
- Service elements, such as loading docks and trash collection locations, shall not be accessible from Primary Streets unless a Primary Street is the only frontage.
- Vehicular or service bay openings shall make up no more than 20% of the total frontage length along Primary Streets, Secondary Streets, or Open Space frontages.
- Where access to loading areas and service elements cross the Sidewalk Corridor, priority shall be given to the pedestrian realm and the following design elements shall be required:
 - The MCSP sidewalks and streetscape standards shall be maintained for any pedestrian islands or indentations created.
 - Bollards or other protective device shall be used to separate pedestrian and vehicular areas.
 - Distinction between vehicular lane and pedestrian areas shall be indicated through changes in grade, color, texture and/or material.

Screening Standards

- Applicable site elements shall be fully screened at all times.
- Refuse collection and refuse handling areas shall be screened by a walled enclosure with gates in accordance with the Fence and Wall Standards of the UDO.

Section III: General Standards

Mechanical, Service, and Loading

Screening Methods

- Vegetative Materials:
 - Vegetative materials shall be planted in two rows in staggered fashion.
 - All trees shall be evergreen with a minimum height at time of planting of at least six feet above the root ball.
 - All shrubs shall be evergreen with the minimum height and spacing necessary to fully screen the item intended for screening (but no less than thirty inches in height) at the time of planting.
 - Vegetative material shall be located immediately adjacent to the element being screened in a planting area a minimum of four feet wide.
- Fencing and Walls
 - Screening is permitted through the use of a fence or wall constructed in accordance with the Fences and Walls Standards of the River North UDO.
- Mechanical Penthouse
 - Rooftop mechanical areas must be fully visually screened.
 - Penthouse height limited to 20'.
 - Penthouse must be setback from the edge of the building roof below, by a distance equal to the penthouse height (1:1)
 - Penthouse walls and design shall minimize its visual impact, and be otherwise complementary to the building's architecture and design.
 - Habitable space is not permitted.
- Parapet Walls
 - Parapet walls or other techniques included as an integral part of the building design shall be used to totally screen any rooftop mechanical equipment from view from adjacent public rights-of-way or open space.
- Integrated Building Elements or Features
 - Building design or other structural features (e.g., knee walls, alcoves, wing walls, roof extensions, etc.) may also be used to fully or partially enclose site features required to be screened.
- Alternative Screening Methods
 - Alternative screening methods or materials that are not listed may be used following approval by the Planning Commission or its designee, provided that they are determined to be comparable to screening methods described in this subsection.

** In order to properly locate and screen mechanical equipment, approval may be required from applicable Metro departments and agencies.

Section III: General Standards

Fences and Walls

Location

- Permitted Locations: Fences and walls constructed in accordance with the standards in this section may be constructed within:
 - The Build-to Zone.
 - A utility easement only through the express written consent from the utility or entity holding the easement.
 - A required landscape area, Tree Protection Zone, or open space.
- Prohibited Locations: No fence or wall shall be installed that:
 - Encroaches into a right-of-way (without approval through the Mandatory Referral process).
 - Blocks or diverts a natural drainage flow on to or off of any other land.
 - Compromises safety by blocking vision at street intersections or obstructs the visibility of vehicles entering or leaving driveways or alleys.
 - Blocks access to any above ground or pad-mounted electrical transformer, equipment vault, fire hydrant or similar device.

Appearance

- All fences shall be installed so that the finished side shall face outward; all bracing shall be on the inside of the fence.
- Fences and walls shall be constructed of any combination of brick, stone, masonry materials, treated wood posts and planks, rot-resistant wood, metal, and wear resistant nonglossy plastics and recycled materials. Chain link fencing shall be coated with dark colored vinyl when visible from a public street or open space (excluding alleys).
- Chain-link fences are prohibited along street and open space frontages (including along greenways or multi-use trails).
- Razor wire is prohibited.
- Fences and walls used to screen refuse areas shall be opaque and include gates that prohibit unauthorized users to access the area.

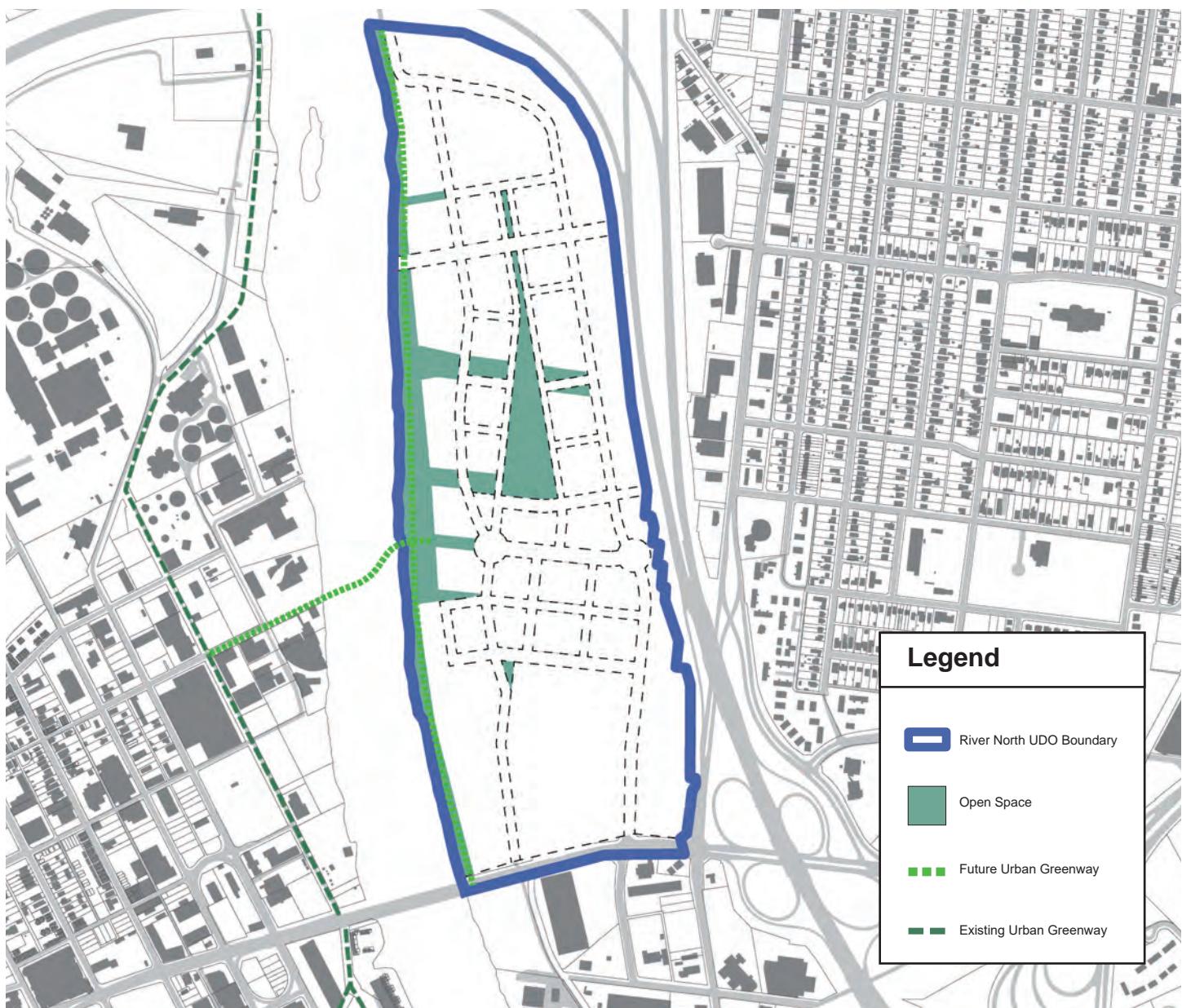
Standards by function and location

- Fences and walls within the Build-to Zone shall not exceed four feet in height.
 - Modifications may be made in order to properly secure playgrounds and parks.
 - The height of fences and walls along a sidewalk shall be measured from sidewalk grade.
- Fences and walls within the Build-to Zone that are greater than three feet high shall be a minimum of thirty percent transparent to allow visibility into the property.
- Fences and walls used to screen parking shall be a minimum of two and one-half feet above the grade of the parking lot.
 - When a fence or wall is combined with plantings the majority of the plantings shall be between the right-of-way and the fence or wall.
- Fences and walls used to screen mechanical, loading and refuse elements shall be a minimum of two feet taller than the element being screened.
- All other fences and walls shall have a maximum height of ten feet measured from grade.
- Fences surrounding athletic fields and courts may exceed the previous height.

Section III: General Standards

Open Space Plan

The design of River North accommodates a variety of formal parks and open spaces as focal points within the community. The Open Space Plan depicts formal greens, squares, and linear parks that create publicly accessible settings for outdoor enjoyment. All of these spaces will be linked by a network of sidewalks, multi-purpose paths, walkable lanes, and bikeways, allowing continuous, non-motorized movement throughout the site, through a sequence of quality open-air environments that ultimately lead to the Cumberland River or a proposed “Central Park” within the center of the neighborhood. Buildings, streets, and parcels should generally be oriented toward open spaces to encourage safe interactive use.



Open Space Plan

Section III: General Standards

Open Space: General Standards

Open Spaces

Actual detailed plans, design, and locations of River North open spaces, parks, greenways, and green connections may vary, subject to constraints and conditions as yet to be determined. However, all proposed open spaces and/or alternatives must be consistent with the intent of the Open Space Plan and UDO.

“Central Park”

A centrally located park, consisting of a minimum of two contiguous acres shall be located with the UDO boundary. The park space shall allow for public gathering and recreation, with activated uses along its edges.

Riverfront Greenway

A north-south greenway with a linear park space will be provided along the riverfront of the Cumberland River. Recreation opportunities, outdoor dining, overlooks, wayfinding, and other interactive programming are appropriate components.

Green Connections

Green connections will link the riverfront greenway and linear park space to the internal open space network and “Central Park” of the larger UDO area. Such connections may serve multiple purposes, but shall facilitate the movement of pedestrians through the open spaces of the UDO.

Modifications may be made in order to properly secure Standards of Title 17 not varied by the following Open Space Standards shall apply within the UDO.

Access

- Every open space shall have a minimum of one primary pedestrian entrance along each street frontage and pedestrian frontage.
- All publicly accessible open space shall meet the appropriate standards of the American's with Disabilities Act.

Paving Materials

- Asphalt may be approved by the Planning Commission or its designee for recreational jogging or bicycle paths only.

Landscaping

- Planting areas shall not impede ingress/egress from buildings or pedestrian traffic.
- Tree and shrub species shall be chosen from the Urban Forestry Recommended and Prohibited Tree and Shrub List based on tree size and planting area provided or an alternative species deemed appropriate by the Urban Forester.

Section III: General Standards

Bonus Height Program

The Bonus Height Program allows additional building height in the River North UDO in exchange for contribution to specified programs that provide benefits to the public. The additional building height shall be entitled if the proposed development contributes to specific public benefits in the amount and manner set forth herein.

Bonus Height Standards

- Upon providing a binding commitment for the specified public benefit, the proposed development project shall be allowed to build within the restrictions of the Subdistrict, up to the Bonus Height Maximum as established within this section.
- Multiple height bonuses may be compounded insofar as the total additional height does not exceed the Bonus Height Maximum for the Subdistrict.
- Additional development rights achieved through the BHP may be transferred to other sites within the UDO, one time to one receiving site, provided the transferred height does not exceed the Bonus Height Maximum of the receiving site. By right height may not be transferred; only bonus height received through the BHP may be transferred.
- Bonus height transfers shall be based on the square footage of the sending site, not the receiving site.
- No building permit shall be issued for bonus height until the Planning Commission has certified compliance with the provisions of this section, upon referral and assurance of compliance from applicable departments.

Bonus Height Chart

| Subdistrict | One | Two |
|-----------------------------|-----------------------------------------------------------|---------------------------------------------------------------|
| Subdistrict Height | 15 stories | 25 stories |
| BONUSES | | |
| LEED Building | Silver = 1 story; Gold = 1 story; Platinum = 2 stories | Silver = 2 stories; Gold = 2 stories; Platinum = 3 stories |
| LEED ND | 2 stories | 2 stories |
| Pervious Surface | 1 story | 2 stories |
| Upper Level Garage Liner | 1 story | 4 stories |
| Underground Parking | 1 story | 3 stories |
| Public Parking | No Bonus | 2 stories |
| Adaptable Garage Levels | 2 stories | 8 stories |
| Shared Parking | No Bonus | 1 story |
| Civil Support Space | 1 story | 2 stories |
| Public Open Space | 2 stories | 8 stories |
| Public Greenway | 2 stories | 4 stories |
| Inclusionary Housing | 3 stories | 10 stories |
| Maximum Bonus Height | 18 stories | 38 stories |

Section III: General Standards

Bonus Height Program

LEED and LEED ND

The U.S. Green Building Council (USGBC) is a non-profit organization that oversees the Leadership in Energy and Environmental Design (LEED) Green Building Rating System.

LEED for Neighborhood Development integrates the principles of smart growth, urbanism and green building into the first national system for neighborhood design. LEED ND goes beyond the building to address sustainability on a neighborhood-wide basis.

The bonuses are specific to each Subdistrict. See the BHP Chart for details.

A different nationally-recognized, third-party system of overseeing green building and/or sustainable development practices may be substituted for LEED. Bonuses will be determined by the Planning Commission based on ratings equivalent to LEED silver, gold, and platinum.

Bonuses for individual buildings are given upon pre-certification of LEED silver, gold and platinum. Bonuses for neighborhoods are given upon pre-certification of LEED ND. Every property within the LEED ND neighborhood may utilize the bonus height. The bonuses are specific to each Subdistrict. See the BHP Chart for details.

The following shall apply to all new construction that utilizes the Bonus Height Program for LEED:

- Prior to issuance of a temporary certificate of occupancy for any use of the development, a report shall be provided for the review of the Department of Codes Administration and the Planning Commission by a LEED accredited professional. The report shall certify that all construction practices and building materials used in the construction are in compliance with the LEED certified plans and shall report on the likelihood of certification. If certification appears likely, temporary certificates of occupancy (as set forth below) may be issued. Monthly reports shall be provided as to the status of certification and the steps being taken

to achieve certification. Once certification is achieved, the initial certificate of LEED compliance, as set forth herein, and a final certificate of occupancy (assuming all other applicable conditions are satisfied) shall be issued.

- To ensure that LEED certification is attained the Department of Codes Administration is authorized to issue a temporary certificate of occupancy once the building is otherwise completed for occupancy and prior to attainment of LEED certification. A temporary certificate of occupancy shall be for a period not to exceed three (3) months (with a maximum of two extensions) to allow necessary time to achieve final certification. Fees for the temporary certificate (and a maximum of two extensions) shall be \$100 or as may otherwise be set by the Metro Council. Once two extensions of the temporary certificate of occupancy are granted, any additional extensions shall be granted only in conjunction with a valid certificate of LEED noncompliance as set forth herein.
- If the property fails to achieve LEED certification, the Department of Codes Administration is authorized to issue a short-term certificate of LEED noncompliance. This certificate will allow the building to retain its certificate of occupancy pending attainment of LEED certification. A certificate of LEED noncompliance shall be for a period not to exceed three (3) months and may be renewed as necessary to achieve certification. The fee for noncompliance shall be issued every time the certificate is issued for up to ten years.
- The fee for a certificate of LEED noncompliance shall be based on the following formula: $F = [(CN-CE)/CN] \times CV \times 0.0075$, where:
 - F is the fee;
 - CN is the minimum number of credits to earn the level of LEED certification for which the project was pre-certified;
 - CE is the number of credits earned as documented by the report; and
 - CV is the Construction Value as set forth on the building permit for the structure.

Section III: General Standards

Bonus Height Program

Pervious Surface

The integration of pervious surfaces into site design and building design benefits the individual development, the neighborhood and the city. Pervious surfaces can reduce stormwater runoff, flood risk, irrigation needs and the burden on infrastructure. Examples of pervious surfaces include pervious pavement, green roofs, bio-swales, landscaping, and green screens. As technology in this field advances, additional pervious surfaces may meet the intent of this standard.

- The number of square feet of Bonus Height shall be twice that of the number of square feet of Pervious Surface. The additional square footage may be used to the Bonus Height Maximum as determined on the BHP Chart.
- Green roofs that are utilized to meet LEED certification may not be “double counted” for both the LEED height bonus and the Pervious Surface height bonus. If the level of LEED certification would be met without the green roof, then the green roof may be counted for the Pervious Surface height bonus.
- Pervious Surfaces may not be double counted if used towards the Public Open Space or Public Greenway Bonuses.

Upper Level Garage Liner

The public realm of the streetscape is improved by lining above ground parking structures with habitable space. See the BHP Chart for a list of Subdistricts in which the Upper Level Garage Liner bonus may be utilized.

- Height bonuses are given for upper levels of habitable space, a minimum of 15' in depth, which masks a parking structure from view along streets or open space (including greenways and multi-use trails).
- The number of square feet of Bonus Height shall be twice that of the number of square feet in Garage Liners. The additional square footage may be used to the Bonus Height Maximum as determined on the BHP Chart.

Underground Parking

The public realm of the streetscape is improved by providing parking in underground structures. See the BHP Chart for a list of Subdistricts in which the Underground Parking bonus may be utilized.

- The number of square feet of Bonus Height shall be equal to the number of square feet in Underground Parking. The additional square footage may be used to the Bonus Height Maximum as determined on the BHP Chart.
- Height bonuses are not given for ground level liners, or upper level liners that are required by the UDO.

Public Parking

Parking accessible to the general public is important to the continued growth and vitality of Downtown. See the BHP Chart for a list of Subdistricts in which the Public Parking bonuses may be utilized.

- The number of square feet of Bonus Height shall be twice that of the number of square feet in Public Parking. The additional square footage may be used to the Bonus Height Maximum as determined on the BHP Chart.
- Public Parking shall be clearly marked as public, and shall be accessible to the public, at all hours that the garage is open, for the lifetime of the building.

Section III: General Standards

Bonus Height Program

Adaptable Garage Levels

Parking Garages built to accommodate future uses, with a ceiling height of 11 feet or greater, are encouraged and desired. See the BHP Chart for a list of Subdistricts in which the Adaptable Garage Levels bonus may be utilized.

- The number of square feet of Bonus Height shall be twice that of the number of square feet in the Parking Garage, so long as the garage is designed with 11 foot high ceilings or greater and an Architect has provided a letter to Planning asserting that the garage can be easily converted to an alternative use if parking is no longer needed or desired. The additional square footage may be used to the Bonus Height Maximum as determined on the BHP Chart.
- Underground parking levels are not applicable for the Adaptable Garage Levels Bonus.

Shared Parking

Shared Parking provides opportunities for businesses and establishments to consolidate parking needs, thereby consuming less physical space to satisfy their joint parking demands. In addition, Shared Parking can consist of Park and Ride, or dedicated car-sharing spaces. See the BHP Chart for a list of Subdistricts in which the Shared Parking Bonus may be utilized:

- The number of square feet of Bonus Height shall be equal to twice the number of square feet in Shared Parking (including Park and Ride or car sharing lots). The additional square footage may be used to the Bonus Height Maximum as determined on the BHP Chart.
- Shared Parking must demonstrate that the parking results in less parking spaces than would typically be provided as individual allocations.
- Parking agreements must be recorded and remain in place for the lifetime of the buildings.
- Park and Ride and car sharing options must demonstrate acceptance by all applicable entities including Metro Departments.

Civil Support Space

The dedication of Civil Support Space offers height bonus for the developer's contribution of space to a specific use or entity that serves to better the neighborhood or community. See the BHP Chart for details for a list of Subdistricts in which the Civil Support Space bonus may be utilized.

- Civil Support Space is typically on the ground level. Upper levels may be appropriate depending on the intended use.
- The number of square feet of Bonus Height shall be twice that of the number of square feet donated to Civil Support Space. The additional square footage may be used to the Bonus Height Maximum as determined on the BHP Chart.
- Civil Support Space shall be dedicated to the chosen use or uses for 15 years. Adherence to this standard shall be checked yearly by the Planning Commission or its designee.

The Planning Commission may require the developer to execute an agreement, restrictive covenant, or other binding restriction on land use that preserves the use of Civil Support Space for the required period before final site plan review.

The following are examples appropriate for Civil Support Spaces:

- Institutional Uses
 - Cultural center
 - Day care center
 - School day care
- Education
 - Community education
- Transportation Uses
 - Transit Center
- Waste Management Uses
 - Recycling collection center
- Recreational, Civic, or Entertainment Uses
 - Community playground
- Other Uses
 - Community garden

Other uses may be appropriate for Civil Support Space. The applicant may propose a different use for Civil Support Space to be approved by the Executive Director.

Section III: General Standards

Bonus Height Program

Public Open Space

Open Space accessible to the general public is critical to the continued health and vitality of River North. See the BHP Chart for a list of Subdistricts in which the Public Open Space bonus may be utilized.

- The number of square feet of Bonus Height shall be seven times that of the number of square feet in Public Open Space. The additional square footage may be used or transferred to the Bonus Height Maximum as determined on the BHP Chart.
- Public Open Space may be provided on the property being developed, or on another property within the UDO. In the latter case, the derived bonus shall be transferred from the Open Space Site to the Development Site.
- Public Open Space shall be clearly marked as public, and shall be accessible to the public, at all hours that the open space is open, in perpetuity.
- In order to qualify for the bonus, all of the following requirements shall be met:
 - Minimum contiguous area of $\frac{1}{4}$ acre.
 - Accessible to the public through a secured public easement, dedication, or agreement with Metro Parks or a Metro approved third party trust.

Public Greenway

Greenways and multi-use paths serve a key dual function: to provide recreational enjoyment for River North, and to provide increased connectivity to destinations in East Nashville that provides a critical alternative mode of transportation for residents and visitors to navigate the surrounding area without the need of a car. See the BHP Chart for a list of Subdistricts in which the Public Greenway bonus may be utilized.

- The number of square feet of Bonus Height shall be 50 times that of the number of linear feet in Public Greenway / multi-use path dedicated. The additional square footage may be used to the Bonus Height Maximum as determined on the BHP Chart.
- Public Greenways requires the dedication of land to Metro (or acceptance of a permanent public easement) for the explicit use of Greenways/multi-use paths.
- In order to qualify for the bonus, all of the following requirements shall be met:
 - Accessible to the public through a secured public easement, dedication, or agreement with Metro Parks.
 - When feasible, pedestrian linkages shall be provided to adjacent neighborhoods and developments.
 - Proposed buildings abutting the Greenway or multiuse path shall include ground level active uses, with at least one direct pedestrian entrance.

Inclusionary Housing

- Bonus Height is available for compliance with Section 17.40.780 of the Zoning Code as shown in the Bonus Height Program Chart.

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Appendix

OCTOBER 2017

DEVELOPMENT CAPACITY EVALUATION STUDY

RIVER NORTH
NASHVILLE, TENNESSEE

PREPARED FOR:
MONROE INVESTMENT PARTNERS, LLC



1101 17TH AVENUE SOUTH
NASHVILLE, TENNESSEE 37212

**DEVELOPMENT CAPACITY EVALUATION STUDY
RIVER NORTH
NASHVILLE, TENNESSEE**

**PREPARED FOR:
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EXECUTIVE SUMMARY

Project Description

The planned River North project proposes the development of approximately 125 acres on the east side of Cumberland River between Jefferson Street and I-24 and I-65 in downtown Nashville. This study evaluates the high-level impacts of the southern 40 acres of the development, which the study will refer to as Phase 1. The traffic analysis is based on more density than is currently contemplated by the developer. Given variables such as local demand and overall economy, it is prudent to underwrite conservatively.

Phase 1 of the development, as considered for this analysis, includes a total of approximately three (3) million square feet of office space, 1,735 residential units, 285,000 square feet of retail/restaurant space, 550 hotel rooms and 186,500 square feet of civic space. While Phase 1 consists of 40 acres and could take 15 years or more depending on economic cycles, and zoning permits significant density, it is anticipated that the entirety of the development will be completed in multiple phases that could take 30 years or more to complete.

The master plan proposes a variety of new roadway extensions, bridges, interchanges and access connections to the interstate system as well as to existing streets. Therefore, the purpose of this study is to evaluate the feasibility and desirability of these access improvements and to determine maximum newly generated traffic that can be managed under low, medium, and high levels of roadways improvements based on these evaluations. Finally, potential transportation strategies were explored and are recommended in order to achieve higher density for the proposed development by improving the overall local and regional mobility of the area.

Data Collection

In order to provide data for the traffic impact analysis, manual traffic counts were conducted at the following intersections:

1. Jefferson Street/Spring Street and Cowan Street
2. Spring Street and North 1st Street
3. Spring Street and Dickerson Pike
4. I-24 On & Off-Ramps at Spring Street
5. I-24 Eastbound Off-ramp at North 1st Street

Traffic counts for the study intersections were conducted in June 2016 by KCI. Specifically, the turning movement counts were conducted from 7:00 – 9:00 AM and 4:00 – 6:00 PM on a typical weekday in June 2016. From the counts, it was determined that the peak hours of traffic flow for the study intersections occurred from 8:00 – 9:00 AM and 4:00 – 5:00 PM.

Evaluations

Various combinations of the potential improvements within the study area were developed. Directional distributions of traffic generated by the proposed project were then established based on the proposed access connections under each scenario and the existing travel patterns developed from the existing peak hour traffic counts.

For the purpose of this study and based on the capacity analysis it was determined that the intersection of Jefferson Street/Spring Street and Cowan Street is the control intersection for the sensitivity analysis. In addition, the proposed development has higher impacts at that intersection during the PM peak hour when compared to the AM peak hour. As a result, for the sensitivity analysis, capacity analyses were conducted at the intersection of Jefferson Street/Spring Street and Cowan Street during the PM peak hour under each of the various scenarios. Finally, the maximum new trip-generated traffic volumes by the proposed development (based on the PM peak hour volumes) which can be accommodated under each scenario were presented.

Conclusions and Recommendations

A review was conducted of the roadway extensions, bridges and interstate access connections that are proposed as part of the River North master plan. Sensitivity analyses were also conducted to estimate the maximum expected newly generated trips by the proposed development, which can be managed by implementing those conceptual improvements within different stages. The suggested improvements are categorized as Low Level, Medium Level, and High Level. Conclusions of the reviews and analyses are as follows:

- The Cleveland Street extension and a connection across I-24 make a significant connection to the East Nashville area and will provide access to Dickerson Pike, Whites Creek Pike, Ellington Parkway (US 31E) and Gallatin Pike. Cleveland Street has a four-lane cross-section from Dickerson Pike to east of Ellington Parkway. Utilizing the highest PM peak hour trip generation (Option 4B) and the associated distribution, the Cleveland Street extension has the potential to add approximately 1,000 PM peak hour trips along the corridor; this serves as a

significant increase over the 9,000 vpd currently served by the corridor. There are currently two (2) all-way stop controlled intersections along this portion of Cleveland Street, located at Meridian Street and Lischey Avenue. Improvements will likely be necessary at these intersections, at the Ellington Parkway ramps, and potentially at other intersections along the corridor when the Cleveland Street extension is constructed.

- Previous versions of the River North master plan included new on and off ramps to I-65 and I-24. Interchange modifications and/or new connections to the interstate system require both state and federal approval and there are strict standards regarding minimum spacing between ramps that must be met in order to obtain the necessary approvals. State and federal approval of any new interstate access is likely to require considerable modifications to the existing interchanges including the employment of one or more strategies to eliminate weaving on the interstate. These strategies include the addition of collector-distributor roads or grade separated ramps (ramp braids). Requirements for these type of freeway modifications are described in the NCHRP 687 report, *Guidelines for Ramp and Interchange Spacing*. Specific details regarding the operations and feasibility of any interchange modifications or additional access points will need to be evaluated more thoroughly before understanding the feasibility of such improvements.
- The two proposed bridges over the Cumberland River have the potential to significantly improve access and provide alternative routes that would help lessen the impact of the project on the interstate system and on Jefferson Street/Spring Street. The current master plan illustrates the northern bridge as a vehicular and multimodal bridge and the southern bridge as a pedestrian and bicycle only bridge. It would be desirable for at least one of the bridges to have significant transit carrying capabilities.
- Consideration should be given to connecting the northern Cumberland River bridge to 3rd Avenue as well to provide more accessibility to and from north Nashville.
- A potential connection to Oldham Street has been discussed during the development of the masterplan. This connection would create a new north/south connection for project related traffic that may relieve development related traffic at the intersection of Jefferson Street/Spring Street and Cowan Street. The effectiveness of this connection could be further supported by

improvements to South 1st Street, which provides access to Woodland Street to the south.

- The Grace Street extension and a connection across I-24 will provide a convenient connection to East Nashville and to Meridian Street, a north/south collector street. In addition, the Grace Street extension has the potential to be a strong bicycle/pedestrian connection to the pedestrian/bicycle bridge over Ellington Parkway. It should be noted that this proposed improvement was not included in the capacity analysis, for the purpose of this study. It was assumed that a portion of the distributed traffic on the Cleveland Street connector would be distributed onto the Grace Street extension, which would result in the same reduction of traffic on Jefferson Street/Spring Street as without the implementation of this improvement.
- As previously described, the maximum full buildout of the southern 40 acres of the development is referred to as Phase 1 in this study. Improvement recommendations at the existing intersection of Jefferson Street/Spring Street and Cowan Street associated with , Phase 1 of the development were also evaluated and are described below.
 - Add additional turning lanes at the intersection of Jefferson Street and Cowan Street such that southbound Cowan Street consists of two or three left-turn lanes, a shared through/right lane and a right-turn lane. Further, an additional westbound lane will enhance capacity at this intersection. A right-turn lane with sufficient storage is recommended on the eastbound approach of Jefferson Street as well. It may be necessary to widen the eastern portion of the Jefferson Street bridge in order to add the recommended eastbound lane along Jefferson Street. Other feasible alternatives which may not require the widening of the bridge in order to accommodate additional eastbound travel lane, should also be considered and analyzed.
- The results of capacity analyses indicated that with low-level roadway improvements within the study area as described in the evaluation section, approximately 22% of the newly generated Phase 1 trips can be accommodated by the study area roadway system. Maximizing the density within the River North development is best accommodated with the high-level roadway improvements described previously in this study. Those improvements include the proposed new connectors/bridges with partial movement accesses to I-24 and/or I-65, providing an additional eastbound travel lane on Jefferson Street

and the I-24 bridge over Spring Street, and additional turning lanes on Cowan Street at Jefferson Street/Spring Street. It is estimated that 133% of the PM peak hour (5,940 vehicles per hour) for Phase 1 can be accommodated by implementing those improvements.

- It should be noted that intersections along Jefferson Street/Spring Street within the study area currently operate at or near capacity levels during peak times. Therefore, improving the operational performance and traffic flow of Jefferson Street/Spring Street within the study area is warranted as of today even without the completion of any stages of River North development. Any development along the east bank is likely to exacerbate this existing need, and access and capacity improvements will be needed to provide adequate traffic operations within the study area .
 - It should be noted that the thresholds of development identified in this study are based on trips that are projected to be generated by the development of the River North project. As the development of River North progresses, the land uses and sizes that are actually developed may be different than those assumed for this study. If this occurs, continuing to use PM peak hour trips as the warranting criteria for improvements will be an effective way to ensure that the recommended improvements are provided when needed.
 - The evaluation of the proposed improvements and estimation of the maximum newly generated trips for the proposed development under each phase can be used as a helpful tool to plan different stages of the development. However, the capacity analysis procedure used in this study was based on several assumptions. It is recommended that the development conduct traffic counts as certain portions of the development is being completed and occupied in order to identify actual trip generation for the developed portions of the River North development. Those counts will provide a stronger foundation to verify the assumptions made in this study and also to explore further improvements using the actual travel patterns in and out of the development.
 - It is important to note that traffic impact assumptions in this study are conservative, meaning analyses of network impacts were limited to the immediate vicinity of the development. Given the site's size and location adjacent to downtown and critical regional roadway junctions, impacts (positive or negative) will occur well beyond the site. Should more robust high-level improvements be constructed, such as additional bridge connections or interstate improvements, functionality of the greater network in this area may in fact improve. Neither TDOT nor Metro Nashville has significant infrastructure improvements planned for the near term in this area, and while new trips will

be added, these potential high-level improvements could provide alternative connections in the downtown area.

- Higher density for the proposed development may be achieved by emphasizing ride-share, and public transportation. Based on Mayor Barry's Transportation Action Agenda (Moving the Music City) plan, Metro Nashville, in partnership with TDOT, is developing a plan called Nashville Complete Trips. As part of the plan, Metro will promote other modes of transportation by reaching out to major employers and connecting employers and commuters to information about transportation options such as the transit and bikeshare systems, flex-scheduling and telecommuting, bike parking, and MTA/RTA park-and-ride locations. This plan would provide more opportunities for public-private partnerships by the proposed development. Such partnerships could be accomplished by providing private ride-share vehicles and/or sponsoring public transportation commutes for the employees. Upon the success of sponsoring other modes of commute, higher density for the proposed development could potentially be achieved with less traffic impacts on the roadway system.

1. INTRODUCTION

The purpose of this study is to evaluate the high-level traffic impacts associated with the southern 40 acres of the proposed River North development project, which the study will refer to as Phase 1, in Nashville, Tennessee. Specifically, a sensitivity analysis was conducted to estimate the maximum newly generated trips, which could be accommodated with the roadway network under various minor and major roadway improvements. The traffic analysis is based on more density than is currently contemplated by the developer. Given variables such as local demand and overall economy, it is prudent to underwrite conservatively.

