

Given &
Find

8.10 A retaining wall with geotextile reinforcement is 6-m high. For the granular backfill, $\gamma_1 = 15.9 \text{ kN/m}^3$ and $\phi'_1 = 30^\circ$. For the geotextile, $T_{all} = 16 \text{ kN/m}$. For the design of the wall, determine S_v , L , and l_f . Use $FS_{(B)} = FS_{(P)} = 1.5$.

$$\begin{aligned} FS_b &:= 1.5 & \phi'_1 &:= 30\text{deg} = 0.524 & \gamma_1 &:= 15.9 \frac{\text{kN}}{\text{m}^3} & z &:= H = 1 \text{ H} \\ FS_p &:= 1.5 & H &:= 6\text{m} & \sigma'_o &:= \gamma_1 \cdot z = 1.59 \times 10^4 \text{ T}^2 \\ T_{all} &:= 16 \frac{\text{kN}}{\text{m}} \end{aligned}$$

METHOD 1. Calculate K_a
2. Determine S_v
3. Find L

$$K_a := \tan\left(45\text{deg} - \frac{\phi'_1}{2}\right)^2 = 0.333 \quad \sigma'_a := K_a \cdot \sigma'_o = 5.3 \times 10^3 \text{ T}^2 \quad \text{EQN 8.55}$$

friction angle at geotextile soil interface $\phi'_f := \frac{2}{3} \cdot \phi'_1 = 0.349$

$$RF_{id} := \frac{1.1 + 2.0}{2} = 1.55 \quad RF_{cr} := \frac{2 + 4}{2} = 3 \quad RF_{cbd} := \frac{1 + 1.15}{2} = 1.075$$

$$T_{ult} := T_{all} \cdot (RF_{id} \cdot RF_{cr} \cdot RF_{cbd}) = 7.998 \times 10^4 \frac{\text{kg}}{\text{s}^2} \quad \text{EQN 8.56}$$

$$S_v := \frac{T_{all}}{\sigma'_a \cdot FS_b} = 2.013 \frac{\text{A}^2 \cdot \text{s}^2}{\text{kg}} \quad S_v := \frac{1}{3} \text{ m} = 0.333 \text{ m} \quad \text{EQN 8.57}$$

Z trials: $z := 5\text{m}$ $z := 4\text{m}$ $z := 3\text{m}$ $z := 2\text{m}$ $z := 1\text{m}$ $z := .5\text{m}$ max when z small

$$L_r := \frac{H - z}{\tan\left(45\text{deg} + \frac{\phi'_1}{2}\right)} = 3.175 \text{ m} \quad \text{EQN 8.58}$$

$$L_e := \frac{S_v \cdot \sigma'_a \cdot FS_p}{2 \cdot \sigma'_o \cdot \tan(\phi'_f)} = 0.229 \text{ m} \quad \text{EQN 8.59}$$

$$L := L_r + L_e = 3.404 \text{ m} \quad L := 3.5 \text{ m}$$

use length of 3.5m

8.11 With the S_v , L , and l_f determined in Problem 8.10, check the overall stability (i.e., factor of safety against overturning, sliding, and bearing capacity failure) of the wall. For the *in situ* soil, $\gamma_2 = 16.8 \text{ kN/m}^3$, $\phi'_2 = 20^\circ$, and $c'_2 = 55 \text{ kN/m}^2$.

$$W_1 := H \cdot L \cdot \gamma_1 = 3.248 \times 10^5 \frac{\text{kg}}{\text{s}^2} \quad x_1 := \frac{L}{2} = 1.702 \text{ m} \quad c'_2 := 55 \frac{\text{kN}}{\text{m}^2} \quad \phi'_2 := 20\text{deg} \quad \gamma_2 := 16.8 \frac{\text{kN}}{\text{m}^3}$$

$$P_a := .5 \cdot \gamma_1 \cdot H^2 \cdot K_a = 9.54 \times 10^4 \frac{\text{kg}}{\text{s}^2}$$

$$FS_{\text{overturning}} := \frac{W_1 \cdot x_1}{P_a \cdot \frac{H}{3}} = 2.897 \quad \text{if}(FS_{\text{overturning}} > 3, \text{"OK"}, \text{"modify"}) = \text{"modify"} \quad \text{EQN 8.50}$$

$$FS_{\text{sliding}} := \frac{W_1 \cdot \tan(\phi'_f)}{P_a} = 1.239$$

if($FS_{\text{sliding}} > 1.5$, "OK" , "modify") = "modify"

EQN 8.51

$$N_c := 14.83 \quad N_q := 6.40 \quad N_\gamma := 5.39$$

table 3.3

$$q_u := c' \cdot N_c + .5 \cdot \gamma_2 \cdot x_1 \cdot N_\gamma = 8.927 \times 10^5 \text{ Pa}$$

$$\sigma'_{o'} := \gamma_1 \cdot H = 9.54 \times 10^4 \text{ Pa}$$

$$FS_{\text{bearing}} := \frac{q_u}{\sigma'_{o'}} = 9.358$$

if($FS_{\text{bearing}} > 3$, "OK!" , "N.G!") = "OK!"

EQN 8.54