

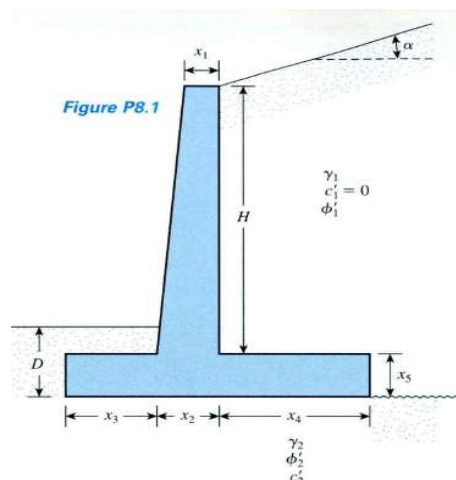
In Problems 8.1 through 8.4, use $\gamma_c := 23.58 \frac{\text{kN}}{\text{m}^3}$ $k_1 := \frac{2}{3}$ $k_2 := \frac{2}{3}$ $P_p := 0$

8.2 Repeat Problem 8.1 with the following:

Wall dimensions: $H = 6.5 \text{ m}$, $x_1 = 0.3 \text{ m}$, $x_2 = 0.6 \text{ m}$, $x_3 = 0.8 \text{ m}$, $x_4 = 2 \text{ m}$,
 $x_5 = 0.8 \text{ m}$, $D = 1.5 \text{ m}$, $\alpha = 0^\circ$

Soil properties: $\gamma_1 = 18.08 \text{ kN/m}^3$, $\phi'_1 = 36^\circ$, $\gamma_2 = 19.65 \text{ kN/m}^3$, $\phi'_2 = 15^\circ$, $c'_2 = 30 \text{ kN/m}^2$

Calculate the factor of safety with respect to overturning, sliding, and bearing capacity



Wall dimensions $H := 6.5 \text{ m}$ $x_1 := .3 \text{ m}$ $x_2 := .6 \text{ m}$ $x_3 := .8 \text{ m}$ $x_4 := 2 \text{ m}$ $x_5 := .8 \text{ m}$ $D := 1.5 \text{ m}$ $\alpha := 0 \text{ deg}$

Soil properties $\gamma_1 := 18.08 \frac{\text{kN}}{\text{m}^3}$ $\gamma_2 := 19.65 \frac{\text{kN}}{\text{m}^3}$ $\phi'_1 := 36 \text{ deg}$ $\phi'_2 := 15 \text{ deg}$ $c'_2 := 30 \frac{\text{kN}}{\text{m}^2}$ $B := x_3 + x_2 + x_4 = 3.4 \text{ m}$

METHOD A) OVERTURNING STABILITY:

- Determine the Rankine Active Force per unit length of Wall
 - Determine K_a (active earth pressure coefficient) and H'
- Determine the horizontal component and moment caused by that, which represent the overturning moment
- Determine the resisting forces and its corresponding moments
- Determine $F_{\text{Overturning}}$

B) SLIDING Sliding Factor of Safety can be calculated with EQ 8.11

C) BEARING CAPACITY FAILURE

- Determine eccentricity and maximum and minimum pressures (pressures at the toe and heel of wall)
 - Use Table 3.3 to determine Bearing Capacity Factors
 - Use Table 3.4 to determine Shape, Depth and Inclination Factors
 - Use Meyerhoff's Equation 3.19 to determine bearing capacity q_u

SOLUTION $H' := H + x_5 = 7.3 \text{ m}$ With $\phi'_1 := 36 \text{ deg}$ $\alpha := 0 \text{ deg}$ $K_a := 0.2596$ Table 7.1

$$P_a := .5 \cdot \gamma_1 \cdot H'^2 \cdot K_a = 1.251 \times 10^5 \frac{\text{kg}}{\text{s}^2} \quad P_a := 125 \frac{\text{kN}}{\text{m}}$$