The proposed 125-acre development will include a mix of land uses including office, retail, hotel, residential, and civic spaces. Currently, the plan for the Phase 1 of the development, as considered for this analysis, includes a total of approximately three (3) million square feet of office space, 1,735 residential units, 285,000 square feet of retail/restaurant space, 550 hotel rooms and 186,500 square feet of civic space. While Phase 1 consists of 40 acres and could take 15 years or more depending on economic cycles, and zoning permits significant density, it is anticipated that the entirety of the development will be completed in multiple phases that could take 30 years or more to complete.

The property is generally bound to the south by Jefferson Street, to the east by Interstate 24 (I-24), to the north by the Interstate 65 (I-65) northbound to I-24 eastbound ramp and on the west by the Cumberland River. Access to the development will be provided at multiple locations as indicated in the attached master plan (see Appendix).

The master plan proposes a variety of new roadway extensions, bridges, interchanges and access connections to the interstate system as well as to existing streets. Therefore, evaluations were conducted for the feasibility and desirability of these access improvements and based on these evaluations, maximum newly generated traffic that can be managed under low, medium, and high levels of roadways improvements were determined. Finally, potential transportation strategies were explored and are recommended in order to achieve higher density for the proposed development by improving the overall local and regional mobility of the area.

It should be noted that the purpose of this study is not to evaluate the traffic impacts associated with the proposed development at each individual intersection within the study area. Rather, this study intends to estimate the maximum new number

of vehicular trips that the whole roadway system in the study area can manage. To achieve that, a control intersection (Spring Street/Jefferson Street and Cowan Street) where the majority of the new trips will be assigned through, was selected and a sensitivity analysis during the worst peak hour (PM peak hour) was conducted to determine the highest manageable capacity at that intersection under various improvements scenarios. Therefore, the results of this study provides maximum newly generated hourly traffic volumes during the PM peak hour after typical internal capture and alternative modes reductions. This study does not provide any specific threshold for the land usage density. However, various land usage scenarios may be developed which generate hourly vehicular trips of equal or less than the maximum PM peak hour trips as estimated in this study.

2. PROJECT DESCRIPTION

The planned River North project proposes the development of approximately 125 acres on the east side of Cumberland River between Jefferson Street and I-24 and I-65 in downtown Nashville. As shown in Figure 1, the site sits just northeast of the Nashville Central Business District (CBD).

Table 1 provides a summary of the land uses and sizes based on Phase 1 of the proposed master plan, as considered in this study, and information provided by the developer team. The current master plan for the River North development is shown in Appendix A.

TABLE 1. PHASE 1 OF THE DEVELOPMENT PROGRAM

| LAND USE | SIZE |
|-------------------|-------------------|
| OFFICE | 3,029,000 SQ. FT. |
| RESIDENTIAL | 1,735 UNITS |
| HOTEL | 550 ROOMS |
| RETAIL/RESTAURANT | 258,000 SQ. FT. |

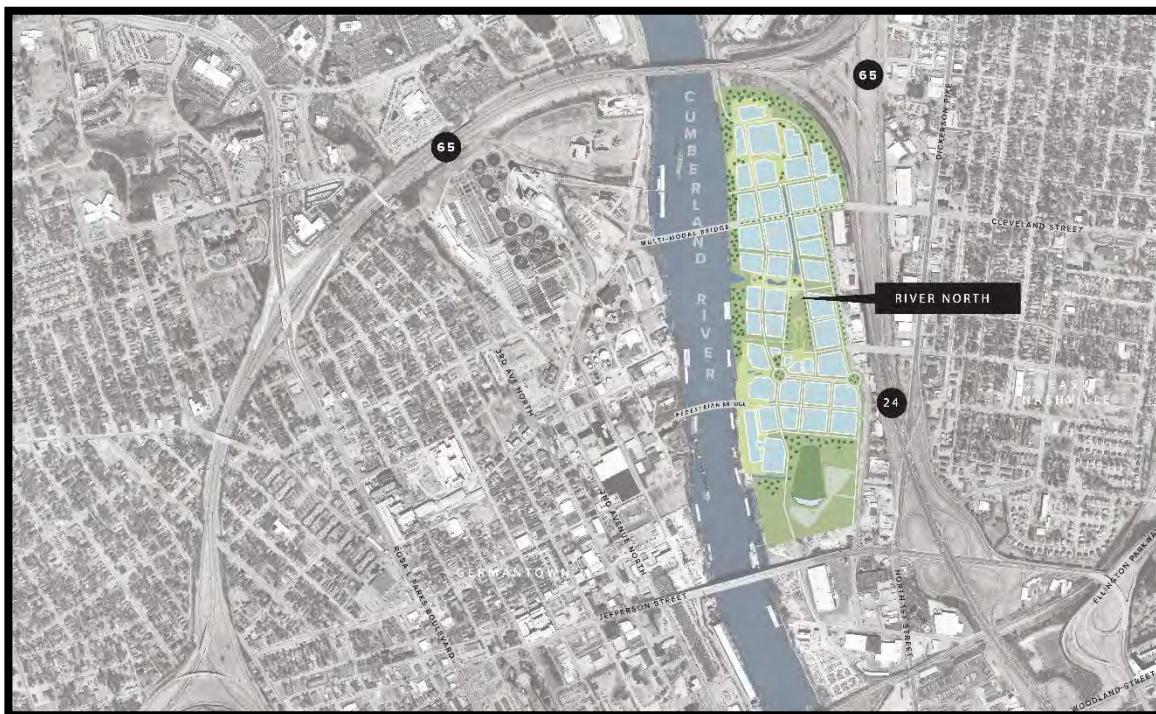


FIGURE 1. LOCATION OF THE PROJECT SITE

3. EXISTING SETTING

3.1 Regional and Local Access

The downtown interstate network consisting of Interstates 24 and 65 will provide regional access to the site. In the vicinity of the site, these six-lane freeway facilities form part of Nashville's "Inner Loop" that encircles the downtown area of Nashville. The nearest interchanges to the site are provided at Spring Street, just east of the site, James Robertson Parkway, located approximately one mile southeast of the site and Brick Church Pike, located approximately 1.5 miles north of the site. Additional regional roadways that provide access to the site are Ellington Parkway, a four-lane expressway, Jefferson Street/Spring Street, a four to six-lane major arterial street, and Dickerson Pike/North 1st Street, another four-lane major arterial street.

Cowan Street, Vashti Street and Brick Church Pike/Baptist World Center Drive will provide local access to the site. In addition, the proposed master plan includes connections across I-24 to connect with Cleveland Street and Grace Street, which are local east-west streets that provide connections to the McFerrin Park, Cleveland Park and East Nashville areas of Nashville. In addition, new multimodal and pedestrian bridges over Cumberland River are proposed in the master plan which will enhance the connectivity of Germantown and Downtown significantly.

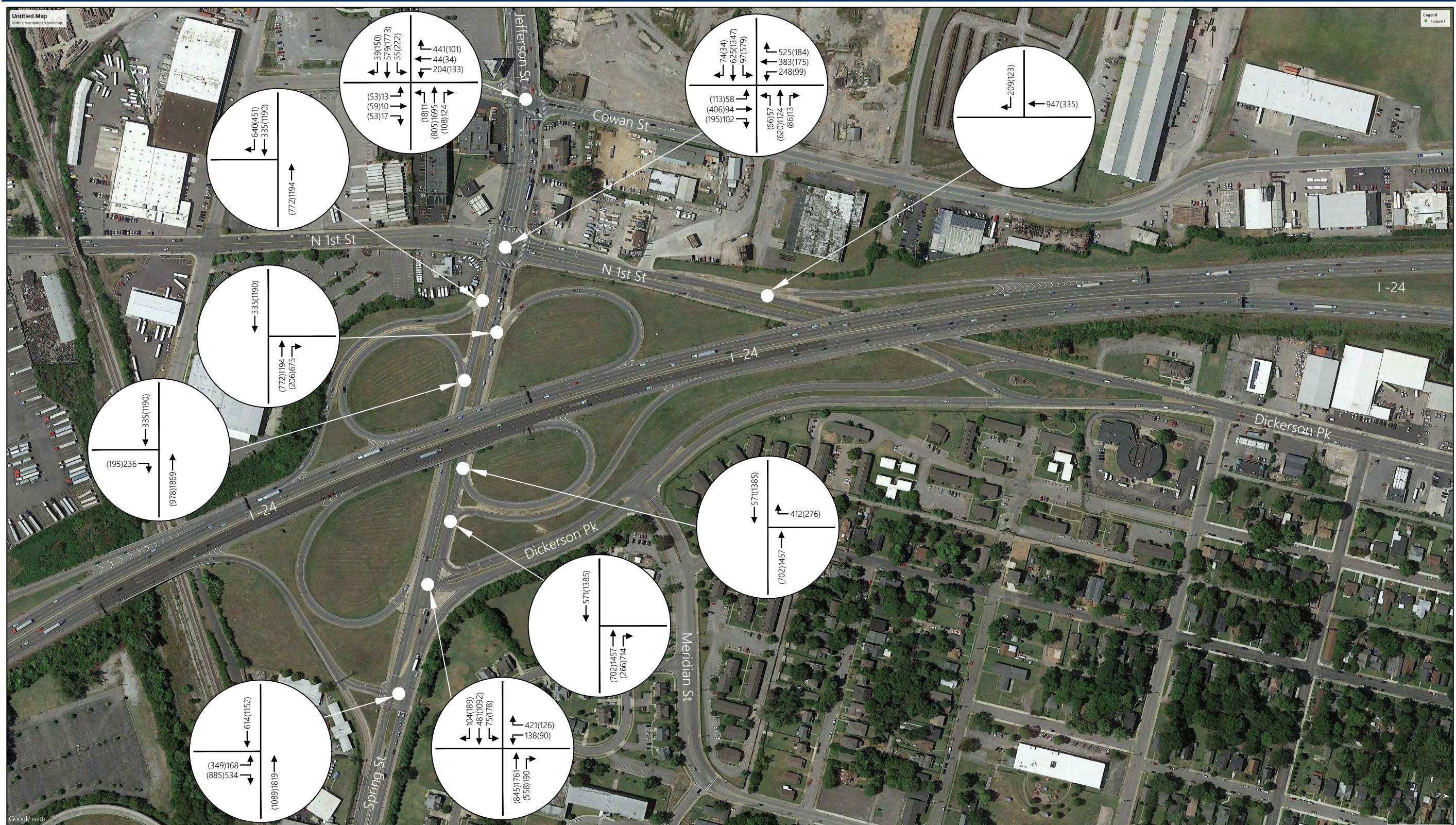
3.2 Existing Traffic Volumes

In addition to examining the classification and laneage of the surrounding roadway network, traffic volume counts located in proximity to the site were available from a variety of sources. One of these sources is TDOT, which has permanent count stations located throughout the state that collect both daily and hourly traffic volumes. Additionally, peak period turning movement traffic counts were collected by KCI at the following locations:

1. Jefferson Street/Spring Street and Cowan Street
2. Spring Street and North 1st Street
3. Spring Street and Dickerson Pike
4. I-24 On & Off-Ramps at Spring Street
5. I-24 Eastbound Off-ramp at North 1st Street

Traffic counts for the study intersections were conducted in June 2016 by KCI. Specifically, the turning movement counts were conducted from 7:00 – 9:00 AM and 4:00 – 6:00 PM on a typical weekday in June 2016. From the counts, it was determined

that the peak hours of traffic flow for the study intersections occurred from 8:00 – 9:00 AM and 4:00 – 5:00 PM. The existing peak hour turning movement volumes are presented in Figure 2. A detailed summary of the turning movement counts is included in Appendix B.

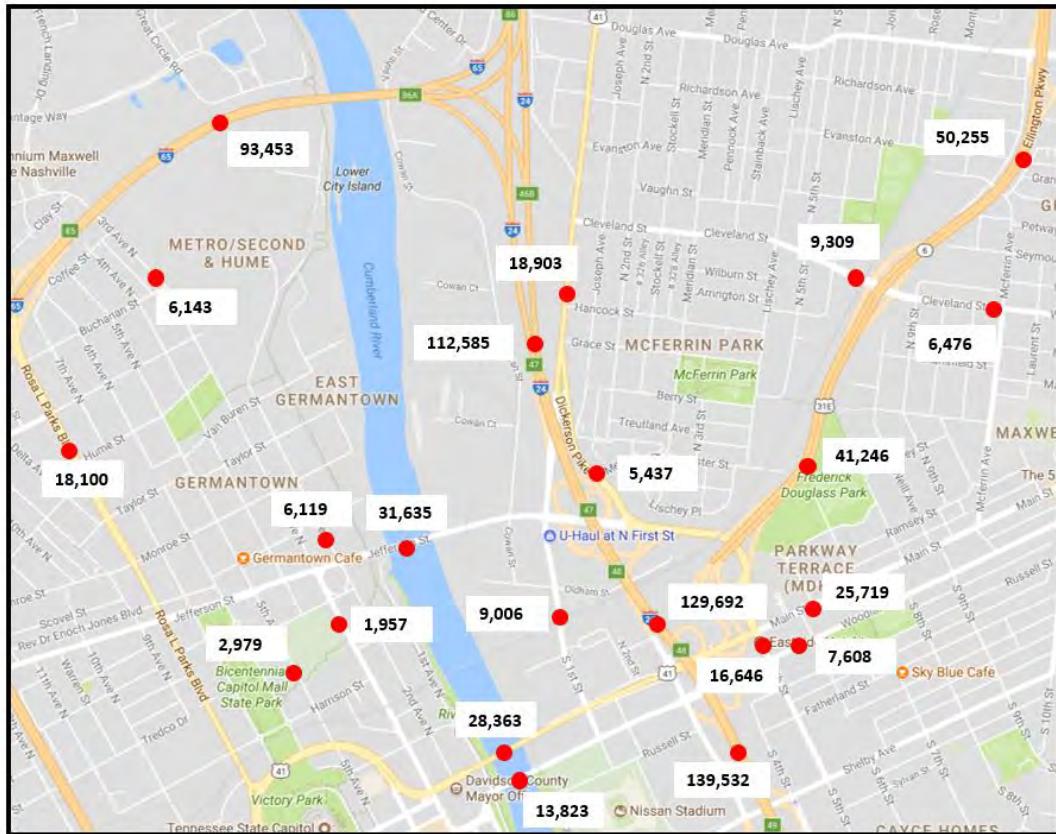


Existing Peak Hour Traffic Volumes
(Not to Scale)

Figure 2.

In addition to the above information, average daily traffic volumes were obtained from the Tennessee Department of Transportation (TDOT). Figure 3 identifies the 2016 annual average daily traffic (AADT) at the TDOT count stations in the study area. TDOT Count Station data is included in Appendix C.

As shown in Figure 3, I-24 and I-65 carry two-way daily volumes in excess of 100,000 vehicles per day. Other streets in the project site vicinity that carry significant daily traffic volumes are Ellington Parkway (50,255 vehicles per day), Jefferson Street (31,635 vehicles per day), Dickerson Pike (18,903 vehicles per day), and James Robertson Parkway (28,363 vehicles per day). Cleveland Street, which the masterplan proposes to extend across I-24 as part of the proposed River North project, has a daily two-way traffic volume of 9,309 vehicles per day.



Source: TDOT

FIGURE 3. 2016 AADT DATA

3.3 Existing Traffic Operations

To determine the current operation of the study intersections, capacity analyses were performed for the AM and PM peak hours. The capacity calculations were performed according to the methods outlined in the *Highway Capacity Manual*, TRB 2010. The capacity analyses result in the determination of a Level of Service (LOS) for an intersection. The LOS is a concept used to describe how well an intersection or roadway operates. LOS A is the best, while LOS F is the worst. LOS D is typically considered as the minimum acceptable LOS for an intersection in an urbanized area. Table 2 present the descriptions of LOS signalized intersections, accordingly.

TABLE 2. DESCRIPTIONS OF LEVEL OF SERVICE FOR SIGNALIZED INTERSECTIONS

| LEVEL OF SERVICE | DESCRIPTION | CONTROL DELAY (sec/veh) |
|------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|
| A | Operations with very low delay. This occurs when progression is extremely favorable. Most vehicles do not stop at all. | ≤ 10 |
| B | Operations with stable flows. This generally occurs with good progression and/or short cycle lengths. More vehicles stop than for LOS A, causing higher levels of average delay. | >10 and ≤ 20 |
| C | Operations with stable flow. Occurs with fair progression and/or longer cycle lengths. The number of vehicles stopping is significant, although many still pass through the intersection without stopping. | >20 and ≤ 35 |
| D | Approaching unstable flow. The influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, or high V/C ratios. Many vehicles stop. | >35 and ≤ 55 |
| E | Unstable flow. This is considered to be the limit for acceptable delay. These high delays generally indicate poor progression, long cycle lengths, and high V/C ratios. | >55 and ≤ 80 |
| F | Unacceptable delay. This condition often occurs with over saturation or with high V/C ratios. Poor progression and long cycle lengths may also cause such delay levels. | >80.0 |

Source: *Highway Capacity Manual*, TRB 2010

The results of the capacity analyses for the existing conditions at the intersections studied are presented in Table 3 and Table 4 for the AM and PM peak hours, accordingly. Each of these intersections is signalized. As shown, the signalized intersection of Jefferson Street and Cowan Street operates at LOS D and LOS C during the AM and PM peak hours, respectively. The intersection of Spring Street and North

1st Street operates at LOS E during the AM peak hour and LOS D during the PM peak hour. The intersection of Spring Street and Dickerson Pike operates at LOS D during the AM peak hour and LOS B during the PM peak hour. The intersection of Spring Street and I-24 WB Off-Ramp operates at LOS B during the AM peak hour and LOS A during the PM peak hour. Capacity analyses worksheets are included in Appendix D.

TABLE 3. EXISTING AM PEAK HOUR LEVELS OF SERVICE

| INTERSECTION | TURNING MOVEMENT | LEVEL OF SERVICE (Average Approach Delay in sec/veh) AM Peak Hour |
|----------------------------------------------|----------------------|-------------------------------------------------------------------------|
| Jefferson Street & Cowan Street | Overall Intersection | D (53.9) |
| Spring Street & North 1 st Street | Overall Intersection | E (69.9) |
| Spring Street & Dickerson Pike* | Overall Intersection | D (35.6) |
| Spring Street & I-24 WB Off-Ramp* | Overall Intersection | B (13.3) |

Note: Asterisks denote intersections that utilize non-NEMA phasing and are, therefore, analyzed using HCM 2000 results

TABLE 4. EXISTING PM PEAK HOUR LEVELS OF SERVICE

| INTERSECTION | TURNING MOVEMENT | LEVEL OF SERVICE (Average Approach Delay in sec/veh) PM Peak Hour |
|----------------------------------------------|----------------------|-------------------------------------------------------------------------|
| Jefferson Street & Cowan Street | Overall Intersection | C (20.1) |
| Spring Street & North 1 st Street | Overall Intersection | D (48.4) |
| Spring Street & Dickerson Pike* | Overall Intersection | B (13.5) |
| Spring Street & I-24 WB Off-Ramp* | Overall Intersection | A (8.8) |

Note: Asterisks denote intersections that utilize non-NEMA phasing and are, therefore, analyzed using HCM 2000 results

4. IMPACTS

4.1 Trip Generation

A traffic generation process was used to estimate the amount of traffic expected to be generated by Phase 1 of the proposed River North development. Factors for the trip generation were taken from ITE's *Trip Generation*, Ninth Edition. As previously discussed, Phase 1 of the proposed development, as considered in this analysis, consists of a total of approximately three (3) million square feet of office space, 1,735 residential units, 285,000 square feet of retail/restaurant space, 550 hotel rooms and 186,500 square feet of civic space. As part of the development of the project site, significant pedestrian infrastructure improvements are planned to be included both within the project site and along the adjacent public rights-of-way. Additionally, the project site is located in an area that already includes a relatively dense mix of land uses with regular transit service. Therefore, using reductions in the base ITE trip generation rates, 5% reductions were applied to account for walking, biking, and transit modes, conservatively.

Data presented in the ITE publication, *Trip Generation Handbook*, shows that developments containing multiple land uses will commonly have internal trips. A process was used to estimate the amount of internal trips that can be expected between land uses based on methodology presented in NCHRP Report 684, "Enhancing Internal Trip Capture Estimation for Mixed-Use Developments." The methodology contained in the NCHRP Report expands on ITE's methodology, including additional land uses and supporting data. The internal trip reduction process resulted in an approximate 22% internal capture rate for the AM, 19% for the PM, and 20% for daily trip generation under full buildout scenario of the proposed development.

Table 6 presents the daily, AM, and PM peak hour trip generation for Phase 1 of the proposed mixed-use development. As shown by Table 6, Phase 1 of the proposed development, as considered in this analysis, is expected to generate approximately 36,949 new trips per day. The AM and PM peak hour trip generations will equal approximately 3,634, and 4,483 new trips, respectively. As it was mentioned previously, the traffic analysis is based on more density than is currently contemplated by the developer. Given variables such as local demand and overall economy, it is prudent to underwrite conservatively. The calculations for trip generation are included in Appendix E.

TABLE 5. DEVELOPMENT TRIP GENERATION (PHASE 1)

| LAND USE | SIZE | GENERATED TRAFFIC ¹ | | | | | |
|-------------------------|----------------|--------------------------------|-----------------|--------------|-----------------|--------------|--|
| | | DAILY TRIPS | AM PEAK HOUR | | PM PEAK HOUR | | |
| | | | ENTER | EXIT | ENTER | EXIT | |
| Office (LUC 710) | 3,029,000 s.f. | 13,328 | 2,163 | 233 | 535 | 2,623 | |
| Retail (LUC 826) | 200,000 s.f. | 6,531 | 52 | 74 | 80 | 102 | |
| Restaurant ² | 58,000 s.f. | 5,549 | 142 | 149 | 187 | 66 | |
| Apartments (LUC 220) | 1,735 d.u. | 8,084 | 151 | 486 | 402 | 233 | |
| Hotel (LUC 310) | 550 rooms | 3,457 | 157 | 27 | 122 | 133 | |
| SUBTOTAL | | 36,949 | 2,665 | 969 | 1,326 | 3,157 | |
| NEW TRIPS | | 36,949 | | 3,634 | | 4,483 | |

Notes:

1) Calculations above represent only new traffic generated by the project site. The internal trips and alternative mode trips are not included in the numbers above.

2) Combination of LUC 931, LUC 932, and LUC 936

Source: *Trip Generation*, Ninth Edition

4.2 Evaluation

As mentioned previously, the master plan proposed a variety of new roadway extensions, bridges, interchanges and access connections to the Interstate system as well as to existing streets. Various combinations of the potential improvements within the study area were developed. Directional distributions of traffic generated by the proposed project were then established based on the proposed access connections under each scenario and the existing travel patterns developed from the existing peak hour traffic counts. Capacity analysis using Synchro 9 along with a sensitivity analysis were then conducted at the critical study intersections to estimate the maximum new trip-generated traffic volumes by the proposed development which can be managed under each scenario.

It should be noted that since the existing operational performance at the study intersections indicated that at least one of the intersections (Spring Street and North 1st Street) operates at LOS E during the peak hours, some improvements are required to be implemented upon the construction of the proposed development at any stage if LOS D operation is to be achieved.

For the purpose of this study and based on the capacity analysis it was determined that the intersection of Jefferson Street/Spring Street and Cowan Street is the control intersection for the sensitivity analysis. In addition, the proposed development has higher impacts at that intersection during the PM peak hour when compared to the AM peak hour. As a result, for the sensitivity analysis, capacity analyses were conducted at the intersection of Jefferson Street/Spring Street and Cowan Street during the PM peak hour under each of the various scenarios.

Directional distribution within the study area and specifically the study intersection of Jefferson Street/Spring Street and Cowan Street varies based on the proposed improvements. Consequently, directional distributions under each scenario were developed and the maximum newly generated trips by the proposed development, which can be managed under each scenario was determined. Description of the proposed improvements, specific directional distributions, and the maximum new trip-generated traffic volumes by the proposed development (based on the PM peak hour volumes) which can be accommodated under each scenario are presented as follows.

4.2.1 Low Level and Medium Level Improvements

Under the low level and medium level improvements scenarios, the proposed developments do not include construction of any new roadway bridges and/or connectors. Moreover, under the low-level improvements scenario, widening of

Jefferson Street/Spring Street within the study area is not being considered. However, under the scenario with medium level improvements, potential improvements which require widening of Jefferson Street/Spring Street within the study area were considered and included in the analysis. Since no new roadway connectors were proposed under either the low level and medium level improvements scenarios, the same directional distribution was utilized for both scenarios. Figure 4, Table 7, and Table 8 present the directional distribution, proposed improvements, and maximum newly generated trips by the proposed development that can be accommodated by implementing those improvements. Conceptual recommended improvements at the intersection of Jefferson Street/Spring Street and Cowan Street under low-level and medium-level improvements scenarios are presented in Figure 5 and Figure 6.

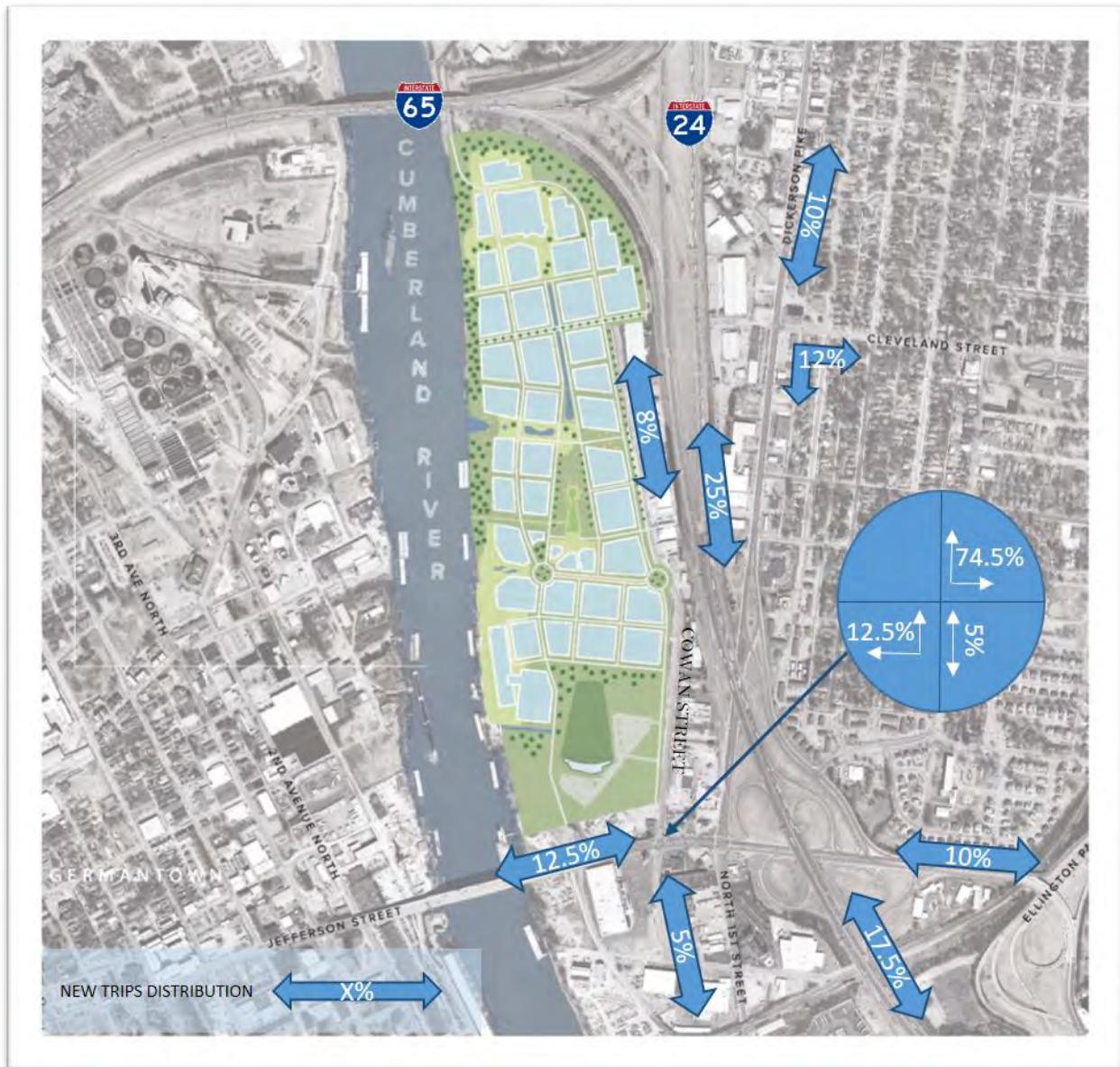


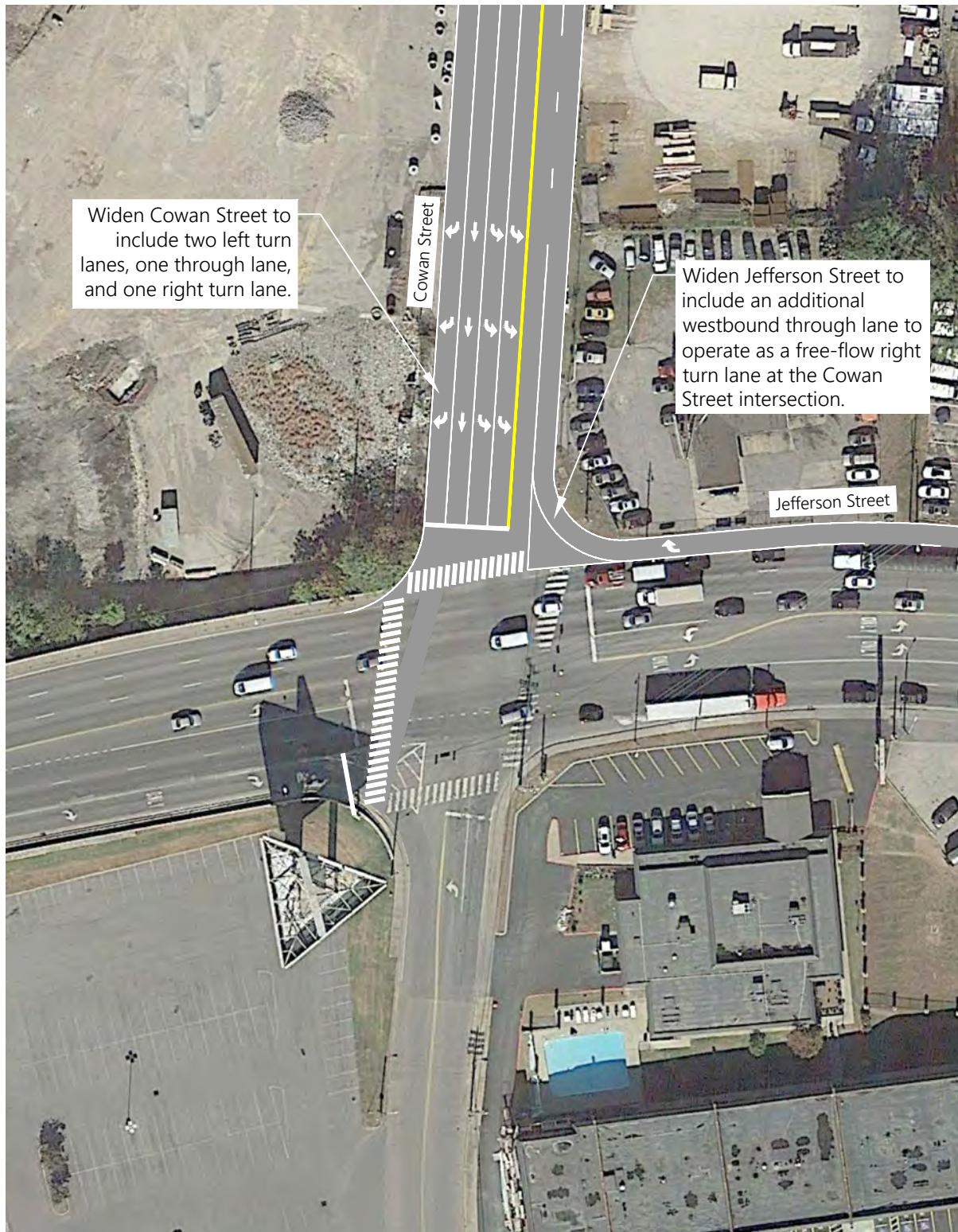
FIGURE 4. DIRECTIONAL DISTRIBUTION OF TRAFFIC GENERATED BY THE PROJECT SITE UNDER LOW-LEVEL AND MEDIUM-LEVEL IMPROVEMENTS

TABLE 6. MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT
DURING PM PEAK HOUR UNDER LOW-LEVEL IMPROVEMENTS SCENARIO

| LOW-LEVEL IMPROVEMENTS | | |
|---------------------------------------------------------------------------------------------------------------|-------|------|
| MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT DURING PM PEAK HOUR | | |
| TOTAL | ENTER | EXIT |
| 983 (22% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour) | 360 | 623 |

TABLE 7. MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT
DURING PM PEAK HOUR UNDER MEDIUM-LEVEL IMPROVEMENTS SCENARIO

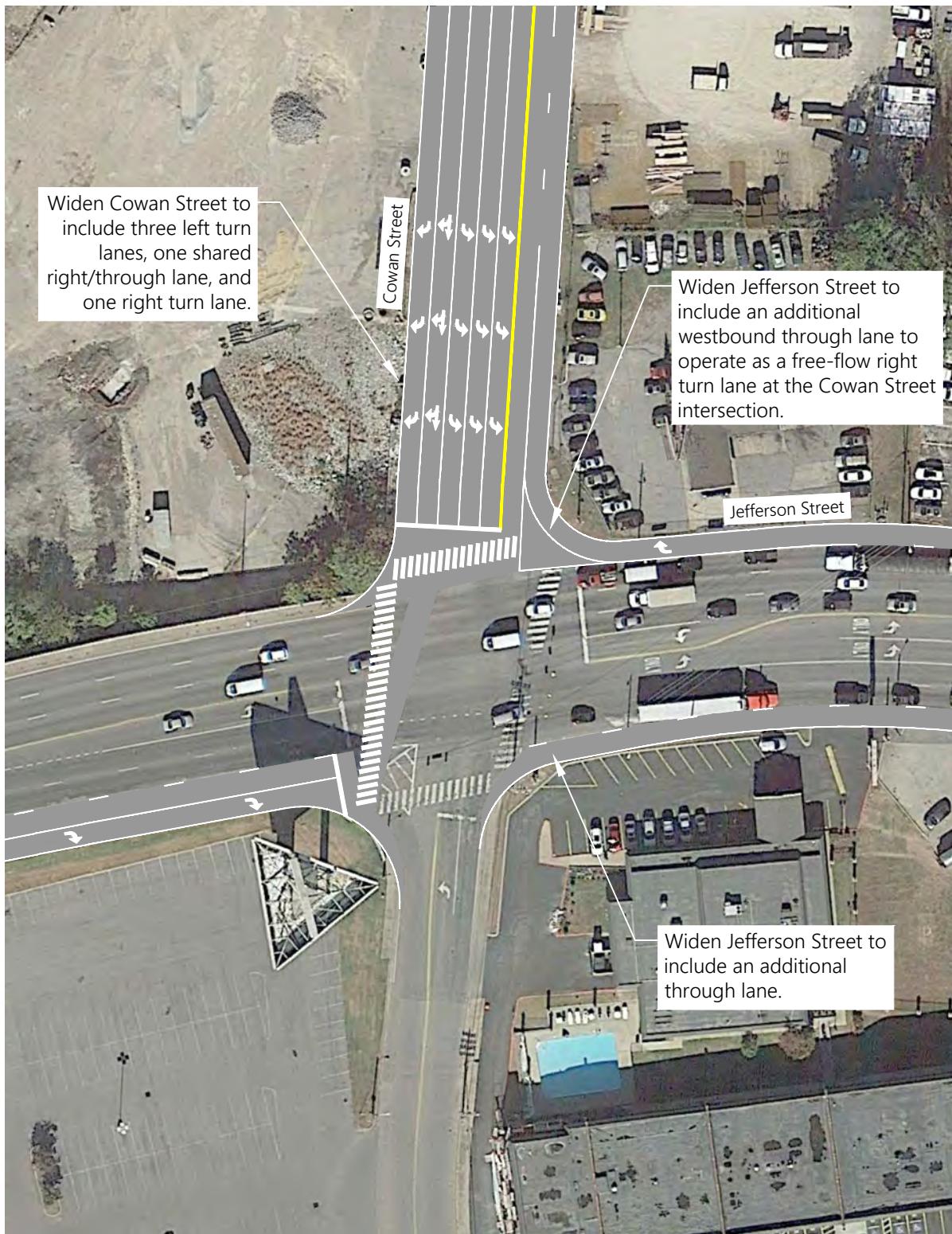
| MEDIUM-LEVEL IMPROVEMENTS | | |
|-----------------------------------------------------------------------------------------------------------------|-------|-------|
| MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT DURING PM PEAK HOUR | | |
| TOTAL | ENTER | EXIT |
| 2,700 (60% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour) | 1,146 | 1,554 |



Recommended Improvements - Low Level Improvements

GRAPHIC SCALE
0' 80' 160'

Figure 5.



Recommended Improvements - Medium Level Improvements



GRAPHIC SCALE
0' 80' 160'

Figure 6.

4.2.2 High-Level Improvements

Under the high-level improvements scenarios, construction of new roadway connectors and bridges were considered as part of the potential developments in addition to the proposed improvements under the medium-level improvements scenario. Several high-level improvement scenarios were evaluated using revised directional distributions that would result with the specific improvements. Directional distributions, proposed improvements, and maximum newly generated trips which can be accommodated by implementing those improvements are presented in the following tables and figures.

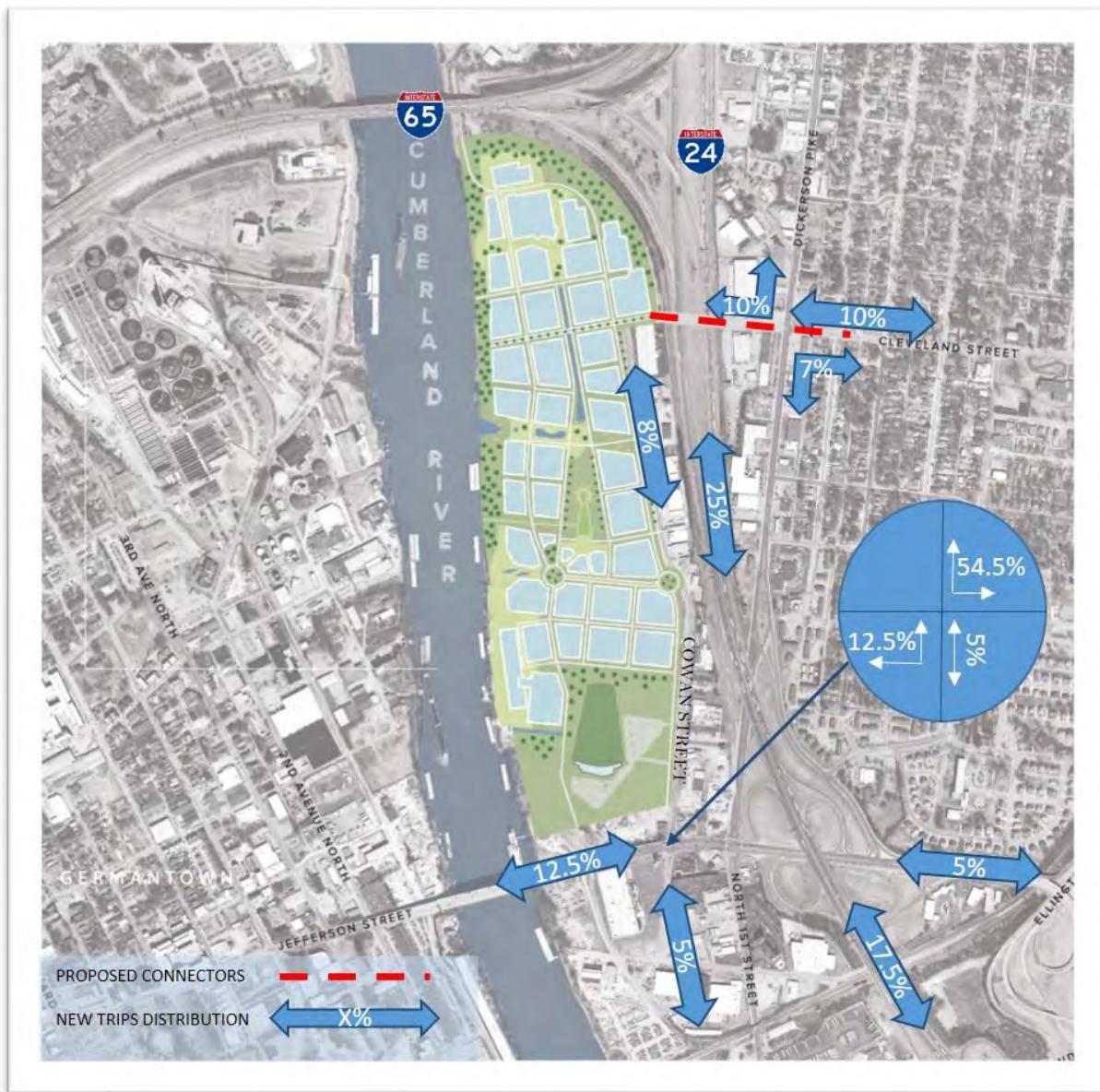


FIGURE 7. DIRECTIONAL DISTRIBUTION OF TRAFFIC GENERATED BY THE PROJECT SITE
HIGH-LEVEL IMPROVEMENTS-OPTION 1

TABLE 8. MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT
DURING PM PEAK HOUR
UNDER HIGH-LEVEL IMPROVEMENTS SCENARIO-OPTION 1

| HIGH-LEVEL IMPROVEMENTS-OPTION 1 | | | |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------|-------|-------|
| <ul style="list-style-type: none"> Provide a new roadway connector across I-24 between Cleveland Street and the proposed development. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 1A | | | |
| Include medium-level improvements #1, and #3 as described in Table 7 in addition to the following: | | | |
| <ul style="list-style-type: none"> Widen Cowan Street southbound to include two left-turn lanes, one shared through/right-turn lane, and one right-turn lane. | | | |
| Note: Widening of the I-24 bridge and ramps improvements within the study area are likely to be required. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 1B | | | |
| Include all the medium-level improvements as described in Table 7. | | | |
| Note: Widening of the I-24 bridge and ramps improvements within the study area are likely to be required. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 1C | | | |
| Include all the low-level improvements as described in Table 6. | | | |
| MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT DURING PM PEAK HOUR | | | |
| OPTIONS | TOTAL | ENTER | EXIT |
| OPTION 1A | 1,350 <i>(30% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 573 | 777 |
| OPTION 1B | 3,240 <i>(72% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 1,375 | 1,865 |
| OPTION 1C | 1,215 <i>(27% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 516 | 699 |

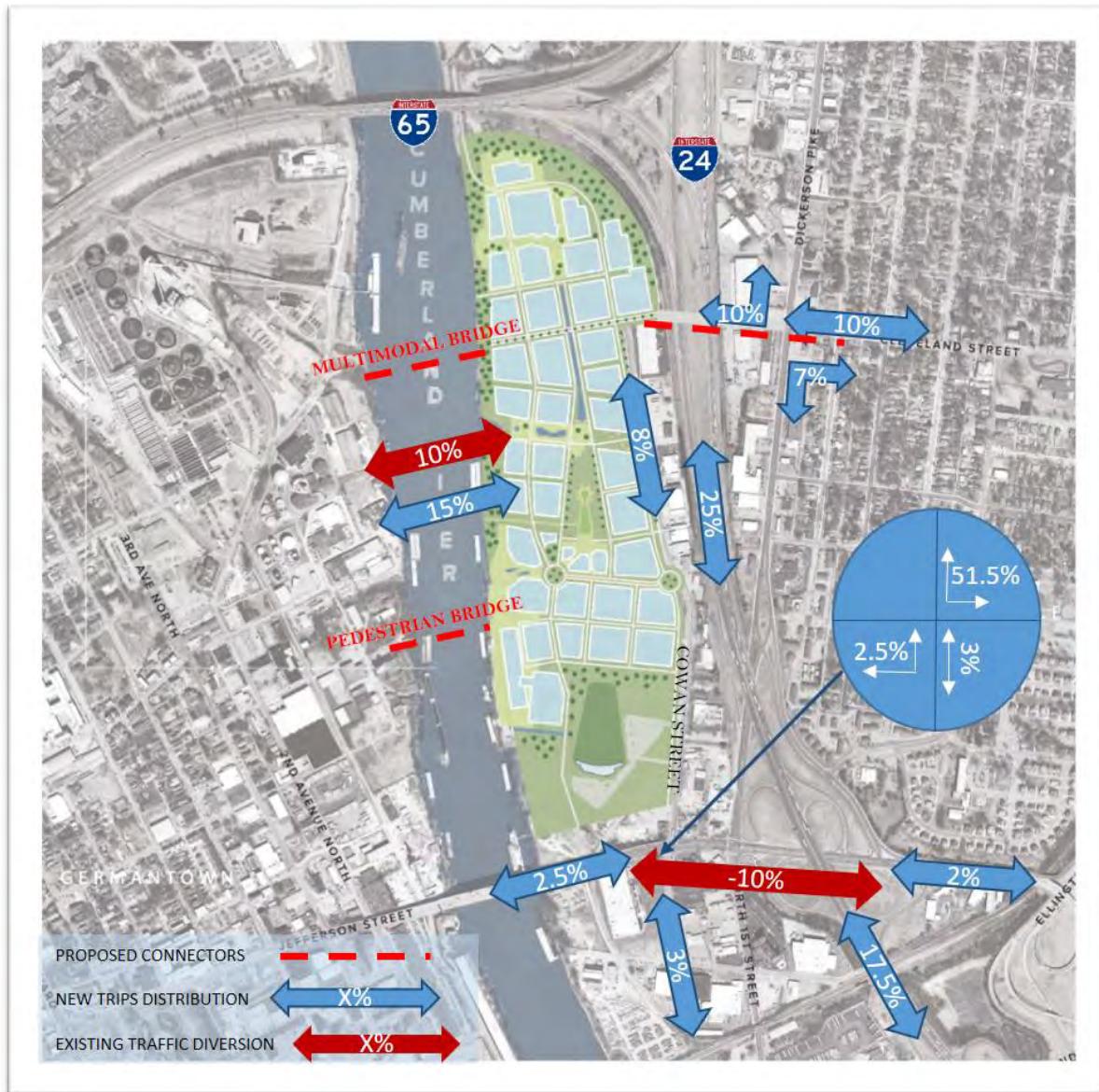


FIGURE 8. DIRECTIONAL DISTRIBUTION OF TRAFFIC GENERATED BY THE PROJECT SITE
HIGH-LEVEL IMPROVEMENTS-OPTION 2

TABLE 9. MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT
DURING PM PEAK HOUR
UNDER HIGH-LEVEL IMPROVEMENTS SCENARIO-OPTION 2

| HIGH-LEVEL IMPROVEMENTS-OPTION 2 | | | |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------|-------|-------|
| <ul style="list-style-type: none"> Provide a new roadway connector across I-24 between Cleveland Street and the proposed development. Provide new pedestrian and multimodal bridge connectors to Germantown over Cumberland River. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 2A | | | |
| Include medium-level improvements #1, and #3 as described in Table 7 in addition to the following: | | | |
| <ul style="list-style-type: none"> Widen Cowan Street southbound to include two left-turn lanes, one shared through/right-turn lane, and one right-turn lane. | | | |
| Note: Widening of the I-24 bridge and ramps improvements within the study area are likely to be required. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 2B | | | |
| Include all the medium-level improvements as described in Table 7. | | | |
| Note: Widening of the I-24 bridge and ramps improvements within the study area are likely to be required. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 2C | | | |
| Include all the low-level improvements as described in Table 6. | | | |
| MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT DURING PM PEAK HOUR | | | |
| OPTIONS | TOTAL | ENTER | EXIT |
| OPTION 2A | 2,970 <i>(66% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 1,261 | 1,709 |
| OPTION 2B | 4,590 <i>(102% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 1,948 | 2,642 |
| OPTION 2C | 1,620 <i>(36% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 688 | 932 |

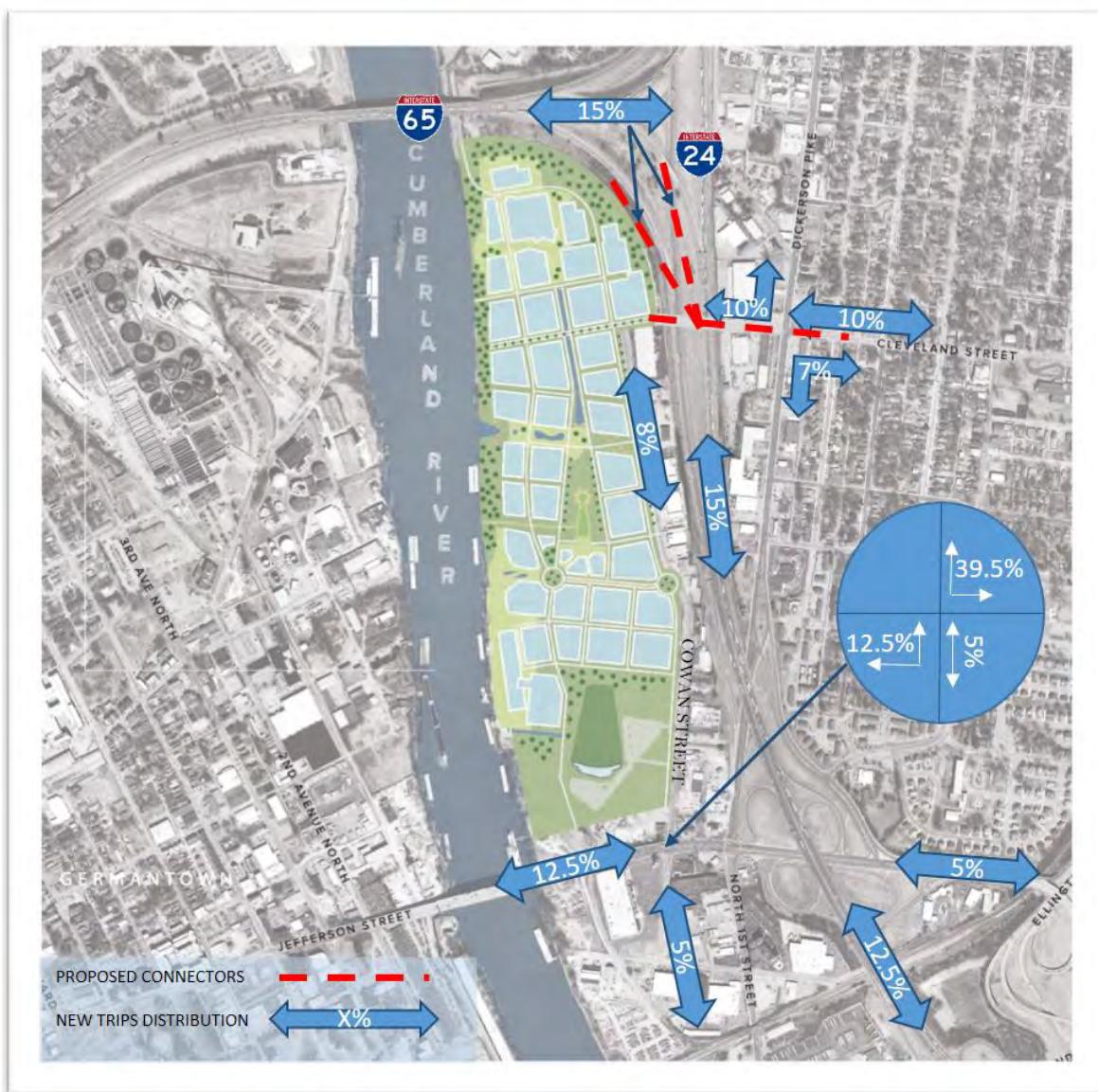


FIGURE 9. DIRECTIONAL DISTRIBUTION OF TRAFFIC GENERATED BY THE PROJECT SITE
HIGH-LEVEL IMPROVEMENTS-OPTION 3

TABLE 10. MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT
DURING PM PEAK HOUR
UNDER HIGH-LEVEL IMPROVEMENTS SCENARIO-OPTION 3

HIGH-LEVEL IMPROVEMENTS-OPTION 3

- Provide a new roadway connector across I-24 between Cleveland Street and the proposed development with partial movements' accesses to Interstate.

ADDITIONAL IMPROVEMENTS-OPTION 3A

Include medium-level improvements #1, and #3 as described in Table 7 in addition to the following:

- Widen Cowan Street southbound to include two left-turn lanes, one shared through/right-turn lane, and one right-turn lane.

Note: Widening of the I-24 bridge and ramps improvements within the study area are likely to be required.

ADDITIONAL IMPROVEMENTS-OPTION 3B

Include all the medium-level improvements as described in Table 7.

Note: Widening of the I-24 bridge and ramps improvements within the study area are likely to be required.

ADDITIONAL IMPROVEMENTS-OPTION 3C

Include all the low-level improvements as described in Table 6.

MAXIMUM NEWLY GENERATED TRAFFIC VOLUMES BY THE PROPOSED DEVELOPMENT DURING PM PEAK HOUR

| OPTIONS | TOTAL | ENTER | EXIT |
|-----------|------------------------------------------------------------------------------------------------------------------------|-------|-------|
| OPTION 3A | 2,970 <i>(66% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 1,261 | 1,709 |
| OPTION 3B | 4,050 <i>(90% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 1,719 | 2,331 |
| OPTION 3C | 1,620 <i>(36% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 688 | 932 |

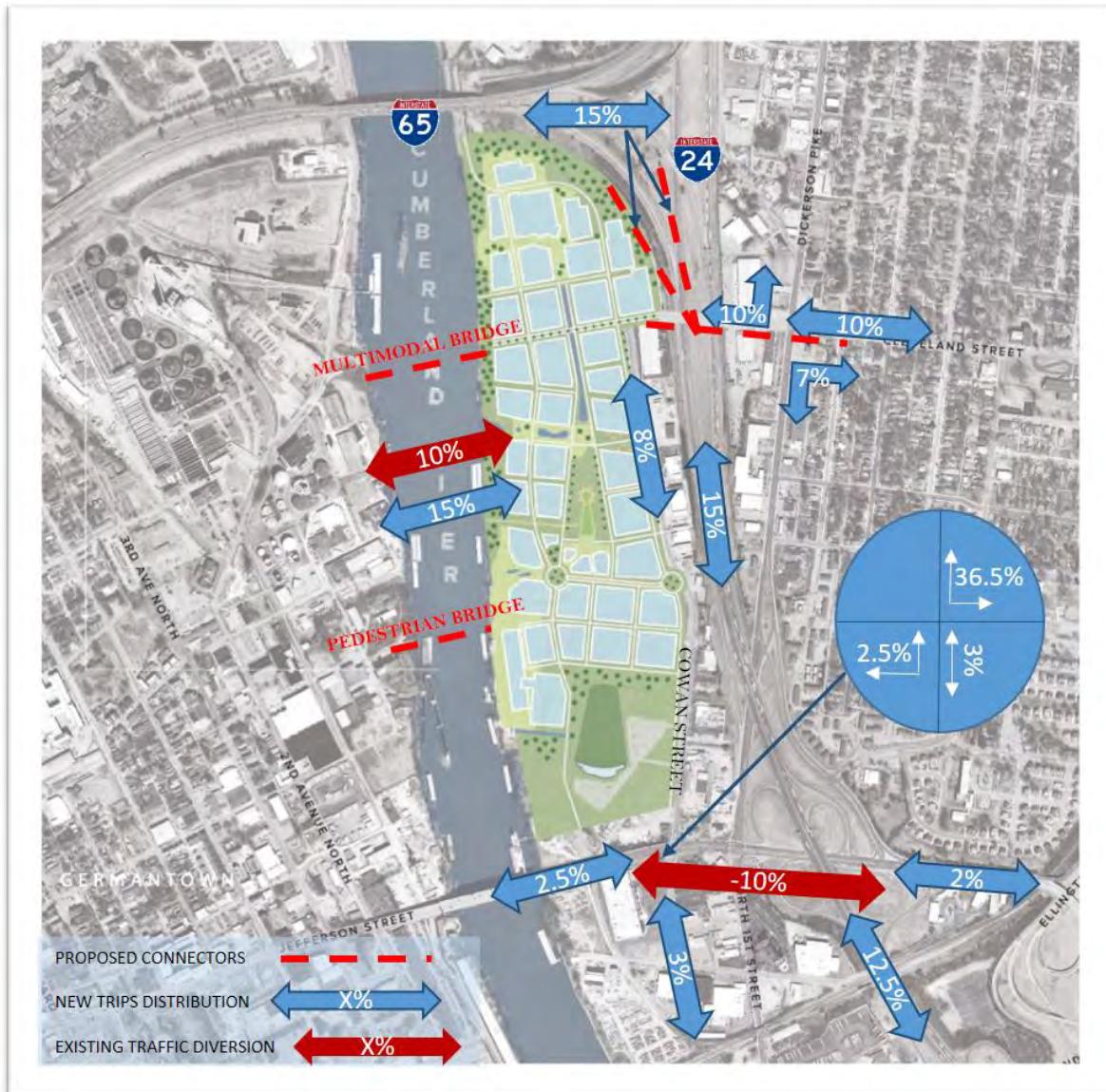


FIGURE 10. DIRECTIONAL DISTRIBUTION OF TRAFFIC GENERATED BY THE PROJECT SITE
HIGH-LEVEL IMPROVEMENTS-OPTION 4

TABLE 11. MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT
DURING PM PEAK HOUR
UNDER HIGH-LEVEL IMPROVEMENTS SCENARIO-OPTION 4

| HIGH-LEVEL IMPROVEMENTS-OPTION 4 | | | |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------|-------|-------|
| <ul style="list-style-type: none"> Provide a new roadway connector across I-24 between Cleveland Street and the proposed development with partial movements' accesses to Interstate. Provide new pedestrian and multimodal bridge connectors to Germantown over Cumberland River. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 4A | | | |
| Include medium-level improvements #1, and #3 as described in Table 7 in addition to the following: | | | |
| <ul style="list-style-type: none"> Widen Cowan Street southbound to include two left-turn lanes, one shared through/right-turn lane, and one right-turn lane. | | | |
| Note: Widening of the I-24 bridge and ramps improvements within the study area are likely to be required. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 4B | | | |
| Include all the medium-level improvements as described in Table 7. | | | |
| Note: Widening of the I-24 bridge and ramps improvements within the study area are likely to be required. | | | |
| ADDITIONAL IMPROVEMENTS-OPTION 4C | | | |
| Include all the low-level improvements as described in Table 6. | | | |
| MAXIMUM NEWLY GENERATED TRIPS BY THE PROPOSED DEVELOPMENT DURING PM PEAK HOUR | | | |
| OPTION | TOTAL | ENTER | EXIT |
| OPTION 4A | 4,050 <i>(90% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 1,719 | 2,331 |
| OPTION 4B | 5,940 <i>(133% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 2,521 | 3,419 |
| OPTION 4C | 2,430 <i>(54% of Newly Generated Trips by Total Buildout of Phase 1 of the Development During the PM Peak Hour)</i> | 1,031 | 1,399 |

4.2.3 Cowan Street Cross-Section

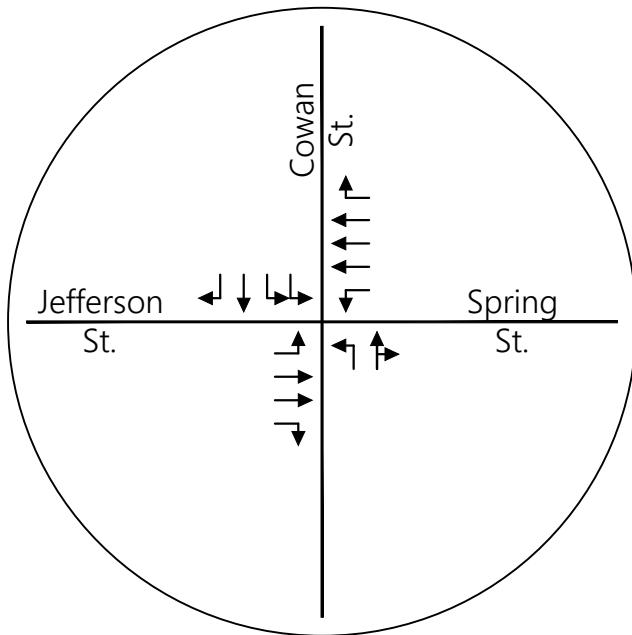
Total projected traffic volumes and lane configurations at the control study intersection of Jefferson Street/Spring Street and Cowan Street are presented in Figure 9 through Figure 13. As shown in the figures, total bi-directional projected traffic volumes on Cowan Street north of Jefferson Street/Spring Street during the PM Peak

hour (worst case) is expected to be within the range of 1,365-4,934 vehicles per hour under various improvements scenarios.

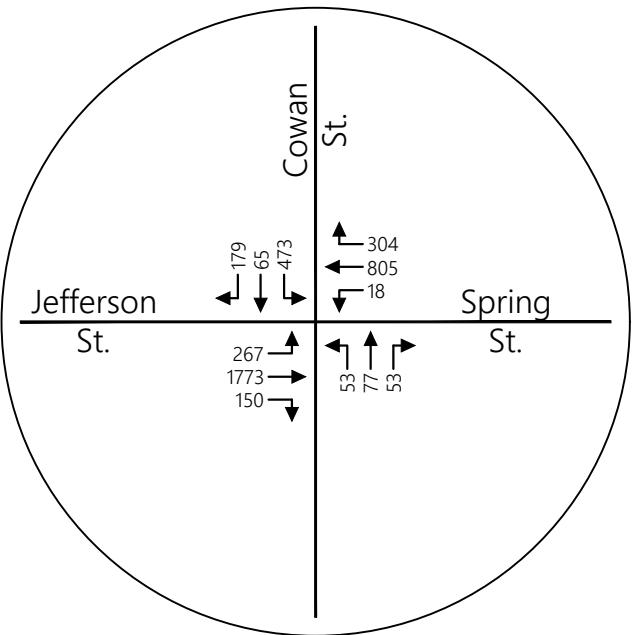
An urban roadway with 4,934 traffic volumes during the peak hour is very likely to carry daily trips of more than 40,000 vehicles per day, which typically requires a six-lane cross-section. The aesthetics and functionality of this wide of a roadway, however, is not compatible with the livability desires for the development or the overall vision for the downtown core – one that is walkable and supports a thriving transit system. The blank slate the site provides allows Metro to “rightsize” this corridor from the concept phase to ensure a functional and livable urban neighborhood environment that flourishes in the near-term, while allowing for strategic right-of-way dedication to adequately accommodate future growth. Whether the roadway needs to be widened to enhance mobility along the corridor, such as through the addition of turn lanes at intersections, dedicated transit lanes, or improvements for non-motorized users, having an appropriate amount of right-of-way already set aside will ensure that future buildings are appropriately located along the street’s frontage and also provide a tremendous amount of cost savings and effort for Metro in the future. Long-term planning considerations such as these also better positions this critical area, which will act as a gateway into and out of downtown, to play an effective role in accomplishing the city’s grander visions for multimodal transportation as growth continues.

Other mobility strategies within the study area could be considered and coordinated between the development team and Metro Nashville in order to achieve the high densities envisioned for the proposed development. Those strategies are likely to improve the mobility of the study area and to avoid extensive widening of Cowan Street. Some of the potential recommendations are described in the conclusions section of this study.

LANE CONFIGURATIONS



TOTAL PROJECTED TRAFFIC VOLUMES



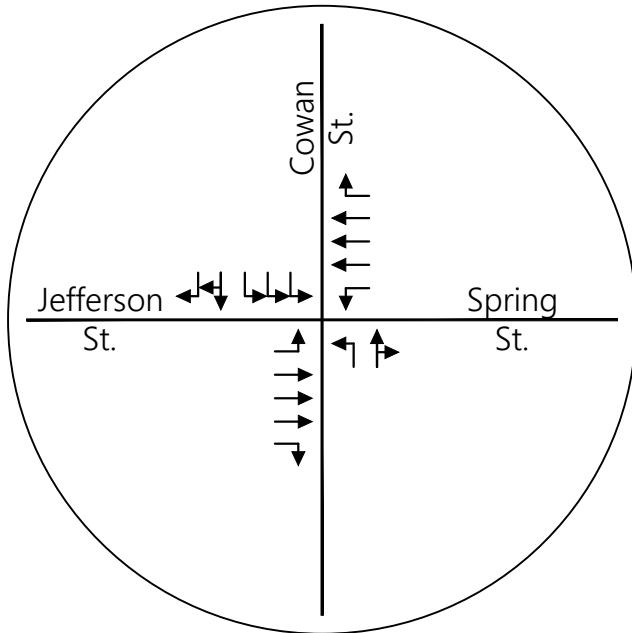
XXX - PM Peak Hour
Traffic Volumes



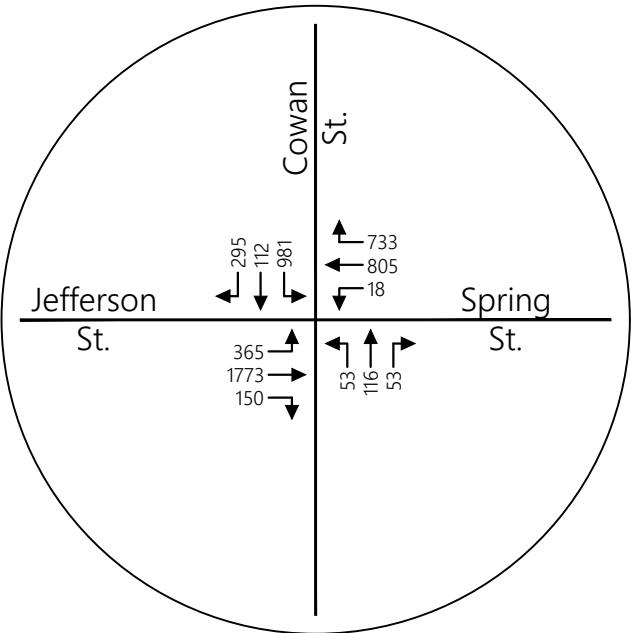
Total Projected Peak Hour Traffic Volumes (Low-Level Improvements)
(Not to Scale)

Figure 11.