Horizontal Component (Overturning Moment):

$$P_h := P_a \cdot \cos(\alpha) = 1.25 \times 10^5 \frac{\text{kg}}{\text{s}^2} \quad P_h := 125 \frac{\text{kN}}{\text{m}} \quad M_o := P_h \cdot \left(\frac{H'}{3} \right) = 3.042 \times 10^5 \text{ N}$$

Resisting Components:

$$P_v := P_a \cdot \sin(\alpha) = 0 \frac{\text{kg}}{\text{s}^2} \quad P_{av} := 0 \frac{\text{kN}}{\text{m}}$$

SEC	AREA (m^2)	W/unit length	M. Arm to C (m)	Moment kN-m/m
1	$A_1 := x_1 \cdot H = 1.95 \text{ m}^2$	$w_1 := \gamma_c \cdot A_1 = 4.598 \times 10^4 \frac{\text{kg}}{\text{s}^2}$	$B_1 := x_3 + x_2 - \frac{x_1}{2} = 1.25 \text{ m}$	$M_1 := w_1 \cdot B_1 = 5.748 \times 10^4 \text{ N}$
1	$A_2 := (x_2 - x_1) \cdot \frac{H}{2} = 0.975 \text{ m}^2$	$w_2 := \gamma_c \cdot A_2 = 2.299 \times 10^4 \frac{\text{kg}}{\text{s}^2}$	$B_2 := x_3 + \frac{2}{3} \left(x_2 - \frac{x_1}{2} \right) = 1.1 \text{ m}$	$M_2 := w_2 \cdot B_2 = 2.529 \times 10^4 \text{ N}$

$$\begin{aligned}
 1 \quad A3 &:= x5 \cdot B = 2.72 \text{ m}^2 & w3 &:= \gamma_c \cdot A3 = 6.414 \times 10^4 \frac{\text{kg}}{\text{s}^2} & B3 &:= \frac{B}{2} = 1.7 \text{ m} & M3 &:= w3 \cdot B3 = 1.09 \times 10^5 \text{ N} \\
 1 \quad A4 &:= x4 \cdot H = 13 \text{ m}^2 & w4 &:= \gamma_1 \cdot A4 = 2.35 \times 10^5 \frac{\text{kg}}{\text{s}^2} & B4 &:= B - \frac{x4}{2} = 2.4 \text{ m} & M4 &:= w4 \cdot B4 = 5.641 \times 10^5 \text{ N} \\
 \Sigma V &:= w1 + w2 + w3 + w4 = 3.681 \times 10^5 \frac{\text{kg}}{\text{s}^2} & \Sigma M_r &:= M1 + M2 + M3 + M4 = 7.559 \times 10^5 \text{ N} \\
 \text{FS}_{\text{overturning}} &:= \frac{\Sigma M_r}{M_o} = 2.485 & \text{if}(\text{FS}_{\text{overturning}} > 2, \text{"OK!"}, \text{"No Good"}) &= \text{"OK!"}
 \end{aligned}$$

Factor of Safety against Sliding

$$\text{EQ 8.11} \quad \text{FS}_{\text{sliding}} := \frac{(\Sigma V \cdot \tan(\phi'_1) + B \cdot c'_1 + P_p)}{P_a \cdot \cos(\alpha)} = 1.063 \quad \text{if}(\text{FS}_{\text{sliding}} > 1.5, \text{"okay"}, \text{"not good"}) = \text{"not good"}$$

FACTOR OF SAFETY AGAINST BEARING CAPACITY FAILURE

$$\text{EQ 8.16, 8.17 and 8.18} \quad e := \frac{B}{2} - \frac{(\Sigma M_r - M_o)}{\Sigma V} = 0.473 \text{ m} \quad \text{if}\left(e < \frac{B}{6}, \text{"okay"}, \text{"not good"}\right) = \text{"okay"}$$

$$\begin{aligned}
 q_{\text{toe}} &:= \frac{\Sigma V}{B} \cdot \left(1 + 6 \cdot \frac{e}{B}\right) = 1.987 \times 10^5 \text{ Pa} & q_{\text{heel}} &:= \frac{\Sigma V}{B} \cdot \left(1 - 6 \cdot \frac{e}{B}\right) = 1.79 \times 10^4 \text{ Pa} & B' &:= (B - 2e) = 2.454 \text{ m}
 \end{aligned}$$