LANE CONFIGURATIONS



TOTAL PROJECTED TRAFFIC VOLUMES

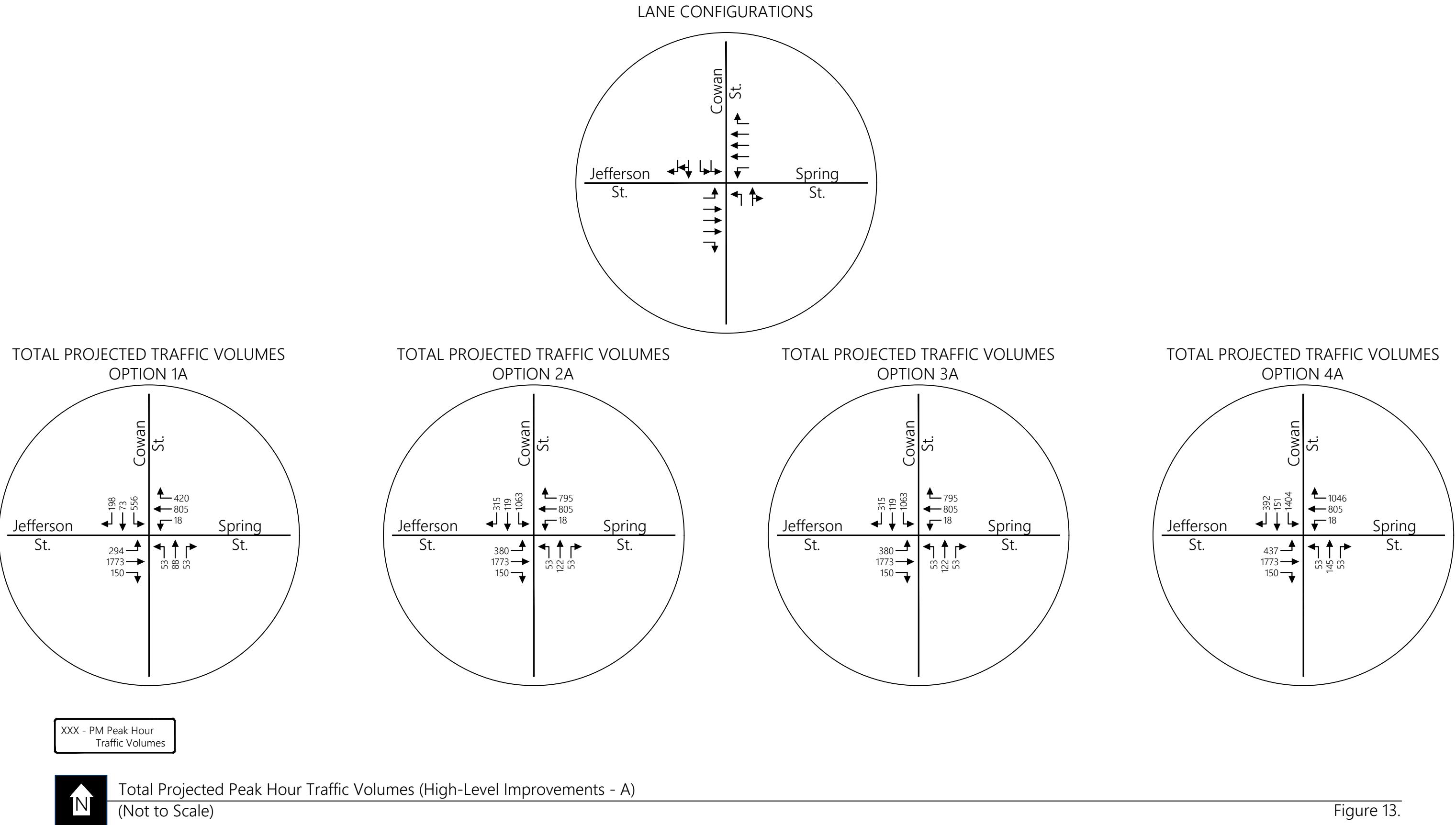


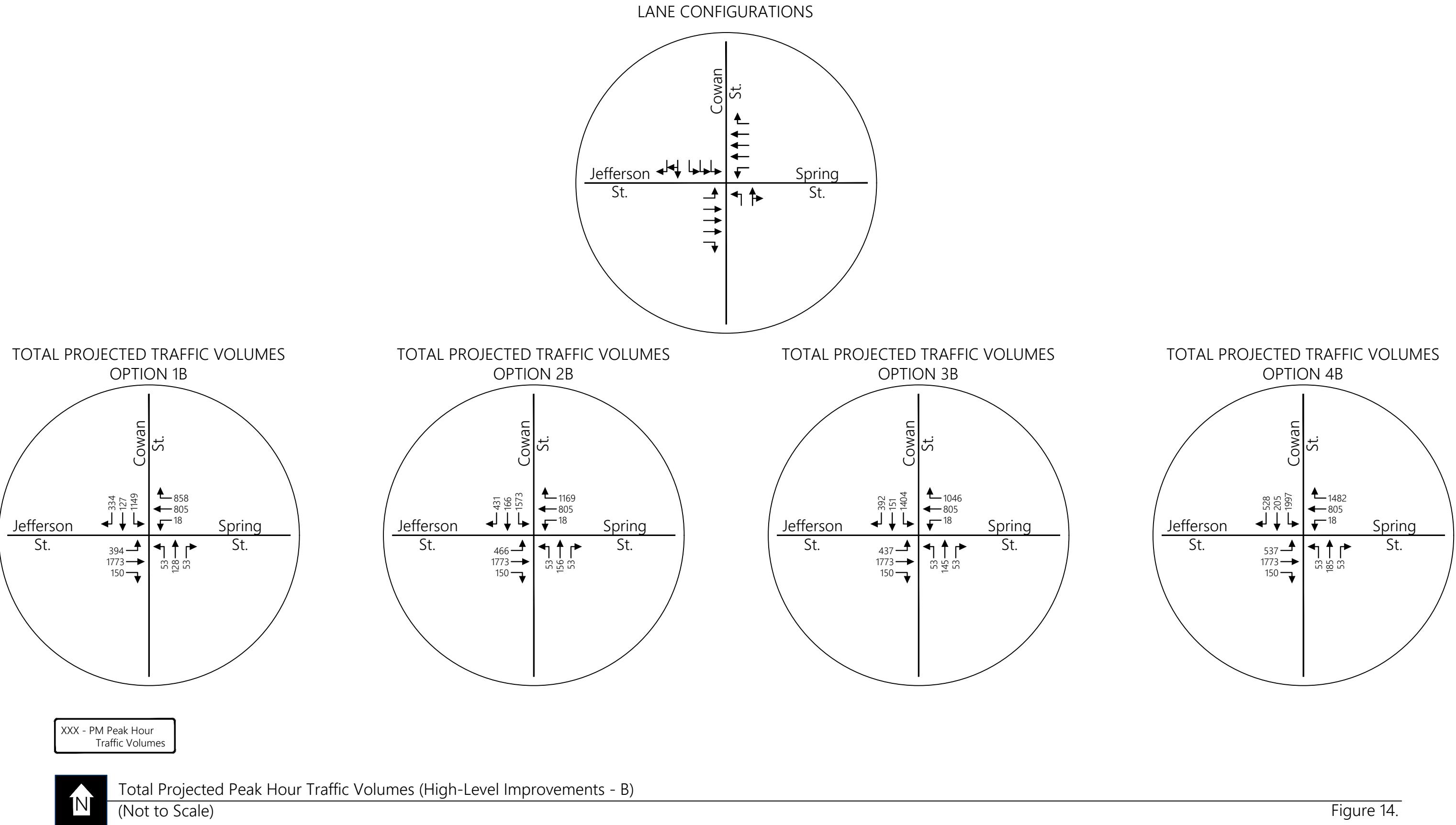
XXX - PM Peak Hour
Traffic Volumes

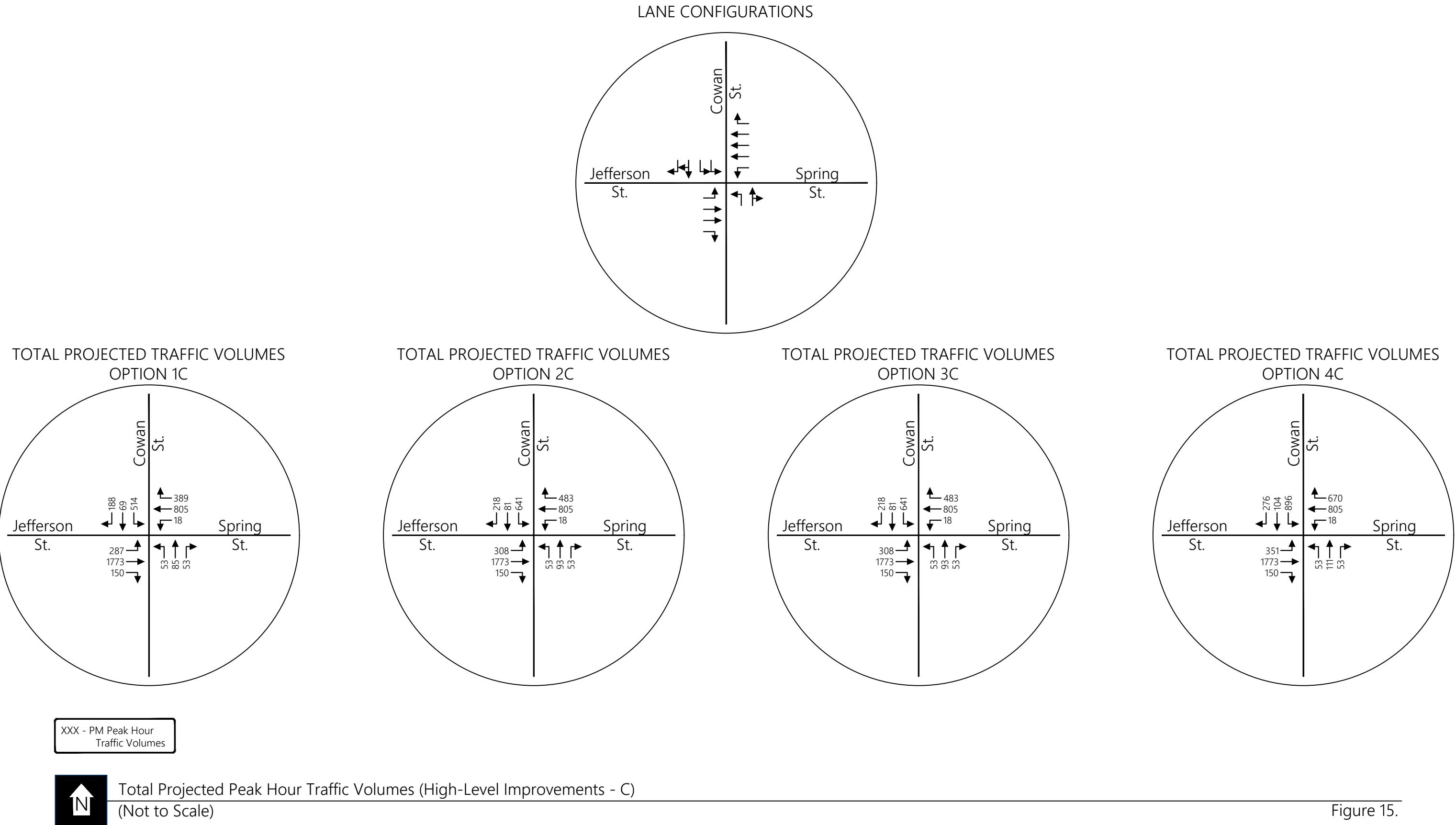


Total Projected Peak Hour Traffic Volumes (Medium-Level Improvements)
(Not to Scale)

Figure 12.







5. CONCLUSIONS AND RECOMMENDATIONS

A review was conducted of the roadway extensions, bridges and interstate access connections that are proposed as part of the River North master plan. This review consisted of evaluating the concepts based on federal and state requirements for the proposed new and modified interchanges and ramps and considering the improvements to network capacity and accessibility that would result with these concepts. Sensitivity analyses were also conducted to estimate the maximum expected newly generated trips by the proposed development, which can be managed by implementing those conceptual improvements within different stages. The suggested improvements are categorized as Low Level, Medium Level, and High Level. Conclusions of the reviews are as follows:

- The Cleveland Street extension and a connection across I-24 make a significant connection to the East Nashville area and will provide access to Dickerson Pike, Whites Creek Pike, Ellington Parkway (US 31E) and Gallatin Pike. Cleveland Street has a four-lane cross-section from Dickerson Pike to east of Ellington Parkway. Utilizing the highest PM peak hour trip generation (Option 4B) and the associated distribution, the Cleveland Street extension has the potential to add approximately 1,000 PM peak hour trips along the corridor; this serves as a significant increase over the 9,000 vpd currently served by the corridor. There are currently two (2) all-way stop controlled intersections along this portion of Cleveland Street, located at Meridian Street and Lischey Avenue. Improvements will likely be necessary at these intersections, at the Ellington Parkway ramps, and potentially at other intersections along the corridor when the Cleveland Street extension is constructed.
- Previous versions of the River North master plan included new on and off ramps to I-65 and I-24. Interchange modifications and/or new connections to the interstate system require both state and federal approval and there are strict standards regarding minimum spacing between ramps that must be met in order to obtain the necessary approvals. State and federal approval of any new interstate access is likely to require considerable modifications to the existing interchanges including the employment of one or more strategies to eliminate weaving on the interstate. These strategies include the addition of collector-distributor roads or grade separated ramps (ramp braids). Requirements for these type of freeway modifications are described in the NCHRP 687 report, *Guidelines for Ramp and Interchange Spacing*. Specific details regarding the operations and feasibility of any interchange modifications or additional access

points will need to be evaluated more thoroughly before understanding the feasibility of such improvements.

- The two proposed bridges over the Cumberland River have the potential to significantly improve access and provide alternative routes that would help lessen the impact of the project on the interstate system and on Jefferson Street/Spring Street. The current master plan illustrates the northern bridge as a vehicular and multimodal bridge and the southern bridge as a pedestrian and bicycle only bridge. It would be desirable for at least one of these bridges to have significant transit carrying capabilities.
- Consideration should be given to connecting the northern Cumberland River bridge to 3rd Avenue as well to provide more accessibility to and from north Nashville.
- A potential connection to Oldham Street has been discussed during the development of the masterplan. This connection would create a new north/south connection for project related traffic that may relieve development related traffic at the intersection of Jefferson Street/Spring Street and Cowan Street. The effectiveness of this connection could be further supported by improvements to South 1st Street, which provides access to Woodland Street to the south.
- The Grace Street extension and a connection across I-24 will provide a convenient connection to East Nashville and to Meridian Street, a north/south collector street. In addition, the Grace Street extension has the potential to be a strong bicycle/pedestrian connection to the pedestrian/bicycle bridge over Ellington Parkway. It should be noted that this proposed improvement was not included in the capacity analysis, for the purpose of this study. It was assumed that a portion of the distributed traffic on Cleveland Street connector would be distributed onto the Grace Street extension, which would result in the same reduction of traffic on Jefferson Street/Spring Street as without the implementation of this improvement.
- As previously described, the maximum full buildout of the southern 40 acres of the development is referred to as Phase 1 in this study. Improvement recommendations at the existing intersection of Jefferson Street/Spring Street and Cowan Street associated with Phase 1 of the development were also evaluated and are described below.

- Add additional turning lanes at the intersection of Jefferson Street and Cowan Street such that southbound Cowan Street consists of two or three left-turn lanes, a shared through/right lane and a right-turn lane. Further, an additional westbound lane will enhance capacity at this intersection. A right-turn lane with sufficient storage is recommended on the eastbound approach of Jefferson Street as well. It may be necessary to widen the eastern portion of the Jefferson Street bridge in order to add the recommended eastbound lane along Jefferson Street. Other feasible alternatives which may not require the widening of the bridge in order to accommodate additional eastbound travel lane, should also be considered and analyzed.
- The results of capacity analyses indicated that with low-level roadway improvements within the study area as described in the evaluation section, approximately 22% of the newly generated Phase 1 trips can be accommodated by the study area roadway system. Maximizing the density within the River North development is best accommodated with the high-level roadway improvements described previously in this study. Those improvements include the proposed new connectors/bridges with partial movement accesses to I-24 and/or I-65, providing additional eastbound travel lane on Jefferson Street and the I-24 bridge over Spring Street, and additional turning lanes on Cowan Street at Jefferson Street/Spring Street. It is estimated that 133% of the PM peak hour (5,940 vehicles per hour) for Phase 1 can be accommodated by implementing those improvements.
- It should be noted that intersections along Jefferson Street/Spring Street within the study area currently operate at or near capacity during peak hours. Therefore, improving the operational performance and traffic flow of Jefferson Street/Spring Street within the study area is warranted as of today even without the completion of any stages of River North development. Any development along the east bank is likely to exacerbate this existing need and access and capacity improvements will be needed to provide adequate traffic operations within the study area.
- It should be noted that the thresholds of development identified in this study are based on trips that are projected to be generated by the development of the River North project. As the development of River North progresses, the land uses and sizes that are actually developed may be different than those assumed for this study. If this occurs, continuing to use PM peak hour trips as

the warranting criteria for improvements will be an effective way to ensure that the recommended improvements are provided when needed.

- The evaluation of the proposed improvements and estimation of the maximum newly generated trips for the proposed development under each phase can be used as a helpful tool to plan different stages of the development. However, the capacity analysis procedure used in this study was based on several assumptions. It is recommended that the development conduct traffic counts as certain portions of the development is being completed and occupied in order to identify actual trip generation for the developed portions of the River North development. Those counts will provide a stronger foundation to verify the assumptions made in this study and also to explore further improvements using the actual travel patterns in and out of the development.
- It is important to note that traffic impact assumptions in this study are conservative, meaning analyses of network impacts were limited to the immediate vicinity of the development. Given the site's size and location adjacent to downtown and critical regional roadway junctions, , impacts (positive or negative) will occur well beyond the site. Should more robust high-level improvements be constructed, such as additional bridge connections or interstate improvements, functionality of the greater network in this area may in fact improve. Neither TDOT nor Metro Nashville has significant infrastructure improvements planned for the near term in this area, and while new trips will be added, these potential high-level improvements could provide alternative connections in the downtown area.
- Higher density for the proposed development may be achieved by emphasizing ride-share, and public transportation. Based on Mayor Barry's Transportation Action Agenda (Moving the Music City) plan, Metro Nashville, in partnership with TDOT, is developing a plan called Nashville Complete Trips. As part of the plan, Metro will promote other modes of transportation by reaching out to major employers and connecting employers and commuters to information about transportation options such as the transit and bikeshare systems, flex-scheduling and telecommuting, bike parking, and MTA/RTA park-and-ride locations. This plan would provide more opportunities for public-private partnerships by the proposed development. Such partnerships could be accomplished by providing private ride-share vehicles and/or sponsoring public transportation commutes for the employees. Upon the success of sponsoring other modes of commute, higher density for the proposed development could potentially be achieved with less traffic impacts on the roadway system.

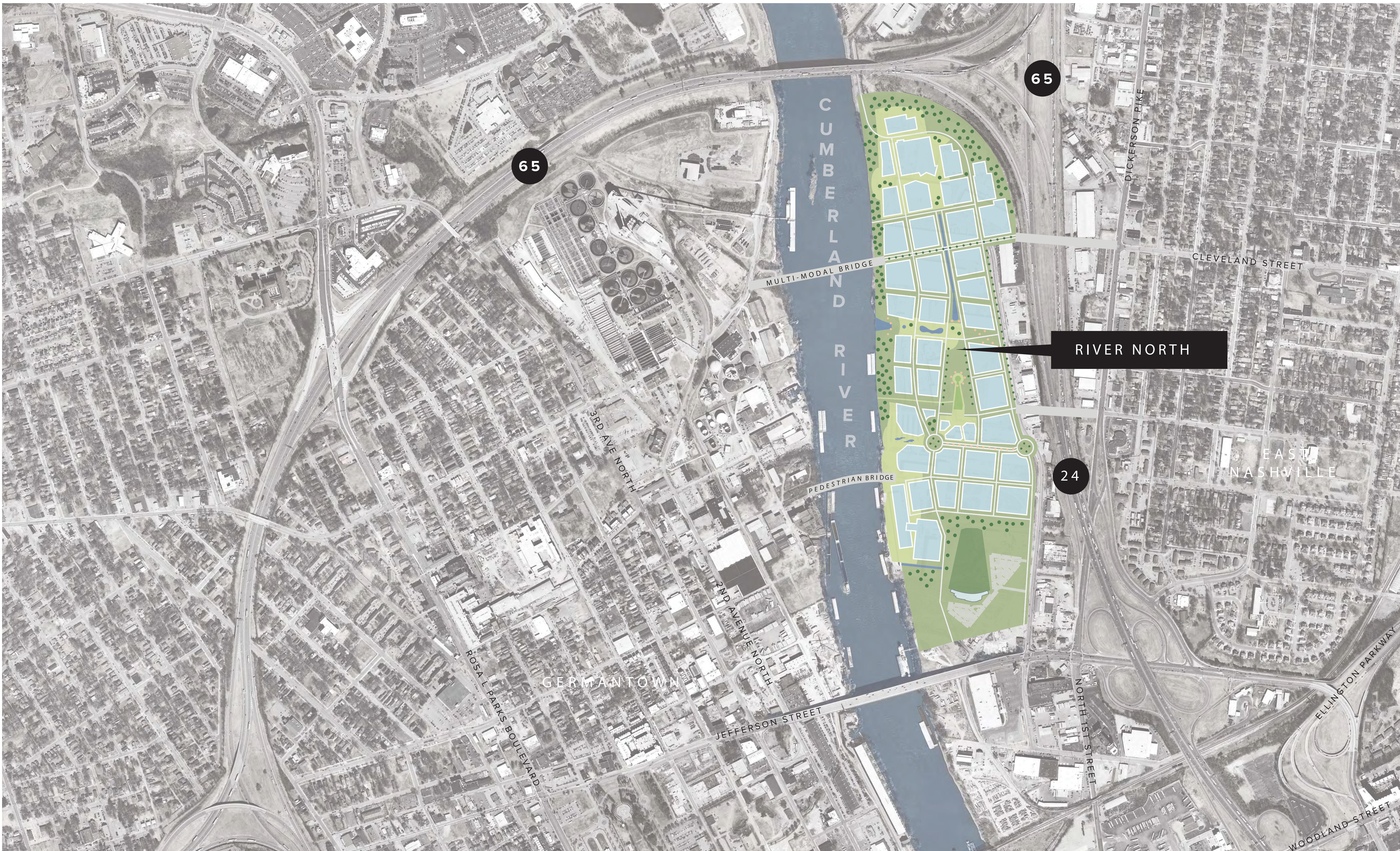
APPENDICES

- APPENDIX A
PRELIMINARY SITE PLAN
- APPENDIX B
DETAILED TURNING MOVEMENT COUNTS
- APPENDIX C
TDOT COUNT DATA
- APPENDIX D
CAPACITY ANALYSES
- APPENDIX E
TRIP GENERATION CALCULATIONS

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APPENDIX A
PRELIMINARY SITE PLAN



LANDINGS

AT RIVER NORTH



| PAD | PARCEL SIZE | GROSS BUILDABLE AREA (SF) | OFFICE (GROSS SF) | RESIDENTIAL (UNITS) | HOTEL (ROOMS) | RETAIL (SF) | NOTES |
|--------|-------------|---------------------------|-------------------|---------------------|---------------|-------------|-----------------------------------------------------------------------|
| A | +/- 2.4 AC | 524,000 | 456,000 | | | 68,000 | RETROFIT FOR RESTAURANTS, ENTERTAINMENT, EXPANDABLE TO ADD OTHER USES |
| B | +/- 1.5 AC | 327,000 | | 310 | | 25,000 | |
| C | +/- 2.2 AC | 480,000 | 455,000 | | | 25,000 | |
| D | +/- 1.8 AC | 393,000 | | 250 | 150 | 20,000 | |
| E | +/- 3.1 AC | 720,000 | | 460 | 250 | | |
| F | +/- 1.6 AC | 458,000 | 368,000 | | | 90,000 | RETAIL, OFFICE |
| G | +/- 1.4 AC | 306,000 | 150,000 | 90 | 150 | 20,000 | |
| H | +/- 1.2 AC | 262,000 | | 250 | | 10,000 | |
| I | +/- 1.8 AC | 395,000 | 395,000 | | | | |
| J | +/- 1.9 AC | 415,000 | | 375 | | | |
| K | +/- 1.9 AC | 415,000 | 415,000 | | | | |
| L | +/- 1.6 AC | 350,000 | 350,000 | | | | |
| M | +/- 1.9 AC | 415,000 | 415,000 | | | | |
| TOTALS | +/- 24.3 AC | 5,460,000 | 3,029,000 | 1,735 | 550 | 258,000 | |

APPENDIX B
DETAILED TURNING MOVEMENT COUNTS



INTERSECTION TRAFFIC VOLUME COUNTS

LOCATION: Dickerson Pike & Spring Street

DATE: 9/20/2016

RECORDER: SCU3FB/Zack Murphy

NOTES:

| LOCATION | Southbound | | | Northbound | | | Westbound | | | Eastbound | | |
|------------------|----------------|---|-----|----------------|---|---|---------------|-------|-------|---------------|-------|-----|
| | Dickerson Pike | | | Dickerson Pike | | | Spring Street | | | Spring Street | | |
| TIME | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 5:00-5:15 AM | | | | | | | | | | | | |
| 6:15-6:30 | | | | | | | | | | | | |
| 6:30-6:45 | | | | | | | | | | | | |
| 6:45-7:00 | | | | | | | | | | | | |
| 7:00-7:15 | 20 | | 59 | | | | 1 | 434 | 58 | 12 | 110 | 31 |
| 7:15-7:30 | 25 | | | 102 | | | | 454 | 43 | 15 | 116 | 29 |
| 7:30-7:45 | 31 | | | 101 | | | | 443 | 50 | 16 | 122 | 27 |
| 7:45-8:00 | 40 | | | 106 | | | | 467 | 43 | 24 | 141 | 24 |
| 8:00-8:15 | 42 | | | 112 | | | | 397 | 54 | 20 | 102 | 34 |
| 8:15-8:30 | 31 | | | 100 | | | | 424 | 45 | 18 | 93 | 21 |
| 8:30-8:45 | 24 | | | 88 | | | | 436 | 45 | 14 | 80 | 31 |
| 8:45-9:00 | 11 | | | 46 | | | | 417 | 58 | 13 | 111 | 27 |
| 9:00-9:15 | | | | | | | | | | | | |
| 9:15-9:30 | | | | | | | | | | | | |
| 9:30-9:45 | | | | | | | | | | | | |
| 9:45-10:00 | | | | | | | | | | | | |
| 10:00-10:15 | | | | | | | | | | | | |
| 10:15-10:30 | | | | | | | | | | | | |
| 10:30-10:45 | | | | | | | | | | | | |
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| 3:45-4:00 | | | | | | | | | | | | |
| 4:00-4:15 | 25 | | 30 | | | | | 227 | 111 | 31 | 253 | 44 |
| 4:15-4:30 | 19 | | 34 | | | | | 213 | 116 | 28 | 271 | 38 |
| 4:30-4:45 | 26 | | 35 | | | | | 234 | 113 | 40 | 268 | 46 |
| 4:45-5:00 | 21 | | 40 | | | | | 208 | 127 | 45 | 282 | 52 |
| 5:00-5:15 | 25 | | 30 | | | | | 202 | 156 | 44 | 262 | 54 |
| 5:15-5:30 | 18 | | 21 | | | | 1 | 203 | 162 | 49 | 289 | 37 |
| 5:30-5:45 | 16 | | 38 | | | | | 182 | 138 | 41 | 233 | 36 |
| 5:45-6:00 | 18 | | 36 | | | | | 196 | 118 | 52 | 256 | 19 |
| 6:00-6:15 | | | | | | | | | | | | |
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| 9:30-9:45 | | | | | | | | | | | | |
| 9:45-10:00 PM | | | | | | | | | | | | |
| TOTAL | 393 | | 357 | | | | 2 | 5,135 | 1,435 | 462 | 3,020 | 539 |
| AM PK HR | 138 | | 421 | | | | | 1,761 | 198 | 75 | 481 | 104 |
| MID PK HR | | | | | | | | | | | | |
| PM PK HR | 90 | | 126 | | | | 1 | 845 | 568 | 178 | 1,092 | 189 |

7:15 AM - 8:15 AM

4:30 PM - 5:30 PM



INTERSECTION TRAFFIC VOLUME COUNTS

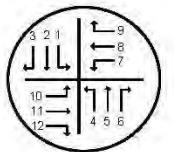
LOCATION: North 1st Street & Jefferson Street
DATE: 9/20/2016
RECORDER: SCU4XC/Zack Murphy
NOTES:

| LOCATION | Southbound | | | Northbound | | | Westbound | | | Eastbound | | |
|------------------|------------------|-------|-------|------------------|-----|-----|------------------|-------|-----|------------------|-------|-----|
| | North 1st Street | | | North 1st Street | | | Jefferson Street | | | Jefferson Street | | |
| TIME | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 6:00-6:15 AM | | | | | | | | | | | | |
| 6:15-6:30 | | | | | | | | | | | | |
| 6:30-6:45 | | | | | | | | | | | | |
| 6:45-7:00 | | | | | | | | | | | | |
| 7:00-7:15 | 87 | 83 | 150 | 12 | 19 | 16 | 18 | 238 | 4 | 26 | 139 | 10 |
| 7:15-7:30 | 64 | 84 | 153 | 7 | 28 | 28 | 16 | 269 | 2 | 20 | 151 | 8 |
| 7:30-7:45 | 65 | 106 | 136 | 15 | 20 | 26 | 11 | 255 | 4 | 23 | 168 | 19 |
| 7:45-8:00 | 65 | 100 | 109 | 21 | 24 | 23 | 13 | 329 | 1 | 27 | 161 | 27 |
| 8:00-8:15 | 54 | 93 | 127 | 15 | 22 | 25 | 17 | 281 | 6 | 27 | 145 | 20 |
| 8:15-8:30 | 60 | 128 | 128 | 16 | 31 | 30 | 26 | 274 | 5 | 24 | 132 | 17 |
| 8:30-8:45 | 47 | 82 | 90 | 13 | 24 | 29 | 20 | 254 | 5 | 25 | 143 | 17 |
| 8:45-9:00 | 60 | 55 | 93 | 25 | 28 | 23 | 17 | 211 | 1 | 43 | 140 | 8 |
| 9:00-9:15 | | | | | | | | | | | | |
| 9:15-9:30 | | | | | | | | | | | | |
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| 3:45-4:00 | | | | | | | | | | | | |
| 4:00-4:15 | 26 | 34 | 42 | 24 | 78 | 32 | 10 | 148 | 17 | 117 | 362 | 5 |
| 4:15-4:30 | 35 | 32 | 57 | 30 | 116 | 48 | 20 | 128 | 13 | 133 | 327 | 4 |
| 4:30-4:45 | 25 | 41 | 48 | 28 | 94 | 66 | 19 | 169 | 31 | 129 | 336 | 4 |
| 4:45-5:00 | 28 | 43 | 45 | 33 | 98 | 33 | 13 | 183 | 16 | 159 | 375 | 6 |
| 5:00-5:15 | 27 | 49 | 41 | 23 | 111 | 47 | 23 | 161 | 19 | 150 | 325 | 10 |
| 5:15-5:30 | 21 | 42 | 50 | 29 | 105 | 47 | 11 | 157 | 20 | 141 | 311 | 14 |
| 5:30-5:45 | 21 | 49 | 40 | 32 | 96 | 24 | 14 | 157 | 27 | 113 | 264 | 9 |
| 5:45-6:00 | 23 | 38 | 46 | 17 | 74 | 21 | 12 | 146 | 16 | 102 | 287 | 10 |
| 6:00-6:15 | | | | | | | | | | | | |
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| 9:15-9:30 | | | | | | | | | | | | |
| 9:30-9:45 | | | | | | | | | | | | |
| 9:45-10:00 PM | | | | | | | | | | | | |
| TOTAL | 698 | 1,059 | 1,367 | 340 | 366 | 520 | 264 | 3,300 | 109 | 1,259 | 3,796 | 188 |
| AM PK HR | 248 | 383 | 525 | 58 | 94 | 102 | 57 | 1,124 | 13 | 97 | 825 | 74 |
| MID PK HR | | | | | | | | | | | | |
| PM PK HR | 99 | 175 | 184 | 113 | 406 | 195 | 86 | 620 | 88 | 579 | 1,347 | 34 |