Using Table 3.3 we have: $\phi'_2 := 15^\circ$ $N_c := 10.98$ $N_q := 3.94$ $N_\gamma := 2.65$

$$p := \frac{D}{B'} = 0.611 \quad F_{\gamma d} := 1 \quad F_{qd} := 1 + 2 \cdot \tan(\phi'_2) \cdot (1 - \sin(\phi'_2))^2 \cdot \left(\frac{D}{B'}\right) = 1.18 \quad F_{cd} := F_{qd} - \frac{(1 - F_{qd})}{N_c \cdot \tan(\phi'_2)} = 1.241$$

$$\psi := \text{atan}\left(\frac{P_a \cdot \cos(\alpha)}{\Sigma V}\right) = 0.327 \quad \psi := 18.736^\circ \quad F_{ci} := \left(1 - \frac{\psi}{90^\circ}\right)^2 = 0.627 \quad F_{qi} := F_{ci} = 0.627 \quad F_{\gamma i} := \left(1 - \frac{\psi}{\phi'_2}\right)^2 = 0.062$$

$$q := \gamma_2 \cdot D = 2.947 \times 10^4 \text{ Pa}$$

$$q_u := c'_2 \cdot N_c \cdot F_{cd} \cdot F_{ci} + q \cdot N_q \cdot F_{qd} \cdot F_{qi} + .5 \cdot \gamma_2 \cdot B' \cdot N_\gamma \cdot F_{\gamma d} \cdot F_{\gamma i} = 3.462 \times 10^5 \text{ Pa}$$

$$\text{FS}_{\text{bearing}} := \frac{q_u}{q_{\text{toe}}} = 1.743 \quad \text{if}(\text{FS}_{\text{bearing}} > 3, \text{"okay"}, \text{"not good"}) = \text{"not good"}$$

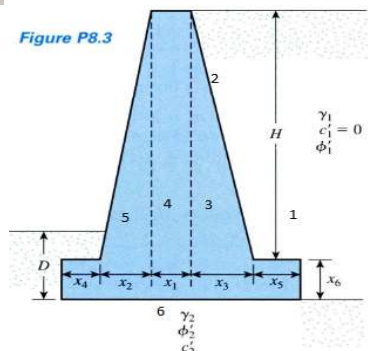
8.4 Repeat Problem 8.3 using Coulomb's active earth pressure in your calculation and letting $\delta' = 2/3 \phi'_1$.

8.3 A gravity retaining wall is shown in Figure P8.3. Calculate the factor of safety with respect to overturning and sliding, given the following data:

Wall dimensions: $H = 6 \text{ m}$, $x_1 = 0.6 \text{ m}$, $x_2 = 2 \text{ m}$, $x_3 = 2 \text{ m}$, $x_4 = 0.5 \text{ m}$, $x_5 = 0.75 \text{ m}$, $x_6 = 0.8 \text{ m}$, $D = 1.5 \text{ m}$

Soil properties: $\gamma_1 = 16.5 \text{ kN/m}^3$, $\phi'_1 = 32^\circ$, $\gamma_2 = 18 \text{ kN/m}^3$, $\phi'_2 = 22^\circ$, $c'_2 = 40 \text{ kN/m}^2$

Use the Rankine active earth pressure in your calculation.



$$\text{wall dimensions} \quad H := 6 \text{ m} \quad x_1 := .6 \text{ m} \quad x_2 := 2 \text{ m} \quad x_3 := 2 \text{ m} \quad x_4 := .5 \text{ m} \quad x_5 := .75 \text{ m} \quad x_6 := .8 \text{ m} \quad D := 1.5 \text{ m}$$

Soil properties $\gamma_1 := 16.5 \frac{\text{kN}}{\text{m}^3}$ $\gamma_2 := 18 \frac{\text{kN}}{\text{m}^3}$ $\phi_1' := 32\text{deg}$ $\phi_2' := 22\text{deg}$ $c_2' := 40 \frac{\text{kN}}{\text{m}^2}$ $B := x_4 + x_2 + x_1 + x_3 + x_5 = 5.85 \text{ m}$

METHOD A) OVERTURNING STABILITY:

$$\delta' := \frac{2}{3} \cdot \phi_1' = 0.372$$

1. Determine the Rankine Active Force per unit length of Wall
 - 1.1 Determine K_a (active earth pressure coefficient) and H'
2. Determine the horizontal component and moment caused by that, which represent the overturning moment
3. Determine the resisting forces and its corresponding moments
4. Determine $F_{\text{Soverturning}}$

B) SLIDING Sliding Factor of Safety can be calculated with EQ 8.11

C) BEARING CAPACITY FAILURE

0. Determine eccentricity and maximum and minimum pressures (pressures at the toe and heel of wall)
1. Use Table 3.3 to determine Bearing Capacity Factors
2. Use Table 3.4 to determine Shape, Depth and Inclination Factors
3. Use Meyerhoff's Equation 3.19 do determine bearing capacity q_u

SOLUTION $H' := H + x_5 = 6.75 \text{ m}$ $\beta := \text{atan}\left(\frac{H}{x_3}\right) \cdot \left(\frac{180}{\pi}\right) = 71.565$ $\beta := 71.566\text{deg}$ $K_a := .439$ K_a table 7.4

With $\phi_1' := 36\text{deg}$ $\alpha := 90 - \frac{\beta}{\text{deg}} + 21.333 = 39.767$ $\alpha := \alpha \cdot \text{deg} = 0.694$

$$P_a := .5 \cdot \gamma_1 \cdot H'^2 \cdot K_a = 1.65 \times 10^5 \frac{\text{kg}}{\text{s}^2}$$

$$P_a := 165 \frac{\text{kN}}{\text{m}}$$

Horizontal Component (Overturning Moment):

$$P_h := P_a \cdot \cos(\alpha) = 1.268 \times 10^5 \frac{\text{kg}}{\text{s}^2}$$

$$P_h := 126 \frac{\text{kN}}{\text{m}}$$

$$M_o := P_h \cdot \left(\frac{H'}{3}\right) = 2.835 \times 10^5 \text{ N}$$

Resisting Components:

$$P_v := P_a \cdot \sin(\alpha) = 1.055 \times 10^5 \frac{\text{kg}}{\text{s}^2}$$

$$P_v := 105 \frac{\text{kN}}{\text{m}}$$

SEC	AREA (m^2)	W/unit length	M. Arm to C (m)	Moment kN-m/m
3	$A_1 := x_3 \cdot \frac{H}{2} = 6 \text{ m}^2$	$w_1 := \gamma_c \cdot A_1 = 1.415 \times 10^5 \frac{\text{kg}}{\text{s}^2}$	$B_1 := B - (x_5 + x_3) + \frac{1 \cdot x_3}{3} = 3.767 \text{ m}$	$M_1 := w_1 \cdot B_1 = 5.329 \times 10^5 \text{ N}$
4	$A_2 := (x_1) \cdot H = 3.6 \text{ m}^2$	$w_2 := \gamma_c \cdot A_2 = 8.489 \times 10^4 \frac{\text{kg}}{\text{s}^2}$	$B_2 := B - \left(x_5 + x_3 + \frac{x_1}{2}\right) = 2.8 \text{ m}$	$M_2 := w_2 \cdot B_2 = 2.377 \times 10^5 \text{ N}$
5	$A_3 := x_2 \cdot H = 12 \text{ m}^2$	$w_3 := \gamma_c \cdot A_3 = 2.83 \times 10^5 \frac{\text{kg}}{\text{s}^2}$	$B_3 := x_4 + \frac{2 \cdot x_2}{3} = 1.833 \text{ m}$	$M_3 := w_3 \cdot B_3 = 5.188 \times 10^5 \text{ N}$
2	$A_4 := x_6 \cdot B = 4.68 \text{ m}^2$	$w_4 := \gamma_c \cdot A_4 = 1.104 \times 10^5 \frac{\text{kg}}{\text{s}^2}$	$B_4 := \frac{B}{2} = 2.925 \text{ m}$	$M_4 := w_4 \cdot B_4 = 3.228 \times 10^5 \text{ N}$