780
1,600
2,448
3,348
3,400
3,451
3,364
3,172
2,340
1,469
708

916
1,858
2,860
3,828
3,899
3,904
3,764
3,688
2,602
1,654
802

7:15 AM - 8:15 AM
4:30 PM - 5:30 PM



North

INTERSECTION TRAFFIC VOLUME COUNTS

LOCATION: Cowan Street & Jefferson Street
DATE: 9/20/2016
RECORDER: SCU5DA/Zack Murphy
NOTES:

| LOCATION | Southbound | | | Northbound | | | Westbound | | | Eastbound | | | |
|------------------|--------------|-----|-----|--------------|-----|-----|------------------|-------|-----|------------------|-------|-----|----|
| | Cowan Street | | | Cowan Street | | | Jefferson Street | | | Jefferson Street | | | |
| TIME | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | |
| 6:00-6:15 AM | | | | | | | | | | | | | |
| 6:15-6:30 | | | | | | | | | | | | | |
| 6:30-6:45 | | | | | | | | | | | | | |
| 6:45-7:00 | | | | | | | | | | | | | |
| 7:00-7:15 | 45 | 13 | 76 | 5 | 2 | 5 | 3 | 361 | 40 | 11 | 128 | 6 | |
| 7:15-7:30 | 48 | 13 | 72 | 1 | 5 | 2 | 5 | 420 | 28 | 12 | 139 | 4 | |
| 7:30-7:45 | 52 | 10 | 133 | 4 | 1 | 4 | 4 | 401 | 29 | 16 | 138 | 12 | |
| 7:45-8:00 | 60 | 11 | 128 | 4 | 1 | 4 | 2 | 435 | 37 | 12 | 166 | 11 | |
| 8:00-8:15 | 44 | 10 | 108 | 4 | 3 | 7 | | 439 | 30 | 15 | 138 | 12 | |
| 8:15-8:30 | 51 | 15 | 79 | 6 | 6 | 5 | 5 | 381 | 36 | 15 | 131 | 18 | |
| 8:30-8:45 | 40 | 10 | 73 | 6 | 3 | 12 | 19 | 375 | 37 | 17 | 123 | 14 | |
| 8:45-9:00 | 44 | 11 | 64 | 6 | 1 | 5 | 16 | 284 | 43 | 16 | 139 | 12 | |
| 9:00-9:15 | | | | | | | | | | | | | |
| 9:15-9:30 | | | | | | | | | | | | | |
| 9:30-9:45 | | | | | | | | | | | | | |
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| 3:30-3:45 | | | | | | | | | | | | | |
| 3:45-4:00 | | | | | | | | | | | | | |
| 4:00-4:15 | 30 | 11 | 30 | 6 | 17 | 14 | 9 | 183 | 52 | 46 | 461 | 25 | |
| 4:15-4:30 | 21 | 16 | 21 | 5 | 10 | 13 | 3 | 197 | 24 | 63 | 442 | 32 | |
| 4:30-4:45 | 46 | 12 | 25 | 14 | 12 | 11 | 7 | 199 | 33 | 62 | 421 | 32 | |
| 4:45-5:00 | 42 | 11 | 27 | 16 | 16 | 14 | 5 | 190 | 30 | 55 | 460 | 44 | |
| 5:00-5:15 | 30 | 8 | 26 | 10 | 15 | 18 | 2 | 199 | 25 | 56 | 456 | 41 | |
| 5:15-5:30 | 15 | 3 | 23 | 13 | 16 | 10 | 4 | 217 | 20 | 49 | 436 | 33 | |
| 5:30-5:45 | 23 | 4 | 18 | 5 | 6 | 11 | 3 | 206 | 26 | 41 | 378 | 19 | |
| 5:45-6:00 | 13 | 6 | 17 | 3 | | | 10 | 4 | 184 | 13 | 32 | 353 | 17 |
| 6:00-6:15 | | | | | | | | | | | | | |
| 6:15-6:30 | | | | | | | | | | | | | |
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| 9:30-9:45 | | | | | | | | | | | | | |
| 9:45-10:00 PM | | | | | | | | | | | | | |
| TOTAL | 604 | 164 | 920 | 108 | 114 | 145 | 91 | 4,671 | 503 | 518 | 4,507 | 332 | |
| AM PK HR | 204 | 44 | 441 | 13 | 10 | 17 | 11 | 1,695 | 124 | 55 | 579 | 39 | |
| MID PK HR | | | | | | | | | | | | | |
| PM PK HR | 133 | 34 | 101 | 53 | 59 | 53 | 18 | 805 | 108 | 222 | 1,773 | 150 | |

695
1,444
2,246
3,117
3,232
3,231
3,158
2,928
2,118
1,370
641

884
1,731
2,605
3,515
3,517
3,509
3,375
3,117
2,231
1,392
652

7:15 AM - 8:15 AM
4:30 PM - 5:30 PM



INTERSECTION TRAFFIC VOLUME COUNTS

LOCATION: Dickerson Pike & Spring Street

DATE: 9/20/2016

RECORDER: SCU3FB/Zack Murphy

NOTES:

| LOCATION | Southbound | | | Northbound | | | Westbound | | | Eastbound | | |
|------------------|----------------|---|-----|----------------|---|---|---------------|-------|-----|---------------|-----|----|
| | Dickerson Pike | | | Dickerson Pike | | | Spring Street | | | Spring Street | | |
| TIME | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 6:00-6:15 AM | | | | | | | | | | | | |
| 6:15-6:30 | | | | | | | | | | | | |
| 6:30-6:45 | | | | | | | | | | | | |
| 6:45-7:00 | | | | | | | | | | | | |
| 7:00-7:15 | 20 | | 59 | | | | 1 | 434 | 58 | 12 | 110 | 31 |
| 7:15-7:30 | 25 | | 102 | | | | | 454 | 43 | 15 | 116 | 29 |
| 7:30-7:45 | 31 | | 101 | | | | | 443 | 50 | 16 | 122 | 27 |
| 7:45-8:00 | 40 | | 106 | | | | | 467 | 43 | 20 | 141 | 24 |
| 8:00-8:15 | 42 | | 112 | | | | | 397 | 54 | 20 | 103 | 24 |
| 8:15-8:30 | 31 | | 100 | | | | | 424 | 45 | 18 | 93 | 21 |
| 8:30-8:45 | 24 | | 69 | | | | | 436 | 45 | 14 | 90 | 31 |
| 8:45-9:00 | 11 | | 46 | | | | | 417 | 58 | 13 | 111 | 27 |
| 9:00-9:15 | | | | | | | | | | | | |
| 9:15-9:30 | | | | | | | | | | | | |
| 9:30-9:45 | | | | | | | | | | | | |
| 9:45-10:00 | | | | | | | | | | | | |
| 10:00-10:15 | | | | | | | | | | | | |
| 10:15-10:30 | | | | | | | | | | | | |
| 10:30-10:45 | | | | | | | | | | | | |
| 10:45-11:00 | | | | | | | | | | | | |
| 11:00-11:15 | | | | | | | | | | | | |
| 11:15-11:30 | | | | | | | | | | | | |
| 11:30-11:45 | | | | | | | | | | | | |
| 11:45-12:00 PM | | | | | | | | | | | | |
| 12:00-12:15 | | | | | | | | | | | | |
| 12:15-12:30 | | | | | | | | | | | | |
| 12:30-12:45 | | | | | | | | | | | | |
| 12:45-1:00 | | | | | | | | | | | | |
| 1:00-1:15 | | | | | | | | | | | | |
| 1:15-1:30 | | | | | | | | | | | | |
| 1:30-1:45 | | | | | | | | | | | | |
| 1:45-2:00 | | | | | | | | | | | | |
| 2:00-2:15 | | | | | | | | | | | | |
| 2:15-2:30 | | | | | | | | | | | | |
| 2:30-2:45 | | | | | | | | | | | | |
| 2:45-3:00 | | | | | | | | | | | | |
| 3:00-3:15 | | | | | | | | | | | | |
| 3:15-3:30 | | | | | | | | | | | | |
| 3:30-3:45 | | | | | | | | | | | | |
| 3:45-4:00 | | | | | | | | | | | | |
| 4:00-4:15 | 25 | | 30 | | | | | 227 | 111 | 31 | 283 | 44 |
| 4:15-4:30 | 19 | | 34 | | | | | 213 | 110 | 28 | 271 | 38 |
| 4:30-4:45 | 26 | | 35 | | | | | 234 | 118 | 40 | 288 | 46 |
| 4:45-5:00 | 21 | | 46 | | | | | 206 | 127 | 45 | 283 | 52 |
| 5:00-5:15 | 25 | | 30 | | | | | 202 | 158 | 44 | 262 | 51 |
| 5:15-5:30 | 16 | | 21 | | | | 1 | 203 | 162 | 48 | 280 | 37 |
| 5:30-5:45 | 16 | | 36 | | | | | 162 | 136 | 41 | 233 | 35 |
| 5:45-6:00 | 18 | | 38 | | | | | 196 | 149 | 52 | 256 | 49 |
| 6:00-6:15 | | | | | | | | | | | | |
| 6:15-6:30 | | | | | | | | | | | | |
| 6:30-6:45 | | | | | | | | | | | | |
| 6:45-7:00 | | | | | | | | | | | | |
| 7:00-7:15 | | | | | | | | | | | | |
| 7:15-7:30 | | | | | | | | | | | | |
| 7:30-7:45 | | | | | | | | | | | | |
| 7:45-8:00 | | | | | | | | | | | | |
| 8:00-8:15 | | | | | | | | | | | | |
| 8:15-8:30 | | | | | | | | | | | | |
| 8:30-8:45 | | | | | | | | | | | | |
| 8:45-9:00 | | | | | | | | | | | | |
| 9:00-9:15 | | | | | | | | | | | | |
| 9:15-9:30 | | | | | | | | | | | | |
| 9:30-9:45 | | | | | | | | | | | | |
| 9:45-10:00 PM | | | | | | | | | | | | |
| TOTAL | 392 | | 957 | | 2 | | 5,135 | 1,435 | 462 | 3,020 | 539 | |
| AM PK HR | 128 | | 421 | | | | 1,761 | 190 | 75 | 481 | 104 | |
| MID PK HR | | | | | | | | | | | | |
| PM PK HR | 90 | | 126 | | 1 | | 845 | 560 | 178 | 1,092 | 169 | |

7:15 AM - 8:15 AM

4:30 PM - 5:30 PM

APPENDIX C
TDOT COUNT DATA

Station Information

Station 000315

Route I0065

Location [LOOPS] NASHVILLE

County Davidson

2016 93453

2015 103738

2014 97381

2013 90804

2012 95882

2011 94309

2010 97235

2009 95364

2008 93222

2007 103115

2006 96998

2005 95853

2004 92334

2003 92746

2002 88952

2001 88756

2000 72471

1999 71002

1998 63474

1997 78111

1996 80782

1995 75045

1994 71493

1993 87432

1992 77718

1991 64934

1990 61368

1989 65028

1988 67146

1987 75000

1986 74018

1985 57516

1984 NA

1983 NA

Station Information

| | |
|----------|-------------------------|
| Station | 000053 |
| Route | SR011 |
| Location | N OF JEFERSON ST BRIDGE |
| County | Davidson |
| 2016 | 18903 |
| 2015 | 17557 |
| 2014 | 16205 |
| 2013 | 16362 |
| 2012 | 16008 |
| 2011 | 15595 |
| 2010 | 15429 |
| 2009 | 18698 |
| 2008 | 17447 |
| 2007 | 18969 |
| 2006 | 20698 |
| 2005 | 20184 |
| 2004 | 22680 |
| 2003 | 21955 |
| 2002 | 21516 |
| 2001 | 21112 |
| 2000 | 21826 |
| 1999 | 21653 |
| 1998 | 24912 |
| 1997 | 22000 |
| 1996 | 19840 |
| 1995 | 25646 |
| 1994 | 16286 |
| 1993 | 14296 |
| 1992 | 16759 |
| 1991 | 28340 |
| 1990 | 22541 |
| 1989 | 26548 |
| 1988 | 28282 |
| 1987 | 21535 |
| 1986 | 21599 |
| 1985 | 19097 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|----------------------|
| Station | 000389 |
| Route | 04915 |
| Location | EASTLAND - SW OF 388 |
| County | Davidson |
| 2016 | 9309 |
| 2015 | 9432 |
| 2014 | 8930 |
| 2013 | 7716 |
| 2012 | 7171 |
| 2011 | 7328 |
| 2010 | 7252 |
| 2009 | 7961 |
| 2008 | 7729 |
| 2007 | 8117 |
| 2006 | 8801 |
| 2005 | 8623 |
| 2004 | 9725 |
| 2003 | 9765 |
| 2002 | 10454 |
| 2001 | 10692 |
| 2000 | 10546 |
| 1999 | 10134 |
| 1998 | 10525 |
| 1997 | 12373 |
| 1996 | 12468 |
| 1995 | 11051 |
| 1994 | 10772 |
| 1993 | 11402 |
| 1992 | 9639 |
| 1991 | 8340 |
| 1990 | 9220 |
| 1989 | 9285 |
| 1988 | 10062 |
| 1987 | 10005 |
| 1986 | 10498 |
| 1985 | 9926 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|----------------------------|
| Station | 000304 |
| Route | SR006 |
| Location | ELLINGTON PKWY - NASHVILLE |
| County | Davidson |
| 2016 | 50255 |
| 2015 | 50371 |
| 2014 | 46513 |
| 2013 | 45282 |
| 2012 | 42915 |
| 2011 | 40692 |
| 2010 | 41316 |
| 2009 | 38007 |
| 2008 | 42233 |
| 2007 | 44400 |
| 2006 | 39093 |
| 2005 | 46319 |
| 2004 | 45875 |
| 2003 | 45418 |
| 2002 | 42341 |
| 2001 | 39381 |
| 2000 | 37385 |
| 1999 | 43710 |
| 1998 | 45690 |
| 1997 | 42037 |
| 1996 | 40757 |
| 1995 | 41146 |
| 1994 | 39959 |
| 1993 | 34825 |
| 1992 | 31816 |
| 1991 | 32874 |
| 1990 | 35477 |
| 1989 | 36798 |
| 1988 | 34849 |
| 1987 | 34485 |
| 1986 | 35573 |
| 1985 | 27535 |
| 1984 | NA |
| 1983 | NA |

Station Information

Station 000387

Route 04915

Location EASTLAND - N OF GALLATIN RD

County Davidson

2016 6476

2015 6489

2014 6265

2013 6203

2012 6339

2011 5818

2010 5618

2009 5755

2008 6020

2007 5875

2006 5629

2005 6184

2004 6790

2003 6685

2002 7884

2001 7798

2000 6328

1999 6968

1998 8187

1997 9124

1996 6463

1995 7957

1994 6075

1993 5493

1992 6500

1991 6470

1990 6329

1989 5547

1988 6408

1987 6576

1986 5468

1985 5864

1984 NA

1983 NA

Station Information

Station 000224

Route SR006

Location ELLINGTON PKWY-E OF SPRING ST

County Davidson

2016 41246

2015 46791

2014 45829

2013 44726

2012 43117

2011 41325

2010 41129

2009 37709

2008 42033

2007 42230

2006 47602

2005 46597

2004 45916

2003 45454

2002 42514

2001 44231

2000 37966

1999 43188

1998 48124

1997 41792

1996 41569

1995 39028

1994 39115

1993 35933

1992 38096

1991 36281

1990 44593

1989 42994

1988 39707

1987 36574

1986 31942

1985 27608

1984 NA

1983 NA

Station Information

| | |
|----------|--------------------------|
| Station | 000223 |
| Route | SR011 |
| Location | NEAR JEFFERSON ST BRIDGE |
| County | Davidson |
| 2016 | 5437 |
| 2015 | 4443 |
| 2014 | 4397 |
| 2013 | 4337 |
| 2012 | 4303 |
| 2011 | 4153 |
| 2010 | 3954 |
| 2009 | 4154 |
| 2008 | 4033 |
| 2007 | 4002 |
| 2006 | 3578 |
| 2005 | 3719 |
| 2004 | 4246 |
| 2003 | 3993 |
| 2002 | 4096 |
| 2001 | 3967 |
| 2000 | 4293 |
| 1999 | 4303 |
| 1998 | 4611 |
| 1997 | 4533 |
| 1996 | 6014 |
| 1995 | 5724 |
| 1994 | 5362 |
| 1993 | 6632 |
| 1992 | 5809 |
| 1991 | 5021 |
| 1990 | 6824 |
| 1989 | 6491 |
| 1988 | 5391 |
| 1987 | 5305 |
| 1986 | 5249 |
| 1985 | 4639 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|----------------------|
| Station | 000300 |
| Route | I0024 |
| Location | [LOOPS] N OF MAIN ST |
| County | Davidson |
| 2016 | 112585 |
| 2015 | 111471 |
| 2014 | 106517 |
| 2013 | 111467 |
| 2012 | 102166 |
| 2011 | 98292 |
| 2010 | 100916 |
| 2009 | 94330 |
| 2008 | 102899 |
| 2007 | 104740 |
| 2006 | 107073 |
| 2005 | 103884 |
| 2004 | 104700 |
| 2003 | 102898 |
| 2002 | 100955 |
| 2001 | 93684 |
| 2000 | 109108 |
| 1999 | 106372 |
| 1998 | 95515 |
| 1997 | 104550 |
| 1996 | 106939 |
| 1995 | 101150 |
| 1994 | 97873 |
| 1993 | 96369 |
| 1992 | 74169 |
| 1991 | 94591 |
| 1990 | 81165 |
| 1989 | 77000 |
| 1988 | 75000 |
| 1987 | 73843 |
| 1986 | 63000 |
| 1985 | 56584 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|-----------------------------|
| Station | 000422 |
| Route | 03262 |
| Location | 3RD AVE N - NEAR I- 65 LOOP |
| County | Davidson |
| 2016 | 6143 |
| 2015 | 5965 |
| 2014 | 4992 |
| 2013 | 6046 |
| 2012 | 5874 |
| 2011 | 6173 |
| 2010 | 6203 |
| 2009 | 6444 |
| 2008 | 6600 |
| 2007 | 6497 |
| 2006 | 6669 |
| 2005 | 6388 |
| 2004 | 5807 |
| 2003 | 5240 |
| 2002 | 4971 |
| 2001 | 5609 |
| 2000 | 5818 |
| 1999 | 5655 |
| 1998 | 6507 |
| 1997 | 4724 |
| 1996 | 6300 |
| 1995 | 6886 |
| 1994 | 5615 |
| 1993 | 5834 |
| 1992 | 5523 |
| 1991 | 5600 |
| 1990 | 5412 |
| 1989 | 5417 |
| 1988 | 5263 |
| 1987 | 5817 |
| 1986 | 5095 |
| 1985 | 5489 |
| 1984 | NA |
| 1983 | NA |

Station Information

Station 000054

Route SR012

Location BETWEEN GARFIELD & HUONE

County Davidson

2016 18100

2015 16877

2014 15329

2013 15980

2012 15088

2011 13575

2010 15577

2009 14619

2008 16223

2007 16673

2006 17369

2005 17433

2004 17169

2003 16450

2002 16472

2001 16346

2000 16651

1999 18127

1998 16435

1997 17786

1996 17583

1995 19397

1994 19713

1993 16156

1992 18345

1991 12821

1990 11934

1989 13510

1988 15975

1987 13146

1986 10792

1985 7992

1984 NA

1983 NA

Station Information

Station 000390

Route NA

Location 2ND AVE. N. - NEAR JEFFERSON ST

County Davidson

2016 6119

2015 6262

2014 5722

2013 5754

2012 5350

2011 5976

2010 5543

2009 5885

2008 5876

2007 5829

2006 5774

2005 5708

2004 5038

2003 5504

2002 5226

2001 5163

2000 5107

1999 5120

1998 4922

1997 5406

1996 5309

1995 5953

1994 2327

1993 4310

1992 4300

1991 4294

1990 3671

1989 4301

1988 4140

1987 5486

1986 3578

1985 4070

1984 NA

1983 NA

Station Information

| | |
|----------|---------------------|
| Station | 000074 |
| Route | 03258 |
| Location | JEFFERSON ST BRIDGE |
| County | Davidson |
| 2016 | 31635 |
| 2015 | 31203 |
| 2014 | 29320 |
| 2013 | 27923 |
| 2012 | 28299 |
| 2011 | 27571 |
| 2010 | 26851 |
| 2009 | 24562 |
| 2008 | 28511 |
| 2007 | 30169 |
| 2006 | 30722 |
| 2005 | 31547 |
| 2004 | 32265 |
| 2003 | 30221 |
| 2002 | 31550 |
| 2001 | 32233 |
| 2000 | 30563 |
| 1999 | 35288 |
| 1998 | 38609 |
| 1997 | 33561 |
| 1996 | 28849 |
| 1995 | 30268 |
| 1994 | NA |
| 1993 | NA |
| 1992 | 24000 |
| 1991 | 23317 |
| 1990 | 18628 |
| 1989 | 22363 |
| 1988 | 23614 |
| 1987 | 26263 |
| 1986 | 22564 |
| 1985 | 26529 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|-------------------------------------|
| Station | 000393 |
| Route | 0F718 |
| Location | 5TH AVE. N. - INSIDE NASHVILLE LOOP |
| County | Davidson |
| 2016 | 2979 |
| 2015 | 2874 |
| 2014 | 3059 |
| 2013 | 2748 |
| 2012 | 2406 |
| 2011 | 2595 |
| 2010 | 2707 |
| 2009 | 2816 |
| 2008 | 3025 |
| 2007 | 3107 |
| 2006 | 3359 |
| 2005 | 3352 |
| 2004 | 3302 |
| 2003 | 3210 |
| 2002 | 3088 |
| 2001 | 2921 |
| 2000 | 3083 |
| 1999 | 3342 |
| 1998 | 3188 |
| 1997 | 3041 |
| 1996 | 2190 |
| 1995 | 2115 |
| 1994 | 2361 |
| 1993 | 2937 |
| 1992 | 2910 |
| 1991 | 2841 |
| 1990 | 2903 |
| 1989 | 3700 |
| 1988 | 3614 |
| 1987 | 3459 |
| 1986 | 3336 |
| 1985 | 4393 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|---------------------|
| Station | 000391 |
| Route | 03262 |
| Location | 3RD AVE - (ONE-WAY) |
| County | Davidson |
| 2016 | 1957 |
| 2015 | 2000 |
| 2014 | 1928 |
| 2013 | 2020 |
| 2012 | 2138 |
| 2011 | 2092 |
| 2010 | 2199 |
| 2009 | 2013 |
| 2008 | 2652 |
| 2007 | 2575 |
| 2006 | 2560 |
| 2005 | 2765 |
| 2004 | 2738 |
| 2003 | 2651 |
| 2002 | 2541 |
| 2001 | 2646 |
| 2000 | 2808 |
| 1999 | 3996 |
| 1998 | 5557 |
| 1997 | 5543 |
| 1996 | 5398 |
| 1995 | 8095 |
| 1994 | 6550 |
| 1993 | 6064 |
| 1992 | 5711 |
| 1991 | 4437 |
| 1990 | 5005 |
| 1989 | 4862 |
| 1988 | 5280 |
| 1987 | 4678 |
| 1986 | 4802 |
| 1985 | 4451 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|-------------------------------------|
| Station | 000154 |
| Route | 03266 |
| Location | N FIRST ST-B/T WOODLAND & SPRING ST |
| County | Davidson |
| 2016 | 9006 |
| 2015 | 9376 |
| 2014 | 8716 |
| 2013 | 8272 |
| 2012 | 8293 |
| 2011 | 8803 |
| 2010 | 8547 |
| 2009 | 11047 |
| 2008 | 9886 |
| 2007 | 11086 |
| 2006 | 12233 |
| 2005 | 11794 |
| 2004 | 13162 |
| 2003 | 12767 |
| 2002 | 11374 |
| 2001 | 10847 |
| 2000 | 11491 |
| 1999 | 13977 |
| 1998 | 13656 |
| 1997 | 16834 |
| 1996 | 14372 |
| 1995 | 20654 |
| 1994 | 16624 |
| 1993 | 13342 |
| 1992 | 13056 |
| 1991 | 10950 |
| 1990 | 13141 |
| 1989 | 14000 |
| 1988 | 13704 |
| 1987 | 15869 |
| 1986 | 16095 |
| 1985 | 16266 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|-------------------------|
| Station | 000194 |
| Route | I0024 |
| Location | B/T SPRING ST & MAIN ST |
| County | Davidson |
| 2016 | 129692 |
| 2015 | 131220 |
| 2014 | 124525 |
| 2013 | 129338 |
| 2012 | 117695 |
| 2011 | 115690 |
| 2010 | 117916 |
| 2009 | 107920 |
| 2008 | 116432 |
| 2007 | 118216 |
| 2006 | 120632 |
| 2005 | 117768 |
| 2004 | 115814 |
| 2003 | 115826 |
| 2002 | 112503 |
| 2001 | 105611 |
| 2000 | 121571 |
| 1999 | 112691 |
| 1998 | 108202 |
| 1997 | 119326 |
| 1996 | 122262 |
| 1995 | 112157 |
| 1994 | 112077 |
| 1993 | 103101 |
| 1992 | 76383 |
| 1991 | 98143 |
| 1990 | 88132 |
| 1989 | 96185 |
| 1988 | 82000 |
| 1987 | 80935 |
| 1986 | 67000 |
| 1985 | 60835 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|-------------------------|
| Station | 000153 |
| Route | 03252 |
| Location | NEAR WOODLAND ST BRIDGE |
| County | Davidson |
| 2016 | 25719 |
| 2015 | 26927 |
| 2014 | 23787 |
| 2013 | 22081 |
| 2012 | 21122 |
| 2011 | 21843 |
| 2010 | 19634 |
| 2009 | 19349 |
| 2008 | 19326 |
| 2007 | 21059 |
| 2006 | 20697 |
| 2005 | 21889 |
| 2004 | 21320 |
| 2003 | 20284 |
| 2002 | 22555 |
| 2001 | 23039 |
| 2000 | 19467 |
| 1999 | 20946 |
| 1998 | 22388 |
| 1997 | 20995 |
| 1996 | 22653 |
| 1995 | 20092 |
| 1994 | 26974 |
| 1993 | 27569 |
| 1992 | 18783 |
| 1991 | 20304 |
| 1990 | 16573 |
| 1989 | 20742 |
| 1988 | 20026 |
| 1987 | 20439 |
| 1986 | 21656 |
| 1985 | 19142 |
| 1984 | NA |
| 1983 | NA |

Station Information

Station 000220

Route 03244

Location E OF I-65

County Davidson

2016 7608

2015 7338

2014 7320

2013 7304

2012 7338

2011 7319

2010 7216

2009 7215

2008 7492

2007 7941

2006 8038

2005 8016

2004 9062

2003 8790

2002 9255

2001 9330

2000 8018

1999 9111

1998 8566

1997 9009

1996 8154

1995 15530

1994 11841

1993 8639

1992 8585

1991 8507

1990 8021

1989 4364

1988 8863

1987 8847

1986 8346

1985 9743

1984 NA

1983 NA

Station Information

| | |
|----------|---------------------------|
| Station | 000488 |
| Route | 03272 |
| Location | 5TH ST - N OF WOODLAND ST |
| County | Davidson |
| 2016 | 16646 |
| 2015 | 16346 |
| 2014 | 16324 |
| 2013 | 15680 |
| 2012 | 15924 |
| 2011 | 14138 |
| 2010 | 14526 |
| 2009 | 17258 |
| 2008 | 15649 |
| 2007 | 16472 |
| 2006 | 17171 |
| 2005 | 16713 |
| 2004 | 16422 |
| 2003 | 15864 |
| 2002 | 14358 |
| 2001 | 15834 |
| 2000 | 16195 |
| 1999 | 16467 |
| 1998 | 19346 |
| 1997 | 15691 |
| 1996 | 19798 |
| 1995 | 19528 |
| 1994 | 16239 |
| 1993 | 14395 |
| 1992 | 13991 |
| 1991 | NA |
| 1990 | NA |
| 1989 | NA |
| 1988 | NA |
| 1987 | NA |
| 1986 | NA |
| 1985 | NA |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|----------------------|
| Station | 000075 |
| Route | SR006 |
| Location | VIC MEM BRIDGE - CBD |
| County | Davidson |
| 2016 | 28363 |
| 2015 | 28174 |
| 2014 | 25326 |
| 2013 | 24513 |
| 2012 | 23735 |
| 2011 | 23308 |
| 2010 | 23759 |
| 2009 | 23321 |
| 2008 | 23917 |
| 2007 | 23220 |
| 2006 | 23923 |
| 2005 | 25387 |
| 2004 | 25162 |
| 2003 | 27026 |
| 2002 | 26835 |
| 2001 | 27907 |
| 2000 | 30207 |
| 1999 | 28434 |
| 1998 | 40316 |
| 1997 | 24041 |
| 1996 | 31519 |
| 1995 | 32169 |
| 1994 | 32390 |
| 1993 | 29739 |
| 1992 | 29592 |
| 1991 | 27111 |
| 1990 | 24410 |
| 1989 | 24233 |
| 1988 | 25669 |
| 1987 | 24163 |
| 1986 | 31721 |
| 1985 | 22134 |
| 1984 | NA |
| 1983 | NA |

Station Information

| | |
|----------|-------------------|
| Station | 000046 |
| Route | 03244 |
| Location | WOODLAND ST - CBD |
| County | Davidson |
| 2016 | 13823 |
| 2015 | 13811 |
| 2014 | 13388 |
| 2013 | 13239 |
| 2012 | 13137 |
| 2011 | 12333 |
| 2010 | 11817 |
| 2009 | 22087 |
| 2008 | 23335 |
| 2007 | 14758 |
| 2006 | 20569 |
| 2005 | 19970 |
| 2004 | 19393 |
| 2003 | 21435 |
| 2002 | 26960 |
| 2001 | 25451 |
| 2000 | 25835 |
| 1999 | 21649 |
| 1998 | 26950 |
| 1997 | 25374 |
| 1996 | 24547 |
| 1995 | 27518 |
| 1994 | 20116 |
| 1993 | 19896 |
| 1992 | 19272 |
| 1991 | 15639 |
| 1990 | 15682 |
| 1989 | 18300 |
| 1988 | 18255 |
| 1987 | 15194 |
| 1986 | 18314 |
| 1985 | 18206 |
| 1984 | NA |
| 1983 | NA |

Station Information

Station 000290

Route I0024

Location N OF SHELBY AVE

County Davidson

2016 139532

2015 141434

2014 134002

2013 138277

2012 127367

2011 124211

2010 128164

2009 116164

2008 122101

2007 122710

2006 127482

2005 125224

2004 123065

2003 124196

2002 120150

2001 112752

2000 127612

1999 120841

1998 117474

1997 128593

1996 130289

1995 119324

1994 118514

1993 110401

1992 89409

1991 101606

1990 99930

1989 95067

1988 88141

1987 83000

1986 82000

1985 75000

1984 NA

1983 NA

APPENDIX D
CAPACITY ANALYSES

EXISTING CONDITIONS
CAPACITY ANALYSES

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North
Existing AM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|-------|------|-------|
| Lane Configurations | ↖ | ↑↑ | ↖ | ↖ | ↑↑↑ | | ↖ | ↑ | | ↖ | ↑ | |
| Traffic Volume (veh/h) | 55 | 579 | 39 | 11 | 1695 | 124 | 13 | 10 | 17 | 204 | 44 | 441 |
| Future Volume (veh/h) | 55 | 579 | 39 | 11 | 1695 | 124 | 13 | 10 | 17 | 204 | 44 | 441 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 60 | 629 | 42 | 12 | 1842 | 135 | 14 | 11 | 18 | 222 | 48 | 479 |
| Adj No. of Lanes | 1 | 2 | 1 | 1 | 3 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 231 | 2212 | 990 | 486 | 2950 | 216 | 51 | 136 | 223 | 327 | 31 | 313 |
| Arrive On Green | 0.03 | 0.63 | 0.63 | 0.02 | 1.00 | 1.00 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 | 0.21 |
| Sat Flow, veh/h | 1774 | 3539 | 1583 | 1774 | 4837 | 353 | 872 | 637 | 1042 | 1375 | 146 | 1459 |
| Grp Volume(v), veh/h | 60 | 629 | 42 | 12 | 1289 | 688 | 14 | 0 | 29 | 222 | 0 | 527 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 1583 | 1774 | 1695 | 1800 | 872 | 0 | 1679 | 1375 | 0 | 1605 |
| Q Serve(g_s), s | 1.8 | 11.3 | 1.4 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 1.9 | 21.5 | 0.0 | 30.0 |
| Cycle Q Clear(g_c), s | 1.8 | 11.3 | 1.4 | 0.4 | 0.0 | 0.0 | 30.0 | 0.0 | 1.9 | 23.5 | 0.0 | 30.0 |
| Prop In Lane | 1.00 | | | 1.00 | | 0.20 | 1.00 | | 0.62 | 1.00 | | 0.91 |
| Lane Grp Cap(c), veh/h | 231 | 2212 | 990 | 486 | 2068 | 1098 | 51 | 0 | 360 | 327 | 0 | 344 |
| V/C Ratio(X) | 0.26 | 0.28 | 0.04 | 0.02 | 0.62 | 0.63 | 0.27 | 0.00 | 0.08 | 0.68 | 0.00 | 1.53 |
| Avail Cap(c_a), veh/h | 287 | 2212 | 990 | 568 | 2068 | 1098 | 51 | 0 | 360 | 327 | 0 | 344 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.69 | 0.69 | 0.69 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 9.6 | 12.0 | 10.1 | 10.3 | 0.0 | 0.0 | 70.0 | 0.0 | 44.0 | 53.4 | 0.0 | 55.0 |
| Incr Delay (d2), s/veh | 0.2 | 0.3 | 0.1 | 0.0 | 1.0 | 1.9 | 1.0 | 0.0 | 0.0 | 4.6 | 0.0 | 253.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.9 | 5.6 | 0.6 | 0.2 | 0.3 | 0.6 | 0.6 | 0.0 | 0.9 | 8.6 | 0.0 | 37.5 |
| LnGrp Delay(d),s/veh | 9.8 | 12.3 | 10.2 | 10.3 | 1.0 | 1.9 | 71.0 | 0.0 | 44.0 | 58.0 | 0.0 | 308.6 |
| LnGrp LOS | A | B | B | B | A | A | E | | D | E | | F |
| Approach Vol, veh/h | | 731 | | | 1989 | | | 43 | | 749 | | |
| Approach Delay, s/veh | | 12.0 | | | 1.4 | | | 52.8 | | 234.3 | | |
| Approach LOS | | B | | | A | | | D | | F | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 10.6 | 92.4 | | 37.0 | 8.5 | 94.5 | | 37.0 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | | 7.0 | | | | |
| Max Green Setting (Gmax), s | 8.0 | 81.0 | | 30.0 | 8.0 | 81.0 | | 30.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 3.8 | 2.0 | | 32.0 | 2.4 | 13.3 | | 32.0 | | | | |
| Green Ext Time (p_c), s | 0.0 | 10.5 | | 0.0 | 0.0 | 10.5 | | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 53.9 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
2: N 1st Street & Spring Street

River North
Existing AM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|-------|-------|
| Lane Configurations | ↑↑ | ↑↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 97 | 625 | 74 | 57 | 1124 | 13 | 58 | 94 | 102 | 248 | 383 | 525 |
| Future Volume (veh/h) | 97 | 625 | 74 | 57 | 1124 | 13 | 58 | 94 | 102 | 248 | 383 | 525 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 105 | 679 | 80 | 62 | 1222 | 14 | 63 | 102 | 111 | 270 | 416 | 571 |
| Adj No. of Lanes | 2 | 2 | 0 | 1 | 2 | 0 | 1 | 2 | 1 | 1 | 1 | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 226 | 1730 | 204 | 446 | 1907 | 22 | 144 | 362 | 162 | 336 | 293 | 498 |
| Arrive On Green | 0.13 | 1.00 | 1.00 | 0.05 | 0.53 | 0.53 | 0.05 | 0.10 | 0.10 | 0.11 | 0.16 | 0.16 |
| Sat Flow, veh/h | 3442 | 3191 | 376 | 1774 | 3584 | 41 | 1774 | 3539 | 1583 | 1774 | 1863 | 3167 |
| Grp Volume(v), veh/h | 105 | 376 | 383 | 62 | 603 | 633 | 63 | 102 | 111 | 270 | 416 | 571 |
| Grp Sat Flow(s),veh/h/ln | 1721 | 1770 | 1796 | 1774 | 1770 | 1856 | 1774 | 1770 | 1583 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 4.0 | 0.0 | 0.0 | 2.6 | 33.9 | 33.9 | 4.4 | 3.7 | 9.5 | 15.5 | 22.0 | 17.8 |
| Cycle Q Clear(g_c), s | 4.0 | 0.0 | 0.0 | 2.6 | 33.9 | 33.9 | 4.4 | 3.7 | 9.5 | 15.5 | 22.0 | 17.8 |
| Prop In Lane | 1.00 | | | 0.21 | 1.00 | | 0.02 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 226 | 959 | 974 | 446 | 942 | 987 | 144 | 362 | 162 | 336 | 293 | 498 |
| V/C Ratio(X) | 0.46 | 0.39 | 0.39 | 0.14 | 0.64 | 0.64 | 0.44 | 0.28 | 0.69 | 0.80 | 1.42 | 1.15 |
| Avail Cap(c_a), veh/h | 226 | 959 | 974 | 493 | 942 | 987 | 153 | 379 | 170 | 336 | 293 | 498 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.92 | 0.92 | 0.92 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 58.5 | 0.0 | 0.0 | 18.4 | 23.2 | 23.3 | 52.6 | 58.1 | 60.7 | 50.8 | 59.0 | 38.5 |
| Incr Delay (d2), s/veh | 1.7 | 1.1 | 1.1 | 0.1 | 3.3 | 3.2 | 0.8 | 0.2 | 8.3 | 12.3 | 208.4 | 87.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 1.9 | 0.3 | 0.3 | 1.2 | 17.3 | 18.1 | 2.2 | 1.8 | 4.5 | 10.3 | 28.2 | 13.8 |
| LnGrp Delay(d),s/veh | 60.2 | 1.1 | 1.1 | 18.5 | 26.6 | 26.4 | 53.4 | 58.3 | 69.0 | 63.2 | 267.4 | 126.2 |
| LnGrp LOS | E | A | A | B | C | C | D | E | E | E | F | F |
| Approach Vol, veh/h | 864 | | | | 1298 | | | 276 | | | 1257 | |
| Approach Delay, s/veh | 8.3 | | | | 26.1 | | | 61.5 | | | 159.4 | |
| Approach LOS | A | | | | C | | | E | | | F | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 15.7 | 81.0 | 22.0 | 21.3 | 14.3 | 82.4 | 14.3 | 29.0 | | | | |
| Change Period (Y+R _c), s | 6.5 | 6.5 | 6.5 | 7.0 | 7.0 | 6.5 | 7.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 8.5 | 74.5 | 15.5 | 15.0 | 11.0 | 71.5 | 8.0 | 22.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 6.0 | 35.9 | 17.5 | 11.5 | 4.6 | 2.0 | 6.4 | 24.0 | | | | |
| Green Ext Time (p_c), s | 0.1 | 2.9 | 0.0 | 1.5 | 0.0 | 2.2 | 0.0 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 69.9 | | | | | | | | | | | |
| HCM 2010 LOS | E | | | | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Spring Street & Dickerson Pike

River North

Existing AM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | SBL2 | SBL | SBR | NWL | NWR |
|-----------------------------------|-------|------|--------|------|---------------------------|------|------|-------|-------|------|------|
| Lane Configurations | | | | | | | | | | | |
| Traffic Volume (vph) | 75 | 481 | 104 | 0 | 1750 | 190 | 138 | 0 | 421 | 0 | 0 |
| Future Volume (vph) | 75 | 481 | 104 | 0 | 1750 | 190 | 138 | 0 | 421 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.5 | 6.5 | 6.5 | | 6.5 | 6.5 | 4.5 | | 4.5 | | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | | 0.91 | 0.91 | 1.00 | | 1.00 | | |
| Frt | 1.00 | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | | 0.85 | | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.95 | | 1.00 | | |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | | 3385 | 1441 | 1770 | | 1583 | | |
| Flt Permitted | 0.04 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.95 | | 1.00 | | |
| Satd. Flow (perm) | 79 | 3539 | 1583 | | 3385 | 1441 | 1770 | | 1583 | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 82 | 523 | 113 | 0 | 1902 | 207 | 150 | 0 | 458 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 36 | 0 | 0 | 43 | 0 | 0 | 123 | 0 | 0 |
| Lane Group Flow (vph) | 82 | 523 | 77 | 0 | 1923 | 143 | 150 | 0 | 335 | 0 | 0 |
| Turn Type | D.P+P | NA | custom | | NA | Perm | Prot | | Prot | | |
| Protected Phases | 1 | 2 | | | 2 3 | | 4 | | 4 | | |
| Permitted Phases | 2 3 | 2 3 | 2 3 | | | 2 3 | | | | | |
| Actuated Green, G (s) | 101.0 | 89.2 | 95.7 | | 95.7 | 95.7 | 23.5 | | 23.5 | | |
| Effective Green, g (s) | 101.0 | 89.2 | 95.7 | | 95.7 | 95.7 | 23.5 | | 23.5 | | |
| Actuated g/C Ratio | 0.72 | 0.64 | 0.68 | | 0.68 | 0.68 | 0.17 | | 0.17 | | |
| Clearance Time (s) | 6.5 | 6.5 | | | | | 4.5 | | 4.5 | | |
| Vehicle Extension (s) | 2.0 | 2.0 | | | | | 2.0 | | 2.0 | | |
| Lane Grp Cap (vph) | 121 | 2419 | 1082 | | 2313 | 985 | 297 | | 265 | | |
| v/s Ratio Prot | c0.03 | 0.13 | | | c0.57 | | 0.08 | | c0.21 | | |
| v/s Ratio Perm | 0.47 | 0.01 | 0.05 | | | 0.10 | | | | | |
| v/c Ratio | 0.68 | 0.22 | 0.07 | | 0.83 | 0.15 | 0.51 | | 1.26 | | |
| Uniform Delay, d1 | 26.7 | 10.7 | 7.4 | | 16.2 | 7.8 | 53.0 | | 58.2 | | |
| Progression Factor | 1.14 | 0.79 | 0.36 | | 0.32 | 0.12 | 1.00 | | 1.00 | | |
| Incremental Delay, d2 | 11.0 | 0.0 | 0.0 | | 1.5 | 0.0 | 0.5 | | 145.2 | | |
| Delay (s) | 41.3 | 8.5 | 2.6 | | 6.7 | 1.0 | 53.5 | | 203.5 | | |
| Level of Service | D | A | A | | A | A | D | | F | | |
| Approach Delay (s) | | 11.3 | | | 6.2 | | | 166.4 | | 0.0 | |
| Approach LOS | | B | | | A | | | F | | A | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 35.6 | | HCM 2000 Level of Service | | | | D | | |
| HCM 2000 Volume to Capacity ratio | | | 0.96 | | | | | | | | |
| Actuated Cycle Length (s) | | | 140.0 | | Sum of lost time (s) | | | | 22.0 | | |
| Intersection Capacity Utilization | | | 85.6% | | ICU Level of Service | | | | E | | |
| Analysis Period (min) | | | 15 | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
4: I-24 WB Off-Ramp & Spring Street

River North
Existing AM



| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|-----------------------------------|-------|------|------|---------------------------|------|-------|
| Lane Configurations | ↑↑ | | | ↑↑ | ↖↖ | ↗ |
| Traffic Volume (vph) | 619 | 0 | 0 | 1772 | 168 | 534 |
| Future Volume (vph) | 619 | 0 | 0 | 1772 | 168 | 534 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.5 | | | 6.5 | 4.5 | 4.0 |
| Lane Util. Factor | 0.95 | | | 0.95 | 0.97 | 1.00 |
| Frt | 1.00 | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 1.00 | | | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 3539 | | | 3539 | 3433 | 1583 |
| Flt Permitted | 1.00 | | | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 3539 | | | 3539 | 3433 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 673 | 0 | 0 | 1926 | 183 | 580 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 673 | 0 | 0 | 1926 | 183 | 580 |
| Turn Type | NA | | | NA | Prot | Free |
| Protected Phases | 6 7 | | | 6 7 | 5 8 | |
| Permitted Phases | | | | | | Free |
| Actuated Green, G (s) | 96.0 | | | 96.0 | 35.0 | 140.0 |
| Effective Green, g (s) | 96.0 | | | 96.0 | 35.0 | 140.0 |
| Actuated g/C Ratio | 0.69 | | | 0.69 | 0.25 | 1.00 |
| Clearance Time (s) | | | | | | |
| Vehicle Extension (s) | | | | | | |
| Lane Grp Cap (vph) | 2426 | | | 2426 | 858 | 1583 |
| v/s Ratio Prot | 0.19 | | | c0.54 | 0.05 | |
| v/s Ratio Perm | | | | | | c0.37 |
| v/c Ratio | 0.28 | | | 0.79 | 0.21 | 0.37 |
| Uniform Delay, d1 | 8.5 | | | 15.2 | 41.6 | 0.0 |
| Progression Factor | 0.69 | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.0 | | | 1.7 | 0.0 | 0.7 |
| Delay (s) | 5.9 | | | 16.9 | 41.6 | 0.7 |
| Level of Service | A | | | B | D | A |
| Approach Delay (s) | 5.9 | | | 16.9 | 10.5 | |
| Approach LOS | A | | | B | B | |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | 13.3 | | | HCM 2000 Level of Service | B | |
| HCM 2000 Volume to Capacity ratio | 0.77 | | | | | |
| Actuated Cycle Length (s) | 140.0 | | | Sum of lost time (s) | 22.0 | |
| Intersection Capacity Utilization | 64.0% | | | ICU Level of Service | B | |
| Analysis Period (min) | 15 | | | | | |

c Critical Lane Group

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North
Existing PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑↑ | | ↑ | ↑ | | ↑ | ↑ | |
| Traffic Volume (veh/h) | 222 | 1773 | 150 | 18 | 805 | 108 | 53 | 59 | 53 | 133 | 34 | 101 |
| Future Volume (veh/h) | 222 | 1773 | 150 | 18 | 805 | 108 | 53 | 59 | 53 | 133 | 34 | 101 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 |
| Adj Flow Rate, veh/h | 241 | 1927 | 163 | 20 | 875 | 117 | 58 | 64 | 58 | 145 | 37 | 110 |
| Adj No. of Lanes | 1 | 2 | 1 | 1 | 3 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 506 | 2279 | 1019 | 122 | 2687 | 358 | 189 | 172 | 156 | 214 | 79 | 235 |
| Arrive On Green | 0.07 | 0.64 | 0.64 | 0.03 | 1.00 | 1.00 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 | 0.19 |
| Sat Flow, veh/h | 1774 | 3539 | 1583 | 1774 | 4542 | 605 | 1236 | 902 | 817 | 1264 | 414 | 1231 |
| Grp Volume(v), veh/h | 241 | 1927 | 163 | 20 | 652 | 340 | 58 | 0 | 122 | 145 | 0 | 147 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 1583 | 1774 | 1695 | 1756 | 1236 | 0 | 1719 | 1264 | 0 | 1645 |
| Q Serve(g_s), s | 7.2 | 59.6 | 5.7 | 0.6 | 0.0 | 0.0 | 6.1 | 0.0 | 8.7 | 15.8 | 0.0 | 11.1 |
| Cycle Q Clear(g_c), s | 7.2 | 59.6 | 5.7 | 0.6 | 0.0 | 0.0 | 17.2 | 0.0 | 8.7 | 24.5 | 0.0 | 11.1 |
| Prop In Lane | 1.00 | | | 1.00 | | 0.34 | 1.00 | | 0.48 | 1.00 | | 0.75 |
| Lane Grp Cap(c), veh/h | 506 | 2279 | 1019 | 122 | 2006 | 1039 | 189 | 0 | 328 | 214 | 0 | 314 |
| V/C Ratio(X) | 0.48 | 0.85 | 0.16 | 0.16 | 0.33 | 0.33 | 0.31 | 0.00 | 0.37 | 0.68 | 0.00 | 0.47 |
| Avail Cap(c_a), veh/h | 589 | 2279 | 1019 | 196 | 2006 | 1039 | 200 | 0 | 344 | 226 | 0 | 329 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.83 | 0.83 | 0.83 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 8.7 | 19.5 | 9.9 | 21.4 | 0.0 | 0.0 | 58.0 | 0.0 | 49.3 | 60.0 | 0.0 | 50.3 |
| Incr Delay (d2), s/veh | 0.3 | 4.1 | 0.3 | 0.2 | 0.4 | 0.7 | 0.3 | 0.0 | 0.3 | 5.7 | 0.0 | 0.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 3.5 | 30.2 | 2.6 | 0.3 | 0.1 | 0.2 | 2.1 | 0.0 | 4.1 | 5.9 | 0.0 | 5.1 |
| LnGrp Delay(d),s/veh | 8.9 | 23.6 | 10.2 | 21.6 | 0.4 | 0.7 | 58.3 | 0.0 | 49.6 | 65.7 | 0.0 | 50.7 |
| LnGrp LOS | A | C | B | C | A | A | E | | D | E | | D |
| Approach Vol, veh/h | | 2331 | | | 1012 | | | 180 | | | 292 | |
| Approach Delay, s/veh | | 21.1 | | | 0.9 | | | 52.4 | | | 58.2 | |
| Approach LOS | | C | | | A | | | D | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 16.5 | 89.8 | | 33.7 | 9.2 | 97.1 | | 33.7 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | | 7.0 | 7.0 | 7.0 | | 7.0 | | | | |
| Max Green Setting (Gmax), s | 16.0 | 75.0 | | 28.0 | 8.0 | 83.0 | | 28.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 9.2 | 2.0 | | 19.2 | 2.6 | 61.6 | | 26.5 | | | | |
| Green Ext Time (p_c), s | 0.3 | 16.2 | | 0.9 | 0.0 | 11.4 | | 0.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 20.1 | | | | | | | | |
| HCM 2010 LOS | | | | C | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
2: N 1st Street & Spring Street

River North
Existing PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|-------|-------|------|------|------|
| Lane Configurations | ↑↑ | ↑↑ | | ↑ | ↑↑ | | ↑ | ↑↑ | ↑ | ↑↑ | ↑↑ | ↑ |
| Traffic Volume (veh/h) | 579 | 1347 | 34 | 66 | 620 | 86 | 113 | 406 | 195 | 99 | 175 | 184 |
| Future Volume (veh/h) | 579 | 1347 | 34 | 66 | 620 | 86 | 113 | 406 | 195 | 99 | 175 | 184 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A _{pbT}) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 629 | 1464 | 37 | 72 | 674 | 93 | 123 | 441 | 212 | 108 | 165 | 217 |
| Adj No. of Lanes | 2 | 2 | 0 | 1 | 2 | 0 | 1 | 2 | 1 | 1 | 1 | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 824 | 2066 | 52 | 251 | 1261 | 174 | 173 | 379 | 170 | 159 | 200 | 339 |
| Arrive On Green | 0.48 | 1.00 | 1.00 | 0.05 | 0.40 | 0.40 | 0.06 | 0.11 | 0.11 | 0.06 | 0.11 | 0.11 |
| Sat Flow, veh/h | 3442 | 3528 | 89 | 1774 | 3126 | 431 | 1774 | 3539 | 1583 | 1774 | 1863 | 3167 |
| Grp Volume(v), veh/h | 629 | 734 | 767 | 72 | 381 | 386 | 123 | 441 | 212 | 108 | 165 | 217 |
| Grp Sat Flow(s),veh/h/ln | 1721 | 1770 | 1847 | 1774 | 1770 | 1787 | 1774 | 1770 | 1583 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 21.0 | 0.0 | 0.0 | 3.7 | 22.9 | 23.0 | 8.0 | 15.0 | 15.0 | 7.6 | 12.1 | 5.7 |
| Cycle Q Clear(g_c), s | 21.0 | 0.0 | 0.0 | 3.7 | 22.9 | 23.0 | 8.0 | 15.0 | 15.0 | 7.6 | 12.1 | 5.7 |
| Prop In Lane | 1.00 | | 0.05 | 1.00 | | 0.24 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 824 | 1036 | 1082 | 251 | 714 | 721 | 173 | 379 | 170 | 159 | 200 | 339 |
| V/C Ratio(X) | 0.76 | 0.71 | 0.71 | 0.29 | 0.53 | 0.53 | 0.71 | 1.16 | 1.25 | 0.68 | 0.83 | 0.64 |
| Avail Cap(c_a), veh/h | 824 | 1036 | 1082 | 257 | 714 | 721 | 173 | 379 | 170 | 159 | 200 | 339 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.53 | 0.53 | 0.53 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 33.2 | 0.0 | 0.0 | 29.2 | 31.7 | 31.8 | 54.1 | 62.5 | 62.5 | 52.4 | 61.2 | 23.3 |
| Incr Delay (d2), s/veh | 2.4 | 2.2 | 2.1 | 0.2 | 2.8 | 2.8 | 11.0 | 98.5 | 151.7 | 9.2 | 22.7 | 3.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 10.1 | 0.6 | 0.6 | 1.8 | 11.8 | 11.9 | 1.4 | 12.5 | 13.7 | 4.1 | 7.5 | 2.6 |
| LnGrp Delay(d),s/veh | 35.6 | 2.2 | 2.1 | 29.4 | 34.6 | 34.6 | 65.1 | 161.0 | 214.2 | 61.6 | 83.9 | 26.4 |
| LnGrp LOS | D | A | A | C | C | C | E | F | F | E | F | C |
| Approach Vol, veh/h | 2130 | | | | 839 | | | 776 | | | 490 | |
| Approach Delay, s/veh | 12.0 | | | | 34.1 | | | 160.4 | | | 53.5 | |
| Approach LOS | B | | | | C | | | F | | | D | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 40.0 | 63.0 | 15.0 | 22.0 | 14.5 | 88.5 | 15.0 | 22.0 | | | | |
| Change Period (Y+R _c), s | 6.5 | 6.5 | 6.5 | 7.0 | 7.0 | 6.5 | 7.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 33.5 | 56.5 | 8.5 | 15.0 | 8.0 | 81.5 | 8.0 | 15.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 23.0 | 25.0 | 9.6 | 17.0 | 5.7 | 2.0 | 10.0 | 14.1 | | | | |
| Green Ext Time (p_c), s | 5.7 | 1.6 | 0.0 | 0.0 | 0.0 | 9.7 | 0.0 | 0.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 48.4 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis

3: Spring Street & Dickerson Pike

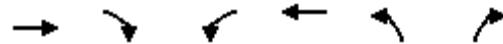
River North

Existing PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | SBL2 | SBL | SBR | NWL | NWR |
|-----------------------------------|-------|------|--------|------|---------------------------|-------|-------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | | | | ↑ | ↑ | ↑ | | |
| Traffic Volume (vph) | 178 | 1092 | 189 | 0 | 845 | 558 | 90 | 0 | 126 | 0 | 0 |
| Future Volume (vph) | 178 | 1092 | 189 | 0 | 845 | 558 | 90 | 0 | 126 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.5 | 6.5 | 6.5 | | 6.5 | 6.5 | 4.5 | | 4.5 | | |
| Lane Util. Factor | 1.00 | 0.95 | 1.00 | | 0.91 | 0.91 | 1.00 | | 1.00 | | |
| Frt | 1.00 | 1.00 | 0.85 | | 0.98 | 0.85 | 1.00 | | 0.85 | | |
| Flt Protected | 0.95 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.95 | | 1.00 | | |
| Satd. Flow (prot) | 1770 | 3539 | 1583 | | 3320 | 1441 | 1770 | | 1583 | | |
| Flt Permitted | 0.23 | 1.00 | 1.00 | | 1.00 | 1.00 | 0.95 | | 1.00 | | |
| Satd. Flow (perm) | 421 | 3539 | 1583 | | 3320 | 1441 | 1770 | | 1583 | | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 193 | 1187 | 205 | 0 | 918 | 607 | 98 | 0 | 137 | 0 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 57 | 0 | 7 | 127 | 0 | 0 | 122 | 0 | 0 |
| Lane Group Flow (vph) | 193 | 1187 | 148 | 0 | 1057 | 334 | 98 | 0 | 15 | 0 | 0 |
| Turn Type | D.P+P | NA | custom | | NA | Perm | Prot | | Prot | | |
| Protected Phases | 1 | 2 | | | 2 3 | | 4 | | 4 | | |
| Permitted Phases | 2 3 | 2 3 | 2 3 | | | 2 3 | | | | | |
| Actuated Green, G (s) | 109.0 | 94.8 | 101.3 | | 101.3 | 101.3 | 15.5 | | 15.5 | | |
| Effective Green, g (s) | 109.0 | 94.8 | 101.3 | | 101.3 | 101.3 | 15.5 | | 15.5 | | |
| Actuated g/C Ratio | 0.78 | 0.68 | 0.72 | | 0.72 | 0.72 | 0.11 | | 0.11 | | |
| Clearance Time (s) | 6.5 | 6.5 | | | | | 4.5 | | 4.5 | | |
| Vehicle Extension (s) | 2.0 | 2.0 | | | | | 2.0 | | 2.0 | | |
| Lane Grp Cap (vph) | 401 | 2560 | 1145 | | 2402 | 1042 | 195 | | 175 | | |
| v/s Ratio Prot | c0.03 | 0.30 | | | 0.32 | | c0.06 | | 0.01 | | |
| v/s Ratio Perm | c0.35 | 0.04 | 0.09 | | | 0.23 | | | | | |
| v/c Ratio | 0.48 | 0.46 | 0.13 | | 0.44 | 0.32 | 0.50 | | 0.09 | | |
| Uniform Delay, d1 | 4.7 | 10.6 | 5.9 | | 7.8 | 7.0 | 58.6 | | 55.9 | | |
| Progression Factor | 0.82 | 0.81 | 0.43 | | 1.11 | 3.36 | 1.00 | | 1.00 | | |
| Incremental Delay, d2 | 0.3 | 0.0 | 0.0 | | 0.0 | 0.1 | 0.7 | | 0.1 | | |
| Delay (s) | 4.2 | 8.6 | 2.5 | | 8.7 | 23.5 | 59.4 | | 56.0 | | |
| Level of Service | A | A | A | | A | C | E | | E | | |
| Approach Delay (s) | | 7.3 | | | 13.2 | | | 57.4 | | 0.0 | |
| Approach LOS | | A | | | B | | | E | | A | |
| Intersection Summary | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 13.5 | | HCM 2000 Level of Service | | | | B | | |
| HCM 2000 Volume to Capacity ratio | | | 0.51 | | | | | | | | |
| Actuated Cycle Length (s) | | | 140.0 | | Sum of lost time (s) | | | | 22.0 | | |
| Intersection Capacity Utilization | | | 58.3% | | ICU Level of Service | | | | B | | |
| Analysis Period (min) | | | 15 | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | |

HCM Signalized Intersection Capacity Analysis
4: I-24 WB Off-Ramp & Spring Street

River North
Existing PM



| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
|-----------------------------------|-------|------|------|---------------------------|-------|-------|
| Lane Configurations | ↑↑ | | | ↑↑ | ↖↖ | ↗ |
| Traffic Volume (vph) | 1152 | 0 | 0 | 1089 | 349 | 885 |
| Future Volume (vph) | 1152 | 0 | 0 | 1089 | 349 | 885 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.5 | | | 6.5 | 4.5 | 4.0 |
| Lane Util. Factor | 0.95 | | | 0.95 | 0.97 | 1.00 |
| Frt | 1.00 | | | 1.00 | 1.00 | 0.85 |
| Flt Protected | 1.00 | | | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 3539 | | | 3539 | 3433 | 1583 |
| Flt Permitted | 1.00 | | | 1.00 | 0.95 | 1.00 |
| Satd. Flow (perm) | 3539 | | | 3539 | 3433 | 1583 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 1252 | 0 | 0 | 1184 | 379 | 962 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 1252 | 0 | 0 | 1184 | 379 | 962 |
| Turn Type | NA | | | NA | Prot | Free |
| Protected Phases | 6 7 | | | 6 7 | 5 8 | |
| Permitted Phases | | | | | | Free |
| Actuated Green, G (s) | 103.5 | | | 103.5 | 27.5 | 140.0 |
| Effective Green, g (s) | 103.5 | | | 103.5 | 27.5 | 140.0 |
| Actuated g/C Ratio | 0.74 | | | 0.74 | 0.20 | 1.00 |
| Clearance Time (s) | | | | | | |
| Vehicle Extension (s) | | | | | | |
| Lane Grp Cap (vph) | 2616 | | | 2616 | 674 | 1583 |
| v/s Ratio Prot | 0.35 | | | 0.33 | 0.11 | |
| v/s Ratio Perm | | | | | c0.61 | |
| v/c Ratio | 0.48 | | | 0.45 | 0.56 | 0.61 |
| Uniform Delay, d1 | 7.4 | | | 7.2 | 50.8 | 0.0 |
| Progression Factor | 0.39 | | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.0 | | | 0.0 | 0.6 | 1.7 |
| Delay (s) | 2.9 | | | 7.2 | 51.5 | 1.7 |
| Level of Service | A | | | A | D | A |
| Approach Delay (s) | 2.9 | | | 7.2 | 15.8 | |
| Approach LOS | A | | | A | B | |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | 8.8 | | | HCM 2000 Level of Service | A | |
| HCM 2000 Volume to Capacity ratio | 0.72 | | | | | |
| Actuated Cycle Length (s) | 140.0 | | | Sum of lost time (s) | 22.0 | |
| Intersection Capacity Utilization | 51.0% | | | ICU Level of Service | A | |
| Analysis Period (min) | 15 | | | | | |