$$\Sigma V := w_1 + w_2 + w_3 + w_4 = 6.197 \times 10^5 \frac{\text{kg}}{\text{s}^2}$$

$$\Sigma M_r := M_1 + M_2 + M_3 + M_4 = 1.612 \times 10^6 \text{ N}$$

$$F_{\text{Soverturning}} := \frac{\Sigma M_r}{M_o} = 5.687$$

if ($F_{\text{Soverturning}} > 2$, "OK!" , "No Good") = "OK!"

Factor of Safety against Sliding

$$\text{EQ 8.11} \quad \text{FSsliding} := \frac{(\Sigma V \cdot \tan(k1 \cdot \phi'2) + B \cdot k2 \cdot c'2 + Pp)}{Pa \cdot \cos(\alpha)} = 2.509 \quad \text{if}(\text{FSsliding} > 1.5, \text{"okay"}, \text{"not good"}) = \text{"okay"}$$

FACTOR OF SAFETY AGAINST BEARING CAPACITY FAILURE

$$e := \frac{B}{2} - \frac{(\Sigma Mr - Mo)}{\Sigma V} = 0.781 \text{ m} \quad \text{EQ 8.16, 8.17 and 8.18} \quad \text{if}\left(e < \frac{B}{6}, \text{"okay"}, \text{"not good"}\right) = \text{"okay"}$$

$$q_{toe} := \frac{\Sigma V}{B} \cdot \left(1 + 6 \cdot \frac{e}{B}\right) = 1.908 \times 10^5 \text{ Pa} \quad q_{heel} := \frac{\Sigma V}{B} \cdot \left(1 - 6 \cdot \frac{e}{B}\right) = 2.108 \times 10^4 \text{ Pa} \quad B' := (B - 2e) = 4.288 \text{ m}$$

Using Table 3.3 we have: $N_q := 23.18$ $N_c := 35.49$ $N_\gamma := 30.22$

$$p := \frac{D}{B'} = 0.35 \quad F_{\gamma d} := 1 \quad F_{qd} := 1 + 2 \cdot \tan(\phi'2) \cdot (1 - \sin(\phi'2))^2 \cdot \left(\frac{D}{B'}\right) = 1.111 \quad F_{cd} := F_{qd} - \frac{(1 - F_{qd})}{N_c \cdot \tan(\phi'2)} = 1.118$$

$$\psi := \text{atan}\left(\frac{Pa \cdot \cos(\alpha)}{\Sigma V}\right) = 0.202 \quad \psi := 18.736 \text{ deg} \quad F_{ci} := \left(1 - \frac{\psi}{90 \cdot \text{deg}}\right)^2 = 0.627 \quad F_{qi} := F_{ci} = 0.627 \quad F_{\gamma i} := \left(1 - \frac{\psi}{\phi'2}\right)^2 = 0.022$$

$$q := \gamma_2 \cdot D = 2.7 \times 10^4 \text{ Pa}$$

$$q_u := c'2 \cdot N_c \cdot F_{cd} \cdot F_{ci} + q \cdot N_q \cdot F_{qd} \cdot F_{qi} + .5 \cdot \gamma_2 \cdot B' \cdot N_\gamma \cdot F_{\gamma d} \cdot F_{\gamma i} = 1.457 \times 10^6 \text{ Pa}$$

$$\text{FSbearing} := \frac{q_u}{q_{toe}} = 7.636 \quad \text{if}(\text{FSbearing} > 3, \text{"okay"}, \text{"not good"}) = \text{"okay"}$$

1