c Critical Lane Group

PROJECTED CONDITIONS
CAPACITY ANALYSES

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-Low-Level
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 267 | 1773 | 150 | 18 | 805 | 376 | 53 | 77 | 53 | 597 | 65 | 179 |
| Future Volume (veh/h) | 267 | 1773 | 150 | 18 | 805 | 376 | 53 | 77 | 53 | 597 | 65 | 179 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 290 | 1927 | 163 | 20 | 875 | 0 | 58 | 84 | 58 | 649 | 71 | 195 |
| Adj No. of Lanes | 1 | 2 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 478 | 1821 | 815 | 75 | 2157 | 672 | 159 | 102 | 71 | 691 | 615 | 523 |
| Arrive On Green | 0.11 | 0.51 | 0.51 | 0.03 | 0.85 | 0.00 | 0.10 | 0.10 | 0.10 | 0.20 | 0.33 | 0.33 |
| Sat Flow, veh/h | 1774 | 3539 | 1583 | 1774 | 5085 | 1583 | 1109 | 1028 | 710 | 3442 | 1863 | 1583 |
| Grp Volume(v), veh/h | 290 | 1927 | 163 | 20 | 875 | 0 | 58 | 0 | 142 | 649 | 71 | 195 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 1583 | 1774 | 1695 | 1583 | 1109 | 0 | 1738 | 1721 | 1863 | 1583 |
| Q Serve(g_s), s | 13.4 | 77.2 | 8.4 | 1.0 | 6.0 | 0.0 | 7.5 | 0.0 | 12.0 | 27.9 | 4.0 | 14.1 |
| Cycle Q Clear(g_c), s | 13.4 | 77.2 | 8.4 | 1.0 | 6.0 | 0.0 | 7.5 | 0.0 | 12.0 | 27.9 | 4.0 | 14.1 |
| Prop In Lane | 1.00 | | | 1.00 | | 1.00 | | 1.00 | | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 478 | 1821 | 815 | 75 | 2157 | 672 | 159 | 0 | 173 | 691 | 615 | 523 |
| V/C Ratio(X) | 0.61 | 1.06 | 0.20 | 0.27 | 0.41 | 0.00 | 0.37 | 0.00 | 0.82 | 0.94 | 0.12 | 0.37 |
| Avail Cap(c_a), veh/h | 574 | 1821 | 815 | 95 | 2157 | 672 | 285 | 0 | 371 | 700 | 832 | 707 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.83 | 0.83 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 19.1 | 36.4 | 19.7 | 36.8 | 7.0 | 0.0 | 64.1 | 0.0 | 66.2 | 59.1 | 35.0 | 38.3 |
| Incr Delay (d2), s/veh | 0.5 | 38.5 | 0.6 | 0.6 | 0.5 | 0.0 | 0.5 | 0.0 | 3.6 | 20.5 | 0.0 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 6.6 | 47.4 | 3.8 | 0.5 | 2.7 | 0.0 | 2.3 | 0.0 | 6.0 | 15.2 | 2.1 | 6.2 |
| LnGrp Delay(d),s/veh | 19.6 | 74.9 | 20.3 | 37.4 | 7.5 | 0.0 | 64.7 | 0.0 | 69.8 | 79.5 | 35.0 | 38.5 |
| LnGrp LOS | B | F | C | D | A | | E | | E | E | C | D |
| Approach Vol, veh/h | | 2380 | | | 895 | | | 200 | | | 915 | |
| Approach Delay, s/veh | | 64.4 | | | 8.1 | | | 68.3 | | | 67.3 | |
| Approach LOS | | E | | | A | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | | | 8 | | | |
| Phs Duration (G+Y+R _c), s | 22.8 | 70.6 | 34.6 | 22.0 | 9.3 | 84.2 | | | 56.6 | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 4.5 | 7.0 | 7.0 | 7.0 | | | 7.0 | | | |
| Max Green Setting (Gmax), s | 24.0 | 38.0 | 30.5 | 32.0 | 4.0 | 58.0 | | | 67.0 | | | |
| Max Q Clear Time (g_c+l1), s | 15.4 | 8.0 | 29.9 | 14.0 | 3.0 | 79.2 | | | 16.1 | | | |
| Green Ext Time (p_c), s | 0.4 | 13.1 | 0.2 | 0.9 | 0.0 | 0.0 | | | 1.0 | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 53.7 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-Medium-Level
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|-------|-------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 365 | 1773 | 150 | 18 | 805 | 964 | 53 | 116 | 53 | 1291 | 112 | 295 |
| Future Volume (veh/h) | 365 | 1773 | 150 | 18 | 805 | 964 | 53 | 116 | 53 | 1291 | 112 | 295 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 397 | 1927 | 163 | 20 | 875 | 0 | 58 | 126 | 58 | 1403 | 271 | 222 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 3 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 432 | 2192 | 682 | 86 | 1360 | 424 | 201 | 113 | 52 | 1473 | 648 | 551 |
| Arrive On Green | 0.18 | 0.43 | 0.43 | 0.01 | 0.27 | 0.00 | 0.04 | 0.09 | 0.09 | 0.28 | 0.35 | 0.35 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1208 | 556 | 5322 | 1863 | 1583 |
| Grp Volume(v), veh/h | 397 | 1927 | 163 | 20 | 875 | 0 | 58 | 0 | 184 | 1403 | 271 | 222 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1765 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 23.5 | 52.1 | 9.8 | 1.2 | 22.8 | 0.0 | 4.4 | 0.0 | 14.0 | 38.8 | 16.7 | 16.0 |
| Cycle Q Clear(g_c), s | 23.5 | 52.1 | 9.8 | 1.2 | 22.8 | 0.0 | 4.4 | 0.0 | 14.0 | 38.8 | 16.7 | 16.0 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.32 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 432 | 2192 | 682 | 86 | 1360 | 424 | 201 | 0 | 165 | 1473 | 648 | 551 |
| V/C Ratio(X) | 0.92 | 0.88 | 0.24 | 0.23 | 0.64 | 0.00 | 0.29 | 0.00 | 1.12 | 0.95 | 0.42 | 0.40 |
| Avail Cap(c_a), veh/h | 736 | 2192 | 682 | 100 | 1360 | 424 | 221 | 0 | 165 | 1490 | 648 | 551 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 32.9 | 39.1 | 27.1 | 42.2 | 48.6 | 0.0 | 58.4 | 0.0 | 68.0 | 53.3 | 37.3 | 37.1 |
| Incr Delay (d2), s/veh | 6.1 | 5.4 | 0.8 | 0.4 | 1.7 | 0.0 | 0.8 | 0.0 | 105.1 | 13.4 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 12.1 | 25.4 | 4.4 | 0.6 | 10.9 | 0.0 | 2.2 | 0.0 | 11.6 | 20.8 | 8.6 | 7.0 |
| LnGrp Delay(d),s/veh | 39.0 | 44.5 | 27.9 | 42.5 | 50.3 | 0.0 | 59.2 | 0.0 | 173.1 | 66.7 | 37.5 | 37.3 |
| LnGrp LOS | D | D | C | D | D | | E | | F | E | D | D |
| Approach Vol, veh/h | | 2487 | | | 895 | | | 242 | | | 1896 | |
| Approach Delay, s/veh | | 42.6 | | | 50.2 | | | 145.8 | | | 59.0 | |
| Approach LOS | | D | | | D | | | F | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 33.4 | 47.1 | 48.5 | 21.0 | 8.8 | 71.6 | 10.3 | 59.2 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 52.0 | 14.0 | 42.0 | 14.0 | 3.0 | 63.0 | 7.5 | 51.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 25.5 | 24.8 | 40.8 | 16.0 | 3.2 | 54.1 | 6.4 | 18.7 | | | | |
| Green Ext Time (p_c), s | 0.8 | 0.0 | 0.7 | 0.0 | 0.0 | 6.2 | 0.0 | 1.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 54.0 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 1A
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 294 | 1773 | 150 | 18 | 805 | 420 | 53 | 88 | 53 | 556 | 73 | 198 |
| Future Volume (veh/h) | 294 | 1773 | 150 | 18 | 805 | 420 | 53 | 88 | 53 | 556 | 73 | 198 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 320 | 1927 | 163 | 20 | 875 | 0 | 58 | 96 | 58 | 604 | 181 | 147 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 415 | 2607 | 812 | 110 | 2060 | 641 | 217 | 114 | 69 | 656 | 508 | 432 |
| Arrive On Green | 0.12 | 0.51 | 0.51 | 0.00 | 0.13 | 0.00 | 0.03 | 0.10 | 0.10 | 0.18 | 0.27 | 0.27 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1089 | 658 | 3548 | 1863 | 1583 |
| Grp Volume(v), veh/h | 320 | 1927 | 163 | 20 | 875 | 0 | 58 | 0 | 154 | 604 | 181 | 147 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1747 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 15.3 | 44.6 | 8.4 | 1.0 | 23.7 | 0.0 | 4.4 | 0.0 | 13.0 | 25.1 | 11.7 | 11.2 |
| Cycle Q Clear(g_c), s | 15.3 | 44.6 | 8.4 | 1.0 | 23.7 | 0.0 | 4.4 | 0.0 | 13.0 | 25.1 | 11.7 | 11.2 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.38 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 415 | 2607 | 812 | 110 | 2060 | 641 | 217 | 0 | 183 | 656 | 508 | 432 |
| V/C Ratio(X) | 0.77 | 0.74 | 0.20 | 0.18 | 0.42 | 0.00 | 0.27 | 0.00 | 0.84 | 0.92 | 0.36 | 0.34 |
| Avail Cap(c_a), veh/h | 570 | 2607 | 812 | 126 | 2060 | 641 | 217 | 0 | 262 | 710 | 621 | 528 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 0.33 | 0.33 | 0.33 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 24.1 | 28.7 | 19.9 | 29.1 | 48.9 | 0.0 | 57.6 | 0.0 | 66.0 | 60.1 | 43.9 | 43.7 |
| Incr Delay (d2), s/veh | 2.7 | 1.9 | 0.6 | 0.2 | 0.5 | 0.0 | 0.7 | 0.0 | 11.1 | 16.0 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 7.8 | 21.3 | 3.8 | 0.5 | 11.2 | 0.0 | 2.2 | 0.0 | 6.9 | 13.8 | 6.1 | 4.9 |
| LnGrp Delay(d),s/veh | 26.8 | 30.6 | 20.4 | 29.3 | 49.4 | 0.0 | 58.3 | 0.0 | 77.0 | 76.1 | 44.1 | 43.9 |
| LnGrp LOS | C | C | C | C | D | | E | | E | E | D | D |
| Approach Vol, veh/h | | 2410 | | | 895 | | | 212 | | | 932 | |
| Approach Delay, s/veh | | 29.4 | | | 48.9 | | | 71.9 | | | 64.8 | |
| Approach LOS | | C | | | D | | E | | | E | | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 24.8 | 67.8 | 34.7 | 22.7 | 8.7 | 83.9 | 9.5 | 47.9 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 31.0 | 38.5 | 30.0 | 22.5 | 3.0 | 66.5 | 5.0 | 50.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 17.3 | 25.7 | 27.1 | 15.0 | 3.0 | 46.6 | 6.4 | 13.7 | | | | |
| Green Ext Time (p_c), s | 0.6 | 8.1 | 0.6 | 0.7 | 0.0 | 10.5 | 0.0 | 1.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 42.8 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 1B
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 394 | 1773 | 150 | 18 | 805 | 858 | 53 | 128 | 53 | 1149 | 127 | 334 |
| Future Volume (veh/h) | 394 | 1773 | 150 | 18 | 805 | 858 | 53 | 128 | 53 | 1149 | 127 | 334 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 428 | 1927 | 163 | 20 | 875 | 0 | 58 | 139 | 58 | 1249 | 307 | 250 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 3 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 435 | 2121 | 660 | 85 | 1239 | 386 | 227 | 160 | 67 | 1293 | 653 | 555 |
| Arrive On Green | 0.19 | 0.42 | 0.42 | 0.01 | 0.24 | 0.00 | 0.04 | 0.13 | 0.13 | 0.24 | 0.35 | 0.35 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1249 | 521 | 5322 | 1863 | 1583 |
| Grp Volume(v), veh/h | 428 | 1927 | 163 | 20 | 875 | 0 | 58 | 0 | 197 | 1249 | 307 | 250 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1771 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 25.2 | 49.8 | 9.4 | 1.2 | 22.0 | 0.0 | 3.9 | 0.0 | 15.3 | 32.5 | 17.9 | 17.1 |
| Cycle Q Clear(g_c), s | 25.2 | 49.8 | 9.4 | 1.2 | 22.0 | 0.0 | 3.9 | 0.0 | 15.3 | 32.5 | 17.9 | 17.1 |
| Prop In Lane | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 0.29 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 435 | 2121 | 660 | 85 | 1239 | 386 | 227 | 0 | 226 | 1293 | 653 | 555 |
| V/C Ratio(X) | 0.98 | 0.91 | 0.25 | 0.23 | 0.71 | 0.00 | 0.26 | 0.00 | 0.87 | 0.97 | 0.47 | 0.45 |
| Avail Cap(c_a), veh/h | 435 | 2121 | 660 | 101 | 1239 | 386 | 231 | 0 | 253 | 1293 | 677 | 576 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 33.5 | 38.3 | 26.5 | 41.8 | 48.4 | 0.0 | 50.4 | 0.0 | 59.9 | 52.4 | 35.4 | 35.1 |
| Incr Delay (d2), s/veh | 38.4 | 7.2 | 0.9 | 0.4 | 2.5 | 0.0 | 0.6 | 0.0 | 22.8 | 17.4 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 21.1 | 24.6 | 4.3 | 0.6 | 10.6 | 0.0 | 2.0 | 0.0 | 8.9 | 18.0 | 9.2 | 7.5 |
| LnGrp Delay(d),s/veh | 71.9 | 45.5 | 27.4 | 42.2 | 50.9 | 0.0 | 50.9 | 0.0 | 82.7 | 69.9 | 35.6 | 35.3 |
| LnGrp LOS | E | D | C | D | D | | D | | F | E | D | D |
| Approach Vol, veh/h | | 2518 | | | 895 | | | 255 | | | 1806 | |
| Approach Delay, s/veh | | 48.8 | | | 50.7 | | | 75.5 | | | 59.2 | |
| Approach LOS | | D | | | D | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 33.0 | 41.1 | 41.0 | 24.9 | 8.7 | 65.4 | 9.8 | 56.1 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 26.0 | 32.0 | 34.0 | 20.0 | 3.0 | 55.0 | 5.6 | 50.9 | | | | |
| Max Q Clear Time (g_c+l1), s | 27.2 | 24.0 | 34.5 | 17.3 | 3.2 | 51.8 | 5.9 | 19.9 | | | | |
| Green Ext Time (p_c), s | 0.0 | 5.7 | 0.0 | 0.6 | 0.0 | 2.6 | 0.0 | 1.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 53.8 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 1C
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 287 | 1773 | 150 | 18 | 805 | 389 | 53 | 85 | 53 | 514 | 69 | 188 |
| Future Volume (veh/h) | 287 | 1773 | 150 | 18 | 805 | 389 | 53 | 85 | 53 | 514 | 69 | 188 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 312 | 1927 | 163 | 20 | 875 | 0 | 58 | 92 | 58 | 559 | 172 | 140 |
| Adj No. of Lanes | 1 | 2 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 442 | 1867 | 835 | 68 | 2164 | 674 | 216 | 110 | 69 | 610 | 481 | 408 |
| Arrive On Green | 0.11 | 0.53 | 0.53 | 0.01 | 0.43 | 0.00 | 0.03 | 0.10 | 0.10 | 0.17 | 0.26 | 0.26 |
| Sat Flow, veh/h | 1774 | 3539 | 1583 | 1774 | 5085 | 1583 | 1774 | 1070 | 674 | 3548 | 1863 | 1583 |
| Grp Volume(v), veh/h | 312 | 1927 | 163 | 20 | 875 | 0 | 58 | 0 | 150 | 559 | 172 | 140 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1744 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 14.3 | 79.1 | 8.1 | 1.0 | 17.9 | 0.0 | 4.4 | 0.0 | 12.7 | 23.2 | 11.3 | 10.8 |
| Cycle Q Clear(g_c), s | 14.3 | 79.1 | 8.1 | 1.0 | 17.9 | 0.0 | 4.4 | 0.0 | 12.7 | 23.2 | 11.3 | 10.8 |
| Prop In Lane | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.39 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 442 | 1867 | 835 | 68 | 2164 | 674 | 216 | 0 | 179 | 610 | 481 | 408 |
| V/C Ratio(X) | 0.71 | 1.03 | 0.20 | 0.29 | 0.40 | 0.00 | 0.27 | 0.00 | 0.84 | 0.92 | 0.36 | 0.34 |
| Avail Cap(c_a), veh/h | 714 | 1867 | 835 | 83 | 2164 | 674 | 216 | 0 | 285 | 662 | 621 | 528 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 20.9 | 35.4 | 18.7 | 37.6 | 29.9 | 0.0 | 57.9 | 0.0 | 66.1 | 61.1 | 45.5 | 45.3 |
| Incr Delay (d2), s/veh | 0.8 | 29.7 | 0.5 | 0.6 | 0.4 | 0.0 | 0.7 | 0.0 | 6.2 | 16.2 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 7.1 | 46.1 | 3.7 | 0.5 | 8.4 | 0.0 | 2.2 | 0.0 | 6.4 | 12.8 | 5.9 | 4.7 |
| LnGrp Delay(d),s/veh | 21.7 | 65.1 | 19.2 | 38.3 | 30.3 | 0.0 | 58.5 | 0.0 | 72.2 | 77.2 | 45.7 | 45.5 |
| LnGrp LOS | C | F | B | D | C | | E | | E | E | D | D |
| Approach Vol, veh/h | 2402 | | | | 895 | | | 208 | | | 871 | |
| Approach Delay, s/veh | 56.4 | | | | 30.5 | | | 68.4 | | | 65.9 | |
| Approach LOS | E | | | | C | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 24.0 | 70.8 | 32.8 | 22.4 | 8.7 | 86.1 | 9.5 | 45.7 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 40.0 | 29.5 | 28.0 | 24.5 | 3.0 | 66.5 | 5.0 | 50.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 16.3 | 19.9 | 25.2 | 14.7 | 3.0 | 81.1 | 6.4 | 13.3 | | | | |
| Green Ext Time (p_c), s | 0.6 | 6.7 | 0.6 | 0.7 | 0.0 | 0.0 | 0.0 | 0.9 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | 53.5 | | | | | | | | | | | |
| HCM 2010 LOS | D | | | | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 2A
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 254 | 1596 | 150 | 18 | 724 | 757 | 53 | 97 | 53 | 1012 | 85 | 144 |
| Future Volume (veh/h) | 254 | 1596 | 150 | 18 | 724 | 757 | 53 | 97 | 53 | 1012 | 85 | 144 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 276 | 1735 | 163 | 20 | 787 | 0 | 58 | 105 | 58 | 1100 | 141 | 124 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 354 | 1890 | 588 | 84 | 1334 | 415 | 241 | 123 | 68 | 1090 | 737 | 626 |
| Arrive On Green | 0.12 | 0.37 | 0.37 | 0.01 | 0.26 | 0.00 | 0.04 | 0.11 | 0.11 | 0.31 | 0.40 | 0.40 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1129 | 624 | 3548 | 1863 | 1583 |
| Grp Volume(v), veh/h | 276 | 1735 | 163 | 20 | 787 | 0 | 58 | 0 | 163 | 1100 | 141 | 124 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1753 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 15.5 | 45.6 | 10.1 | 1.2 | 18.9 | 0.0 | 4.0 | 0.0 | 12.8 | 43.0 | 6.9 | 7.2 |
| Cycle Q Clear(g_c), s | 15.5 | 45.6 | 10.1 | 1.2 | 18.9 | 0.0 | 4.0 | 0.0 | 12.8 | 43.0 | 6.9 | 7.2 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.36 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 354 | 1890 | 588 | 84 | 1334 | 415 | 241 | 0 | 191 | 1090 | 737 | 626 |
| V/C Ratio(X) | 0.78 | 0.92 | 0.28 | 0.24 | 0.59 | 0.00 | 0.24 | 0.00 | 0.85 | 1.01 | 0.19 | 0.20 |
| Avail Cap(c_a), veh/h | 354 | 1890 | 588 | 100 | 1334 | 415 | 242 | 0 | 250 | 1090 | 798 | 679 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 32.7 | 42.0 | 30.8 | 40.8 | 45.1 | 0.0 | 52.6 | 0.0 | 61.3 | 48.5 | 27.7 | 27.8 |
| Incr Delay (d2), s/veh | 9.7 | 8.7 | 1.2 | 0.4 | 1.4 | 0.0 | 0.5 | 0.0 | 15.7 | 29.6 | 0.0 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 8.5 | 22.9 | 4.6 | 0.6 | 9.1 | 0.0 | 2.0 | 0.0 | 7.0 | 25.5 | 3.6 | 3.2 |
| LnGrp Delay(d),s/veh | 42.4 | 50.6 | 32.0 | 41.2 | 46.5 | 0.0 | 53.1 | 0.0 | 77.0 | 78.1 | 27.7 | 27.8 |
| LnGrp LOS | D | D | C | D | D | | D | | E | F | C | C |
| Approach Vol, veh/h | 2174 | | | | 807 | | | | 221 | | | 1365 |
| Approach Delay, s/veh | 48.2 | | | | 46.3 | | | | 70.7 | | | 68.3 |
| Approach LOS | D | | | | D | | | | E | | | E |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 24.0 | 43.7 | 50.0 | 22.3 | 8.7 | 59.0 | 9.9 | 62.4 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 17.0 | 32.0 | 43.0 | 20.0 | 3.0 | 46.0 | 5.5 | 60.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 17.5 | 20.9 | 45.0 | 14.8 | 3.2 | 47.6 | 6.0 | 9.2 | | | | |
| Green Ext Time (p_c), s | 0.0 | 6.6 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 0.9 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 55.0 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 2B
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|-------|-------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 271 | 1596 | 150 | 18 | 724 | 1111 | 53 | 117 | 53 | 1494 | 113 | 167 |
| Future Volume (veh/h) | 271 | 1596 | 150 | 18 | 724 | 1111 | 53 | 117 | 53 | 1494 | 113 | 167 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 295 | 1735 | 163 | 20 | 787 | 0 | 58 | 127 | 58 | 1624 | 167 | 152 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 3 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 364 | 1843 | 574 | 81 | 1196 | 372 | 219 | 113 | 51 | 1769 | 753 | 640 |
| Arrive On Green | 0.14 | 0.36 | 0.36 | 0.01 | 0.24 | 0.00 | 0.04 | 0.09 | 0.09 | 0.33 | 0.40 | 0.40 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1212 | 553 | 5322 | 1863 | 1583 |
| Grp Volume(v), veh/h | 295 | 1735 | 163 | 20 | 787 | 0 | 58 | 0 | 185 | 1624 | 167 | 152 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1765 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 17.1 | 46.2 | 10.2 | 1.2 | 19.6 | 0.0 | 4.1 | 0.0 | 13.0 | 41.0 | 8.2 | 8.9 |
| Cycle Q Clear(g_c), s | 17.1 | 46.2 | 10.2 | 1.2 | 19.6 | 0.0 | 4.1 | 0.0 | 13.0 | 41.0 | 8.2 | 8.9 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.31 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 364 | 1843 | 574 | 81 | 1196 | 372 | 219 | 0 | 164 | 1769 | 753 | 640 |
| V/C Ratio(X) | 0.81 | 0.94 | 0.28 | 0.25 | 0.66 | 0.00 | 0.27 | 0.00 | 1.13 | 0.92 | 0.22 | 0.24 |
| Avail Cap(c_a), veh/h | 497 | 1843 | 574 | 97 | 1196 | 372 | 219 | 0 | 164 | 1901 | 798 | 679 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 34.2 | 43.2 | 31.7 | 43.2 | 48.4 | 0.0 | 54.5 | 0.0 | 63.5 | 44.9 | 27.3 | 27.5 |
| Incr Delay (d2), s/veh | 5.0 | 11.1 | 1.2 | 0.4 | 2.1 | 0.0 | 0.6 | 0.0 | 109.1 | 7.0 | 0.1 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 8.8 | 23.6 | 4.7 | 0.6 | 9.4 | 0.0 | 2.0 | 0.0 | 11.3 | 21.3 | 4.2 | 3.9 |
| LnGrp Delay(d),s/veh | 39.3 | 54.3 | 33.0 | 43.7 | 50.5 | 0.0 | 55.2 | 0.0 | 172.6 | 51.9 | 27.4 | 27.6 |
| LnGrp LOS | D | D | C | D | D | | E | | F | D | C | C |
| Approach Vol, veh/h | 2193 | | | | 807 | | | 243 | | | 1943 | |
| Approach Delay, s/veh | 50.7 | | | | 50.4 | | | 144.5 | | | 47.9 | |
| Approach LOS | D | | | | D | | | F | | | D | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 26.5 | 39.9 | 53.5 | 20.0 | 8.7 | 57.7 | 10.0 | 63.6 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 30.0 | 19.0 | 50.0 | 13.0 | 3.0 | 46.0 | 5.5 | 60.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 19.1 | 21.6 | 43.0 | 15.0 | 3.2 | 48.2 | 6.1 | 10.9 | | | | |
| Green Ext Time (p_c), s | 0.5 | 0.0 | 3.5 | 0.0 | 0.0 | 0.0 | 0.0 | 1.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 54.0 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 2C
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 239 | 1596 | 150 | 18 | 724 | 463 | 53 | 80 | 53 | 613 | 62 | 124 |
| Future Volume (veh/h) | 239 | 1596 | 150 | 18 | 724 | 463 | 53 | 80 | 53 | 613 | 62 | 124 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 260 | 1735 | 163 | 20 | 787 | 0 | 58 | 87 | 58 | 666 | 118 | 101 |
| Adj No. of Lanes | 1 | 2 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 409 | 1777 | 795 | 74 | 2118 | 659 | 221 | 103 | 68 | 716 | 528 | 449 |
| Arrive On Green | 0.10 | 0.50 | 0.50 | 0.00 | 0.14 | 0.00 | 0.03 | 0.10 | 0.10 | 0.20 | 0.28 | 0.28 |
| Sat Flow, veh/h | 1774 | 3539 | 1583 | 1774 | 5085 | 1583 | 1774 | 1044 | 696 | 3548 | 1863 | 1583 |
| Grp Volume(v), veh/h | 260 | 1735 | 163 | 20 | 787 | 0 | 58 | 0 | 145 | 666 | 118 | 101 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1740 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 12.2 | 71.8 | 8.6 | 1.0 | 21.1 | 0.0 | 4.4 | 0.0 | 12.3 | 27.7 | 7.3 | 7.3 |
| Cycle Q Clear(g_c), s | 12.2 | 71.8 | 8.6 | 1.0 | 21.1 | 0.0 | 4.4 | 0.0 | 12.3 | 27.7 | 7.3 | 7.3 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.40 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 409 | 1777 | 795 | 74 | 2118 | 659 | 221 | 0 | 171 | 716 | 528 | 449 |
| V/C Ratio(X) | 0.64 | 0.98 | 0.21 | 0.27 | 0.37 | 0.00 | 0.26 | 0.00 | 0.85 | 0.93 | 0.22 | 0.23 |
| Avail Cap(c_a), veh/h | 497 | 1777 | 795 | 89 | 2118 | 659 | 221 | 0 | 238 | 757 | 621 | 528 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 0.33 | 0.33 | 0.33 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 22.6 | 36.5 | 20.7 | 37.7 | 46.9 | 0.0 | 58.5 | 0.0 | 66.5 | 58.8 | 41.1 | 41.1 |
| Incr Delay (d2), s/veh | 0.9 | 16.5 | 0.6 | 0.5 | 0.4 | 0.0 | 0.6 | 0.0 | 13.8 | 17.0 | 0.1 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 6.0 | 39.0 | 3.9 | 0.5 | 10.0 | 0.0 | 2.2 | 0.0 | 6.6 | 15.3 | 3.7 | 3.2 |
| LnGrp Delay(d),s/veh | 23.5 | 52.9 | 21.3 | 38.2 | 47.2 | 0.0 | 59.1 | 0.0 | 80.3 | 75.8 | 41.2 | 41.2 |
| LnGrp LOS | C | D | C | D | D | | E | | F | E | D | D |
| Approach Vol, veh/h | | 2158 | | | 807 | | | 203 | | | 885 | |
| Approach Delay, s/veh | | 47.0 | | | 47.0 | | | 74.3 | | | 67.3 | |
| Approach LOS | | D | | | D | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 21.5 | 69.5 | 37.3 | 21.7 | 8.7 | 82.3 | 9.5 | 49.5 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 22.0 | 47.5 | 32.0 | 20.5 | 3.0 | 66.5 | 5.0 | 50.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 14.2 | 23.1 | 29.7 | 14.3 | 3.0 | 73.8 | 6.4 | 9.3 | | | | |
| Green Ext Time (p_c), s | 0.3 | 10.3 | 0.6 | 0.4 | 0.0 | 0.0 | 0.0 | 0.7 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 52.8 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 3A
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 380 | 1773 | 150 | 18 | 805 | 606 | 53 | 122 | 53 | 807 | 119 | 315 |
| Future Volume (veh/h) | 380 | 1773 | 150 | 18 | 805 | 606 | 53 | 122 | 53 | 807 | 119 | 315 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 413 | 1927 | 163 | 20 | 875 | 0 | 58 | 133 | 58 | 877 | 289 | 236 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 432 | 2026 | 631 | 84 | 1112 | 346 | 235 | 157 | 68 | 873 | 661 | 562 |
| Arrive On Green | 0.19 | 0.40 | 0.40 | 0.01 | 0.22 | 0.00 | 0.04 | 0.13 | 0.13 | 0.25 | 0.35 | 0.35 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1231 | 537 | 3548 | 1863 | 1583 |
| Grp Volume(v), veh/h | 413 | 1927 | 163 | 20 | 875 | 0 | 58 | 0 | 191 | 877 | 289 | 236 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1768 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 23.2 | 47.7 | 9.0 | 1.1 | 21.1 | 0.0 | 3.7 | 0.0 | 13.7 | 32.0 | 15.4 | 14.7 |
| Cycle Q Clear(g_c), s | 23.2 | 47.7 | 9.0 | 1.1 | 21.1 | 0.0 | 3.7 | 0.0 | 13.7 | 32.0 | 15.4 | 14.7 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.30 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 432 | 2026 | 631 | 84 | 1112 | 346 | 235 | 0 | 226 | 873 | 661 | 562 |
| V/C Ratio(X) | 0.96 | 0.95 | 0.26 | 0.24 | 0.79 | 0.00 | 0.25 | 0.00 | 0.85 | 1.00 | 0.44 | 0.42 |
| Avail Cap(c_a), veh/h | 432 | 2026 | 631 | 102 | 1112 | 346 | 235 | 0 | 279 | 873 | 716 | 609 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 32.5 | 37.9 | 26.2 | 41.4 | 47.9 | 0.0 | 46.8 | 0.0 | 55.5 | 49.0 | 32.0 | 31.8 |
| Incr Delay (d2), s/veh | 31.9 | 11.4 | 1.0 | 0.4 | 4.2 | 0.0 | 0.5 | 0.0 | 15.2 | 31.5 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 18.4 | 24.4 | 4.1 | 0.6 | 10.3 | 0.0 | 1.8 | 0.0 | 7.7 | 19.5 | 8.0 | 6.4 |
| LnGrp Delay(d),s/veh | 64.4 | 49.2 | 27.2 | 41.8 | 52.1 | 0.0 | 47.3 | 0.0 | 70.7 | 80.5 | 32.2 | 32.0 |
| LnGrp LOS | E | D | C | D | D | | D | | E | F | C | C |
| Approach Vol, veh/h | 2503 | | | | 895 | | | 249 | | | 1402 | |
| Approach Delay, s/veh | 50.3 | | | | 51.9 | | | 65.2 | | | 62.4 | |
| Approach LOS | D | | | | D | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 32.0 | 35.4 | 39.0 | 23.6 | 8.6 | 58.8 | 9.5 | 53.1 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 25.0 | 24.5 | 32.0 | 20.5 | 3.0 | 46.5 | 5.0 | 50.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 25.2 | 23.1 | 34.0 | 15.7 | 3.1 | 49.7 | 5.7 | 17.4 | | | | |
| Green Ext Time (p_c), s | 0.0 | 1.2 | 0.0 | 0.8 | 0.0 | 0.0 | 0.0 | 1.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 54.7 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 3B
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|-------|-------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 437 | 1773 | 150 | 18 | 805 | 788 | 53 | 145 | 53 | 1054 | 151 | 392 |
| Future Volume (veh/h) | 437 | 1773 | 150 | 18 | 805 | 788 | 53 | 145 | 53 | 1054 | 151 | 392 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 475 | 1927 | 163 | 20 | 875 | 0 | 58 | 158 | 58 | 1146 | 360 | 295 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 3 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 502 | 2348 | 731 | 99 | 1300 | 405 | 186 | 108 | 40 | 1295 | 567 | 482 |
| Arrive On Green | 0.22 | 0.46 | 0.46 | 0.01 | 0.26 | 0.00 | 0.04 | 0.08 | 0.08 | 0.24 | 0.30 | 0.30 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1301 | 478 | 5322 | 1863 | 1583 |
| Grp Volume(v), veh/h | 475 | 1927 | 163 | 20 | 875 | 0 | 58 | 0 | 216 | 1146 | 360 | 295 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1778 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 27.6 | 46.0 | 8.6 | 1.2 | 21.7 | 0.0 | 4.2 | 0.0 | 11.6 | 29.1 | 23.3 | 22.3 |
| Cycle Q Clear(g_c), s | 27.6 | 46.0 | 8.6 | 1.2 | 21.7 | 0.0 | 4.2 | 0.0 | 11.6 | 29.1 | 23.3 | 22.3 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.27 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 502 | 2348 | 731 | 99 | 1300 | 405 | 186 | 0 | 147 | 1295 | 567 | 482 |
| V/C Ratio(X) | 0.95 | 0.82 | 0.22 | 0.20 | 0.67 | 0.00 | 0.31 | 0.00 | 1.47 | 0.89 | 0.63 | 0.61 |
| Avail Cap(c_a), veh/h | 673 | 2348 | 731 | 116 | 1300 | 405 | 211 | 0 | 147 | 1559 | 633 | 538 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 31.9 | 32.7 | 22.6 | 39.1 | 46.9 | 0.0 | 55.7 | 0.0 | 64.2 | 51.1 | 42.0 | 41.6 |
| Incr Delay (d2), s/veh | 16.9 | 3.4 | 0.7 | 0.3 | 2.1 | 0.0 | 0.9 | 0.0 | 242.8 | 5.0 | 1.1 | 1.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 20.3 | 22.1 | 3.9 | 0.6 | 10.4 | 0.0 | 2.1 | 0.0 | 15.6 | 14.8 | 12.2 | 9.9 |
| LnGrp Delay(d),s/veh | 48.8 | 36.0 | 23.3 | 39.4 | 48.9 | 0.0 | 56.7 | 0.0 | 307.0 | 56.1 | 43.1 | 42.6 |
| LnGrp LOS | D | D | C | D | D | | E | | F | E | D | D |
| Approach Vol, veh/h | | 2565 | | | 895 | | | 274 | | | 1801 | |
| Approach Delay, s/veh | | 37.6 | | | 48.7 | | | 254.0 | | | 51.3 | |
| Approach LOS | | D | | | D | | | F | | | D | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 37.6 | 42.8 | 41.1 | 18.6 | 8.7 | 71.6 | 10.0 | 49.6 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 44.0 | 15.4 | 41.0 | 11.6 | 3.0 | 56.4 | 7.5 | 47.6 | | | | |
| Max Q Clear Time (g_c+l1), s | 29.6 | 23.7 | 31.1 | 13.6 | 3.2 | 48.0 | 6.2 | 25.3 | | | | |
| Green Ext Time (p_c), s | 1.0 | 0.0 | 3.0 | 0.0 | 0.0 | 6.0 | 0.0 | 1.8 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 54.6 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 3C
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 308 | 1773 | 150 | 18 | 805 | 380 | 53 | 93 | 53 | 502 | 81 | 218 |
| Future Volume (veh/h) | 308 | 1773 | 150 | 18 | 805 | 380 | 53 | 93 | 53 | 502 | 81 | 218 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 335 | 1927 | 163 | 20 | 875 | 0 | 58 | 101 | 58 | 546 | 200 | 162 |
| Adj No. of Lanes | 1 | 2 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 498 | 1859 | 832 | 68 | 2105 | 655 | 217 | 120 | 69 | 598 | 484 | 412 |
| Arrive On Green | 0.12 | 0.53 | 0.53 | 0.02 | 0.83 | 0.00 | 0.03 | 0.11 | 0.11 | 0.17 | 0.26 | 0.26 |
| Sat Flow, veh/h | 1774 | 3539 | 1583 | 1774 | 5085 | 1583 | 1774 | 1112 | 638 | 3548 | 1863 | 1583 |
| Grp Volume(v), veh/h | 335 | 1927 | 163 | 20 | 875 | 0 | 58 | 0 | 159 | 546 | 200 | 162 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1750 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 15.7 | 78.8 | 8.2 | 1.0 | 6.8 | 0.0 | 4.4 | 0.0 | 13.4 | 22.7 | 13.4 | 12.7 |
| Cycle Q Clear(g_c), s | 15.7 | 78.8 | 8.2 | 1.0 | 6.8 | 0.0 | 4.4 | 0.0 | 13.4 | 22.7 | 13.4 | 12.7 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.36 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 498 | 1859 | 832 | 68 | 2105 | 655 | 217 | 0 | 189 | 598 | 484 | 412 |
| V/C Ratio(X) | 0.67 | 1.04 | 0.20 | 0.29 | 0.42 | 0.00 | 0.27 | 0.00 | 0.84 | 0.91 | 0.41 | 0.39 |
| Avail Cap(c_a), veh/h | 884 | 1859 | 832 | 83 | 2105 | 655 | 217 | 0 | 286 | 662 | 621 | 528 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 19.3 | 35.6 | 18.8 | 37.5 | 8.2 | 0.0 | 57.2 | 0.0 | 65.6 | 61.3 | 46.0 | 45.8 |
| Incr Delay (d2), s/veh | 0.6 | 31.0 | 0.5 | 0.6 | 0.4 | 0.0 | 0.7 | 0.0 | 8.3 | 15.3 | 0.2 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 7.7 | 46.2 | 3.7 | 0.5 | 3.2 | 0.0 | 2.2 | 0.0 | 6.9 | 12.4 | 6.9 | 5.6 |
| LnGrp Delay(d),s/veh | 19.9 | 66.6 | 19.4 | 38.1 | 8.6 | 0.0 | 57.8 | 0.0 | 73.9 | 76.5 | 46.2 | 46.0 |
| LnGrp LOS | B | F | B | D | A | | E | | E | E | D | D |
| Approach Vol, veh/h | | 2425 | | | 895 | | | 217 | | | 908 | |
| Approach Delay, s/veh | | 56.9 | | | 9.3 | | | 69.6 | | | 64.4 | |
| Approach LOS | | E | | | A | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 25.4 | 69.1 | 32.3 | 23.2 | 8.7 | 85.8 | 9.5 | 46.0 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 51.0 | 18.5 | 28.0 | 24.5 | 3.0 | 66.5 | 5.0 | 50.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 17.7 | 8.8 | 24.7 | 15.4 | 3.0 | 80.8 | 6.4 | 15.4 | | | | |
| Green Ext Time (p_c), s | 0.7 | 6.8 | 0.6 | 0.8 | 0.0 | 0.0 | 0.0 | 1.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 49.5 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 4A
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 265 | 1596 | 150 | 18 | 724 | 736 | 53 | 111 | 53 | 984 | 104 | 159 |
| Future Volume (veh/h) | 265 | 1596 | 150 | 18 | 724 | 736 | 53 | 111 | 53 | 984 | 104 | 159 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 288 | 1735 | 163 | 20 | 787 | 0 | 58 | 121 | 58 | 1070 | 158 | 143 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 365 | 1883 | 586 | 84 | 1263 | 393 | 246 | 140 | 67 | 1064 | 739 | 629 |
| Arrive On Green | 0.13 | 0.37 | 0.37 | 0.01 | 0.25 | 0.00 | 0.04 | 0.12 | 0.12 | 0.30 | 0.40 | 0.40 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1191 | 571 | 3548 | 1863 | 1583 |
| Grp Volume(v), veh/h | 288 | 1735 | 163 | 20 | 787 | 0 | 58 | 0 | 179 | 1070 | 158 | 143 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1762 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 16.4 | 45.7 | 10.1 | 1.2 | 19.3 | 0.0 | 4.0 | 0.0 | 14.0 | 42.0 | 7.8 | 8.4 |
| Cycle Q Clear(g_c), s | 16.4 | 45.7 | 10.1 | 1.2 | 19.3 | 0.0 | 4.0 | 0.0 | 14.0 | 42.0 | 7.8 | 8.4 |
| Prop In Lane | 1.00 | | | 1.00 | | 1.00 | 1.00 | | 0.32 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 365 | 1883 | 586 | 84 | 1263 | 393 | 246 | 0 | 207 | 1064 | 739 | 629 |
| V/C Ratio(X) | 0.79 | 0.92 | 0.28 | 0.24 | 0.62 | 0.00 | 0.24 | 0.00 | 0.87 | 1.01 | 0.21 | 0.23 |
| Avail Cap(c_a), veh/h | 482 | 1883 | 586 | 100 | 1263 | 393 | 247 | 0 | 252 | 1064 | 785 | 667 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 33.2 | 42.1 | 30.9 | 41.9 | 46.8 | 0.0 | 51.6 | 0.0 | 60.7 | 49.0 | 27.8 | 28.0 |
| Incr Delay (d2), s/veh | 4.5 | 8.9 | 1.2 | 0.4 | 1.7 | 0.0 | 0.5 | 0.0 | 19.7 | 28.9 | 0.1 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 8.5 | 22.9 | 4.6 | 0.6 | 9.2 | 0.0 | 2.0 | 0.0 | 7.9 | 24.8 | 4.0 | 3.7 |
| LnGrp Delay(d),s/veh | 37.7 | 51.1 | 32.1 | 42.3 | 48.5 | 0.0 | 52.1 | 0.0 | 80.4 | 77.9 | 27.9 | 28.1 |
| LnGrp LOS | D | D | C | D | D | | D | | F | F | C | C |
| Approach Vol, veh/h | | 2186 | | | 807 | | | 237 | | | 1371 | |
| Approach Delay, s/veh | | 47.9 | | | 48.3 | | | 73.5 | | | 66.9 | |
| Approach LOS | | D | | | D | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 25.8 | 41.8 | 49.0 | 23.4 | 8.7 | 58.8 | 9.9 | 62.6 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 28.0 | 22.0 | 42.0 | 20.0 | 3.0 | 47.0 | 5.5 | 59.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 18.4 | 21.3 | 44.0 | 16.0 | 3.2 | 47.7 | 6.0 | 10.4 | | | | |
| Green Ext Time (p_c), s | 0.4 | 0.6 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 1.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 55.0 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan St & Jefferson St/Spring St

River North-High-Level-Option 4B
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 285 | 1596 | 150 | 18 | 724 | 1028 | 53 | 135 | 53 | 1381 | 137 | 186 |
| Future Volume (veh/h) | 285 | 1596 | 150 | 18 | 724 | 1028 | 53 | 135 | 53 | 1381 | 137 | 186 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 310 | 1735 | 163 | 20 | 787 | 0 | 58 | 147 | 58 | 1501 | 189 | 176 |
| Adj No. of Lanes | 1 | 3 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 3 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 371 | 1806 | 562 | 82 | 1112 | 346 | 257 | 169 | 67 | 1515 | 742 | 631 |
| Arrive On Green | 0.15 | 0.36 | 0.36 | 0.01 | 0.22 | 0.00 | 0.04 | 0.13 | 0.13 | 0.28 | 0.40 | 0.40 |
| Sat Flow, veh/h | 1774 | 5085 | 1583 | 1774 | 5085 | 1583 | 1774 | 1272 | 502 | 5322 | 1863 | 1583 |
| Grp Volume(v), veh/h | 310 | 1735 | 163 | 20 | 787 | 0 | 58 | 0 | 205 | 1501 | 189 | 176 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1695 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1774 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 17.0 | 43.4 | 9.6 | 1.1 | 18.6 | 0.0 | 3.6 | 0.0 | 14.7 | 36.5 | 8.8 | 9.8 |
| Cycle Q Clear(g_c), s | 17.0 | 43.4 | 9.6 | 1.1 | 18.6 | 0.0 | 3.6 | 0.0 | 14.7 | 36.5 | 8.8 | 9.8 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.28 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 371 | 1806 | 562 | 82 | 1112 | 346 | 257 | 0 | 235 | 1515 | 742 | 631 |
| V/C Ratio(X) | 0.84 | 0.96 | 0.29 | 0.24 | 0.71 | 0.00 | 0.23 | 0.00 | 0.87 | 0.99 | 0.25 | 0.28 |
| Avail Cap(c_a), veh/h | 448 | 1806 | 562 | 101 | 1112 | 346 | 263 | 0 | 273 | 1515 | 775 | 659 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 32.7 | 41.0 | 30.1 | 41.6 | 47.0 | 0.0 | 46.2 | 0.0 | 55.3 | 46.3 | 26.2 | 26.5 |
| Incr Delay (d2), s/veh | 9.4 | 13.8 | 1.3 | 0.6 | 3.8 | 0.0 | 0.4 | 0.0 | 20.8 | 20.9 | 0.1 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 9.2 | 22.5 | 4.4 | 0.6 | 9.1 | 0.0 | 1.8 | 0.0 | 8.6 | 20.9 | 4.6 | 4.3 |
| LnGrp Delay(d),s/veh | 42.2 | 54.8 | 31.4 | 42.2 | 50.8 | 0.0 | 46.7 | 0.0 | 76.1 | 67.2 | 26.3 | 26.6 |
| LnGrp LOS | D | D | C | D | D | | D | | E | E | C | C |
| Approach Vol, veh/h | 2208 | | | | 807 | | | 263 | | | 1866 | |
| Approach Delay, s/veh | 51.3 | | | | 50.6 | | | 69.6 | | | 59.2 | |
| Approach LOS | D | | | | D | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 26.4 | 35.4 | 44.0 | 24.2 | 8.6 | 53.2 | 9.4 | 58.8 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 25.0 | 20.0 | 37.0 | 20.0 | 3.0 | 42.0 | 5.4 | 54.1 | | | | |
| Max Q Clear Time (g_c+l1), s | 19.0 | 20.6 | 38.5 | 16.7 | 3.1 | 45.4 | 5.6 | 11.8 | | | | |
| Green Ext Time (p_c), s | 0.4 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 | 0.0 | 1.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 55.0 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

HCM 2010 Signalized Intersection Summary
1: Cowan Street & Jefferson Street/Spring Street

River North-High-Level-Option 4C
Projected PM

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|---------------------------------------|------|------|------|------|------|------|------|------|------|------|------|------|
| Lane Configurations | ↑ | ↑↑ | ↑ | ↑ | ↑↑↑ | ↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ |
| Traffic Volume (veh/h) | 248 | 1596 | 150 | 18 | 724 | 485 | 53 | 90 | 53 | 644 | 76 | 136 |
| Future Volume (veh/h) | 248 | 1596 | 150 | 18 | 724 | 485 | 53 | 90 | 53 | 644 | 76 | 136 |
| Number | 1 | 6 | 16 | 5 | 2 | 12 | 7 | 4 | 14 | 3 | 8 | 18 |
| Initial Q (Q _b), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1863 | 1900 | 1863 | 1863 | 1863 |
| Adj Flow Rate, veh/h | 270 | 1735 | 163 | 20 | 787 | 0 | 58 | 98 | 58 | 700 | 132 | 116 |
| Adj No. of Lanes | 1 | 2 | 1 | 1 | 3 | 1 | 1 | 1 | 0 | 2 | 1 | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 428 | 1729 | 773 | 68 | 2011 | 626 | 225 | 114 | 68 | 743 | 553 | 470 |
| Arrive On Green | 0.10 | 0.49 | 0.49 | 0.01 | 0.40 | 0.00 | 0.03 | 0.10 | 0.10 | 0.21 | 0.30 | 0.30 |
| Sat Flow, veh/h | 1774 | 3539 | 1583 | 1774 | 5085 | 1583 | 1774 | 1098 | 650 | 3548 | 1863 | 1583 |
| Grp Volume(v), veh/h | 270 | 1735 | 163 | 20 | 787 | 0 | 58 | 0 | 156 | 700 | 132 | 116 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 1583 | 1774 | 1695 | 1583 | 1774 | 0 | 1748 | 1774 | 1863 | 1583 |
| Q Serve(g_s), s | 13.1 | 73.3 | 8.8 | 1.0 | 16.6 | 0.0 | 4.4 | 0.0 | 13.2 | 29.1 | 8.0 | 8.3 |
| Cycle Q Clear(g_c), s | 13.1 | 73.3 | 8.8 | 1.0 | 16.6 | 0.0 | 4.4 | 0.0 | 13.2 | 29.1 | 8.0 | 8.3 |
| Prop In Lane | 1.00 | | | 1.00 | 1.00 | | 1.00 | 1.00 | | 0.37 | 1.00 | 1.00 |
| Lane Grp Cap(c), veh/h | 428 | 1729 | 773 | 68 | 2011 | 626 | 225 | 0 | 182 | 743 | 553 | 470 |
| V/C Ratio(X) | 0.63 | 1.00 | 0.21 | 0.29 | 0.39 | 0.00 | 0.26 | 0.00 | 0.86 | 0.94 | 0.24 | 0.25 |
| Avail Cap(c_a), veh/h | 728 | 1729 | 773 | 83 | 2011 | 626 | 225 | 0 | 239 | 757 | 621 | 528 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 0.73 | 0.73 | 0.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 22.9 | 38.4 | 21.9 | 38.4 | 32.4 | 0.0 | 57.7 | 0.0 | 66.1 | 58.4 | 39.9 | 40.0 |
| Incr Delay (d2), s/veh | 0.6 | 22.5 | 0.6 | 0.6 | 0.4 | 0.0 | 0.6 | 0.0 | 16.9 | 19.5 | 0.1 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 6.4 | 41.2 | 4.0 | 0.5 | 7.9 | 0.0 | 2.2 | 0.0 | 7.2 | 16.3 | 4.2 | 3.7 |
| LnGrp Delay(d),s/veh | 23.4 | 60.9 | 22.5 | 39.1 | 32.8 | 0.0 | 58.3 | 0.0 | 83.0 | 77.9 | 40.0 | 40.1 |
| LnGrp LOS | C | F | C | D | C | | E | | F | E | D | D |
| Approach Vol, veh/h | 2168 | | | | 807 | | | | 214 | | | 948 |
| Approach Delay, s/veh | 53.3 | | | | 33.0 | | | | 76.3 | | | 68.0 |
| Approach LOS | D | | | | C | | | E | | | E | |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+R _c), s | 22.7 | 66.3 | 38.4 | 22.6 | 8.7 | 80.3 | 9.5 | 51.5 | | | | |
| Change Period (Y+R _c), s | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 4.5 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 41.0 | 28.5 | 32.0 | 20.5 | 3.0 | 66.5 | 5.0 | 50.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 15.1 | 18.6 | 31.1 | 15.2 | 3.0 | 75.3 | 6.4 | 10.3 | | | | |
| Green Ext Time (p_c), s | 0.5 | 6.2 | 0.3 | 0.5 | 0.0 | 0.0 | 0.0 | 0.8 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2010 Ctrl Delay | | | | 53.9 | | | | | | | | |
| HCM 2010 LOS | | | | D | | | | | | | | |
| Notes | | | | | | | | | | | | |

APPENDIX E
TRIP GENERATION CALCULATIONS

TRIP GENERATION

River North Mixed-Use Development-Phase 1 Evaluation

Office – 3,029,000 square feet

Use ITE Land Use Code 710 and associated trip generation rates for 24-hour total trips and peak hour trips.

Average Daily Traffic – Use Average Rate for Average Daily Traffic on a Weekday

$$\text{LN } (T) = 0.76 \text{ LN } (X/1000) + 3.68$$

$$\text{LN } (T) = 0.76 \text{ LN } (3,029) + 3.68$$

$$T = 17,538$$

A.M. Peak Hour - Use Average Rate for AM Peak Hour of the Adjacent Street (between 7:00 AM and 9:00 AM)

$$\text{LN } (T) = 0.8 \text{ LN } (X/1000) + 1.57$$

$$\text{LN } (T) = 0.8 \text{ LN } (3,029) + 1.57$$

$$T = 2,930$$

$$\text{Enter} = 0.88 (2,930) = 2,578$$

$$\text{Exit} = 0.12 (2,930) = 352$$

P.M. Peak Hour - Use Average Rate for PM Peak Hour of the Adjacent Street (between 4:00 PM and 6:00 PM)

$$T = 1.12 (X/1000) + 78.45$$

$$T = 1.12 (3,029) + 78.45$$

$$T = 3,471$$

$$\text{Enter} = 0.17 (3,471) = 590$$

$$\text{Exit} = 0.83 (3,471) = 2,881$$

TRIP GENERATION

River North Mixed-Use Development – Phase 1 Evaluation

Apartment – 1,735 Units

Use ITE Land Use Code 220 and associated trip generation rates for 24-hour total trips and peak hour trips.

Average Daily Traffic – Use the Fitted Curve Equation for Average Daily Traffic on a Weekday

$$T = 6.06 (X) + 123.56$$

$$T = 6.06 (1,735) + 123.56$$

$$T = 10,638$$

A.M. Peak Hour - Use the Fitted Curve Equation for the AM Peak Hour of the Adjacent Street Traffic (one hour between 7:00 AM and 9:00 AM) on a Weekday

$$T = 0.49 (X) + 3.73$$

$$T = 0.49 (1,735) + 3.73$$

$$T = 854$$

$$\text{Enter} = 0.20 (854) = 171$$

$$\text{Exit} = 0.80 (854) = 683$$

P.M. Peak Hour - Use the Fitted Curve Equation for the PM Peak Hour of the Adjacent Street Traffic (one hour between 4:00 PM and 6:00 PM) on a Weekday

$$T = 0.55 (X) + 17.65$$

$$T = 0.55 (1,735) + 17.65$$

$$T = 972$$

$$\text{Enter} = 0.65 (972) = 632$$

$$\text{Exit} = 0.35 (972) = 340$$

TRIP GENERATION

River North Mixed-Use Development – Phase 1 Evaluation

Hotel – 550 Rooms

Use ITE Land Use Code 310 and associated trip generation rates for 24-hour total trips and peak hour trips.

Average Daily Traffic – Use the Fitted Curve Equation for Average Daily Traffic on a Weekday

$$T = 8.95 (X) - 373.16$$

$$T = 8.95 (550) - 373.16$$

$$T = 4,549$$

A.M. Peak Hour - Use the Fitted Curve Equation for the AM Peak Hour of the Adjacent Street Traffic (one hour between 7:00 AM and 9:00 AM) on a Weekday

$$T = 0.53 (X)$$

$$T = 0.53 (550)$$

$$T = 292$$

$$\text{Enter} = 0.59 (292) = 172$$

$$\text{Exit} = 0.41 (292) = 120$$

P.M. Peak Hour - Use the Fitted Curve Equation for the PM Peak Hour of the Adjacent Street Traffic (one hour between 4:00 PM and 6:00 PM) on a Weekday

$$T = 0.60 (X)$$

$$T = 0.60 (550)$$

$$T = 330$$

$$\text{Enter} = 0.51 (330) = 168$$

$$\text{Exit} = 0.49 (330) = 162$$

TRIP GENERATION

River North Mixed-Use Development – Phase 1 Evaluation

Specialty Retail – 200,000 square feet

Use ITE Land Use Code 826 and associated trip generation rates for 24-hour total trips and peak hour trips.

Average Daily Traffic

$$T = 42.78 (X/1000) + 37.66$$

$$T = 42.78 (200) + 37.66$$

$$T = 8,594$$

AM Peak Hour – None in the Trip Gen Manual- Assumed 50% of the PM Peak Hour.

PM Peak Hour - Use PM Peak Hour of the Adjacent Street (between 4:00 and 6:00 PM)

$$T = 2.40(X/1000) + 21.48$$

$$T = 2.40(200) + 21.48$$

$$T = 501$$

$$\text{Enter} = 0.44 (501) = 221$$

$$\text{Exit} = 0.56 (501) = 281$$

TRIP GENERATION

River North Mixed-Use Development – Phase 1 Evaluation

Quality Restaurant – 27,840 square feet

Use ITE Land Use Code 931 and associated trip generation rates for 24-hour total trips and peak hour trips.

Average Daily Traffic

$$T = 89.95 (X/1000)$$

$$T = 89.95 (27.840)$$

$$T = 2,504$$

A.M. Peak Hour - Use average rate for the AM Peak Hour of the Adjacent Street (between 7:00 AM and 9:00 AM). Directional Distribution not provided, use AM Peak Hour of Generator distribution.

$$T = 0.81 (X/1000)$$

$$T = 0.81 (27.840)$$

$$T = 23$$

$$\text{Enter} = 0.82 (23) = 18$$

$$\text{Exit} = 0.18 (23) = 5$$

P.M. Peak Hour - Use average rate for the PM Peak Hour of the Adjacent Street (between 4:00 PM and 6:00 PM)

$$T = 7.49 (X/1000)$$

$$T = 7.49 (27.840)$$

$$T = 209$$

$$\text{Enter} = 0.67 (209) = 140$$

$$\text{Exit} = 0.33 (209) = 69$$

TRIP GENERATION

River North Mixed-Use Development – Phase 1 Evaluation

High Turnover Restaurant – 27,840 square feet

Use ITE Land Use Code 932 and associated trip generation rates for 24-hour total trips and peak hour trips.

Average Daily Traffic

$$T = 127.15 \text{ (X/1000)}$$

$$T = 127.15 (27.840)$$

$$T = 3,540$$

A.M. Peak Hour - Use average rate for the AM Peak Hour of the Adjacent Street (between 7:00 AM and 9:00 AM). Directional Distribution not provided, use AM Peak Hour of Generator distribution.

$$T = 10.81 \text{ (X/1000)}$$

$$T = 10.81 (27.840)$$

$$T = 301$$

$$\text{Enter} = 0.55 (301) = 166$$

$$\text{Exit} = 0.45 (301) = 135$$

P.M. Peak Hour - Use average rate for the PM Peak Hour of the Adjacent Street (between 4:00 PM and 6:00 PM)

$$T = 9.85 \text{ (X/1000)}$$

$$T = 9.85 (27.840)$$

$$T = 274$$

$$\text{Enter} = 0.60 (274) = 164$$

$$\text{Exit} = 0.40 (274) = 110$$

TRIP GENERATION

River North Mixed-Use Development – Phase 1 Evaluation

Coffee/Donut Shop without Drive-Through Window – 2,320 square feet

Use ITE Land Use Code 936 and associated trip generation rates peak hour trips.

Average Daily Traffic – Assume AM peak hour trips account for 20% of average daily traffic

T = 5 (AM Peak Hour)

T = 5 (251)

T = 1,257

A.M. Peak Hour – Use AM Peak Hour of the Adjacent Street (between 7:00 AM and 9:00 AM)

T = 108.38 (X/1000)

T = 108.38 (2.320)

T = 251

Enter = 0.51 (251) = 128

Exit = 0.49 (251) = 123

P.M. Peak Hour - Use PM Peak Hour of the Adjacent Street (between 4:00 PM and 6:00 PM)

T = 40.75 (X/1000)

T = 40.75 (2.320)

T = 95

Enter = 0.50 (95) = 47

Exit = 0.50 (95) = 47

NCHRP 684 Internal Trip Capture Estimator

| | | | |
|-----------------------|--------------|---------------|-----------------------|
| Project Name: | River North | Organization: | KCI Technologies, Inc |
| Project Location: | | Performed By: | |
| Scenario Description: | | Date: | |
| Analysis Year: | | Checked By: | |
| Analysis Period: | AM Peak Hour | Date: | |

Table 1-A: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate)

| Land Use | Development Data | | | Estimated Vehicle-Trips | | |
|----------------------|------------------|----------|-------|-------------------------|----------|---------|
| | ITE LUCs1 | Quantity | Units | Total | Entering | Exiting |
| Office | 710 | 0 | ksf | 2,930 | 2,578 | 352 |
| Retail | 826 | 0 | ksf | 251 | 110 | 140 |
| Restaurant | 932/931/ 936 | 0 | ksf | 575 | 312 | 263 |
| Cinema/Entertainment | 445 | 0 | seats | 0 | 0 | 0 |
| Residential | 220,230 | 0 | du | 854 | 171 | 683 |
| Hotel | 310 | 0 | rooms | 292 | 172 | 120 |
| All Other Uses | - | 0 | - | 0 | 0 | 0 |
| Total | - | - | - | 4,901 | 3,344 | 1,557 |

Table 2-A: Mode Split and Vehicle Occupancy Estimates

| Land Use | Entering Trips | | | Exiting Trips | | |
|----------------------|----------------|-----------|-----------------|---------------|-----------|-----------------|
| | Veh. Occ. | % Transit | % Non-Motorized | Veh. Occ. | % Transit | % Non-Motorized |
| Office | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Retail | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Restaurant | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Cinema/Entertainment | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Residential | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Hotel | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| All Other Uses2 | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Total | | | | | | |

Table 3-A: Average Land Use Interchange Distances (Feet Walking Distance)

| Origin (From) | Destination (To) | | | | | |
|----------------------|------------------|--------|------------|----------------------|-------------|-------|
| | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office | 0 | 500 | 500 | 500 | 500 | 500 |
| Retail | 500 | 0 | 500 | 500 | 500 | 500 |
| Restaurant | 500 | 500 | 0 | 500 | 500 | 500 |
| Cinema/Entertainment | 500 | 500 | 500 | 0 | 500 | 500 |
| Residential | 500 | 500 | 500 | 500 | 0 | 500 |
| Hotel | 500 | 500 | 500 | 500 | 500 | 0 |

Table 4-A: Internal Person-Trip Origin-Destination Matrix

| Origin (From) | Destination (To) | | | | | |
|----------------------|------------------|--------|------------|----------------------|-------------|-------|
| | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office | 35 | 72 | 0 | 0 | 0 | 0 |
| Retail | 41 | 18 | 0 | 3 | 0 | 0 |
| Restaurant | 81 | 9 | 0 | 9 | 7 | 0 |
| Cinema/Entertainment | 0 | 0 | 0 | 0 | 0 | 0 |
| Residential | 102 | 7 | 62 | 0 | 0 | 0 |
| Hotel | 77 | 4 | 11 | 0 | 0 | 0 |

Table 5-A: Computations Summary

| | Total | Entering | Exiting |
|-------------------------------|-------|----------|---------|
| All Person-Trips | 4,901 | 3,344 | 1,557 |
| Internal Trips | 1,076 | 538 | 538 |
| Internal Capture Percentage | 22.0% | 16.1% | 34.5% |
| External Vehicle-Trips3 | 3,825 | 2,806 | 1,019 |
| External Transit-Trips4 | 0 | 0 | 0 |
| External Non-motorized Trips4 | 0 | 0 | 0 |

Table 6-A: Internal Trip Capture Percentages by Land Use

| Land Use | Entering Trips | Exiting Trips |
|----------------------|----------------|---------------|
| Office | 11.7% | 30.4% |
| Retail | 49.9% | 44.2% |
| Restaurant | 52.2% | 40.4% |
| Cinema/Entertainment | #DIV/0! | #DIV/0! |
| Residential | 7.0% | 25.0% |
| Hotel | 4.1% | 77.0% |

1 Land Use Codes (LUCs) from Trip Generation Informational Report, ITE.

2 Total estimate for all other land uses at mixed-use development site-not subject to internal trip capture computations in this estimator.

3 Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-A

4 Person-trips

NCHRP 684 Internal Trip Capture Estimator

| | | | |
|-----------------------|--------------|---------------|-----------------------|
| Project Name: | | Organization: | KCI Technologies, Inc |
| Project Location: | | Performed By: | |
| Scenario Description: | | Date: | |
| Analysis Year: | | Checked By: | |
| Analysis Period: | PM Peak Hour | Date: | |

Table 1-P: Base Vehicle-Trip Generation Estimates (Single-Use Site Estimate)

| Land Use | Development Data | | | Estimated Vehicle-Trips | | |
|----------------------|------------------|----------|-------|-------------------------|----------|---------|
| | ITE LUCs1 | Quantity | Units | Total | Entering | Exiting |
| Office | 710 | 0 | ksf | 3,471 | 590 | 2,881 |
| Retail | 826 | 0 | ksf | 501 | 221 | 281 |
| Restaurant | 932/931/ 936 | 0 | ksf | 577 | 352 | 226 |
| Cinema/Entertainment | 445 | 0 | seats | 0 | 0 | 0 |
| Residential | 220,230 | 0 | du | 972 | 632 | 340 |
| Hotel | 310 | 0 | rooms | 330 | 168 | 162 |
| All Other Uses | - | 0 | - | 0 | 0 | 0 |
| Total | - | - | - | 5,852 | 1,962 | 3,889 |

Table 2-P: Mode Split and Vehicle Occupancy Estimates

| Land Use | Entering Trips | | | Exiting Trips | | |
|----------------------|----------------|-----------|-----------------|---------------|-----------|-----------------|
| | Veh. Occ. | % Transit | % Non-Motorized | Veh. Occ. | % Transit | % Non-Motorized |
| Office | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Retail | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Restaurant | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Cinema/Entertainment | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Residential | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Hotel | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| All Other Uses2 | 1.00 | 0% | 0% | 1.00 | 0% | 0% |
| Total | | | | | | |

Table 3-P: Average Land Use Interchange Distances (Feet Walking Distance)

| Origin (From) | Destination (To) | | | | | |
|----------------------|------------------|--------|------------|----------------------|-------------|-------|
| | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office | 0 | 500 | 500 | 500 | 500 | 500 |
| Retail | 500 | 0 | 500 | 500 | 500 | 500 |
| Restaurant | 500 | 500 | 0 | 500 | 500 | 500 |
| Cinema/Entertainment | 500 | 500 | 500 | 0 | 500 | 500 |
| Residential | 500 | 500 | 500 | 500 | 0 | 500 |
| Hotel | 500 | 500 | 500 | 500 | 500 | 0 |

Table 4-P: Internal Person-Trip Origin-Destination Matrix

| Origin (From) | Destination (To) | | | | | |
|----------------------|------------------|--------|------------|----------------------|-------------|-------|
| | Office | Retail | Restaurant | Cinema/Entertainment | Residential | Hotel |
| Office | | 18 | 7 | 0 | 95 | 0 |
| Retail | 6 | | 81 | 0 | 73 | 14 |
| Restaurant | 7 | 93 | | 0 | 41 | 16 |
| Cinema/Entertainment | 0 | 0 | 0 | | 0 | 0 |
| Residential | 14 | 22 | 49 | 0 | | 10 |
| Hotel | 0 | 4 | 18 | 0 | 0 | |

Table 5-P: Computations Summary

| | Total | Entering | Exiting |
|-------------------------------|-------|----------|---------|
| All Person-Trips | 5,852 | 1,962 | 3,889 |
| Internal Trips | 1,136 | 568 | 568 |
| Internal Capture Percentage | 19.4% | 28.9% | 14.6% |
| External Vehicle-Trips3 | 4,716 | 1,394 | 3,321 |
| External Transit-Trips4 | 0 | 0 | 0 |
| External Non-motorized Trips4 | 0 | 0 | 0 |

Table 6-P: Internal Trip Capture Percentages by Land Use

| Land Use | Entering Trips | Exiting Trips |
|----------------------|----------------|---------------|
| Office | 4.6% | 4.2% |
| Retail | 62.1% | 62.0% |
| Restaurant | 44.1% | 69.5% |
| Cinema/Entertainment | #DIV/0! | #DIV/0! |
| Residential | 33.1% | 27.9% |
| Hotel | 23.8% | 13.6% |

1 Land Use Codes (LUCs) from Trip Generation Informational Report, ITE.

2 Total estimate for all other land uses at mixed-use development site-not subject to internal trip capture computations in this estimator.

3 Vehicle-trips computed using the mode split and vehicle occupancy values provided in Table 2-P

4 Person-trips

TRIP GENERATION
TOTAL SITE-GENERATED TRAFFIC

| LAND USE | SIZE | DAILY TRAFFIC | GENERATED TRAFFIC | | | |
|------------------|----------------|---------------|-------------------|--------------|--------------|--------------|
| | | | AM PEAK HR. | | PM PEAK HR. | |
| | | | ENTER | EXIT | ENTER | EXIT |
| Office | 3,029,000 s.f. | 17,538 | 2,578 | 352 | 590 | 2,881 |
| Specialty Retail | 200,000 s.f. | 8,594 | 110 | 140 | 221 | 281 |
| Restaurant | 58,000 s.f. | 7,301 | 312 | 263 | 352 | 226 |
| Apartments | 1,735 d.u. | 10,638 | 171 | 683 | 632 | 340 |
| Hotel | 550 rooms | 4,549 | 172 | 120 | 168 | 162 |
| TOTAL | | 48,620 | 3,343 | 1,558 | 1,963 | 3,890 |

TRIP GENERATION
INTERNAL SITE-GENERATED TRAFFIC

Assumes: **20%** Internal (for daily traffic)

use internal capture spread sheet for AM and PM reduction factor

| LAND USE | SIZE | DAILY TRAFFIC | GENERATED TRAFFIC | | | |
|------------------|----------------|---------------|-------------------|------------|-------------|------------|
| | | | AM PEAK HR. | | PM PEAK HR. | |
| | | | ENTER | EXIT | ENTER | EXIT |
| Office | 3,029,000 s.f. | 3,508 | 301 | 107 | 27 | 120 |
| Specialty Retail | 200,000 s.f. | 1,719 | 55 | 62 | 137 | 174 |
| Restaurant | 58,000 s.f. | 1,460 | 163 | 106 | 155 | 157 |
| Apartments | 1,735 d.u. | 2,128 | 12 | 171 | 209 | 95 |
| Hotel | 550 rooms | 910 | 7 | 92 | 40 | 22 |
| TOTAL | | 9,725 | 538 | 538 | 568 | 568 |

TRIP GENERATION
EXTERNAL SITE-GENERATED TRAFFIC

Assumes: **20%** Internal (for daily traffic)

| LAND USE | SIZE | DAILY TRAFFIC | GENERATED TRAFFIC | | | |
|------------------|----------------|---------------|-------------------|--------------|--------------|--------------|
| | | | AM PEAK HR. | | PM PEAK HR. | |
| | | | ENTER | EXIT | ENTER | EXIT |
| Office | 3,029,000 s.f. | 14,030 | 2,277 | 245 | 563 | 2,761 |
| Specialty Retail | 200,000 s.f. | 6,875 | 55 | 78 | 84 | 107 |
| Restaurant | 58,000 s.f. | 5,841 | 149 | 157 | 197 | 69 |
| Apartments | 1,735 d.u. | 8,510 | 159 | 512 | 423 | 245 |
| Hotel | 550 rooms | 3,639 | 165 | 28 | 128 | 140 |
| TOTAL | | 38,895 | 2,805 | 1,020 | 1,395 | 3,322 |

| TRIP GENERATION ALTERNATE MODE SITE-GENERATED TRAFFIC | | | | | | | | |
|----------------------------------------------------------|----------------|------------------|-------------------|-----------|-------------|------------|------|--|
| LAND USE | SIZE | DAILY TRAFFIC | GENERATED TRAFFIC | | | | Use: | |
| | | | AM PEAK HR. | | PM PEAK HR. | | | |
| | | | ENTER | EXIT | ENTER | EXIT | | |
| Office | 3,029,000 s.f. | 702 | 114 | 12 | 28 | 138 | 5% | |
| Specialty Retail | 200,000 s.f. | 344 | 3 | 4 | 4 | 5 | 5% | |
| Restaurant | 58,000 s.f. | 292 | 7 | 8 | 10 | 3 | 5% | |
| Apartments | 1,735 d.u. | 426 | 8 | 26 | 21 | 12 | 5% | |
| Hotel | 550 rooms | 182 | 8 | 1 | 6 | 7 | 5% | |
| TOTAL | | 1,338 | 124 | 24 | 42 | 146 | | |

| TRIP GENERATION NEW SITE-GENERATED VEHICULAR TRAFFIC | | | | | | | | |
|---------------------------------------------------------|----------------|------------------|-------------------|------------|--------------|--------------|--|--|
| LAND USE | SIZE | DAILY TRAFFIC | GENERATED TRAFFIC | | | | | |
| | | | AM PEAK HR. | | PM PEAK HR. | | | |
| | | | ENTER | EXIT | ENTER | EXIT | | |
| Office | 3,029,000 s.f. | 13,328 | 2,163 | 233 | 535 | 2,623 | | |
| Specialty Retail | 200,000 s.f. | 6,531 | 52 | 74 | 80 | 102 | | |
| Restaurant | 58,000 s.f. | 5,549 | 142 | 149 | 187 | 66 | | |
| Apartments | 1,735 d.u. | 8,084 | 151 | 486 | 402 | 233 | | |
| Hotel | 550 rooms | 3,457 | 157 | 27 | 122 | 133 | | |
| TOTAL | | 36,949 | 2,665 | 969 | 1,326 | 3,157 | | |